

Appendix G

List of Technical Studies

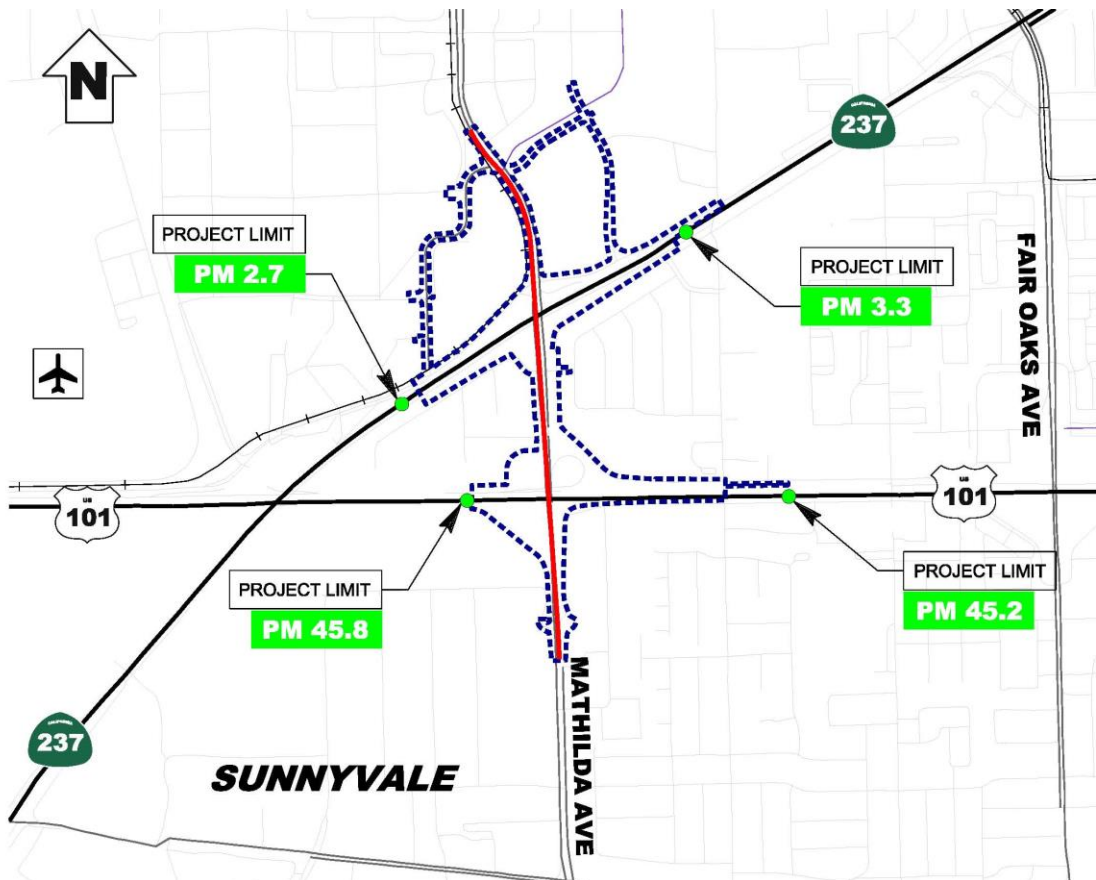
Appendix G List of Technical Studies

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|---|--|
| Air Quality Study Report | ICF International |
| Historic Resources Compliance Report/ Archaeological Survey Report | ICF International |
| Community Impact Assessment | ICF International |
| Initial Site Assessment | BASELINE Environmental Consulting |
| Natural Environment Study – Minimal Impacts Noise Study Report | ICF International |
| Paleontological Identification Report | ICF International |
| Preliminary Geological Assessment Summary of Floodplain Encroachment Traffic | BASELINE Environmental Consulting WRECO |
| Operations Assessment Report | Fehr and Peers |
| Visual Impact Assessment (Minor) | ICF International |
| Water Quality Assessment Report | WRECO |
| Wetland Assessment Technical Memorandum | ICF International |

Air Quality Study Report

for the

MATHILDA AVENUE IMPROVEMENTS AT SR 237 AND US 101 PROJECT



Prepared for:

Santa Clara Valley Transportation Authority
California Department of Transportation
District 4

Prepared by:

ICF International

Dated: May 2016

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Air Quality Study Report

for the

MATHILDA AVENUE IMPROVEMENTS AT SR 237 AND US 101 PROJECT

on Mathilda Avenue from Almanor Avenue to Innovation Way; on SR 237 from 0.3 mile south of US 101/SR 237 Junction to 0.3 mile east of Mathilda Avenue Undercrossing; and on US 101 from 0.3 mile south of Mathilda Avenue to SR 237/US 101/SR 237 Junction in the City of Sunnyvale, Santa Clara County

SCL-237-PM 2.7/3.3; SCL-101-PM 45.2/45.8
EA 04-4H2900/Project ID 0413000204

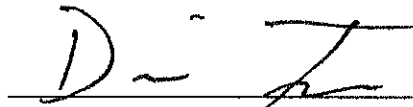
May 2016

U.S. DEPARTMENT OF TRANSPORTATION
STATE OF CALIFORNIA

and

Cooperating Agency: Santa Clara Valley Transportation Authority

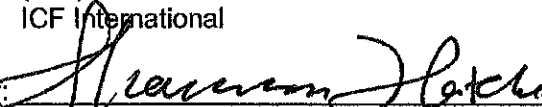
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Statement of Compliance: Produced in compliance with California Environmental Quality Act (CEQA) requirements, as appropriate, to meet the level of analysis and documentation that has been determined necessary for this project.

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List of Acronyms and Abbreviations

| | |
|----------------|---|
| AADT | annual average daily traffic |
| AB | Assembly Bill |
| ARB | California Air Resources Board |
| BAAQMD | Bay Area Air Quality Management District |
| BMP | best management practice |
| CAAQS | California Ambient Air Quality Standards |
| California CAA | California Clean Air Act |
| Caltrans | California Department of Transportation |
| CEQA | California Environmental Quality Act |
| CFR | Code of Federal Regulations |
| CH4 | methane |
| CO | carbon monoxide |
| EIR | Environmental Impact Report |
| EO | Executive Order |
| EPA | U.S Environmental Protection Agency |
| FCAA | Federal Clean Air Act |
| FHWA | Federal Highway Administration |
| FTIP | Federal Transportation Improvement Program |
| General Plan | City of Sunnyvale's General Plan |
| GHG | greenhouse gas |
| HOV | high-occupancy vehicle |
| H2S | hydrogen sulfide |
| I-880 | Interstate 880 |
| LOS | level of service |
| mph | miles per hour |
| MPO | Metropolitan Planning Organization |
| MSAT | mobile source air toxics |
| MTC | Metropolitan Transportation Commission |
| N2O | nitrous oxide |
| NAAQs | National Ambient Air Quality Standards |
| NEPA | National Environmental Policy Act |
| NO2 | nitrogen dioxide |
| NOX | oxides of nitrogen |
| O3 | ozone |
| Pb | lead |
| PG&E | Pacific Gas & Electric |
| PM | post mile or Particulate Matter (depending on context) |
| POAQC | Projects of Air Quality Concern |
| ppm | parts per million |
| Project | Mathilda Avenue Improvements at SR 237 and US 101 Project |
| ROG | reactive organic gases |
| RTP | Regional Transportation Plan |
| SB | Senate Bill |
| SCS | Sustainable Communities Strategy |
| SIP | State Implementation Plan |
| SO2 | sulfur dioxide |

SOX sulfur oxide
SR 237 State Route 237
US 101 U.S. Highway 101
VMT vehicle miles traveled
VTA Santa Clara Valley Transportation Authority

Chapter 1 – Executive Summary

1.1 Purpose of the Air Quality Study Report

This report was prepared for the Mathilda Avenue Improvements at SR 237 and US 101 Project. The California Department of Transportation (Caltrans), in cooperation with the Santa Clara Valley Transportation Authority (VTA) and the City of Sunnyvale, is proposing the “Mathilda Avenue Improvements at SR 237 and US 101 Project” (Project) to improve Mathilda Avenue in the City of Sunnyvale from Almanor Avenue/Ahwanee Avenue to Innovation Way, including on- and off-ramp improvements at the State Route (SR) 237/Mathilda Avenue and U.S. Highway 101 (US 101)/Mathilda Avenue interchanges. On SR 237, the Project limits are from 0.3 mile east of the US 101/SR 237 interchange (post mile [PM] 2.7) to 0.3 mile east of the Mathilda Avenue undercrossing (PM 3.3). On US 101, the Project limits are from 0.5 mile south of the Mathilda Avenue overcrossing (PM 45.2) to 0.3 mile south of the SR 237/US 101 interchange (PM 45.8). The total length of the Project on Mathilda Avenue is approximately one mile.

This report is intended to support the preparation of California Environmental Quality Act (CEQA) documentation for Caltrans. Caltrans is the CEQA lead agency for the Project. This report also supports efforts to obtain agreements, permits, and concurrence needed to construct the Project. This report evaluates the effects of the project on air quality resources and climate change, based on system-wide measures of effectiveness and intersection traffic volumes under existing (2013), opening year (2018), and design year (2040) conditions as reported in the *Traffic Analysis Operations Report: Mathilda Avenue Improvements between SR 237 and US 101 Project* (Fehr & Peers 2016a).

Three alternatives, including the No-Build Alternative, are analyzed in this document. The design features for the two Build Alternatives include reconfiguration of the US 101 and SR 237 interchanges with Mathilda Avenue. This includes modification to on- and off-ramps; removal, addition, and signalization of intersections; and provision of new left-turn lanes. In addition, the Build Alternatives would require modification to bicycle and pedestrian facilities, utilities, storm water treatment facilities, street lighting, ramp metering, signage, retaining walls, and light rail crossing facilities. The Project is found in the 2013 Regional Transportation Plan (RTP) titled *Plan Bay Area* (2040 RTP) (Metropolitan Transportation Commission 2014). Engineering for the Project is programmed in the Metropolitan Transportation Commission (MTC) financially constrained 2015 Transportation Improvement Program (TIP).

1.2 Scope and Content of the Report

This report describes the Project’s regulatory and environmental setting, the environmental consequences of the Project, and measures to avoid, minimize, or mitigate adverse impacts of the Project on air quality resources. This report is organized as described here.

- Chapter 1, *Introduction*, introduces the report and describes the purpose, scope, and content of the report, as well as provides a summary of the Project impacts; avoidance, minimization and/or mitigation measures; and significance conclusions that are discussed later in the report.
- Chapter 2, *Project Description*, describes the Project’s characteristics, including location, purpose, need, and the alternatives associated with the Project.

- Chapter 3, *Affected Environment, Environmental Consequences, and Avoidance, Minimization, and/or Mitigation Measures*, describes the regulatory and physical setting, discloses the environmental effects of the alternatives and the methods used to evaluate them, and identifies measures to avoid, minimize, and/or mitigate adverse effects associated with the alternatives.
- Chapter 4, *References Cited*, describes the printed references and personal communications used to prepare this report.

1.3 Summary

Table 1-1 provides a summary of the impacts, significance conclusions, and avoidance, minimization, and/or mitigation measures discussed in this report.

Table 1-1. Summary of Analysis, Conclusions, and Avoidance, Minimization, and/or Mitigation Measures Associated with the Project

| Analysis | Conclusions | Avoidance, Minimization, and/or Mitigation Measures |
|---|--|--|
| Conformity of the Regional Transportation Plan with the State Implementation Plan | The Project is listed in the conforming 2015 Transportation Improvement Program and the 2040 Regional Transportation Plan/Sustainable Communities Strategy. | None Required |
| Potential Violations of Carbon Monoxide (CO) California Ambient Air Quality Standards (CAAQS) | The Build Alternatives are not anticipated to exceed 1- or 8-hour CO CAAQS under 2018 or 2040 conditions. | None Required |
| Potential Violations of particulate matter (PM) 10 and PM2.5 CAAQS | Santa Clara County is currently classified as a nonattainment area with regards to the PM10 and PM2.5 CAAQS. However, due to no increase in truck percentages between the No Build and Build Alternatives, as well as a total decrease in delay during both AM and PM peak hours, the Project does not meet the criteria for how a Project of Air Quality Concern is defined under the FCAA. | None Required |
| Potential for Generation of Mobile Source Air Toxics (MSAT) Emissions | The Build Alternatives associated with this Project would result in a decrease in traffic volumes when compared to No Build conditions and would not result in increases in any MSAT emissions under either Build Alternative for 2018 or 2040 conditions when compared to the No Build Alternative. Thus based on Federal Highway Association's 2012 MSAT guidance, this Project is considered to have No Meaningful Potential MSAT Effects, and a quantitative analysis of MSAT emissions is not required. | None Required |

| Analysis | Conclusions | Avoidance, Minimization, and/or Mitigation Measures |
|--|---|---|
| Generation of Operation-Related Emissions of reactive organic gases (ROG), oxides of nitrogen (NO _x), CO, PM ₁₀ , and PM _{2.5} . | <p>Both Build Alternatives would result in decreases in ROG, NO_x, CO, PM₁₀, and PM_{2.5} between existing (2013) and opening (2018) year conditions.</p> <p>Both Build Alternatives would result in decreases in ROG, NO_x, CO, and PM_{2.5}, with an increase in PM₁₀ emissions, between existing (2013) and design (2040) year conditions.</p> <p>Compared to No Build conditions in 2018, Build Alternative 1 shows a decrease in all pollutants, except for no change in ROG emissions. Build Alternative 2 would result in a slight increase in ROG emissions, no change in PM_{2.5} emissions, and decreases in NO_x, CO, and PM₁₀ emissions.</p> <p>Compared to No Build conditions in 2040, Build Alternative 1 shows a decrease in all pollutants while Alternative 2 would result in a slight increase in NO_x emissions, no change in ROG emissions, and decreases in CO, PM₁₀, and PM_{2.5} emissions.</p> | None Required |
| Potential Temporary Increase in ROG, NO _x , CO, PM ₁₀ , and PM _{2.5} Emissions during Grading and Construction Activities | The Project would result in temporary increases in ROG, NO _x , CO, PM ₁₀ , and PM _{2.5} during construction. | Addressed by construction-related air pollution and dust control measures in Caltrans Standard Specifications Section 14 and BAAQMD Feasible Control Measures for Construction Emissions of Particulate Matter. |
| Potential for Generation of Greenhouse Gas (GHG) Emissions | The Project would result in minor increases in GHG emissions during construction but decreases in GHG emissions during long-term operation. Operational emissions decreases are a result of more fuel efficient vehicles in future years as well as an increase in VMT in more fuel efficient speed bins in future years as a result of the Project. | None Required |

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Chapter 2 – Project Description

2.1 Introduction

The California Department of Transportation (Caltrans), in cooperation with the Santa Clara Valley Transportation Authority (VTA) and the City of Sunnyvale (City), is proposing the “Mathilda Avenue Improvements at SR 237 and US 101 Project” (Project) to improve Mathilda Avenue in the City of Sunnyvale from Almanor Avenue/Ahwanee Avenue to Innovation Way, including on- and off-ramp improvements at the State Route (SR) 237/Mathilda Avenue and U.S. Highway 101 (US 101)/Mathilda Avenue interchanges. On SR 237, the Project limits are from 0.3 mile east of the US 101/SR 237 interchange (post mile [PM] 2.7) to 0.3 mile east of the Mathilda Avenue undercrossing (PM 3.3). On US 101, the Project limits are from 0.5 mile south of Mathilda Avenue overcrossing (PM 45.2) to 0.3 mile south of SR 237/US 101 interchange (PM 45.8). The total length of the Project on Mathilda Avenue is approximately 1 mile. **Figure 1** shows the location of the Project.

The Project is subject to state environmental review requirements and is being prepared in compliance with the California Environmental Quality Act (CEQA). Caltrans is the lead agency under CEQA. The Project is included in the 2015 Federal Statewide Transportation Improvement Program (ID No. SCL130001). The Project is included in the Metropolitan Transportation Commission (MTC) *Plan Bay Area*, adopted July 18, 2013 (Project No. 240554). The Project is also identified in the VTA’s Valley Transportation Plan 2040 under ID H43 and in the City of Sunnyvale’s Capital Improvement Program for Fiscal Year 2013/2014 as Project No. 826890.

The City has committed local funding to the development of the Project. Other funding sources have yet to be determined, but may include a combination of state and/or local transportation funds.

2.2 Project Background

The State Route 237/Mathilda Avenue and US 101/Mathilda Avenue interchanges are primary access points on the state highway system for the City of Sunnyvale and important local destinations, such as downtown Sunnyvale, the Sunnyvale Caltrain station to the south, and an expanding high-tech business district to the north. The Project is also located within the “Golden Triangle,” an area bordered by US 101, SR 237, and Interstate 880 (I-880) that includes parts of Sunnyvale, Santa Clara, North San Jose, and Milpitas. The Golden Triangle is named for the high concentration of employment centers within this area. US 101, SR 237, and I-880 are heavily used commute corridors to destinations within and beyond the Golden Triangle.

2.2.1 Mathilda Avenue

Within the Project area, Mathilda Avenue is a six-lane divided local roadway. Mathilda Avenue serves as the main access route to residential communities on the east side of Mathilda Avenue and is the only access route to the landlocked area within the US 101/SR 237/Mathilda Avenue triangle via Ross Drive. Mathilda Avenue is also one of City of Sunnyvale’s designated truck routes for trucks that weigh more than 3 tons. The speed limit is 45 miles per hour (mph). On-street parking is prohibited within the Project area. Approximately 45,000 vehicles travel on Mathilda Avenue south of SR 237 on an average weekday.

2.2.2 SR 237

SR 237 (Calaveras Boulevard) east of I-880 is primarily a six-lane divided roadway. Within the Project area, SR 237 provides two mixed-flow lanes in each direction. On eastbound SR 237, a high-occupancy vehicle (HOV) lane is provided east of Mathilda Avenue, which becomes an HOV/express lane from east of Zanker Road to the eastbound SR 237/northbound I-880 direct connector ramp. On westbound SR 237, an HOV/express lane that begins at the southbound I-880/westbound SR 237 direct connector ramp becomes an HOV lane from North First Street to just east of Fair Oaks Avenue. Within the Project area, auxiliary lanes are provided in each direction between US 101 and Mathilda Avenue on SR 237. There is also an auxiliary lane on westbound SR 237 between Fair Oaks Avenue and Mathilda Avenue. SR 237 is a link for trucking between the southern part of the San Francisco Peninsula and the East Bay, providing the first connection south of the Dumbarton Bridge. SR 237 east of Mathilda Avenue currently carries approximately 90,000 vehicles daily.

The SR 237/Mathilda Avenue interchange is a full “tight” diamond interchange that accommodates all ramp movements, with access to and from east and westbound SR 237. All ramp termini are signalized. The westbound SR 237 on-ramp has existing ramp metering equipment installed; however, there is no existing ramp metering equipment installed for the eastbound SR 237 on-ramp.

2.2.3 US 101

Within the Project area, US 101 provides three mixed-flow lanes plus one HOV lane in each direction, while an auxiliary lane is also provided in the southbound direction between SR 237 and Mathilda Avenue. US 101 south of Mathilda Avenue currently carries approximately 154,000 vehicles daily.

The Moffett Park Drive/US 101 northbound on-ramp is a one-lane on-ramp, located along Moffett Park Drive west of the Mathilda Avenue/Moffett Park Drive intersection. This on-ramp merges with the westbound SR 237 off-ramp that connects to northbound US 101. The ramp terminus is signalized, and the on-ramp is not metered.

The US 101/Mathilda Avenue interchange is a partial cloverleaf interchange with access to all but two movements: southbound Mathilda Avenue to northbound US 101 and southbound US 101 to northbound Mathilda Avenue. None of the ramp termini are signalized; however, all of the on-ramps are metered.

2.2.4 Transit Facilities in the Project Area

Two VTA light rail transit stations, Moffett Park and Lockheed Martin, are located within the Project area and serve the business district north of SR 237. VTA also operates a local bus service with four bus stops on Mathilda Avenue. The Sunnyvale Caltrain Station is located in downtown Sunnyvale, adjacent to West Evelyn Avenue. These transit facilities serve passengers who would otherwise use the local roadways and state highway system for commuting purposes.

2.3 Project Purpose and Need

The primary purpose of the Project is to improve traffic operations on Mathilda Avenue through the US 101 and SR 237 interchanges. Due to the close proximity of the SR 237 and US 101 interchanges (less than 1 mile), modification of one interchange would affect the other.

Specifically, the purposes of the Project are to:

- Reduce congestion and improve traffic operations along Mathilda Avenue and at the SR 237/Mathilda Avenue and US 101/Mathilda Avenue interchanges.
- Improve mobility for all travel modes in the area, including motor vehicles, transit, bicycles, and pedestrians.
- Provide standard crosswalks and sidewalks along Mathilda Avenue, improving access to local destinations such as Moffett Park, the VTA light rail transit stations, and downtown Sunnyvale.

The Project is needed for the following reasons:

- Regional growth and new local development, combined with inefficient roadway operations, have resulted in substantial traffic congestion on Mathilda Avenue.
- Efficient access for all travel modes into and out of downtown Sunnyvale and development to the north of SR 237 is critical to a healthy and sustainable economy. Congestion on Mathilda Avenue adversely affects the economic vitality of the City of Sunnyvale.

Overall, the Project is needed to address several issues in the Project area, including roadway deficiencies, lack of or discontinuous bicycle and pedestrian access, improvement of local roadway and freeway ramp operations, and provision of access to current and future economic development.

2.4 Project Alternatives

The Project alternatives that were developed to meet the purpose and need of the Project include Alternative 1, Alternative 2, and the No-Build Alternative (refer to **Figures 2a** and **2b**). The Build Alternatives would provide for all turning movements on Mathilda Avenue at the US 101 and SR 237 interchanges. No new freeway connections are proposed. No modifications to existing structures are required to accommodate the Project improvements. Under the No-Build Alternative, no changes would be made to the existing local roadway or freeway ramps within the Project limits. No construction activities would occur, and there would be no change in the operation of existing facilities.

The design features of the two Build Alternatives include reconfiguration of the US 101 and SR 237 interchanges at Mathilda Avenue. The Build Alternatives include design variations for reconfigured roadways and intersections as well as the construction of new signalized intersections. Proposed improvements included in both Build Alternatives south of Ross Drive along Mathilda Avenue and at the US 101 interchange are identical. These improvements include new bicycle and pedestrian facilities, utility relocations, new storm water treatment facilities, enhanced lighting, ramp metering modifications, overhead signage modifications, and a new retaining wall. In addition to the improvements listed above, Build Alternative 2 includes a diverging diamond interchange¹ design north of Ross Drive on Mathilda Avenue (**Figure 3**).

¹ A diverging diamond interchange, also called a double crossover diamond interchange, is a type of diamond interchange where traffic briefly crosses over to the left (opposite) side of the roadway, guided by traffic signals at each crossover. This allows vehicles to turn left onto freeway on-ramps without stopping and without conflicting with through traffic. The signals at ramp terminal intersections can be operated with two signal phases (a signal phase allows for traffic at an intersection to cycle through specific movements for each direction) instead of three.

2.4.1 Roadway Improvements

The Build Alternatives would consist of the following roadway improvements:

- Provide three continuous through lanes in each direction on Mathilda Avenue.
- Remove northbound US 101 loop off-ramp and shift traffic to northbound US 101 diagonal off-ramp.
- Realign and widen northbound US 101 ramps and signalize ramp intersection with Mathilda Avenue, and construct left-turn lane on southbound Mathilda Avenue to access northbound US 101 loop on-ramp.
- Realign southbound US 101 off-ramp and loop on-ramp and signalize ramp intersection with Mathilda Avenue.
- Modify Mathilda Avenue/Ross Drive signal intersection.
- Close Moffett Park Drive between Bordeaux Drive and Mathilda Avenue, replace with a Class I bikeway (as described below), and shift traffic to Bordeaux Drive and Innovation Way.²
- Remove westbound SR 237 ramp signal intersection. Realign westbound SR 237 off-ramp opposite Moffett Park Drive and modify signal intersection.
- Build Alternative 1 would modify westbound SR 237 ramps to provide a diamond configuration.
- Build Alternative 2 would modify Mathilda Avenue and SR 237 ramps to provide a diverging diamond configuration (see **Figure 2b** and **Figure 3**). Eastbound Moffett Park Drive between Innovation Way and Mathilda Avenue would be diverted to Innovation Way to access Mathilda Avenue.

2.4.2 Bicycle and Pedestrian Facilities

Enhanced bicycle and pedestrian facilities would be provided. Bicycle improvements on Mathilda Avenue would consist of both Class II and Class III bikeways³, based on available pavement widths within the Project limits, and connect to the existing Class III bikeway north of Innovation Way and the Class I bikeway adjacent to the Sunnyvale West Channel. Bicycle improvements on Moffett Park Drive would consist of a Class I bikeway between Bordeaux Drive and Mathilda Avenue. Between Mathilda Avenue and Innovation Way, Class II and Class III bikeways would be considered, based on available pavement widths within the Project limits. A continuous sidewalk would be provided on the east side of Mathilda Avenue within the Project limits, with crosswalks, curb ramps, and pedestrian countdown signals at each intersection. The new crosswalks at the reconfigured ramp intersections would be signalized.

2.4.3 Utility Relocations

The Build Alternatives would include utility relocations, as necessary, to construct the above-described improvements. Build Alternative 1 would require relocation of Verizon telecommunication

² Innovation Way would be extended from Mathilda Avenue to Bordeaux Drive by the Moffett Place development project.

³ Class I bikeway is a bicycle path (completely separate from the roadway). Class II bikeway is a bicycle lane (buffered from roadway). Class III bikeway is bicycle route (“sharrow”) [Source: Highway Design Manual Index 1002.1]

lines and relocation of a City 8-inch recycled water line along the current alignment of Moffett Park Drive east of Mathilda Avenue. Build Alternative 2 would require relocation of a 6-inch PG&E underground gas line and a 12 kilovolt PG&E underground electrical line along the current alignment of Moffett Park Drive west of Mathilda Avenue. Both Build Alternatives could require adjustments to three PG&E electrical pole wires to accommodate ramp modifications at the Mathilda Avenue/US 101 interchange. Utility covers would be adjusted to grade in areas of pavement rehabilitation.

2.4.4 Storm Water Treatment

The proposed interchange ramp modifications are expected to result in the fill or removal of existing ditches, modification or relocation of existing longitudinal drainage structures, and construction of new drainage structures. The Build Alternative's drainage design would maintain existing drainage patterns; however, during construction, temporary drainage facilities may be required to redirect runoff from construction areas.

The storm water treatment facilities for both Build Alternatives may include biofiltration strips, biofiltration swales, bioretention basins, and/or detention basins within the state right-of-way near the on- and off-ramps and within City of Sunnyvale right-of-way along the roadway.

2.4.5 Enhanced Lighting

The Build Alternatives would both provide enhanced lighting to improve roadway visibility for drivers during nighttime hours. Overhead lighting would be maintained or installed at all ramps. The lights would either be supported on a cast-in-drilled-hole pile, with a typical diameter of 2.5 feet and depth of 5 feet, or mounted on a structure above grade.

2.4.6 Ramp Metering

Ramp metering facilities already exist at the northbound US 101 loop on-ramp, southbound US 101 ramps, and westbound SR 237 on-ramp. Because these ramps would be modified and realigned under both Build Alternatives, the affected ramp metering equipment would also be modified.

2.4.7 Overhead Signage

Updated overhead signs in each direction on SR 237 and US 101 would inform motorists of the approaching on- and off-ramps associated with the Project. The overhead sign structure mounted to the Mathilda Avenue overcrossing on northbound US 101 would be removed because it applies to the existing loop off-ramp, which is being relocated and integrated as both a west and east Mathilda Avenue access route from northbound US 101. The northbound US 101 off-ramp sign would be impacted by the off-ramp widening; therefore, it would be removed and replaced just south of the Borregas Bicycle/Pedestrian Overcrossing.

2.4.8 Light Rail Facilities

VTA light rail transit facilities that cross the Moffett Park Drive/Innovation Way and Mathilda Avenue/Innovation Way intersections would be coordinated with traffic signal modifications, which would be location specific. The final locations for new traffic signals would be determined during subsequent design phases.

2.4.9 Retaining Walls and Sound Barriers

The Project would require construction of three retaining walls to minimize the amount of earthwork and right-of-way acquisitions required. The location of proposed retaining walls are at the southbound US 101 diagonal off-ramp/southbound US 101 loop on-ramp, the northbound US 101 off-ramp/northbound US 101 loop on-ramp, and along the west side of Mathilda Avenue. Retaining walls will be aesthetically treated to blend into the surrounding environment and match nearby adjacent walls.

To accommodate proposed realignment and widening of the northbound US 101 off-ramp to Mathilda Avenue, the Project would remove and replace approximately 1,000 feet of the existing 10-foot high noise barrier adjacent to the ramp and West Weddell Drive. The replacement wall would be supported on a retaining wall and located at the widened edge of pavement. Noise barriers will be textured and/ or stained to blend into the surrounding environment, match nearby adjacent walls, and reduce glare and potential for graffiti.

2.4.10 Construction and Staging Areas

Construction of either of the Build Alternatives would take approximately 1 year. A combination of day and night work is anticipated. Weekend work is not anticipated. Short-term lane and ramp closures would be necessary to facilitate construction. Prior to construction, a Traffic Management Plan would be prepared to minimize or prevent delay and inconvenience to the traveling public. The Traffic Management Plan would address all traffic-related aspects of construction, pedestrian access and safety, and bicycle access and safety. Staging/laydown areas for equipment and materials would be needed during Project construction. Construction staging areas would be located within the state right-of-way adjacent to Mathilda Avenue. Potential locations are shown on **Figure 4** and include:

- Within the northbound US 101 loop off-ramp
- Between the northbound US 101 diagonal off-ramp and northbound loop on-ramp
- Within the southbound US 101 loop on-ramp
- Between the southbound US 101 loop on-ramp and diagonal off-ramp
- Between the westbound SR 237 ramps and Moffett Park Drive

Chapter 3 – Affected Environment

3.1 Physical Setting

Ambient air quality is affected by climatological conditions, topography, and the types and amounts of pollutants emitted. The following discussion describes relevant characteristics of the air basin and offers an overview of conditions affecting pollutant ambient air concentrations in the basin.

3.1.1 Climate and Topography

The Project lies within the Santa Clara Valley region of the San Francisco Bay Area Air Basin. The northwest-southeast oriented Santa Clara Valley is bounded by the Santa Cruz Mountains to the west, the Diablo Range to the east, the San Francisco Bay to the north and the convergence of the Gabilan Range and the Diablo Range to the south. Temperatures are warm in summer, under mostly clear skies, although a relatively large diurnal range results in cool nights. Winter temperatures are mild, except for very cool but generally frostless mornings. At the northern end of the Santa Clara Valley, the San Jose Airport mean maximum temperatures range from the high 70s to the low 80s Fahrenheit during the summer to the high 50s to the low 60s during the winter, and mean minimum temperatures range from the high 50s during the summer to the low 40s during the winter. Further inland where the moderating effect of the Bay is not as strong, temperature extremes are greater. Rainfall amounts are modest, ranging from 13 inches in the lowlands to 20 inches in the hills.

Figure 5 indicates the predominant wind direction in the region based on meteorological data from Moffett Federal Airfield in Sunnyvale, about one mile west of the Project (California Air Resources Board 2015). The center of Figure 5 denotes the weather station at Moffett Federal Airfield. The wind patterns in the Valley are influenced greatly by the terrain, resulting in a prevailing flow roughly parallel to the Valley's northwest-southeast axis with a north-northwesterly sea breeze extending up the valley during the afternoon and early evening and a light south-southeasterly drainage flow occurring during the late evening and early morning. In summer a convergence zone is sometimes observed in the southern end of the Valley between Gilroy and Morgan Hill, when air flowing from the Monterey Bay through the Pajaro Gap gets channeled northward into the south end of the Santa Clara Valley and meets with the prevailing north-northwesterlies. Speeds are greatest in the spring and summer, and least in the fall and winter seasons. Nighttime and early morning hours have light winds and are frequently calm in all seasons, while summer afternoon and evenings are quite breezy. Strong winds are rare, coming only with an occasional winter storm.

The air pollution potential of the Santa Clara Valley is high. The valley has a large population and the largest complex of mobile sources in the Bay Area making it a major source of carbon monoxide (CO), particulate, and photochemical air pollution. In addition, photochemical precursors from San Francisco, San Mateo, and Alameda counties can be carried along by the prevailing winds to the Santa Clara Valley, making it also a major ozone receptor. Geographically, the valley tends to channel pollutants to the southeast with its northwest/southeast orientation, and concentrate pollutants by its narrowing to the southeast. Meteorologically, on high-ozone low-inversion summer days, the pollutants can be recirculated by the prevailing northwesterlies in the afternoon and the light drainage flow in the late evening and early morning, increasing the impact of emissions significantly. On high particulate and CO days during late fall and winter, clear, calm, and cold conditions associated with a strong surface-based temperature inversion prevail.

3.2 Regulatory Setting

The Project is located in the Santa Clara County portion of the Bay Area Air Quality Management District (BAAQMD). The BAAQMD has jurisdiction over air quality issues in the seven Bay Area counties—Alameda, Contra Costa, Marin, San Francisco, San Mateo, Santa Clara, and Napa—and portions of southwestern Solano and southern Sonoma counties. The BAAQMD administers air quality regulations developed at the federal, state, and local levels. Federal, state, and local air quality regulations applicable to the Build Alternatives are described below.

3.2.1 Federal Air Quality Standards

The Federal Clean Air Act (FCAA), as amended in 1990, is the federal law that governs air quality. The California Clean Air Act (California CAA) of 1988 is its companion state law. These laws, and related regulations by the U.S. Environmental Protection Agency (EPA) and California Air Resources Board (ARB), set standards for the quantity of pollutants that can be in the air. At the federal level, these standards are called National Ambient Air Quality Standards (NAAQS). At the state level, these standards are called California Ambient Air Quality Standards (CAAQS). NAAQS and CAAQS ambient air quality standards have been established for six transportation-related criteria pollutants that have been linked to potential health concerns. The criteria pollutants are: CO, nitrogen dioxide (NO₂), ozone (O₃), particulate matter (PM, broken down for regulatory purposes into particles of 10 micrometers or smaller [PM₁₀] and particles of 2.5 micrometers and smaller [PM_{2.5}]), lead (Pb), and sulfur dioxide (SO₂). In addition, state standards exist for visibility reducing particles, sulfates, hydrogen sulfide (H₂S), and vinyl chloride. The NAAQS and CAAQS are set at a level that protects public health with a margin of safety and are subject to periodic review and revision. The NAAQS and CAAQS are listed together in Table 3-1. Both state and federal regulatory schemes also cover toxic air contaminants (air toxics). Some criteria pollutants are also air toxics or may include certain air toxics within their general definition.

Federal and state air quality standards and regulations provide the basic scheme for project-level air quality analysis under the National Environmental Policy Act (NEPA) and CEQA. In addition to this type of environmental analysis, a parallel “Conformity” requirement under the FCAA also applies.

Table 3-1. National and California Ambient Air Quality Standards Applicable in California

| Pollutant | Symbol | Average Time | Standard (ppm) | | Standard (µg/m ³) | | Violation Criteria | |
|-----------------------------------|----------------------------------|------------------------|----------------|----------|-------------------------------|----------|------------------------|---|
| | | | California | National | California | National | California | National |
| Ozone | O ₃ | 1 hour | 0.09 | NA | 180 | NA | If exceeded | NA |
| | | 8 hours | 0.070 | 0.070 | 137 | 137 | If exceeded | If fourth highest 8-hour concentration in a year, averaged over 3 years, is exceeded at each monitor within an area |
| Carbon monoxide | CO | 8 hours | 9.0 | 9 | 10,000 | 10,000 | If exceeded | If exceeded on more than 1 day per year |
| | | 1 hour | 20 | 35 | 23,000 | 40,000 | If exceeded | If exceeded on more than 1 day per year |
| (Lake Tahoe only) | | 8 hours | 6 | NA | 7,000 | NA | If equaled or exceeded | NA |
| Nitrogen dioxide | NO ₂ | Annual arithmetic mean | 0.030 | 0.053 | 57 | 100 | If exceeded | If exceeded on more than 1 day per year |
| | | 1 hour | 0.18 | 0.100 | 339 | 188 | If exceeded | NA |
| Sulfur dioxide | SO ₂ | Annual arithmetic mean | NA | 0.030 | NA | NA | NA | If exceeded |
| | | 24 hours | 0.04 | 0.14 | 105 | NA | If exceeded | If exceeded on more than 1 day per year |
| | | 1 hour | 0.25 | 75 | 655 | 196 | If exceeded | NA |
| Hydrogen sulfide | H ₂ S | 1 hour | 0.03 | NA | 42 | NA | If equaled or exceeded | NA |
| Vinyl chloride | C ₂ H ₃ Cl | 24 hours | 0.01 | NA | 26 | NA | If equaled or exceeded | NA |
| Inhalable Particulate Matter (PM) | PM10 | Annual arithmetic mean | NA | NA | 20 | NA | If exceeded | If exceeded at each monitor within area |
| | | 24 hours | NA | NA | 50 | 150 | If exceeded | If exceeded on more than 1 day per year |
| | PM2.5 | Annual arithmetic mean | NA | NA | 12 | 12.0 | If exceeded | If 3-year average from single or multiple community-oriented monitors is exceeded |
| | | 24 hours | NA | NA | NA | 35 | NA | If 3-year average of 98 th percentile at each population-oriented monitor within an area is exceeded |

| Pollutant | Symbol | Average Time | Standard (ppm) | | Standard ($\mu\text{g}/\text{m}^3$) | | Violation Criteria | |
|-------------------|-----------------|-------------------------|----------------|----------|---------------------------------------|----------|------------------------|---|
| | | | California | National | California | National | California | National |
| Sulfate particles | SO ₄ | 24 hours | NA | NA | 25 | NA | If equaled or exceeded | NA |
| Lead particles | Pb | Calendar quarter | NA | NA | NA | 1.5 | NA | If exceeded on more than 1 day per year |
| | | 30-day average | NA | NA | 1.5 | NA | If equaled or exceeded | NA |
| | | Rolling 3-month average | NA | NA | NA | 0.15 | If equaled or exceeded | Averaged over a rolling 3-month period |

Source: California Air Resources Board 2015

Notes: All standards are based on measurements at 25°C and 1 atmosphere pressure; national standards shown are the primary (health effects) standards; ppm = parts per million; $\mu\text{g}/\text{m}^3$ = micrograms per cubic meter; NA = not applicable.

3.2.2 FCAA Conformity Requirements for Transportation

FCAA Section 176(c) prohibits the U.S. Department of Transportation and other federal agencies from funding, authorizing, or approving plans, programs, or projects that are not first found to conform to State Implementation Plan (SIP) for achieving the goals of FCAA requirements related to the NAAQS. The Transportation Conformity Act takes place on two levels: the regional, or planning and programming, level, and the project level. A project must conform at both levels to be approved. Conformity requirements apply only in nonattainment and maintenance (former non-attainment) areas for the NAAQS, and only for the specific NAAQS that are or were violated. EPA regulations at 40 CFR 93 govern the conformity process.

Regional conformity is concerned with how well the regional transportation system supports plans for attaining the standards set for CO, NO₂, ozone, and particulate matter (PM₁₀ and PM_{2.5}), and in some areas sulfur dioxide (SO₂). California is nonattainment or maintenance for all of these transportation-related criteria pollutants except SO₂, and also has a nonattainment area for lead. However, lead is not currently required by the FCAA to be covered in transportation conformity analysis. Regional conformity is based on Regional Transportation Plans (RTPs) and Federal Transportation Improvement Programs (FTIPs) that include all of the transportation projects planned for a region over a period of at least 20 years for the RTP and 4 years for the FTIP. RTP and FTIP conformity is based on use of travel demand and air quality models to determine whether or not implementation of those projects would conform to emission budgets or other tests showing that requirements of the FCAA and SIP are met. If the Metropolitan Planning Organization (MPO) and the Federal Highway Administration (FHWA) make determinations that the RTP and FTIP are in conformity with the SIP for achieving the goals of the FCAA. Otherwise, the projects in the RTP and/or FTIP must be modified until conformity is attained. If the design, concept, scope, and open to traffic schedule of a proposed transportation project are the same as described in the RTP and FTIP, then the project is deemed to meet regional conformity requirements for purposes of project-level analysis.

Conformity at the project-level also requires hot-spot analysis if an area is nonattainment or maintenance for CO and/or particulate matter (PM₁₀ and PM_{2.5}). A region is nonattainment if one or more monitoring stations in the region measures violation of the relevant standard, and the EPA officially designates the area nonattainment. Areas that were previously designated as nonattainment areas but subsequently meet the standard may be officially redesignated to attainment by the EPA, and are then called maintenance areas. Conformity does include some specific procedural and documentation standards for projects that require a hot-spot analysis. In general, projects must not cause the hot-spot-related CO standard to be violated, and must not cause any increase in the number and severity of violations in nonattainment areas. If a known CO or particulate matter violation is located in the project vicinity, the project must include measures to reduce or eliminate the existing violation(s) as well.

The concept of transportation conformity was introduced in the FCAA 1977 amendments. Transportation conformity requires that no federal dollars be used to fund a transportation project unless it can be clearly demonstrated that the project would not cause or contribute to violations of the NAAQS. Conformity requirements were made substantially more rigorous in the 1990 CAAA, and the transportation conformity regulation that details implementation of the new requirements was issued in November 1993.

The U.S. Department of Transportation and EPA developed guidance for determining conformity of transportation plans, programs, and projects in November 1993 in the Transportation Conformity Rule (*40 Code of Federal Regulations [CFR] 51 and 40 CFR 93*). The demonstration of conformity to the SIP is the responsibility of the local MPO, which is also responsible for preparing RTPs and associated demonstration of SIP conformity. Section 93.114 of the Transportation Conformity Rule, states that “there must be a currently conforming regional transportation plan and transportation improvement plan at the time of project approval.”

MTC is the designated federal MPO and state regional transportation planning agency for Santa Clara County. As such, the MTC coordinates the region’s major transportation projects and programs, and promotes regionalism in transportation investment decisions.

The RTP and FTIP list projects whose emissions are within the budget planned in the SIP, with the goal of attaining NAAQS. The FTIP is also in accord with the EPA’s Transportation Conformity Rule as it pertains to attainment of air quality standards in the BAAQMD. The federally required RTP and FTIP are comprehensive listings of all transportation projects that receive federal funds or that are subject to a federally required action, such as a review for impacts on air quality.

The FTIP sets forth the MTC’s investment priorities for transit and transit-related improvements, highways, roadways, and other surface transportation improvements in the Santa Clara County region. The MTC prepares and adopts the FTIP every two years. In addition to (1) demonstrating that a project has been identified in an approved RTP or FTIP and incorporated in an EPA-approved SIP or (2) demonstrating that a project is exempt from conformity requirements, agencies constructing transportation projects must demonstrate that they do not exacerbate an existing NAAQS violation or create a new exceedance.

The Project is proposed to be partially funded by the City of Sunnyvale and other local sources. The Project is found in the 2013 RTP titled *Plan Bay Area (2040 RTP)*, Online Project Database as Project ID 240443 (Metropolitan Transportation Commission 2014). The FHWA and Federal Transit Administration found the 2040 RTP to be in conformity with the SIP on July 18, 2013. The Project is also included in MTC’s financially constrained 2015 Transportation Improvement Program (TIP) as TIP ID SCL130001. The TIP has been updated to be consistent with the RTP as part of the 2015 TIP process. Considering that MTC is only required to adopt a new TIP once every four years, and the 2013 TIP was approved by FHWA and Federal Transit Administration on August 12, 2013, MTC performed a simple update of the 2013 TIP to incorporate MTC’s TIP into the FTIP. The four-year time period of the 2015 TIP (Fiscal Year [FY] 2014-15 through FY 2017–18) is within the six-year time period (FY 2012–13 through FY 2017–18) previously adopted by MTC for the 2013 TIP. Since the 2015 TIP period is entirely contained within the period previously approved by MTC, there are few projects being added that have not previously received a TIP action. The 2015 TIP is simply updating the project costs, scopes, and schedules, and identifying two years of project funding (FY 2012–13 and 2013–14) as prior years, with corresponding updates to other elements of the TIP. The design concept and scope of either Build Alternative is consistent with the project description in the 2040 RTP and the 2015 TIP, and the assumptions in MTC’s regional emissions analysis.

The design concept and scope of the Mathilda Avenue Improvements Project is consistent with the project description in the most recent 2040 RTP and the 2015 TIP. The design concept and scope of the Project are consistent with the project listings in the 2040 RTP and 2015 TIP and would not interfere with timely implementation of Transportation Control Measures.

Attainment Status

The EPA has classified all of Santa Clara County as being a marginal nonattainment area for 8-hour ozone NAAQS and nonattainment for PM_{2.5}, as shown in Table 3-2. For CO NAAQS, the EPA has classified Santa Clara County as a moderate maintenance area (≤ 12.7 parts per million [ppm]) (U.S. Environmental Protection Agency 2015). For PM₁₀ NAAQS the EPA has designated Santa Clara County as an unclassified area.

Table 3-2. Attainment Status of Santa Clara County

| Pollutant | Attainment Status | |
|---------------------------------------|-------------------|------------------------|
| | State | Federal |
| 8-hour Ozone | Nonattainment | Marginal Nonattainment |
| Carbon Monoxide | Attainment | Moderate Maintenance |
| Particulate Matter (PM) ₁₀ | Nonattainment | Unclassified |
| PM _{2.5} | Nonattainment | Nonattainment |

3.2.3 State Air Quality Standards

Responsibility for achieving CAAQS (see Table 3-1), which, for certain pollutants and averaging periods, are more stringent than federal standards, is placed on the California Air Resources Board (ARB) and local air pollution control districts. State standards are achieved through district-level air quality management plans that are incorporated into the SIP.

ARB traditionally has established state air quality standards, maintained oversight authority in air quality planning, developed programs for reducing emissions from motor vehicles, developed air emission inventories, collected air quality and meteorological data, and approved SIPs. Responsibilities of air districts include overseeing stationary source emissions, approving permits, maintaining emissions inventories, maintaining air quality stations, overseeing agricultural burning permits, and reviewing air quality-related sections of environmental documents required under CEQA.

The California CAA of 1988 substantially added to the authority and responsibilities of air districts. The California CAA designates air districts as lead air quality planning agencies, requires air districts to prepare air quality plans, and grants air districts authority to implement Transportation Control Measures.

The California CAA focuses on attainment of the CAAQS and requires designation of attainment and nonattainment areas with respect to these standards. The act also requires that local and regional air districts expeditiously adopt and prepare an air quality attainment plan (Clean Air Plan) if the district violates state air quality standards for ozone, CO, SO₂, or NO₂. These plans are specifically designed to attain state standards and must be designed to achieve an annual 5 percent reduction in district-wide emissions of each nonattainment pollutant or its precursors. No locally prepared attainment plans are required for areas that violate the state PM₁₀ standards; ARB is responsible for developing plans and projects that achieve compliance with the state PM₁₀ standards.

ARB has classified Santa Clara County as a nonattainment area for 1- and 8-hour ozone, PM₁₀, and PM_{2.5} CAAQS, as shown in Table 3-2 (California Air Resources Board 2014). For CO CAAQS, ARB has classified Santa Clara County as an attainment area.

The California CAA requires that the CAAQS be met as expeditiously as practicable, but, unlike the FCAA, does not set precise attainment deadlines. Instead, the act establishes increasingly stringent requirements for areas that will require more time to achieve the standards.

The California CAA emphasizes the control of “indirect and area-wide sources” of air pollutant emissions. The act gives local air pollution control districts explicit authority to regulate indirect sources of air pollution and to establish Transportation Control Measures. The California CAA does not define the terms *indirect sources* and *area-wide sources*. However, Section 110 of the FCAA defines an indirect source as

a facility, building, structure, installation, real property, road, or highway which attracts, or may attract, mobile sources of pollution. Such term includes parking lots, parking garages, and other facilities subject to any measure for management of parking supply....

Transportation Control Measures are defined in the California CAA as “any strategy to reduce trips, vehicle use, vehicle miles traveled, vehicle idling, or traffic congestion for the purpose of reducing vehicle emissions.”

3.2.4 Climate Change Regulatory Requirements

Climate change refers to long-term changes in temperature, precipitation, wind patterns, and other elements of the earth’s climate system. An ever-increasing body of scientific research attributes these climatological changes to greenhouse gases (GHGs), particularly those generated from the production and use of fossil fuels.

While climate change has been a concern for several decades, the establishment of the Intergovernmental Panel on Climate Change by the United Nations and World Meteorological Organization’s in 1988 has led to increased efforts devoted to GHG emissions reduction and climate change research and policy. These efforts are primarily concerned with the emissions of GHGs related to human activity that include carbon dioxide (CO₂), methane, nitrous oxide, tetrafluoromethane, hexafluoroethane, sulfur hexafluoride, HFC-23 (fluoroform), HFC-134a (1, 1, 1, 2 –tetrafluoroethane), and HFC-152a (difluoroethane).

There are typically two terms used when discussing the impacts of climate change. “Greenhouse Gas (GHG) Mitigation” is a term for reducing GHG emissions in order to reduce or “mitigate” the impacts of climate change. “Adaptation,” refers to the effort of planning for and adapting to impacts due to climate change (such as adjusting transportation design standards to withstand more intense storms and higher sea levels).⁴

Transportation sources (passenger cars, light duty trucks, other trucks, buses, and motorcycles) in the state of California make up the largest source (second to electricity generation) of GHG emitting sources. Conversely, the main source of GHG emissions in the United States is electricity generation followed by transportation. The dominant GHG emitted is CO₂, mostly from fossil fuel combustion.

⁴ http://climatechange.transportation.org/ghg_mitigation/

There are four primary strategies for reducing GHG emissions from transportation sources: 1) improve system and operation efficiencies, 2) reduce growth of vehicle miles traveled (VMT), 3) transition to lower GHG fuels, and 4) improve vehicle technologies. To be most effective, all four should be pursued collectively.⁵ The following regulatory setting section outlines state and federal efforts to comprehensively reduce GHG emissions from transportation sources.

State

With the passage of several pieces of legislation including State Senate and Assembly Bills and Executive Orders, California launched an innovative and proactive approach to dealing with GHG emissions and climate change at the state level.

Assembly Bill (AB) 1493 (AB 1493), Pavley. Vehicular Emissions: Greenhouse Gases (AB 1493), 2002: requires the ARB to develop and implement regulations to reduce automobile and light truck GHG emissions. These stricter emissions standards were designed to apply to automobiles and light trucks beginning with the 2009-model year. In June 2009, the EPA Administrator granted a CAA waiver of preemption to California. This waiver allowed California to implement its own GHG emission standards for motor vehicles beginning with model year 2009. California agencies will be working with federal agencies to conduct joint rulemaking to reduce GHG emissions for passenger cars model years 2017–2025.

Executive Order (EO) S-3-05: signed on June 1, 2005, by Governor Arnold Schwarzenegger, the goal of this EO is to reduce California's GHG emissions to: 1) 2000 levels by 2010, 2) 1990 levels by the 2020, and 3) 80 percent below the 1990 levels by the year 2050. In 2006, this goal was further reinforced with the passage of AB 32.

AB32 (AB 32), the Global Warming Solutions Act of 2006: AB 32 sets the same overall GHG emissions reduction goals as outlined in EO S-3-05, while further mandating that ARB create a plan, which includes market mechanisms, and implement rules to achieve “real, quantifiable, cost-effective reductions of greenhouse gases.” EO S-20-06 further directs state agencies to begin implementing AB 32, including the recommendations made by the state's Climate Action Team.

EO S-20-06 (October 18, 2006): This order establishes the responsibilities and roles of the Secretary of the California Environmental Protection Agency and state agencies with regard to climate change.

EO S-01-07: Governor Schwarzenegger set forth the low carbon fuel standard for California. Under this EO, the carbon intensity of California's transportation fuels is to be reduced by at least 10 percent by 2020.

Senate Bill (SB) 97 (Chapter 185, 2007): required the Governor's Office of Planning and Research to develop recommended amendments to the State of California Environmental Quality Act Guidelines for addressing GHG emissions. The Amendments became effective on March 18, 2010.

SB 375, Chapter 728, 2008, Sustainable Communities and Climate Protection: This bill requires ARB to set regional emissions reduction targets from passenger vehicles. The Metropolitan Planning Organization for each region must then develop a Sustainable Communities Strategy that integrates transportation, land use, and housing policies to plan for the achievement of the emissions target for their region.

⁵ http://www.fhwa.dot.gov/environment/climate_change/mitigation/

SB 391, Chapter 585, 2009 California Transportation Plan: This bill requires the state's long-range transportation plan to meet California's climate change goals under AB 32.

Federal

Although climate change and GHG reduction are a concern at the federal level, currently no regulations or legislation have been enacted specifically addressing GHG emissions reductions and climate change at the project level. Neither the EPA nor the FHWA has issued explicit guidance or methods to conduct project-level GHG analysis.⁶ FHWA supports the approach that climate change considerations should be integrated throughout the transportation decision-making process, from planning through project development and delivery. Addressing climate change mitigation and adaptation up front in the planning process will assist in decision-making and improve efficiency at the program level, and will inform the analysis and stewardship needs of project-level decision-making. Climate change considerations can be integrated into many planning factors, such as supporting economic vitality and global efficiency, increasing safety and mobility, enhancing the environment, promoting energy conservation, and improving the quality of life.

The four strategies outlined by FHWA to lessen climate change impacts correlate with efforts that the state is undertaking to deal with transportation and climate change. These strategies include improved transportation system efficiency, cleaner fuels, cleaner vehicles, and a reduction in travel activity.

Climate change and its associated effects are being addressed through various efforts at the federal level to improve fuel economy and energy efficiency, such as the "National Clean Car Program" and EO 13514, *Federal Leadership in Environmental, Energy and Economic Performance*.

EO 13514 (October 5, 2009): This order is focused on reducing greenhouse gases internally in federal agency missions, programs and operations, but also direct federal agencies to participate in the Interagency Climate Change Adaptation Task Force, which is engaged in developing a national strategy for adaptation to climate change.

The EPA's authority to regulate GHG emissions stems from the U.S. Supreme Court decision in *Massachusetts v. EPA* (2007). The Supreme Court ruled that GHGs meet the definition of air pollutants under the existing FCAA and must be regulated if these gases could be reasonably anticipated to endanger public health or welfare. Responding to the Court's ruling, the EPA finalized an endangerment finding in December 2009. Based on scientific evidence, it found that six GHGs constitute a threat to public health and welfare. Thus, it is the Supreme Court's interpretation of the existing Act and the EPA's assessment of the scientific evidence that form the basis for the EPA's regulatory actions. The EPA, in conjunction with the National Highway Traffic Safety Administration issued the first of a series of GHG emission standards for new cars and light-duty vehicles in April 2010.⁷

The EPA and the National Highway Traffic Safety Administration are taking coordinated steps to enable the production of a new generation of clean vehicles with reduced GHG emissions and improved fuel efficiency from on-road vehicles and engines. These next steps include developing the first-ever GHG regulations for heavy-duty engines and vehicles, as well as additional light-duty vehicle GHG regulations.

⁶ To date, no national standards have been established regarding mobile source GHGs, nor has the EPA established any ambient standards, criteria, or thresholds for GHGs resulting from mobile sources.

⁷ <http://www.c2es.org/federal/executive/epa/greenhouse-gas-regulation-faq>

The final combined standards that made up the first phase of this national program apply to passenger cars, light-duty trucks, and medium-duty passenger vehicles, covering model years 2012–2016. The standards implemented by this program are expected to reduce GHG emissions by an estimated 960 million metric tons and 1.8 billion barrels of oil over the lifetime of the vehicles sold under the program (model years 2012–2016).

On August 28, 2012, the EPA and the National Highway Traffic Safety Administration issued a joint Final Rulemaking to extend the National Program for fuel economy standards to model year 2017–2025 passenger vehicles. Over the lifetime of the model year 2017–2025 standards this program is projected to save approximately 2 billion metric tons of GHG emissions and 4 billion barrels of oil.

The complementary EPA and National Highway Traffic Safety Administration standards that make up the Heavy-Duty National Program apply to combination tractors (semi-trucks), heavy-duty pickup trucks and vans, and vocational vehicles (including buses and refuse or utility trucks). Together, these standards will cut GHG emissions and domestic oil use significantly. This program responds to President Barack Obama’s 2010 request to jointly establish GHG emissions and fuel efficiency standards for the medium- and heavy-duty highway vehicle sector. The agencies estimate that the combined standards will reduce CO₂ emissions by about 270 million metric tons and save about 530 million barrels of oil over the life of model year 2014–2018 heavy-duty vehicles.

3.2.5 Existing Air Quality Conditions

Existing air quality conditions in the Project area can be characterized in terms of the ambient air quality standards that the federal and state governments have established for various pollutants (see Table 3-1) and by monitoring data collected in the region. The existing AQ environment can be characterized by monitoring data from the nearest representative monitoring station, which are run by the ARB, EPA, and BAAQMD. There are only 6 monitoring stations located within Santa Clara County, and the nearest stations were used to characterize the Project area. These stations are used by the ARB and EPA to determine whether the County and Air Basin meet state and federal AQ standards and to determine the region’s attainment status related to these standards. Data from these monitoring stations must meet certain criteria in order to comply with and be used for these purposes. Monitoring data concentrations are typically expressed in terms of ppm or µg/m³. The nearest air quality monitoring station to the vicinity of the Project area is located in the City of Cupertino on Voss Avenue. This station is about 6.0 miles southwest of the Project site and monitored for all criteria pollutants until 2014, except for CO, which was monitored until 2013. The closest monitoring station that monitors for all criteria pollutants through the most current reporting year of 2014 is located in the City of San Jose on Jackson Street, about 7.5 miles southeast of the Project site. Table 3-3 summarizes air quality monitoring data from the Cupertino and San Jose monitoring stations during the last 3 years for which complete data are available (2012–2014).

Table 3-3 indicates that the San Jose monitoring station exceeded the state 1-hour ozone standard once in 2012 and the state and national 8-hour standards once for each standard during 2013. The Cupertino monitoring station also experienced an exceedance of the state and national 8-hour standard once during 2013. The San Jose station has exceeded the state PM₁₀ standard and the federal PM_{2.5} standard in multiple instances for all reported years during the 3-year monitoring period, while no violations of the state or federal CO standards have occurred at these monitoring stations during this 3-year monitoring period.

Table 3-3. Ambient Air Quality Monitoring Data Measured at the Voss Avenue (Cupertino) and Jackson Street (San Jose) Monitoring Stations

| Pollutant Standards | Cupertino | | | San Jose | | |
|---|-----------|-------|------|----------|-------|-------|
| | 2012 | 2013 | 2014 | 2012 | 2013 | 2014 |
| 1-Hour Ozone | | | | | | |
| Maximum 1-hour concentration (ppm) | 0.083 | 0.091 | -- | 0.101 | 0.093 | 0.089 |
| 1-hour California designation value | 0.13 | 0.09 | -- | 0.09 | 0.09 | 0.09 |
| 1-hour expected peak day concentration | -- | 0.085 | -- | 0.093 | 0.087 | 0.088 |
| Number of days standard exceeded ^a | | | | | | |
| CAAQS 1-hour (>0.09 ppm) | 0 | 0 | -- | 1 | 0 | 0 |
| 8-Hour Ozone | | | | | | |
| National maximum 8-hour concentration (ppm) | 0.066 | 0.077 | -- | 0.062 | 0.079 | 0.066 |
| National second-highest 8-hour concentration (ppm) | 0.062 | 0.069 | -- | 0.060 | 0.066 | 0.066 |
| State maximum 8-hour concentration (ppm) | 0.067 | 0.078 | -- | 0.063 | 0.080 | 0.066 |
| State second-highest 8-hour concentration (ppm) | 0.062 | 0.070 | -- | 0.061 | 0.067 | 0.066 |
| 8-hour national designation value | -- | 0.062 | -- | 0.061 | 0.058 | 0.060 |
| 8-hour California designation value | 0.092 | 0.070 | -- | 0.070 | 0.067 | 0.067 |
| 8-hour expected peak day concentration | -- | 0.071 | -- | 0.070 | 0.067 | 0.070 |
| Number of days standard exceeded ^a | | | | | | |
| NAAQS 8-hour (>0.075 ppm) | 0 | 1 | -- | 0 | 1 | 0 |
| CAAQS 8-hour (>0.070 ppm) | 0 | 1 | -- | 0 | 1 | 0 |
| Carbon Monoxide (CO) | | | | | | |
| National ^b maximum 8-hour concentration (ppm) | 0.73 | -- | -- | 1.86 | 2.5 | 1.9 |
| National ^b second-highest 8-hour concentration (ppm) | 0.71 | -- | -- | 1.85 | 2.1 | 1.9 |
| California ^c maximum 8-hour concentration (ppm) | 0.73 | -- | -- | 1.86 | -- | -- |
| California ^c second-highest 8-hour concentration (ppm) | 0.71 | -- | -- | 1.85 | -- | -- |
| Expected peak day concentration (ppm) | 0.98 | -- | -- | 2.18 | -- | -- |
| Number of days standard exceeded ^a | | | | | | |
| NAAQS 8-hour (\geq 9 ppm) | 0 | -- | -- | 0 | 0 | 0 |
| CAAQS 8-hour (\geq 9.0 ppm) | 0 | -- | -- | 0 | -- | -- |
| Particulate Matter (PM10)^d | | | | | | |
| National ^b maximum 24-hour concentration ($\mu\text{g}/\text{m}^3$) | 39.1 | 31.0 | -- | 56.5 | 55.8 | 56.4 |
| National ^b second-highest 24-hour concentration ($\mu\text{g}/\text{m}^3$) | 33.2 | 27.8 | -- | 46.1 | 53.7 | 52.0 |
| State ^c maximum 24-hour concentration ($\mu\text{g}/\text{m}^3$) | 41.5 | 33.5 | -- | 59.6 | 58.1 | 54.7 |
| State ^c second-highest 24-hour concentration ($\mu\text{g}/\text{m}^3$) | 33.4 | 29.5 | -- | 48.8 | 57.1 | 49.6 |
| State annual average concentration ($\mu\text{g}/\text{m}^3$) ^e | 13.5 | 14.5 | -- | 18.8 | 22.2 | 20.0 |
| National annual average concentration ($\mu\text{g}/\text{m}^3$) | 13.1 | 14.0 | -- | 18.8 | 21.6 | 19.5 |
| Number of days standard exceeded ^a | | | | | | |
| NAAQS 24-hour (>150 $\mu\text{g}/\text{m}^3$) ^f | 0.0 | 0.0 | -- | 0.0 | 0.0 | 0.0 |
| CAAQS 24-hour (>50 $\mu\text{g}/\text{m}^3$) ^f | 0.0 | 0.0 | -- | 2.9 | 15.2 | 3.1 |

| Pollutant Standards | Cupertino | | | San Jose | | |
|---|-----------|------|------|----------|------|------|
| | 2012 | 2013 | 2014 | 2012 | 2013 | 2014 |
| Particulate Matter (PM2.5) | | | | | | |
| National ^b maximum 24-hour concentration ($\mu\text{g}/\text{m}^3$) | – | – | – | 38.4 | 57.7 | 60.4 |
| National ^b second-highest 24-hour concentration ($\mu\text{g}/\text{m}^3$) | – | – | – | 36.6 | 45.9 | 37.3 |
| State ^c maximum 24-hour concentration ($\mu\text{g}/\text{m}^3$) | 27.5 | 38.9 | – | 38.4 | 57.7 | 60.4 |
| State ^c second-highest 24-hour concentration ($\mu\text{g}/\text{m}^3$) | 26.6 | 31.0 | – | 36.6 | 45.9 | 37.3 |
| National annual designation value ($\mu\text{g}/\text{m}^3$) | – | – | – | -- | 10.3 | 10.0 |
| National annual average concentration ($\mu\text{g}/\text{m}^3$) | – | – | – | 9.1 | 11.8 | 8.4 |
| State annual designation value ($\mu\text{g}/\text{m}^3$) | – | 9 | – | 10 | 12 | 12 |
| State annual average concentration ($\mu\text{g}/\text{m}^3$) ^e | – | 8.5 | – | -- | 12.4 | 8.4 |
| Number of days standard exceeded ^a | | | | | | |
| NAAQS 24-hour ($>35 \mu\text{g}/\text{m}^3$) | – | – | – | 2.1 | 4.0 | 2.0 |

Sources: California Air Resources Board 2016; U.S. Environmental Protection Agency 2016.

Notes: CAAQS = California ambient air quality standards.

NAAQS = national ambient air quality standards.

– = insufficient data available to determine the value.

ppm = parts per million

$\mu\text{g}/\text{m}^3$ = micrograms per cubic meter

^a An exceedance is not necessarily a violation.

^b National statistics are based on standard conditions data. In addition, national statistics are based on samplers using federal reference or equivalent methods.

^c State statistics are based on local conditions data, except in the South Coast Air Basin, for which statistics are based on standard conditions data. In addition, state statistics are based on California approved samplers.

^d Measurements usually are collected every 6 days.

^e State criteria for ensuring that data are sufficiently complete for calculating valid annual averages are more stringent than the national criteria.

^f Mathematical estimate of how many days concentrations would have been measured as higher than the level of the standard had each day been monitored.

3.2.6 Description of Pollutants

The following is a general description of the pollutants for which there are standards (criteria pollutants) and ambient measurements: Ozone, and its precursors, reactive organic gases (ROG) and oxides of nitrogen (NO_x); sulfates; visibility reducing particles; NO_2 ; and PM10 and PM2.5 are considered to be regional pollutants because they or their precursors affect air quality on a regional scale— NO_2 reacts photochemically with reactive organic gases to form ozone, while PM10 and PM2.5 can form from chemical reaction of atmospheric chemicals, including NO_x , sulfates, nitrates, and ammonia. These processes can occur at some distance downwind of the source of pollutants. Pollutants such as CO, SO_2 , lead, and PM10 are considered to be local pollutants because they tend to disperse rapidly with distance from the source. Although PM10 and PM2.5 are considered to be regional pollutants, they can also be localized pollutants, as direct emissions of PM10 from automobile exhaust can accumulate in the air locally near the emission source.

Ozone

Ozone is a respiratory irritant that increases susceptibility to respiratory infections. It is also an oxidant that can cause substantial damage to vegetation and other materials.

Ozone is not emitted directly into the air but is formed by a photochemical reaction in the atmosphere. The ozone precursors ROG and NO_x react in the atmosphere in the presence of sunlight

to form ozone. Because photochemical reaction rates depend on the intensity of ultraviolet light and air temperature, ozone is primarily a summer air pollution problem.

Carbon Monoxide

CO is a public health concern because it combines readily with hemoglobin and reduces the amount of oxygen transported in the bloodstream. CO can cause health problems such as fatigue, headache, confusion, dizziness, and even death.

Motor vehicles are the dominant source of CO emissions in most areas. High CO levels develop primarily during winter when periods of light winds combine with the formation of ground-level temperature inversions (typically from the evening through early morning). These conditions result in reduced dispersion of vehicle emissions. Motor vehicles also exhibit increased CO emission rates at low air temperatures.

Inhalable Particulate Matter

Particulates can damage human health and retard plant growth. Health concerns associated with suspended particulate matter focus on those particles small enough to reach the lungs when inhaled. Particulates also reduce visibility and corrode materials.

PM10 sources in Solano County comprise both rural and urban sources, including agricultural burning, tilling of agricultural fields, industrial emissions, dust suspended by vehicle traffic, and secondary aerosols formed by reactions in the atmosphere.

The federal and state ambient air quality standard for particulate matter applies to two classes of particulates: PM2.5 and PM10.

Carbon Dioxide

CO₂ is the most important anthropogenic GHG and accounts for more than 75 percent of all anthropogenic GHG emissions. Its long atmospheric lifetime (on the order of decades to centuries) ensures that atmospheric concentrations of CO₂ will remain elevated for decades after GHG mitigation efforts to reduce GHG concentrations are promulgated (Intergovernmental Panel on Climate Change 2007).

Increasing concentrations of CO₂ in the atmosphere are primarily a result of emissions from the burning of fossil fuels, gas flaring, cement production, and land use changes. Three quarters of anthropogenic CO₂ emissions are the result of fossil fuel burning (and to a very small extent, cement production), and approximately one quarter of emissions are the result of land use change (Intergovernmental Panel on Climate Change 2007).

Anthropogenic emissions of CO₂ have increased concentrations in the atmosphere most notably since the industrial revolution; the concentration of CO₂ has increased from about 280 ppm to 390 ppm from 1750 to 2011 (Intergovernmental Panel on Climate Change 2013:161). The Intergovernmental Panel on Climate Change estimates that the present atmospheric concentration of CO₂ has not been exceeded in the last nearly 1 million years (Intergovernmental Panel on Climate Change 2007:100).

Nitrogen Dioxide

Nitrogen oxides are a family of highly reactive gases that are primary precursors to the formation of ground-level ozone, reacting in the atmosphere to form acid rain. NO_x , a mixture of NO and NO_2 , are produced from natural sources, motor vehicles, and other fuel combustion processes. NO is colorless and odorless and is [oxidized](#) in the atmosphere to form NO_2 . NO_2 is an odorous, brown, acidic, highly corrosive gas that can affect human health and the environment. NO_x are critical components of photochemical smog. NO_2 produces the yellowish-brown color of the smog. The EPA has set an NAAQS standard for NO_2 but not for NO.

NO_x can irritate the lungs, cause lung damage, and lower resistance to respiratory infections such as influenza. The effects of short-term exposure are still unclear, but continued or frequent exposure to concentrations that are typically much higher than those normally found in the ambient air may cause increased incidence of acute respiratory illness in children. Health effects associated with NO_x are an increase in the incidence of chronic bronchitis and lung irritation. Chronic exposure to NO_2 may lead to eye and mucus membrane aggravation along with pulmonary dysfunction. NO_x can cause fading of textile dyes and additives, deterioration of cotton and nylon, and corrosion of metals due to the production of particulate nitrates. Airborne NO_x can impair visibility. NO_x is a major component of acid deposition in California. NO_x may affect both terrestrial and aquatic ecosystems. NO_x in the air is a potentially significant contributor to a number of environmental effects, such as acid rain and eutrophication in coastal waters. Eutrophication occurs when a body of water suffers an increase in nutrients that reduces the amount of oxygen in the water, producing an environment that is destructive to fish and other animal life.

Sulfur Oxides

SO_x gases are a family of colorless, pungent gases, which include SO_2 and are formed primarily by combustion of sulfur-containing fossil fuels (mainly coal and oil), metal smelting, and other industrial processes. SO_x can react to form sulfates, which significantly reduce visibility. SO_x is a precursor to particulate matter formation, which is in nonattainment in the Project area.

The major health concerns associated with exposure to high concentrations of SO_x include effects related to breathing, respiratory illness, alterations in pulmonary defenses, and aggravation of existing cardiovascular disease. Major subgroups of the population that are most sensitive to SO_x include individuals with cardiovascular disease or chronic lung disease (such as bronchitis or emphysema), as well as children and the elderly. Emissions of SO_x can also damage the foliage of trees and agricultural crops. Together, SO_x and NO_x are the major precursors to acid rain, which is associated with the acidification of lakes and streams and accelerated corrosion of buildings and monuments.

Lead

Lead is a metal that is a natural constituent of air, water, and the biosphere. Lead is neither created nor destroyed in the environment, so it essentially persists forever. Lead was used several decades ago to increase the octane rating in automotive fuel. Because gasoline-powered automobile engines were a major source of airborne lead through the use of leaded fuels and the use of leaded fuel has been mostly phased out, the ambient concentrations of lead have dropped dramatically.

Short-term exposure to high levels of lead can cause vomiting, diarrhea, convulsions, coma, or even death. However, even small amounts of lead can be harmful, especially to infants, young

children, and pregnant women. Symptoms of long-term exposure to lower lead levels may be less noticeable but are still serious. Anemia is common, and damage to the nervous system may cause impaired mental function. Other symptoms are appetite loss, abdominal pain, constipation, fatigue, sleeplessness, irritability, and headache. Continued excessive exposure, as in an industrial setting, can affect the kidneys.

Lead exposure is most serious for young children because they absorb lead more easily than adults and are more susceptible to its harmful effects. Even low-level exposure may harm the intellectual development, behavior, size, and hearing of infants. During pregnancy, especially in the last trimester, lead can cross the placenta and affect the fetus. Female workers exposed to high levels of lead have more miscarriages and stillbirths.

Toxic Air Contaminants/Mobile Source Air Toxics

Toxic air contaminants are pollutants that may result in an increase in mortality or serious illness, or that may pose a present or potential hazard to human health. Health effects of toxic air contaminants include cancer, birth defects, neurological damage, damage to the body's natural defense system, and diseases that lead to death. In 1998, following a 10-year scientific assessment process, ARB identified particulate matter from diesel-fueled engines as a toxic air contaminant. Compared to other air toxics that ARB has identified and controlled, diesel particulate matter emissions are estimated to be responsible for about 70 percent of the total ambient air toxics risk (California Air Resources Board 2000).

The CAAA made controlling air toxic emissions a national priority, by which Congress mandated that the EPA regulate 188 air toxics. These substances are also known as hazardous air pollutants. In the EPA's latest rule, *Control of Emissions of Hazardous Air Pollutants from Mobile Sources (Federal Registry, Vol. 72, No. 37, page 8430, February 2007)* it identified a group of 93 compounds emitted from mobile sources that are listed in their Integrated Risk Information System. This system is a comprehensive database of specific substances known to cause human health effects. In addition, the EPA identified the following seven compounds as priority mobile source air toxics (MSATs):

- Acrolein.
- Benzene.
- 1,3-Butadiene.
- Diesel particulate matter/diesel exhaust organic gases.
- Formaldehyde.
- Naphthalene.
- Polycyclic organic matter.

While FHWA considers these the priority MSATs, the list is subject to change and may be adjusted in consideration of future rules.

To address emissions of MSATs, the EPA has issued a number of regulations, including the 2007 rule mentioned above, that will dramatically decrease MSATs through cleaner fuels and cleaner engines.

The issue of air toxics is an emerging area of analysis and continuing research. Although much work has been done to assess the overall health risk of air toxics, many questions remain unanswered. In particular, the tools and techniques available for assessing project-specific health impacts from MSATs are currently limited. Given the emerging state of the science and of project-level analysis techniques, there are no established criteria for determining when MSAT emissions should be considered a significant issue in the context of NEPA.

FHWA released guidance for factoring mobile source health risks into project-level decision making under NEPA in December 2012 (U.S. Federal Highway Administration 2012). However, the EPA has not established regulatory concentration targets for the seven relevant MSAT pollutants appropriate for use in the project development process. The FHWA recommends MSAT analyses be conducted using the EPA's latest version of the Motor Vehicle Emissions Simulator model, released on October 30, 2012, which estimates on- and off-road MSAT emissions from motor vehicles. FHWA's guidance advises the assessment of MSATs in NEPA documents (U.S. Federal Highway Administration 2012).

3.2.7 Sensitive Receptors

BAAQMD generally defines a sensitive receptor as a facility or land use that houses or attracts members of the population, such as children, the elderly, and people with illnesses, who are particularly sensitive to the effects of air pollutants.

The Project area is located within an existing urban environment that is home to a number of sensitive receptors. Sensitive receptors in the vicinity of the Project area that could be affected by the Project are identified in **Figure 6** and summarized below. Figure 6 does not include the locations of scattered or individual sensitive receptors. Note the sensitive receptors indicated in Figure 6 are not representative of the receptors modeled in the CO hot-spot analysis presented in Impact AQ-2. Land use compatibility issues relative to the siting of pollution-emitting sources or the siting of sensitive receptors must be considered. In the case of schools, state law requires that siting decisions consider the potential for toxic or harmful air emissions in the surrounding area.

Residential

- Single-family residences 25 feet east of the Project site.
- Multi-family residences 50 feet east of the southern part of the Project site.
- Mobile home residences 150 feet southeast of the eastern part of the Project site.

Educational

- Columbia Middle School 920 feet southeast of the eastern part of the Project site.
- Foothill De Anza Community College Campus at Onizuka (opening in late 2016) 30 feet from the western part of the Project site.

Recreational

- Orchard Gardens Park 220 feet east of the eastern part of the Project site.
- Columbia Park 615 feet southeast of the eastern part of the Project site
- John W. Christian Greenbelt 350 feet north of the eastern part of the Project site.

3.3 Environmental Consequences

3.3.1 Methods

The Build Alternatives would generate construction-related and operational emissions. The methodology used to evaluate construction and operational effects is described below.

Operational Impact Assessment Methodology

The primary operational emissions associated with the Build Alternatives are CO, PM₁₀, PM_{2.5}, the ozone precursors ROG and NO_x, and CO₂ emitted as vehicle exhaust. The evaluation of transportation conformity with regards to criteria pollutants was done by evaluating the inclusion of the Project in the most recent RTP and TIP. In addition, the effects of criteria pollutants (ozone precursors, CO, PM₁₀, and PM_{2.5}), as well as CO₂ emissions, were quantified with Caltrans' [CT-EMFAC emission modeling program (version 6.0) and traffic data provided by the Project traffic engineers, Fehr & Peers (Fehr & Peers 2016). The effects of localized CO hot-spot emissions were evaluated through CO dispersion modeling using the *Transportation Project-Level Carbon Monoxide Protocol* developed for Caltrans by the Institute of Transportation Studies at the University of California, Davis (Garza et al. 1997) and traffic data provided by the Project traffic engineers, Fehr & Peers (Fehr & Peers 2016a, 2016b). The effects of localized PM were evaluated using the EPA and FHWA's guidance manual, *Transportation Conformity Guidance for Qualitative Hot-spot Analyses in PM_{2.5} and PM₁₀ Nonattainment and Maintenance Areas* (Federal Highway Administration and U.S. Environmental Protection Agency 2006). MSAT emissions were evaluated using the FHWA's *Interim Guidance on Mobile Source Air Toxic Analysis in NEPA documents* (Federal Highway Administration 2012).

Inclusion in RTP and TIP

The Build Alternatives are located in a marginal nonattainment area with regards to the federal 8-hour ozone standard. Because ozone and its precursors are regional pollutants, the Project must be evaluated under the transportation conformity requirements described earlier. An affirmative regional conformity determination must be made before the Project can proceed. Such a determination is not required if the Project is described in an approved RTP and/or TIP and the Project has not been altered in design concept or scope.

Project-Level Hot-Spot

Carbon Monoxide

A CO hot-spot analysis is based on the CO Protocol developed for Caltrans by the Institute of Transportation Studies at the University of California, Davis (Garza et al. 1997). This CO protocol details a qualitative step-by-step procedure to determine whether Project-related CO concentrations have a potential to generate new air quality violations, worsen existing violations, or delay attainment of CAAQS for CO.

PM_{2.5}

As previously indicated, Santa Clara County is designated by the ARB as a nonattainment area for the state PM₁₀ and PM_{2.5} standards.

On March 10, 2006, the EPA published a final rule that establishes the transportation conformity criteria and procedures for determining which transportation projects must be analyzed for local

air quality impacts in PM2.5 and PM10 nonattainment and maintenance areas. The final rule requires PM2.5 hot-spot analyses to be performed for Projects of Air Quality Concern (POAQC) or any other project identified by the PM2.5 SIP as a localized air quality concern. Section 93.123(b)(1) of the Conformity Rule defines the following projects that require a PM2.5 or PM10 hot-spot analysis (Table 3-4).

Table 3-4. POAQCs as Defined by Section 93.123(b)(1) of the Conformity Rule

| Section 93.123(b)(1) Subsection | Type of Project |
|------------------------------------|---|
| i | New highway projects that have a significant number of diesel vehicles, and expanded highway projects that have a significant increase in the number of diesel vehicles. |
| ii | Projects affecting intersections that are at LOS D, E, or F with a significant number of diesel vehicles, or those that will change to LOS D, E, or F because of increased traffic volumes from a significant number of diesel vehicles related to the project. |
| iii | New bus and rail terminals and transfer points that have a significant number of diesel vehicles congregating at a single location. |
| iv | Expanded bus and rail terminals and transfer points that significantly increase the number of diesel vehicles congregating at a single location. |
| v | Projects in or affecting locations, areas, or categories of sites which are identified in the PM2.5 or PM10 applicable implementation plan or implementation plan submission, as appropriate, as sites of violation or possible violation. |

Source: 40 CFR 93.123(b)(1)

LOS= level of service

In November 2015, the EPA issued a guidance document titled *Transportation Conformity Guidance for Quantitative Hot-Spot Analyses in PM2.5 and PM10 Nonattainment and Maintenance Areas* (U.S. Environmental Protection Agency 2015c). This guidance details the procedure to conduct quantitative hot-spot analyses to determine whether project-related particulate emissions have a potential to generate new air quality violations, worsen existing violations, or delay attainment of ambient air quality standards for PM2.5 or PM10. Because the Project is not subject to federal NEPA or transportation conformity requirements, project-level PM10 and PM2.5 hot-spot analyses that includes interagency consultation through MTC’s Air Quality Conformity Task Force is not required for the proposed Project (Brazil pers. Comm.). However, because the Project area is designated as a nonattainment area for the State PM10 and PM2.5 standards, the determination of whether the Project is or is not a POAQC is used to evaluate PM hot-spots for CEQA purposes.

For the assessment of PM hotspots, the final rule is that a hot-spot analysis is to be performed only for POAQCs. POAQCs are certain highway and transit projects that involve significant levels of diesel traffic or any other project identified in the PM2.5 or PM10 SIP as a localized air quality concern. The following list provides examples of POAQCs.

- A project on a new highway or expressway that serves a significant volume of diesel truck traffic, such as facilities with greater than 125,000 annual average daily traffic (AADT) where 8 percent or more of such AADT is diesel truck traffic.
- New exit ramps and other highway facility improvements to connect a highway or expressway to a major freight, bus, or intermodal terminal.

- Expansion of an existing highway or other facility that affects a congested intersection (operated at level of service (LOS) D, E, or F) that has a significant increase in the number of diesel trucks.
- Similar highway projects that involve a significant increase in the number of diesel transit busses and/or diesel trucks.

The EPA noted in the March 2006 final rule that the examples below are considered to be the most likely projects that would be considered a POAQC under Section 93.123(b)(1)iii and iv listed above.

- A major new bus or intermodal terminal that is considered to be a “regionally significant project.”
- An existing bus or intermodal terminal that has a large vehicle fleet where the number of diesel buses increases by 50 percent or more, as measured by bus arrivals.

The EPA noted in the March 2006 final rule that the examples below are considered to be the most likely projects that would not be considered a POAQC under Section 93.123(b)(1)i and ii listed above.

- Any new or expanded highway project that primarily services gasoline vehicle traffic (i.e., does not involve a significant number or increase in the number of diesel vehicles), including such projects involving congested intersections operating at LOS D, E, or F.
- An intersection channelization project or interchange configuration project that involves either turn lanes or slots, or lanes or movements that are physically separated. These kinds of projects improve freeway operations by smoothing traffic flow and vehicle speeds by improving weave and merge operations, which would not be expected to create or worsen PM2.5 or PM10 violations.
- Intersection channelization projects, traffic circles or roundabouts, intersection signalization projects at individual intersections, and interchange reconfiguration projects that are designed to improve traffic flow and vehicle speeds, and do not involve any increases in idling. Thus, they would be expected to have a neutral or positive influence on PM2.5 or PM10 emissions.

The EPA noted in the March 2006 final rule that the examples below are considered to be the most likely projects that would not be considered a POAQC under Section 93.123(b)(1)iii and iv listed above:

- A new or expanded bus terminal that is serviced by non-diesel vehicles (e.g., compressed natural gas) or hybrid-electric vehicles.
- A 50 percent increase in daily arrivals at a small terminal (e.g., a facility with 10 buses in the peak hour).

For projects identified as not being a POAQC, quantitative PM2.5 and PM10 (for regions without an approved conformity SIP) hot-spot analyses are not required. For these types of projects, state and local project sponsors should briefly document that hot-spot requirements were met without a hot-spot analysis, since such projects have been found to not be of air quality concern under *40 CFR 93.123(b)(1)*. Because this analysis assumes the area is classified as a nonattainment area for the state PM10 and PM2.5 standards, a determination is required to be made as to whether it would result in a PM10 or PM2.5 hot-spot.

Mobile-Source Air Toxics

The FHWA has issued an updated interim guidance using a tiered approach on how MSATs should be addressed in NEPA documents for highway projects (Federal Highway Administration 2012). Depending on the specific project circumstances, FHWA has identified the following three levels of analysis.

1. No analysis for exempt projects or projects that have no potential for meaningful MSAT effects.
2. Qualitative analysis for projects with low potential MSAT effects.
3. Quantitative analysis to differentiate alternatives for projects with higher potential MSAT effects.

Exempt Projects or Projects with No Meaningful Potential MSAT Effects

The types of projects included in this category—those that are exempt or have no meaningful potential MSAT effects—are listed below.

- Projects qualifying as a categorical exclusion under 23 CFR 771.117(c).
- Projects exempt under the FCAA Conformity Rule under 40 CFR 93.126.
- Other projects with no meaningful impacts on traffic volumes or vehicle mix.

For projects that are categorically excluded under 23 CFR 771.117(c), or are exempt from all conformity requirements under the FCAA pursuant to 40 CFR 93.126, no analysis or discussion of MSAT is necessary. Documentation sufficient to demonstrate that the project qualifies as a categorical exclusion or exempt project will suffice. For other projects with no or negligible traffic impacts, regardless of the class of NEPA environmental document, no MSAT analysis is recommended.⁸ However, the project record should document the basis for the determination of “no meaningful potential impacts” with a brief description of the factors considered.

Projects with Low Potential MSAT Effects

The types of projects included in this category—projects with low potential MSAT effects—are those that serve to improve operations of highway, transit, or freight without adding substantial new capacity or without creating a facility that is likely to meaningfully increase MSAT emissions. This category covers a broad range of projects.

FHWA anticipates that most highway projects that need an MSAT assessment will fall into this category. Any projects not meeting the criteria for exempt projects or projects without meaningful potential effects (discussed above) or projects with higher potential MSAT effects (discussed below) should be included in this category. Examples of these types of projects are minor widening projects, new interchanges, replacing a signalized intersection on a surface street, or projects where design year traffic is projected to be less than 140,000 to 150,000 AADT.

For these projects, a qualitative assessment of emissions projections should be conducted. This qualitative assessment would compare, in narrative form, the expected effect of the project on traffic volumes, vehicle mix, or routing of traffic and the associated changes in MSAT for the

⁸ The types of projects categorically excluded under 23 CFR 771.117(d) or exempt from project-level conformity requirements under 40 CFR 93.127 do not warrant an automatic exemption from an MSAT analysis, but they usually will have no meaningful impact.

project alternatives, including the No Build Alternative, based on VMT, vehicle mix, and speed. It would also discuss national trend data projecting substantial overall reductions in emissions due to stricter engine and fuel regulations issued by the EPA. Because the emission effects of these projects typically are low, we expect there would be no appreciable difference in overall MSAT emissions among the various alternatives.

Projects with Higher Potential MSAT Effects

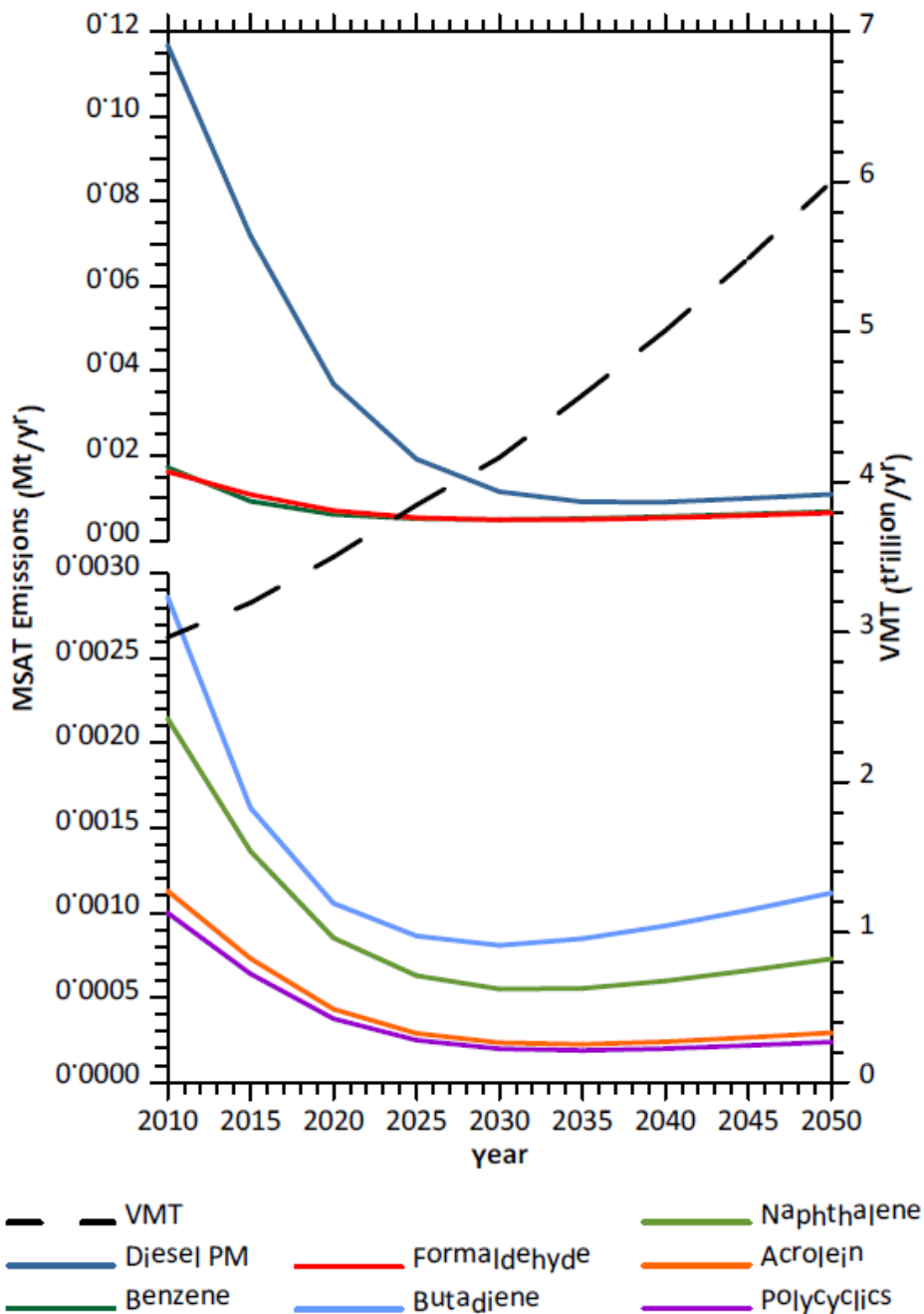
This category includes projects that have the potential for meaningful differences in MSAT emissions among project alternatives. It is expected a limited number of projects would meet the criteria to fall into this category, which are as follows.

- Projects that create or significantly alter a major intermodal freight facility that has the potential to concentrate high levels of diesel particulate matter in a single location, involving a significant number of diesel vehicles for new projects or accommodating a significant increase in the number of diesel vehicles for expansion projects.
- Projects that create new capacity or add significant capacity to urban highways, such as interstates, urban arterials, or urban collector-distributor routes with traffic volumes where the AADT is projected to be in the range of 140,000 to 150,000⁹, or greater, by the design year.
- Projects that are proposed to be located in proximity to populated areas.

Projects falling within this category should be more rigorously assessed for impacts, including a quantitative analysis to forecast local-specific emission trends of the priority MSAT for each alternative. Based on regulations now in effect, an analysis of national trends with the EPA's Motor Vehicle Emissions Simulator model, as shown in **Figure 7** even if VMT increases by 102 percent as assumed from 2010 to 2050, a combined reduction of 83 percent in the total annual emissions for the priority MSAT is projected for the same time period.

⁹ Using the EPA's Motor Vehicle Emissions Simulator 2010b emissions model, FHWA staff determined that this range of AADT would result in emissions significantly lower than the California CAA definition of a major hazardous air pollutant source, i.e., 25 tons per year for all hazardous air pollutants or 10 tons per year for any single hazardous air pollutant. Variations in conditions such as congestion or vehicle mix could warrant a different range for AADT; if this range does not seem appropriate for a project, project proponents can consult with the contacts from Office of Natural Environment and Office of Project Development and Environmental Review identified in the FHWA interim MSAT guidance (U.S. Federal Highway Administration 2012).

Figure 7. Projected National MSAT Emission Trends 2010–2050 For Vehicles Operating On Roadways Using the EPA’s Motor Vehicle Emissions Simulator 2010b Model



Note: Trends for specific locations may be different, depending on locally derived information representing vehicle-miles travelled, vehicle speeds, vehicle mix, fuels, emission control programs, meteorology, and other factors

Applicable Project MSAT Category Assessment

The purpose of this Project is to reduce congestion and improve traffic operations on Mathilda Avenue at SR 237 and US 101 by reconfiguring the US 101 and SR 237 interchanges with Mathilda Avenue. This includes modification to on- and off-ramps; removal, addition, and signalization of intersections; and provision of new left-turn lanes. This Project has been determined to generate minimal air quality impacts for CAAA criteria pollutants and has not been linked with any special MSAT concerns. The Build Alternatives associated with this Project would result in a decrease in traffic volumes when compared to No Build conditions, as shown in Table 3-5, but would not result in changes in vehicle mix, basic Project location, or any other factor that would cause an increase in MSAT impacts of the Build Alternatives from that of the No-Build Alternative. An evaluation of MSAT emissions was performed using traffic data provided by the Project traffic engineers, Fehr & Peers, and the CT-EMFAC model v6.0.

Mass Emissions and Dispersion Modeling

Predicting the ambient air quality impacts of pollutant emissions requires an assessment of the transport, dispersion, chemical transformation, and removal processes that affect pollutant emissions after their release from a source. Gaussian dispersion models are frequently used for such analyses. The term *Gaussian dispersion* refers to a general type of mathematical equation used to describe the horizontal and vertical distribution of pollutants downwind from an emission source.

Gaussian dispersion models treat pollutant emissions as being carried downwind in a defined plume, subject to horizontal and vertical mixing with the surrounding atmosphere. The plume spreads horizontally and vertically with a reduction in pollutant concentrations as it travels downwind. Mixing with the surrounding atmosphere is greatest at the edge of the plume, resulting in lower pollutant concentrations outward (horizontally and vertically) from the center of the plume. This decrease in concentration outward from the center of the plume is treated as following a Gaussian (“normal”) statistical distribution. Horizontal and vertical mixing generally occur at different rates. Because turbulent motions in the atmosphere occur on a variety of spatial and time scales, vertical and horizontal mixing also vary with distance downwind from the emission source.

CT-EMFAC Model. CT-EMFAC v6.0 is a California-specific project-level analysis tool developed for Caltrans by the University of California, Davis to model criteria pollutant, MSAT, and CO₂ emissions from on-road mobile sources. The model uses the latest version of ARB California Mobile Source Emission Inventory and Emission Factors model, EMFAC2014, to quantify running exhaust and running loss emissions using user-input traffic data, including peak-hour and off-peak-hour VMT data allocated into 5-mph speed bins. Running exhaust emissions are emitted from the vehicle tailpipe while the vehicle is traveling, while running loss emissions are evaporative total organic gases emissions that occur when hot fuel vapors escape from the fuel system or overwhelm the carbon canister while the vehicle is operating. CT-EMFAC will estimate emission factors and project-level emissions for the following pollutants:

- **Criteria pollutants:** Ozone precursors (total organic gases and NO_x), CO, sulfur oxides, PM₁₀, and PM_{2.5}.
- **Greenhouse gases:** CO₂.
- **Mobile Source Air Toxics:** diesel particulate matter, formaldehyde, naphthalene, benzene, 1,3-butadiene, polycyclic organic matter, and acrolein.

The CALINE4 Model. The ambient air quality effects of traffic emissions were evaluated using the CALINE4 v2.1 dispersion model (Benson 1989). CALINE4 is a Gaussian dispersion model specifically designed to evaluate air quality impacts of roadway projects. Each roadway link analyzed in the model is treated as a sequence of short segments. Each segment of a roadway link is treated as a separate emission source producing a plume of pollutants which disperses downwind. Pollutant concentrations at any specific location are calculated using the total contribution from overlapping pollution plumes originating from the sequence of roadway segments.

When winds are essentially parallel to a roadway link, pollution plumes from all roadway segments overlap. This produces high concentrations near the roadway (near the center of the overlapping pollution plumes) and low concentrations well away from the roadway (at the edges of the overlapping pollution plumes). When winds are at an angle to the roadway link, pollution plumes from distant roadway segments make essentially no contribution to the pollution concentration observed at a receptor location. Under such crosswind situations, pollutant concentrations near the highway are lower than under parallel wind conditions (fewer overlapping plume contributions), while pollutant concentrations away from the highway may be greater than would occur with parallel winds (near the center of at least some pollution plumes).

The CALINE4 model employs a “mixing cell” approach to estimating pollutant concentrations over the roadway itself. The size of the mixing cell over each roadway segment is based on the width of the traffic lanes of the highway (generally 12 feet per lane) plus an additional turbulence zone on either side (generally 10 feet on each side). Parking lanes and roadway shoulders are not counted as traffic lanes. The height of the mixing cell is calculated by the model.

Pollutants emitted along a highway link are treated as being well-mixed within the mixing cell volume due to mechanical turbulence from moving vehicles and convective mixing due to the temperature of vehicle exhaust gases. Pollutant concentrations downwind from the mixing cell are calculated using horizontal and vertical dispersion rates, which are a function of various meteorological and ground surface conditions.

Criteria Pollutant Emission Modeling

The estimation of criteria pollutant emissions associated with the Build Alternatives was conducted using the CT-EMFAC model and vehicle activity data provided by the Project traffic engineer, Fehr & Peers (see Appendix B).

Roadway and Traffic Conditions. Modeled traffic volumes and operating conditions were obtained from the traffic data prepared by the Project traffic engineers, Fehr & Peers (see Appendix B). Emission of the ozone precursors ROG and NO_x and emission of CO, PM₁₀, PM_{2.5}, and CO₂ were modeled for existing year (2013), opening year (2018) with and without the Project, and design-future year (2040) with and without Project conditions. Fehr & Peers provided AM and PM peak hour VMT data, non-peak hour VMT data, and VMT distribution by 5-mph speed bins (5 mph to 70 mph). VMT data included vehicle activity for affected roadways in the immediate Project region. The traffic data used for emissions modeling is summarized in Tables 3-6 through 3-8.

Table 3-5. Criteria Pollutant, MSAT, and CO₂ Modeling VMT Data Alternatives Comparison

| Comparison of VMT by Alternatives | Increase in Daily VMT | Increase in Annual VMT^a |
|--|------------------------------|---|
| Comparison of 2018 Build Conditions to Existing Conditions | | |
| 2018 No Build—Existing | 180,183 | 62,523,364 |
| 2018 Build Alternative 1—Existing | 164,333 | 57,023,689 |
| 2018 Build Alternative 2—Existing | 172,310 | 59,791,476 |
| Comparison of 2040 Build Conditions to Existing Conditions | | |
| 2040 No Build—Existing | 694,990 | 241,161,552 |
| 2040 Build Alternative 1—Existing | 633,857 | 219,948,514 |
| 2040 Build Alternative 2—Existing | 664,623 | 230,624,266 |
| Comparison of 2018 Build Conditions to 2018 No Build Conditions | | |
| 2018 Build Alternative 1—2018 No Build | -15,849 | -5,499,676 |
| 2018 Build Alternative 2—2018 No Build | -7,873 | -2,731,889 |
| Comparison of 2040 Build Conditions to 2040 No Build Conditions | | |
| 2040 Build Alternative 1—2040 No Build | -61,133 | -21,213,037 |
| 2040 Build Alternative 2—2040 No Build | -30,367 | -10,537,286 |

^a Annual VMT values derived from Daily VMT values multiplied by 347, per ARB methodology (California Air Resources Board 2008).
Source: Brooke pers. comm.

Table 3-6. VMT by Speed Bin—AM Peak Period*

| Bin Name | Bin Actual | 2013 | | 2018 No Project | | 2018 Build 1 | | 2018 Build 2 | | 2040 No Build | | 2040 Build 1 | | 2040 Build 2 | |
|----------|-------------|-----------|--------|-----------------|--------|--------------|--------|--------------|--------|---------------|--------|--------------|--------|--------------|--------|
| | | VMT | % | VMT | % | VMT | % | VMT | % | VMT | % | VMT | % | VMT | % |
| 5 | 0.00-5.00 | 98 | 0.0% | 197 | 0.0% | 204 | 0.0% | 633 | 0.2% | 478 | 0.1% | 507 | 0.1% | 2160 | 0.4% |
| 10 | 5.01-10.00 | 303 | 0.1% | 969 | 0.2% | 611 | 0.1% | 962 | 0.2% | 2873 | 0.6% | 1491 | 0.3% | 2846 | 0.6% |
| 15 | 10.01-15.00 | 3865 | 1.0% | 4692 | 1.1% | 4868 | 1.2% | 4872 | 1.2% | 7056 | 1.4% | 7733 | 1.5% | 7750 | 1.5% |
| 20 | 15.01-20.00 | 4359 | 1.1% | 5105 | 1.2% | 5556 | 1.3% | 4915 | 1.2% | 7234 | 1.4% | 8974 | 1.8% | 6504 | 1.3% |
| 25 | 20.01-25.00 | 28136 | 7.3% | 34157 | 8.2% | 37802 | 9.1% | 39490 | 9.5% | 51360 | 10.2% | 65420 | 13.0% | 71930 | 14.1% |
| 30 | 25.01-30.00 | 14053 | 3.6% | 26750 | 6.4% | 23258 | 5.6% | 22197 | 5.3% | 63026 | 12.5% | 49556 | 9.9% | 45463 | 8.9% |
| 35 | 30.01-35.00 | 88827 | 23.0% | 104724 | 25.1% | 106108 | 25.5% | 106660 | 25.5% | 150142 | 29.8% | 155480 | 30.9% | 157612 | 31.0% |
| 40 | 35.01-40.00 | 22993 | 6.0% | 24439 | 5.9% | 24696 | 5.9% | 24934 | 6.0% | 28572 | 5.7% | 29564 | 5.9% | 30480 | 6.0% |
| 45 | 40.01-45.00 | 79868 | 20.7% | 75581 | 18.1% | 70605 | 17.0% | 72381 | 17.3% | 63332 | 12.6% | 44140 | 8.8% | 50988 | 10.0% |
| 50 | 45.01-50.00 | 66085 | 17.1% | 52539 | 12.6% | 53832 | 12.9% | 54645 | 13.1% | 13834 | 2.7% | 18822 | 3.7% | 21960 | 4.3% |
| 55 | 50.01-55.00 | 39173 | 10.2% | 44915 | 10.8% | 45511 | 10.9% | 41483 | 9.9% | 61320 | 12.2% | 63619 | 12.7% | 48083 | 9.4% |
| 60 | 55.01-60.00 | 38039 | 9.9% | 42535 | 10.2% | 43024 | 10.3% | 44607 | 10.7% | 55379 | 11.0% | 57268 | 11.4% | 63374 | 12.4% |
| 65 | 60.01-65.00 | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% |
| 70 | 65.01-70.00 | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% |
| TOTAL | | 385800.19 | 100.0% | 416601.68 | 100.0% | 416075.11 | 100.0% | 417779.48 | 100.0% | 504605.92 | 100.0% | 502574.87 | 100.0% | 509148.88 | 100.0% |

*AM Peak Period is between 5:00 a.m. and 9:00 a.m.

VMT: vehicle miles traveled

Table 3-7. VMT by Speed Bin—PM Peak Period*

| Bin Name | Bin Actual | 2013 | | 2018 No Project | | 2018 Build 1 | | 2018 Build 2 | | 2040 No Build | | 2040 Build 1 | | 2040 Build 2 | |
|----------|-------------|-----------|--------|-----------------|--------|--------------|--------|--------------|--------|---------------|--------|--------------|--------|--------------|--------|
| | | VMT | % | VMT | % | VMT | % | VMT | % | VMT | % | VMT | % | VMT | % |
| 5 | 0.00-5.00 | 293 | 0.1% | 577 | 0.1% | 783 | 0.2% | 941 | 0.2% | 1388 | 0.2% | 2183 | 0.4% | 2795 | 0.5% |
| 10 | 5.01-10.00 | 251 | 0.1% | 1134 | 0.2% | 1105 | 0.2% | 1101 | 0.2% | 3656 | 0.6% | 3545 | 0.6% | 3527 | 0.6% |
| 15 | 10.01-15.00 | 5136 | 1.2% | 7087 | 1.5% | 7009 | 1.5% | 7757 | 1.7% | 12663 | 2.2% | 12359 | 2.2% | 15246 | 2.7% |
| 20 | 15.01-20.00 | 5358 | 1.3% | 11279 | 2.4% | 8687 | 1.9% | 7830 | 1.7% | 28194 | 4.8% | 18199 | 3.2% | 14892 | 2.6% |
| 25 | 20.01-25.00 | 34060 | 8.0% | 60324 | 12.9% | 57483 | 12.4% | 57049 | 12.3% | 135364 | 23.1% | 124405 | 21.9% | 122731 | 21.3% |
| 30 | 25.01-30.00 | 15062 | 3.5% | 27008 | 5.8% | 30406 | 6.6% | 32192 | 6.9% | 61140 | 10.4% | 74247 | 13.1% | 81135 | 14.1% |
| 35 | 30.01-35.00 | 157544 | 37.0% | 158957 | 34.0% | 158170 | 34.2% | 157845 | 34.0% | 162994 | 27.8% | 159958 | 28.1% | 158706 | 27.6% |
| 40 | 35.01-40.00 | 92567 | 21.7% | 82453 | 17.6% | 80275 | 17.3% | 77890 | 16.8% | 53556 | 9.1% | 45157 | 7.9% | 35957 | 6.3% |
| 45 | 40.01-45.00 | 39088 | 9.2% | 35692 | 7.6% | 36547 | 7.9% | 39032 | 8.4% | 25988 | 4.4% | 29287 | 5.2% | 38874 | 6.8% |
| 50 | 45.01-50.00 | 36831 | 8.6% | 30609 | 6.5% | 31729 | 6.9% | 31825 | 6.8% | 12830 | 2.2% | 17152 | 3.0% | 17521 | 3.0% |
| 55 | 50.01-55.00 | 12584 | 3.0% | 17225 | 3.7% | 15374 | 3.3% | 15901 | 3.4% | 30486 | 5.2% | 23346 | 4.1% | 25378 | 4.4% |
| 60 | 55.01-60.00 | 27254 | 6.4% | 35481 | 7.6% | 35366 | 7.6% | 35318 | 7.6% | 58986 | 10.0% | 58545 | 10.3% | 58358 | 10.1% |
| 65 | 60.01-65.00 | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% |
| 70 | 65.01-70.00 | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% |
| TOTAL | | 426027.71 | 100.0% | 467824.69 | 100.0% | 462934.24 | 100.0% | 464681.68 | 100.0% | 587244.6 | 100.0% | 568381.46 | 100.0% | 575121.59 | 100.0% |

*PM Peak Period is between 3:00 p.m. and 7:00 p.m.
VMT: vehicle miles traveled

Table 3-8. VMT by Speed Bin—Non-Peak*

| Bin Name | Bin Actual | 2013 | | 2018 No Project | | 2018 Build 1 | | 2018 Build 2 | | 2040 No Build | | 2040 Build 1 | | 2040 Build 2 | |
|----------|---------------|---------|--------|-----------------|--------|--------------|--------|--------------|--------|---------------|--------|--------------|--------|--------------|--------|
| | | VMT | % | VMT | % | VMT | % | VMT | % | VMT | % | VMT | % | VMT | % |
| 5 | 0.00-5.00 | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% |
| 10 | 5.01-10.00 | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% |
| 15 | 10.01 - 15.00 | 11037 | 1.0% | 15477 | 1.3% | 14926 | 1.3% | 15384 | 1.3% | 28162 | 1.9% | 26036 | 1.8% | 27805 | 1.9% |
| 20 | 15.01-20.00 | 13792 | 1.3% | 15073 | 1.3% | 15263 | 1.3% | 15468 | 1.3% | 18734 | 1.2% | 19467 | 1.3% | 20256 | 1.4% |
| 25 | 20.01-25.00 | 88317 | 8.1% | 111797 | 9.3% | 114091 | 9.6% | 114626 | 9.6% | 178882 | 11.8% | 187731 | 12.8% | 189793 | 12.7% |
| 30 | 25.01-30.00 | 35346 | 3.2% | 35978 | 3.0% | 36751 | 3.1% | 36883 | 3.1% | 37782 | 2.5% | 40767 | 2.8% | 41276 | 2.8% |
| 35 | 30.01-35.00 | 236677 | 21.6% | 266257 | 22.1% | 261711 | 21.9% | 262209 | 21.9% | 350770 | 23.2% | 333236 | 22.6% | 335156 | 22.5% |
| 40 | 35.01-40.00 | 5117 | 0.5% | 6967 | 0.6% | 7178 | 0.6% | 7111 | 0.6% | 12254 | 0.8% | 13067 | 0.9% | 12808 | 0.9% |
| 45 | 40.01-45.00 | 0 | 0.0% | 1227 | 0.1% | 1223 | 0.1% | 1223 | 0.1% | 4731 | 0.3% | 4716 | 0.3% | 4717 | 0.3% |
| 50 | 45.01-50.00 | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% |
| 55 | 50.01-55.00 | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% |
| 60 | 55.01-60.00 | 706296 | 64.4% | 751391 | 62.4% | 742591 | 62.2% | 745355 | 62.2% | 880234 | 58.2% | 846291 | 57.5% | 856952 | 57.6% |
| 65 | 60.01-65.00 | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% |
| 70 | 65.01-70.00 | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% | 0 | 0.0% |
| TOTAL | | 1096582 | 100.0% | 1204166.2 | 100.0% | 1193734 | 100.0% | 1198258.5 | 100.0% | 1511549.4 | 100.0% | 1471311 | 100.0% | 1488762.7 | 100.0% |

*Non-Peak is defined as between 9:00 a.m. and 3:00 p.m., and 7:00 p.m. and 5:00 a.m.
VMT: vehicle miles traveled

Vehicle Emission Rates. Vehicle emission rates were determined using the Caltrans' CT-EMFAC model version 6.0. VMT distribution by speed bin data was prepared by the Project traffic engineers, Fehr & Peers and is presented in Tables 3-6 through 3-8 (see Appendix B). The CT-EMFAC program assumed the San Francisco Bay Area Air Basin Santa Clara County regional traffic data, operating annually. Truck percentages on US 101 and SR 237 were also based on traffic data prepared by the Project traffic engineers, Fehr & Peers (see Appendix B). Appendix A presents the CT-EMFAC emission factor and emission calculation output files.

Carbon Monoxide Modeling Procedures

Roadway and Traffic Conditions. CO hotspots were evaluated at roadway intersections within the Project area. Existing year (2013), opening year (2018) No Build and Build Alternatives 1 and 2, and design-future year (2040) No Build and Build Alternatives 1 and 2 conditions were modeled. Modeled traffic volumes and operating conditions were obtained from the traffic data prepared by the Project traffic engineers, Fehr & Peers (Fehr & Peers 2016b). Ambient CO concentrations near the roadway under future Project conditions were modeled using CALINE4 (Benson 1989). Only the p.m. peak hour traffic was modeled, as the LOS and delays would generally be worse in the p.m. peak hour than in the a.m. peak hour. CO intersection modeling was conducted for the following intersections (under the specified Project build conditions):

- Mathilda Avenue and Moffett Park Drive (Existing and No Build).
- Mathilda Avenue and 237 westbound ramps (Existing and No Build).
- Mathilda Avenue and Moffett Park Drive-237 westbound off-ramp (Build Alternative 1).
- Mathilda Ave and 237 westbound on-ramp (Build Alternative 1).
- Mathilda Ave and 101 northbound ramps (Existing and No Build).
- Mathilda Ave and 101 northbound ramps (Build Alternatives 1 and 2)
- Mathilda Ave and 101 southbound ramps (Existing and No Build).
- Mathilda Ave and 101 southbound ramps (Build Alternatives 1 and 2).
- Mathilda Ave and Almanor Ave-Ahwanee Ave (Existing, No Build and Build Alternatives 1 and 2).
- Innovation Way and Juniper Networks Drive (Existing, No Build and Build Alternatives 1 and 2).
- Bordeaux Drive and Innovation Way (Existing and No Build).
- Bordeaux Drive and Innovation Way (Build Alternatives 1 and 2).

These intersections and segments were chosen because they were identified in the traffic analysis prepared by Fehr & Peers as the greatest impacted intersections and segments (i.e., highest traffic volumes and worst levels of congestion/delay) in the vicinity of the Project area (Fehr & Peers 2016a).

Vehicle Emission Rates. Vehicle emission rates were determined using ARB's EMFAC2014 emission rate program. Traffic speeds were based on data prepared by the Project traffic engineers, Fehr & Peers (see Appendix B). For intersection modeling, free flow traffic speeds were adjusted to a speed of 5.0 mph for vehicles entering and exiting intersection segments to represent a worst-case scenario, as 5.0 mph is the lowest speed EMFAC allows. Modeling procedures followed the guidelines recommended in Appendix B of the CO Protocol (Garza et al. 1997). The program assumed Santa Clara County regional traffic data, averaged for each subarea, operating during the winter months. A mean January temperature of 3.9° Celsius was assumed. Appendix A presents the EMFAC2014 and CALINE4 model output files.

Receptor Locations. For intersection modeling, CO concentrations were estimated at 4 receptor locations located at each of the intersections analyzed, for a total of 48 receptors. The receptors were placed at the edge of the mixing zone from the corner of each intersection, accounting for the intersection dimensions as determined by the number of lanes in each direction. The mixing zone is defined by a 3-meter buffer from the outer edge of a roadway. Receptors were modeled at the edge of the mixing zone to represent a worst-case scenario as the nearest location in which a receptor could potentially be located adjacent to a traveled roadway. The modeled receptors (Receptors 1–48) are not representative of the actual sensitive receptors indicated in Figure 6 and represent receptors located at the nearest possible location at the intersection of the modeled mixing zones. Receptors were chosen based on the CO Protocol (Garza et al. 1997). Receptor heights were set at 5.9 feet (or 1.8 meters).

Meteorological Conditions. Meteorological inputs to the CALINE4 model were determined using methodology recommended in Appendix B of the CO Protocol (Garza et al. 1997). The meteorological conditions used in the modeling represent a calm winter period. Worst-case wind angles were modeled to determine a worst-case concentration for each receptor. The meteorological inputs include: 0.5 meters per second wind speed, ground-level temperature inversion (atmospheric stability class G), wind direction standard deviation equal to 5 degrees, ambient temperature of 3.9° Celsius, and a mixing height of 1,000 meters.

Background Concentrations and 8-Hour Values. To account for sources of CO not included in the modeling, a background concentration of 2.63 ppm was added to the modeled cumulative 1-hour values, while a background concentration of 2.10 ppm was added to the modeled cumulative 8-hour values. Background concentration data for 1- and 8-hour CO values were obtained from the EPA's Air Data webpage (U.S. Environmental Protection Agency 2016). Maximum monitored 1- and 8-hour CO values from the nearest monitoring station with reported CO monitoring values (San Jose) for the years 2012–2014 were averaged to obtain a background concentration. 8-hour modeled values were calculated from the 1-hour values using a persistence factor of 0.7. Background concentrations for opening year (2018) with and without Project, and design-future year (2040) with and without Project conditions were assumed to be the same as those for the current year. Actual 1- and 8-hour background concentrations in future years would likely be lower than those used in the CO modeling analysis because the trend in CO emissions and concentrations is decreasing because of continuing improvements in engine technology and the retirement of older, higher-emitting vehicles.

Construction Impact Assessment Methodology

Construction activity is a source of dust and exhaust emissions that can have substantial temporary impacts on local air quality (i.e., exceeding state air quality standards for ozone, CO, PM10, and PM2.5). Such emissions would result from earthmoving and use of heavy equipment, as well as land clearing, ground excavation, cut-and-fill operations, and roadway construction. Emissions

can vary substantially from day to day, depending on the level of activity, the specific operations, and the prevailing weather. A major portion of dust emissions for the Build Alternatives would likely be caused by construction traffic on temporary areas.

Construction Emissions Modeling

The Road Construction Emissions Model

Construction emissions of ROG, NO_x, CO, PM10, PM2.5, and CO₂ were estimated using the Sacramento Metropolitan Air Quality Management District's Road Construction Emissions Model (Version 7.1.5.1). The road construction model is a public-domain spreadsheet model formatted as a series of individual worksheets available to estimate construction-related emissions for roadway projects. The model enables users to estimate emissions using a minimum amount of project-specific information. The model estimates emissions for load hauling (on-road heavy-duty vehicle trips), worker commute trips, construction site fugitive dust (PM10 and PM2.5), and off-road construction vehicles. This analysis is based on anticipated construction equipment calculated by the Road Construction Emissions Model, which estimates construction equipment based on project size, duration of construction activities, and level of daily construction activities.

While exhaust emissions are estimated for each activity, fugitive dust estimates are currently limited to major dust-generating activities, which include grubbing/land clearing and grading/excavation. In addition, dust estimates do not account for control measures required by BAAQMD.

Construction activity for the Project is expected to occur over 12 months. Model defaults were used to define the phasing of construction activities, with the four phases titled Grubbing/Land Clearing, Grading/Excavation, Drainage/Utilities/Sub-Grade, and Paving. Table 3-9 summarizes the construction phasing assumed in the modeling, including the schedule and primary construction activities. Construction phases would occur sequentially starting in 2018. Table 3-9 identifies the length, area, and soil import/export assumptions for the entire Project. It was assumed that a maximum of 2.5 acres of the phase area would be disturbed on a daily basis. Equipment and vehicles required to construct each phase were developed using model defaults and the Project-specific data summarized in Table 3-9, as well as input from the Project engineers (Lee pers. comm.).

Table 3-9. Construction Modeling Assumptions for Project

| Phase | Activity | Start Year | Months | Length (Miles) | Area (Acres) | Soil (cubic yards per day) |
|-------|------------------------------|------------|--------|----------------|--------------|----------------------------|
| 1 | Grubbing/Land Clearing | | 1.2 | | | |
| 2 | Grading/Excavation | 2018 | 4.8 | 0.85 | 22.00 | 200.00 |
| 3 | Drainage/Utilities/Sub-Grade | | 4.2 | | | |
| 4 | Paving | | 1.8 | | | |

Source: Lee pers. comm.

3.3.2 Impacts

This section discusses air quality impacts that could result from Project implementation.

Conformity of the Regional Transportation Plan with the State Implementation Plan

The Project is listed in the 2015 TIP (TIP ID SCL130001). The 2015 TIP was updated on December 15, 2014, and the approved changes will not impact MTC's financial constraint or the region's air quality conformity. In addition, the Project is listed in the currently conforming 2040 RTP/SCS *Plan Bay Area 2013* Online Project Database as Project ID 240443. Accordingly, the regional emissions modeling that was conducted for the 2040 RTP/SCS ensures that, prior to preparation of the final environmental document for the Project, the design, concept, and scope for the Project will be consistent with the description in the 2040 RTP/SCS and the "open to traffic" assumptions in MTC's regional emissions analysis. The Project's regional conformity determination requirement is satisfied.

Potential Violations of Carbon Monoxide CAAQS

Existing year (2013), opening year (2018) No Build and Build Alternatives, and design-future year (2040) No Build and Build Alternatives conditions were modeled to evaluate CO concentrations relative to the CAAQS. As previously discussed, emissions of CO concentrations are estimated for roadway intersections within the Project area. These roadway intersections and segments were modeled because they represent the roadway intersections and segments in the vicinity of the Project area with the highest traffic volumes and worst levels of congestion/delay. Table 3-10 summarizes the results of the intersection and segment CO modeling, respectively, and indicate that CO concentrations are not anticipated to exceed the 1- or 8- hour CAAQS which are 20 ppm and 9 ppm, respectively, under any of the Build Alternatives or the No-Build Alternative.

Table 3-10. CO Modeling Concentration Results (Parts per Million)

| Intersection | Receptor ^a | Existing (2013) | | Opening Year (2018) No Build | | Opening Year (2018) Build Alternative 1 | | Opening Year (2018) Build Alternative 2 | | Design Year (2040) No Build | | Design Year (2040) Build Alternative 1 | | Design Year (2040) Build Alternative 2 | |
|--|-----------------------|----------------------|----------------------|------------------------------|----------------------|---|----------------------|---|----------------------|-----------------------------|----------------------|--|----------------------|--|----------------------|
| | | 1-hr CO ^b | 8-hr CO ^c | 1-hr CO ^b | 8-hr CO ^c | 1-hr CO ^b | 8-hr CO ^c | 1-hr CO ^b | 8-hr CO ^c | 1-hr CO ^b | 8-hr CO ^c | 1-hr CO ^b | 8-hr CO ^c | 1-hr CO ^b | 8-hr CO ^c |
| 3A. Mathilda Avenue/Moffett Park Drive (Existing/No Build) | 1 | 4.73 | 3.57 | 3.83 | 2.94 | N/A | N/A | N/A | N/A | 3.63 | 2.80 | N/A | N/A | N/A | N/A |
| | 2 | 4.43 | 3.36 | 3.63 | 2.80 | N/A | N/A | N/A | N/A | 3.53 | 2.73 | N/A | N/A | N/A | N/A |
| | 3 | 5.03 | 3.78 | 3.93 | 3.01 | N/A | N/A | N/A | N/A | 3.83 | 2.94 | N/A | N/A | N/A | N/A |
| | 4 | 4.23 | 3.22 | 3.63 | 2.80 | N/A | N/A | N/A | N/A | 3.53 | 2.73 | N/A | N/A | N/A | N/A |
| 3B. Mathilda Ave/SR 237 westbound Ramps (Existing/No Build) | 5 | 4.53 | 3.43 | 4.23 | 3.22 | N/A | N/A | N/A | N/A | 3.83 | 2.94 | N/A | N/A | N/A | N/A |
| | 6 | 5.33 | 3.99 | 3.53 | 2.73 | N/A | N/A | N/A | N/A | 3.53 | 2.73 | N/A | N/A | N/A | N/A |
| | 7 | 5.23 | 3.92 | 4.13 | 3.15 | N/A | N/A | N/A | N/A | 4.03 | 3.08 | N/A | N/A | N/A | N/A |
| | 8 | 5.03 | 3.78 | 3.53 | 2.73 | N/A | N/A | N/A | N/A | 3.63 | 2.80 | N/A | N/A | N/A | N/A |
| 3A. Mathilda Avenue/Moffett Park Drive-SR 237 westbound Off-Ramp (Build Alternative 1) | 9 | N/A | N/A | N/A | N/A | 4.53 | 3.43 | N/A | N/A | N/A | N/A | 4.23 | 3.22 | N/A | N/A |
| | 10 | N/A | N/A | N/A | N/A | 3.73 | 2.87 | N/A | N/A | N/A | N/A | 3.63 | 2.80 | N/A | N/A |
| | 11 | N/A | N/A | N/A | N/A | 4.43 | 3.36 | N/A | N/A | N/A | N/A | 4.03 | 3.08 | N/A | N/A |
| | 12 | N/A | N/A | N/A | N/A | 3.53 | 2.73 | N/A | N/A | N/A | N/A | 3.53 | 2.73 | N/A | N/A |
| 3B. Mathilda Avenue/SR 237 westbound On-Ramp (Build Alternative 1) | 13 | N/A | N/A | N/A | N/A | 4.43 | 3.36 | N/A | N/A | N/A | N/A | 4.13 | 3.15 | N/A | N/A |
| | 14 | N/A | N/A | N/A | N/A | 3.53 | 2.73 | N/A | N/A | N/A | N/A | 3.33 | 2.59 | N/A | N/A |
| | 15 | N/A | N/A | N/A | N/A | 4.53 | 3.43 | N/A | N/A | N/A | N/A | 4.13 | 3.15 | N/A | N/A |
| | 16 | N/A | N/A | N/A | N/A | 3.53 | 2.73 | N/A | N/A | N/A | N/A | 3.43 | 2.66 | N/A | N/A |
| 6. Mathilda Avenue/US 101 northbound Ramps (Existing/No Build) | 17 | 6.53 | 4.83 | 4.83 | 3.64 | N/A | N/A | N/A | N/A | 4.43 | 3.36 | N/A | N/A | N/A | N/A |
| | 18 | 4.53 | 3.43 | 3.73 | 2.87 | N/A | N/A | N/A | N/A | 3.53 | 2.73 | N/A | N/A | N/A | N/A |
| | 19 | 6.33 | 4.69 | 4.73 | 3.57 | N/A | N/A | N/A | N/A | 4.33 | 3.29 | N/A | N/A | N/A | N/A |
| | 20 | 4.83 | 3.64 | 3.83 | 2.94 | N/A | N/A | N/A | N/A | 3.63 | 2.80 | N/A | N/A | N/A | N/A |
| 7. Mathilda Avenue/US 101 southbound Ramps (Existing/No Build) | 21 | 6.63 | 4.90 | 4.93 | 3.71 | N/A | N/A | N/A | N/A | 4.53 | 3.43 | N/A | N/A | N/A | N/A |
| | 22 | 5.23 | 3.92 | 4.13 | 3.15 | N/A | N/A | N/A | N/A | 3.93 | 3.01 | N/A | N/A | N/A | N/A |
| | 23 | 5.63 | 4.20 | 4.33 | 3.29 | N/A | N/A | N/A | N/A | 4.03 | 3.08 | N/A | N/A | N/A | N/A |
| | 24 | 5.03 | 3.78 | 3.93 | 3.01 | N/A | N/A | N/A | N/A | 3.73 | 2.87 | N/A | N/A | N/A | N/A |

| Intersection | Receptor ^a | Existing (2013) | | Opening Year (2018) No Build | | Opening Year (2018) Build Alternative 1 | | Opening Year (2018) Build Alternative 2 | | Design Year (2040) No Build | | Design Year (2040) Build Alternative 1 | | Design Year (2040) Build Alternative 2 | |
|---|-----------------------|----------------------|----------------------|------------------------------|----------------------|---|----------------------|---|----------------------|-----------------------------|----------------------|--|----------------------|--|----------------------|
| | | 1-hr CO ^b | 8-hr CO ^c | 1-hr CO ^b | 8-hr CO ^c | 1-hr CO ^b | 8-hr CO ^c | 1-hr CO ^b | 8-hr CO ^c | 1-hr CO ^b | 8-hr CO ^c | 1-hr CO ^b | 8-hr CO ^c | 1-hr CO ^b | 8-hr CO ^c |
| 6. Mathilda Avenue/US 101 northbound Ramps (Build Alternatives 1 and 2) | 25 | N/A | N/A | N/A | N/A | 4.03 | 3.08 | 3.93 | 3.01 | N/A | N/A | 3.73 | 2.87 | 3.63 | 2.80 |
| | 26 | N/A | N/A | N/A | N/A | 4.03 | 3.08 | 4.03 | 3.08 | N/A | N/A | 3.83 | 2.94 | 3.83 | 2.94 |
| | 27 | N/A | N/A | N/A | N/A | 4.43 | 3.36 | 4.33 | 3.29 | N/A | N/A | 4.13 | 3.15 | 3.93 | 3.01 |
| | 28 | N/A | N/A | N/A | N/A | 4.03 | 3.08 | 3.93 | 3.01 | N/A | N/A | 3.83 | 2.94 | 3.73 | 2.87 |
| 7. Mathilda Avenue/US 101 southbound Ramps (Build Alternatives 1 and 2) | 29 | N/A | N/A | N/A | N/A | 4.83 | 3.64 | 4.83 | 3.64 | N/A | N/A | 4.53 | 3.43 | 4.43 | 3.36 |
| | 30 | N/A | N/A | N/A | N/A | 4.13 | 3.15 | 4.03 | 3.08 | N/A | N/A | 3.93 | 3.01 | 3.93 | 3.01 |
| | 31 | N/A | N/A | N/A | N/A | 4.83 | 3.64 | 4.73 | 3.57 | N/A | N/A | 4.53 | 3.43 | 4.33 | 3.29 |
| | 32 | N/A | N/A | N/A | N/A | 4.03 | 3.08 | 3.93 | 3.01 | N/A | N/A | 3.83 | 2.94 | 3.83 | 2.94 |
| 8. Mathilda Avenue/ Almanor Avenue/ Ahwanee Avenue | 33 | 5.43 | 4.06 | 4.23 | 3.22 | 4.23 | 3.22 | 4.13 | 3.15 | 3.93 | 3.01 | 3.93 | 3.01 | 3.73 | 2.87 |
| | 34 | 5.13 | 3.85 | 4.03 | 3.08 | 4.03 | 3.08 | 4.03 | 3.08 | 3.83 | 2.94 | 3.83 | 2.94 | 3.63 | 2.80 |
| | 35 | 5.63 | 4.20 | 4.33 | 3.29 | 4.33 | 3.29 | 4.23 | 3.22 | 4.03 | 3.08 | 4.03 | 3.08 | 3.73 | 2.87 |
| | 36 | 4.43 | 3.36 | 3.63 | 2.80 | 3.63 | 2.80 | 3.63 | 2.80 | 3.53 | 2.73 | 3.53 | 2.73 | 3.43 | 2.66 |
| 12. Innovation Way/Juniper Networks Drive | 37 | 3.23 | 2.52 | 3.03 | 2.38 | 3.13 | 2.45 | 3.33 | 2.59 | 3.03 | 2.38 | 3.13 | 2.45 | 3.23 | 2.52 |
| | 38 | 3.63 | 2.80 | 3.23 | 2.52 | 3.23 | 2.52 | 3.53 | 2.73 | 3.13 | 2.45 | 3.23 | 2.52 | 3.33 | 2.59 |
| | 39 | 3.33 | 2.59 | 3.13 | 2.45 | 3.13 | 2.45 | 3.33 | 2.59 | 3.13 | 2.45 | 3.23 | 2.52 | 3.33 | 2.59 |
| | 40 | 3.33 | 2.59 | 3.03 | 2.38 | 3.13 | 2.45 | 3.23 | 2.52 | 3.13 | 2.45 | 3.13 | 2.45 | 3.23 | 2.52 |
| 13. Bordeaux Drive/Innovation Way (Existing/No Build) | 41 | 2.93 | 2.31 | 2.83 | 2.24 | N/A | N/A | N/A | N/A | 2.73 | 2.17 | N/A | N/A | N/A | N/A |
| | 42 | 2.83 | 2.24 | 2.73 | 2.17 | N/A | N/A | N/A | N/A | 2.73 | 2.17 | N/A | N/A | N/A | N/A |
| | 43 | 2.93 | 2.31 | 2.83 | 2.24 | N/A | N/A | N/A | N/A | 2.73 | 2.17 | N/A | N/A | N/A | N/A |
| | 44 | 2.83 | 2.24 | 2.73 | 2.17 | N/A | N/A | N/A | N/A | 2.73 | 2.17 | N/A | N/A | N/A | N/A |
| 13. Bordeaux Drive/Innovation Way (Build Alternatives 1 and 2) | 45 | N/A | N/A | N/A | N/A | 3.03 | 2.38 | 3.03 | 2.38 | N/A | N/A | 3.03 | 2.38 | 3.03 | 2.38 |
| | 46 | N/A | N/A | N/A | N/A | 3.13 | 2.45 | 3.13 | 2.45 | N/A | N/A | 3.13 | 2.45 | 3.13 | 2.45 |
| | 47 | N/A | N/A | N/A | N/A | 2.93 | 2.31 | 2.93 | 2.31 | N/A | N/A | 2.93 | 2.31 | 2.93 | 2.31 |
| | 48 | N/A | N/A | N/A | N/A | 3.03 | 2.38 | 3.03 | 2.38 | N/A | N/A | 3.03 | 2.38 | 3.03 | 2.38 |

a Receptors are located at 3 meters from the intersection, at each of the four corners. All intersections modeled have two intersecting roadways.

b Average 1-hour background concentration between 2012 and 2014 was 2.63 ppm (U.S. Environmental Protection Agency 2016).

c Average 8-hour background concentration between 2012 and 2014 was 2.10 ppm (U.S. Environmental Protection Agency 2016).

Potential Violations of PM10 and PM2.5 CAAQS

The EPA's transportation conformity rules stipulate that transportation projects considered a POAQC, or any other project that is identified by the PM2.5 SIP as a localized air quality concern, must be analyzed for local air quality impacts (i.e., hot-spots) in PM2.5 nonattainment and maintenance areas. As previously indicated, Santa Clara County is designated by the ARB as a nonattainment area for the PM10 and PM2.5 CAAQS standard. As previously indicated, the project is not subject to federal NEPA or transportation conformity requirements and interagency consultation through MTC's Air Quality Conformity Task Force is not required for the proposed project, as confirmed by MTC staff (Brazil pers. Comm.). Therefore, a project-level PM10 and PM2.5 analysis using EPA's POAQC guidance is performed to ensure the project would not result in a PM10 nor PM2.5 hot-spot and result in an exceedance of the PM10 or PM2.5 CAAQS.

As discussed in Section 3.2, *Regulatory Setting*, a quantitative hot-spot analysis is only required for projects identified as a POAQC, as defined in 40 CFR 93.123(b)(1). As described below, the Project does not meet any of the project types considered to be POAQC by the EPA's final rule. Accordingly, the Project is not considered to be a POAQC, and project-level particulate matter conformity determination requirements are thus satisfied. While the Project is not subject to PM conformity requirements, Caltrans uses the POAQC analysis process to determine whether the Project would result in a potential PM hot-spot under CEQA.

- (i) **New highway projects that have a significant number of diesel vehicles, and expanded highway projects that have a significant increase in the number of diesel vehicles.** Appendix B from the EPA's *Transportation Conformity Guidance for Quantitative Hot-Spot Analyses in PM2.5 and PM10 Nonattainment and Maintenance Areas* provides guidance on what types of projects may be projects of local air quality concern 40 CFR 93.123(b)(1). Appendix B indicates that a facility with an ADT of 125,000 and 8 percent trucks (10,000 truck ADT) are likely considered a POAQC. The Project would improve operations on Mathilda Avenue through the US 101 and SR 237 interchanges to reduce existing and future traffic congestion. For existing freeway facilities, the effect of a project on truck volumes is normally the main point on which this criterion is judged. Table 3-11 indicates that AADT on the four road segments on and around SR 65 under design year (2040) conditions, which represents the year with maximum AADT, will vary between approximately 51,000 and 65,000 on SR 237 and approximately 87,000 and 102,000 on US 101, depending on the direction of traffic flow. Heavy-duty trucks comprise 3.86 percent of US 101 AADT and 2.95 percent of SR 237 AADT, resulting in a truck AADT of 3,366 to 3,914 on US 101 and 1,520 to 1,913 on SR 237 (Fehr & Peers 2016). Truck percentages on SR 237 and US 101 would remain constant for all years of analysis and for all Build or No Build Alternatives (i.e., the Project would not affect truck percentages between the Build and No Build Alternatives). Truck volumes proportionally increase as total AADT increases with time but predicted truck volumes would be well below the EPA's guidance criteria of 8 percent or 10,000 vehicles per day (maximum truck volume is 3,914). Accordingly, the Build Alternatives would not serve a significant number of diesel vehicles or result in a significant increase in diesel vehicles.
- (ii) **Projects affecting intersections that are at LOS D, E, or F with a significant number of diesel vehicles, or those that will change to LOS D, E, or F because of**

increased traffic volumes from a significant number of diesel vehicles related to the project. Peak-hour LOS and delay at study area intersections under existing (2013), opening (2018), and design year (2040) conditions are presented in Tables 5-2 and 6-1 in the Final Traffic Operations Analysis Report for the Mathilda Avenue Improvements Project (Fehr & Peers 2016a).. Table 5-2 indicates three degradations in opening year LOS between No Build and Build Alternative 1 and four degradations in opening year LOS between No Build and Build Alternative 2. However, Table 5-2 indicates six improvements each in opening year LOS between No Build and Build Alternatives 1 and 2. Table 5-2 also indicates total vehicle hours of delay during the AM peak hour would decrease from 1,319 under opening year No Build conditions to 493 hours and 773 hours for Build Alternative 1 and Build Alternative 2 conditions, respectively. Also, Table 5-2 indicates total vehicle hours of delay during the PM peak hour would decrease from 1,504 under opening year No Build conditions to 1,285 hours and 1,107 hours for Build Alternative 1 and Build Alternative 2 conditions, respectively. Table 6-1 indicates four degradations in design year LOS between No Build and Build Alternative 1 and two degradations in design year LOS between No Build and Build Alternative 2. However, Table 6-1 indicates two improvements in design year LOS between No Build and Build Alternative 1 and zero improvements in design year LOS between No Build and Build Alternative 2. However, Table 6-1 also indicates total vehicle hours of delay during the AM peak hour would decrease from 2,989 under design year No Build conditions to 1,948 hours and 2,582 hours for Build Alternative 1 and Build Alternative 2 conditions, respectively. Also, Table 6-1 indicates total vehicle hours of delay during the PM peak hour would decrease from 3,830 under design year No Build conditions to 3,130 hours and 3,262 hours for Build Alternative 1 and Build Alternative 2 conditions, respectively.

- (iii) **New bus and rail terminals and transfer points that have a significant number of diesel vehicles congregating at a single location.** The Project does not include new bus or rail terminals and transfer points.
- (iv) **Expanded bus and rail terminals and transfer points that significantly increase the number of diesel vehicles congregating at a single location.** The Project does not include expanded bus or rail terminals and transfer points.
- (v) **Projects in or affecting locations, areas, or categories of sites which are identified in the PM2.5 or PM10 applicable implementation plan or implementation plan submission, as appropriate, as sites of violation or possible violation.** Currently, there is no SIP for the federal PM2.5 standard.

Table 3-11. AADT Volumes and Truck Percentages

| Segments | Existing Conditions (2013) | | | Opening Year (2018) | | | Design Year (2040) | | |
|---------------------|----------------------------|--------------|--------------|---------------------|--------------|--------------|--------------------|--------------|--------------|
| | AADT | Truck AADT | % Truck | AADT | Truck AADT | % Truck | AADT | Truck AADT | % Truck |
| US 101 Northbound | 78352 | 3,025 | 3.86% | 80647 | 3,113 | 3.86% | 87205 | 3,367 | 3.86% |
| US 101 Southbound | 75943 | 2,932 | 3.86% | 82541 | 3,187 | 3.86% | 101393 | 3,914 | 3.86% |
| US 101 TOTAL | 154295 | 5,956 | 3.86% | 163188 | 6,300 | 3.86% | 188598 | 7,280 | 3.86% |
| SR 237 Westbound | 60933 | 1,798 | 2.95% | 61945 | 1,828 | 2.95% | 64835 | 1,913 | 2.95% |
| SR 237 Eastbound | 39206 | 1,157 | 2.95% | 42406 | 1,251 | 2.95% | 51547 | 1,521 | 2.95% |
| SR 237 TOTAL | 100139 | 2,955 | 2.95% | 104351 | 3,079 | 2.95% | 116382 | 3,434 | 2.95% |

Source: Brooke pers. comm.
AADT = annual average daily traffic

Based on the discussion above, the Project would not be considered a POAQC, as defined by 40 CFR 93.123(b)(1). Therefore, the Project is not anticipated to result in a PM hot-spot.

Potential for Generation of MSAT Emissions

The area of air toxics analysis is a new and emerging issue and is a continuing area of research. Currently, there are limited tools and techniques available for assessing project-specific health impacts from MSATs, as there are no established criteria for determining when MSAT emissions should be considered a significant issue in the NEPA context.

To comply with Council on Environmental Quality regulations (*40 CFR 1502.22[b]*) regarding incomplete or unavailable information, Appendix C contains discussion regarding how air toxics analysis is an emerging field and current scientific techniques, tools, and data are not sufficient to accurately estimate human health impacts that would result from a transportation project in a way that would be useful to decision-makers. Also in compliance with *40 CFR 150.22(b)*, Appendix C contains a summary of current studies regarding the health impacts of MSATs.

The purpose of this Project is to reduce congestion and improve traffic operations on Mathilda Avenue at SR 237 and US 101 by reconfiguring the US 101 and SR 237 interchanges with Mathilda Avenue. This includes modification to on- and off-ramps; removal, addition, and signalization of intersections; and provision of new left-turn lanes. This Project has been determined to generate minimal air quality impacts for CAAA criteria pollutants and has not been linked with any special MSAT concerns. The Build Alternatives associated with this Project would result in a decrease in traffic volumes when compared to No Build conditions, as shown in Table 3-5, but would not result in changes in vehicle mix, basic project location, or any other factor that would cause an increase in MSAT impacts of the Build Alternatives from that of the No-Build Alternative.

Table 3-12 indicates that implementation of the Build Alternatives would not result in increases in any MSAT emissions under either Build Alternative for 2018 or 2040 conditions when compared to the No Build Alternative. Therefore, this Project would have no meaningful potential MSAT effects.

Moreover, EPA regulations for vehicle engines and fuels will cause overall MSAT emissions to decline significantly over the next several decades. Based on regulations now in effect, an analysis of national trends with the EPA's Motor Vehicle Emissions Simulator model forecasts a combined reduction of over 80 percent in the total annual emission rate for the priority MSAT from 2010 to 2050 while vehicle-miles of travel are projected to increase by over 100 percent. This will both reduce the background level of MSAT as well as the possibility of even minor MSAT emissions from this Project.

Table 3-12. Mathilda Avenue Improvements Project MSAT Emissions (pounds per day)

| Scenario | Naphthalene | Acrolein | Benzene | 1, 3- Butadiene | Formaldehyde | Diesel Particulate Matter | Polycyclic Organic Matter |
|--|-------------|----------|---------|--------------------|--------------|---------------------------------|---------------------------------|
| 2013 Existing | 0 | 0 | 10 | 2 | 16 | 29 | 0 |
| 2018 No-Build Alt | 0 | 0 | 5 | 1 | 6 | 6 | 0 |
| 2018 Build Alt 1 | 0 | 0 | 5 | 1 | 6 | 6 | 0 |
| 2018 Build Alt 2 | 0 | 0 | 5 | 1 | 6 | 6 | 0 |
| 2040 No-Build Alt | 0 | 0 | 3 | 1 | 5 | 1 | 0 |
| 2040 Build Alt 1 | 0 | 0 | 3 | 1 | 5 | 1 | 0 |
| 2040 Build Alt 2 | 0 | 0 | 3 | 1 | 5 | 1 | 0 |
| Comparison of Build Alternatives to Existing Conditions | | | | | | | |
| 2018 No-Build Alt | 0 | 0 | -6 | -1 | -9 | -24 | 0 |
| 2018 Build Alt 1 | 0 | 0 | -6 | -1 | -9 | -24 | 0 |
| 2018 Build Alt 2 | 0 | 0 | -6 | -1 | -9 | -24 | 0 |
| 2040 No-Build Alt | -0.2 | -0.3 | -7.1 | -1.5 | -11.0 | -28.1 | -0.3 |
| 2040 Build Alt 1 | -0.2 | -0.3 | -7.1 | -1.5 | -11.1 | -28.1 | -0.3 |
| 2040 Build Alt 2 | -0.2 | -0.3 | -7.1 | -1.5 | -11.0 | -28.1 | -0.3 |
| Comparison of Build Alternatives to No Build Conditions | | | | | | | |
| 2018 Build Alt 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2018 Build Alt 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2040 Build Alt 1 | 0.0 | 0.0 | -0.1 | 0.0 | -0.1 | 0.0 | 0.0 |
| 2040 Build Alt 2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |

Note: Emissions calculations based on CT-EMFAC v6.0.
Alt = Alternative

Potential for Generation of Operation-Related Emissions of reactive organic gases (ROG), oxides of nitrogen (NO_x), Carbon Monoxide, and Particulate Matter

Long-term air quality impacts are those associated with motor vehicles operating on the roadway network, predominantly those operating in the Project vicinity. Emission of ROG, NO_x, CO, PM10, PM2.5, and CO₂ for existing year (2013), opening year (2018) No Build and Build Alternatives, and design-future year (2040) No Build and Build Alternative Project conditions were evaluated through modeling conducted using Caltrans' CT-EMFAC model and vehicle activity data provided by the Project traffic engineer, Fehr & Peers (see Appendix B).

Table 3-13 summarizes the modeled yearly emissions. The differences in emissions between with- and without-Project conditions represent emissions generated directly as a result of implementation of the Build Alternatives. Vehicular emission rates are anticipated to lessen in future years due to continuing improvements in engine technology and the retirement of older, higher-emitting vehicles.

Table 3-13. Mathilda Avenue Improvements Project-Related Criteria Pollutant Emissions (pounds per day)

| Scenario | ROG | NO _x | CO | PM10 | PM2.5 |
|--|------|-----------------|--------|------|-------|
| 2013 Existing | 313 | 2,070 | 7,727 | 243 | 117 |
| 2018 No-Build Alternative | 147 | 977 | 3,991 | 237 | 101 |
| 2018 Build Alternative 1 | 147 | 970 | 3,962 | 235 | 100 |
| 2018 Build Alternative 2 | 148 | 975 | 3,980 | 236 | 101 |
| 2040 No-Build Alternative | 100 | 350 | 2,217 | 283 | 115 |
| 2040 Build Alternative 1 | 98 | 343 | 2,169 | 277 | 113 |
| 2040 Build Alternative 2 | 100 | 351 | 2,200 | 280 | 114 |
| Comparison of Build Alternatives to Existing | | | | | |
| 2018 No-Build Alternative | -166 | -1,093 | -3,737 | -6 | -16 |
| 2018 Build Alternative 1 | -166 | -1,100 | -3,765 | -8 | -17 |
| 2018 Build Alternative 2 | -165 | -1,096 | -3,747 | -7 | -16 |
| 2040 No-Build Alternative | -213 | -1,720 | -5,511 | 40 | -2 |
| 2040 Build Alternative 1 | -215 | -1,727 | -5,558 | 34 | -5 |
| 2040 Build Alternative 2 | -213 | -1,719 | -5,527 | 37 | -3 |
| Comparison of Build Alternatives to No Build Conditions | | | | | |
| 2018 Build Alternative 1 | 0 | -7 | -28 | -2 | -1 |
| 2018 Build Alternative 2 | 1 | -2 | -10 | -1 | 0 |
| 2040 Build Alternative 1 | -2 | -7 | -47 | -7 | -3 |
| 2040 Build Alternative 2 | 0 | 1 | -17 | -3 | -1 |
| <i>BAAQMD Threshold</i> | 54 | 54 | - | 82 | 54 |

Note: Emissions calculations based on CT-EMFAC v6.0.

Emissions associated with implementation of the Project were obtained by comparing future with-Project emissions to future without-Project emissions for both the opening year (2018) and design-future year (2040) scenarios. Because Caltrans has statewide jurisdiction, and the setting for projects varies so extensively across the state, Caltrans has not and has no intention to develop thresholds of significance for CEQA. Further, because most air district thresholds have not been established by regulation or by delegation down from a federal or state agency with regulatory authority over Caltrans, Caltrans is not required to adopt those thresholds in Caltrans' documents. Nevertheless, Project-level operational emissions are presented in Table 3-13. BAAQMD's adopted thresholds of significance for Project-level operational-related criteria pollutant emissions are presented for informational purposes.

In 2018, Build Alternatives 1 and 2 would result in decreases in all pollutants compared to existing conditions. Compared to No Build conditions in 2018, Build Alternative 1 shows a decrease in all pollutants, except for no change in ROG emissions. Build Alternative 2 would result in a slight increase in ROG emissions, no change in PM2.5 emissions, and decreases in NO_x, CO, and PM10 emissions.

In 2040, Build Alternatives 1 and 2 would result in decreases in all pollutants, except for an increase in PM10 emissions, compared to existing conditions. Compared to No Build conditions in 2040, Build Alternative 1 shows a decrease in all pollutants while Alternative 2 would result in a slight increase in NO_x emissions, no change in ROG emissions and decreases in CO, PM10, and PM2.5 emissions.

Potential for Temporary Increase in Ozone Precursors (ROG and NO_x), CO, and PM₁₀ Emissions during Grading and Construction Activities

Implementation of all Build Alternatives would result in the construction of widened and reconfigured roads as well as intersection improvements. Temporary construction emissions would result from grubbing/land clearing, grading/excavation, drainage/utilities/subgrade construction, and paving activities and construction worker commuting patterns. Pollutant emissions would vary daily, depending on the level of activity, specific operations, and prevailing weather.

The Sacramento Metropolitan Air Quality Management District's Road Construction Emissions Model (Version 7.1.5.1) was used to estimate construction-related ozone precursors ROG and NO_x, CO, PM₁₀, PM_{2.5}, and CO₂ emissions from construction activities. Construction is expected to begin in 2018 with a construction period lasting approximately 12 months. It was assumed that construction activities would occur for 8 hours per day over this period. The total Project length was assumed to be 0.85 miles, and total area of disturbed ground for either Build Alternative was assumed to be 22 acres. The maximum amount of acreage disturbed per day was assumed to be 2.5 acres. It was also assumed that 200 cubic yards of soil per day would be imported with an average haul truck capacity of 10 cubic yards.

The emissions shown in Table 3-14 assume no concurrent construction activities. To provide a realistic, yet conservative scenario, maximum daily emissions were estimated assuming all equipment would operate at the same time during the individual construction phases. Because of this conservative assumption, actual emissions could be less than those forecasted. If construction is delayed or occurs over a longer time period, emissions could be reduced because of (1) a more modern and cleaner burning construction equipment fleet mix, and/or (2) a less intensive build-out schedule (i.e., fewer daily emissions occurring over a longer time interval).

Table 3-14 summarizes maximum daily emissions levels for the proposed construction year 2018. Because Caltrans has statewide jurisdiction, and the setting for projects varies so extensively across the state, Caltrans has not and has no intention to develop thresholds of significance for CEQA. Further, because most air district thresholds have not been established by regulation or by delegation down from a federal or state agency with regulatory authority over Caltrans, Caltrans is not required to adopt those thresholds in Caltrans' documents. Nevertheless, BAAQMD thresholds of significance are provided for reference.

Table 3-14. Worst-Case Construction Emission Estimates (pounds per day)

| Project Phases | ROG | CO | NO _x | Total | | Fugitive | | Fugitive | |
|------------------------------------|-----|------|-----------------|-------|--------------|-----------|-------------|---------------|------------|
| | | | | PM10 | Exhaust PM10 | Dust PM10 | Total PM2.5 | Exhaust PM2.5 | Dust PM2.5 |
| Grubbing/Land Clearing | 1.4 | 11.0 | 15.4 | 25.7 | 0.7 | 25.0 | 5.8 | 0.6 | 5.2 |
| Grading/Excavation | 8.4 | 50.9 | 96.0 | 29.5 | 4.5 | 25.0 | 9.2 | 4.0 | 5.2 |
| Drainage/Utilities/Sub-Grade | 4.7 | 28.6 | 43.5 | 27.5 | 2.5 | 25.0 | 7.4 | 2.2 | 5.2 |
| Paving | 2.1 | 14.8 | 19.1 | 1.2 | 1.2 | - | 1.1 | 1.1 | - |
| Maximum (pounds/day) | 8.4 | 50.9 | 96.0 | 29.5 | 4.5 | 25.0 | 9.2 | 4.0 | 5.2 |
| BAAQMD Threshold | 54 | - | 54 | - | 82 | BMPs | - | 54 | BMPs |
| Total (tons/ construction project) | 0.7 | 4.4 | 7.7 | 3.2 | 0.4 | 2.8 | 0.9 | 0.3 | 0.6 |

ROG = reactive organic acids; CO = carbon monoxide; NO_x = oxides of nitrogen; PM = particulate matter; BMPs = best management practices

Construction activities are subject to requirements found in the *Standard Specifications for Construction of Local Streets and Roads* (California Department of Transportation 2010), Section 14-9.02, which includes specifications relating to air pollution control by complying with air pollution control rules, regulations, ordinances, and statutes that apply to work performed under the contract, including air pollution control rules, regulations, ordinances, and statutes provided in Government Code Section 11017 (Public Contract Code §10231) while standard specification Section 14-9.03 addresses dust control and palliative requirements. Implementation of Caltrans' standard specification and measures to control dust during construction would help to minimize air quality impacts from construction activities.

Naturally Occurring Asbestos

According to the California Department of Conservation's 2000 publication, *A General Location Guide for Ultramafic Rock in California*, there are no geologic features normally associated with naturally occurring asbestos (i.e., serpentine rock or ultramafic rock near fault zones) in or near the Project area (California Department of Conservation 2000). As such, there is no potential for impacts related to naturally occurring asbestos emissions during construction activities. However, construction activities that involve the demolition of any building or structure containing asbestos would be subject to the EPA's National Emissions Standards for Hazardous Air Pollutants and ARB's Airborne Toxic Control Measures.

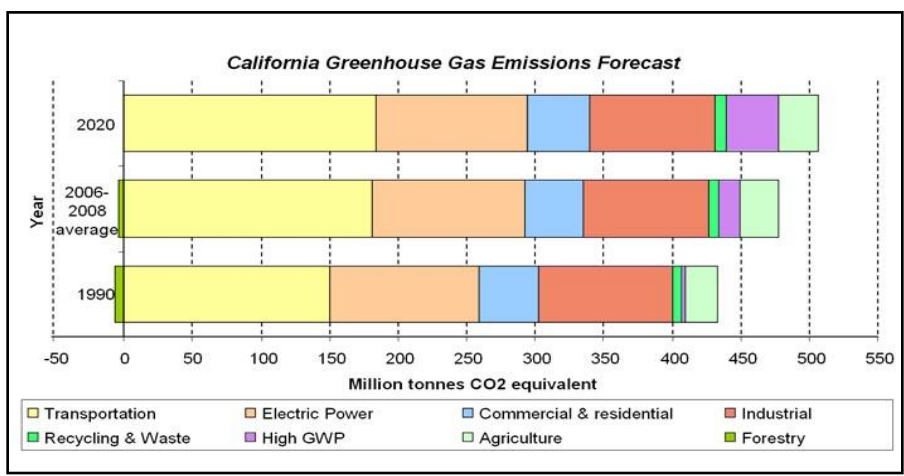
Potential for Generation of Greenhouse Gas Emissions

An individual project does not generate enough GHG emissions to significantly influence global climate change. Rather, global climate change is a cumulative impact. This means that a project may participate in a potential impact through its incremental contribution combined with the contributions of all other sources of GHG.¹⁰ In assessing cumulative impacts, it must be determined

¹⁰ This approach is supported by the AEP: Recommendations by the Association of Environmental Professionals on How to Analyze GHG Emissions and Global Climate Change in CEQA Documents (March

if a project's incremental effect is "cumulatively considerable" (see CEQA Guidelines sections 15064(h)(1) and 15130). To make this determination the incremental impacts of the project must be compared with the effects of past, current, and probable future projects. To gather sufficient information on a global scale of all past, current, and future projects in order to make this determination is a difficult if not impossible task.

The [AB 32](#) Scoping Plan contains the main strategies California will use to reduce GHG. As part of its supporting documentation for the Draft Scoping Plan, ARB released the GHG inventory for California (Forecast last updated: 28 October 2010) (Figure 8). The forecast is an estimate of the emissions expected to occur in the year 2020 if none of the foreseeable measures included in the Scoping Plan were implemented. The base year used for forecasting emissions is the average of statewide emissions in the GHG inventory for 2006, 2007, and 2008.



Source: <http://www.arb.ca.gov/cc/inventory/data/forecast.htm>

Figure 8. California Greenhouse Gas Forecast

Caltrans and its parent agency, the Business, Transportation, and Housing Agency, have taken an active role in addressing GHG emission reduction and climate change. Recognizing that 98 percent of California's GHG emissions are from the burning of fossil fuels and 40 percent of all human made GHG emissions are from transportation, the Department has created and is implementing the Climate Action Program at Caltrans that was published in December 2006 (see Climate Action Program at Caltrans, December 2006).¹¹

3.3.3 Operational Emissions

Future year GHG emissions associated with implementation of the Project were obtained by comparing future with-Project emissions to future no-Project emissions for both the opening (2018) and design (2040) years. It is important to note that CO₂ emissions are useful only for a comparison between Build Alternatives. The numbers are not necessarily an accurate reflection of what the true CO₂ emissions will be because CO₂ emissions are dependent on factors that are not part

5, 2007), as well as the SCAQMD (Chapter 6: The CEQA Guide, April 2011) and the US Forest Service (Climate Change Considerations in Project Level NEPA Analysis, July 13, 2009).

¹¹ Caltrans Climate Action Program is located at the following web address: http://www.dot.ca.gov/hq/tpp/offices/ogm/key_reports_files/State_Wide_Strategy/Caltrans_Climate_Action_Program.pdf

of the emissions model, such as the fuel mix¹², rate of acceleration, and the aerodynamics and efficiency of the vehicles.

Future year GHG emissions associated with implementation of the Build Alternatives were obtained by comparing future with-Project emissions to future no-Project emissions for both the opening (2018) and design (2040) years. Table 3-15 presents Project-level emissions and indicates that under 2018 and 2040 conditions implementation of the Build Alternatives is anticipated to result in decreases in CO₂ emissions when compared to the future No Build conditions. These increases are attributed to decreases in VMT between the no-Project and with-Project conditions.

Table 3-15. Estimated Greenhouse Gas Emissions from Operation of Mathilda Avenue Improvements Project (metric tons per year)

| Year | Annual VMT | Emissions | | |
|-------------------------------|-------------|-----------------|--------------------|-------------------|
| | | CO ₂ | Other ^a | CO ₂ e |
| 2013 Baseline | 662,218,242 | 266,191 | 13,310 | 279,501 |
| 2018 No-Build Alternative | 724,741,607 | 250,062 | 12,503 | 262,565 |
| 2018 Build Alternative 1 | 719,241,931 | 248,217 | 12,411 | 260,628 |
| 2018 Build Alternative 2 | 722,009,718 | 249,446 | 12,472 | 261,919 |
| 2040 No-Build Alternative | 903,379,794 | 211,441 | 10,572 | 222,014 |
| 2040 Build Alternative 1 | 882,166,756 | 206,746 | 10,337 | 217,083 |
| 2040 Build Alternative 2 | 892,842,508 | 209,850 | 10,493 | 220,343 |
| Comparison to Existing | | | | |
| 2018 No-Build Alternative | 62,523,365 | -16,129 | -806 | -16,936 |
| 2018 Build Alternative 1 | 57,023,689 | -17,974 | -899 | -18,873 |
| 2018 Build Alternative 2 | 59,791,476 | -16,745 | -837 | -17,582 |
| 2040 No-Build Alternative | 241,161,552 | -54,750 | -2,737 | -57,487 |
| 2040 Build Alternative 1 | 219,948,514 | -59,445 | -2,972 | -62,417 |
| 2040 Build Alternative 2 | 230,624,266 | -56,341 | -2,817 | -59,158 |
| Comparison to No Build | | | | |
| 2018 Build Alternative 1 | -5,499,676 | -1,845 | -92 | -1,937 |
| 2018 Build Alternative 2 | -2,731,889 | -615 | -31 | -646 |
| 2040 Build Alternative 1 | -21,213,037 | -4,695 | -235 | -4,930 |
| 2040 Build Alternative 2 | -10,537,286 | -1,591 | -80 | -1,671 |

^a Includes methane (CH₄), nitrous oxide (N₂O), and other trace GHGs emissions emitted by typical passenger vehicles (U.S. Environmental Protection Agency 2015).
CO₂e = carbon dioxide equivalent

MTC's 2040 RTP includes performance objectives to reduce per-capita delay while improving roadway safety. As indicated in the EIR prepared for MTC's 2040 RTP, the RTP would help to reduce congestion by reducing vehicle hours of delay and increasing average network speed. If implemented, the Project would be consistent with the RTP in this regards as it is anticipated to help to reduce congestion by reducing vehicle hours of delay and increasing average network speed. The Project also includes various mitigation measures, detailed below, that will reduce the Project's GHG's emissions.

¹² EMFAC model emission rates are only for direct engine-out CO₂ emissions, not for full fuel cycle. In addition, fuel cycle emission rates can vary dramatically depending on the amount of additives, such as ethanol, and the source of the fuel components.

Transportation accounts for 40 percent of the Bay Area's GHG emissions. The MTC understands the urgent need to address climate change. The MTC coordinates regional planning efforts with the BAAQMD, Association of Bay Area Governments, the Bay Conservation and Development Commission, as part of the Joint Policy Committee. The Transportation Climate Action Campaign within the Joint Policy Committee seeks to enable climate friendly behaviors, reduce the Bay Area's carbon footprint, and lay the groundwork for ongoing future climate change initiatives . (MTC 2016).

In late 2009, MTC programmed \$80 million over a 3-year period to implement the Climate Initiatives Program. In partnership with the BAAQMD, MTC is developing a region-wide campaign for the Climate Initiatives Public Outreach Program to reduce transportation-related GHG emissions through a public education and branding campaign that will educate and encourage the public to make transportation choices that reduce GHG emissions.

The EIR for the 2040 RTP states that while increases in VMT over the planning period are contributing somewhat to the significant cumulative impact of global climate change, the Project's contribution to the significant cumulative impact of global climate change is not cumulatively considerable. MTC's RTP identifies four criteria related to the emissions of GHGs to determine if the RTP would have a potentially significant adverse impact.

1. Fail to reduce per capita passenger vehicle and light duty truck CO₂ emissions by seven percent by 2020 and by 15 percent by 2035 as compared to 2005 baseline, per SB 375.

The RTP was found to be consistent with SB 375, as modeled CO₂ emissions met the SB 375 targeted reductions for per capita car and light duty truck emissions. In fact, the RTP was found to result in greater emission reductions than the SB 375 targets.

2. Result in a net increase in direct and indirect GHG emissions in 2040 when compared to existing conditions.

Forecast GHG emissions are expected to decline with the implementation of the RTP when considering scoping plan reductions for electricity and natural gas, recycling and waste, and implementation of Pavley and the LCFS regulations. Overall emissions in 2040 are expected to be less than under existing conditions.

3. Substantially impede attainment of goals set forth in EO S-3-05 and EO B-16-2012.

Because the goals of EOs S-3-05 and B-16-2012 are more than 35 years into the future, the RTP assessment considered the following factors:

- Per capita car and light duty truck emissions decline from 2005 through 2040, and are expected to continue to decline into the future;
- Total GHG emissions from land use and transportation are expected to decline from 2010 through 2040, and are expected to continue to decline into the future;
- New innovations in technology and science are expected, along with continued market shift towards green building and zero emission vehicles; and
- The RTP and SCS must be updated every 4 years, providing frequent opportunities to reevaluate progress towards executive order achievement. Therefore, the Bay Area is heading in the direction of achieving the executive order goals, and does not impede achievement of these identified goals.

4. Substantially conflict with any other applicable plan, policy or regulation adopted for the purpose of reducing the emissions of GHGs.

The RTP was found to be consistent with state goals and mandates. Further, it is not expected that the RTP would conflict with local CAPs or GHG reduction plans as they are complimentary efforts towards the reduction of GHG emissions in line with state goals and mandates. Therefore, the RTP is expected to be consistent with other GHG reduction plans.

Within the RTP are various funded regional policy efforts that address the Bay Area's contribution to global climate change, including the Bay Area Regional Agency Climate Protection Program, the Transportation Climate Action Campaign, and the Bay Area 2010 Clean Air Plan.

MTC, as part of their mitigation, commits to working with the Association of Bay Area Governments, the Bay Conservation and Development Commission, and the BAAQMD, through the Joint Policy Committee, to develop green construction policies and best practices that encourage that will reduce impacts related to GHG emissions. Individual projects carried out as part of the RTP shall consider adopting appropriate best practice measures (BMPs) that would minimize or eliminate cumulatively considerable impacts related to climate change. BMPs may include using alternative fueled (e.g., biodiesel, electric) construction vehicles/equipment for at least 15 percent of the fleet; using local building materials for at least 10 percent; and recycling or reusing at least 50 percent of construction waste or demolition materials. One of the main strategies in the Department's Climate Action Program to reduce GHG emissions is to make California's transportation system more efficient. Consistent with Caltrans requirements, a discussion of how the modal choice for the project was made in the early planning phases of the project is included as part of this analysis. There were 18 initial interchange alternatives considered in order to reduce congestion and GHG emissions through increased efficiency of the local transportation system. Project alternatives were screened based on the ability of each alternative to meet the Project's defined purpose and need, potential for environmental impacts, cost, and ability to provide adequate traffic operation improvements. Transportation Demand Management, Transportation System Management, and Mass Transit alternatives were considered but eliminated from further discussion because the Build Alternatives already include measures to improve accessibility for other modes of travel (bicycle and pedestrian facilities) and would improve traffic signal coordination. Furthermore, implementation of other measures typically included as part of Transportation Demand Management and Transportation System Management alternatives, as well as a stand-alone Mass Transit alternative, would not meet the Project purpose and need.

3.3.4 Construction Emissions

Construction GHG emissions include emissions produced as a result of material processing, emissions produced by on-site construction equipment, and emissions arising from traffic delays due to construction. The Sacramento Metropolitan Air Quality Management District's Road Construction Emissions Model (Version 7.1.5.1) was used to estimate CO₂ emissions from construction activities. The Road Construction Emissions Model does not include emission factors for CH₄ or nitrous oxide (N₂O) for off-road diesel equipment. Emissions of CH₄ and N₂O from diesel-powered equipment were determined by scaling the CO₂ emissions quantified by the ratio of CH₄/CO₂ (0.000056) and N₂O/CO₂ (0.000025) (Climate Registry 2015).

Table 3-16 summarizes estimated GHG emissions generated by on-site construction equipment over the 12-month construction period. These emissions would be produced at different levels throughout the construction phase; their frequency and occurrence can be reduced through inno-

variations in plans and specifications and by implementing better traffic management during construction phases. In addition, with innovations such as longer pavement lives, improved traffic management plans, and changes in materials, the GHG emissions produced during construction can be mitigated to some degree by longer intervals between maintenance and rehabilitation events. Measures to reduce construction emissions include maintenance of construction equipment and vehicles, limiting of construction vehicle idling time, and scheduling and routing of construction traffic to reduce engine emissions.

While there are minor short-term construction-related GHG emissions, the operational analysis indicates the Project would result in a net decrease in GHG emissions (Table 3-15) that would ultimately offset these temporary increases in construction GHG emissions.

Table 3-16. GHG Emissions from Construction of Project (metric tons per year)

| Diesel Equipment | | | |
|------------------|-----------------|------------------|-------------------|
| CO ₂ | CH ₄ | N ₂ O | CO ₂ e |
| 971.1 | 0.05 | 0.02 | 977.8 |

CO₂ = carbon dioxide; CH₄ = methane; N₂O = nitrous oxide; CO₂e = carbon dioxide equivalent

3.3.5 AB 32 Compliance

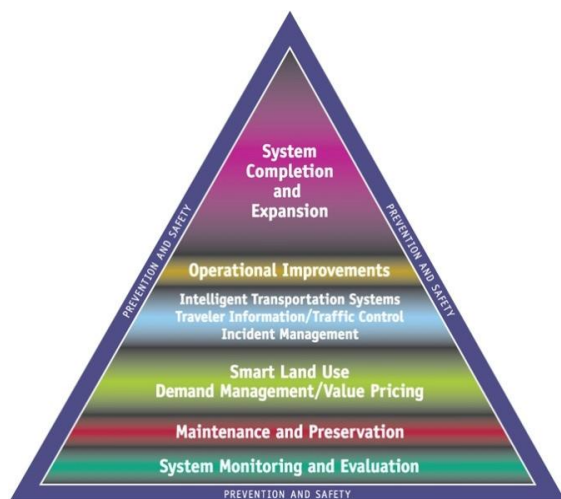


Figure 9: Mobility Pyramid

Caltrans continues to be involved on the Governor's Climate Action Team as the ARB works to implement EOs S-3-05 and S-01-07 and help achieve the targets set forth in AB 32. Many of the strategies Caltrans is using to help meet the targets in AB 32 come from Former Governor Arnold Schwarzenegger's Strategic Growth Plan for California. The Strategic Growth Plan targeted a significant decrease in traffic congestion below 2008 levels and a corresponding reduction in GHG emissions, while accommodating growth in population and the economy. The Strategic Growth Plan relies on a complete systems approach to attain CO₂ reduction goals: system monitoring and evaluation, maintenance and preservation, smart land use and demand management, and operational improvements as shown in **Figure 9: The Mobility Pyramid**.

Caltrans is supporting efforts to reduce vehicle miles traveled by planning and implementing smart land use strategies: job/housing proximity, transit-oriented communities, and high-density housing along transit corridors. Caltrans works closely with local jurisdictions on planning activities, but does not have local land use planning authority. Caltrans also assists efforts to improve the energy efficiency of the transportation sector by increasing vehicle fuel economy in new cars, light and heavy-duty trucks; Caltrans is doing this by supporting on-going research efforts at universities, by supporting legislative efforts to increase fuel economy, and by participating on the Climate Action Team. It is important to note, however, that control of fuel economy standards is held by the EPA and ARB.

Caltrans is also working towards enhancing the state's transportation planning process to respond to future challenges. Similar to requirements for RTPs under SB 375 (Steinberg 2008), SB 391

(Liu 2009) requires the state's long-range transportation plan to meet California's climate change goals under AB 32.

The California Transportation Plan is a statewide, long-range transportation plan to meet our future mobility needs and reduce GHG emissions. The California Transportation Plan defines performance-based goals, policies, and strategies to achieve our collective vision for California's future, statewide, integrated, multimodal transportation system.

The purpose of the California Transportation Plan is to provide a common policy framework that will guide transportation investments and decisions by all levels of government, the private sector, and other transportation stakeholders. Through this policy framework, the California Transportation Plan 2040 will identify the statewide transportation system needed to achieve maximum feasible GHG emission reductions while meeting the state's transportation needs.

Table 3-17 summarizes Caltrans and other statewide efforts that it is implementing to reduce GHG emissions. More detailed information about each strategy is included in the [Climate Action Program at Caltrans](#) (December 2006).

Caltrans Director's Policy 30 Climate Change (June 22, 2012) is intended to establish a policy that will ensure coordinated efforts to incorporate climate change into Caltrans decisions and activities.

Caltrans Activities to Address Climate Change (April 2013)¹³ provides a comprehensive overview of activities undertaken by Caltrans statewide to reduce GHG emissions resulting from agency operations.

The following measures will also be included in the Project to reduce the GHG emissions and potential climate change impacts from the Project:

1. Landscaping reduces surface warming and, through photosynthesis, decreases CO₂. The Project proposes replanting to the extent feasible where existing landscaping occurs. All areas of ground disturbance due to construction activities will receive permanent erosion control utilizing native seeds and plants. If trees cannot be replaced within the Project site, in-lieu fees will be paid to an appropriate fund so that trees can be planted elsewhere within the City of Sunnyvale limits. These trees will help offset any potential CO₂ emissions increase.
2. According to Caltrans Standard Specifications, the contractor must comply with all local Air Pollution Control District's rules, ordinances, and regulations for air quality restrictions. BAAQMD recommends idling times shall be minimized either by shutting equipment off when not in use or reducing the maximum idling time to 5 minutes (as required by the California airborne toxics control measure Title 13, Section 2485 of California Code of Regulations [CCR]). Clear signage shall be provided for construction workers at all access points.

¹³ http://www.dot.ca.gov/hq/tpp/offices/orip/climate_change/projects_and_studies.shtml

Table 3-17. Climate Change/Carbon Dioxide (CO₂) Reduction Strategies

| Strategy | Program | Partnership | | Method/Process | Estimated CO ₂ Savings Million Metric Tons | |
|--|--|--|--|--|--|---------------|
| | | Lead | Agency | | 2010 | 2020 |
| Smart Land Use | Intergovernmental Review | Caltrans | Local governments | Review and seek to mitigate development proposals | Not Estimated | Not Estimated |
| | Planning Grants | Caltrans | Local and regional agencies & other stakeholders | Competitive selection process | Not Estimated | Not Estimated |
| | Regional Plans and Blueprint Planning | Regional Agencies | Caltrans | Regional plans and application process | 0.975 | 7.8 |
| Operational Improvements & Intelligent Transportation System Deployment | Strategic Growth Plan | Caltrans | Regions | State Intelligent Transportation System; Congestion Management Plan | 0.07 | 2.17 |
| Mainstream Energy & Greenhouse Gas into Plans and Projects | Office of Policy Analysis & Research; Division of Environmental Analysis | Interdepartmental effort | | Policy establishment, guidelines, technical assistance | Not Estimated | Not Estimated |
| Educational & Information Program | Office of Policy Analysis & Research | Interdepartmental, California Environmental Protection Agency, Programmatic Agreement, Air Resources Board (ARB), California Energy Commission | | Analytical report, data collection, publication, workshops, outreach | Not Estimated | Not Estimated |
| Fleet Greening & Fuel Diversification | Division of Equipment | Department of General Services | | Fleet Replacement | 0.0045 | 0.0065 |
| | | | | Biodiesel (B) 20 | | 0.045 |
| | | | | B100 | | 0.0225 |
| Non-vehicular Conservation Measures | Energy Conservation Program | Green Action Team | | Energy Conservation Opportunities | 0.117 | 0.34 |
| Portland Cement | Office of Rigid Pavement | Cement and Construction Industries | | 2.5% limestone cement mix | 1.2 | 4.2 |
| | | | | 25% fly ash cement mix > 50% fly ash/slag mix | 0.36 | 3.6 |
| Goods Movement | Office of Goods Movement | California Environmental Protection Agency, ARB, Business, Transportation and Housing Agency, Metropolitan Planning Organizations | | Goods Movement Action Plan | Not Estimated | Not Estimated |
| Total | | | | | 2.72 | 18.18 |

3.3.6 Adaptation Strategies

Adaptation strategies refer to how Caltrans and others can plan for the effects of climate change on the state's transportation infrastructure and strengthen or protect the facilities from damage. Climate change is expected to produce increased variability in precipitation, rising temperatures, rising sea levels, variability in storm surges and intensity, and the frequency and intensity of wild-fires. These changes may affect the transportation infrastructure in various ways, such as damage to roadbeds from longer periods of intense heat; increasing storm damage from flooding and erosion; and inundation from rising sea levels. These effects will vary by location and may, in the most extreme cases, require that a facility be relocated or redesigned. There may also be economic and strategic ramifications as a result of these types of impacts on the transportation infrastructure.

At the federal level, the Climate Change Adaptation Task Force, co-chaired by the Council on Environmental Quality, the Office of Science and Technology Policy, and the National Oceanic and Atmospheric Administration, released its interagency task force progress report on October 28, 2011¹⁴, outlining the federal government's progress in expanding and strengthening the Nation's capacity to better understand, prepare for, and respond to extreme events and other climate change impacts. The report provides an update on actions in key areas of federal adaptation, including: building resilience in local communities, safeguarding critical natural resources such as freshwater, and providing accessible climate information and tools to help decision-makers manage climate risks.

Climate change adaptation must also involve the natural environment as well. Efforts are underway on a statewide-level to develop strategies to cope with impacts on habitat and biodiversity through planning and conservation. The results of these efforts will help California agencies plan and implement mitigation strategies for programs and projects.

On November 14, 2008, then-Governor Arnold Schwarzenegger signed EO S-13-08 which directed a number of state agencies to address California's vulnerability to sea level rise caused by climate change. This EO set in motion several agencies and actions to address the concern of sea level rise.

In addition to addressing projected sea level rise, the California Natural Resources Agency (Resources Agency) was directed to coordinate with local, regional, state and federal public and private entities to develop [The California Climate Adaptation Strategy](#) (Dec 2009)¹⁵, which summarizes the best-known science on climate change impacts on California, assesses California's vulnerability to the identified impacts, and then outlines solutions that can be implemented within and across state agencies to promote resiliency.

The strategy outline is in direct response to [EO S-13-08](#) that specifically asked the Resources Agency to identify how state agencies can respond to rising temperatures, changing precipitation patterns, sea level rise, and extreme natural events. Numerous other state agencies were involved in the creation of the Adaptation Strategy document, including the California Environmental Protection Agency; Business, Transportation and Housing; Health and Human Services; and the Department of Agriculture. The document is broken down into strategies for different sectors that include: Public Health; Biodiversity and Habitat; Ocean and Coastal Resources; Water Management; Agriculture; Forestry; and Transportation and Energy Infrastructure. As data continues to

¹⁴ <http://www.whitehouse.gov/administration/eop/ceq/initiatives/adaptation>

¹⁵ <http://www.energy.ca.gov/2009publications/CNRA-1000-2009-027/CNRA-1000-2009-027-F.PDF>

be developed and collected, the state's adaptation strategy will be updated to reflect current findings.

The National Academy of Science was directed to prepare a Sea Level Rise Assessment Report¹⁶ to recommend how California should plan for future sea level rise. The report was released in June 2012 and included:

- Relative sea level rise projections for California, Oregon, and Washington taking into account coastal erosion rates, tidal impacts, El Niño and La Niña events, storm surge and land subsidence rates.
- The range of uncertainty in selected sea level rise projections.
- A synthesis of existing information on projected sea level rise impacts on state infrastructure (such as roads, public facilities and beaches), natural areas, and coastal and marine ecosystems.
- A discussion of future research needs regarding sea level rise.

In 2010, interim guidance was released by The Coastal Ocean Climate Action Team as well as Caltrans as a method to initiate action and discussion of potential risks to the states infrastructure due to projected sea level rise. Subsequently, the Coastal Ocean Climate Action Team updated the Sea Level Rise guidance to include information presented in the National Academies Study.

All state agencies that are planning to construct projects in areas vulnerable to future sea level rise are directed to consider a range of sea level rise scenarios for the years 2050 and 2100 to assess project vulnerability and, to the extent feasible, reduce expected risks and increase resiliency to sea level rise. Sea level rise estimates should also be used in conjunction with information on local uplift and subsidence, coastal erosion rates, predicted higher high water levels, storm surge and storm wave data

All projects that have filed a Notice of Preparation as of the date of the EO S-13-08, and/or are programmed for construction funding through 2013, or are routine maintenance projects may, but are not required to, consider these planning guidelines. The Project is outside the coastal zone and direct impacts on transportation facilities due to projected sea-level rise are not expected.

EO S-13-08 also directed the Business, Transportation, and Housing Agency to prepare a report to assess vulnerability of transportation systems to sea level rise affecting safety, maintenance and operational improvements of the system, and economy of the state. Caltrans continues to work on assessing the transportation system vulnerability to climate change, including the effect of sea level rise.

Currently, Caltrans is working to assess which transportation facilities are at greatest risk from climate change effects. However, without statewide planning scenarios for relative sea level rise and other climate change effects, Caltrans has not been able to determine what change, if any, may be made to its design standards for its transportation facilities. Once statewide planning scenarios become available, Caltrans will be able review its current design standards to determine what changes, if any, may be needed to protect the transportation system from sea level rise.

¹⁶ *Sea Level Rise for the Coasts of California, Oregon, and Washington: Past, Present, and Future* (2012) is available at: http://www.nap.edu/catalog.php?record_id=13389.

Climate change adaptation for transportation infrastructure involves long-term planning and risk management to address vulnerabilities in the transportation system from increased precipitation and flooding; the increased frequency and intensity of storms and wildfires; rising temperatures; and rising sea levels. Caltrans is an active participant in the efforts being conducted in response to EO S-13-08 and is mobilizing to be able to respond to the National Academy of Science Sea Level Rise Assessment Report.

3.4 Avoidance, Minimization, and/or Mitigation Measures

Implement California Department of Transportation Standard Specification Section 14

To control the generation of construction-related air pollutants and dust, the Project proponent will follow Standard Specification Section 14, “Environmental Stewardship,” which addresses the contractor’s responsibility on many items of concern, such as air pollution; protection of lakes, streams, reservoirs, and other water bodies; use of pesticides; safety; sanitation; convenience for the public; and damage or injury to any person or property as a result of any construction operation. Section 14-9.02, which includes specifications relating to air pollution control by complying with air pollution control rules, regulations, ordinances, and statutes that apply to work performed under the contract, including air pollution control rules, regulations, ordinances, and statutes provided in Government Code Section 11017 (Public Contract Code Section 10231). Section 14-9.03 is directed at controlling dust.

Implement Basic and Additional Control Measures for Construction Emissions of Fugitive Dust

Additional measures to control dust required by the BAAQMD (see Table 3-18) shall be implemented to the extent practicable when the measures have not already been incorporated and do not conflict with requirements of Caltrans’s Standard Specifications, Special Provisions, National Pollutant Discharge Elimination System permit, and the Biological Opinions, Clean Water Act Section 404 permit, Clean Water Act Section 401 Certification, and other permits issued for the Project.

Table 3-18. BAAQMD Feasible Control Measures for Construction Emissions of Particulate Matter

| Basic Construction Mitigation Measures Recommended for ALL Projects | |
|--|--|
| 1. | All exposed surfaces (e.g., parking areas, staging areas, soil piles, graded areas, and unpaved access roads) shall be watered two times per day. |
| 2. | All haul trucks transporting soil, sand, or other loose material off-site shall be covered. |
| 3. | All visible mud or dirt track-out onto adjacent public roads shall be removed using wet power vacuum street sweepers at least once per day. The use of dry power sweeping is prohibited. |
| 4. | All vehicle speeds on unpaved roads shall be limited to 15 mph. |
| 5. | All roadways, driveways, and sidewalks to be paved shall be completed as soon as possible. Building pads shall be laid as soon as possible after grading unless seeding or soil binders are used. |
| 6. | Post a publicly visible sign with the telephone number and person to contact at the lead agency regarding dust complaints. This person shall respond and take corrective action within 48 hours. The Air District’s phone number shall also be visible to ensure compliance with applicable regulations. |

Additional Construction Mitigation Measures Recommended for Projects with Construction Emissions Above the Threshold

1. All exposed surfaces shall be watered at a frequency adequate to maintain minimum soil moisture of 12%. Moisture content can be verified by lab samples or moisture probe.
2. All excavation, grading, and/or demolition activities shall be suspended when average wind speeds exceed 20 mph.
3. Wind breaks (e.g., trees, fences) shall be installed on the windward side(s) of actively disturbed areas of construction. Wind breaks should have at maximum 50% air porosity.
4. Vegetative ground cover (e.g., fast-germinating native grass seed) shall be planted in disturbed areas as soon as possible and watered appropriately until vegetation is established.
5. The simultaneous occurrence of excavation, grading, and ground-disturbing construction activities on the same area at any one time shall be limited. Activities shall be phased to reduce the amount of disturbed surfaces at any one time.
6. All trucks and equipment, including their tires, shall be washed off prior to leaving the site.
7. Site accesses to a distance of 100 feet from the paved road shall be treated with a 6- to 12-inch compacted layer of wood chips, mulch, or gravel.
8. Sandbags or other erosion control measures shall be installed to prevent silt runoff to public roadways from sites with a slope greater than 1%.

Source: Bay Area Air Quality Management District 2011.

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Chapter 4 – References

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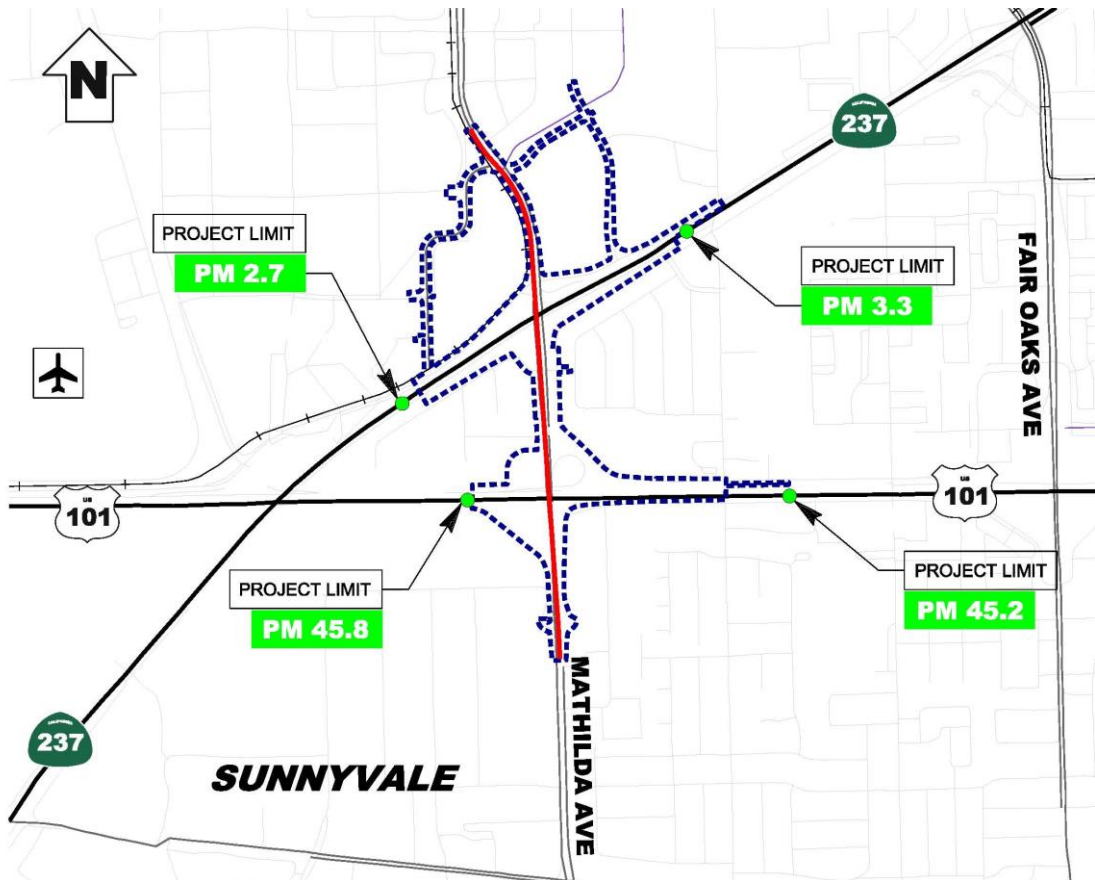
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Community Impact Assessment

for the

MATHILDA AVENUE IMPROVEMENTS AT SR 237 AND US 101 PROJECT



Prepared for:

Santa Clara Valley Transportation Authority
California Department of Transportation
District 4

Prepared by:

ICF, International

Dated: May 2016

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Community Impact Assessment

for the

MATHILDA AVENUE IMPROVEMENTS AT S R 237 AND US 101 PROJECT

on Mathilda Avenue from Almanor Avenue to Innovation Way; on SR 237 from 0.3 mile south of US 101/SR 237 Junction to 0.3 mile east of Mathilda Avenue Undercrossing; and on US 101 from 0.3 mile south of Mathilda Avenue to SR 237/US 101/SR 237 Junction in the City of Sunnyvale, Santa Clara County

SCL-237-PM 2.7/3.3; SCL-101-PM 45.2/45.8
EA 04-4H2900/Project ID 0413000204

May 2016

CALIFORNIA DEPARTMENT OF TRANSPORTATION
and

Cooperating Agency: Santa Clara Valley Transportation Authority

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Statement of Compliance: Produced in compliance with California Environmental Quality Act (CEQA) requirements, as appropriate, to meet the level of analysis and documentation that has been determined necessary for this project.

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List of Acronyms and Abbreviations

| | |
|--------------|---|
| ABAG | Association of Bay Area Governments |
| Caltrans | California Department of Transportation |
| CEQA | California Environmental Quality Act |
| CIA | Community Impact Assessment |
| CT | census tract |
| DDI | Diverging Diamond Interchange |
| EIR | Environmental Impact Report |
| General Plan | City of Sunnyvale's General Plan |
| HOV | high-occupancy vehicle |
| I-880 | Interstate 880 |
| ICF | ICF International |
| LRT | light-rail transit |
| mph | miles per hour |
| PG&E | Pacific Gas & Electric |
| PM | post mile |
| Project | Mathilda Avenue Improvements at SR 237 and US 101 Project |
| ROW | right-of-way |
| SR 237 | State Route 237 |
| TCE | temporary construction easement |
| TMP | Traffic Management Plan |
| US 101 | U.S. Highway 101 |
| VTA | Santa Clara Valley Transportation Authority |

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Chapter 1 – Executive Summary

The purpose of this Community Impact Assessment (CIA) is to evaluate community impacts as a result of the Mathilda Avenue Improvements at SR 237 and US 101 Project (Project). This CIA was prepared by ICF International (ICF) with review and approval by the California Department of Transportation (Caltrans). This document is intended to serve as a supporting technical memorandum for the Project's Environmental Impact Report (EIR).

This CIA follows the guidance provided in Caltrans' Standard Environmental Reference, including the *Community Impact Assessment Standard Environmental Reference: Environmental Handbook Volume 4* (Caltrans 2011), and the CIA work plan prepared in September 2015.

Under the California Environmental Quality Act (CEQA), an economic or social change by itself is not to be considered a significant effect on the environment. However, if a social or economic change is related to a physical change, then a social or economic change may be considered in determining whether the physical change is significant. Since this Project would result in physical change to the environment, it is appropriate to consider changes to community character and cohesion in assessing the significance of the Project's effects.

As discussed in the following chapters, the Project would not result in long-term adverse impacts on the population or communities within the Project study area. Generally, the adverse impacts resulting from the Project would be temporary and related to construction delays and detours. The majority of the Project would be constructed within existing Caltrans and City of Sunnyvale right-of-way (ROW) with one partial permanent ROW acquisition required from the Sheraton Hotel at 1108 N. Mathilda Avenue. Upon completion of construction, the Project would result in beneficial impacts on the community by easing existing congestion and providing enhanced pedestrian and bicycle access, which would result in improved connection to community centers and businesses.

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Chapter 2 – Project Description

2.1 Introduction

Caltrans, in cooperation with the Santa Clara Valley Transportation Authority (VTA) and the City of Sunnyvale, is proposing the “Mathilda Avenue Improvements at SR 237 and US 101 Project” (Project) to improve Mathilda Avenue in the City of Sunnyvale from Almanor Avenue/Ahwanee Avenue to Innovation Way, including on- and off-ramp improvements at the State Route (SR) 237/Mathilda Avenue and U.S. Highway 101 (US 101)/Mathilda Avenue interchanges. On SR 237, the Project limits are from 0.3 mile east of the US 101/SR 237 interchange (post mile [PM] 2.7) to 0.3 mile east of the Mathilda Avenue undercrossing (PM 3.3). On US 101, the Project limits are from 0.5 mile south of Mathilda Avenue overcrossing (PM 45.2) to 0.3 mile south of SR 237/US 101 interchange (PM 45.8). The total length of the Project on Mathilda Avenue is approximately one mile. **Figure 1** shows the location of the Project.

The Project is subject to state environmental review requirements and is being prepared in compliance with CEQA. Caltrans is the lead agency under CEQA. The Project is included in the 2015 Federal Statewide Transportation Improvement Program (ID No. SCL130001). The Project is included in the Metropolitan Transportation Commission *Plan Bay Area*, adopted July 18, 2013 (Project No. 240554). The Project is also identified in the VTA’s Valley Transportation Plan 2040 under ID H43 and in the City of Sunnyvale’s Capital Improvement Program for Fiscal Year 2013/2014 as Project No. 826890.

The City has committed local funding to the development of the Project. Other funding sources have yet to be determined, but may include a combination of state and/or local transportation funds.

2.2 Project Background

The SR 237/Mathilda Avenue and US 101/Mathilda Avenue interchanges are primary access points on the state highway system for the City of Sunnyvale and important local destinations, such as downtown Sunnyvale, the Sunnyvale Caltrain station to the south, and an expanding high-tech business district to the north. The Project is also located within the “Golden Triangle,” an area bordered by US 101, SR 237, and Interstate 880 (I-880) that includes parts of Sunnyvale, Santa Clara, North San Jose, and Milpitas. The Golden Triangle is named for the high concentration of employment centers within this area. US 101, SR 237, and I-880 are heavily used commute corridors to destinations within and beyond the Golden Triangle.

2.2.1 Mathilda Avenue

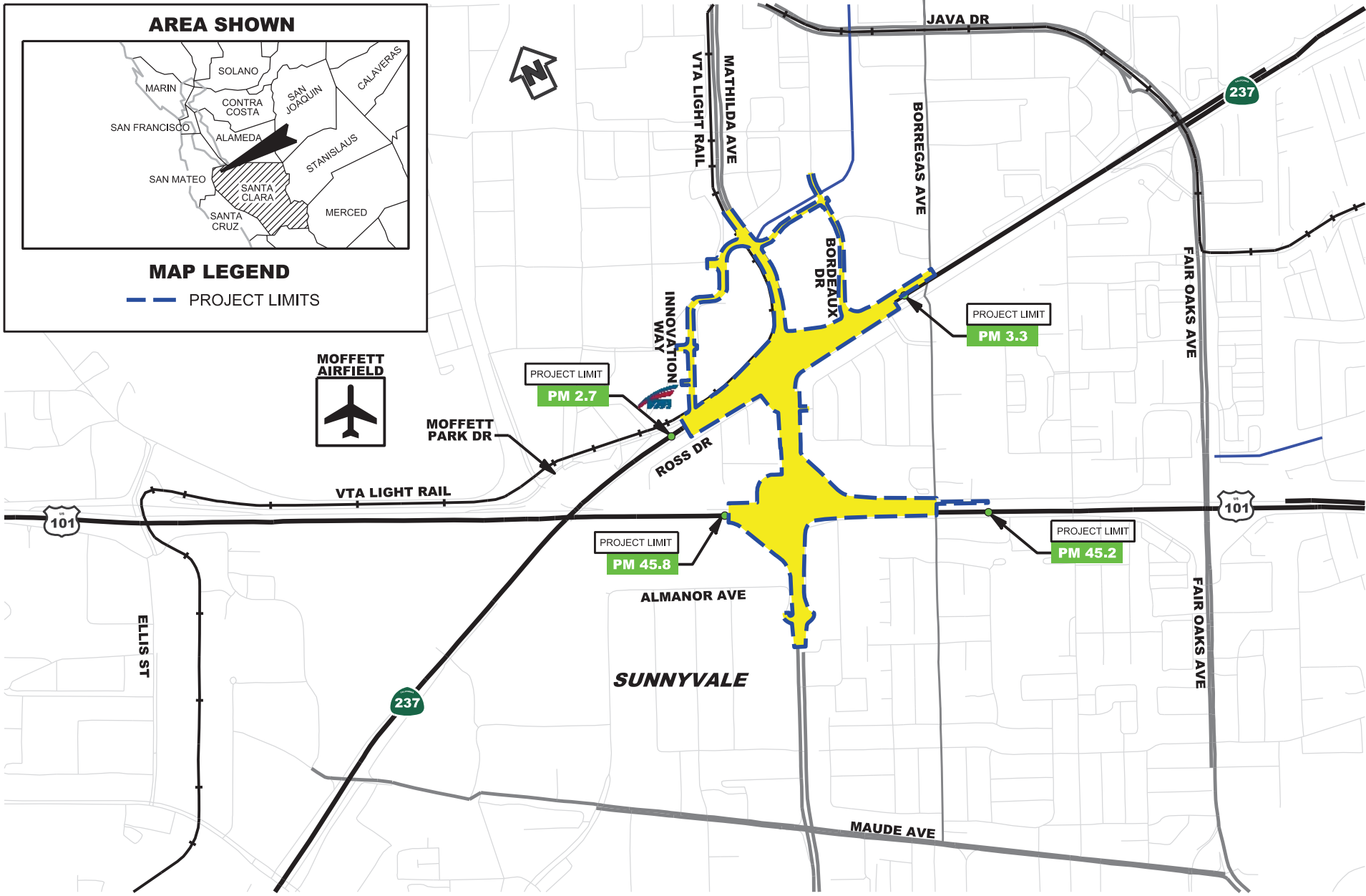
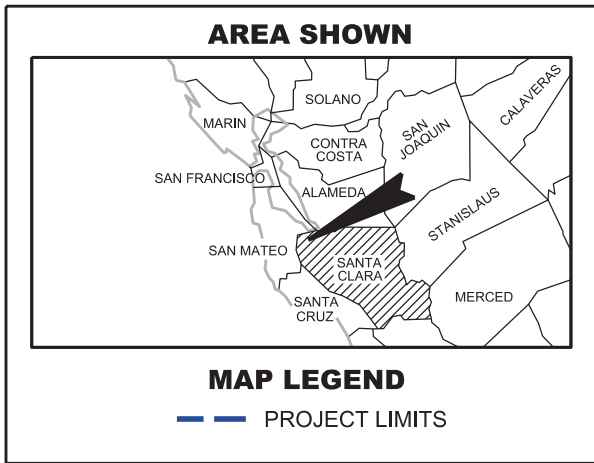
Within the Project area, Mathilda Avenue is a six-lane divided local roadway. Mathilda Avenue serves as the main access route to residential communities on the east side of Mathilda Avenue and is the only access route to the landlocked area within the US 101/SR 237/Mathilda Avenue triangle via Ross Drive. Mathilda Avenue is also one of City of Sunnyvale’s designated truck routes for trucks that weigh more than three tons. The speed limit is 45 miles per hour (mph). On-street parking is prohibited within the Project area. Approximately 45,000 vehicles travel on Mathilda Avenue south of SR 237 on an average weekday.

Existing congestion and delay on Mathilda Avenue within the Project area is associated with the following roadway deficiencies:

- Four closely spaced signalized intersections along Mathilda Avenue (Ross Drive, eastbound SR 237 ramp termini, westbound SR 237 ramp termini, and Moffett Park Drive) at and adjacent to the SR 237 interchange provide inadequate storage for queuing vehicles, and limited green time for conflicting turning movements.
- Uncontrolled ramp movements at the US 101 interchange ramps at Mathilda Avenue and their close proximity to signalized intersections (Ross Drive and Almanor Avenue/Ahwanee Avenue) provide limited distance for traffic to move into the desired lane of travel. This is further exacerbated by queues during peak periods at adjacent signalized intersections. Furthermore, the distribution of queues across available travel lanes is uneven, since some turning movement volumes are heavier than others.
- The US 101/SR 237 interchange to the west of the Project area does not provide for all turning movements. As a result, Mathilda Avenue carries both local and regional (freeway) traffic in both directions between US 101 and SR 237. Westbound SR 237 to southbound US 101 drivers utilize southbound Mathilda Avenue, and northbound US 101 to eastbound SR 237 drivers utilize northbound Mathilda Avenue.
- The US 101/Mathilda Avenue interchange does not provide for all turning movements. As a result, southbound Mathilda Avenue to northbound US 101 and southbound US 101 to northbound Mathilda Avenue drivers shift to the SR 237/Mathilda Avenue interchange or other routes.
- Southbound Mathilda Avenue reduces from three lanes to two lanes between Ross Drive and the northbound US 101 loop off-ramp merge lane, which results in a bottleneck for through traffic.
- The northbound US 101 loop ramps have a cloverleaf configuration. The short distance between the ramps results in traffic entering and exiting the freeway at much slower speeds, and this in turn affects freeway operations.

High levels of traffic congestion and inefficient operations adversely affect pedestrian, bicycle, and transit access within the Project area. Existing bicycle and pedestrian facilities in the area include the following deficiencies:

- No sidewalk or crosswalks along the west side of Mathilda Avenue are provided at the following locations:
 - Between Almanor Avenue/Ahwanee Avenue and the southbound US 101 off-ramp.
 - Between the northbound US 101 loop-off-ramp and Moffett Park Drive.
- Crosswalks at the US 101 ramps along the west side of Mathilda Avenue are not signalized.
- Using the crosswalk south of Ross Drive to access bus stops on both sides of Mathilda Avenue is a safety concern for local residents, particularly for the elderly and children.



November 2015



Prepared By:
WMH

Mathilda Avenue Improvement at SR 237 and US 101

PROJECT LOCATION MAP

Figure
1

- No designated bicycle facilities are provided along Mathilda Avenue in the Project area.
- Bicycle lanes on Moffett Park Drive between Bordeaux Drive and Innovation Way are discontinuous.

2.2.2 SR 237

SR 237 (Calaveras Boulevard) east of I-880 is primarily a six-lane divided roadway. Within the Project area, SR 237 provides two mixed-flow lanes in each direction. On eastbound SR 237, a high-occupancy vehicle (HOV) lane is provided east of Mathilda Avenue, which becomes an HOV/express lane from east of Zanker Road to the eastbound SR 237/northbound I-880 direct connector ramp. On westbound SR 237, an HOV/express lane that begins at the southbound I-880/westbound SR 237 direct connector ramp becomes an HOV lane from North First Street to just east of Fair Oaks Avenue. Within the Project area, auxiliary lanes are provided in each direction between US 101 and Mathilda Avenue on SR 237. There is also an auxiliary lane on westbound SR 237 between Fair Oaks Avenue and Mathilda Avenue. SR 237 is a link for trucking between the southern part of the San Francisco Peninsula and the East Bay, providing the first connection south of the Dumbarton Bridge. SR 237 east of Mathilda Avenue currently carries approximately 90,000 vehicles daily.

The SR 237/Mathilda Avenue interchange is a full “tight” diamond interchange¹ that accommodates all ramp movements, with access to and from east and westbound SR 237. All ramp termini are signalized. The westbound SR 237 on-ramp has existing ramp metering equipment installed; however, there is no existing ramp metering equipment installed for the eastbound SR 237 on-ramp.

2.2.3 US 101

Within the Project area, US 101 provides three mixed-flow lanes plus one HOV lane in each direction, while an auxiliary lane is also provided in the southbound direction between SR 237 and Mathilda Avenue. US 101 south of Mathilda Avenue currently carries approximately 154,000 vehicles daily.

The Moffett Park Drive/US 101 northbound on-ramp is a one-lane on-ramp, located along Moffett Park Drive west of the Mathilda Avenue/Moffett Park Drive intersection. This on-ramp merges with the westbound SR 237 off-ramp that connects to northbound US 101. The ramp terminus is signalized, and the on-ramp is not metered.

The US 101/Mathilda Avenue interchange is a partial cloverleaf interchange with access to all but two movements: southbound Mathilda Avenue to northbound US 101 and southbound US 101 to northbound Mathilda Avenue. None of the ramp termini are signalized; however, all of the on-ramps are metered.

¹A full “tight” diamond interchange, also known as a compressed diamond interchange, has two closely spaced signalized intersections at the crossing of the freeway/highway ramp terminals (in this case, SR 237) and the side street (in this case, Mathilda Avenue). This interchange type is typically used in urban and suburban areas where ROW is a constraint.

2.2.4 Transit Facilities in the Project Area

Two VTA light rail transit (LRT) stations, Moffett Park and Lockheed Martin, are located within the Project area and serve the business district north of SR 237. VTA also operates a local bus service with four bus stops on Mathilda Avenue. The Sunnyvale Caltrain Station is located in downtown Sunnyvale, adjacent to West Evelyn Avenue.

2.3 Project Purpose and Need

The primary purpose of the Project is to improve traffic operations on Mathilda Avenue through the US 101 and SR 237 interchanges. Due to the close proximity of the SR 237 and US 101 interchanges (less than one mile), modification of one interchange would affect the other.

Specifically, the purposes of the Project are to:

- Reduce congestion and improve traffic operations along Mathilda Avenue and at the SR 237/Mathilda Avenue and US 101/Mathilda Avenue interchanges.
- Improve mobility for all travel modes in the area, including motor vehicles, transit, bicycles, and pedestrians.
- Provide standard crosswalks and sidewalks along Mathilda Avenue, improving access to local destinations such as Moffett Park, the VTA LRT stations, and downtown Sunnyvale.

The Project is needed for the following reasons:

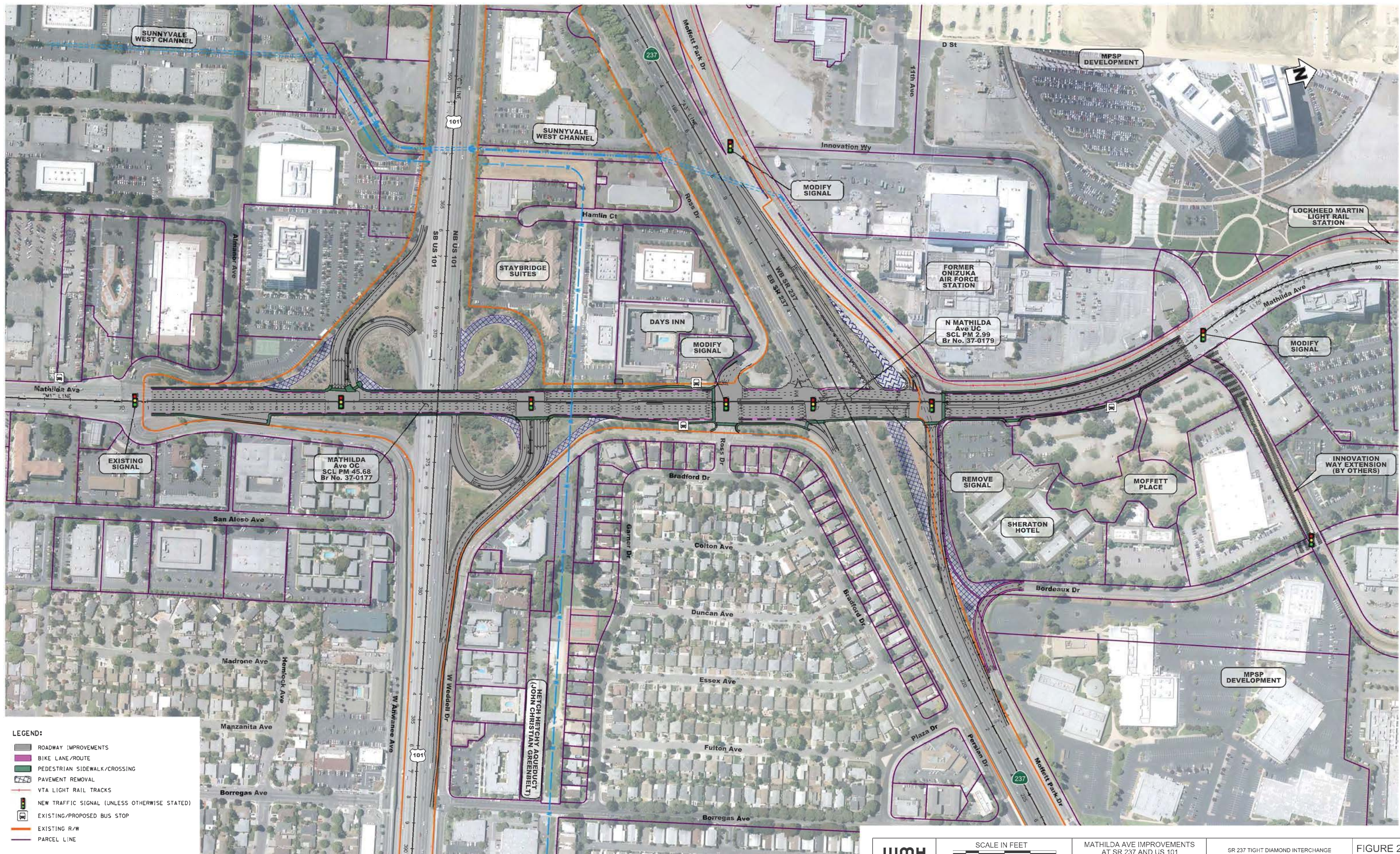
- Regional growth and new local development, combined with inefficient roadway operations, have resulted in substantial traffic congestion on Mathilda Avenue; and
- Efficient access for all travel modes into and out of downtown Sunnyvale and development to the north of SR 237 is critical to a healthy and sustainable economy. Congestion on Mathilda Avenue adversely affects the economic vitality of the City of Sunnyvale.

Overall, the Project is needed to address several issues in the Project area, including roadway deficiencies, lack of or discontinuous bicycle and pedestrian access, improvement of local roadway and freeway ramp operations, and provision of access to current and future economic development.

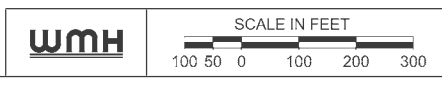
2.4 Project Alternatives

The Project alternatives that were developed to meet the purpose and need of the Project include Alternative 1 (refer to **Figure 2a**), Alternative 2 (refer to **Figure 2b**), and the No-Build Alternative. The Build Alternatives would provide for all turning movements on Mathilda Avenue at the US 101 and SR 237 interchanges. No new freeway connections are proposed. No modifications to existing structures are required to accommodate the proposed Project improvements. Under the No-Build Alternative, no changes would be made to the existing local roadway or freeway ramps within the Project limits. No construction activities would occur, and there would be no change in the operation of existing facilities.

The design features of the two Build Alternatives include reconfiguration of the US 101 and SR 237 interchanges at Mathilda Avenue. The Build Alternatives include design variations for reconfigured roadways and intersections as well as the construction of new signalized intersections. Proposed improvements included in both Build Alternatives south of Ross Drive along Mathilda



- LEGEND:**
- ROADWAY IMPROVEMENTS
 - BIKE LANE/ROUTE
 - PEDESTRIAN SIDEWALK/CROSSING
 - PAVEMENT REMOVAL
 - VTA LIGHT RAIL TRACKS
 - NEW TRAFFIC SIGNAL (UNLESS OTHERWISE STATED)
 - EXISTING/PROPOSED BUS STOP
 - EXISTING R/W
 - PARCEL LINE

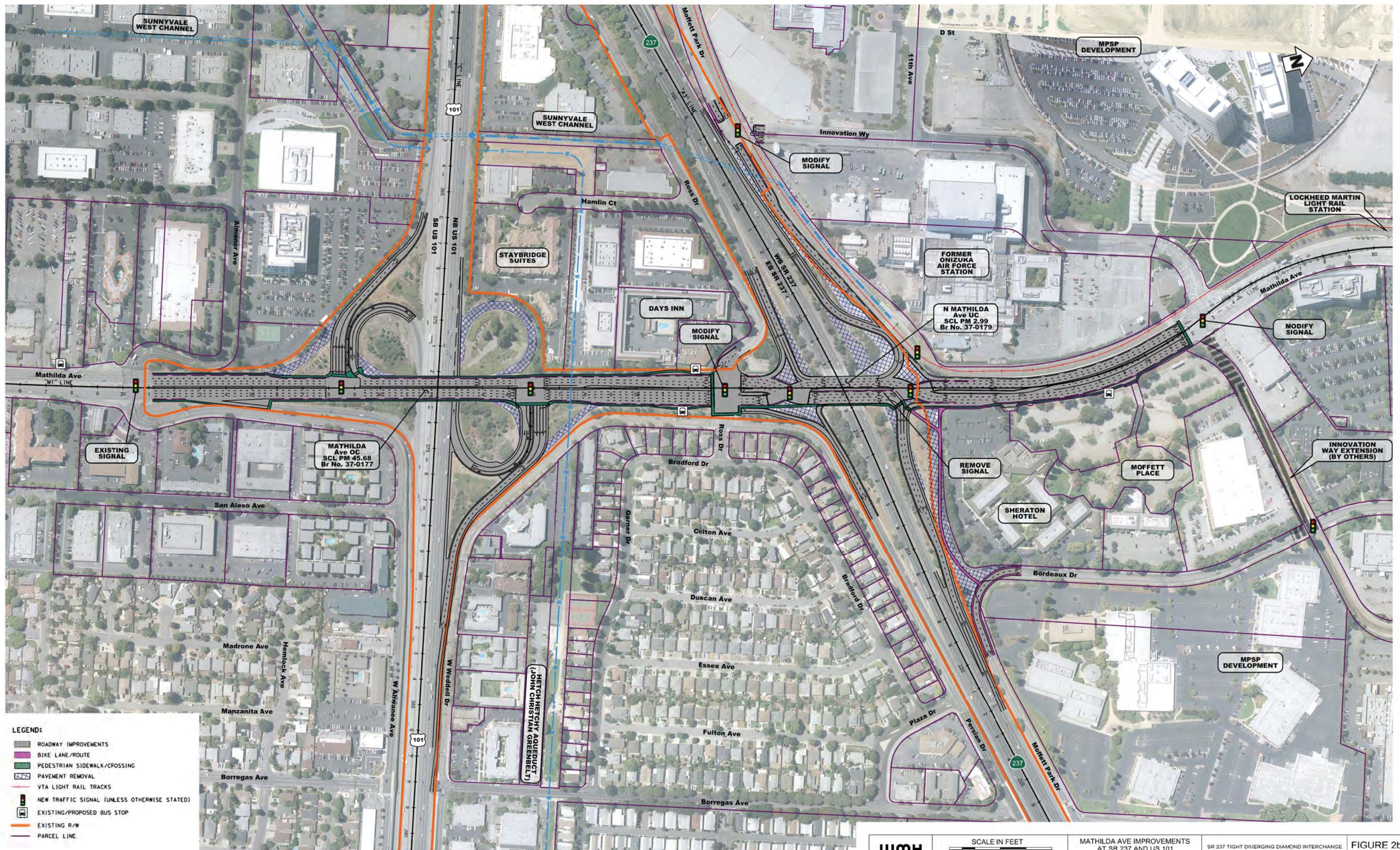


MATHILDA AVE IMPROVEMENTS
 AT SR 237 AND US 101
 SCL 237 - PM 2.7/3.3
 SCL 101 - PM 45.4/45.8

SR 237 TIGHT DIAMOND INTERCHANGE
 AND US 101 FULL PAR-CLO INTERCHANGE

FIGURE 2a
 JULY 2015

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 1508282324



- LEGEND:**
- ROADWAY IMPROVEMENTS
 - BIKE LANE/ROUTE
 - PEDESTRIAN SIDEWALK/CROSSING
 - PAVEMENT REMOVAL
 - VTA LIGHT RAIL TRACKS
 - NEW TRAFFIC SIGNAL (UNLESS OTHERWISE STATED)
 - EXISTING/PROPOSED BUS STOP
 - EXISTING R/W
 - PARCEL LINE

wmh SCALE IN FEET
 100 50 0 100 200 300

**MATHILDA AVE IMPROVEMENTS
 AT SR 237 AND US 101
 SCL 237 - PM 2.7/3.3
 SCL 101 - PM 4.4/5.8**

SR 237 TIGHT DIVERGING DIAMOND INTERCHANGE
 AND US 101 FULL PAR-CLO INTERCHANGE

FIGURE 2b
 JULY 2015

K:\237_101_maths\101_0600_CAD\enhancements\PSR\PSR237-101-MATHILDA_A11-2.dgn

Avenue and at the US 101 interchange are identical. These improvements include new bicycle and pedestrian facilities, utility relocations, new stormwater treatment facilities, enhanced lighting, ramp metering modifications, overhead signage modifications, and a new retaining wall. In addition to the improvements listed above, Build Alternative 2 includes a diverging diamond interchange² (DDI) design north of Ross Drive on Mathilda Avenue (**Figure 3**).

2.4.1 Roadway Improvements

The Build Alternatives would consist of the following roadway improvements:

- Provide three continuous through lanes in each direction on Mathilda Avenue.
- Remove northbound US 101 loop off-ramp and shift traffic to northbound US 101 diagonal off-ramp.
- Realign and widen northbound US 101 ramps and signalize ramp intersection with Mathilda Avenue, and construct left-turn lane on southbound Mathilda Avenue to access northbound US 101 loop on-ramp.
- Realign southbound US 101 off-ramp and loop on-ramp and signalize ramp intersection with Mathilda Avenue.
- Modify Mathilda Avenue/Ross Drive signal intersection.
- Close Moffett Park Drive between Bordeaux Drive and Mathilda Avenue, replace with a Class I bikeway (as described below), and shift traffic to Bordeaux Drive and Innovation Way.³
- Remove westbound SR 237 ramp signal intersection. Realign westbound SR 237 off-ramp opposite Moffett Park Drive and modify signal intersection.
- Build Alternative 1 would modify westbound SR 237 ramps to provide a diamond configuration.
- Build Alternative 2 would modify Mathilda Avenue and SR 237 ramps to provide a diverging diamond configuration (refer to **Figure 2b** and **Figure 3**). Eastbound Moffett Park Drive between Innovation Way and Mathilda Avenue would be diverted to Innovation Way to access Mathilda Avenue.

2.4.2 Bicycle and Pedestrian Facilities

Enhanced bicycle and pedestrian facilities would be provided. Bicycle improvements on Mathilda Avenue would consist of both Class II and Class III bikeways⁴, based on available pavement

² A diverging diamond interchange, also called a double crossover diamond interchange, is a type of diamond interchange where traffic briefly crosses over to the left (opposite) side of the roadway, guided by traffic signals at each crossover. This allows vehicles to turn left onto freeway on-ramps without stopping and without conflicting with through traffic. The signals at ramp terminal intersections can be operated with two signal phases (a signal phase allows for traffic at an intersection to cycle through specific movements for each direction) instead of three.

³ Innovation Way would be extended from Mathilda Avenue to Bordeaux Drive by the Moffett Place development project.

⁴ Class I bikeway is a bicycle path (completely separate from the roadway). Class II bikeway is a bicycle lane (buffered from roadway). Class III bikeway is bicycle route (“sharrow”) [Source: Highway Design Manual Index 1002.1]

widths within the Project limits, and connect to the existing Class III bikeway north of Innovation Way and the Class I bikeway adjacent to the Sunnyvale West Channel. Bicycle improvements on Moffett Park Drive would consist of a Class I bikeway between Bordeaux Drive and Mathilda Avenue. Between Mathilda Avenue and Innovation Way, Class II and Class III bikeways would be considered, based on available pavement widths within the Project limits. A continuous sidewalk would be provided on the east side of Mathilda Avenue within the Project limits, with crosswalks, curb ramps, and pedestrian countdown signals at each intersection. The new crosswalks at the reconfigured ramp intersections would be signalized.

2.4.3 Utility Relocations

The Build Alternatives would include utility relocations, as necessary, to construct the above-described improvements. Build Alternative 1 would require relocation of Verizon telecommunication lines and relocation of a City eight-inch recycled water line along the current alignment of Moffett Park Drive east of Mathilda Avenue. Build Alternative 2 would require relocation of a six-inch PG&E underground gas line and a 12kV PG&E underground electrical line along the current alignment of Moffett Park Drive west of Mathilda Avenue. Both Build Alternatives could require adjustments to three PG&E electrical pole wires to accommodate ramp modifications at the Mathilda Avenue/US 101 interchange. Utility covers would be adjusted to grade in areas of pavement rehabilitation.

2.4.4 Stormwater Treatment

The proposed interchange ramp modifications are expected to result in the fill or removal of existing ditches, modification or relocation of existing longitudinal drainage structures, and construction of new drainage structures. The Build Alternative's drainage design would maintain existing drainage patterns; however, during construction, temporary drainage facilities may be required to redirect runoff from construction areas.

The stormwater treatment facilities for both Build Alternatives may include biofiltration strips, biofiltration swales, bioretention basins, and/or detention basins within the state ROW near the on- and off-ramps and within City of Sunnyvale ROW along the roadway.

2.4.5 Enhanced Lighting

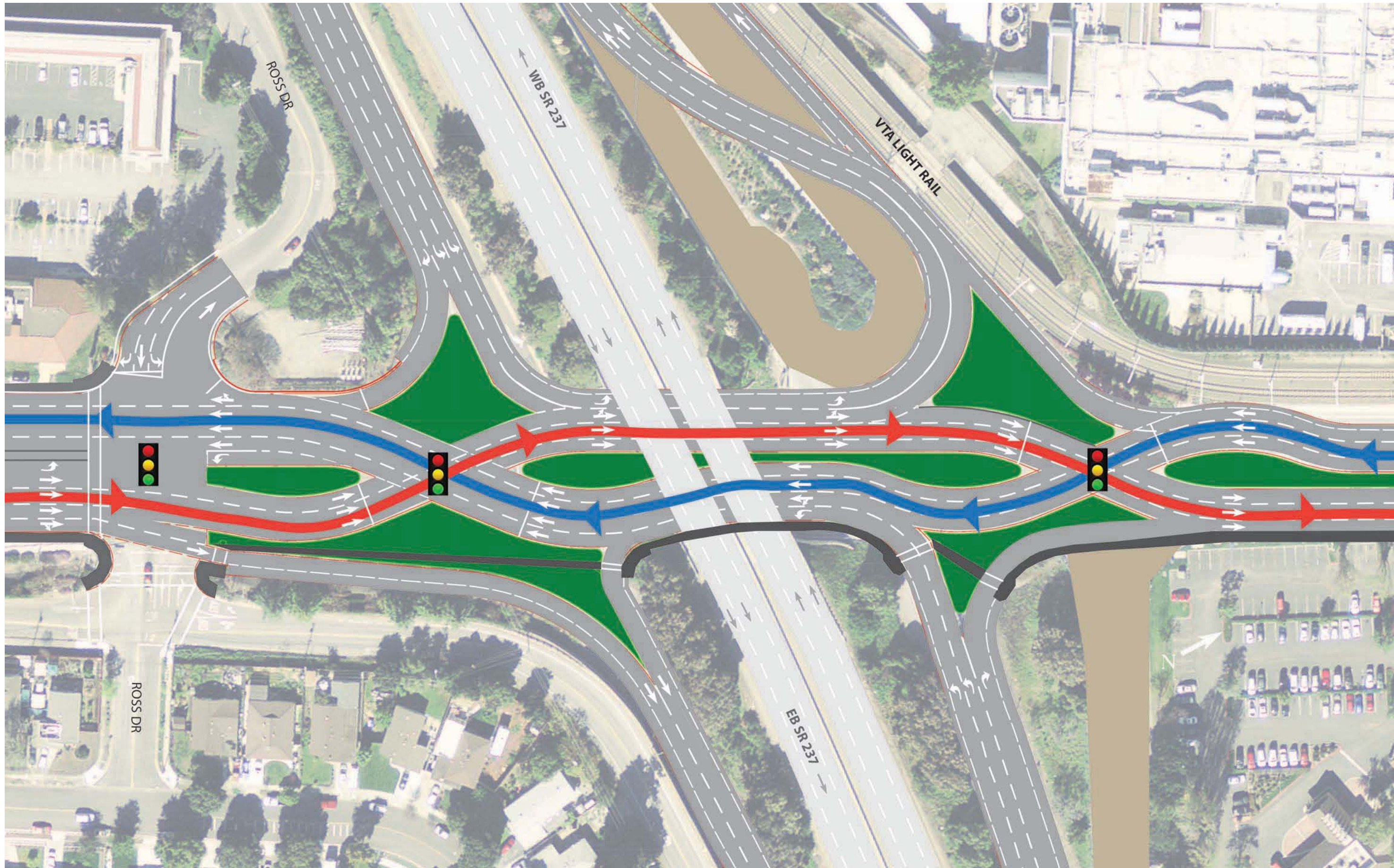
The Build Alternatives would both provide enhanced lighting to improve roadway visibility for drivers during nighttime hours. Overhead lighting would be maintained or installed at all ramps. The lights would either be supported on a cast-in-drilled-hole pile, with a typical diameter of 2.5 feet and depth of 5 feet, or mounted on a structure above grade.

2.4.6 Ramp Metering

Ramp metering facilities already exist at the northbound US 101 loop on-ramp, southbound US 101 ramps, and westbound SR 237 on-ramp. Because these ramps would be modified and realigned under both Build Alternatives, the affected ramp metering equipment would also be modified.

2.4.7 Overhead Signage

Updated overhead signs in each direction on SR 237 and US 101 would inform motorists of the approaching on- and off- ramps associated with the Project. The overhead sign structure mounted



NOT TO SCALE

MATHILDA AVE IMPROVEMENTS
 AT SR 237 AND US 101
 SCL 237 - PM 2.7/3.3
 SCL 101 - PM 4.5/4.8

DIVERGING DIAMOND
 INTERCHANGE (DDI) ILLUSTRATION

FIGURE 3
 JULY 2015

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1/2/2015 10:45:11 AM

to the Mathilda Avenue overcrossing on northbound US 101 would be removed because it applies to the existing loop off-ramp, which is being relocated and integrated as both a west and east Mathilda Avenue access route from northbound US 101. The northbound US 101 off-ramp sign would be impacted by the off-ramp widening, therefore, it would be removed and replaced just south of the Borregas Bicycle/Pedestrian Overcrossing.

2.4.8 Light Rail Facilities

VTA LRT facilities that cross the Moffett Park Drive/Innovation Way and Mathilda Avenue/Innovation Way intersections would be coordinated with traffic signal modifications, which would be location specific. The final locations for new traffic signals would be determined during subsequent design phases.

2.4.9 Retaining Walls and Sound Barriers

The Project would require construction of three retaining walls to minimize the amount of earthwork and right of way acquisitions required. The location of proposed retaining walls are at the southbound US 101 diagonal off-ramp/ southbound US 101 loop on-ramp, the northbound US 101 off-ramp/ northbound US 101 loop on-ramp, and along the west side of Mathilda Avenue. Retaining walls will be aesthetically treated to blend into the surrounding environment and match nearby adjacent walls.

To accommodate proposed realignment and widening of the northbound US 101 off-ramp to Mathilda Avenue, the Project would remove and replace approximately 1,000 feet of the existing 10-foot high noise barrier adjacent to the ramp and West Weddell Drive. The replacement wall would be supported on a retaining wall and located at the widened edge of pavement. Noise barriers will be textured and/ or stained to blend into the surrounding environment, match nearby adjacent walls, and reduce glare and potential for graffiti.

2.4.10 Construction and Staging Areas

Construction of either of the Build Alternatives would take approximately one year. A combination of day and night work is anticipated. Weekend work is not anticipated. Short-term lane and ramp closures would be necessary to facilitate construction. Prior to construction, a Traffic Management Plan (TMP) would be prepared to minimize or prevent delay and inconvenience to the traveling public. The TMP would address all traffic-related aspects of construction, pedestrian access and safety, and bicycle access and safety. Staging/laydown areas for equipment and materials would be needed during Project construction. Construction staging areas would be located within the state ROW adjacent to Mathilda Avenue. Potential locations are shown on **Figure 4** and include:

- Within the northbound US 101 loop off-ramp,
- Between the northbound US 101 diagonal off-ramp and northbound loop on-ramp,
- Within the southbound US 101 loop on-ramp,
- Between the southbound US 101 loop on-ramp and diagonal off-ramp, and
- Between the westbound SR 237 ramps and Moffett Park Drive.

2.5 Summary of Public Involvement Activities

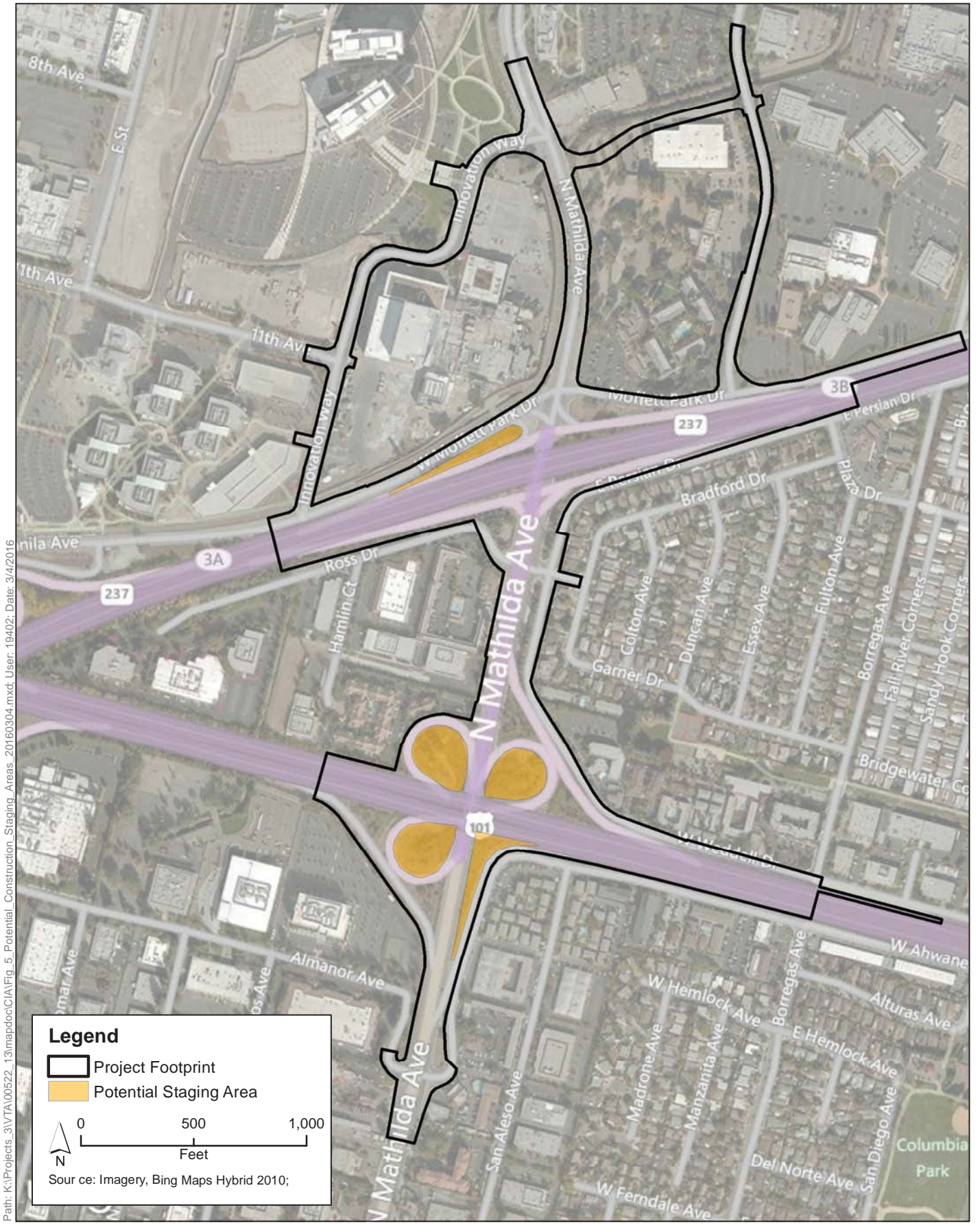
In 2014, a City Council Study Session was held in the City of Sunnyvale to seek input on the proposed Project. The session was attended by City Councilmembers, staff from the City of Sunnyvale and VTA, and members of the public. Appendix A includes a summary of the meeting.

A Notice of Preparation to prepare an EIR/ Environmental Assessment (EA)⁵ was circulated from August 18, 2015 to September 16, 2015. An environmental scoping meeting was held at the Columbia Middle School in the City of Sunnyvale on August 27, 2015. Approximately 4,600 notices for the scoping meeting were mailed to residences and businesses within a 0.25 mile radius of the Project footprint. . A public meeting flyer was hand distributed to businesses along Mathilda Avenue from Almanor Avenue to Innovation Way and the City of Sunnyvale Public Library. A meeting notice was posted on the VTA website, VTA Headways Blog, VTA Twitter feed, and VTA Facebook page, and sent to local media outlets. Notices were published in five newspapers (Sunnyvale Sun, Viet Nam Daily, Philippines Today, Sing Tao Daily, and El Observador). A project factsheet was translated in five languages (Spanish, Chinese, Vietnamese, Korean, and Tagalog) and posted on the Project website. An email notification about the scoping meeting was sent to agencies, organizations, and individual stakeholders. The meeting notice was published in VTA's August Take-One passenger newsletter. The scoping meeting was attended by approximately 37 persons. A total of 21 public comments were received during the scoping period. These comments included recommendations from both members of the public and local jurisdictions to consider bicycle, pedestrian, and vehicle safety; bicycle and pedestrian routes; the Moffett Park Drive closure; air quality; and connections to local transit. Subsequently, the Project was presented to the VTA Bicycle and Pedestrian Committee on October 7, 2015. Refer to Appendix A for a list of public meetings held for the Project and a copy of notices prepared for the scoping meeting.

Public input on the Project will be further solicited during the review period for the Draft EIR (anticipated July 2016), which will last for a minimum of 45 days. The public will be notified of the release of the Draft EIR through a number of methods, including, but not limited to:

- Postings on the Caltrans and VTA websites;
- Mailing announcements to interested agencies, residents, and businesses within 0.25 miles of the Project area;;
- Notice placements in the Sunnyvale Public Library;
- Email notifications to local and regional jurisdictions, and stakeholders including neighborhood associations and business groups from the scoping period;
- Postings on social media, including Twitter and Facebook, and VTA's Headways blog.
- Publishing announcements in newspapers, including non-English papers, as was done for the scoping meeting (above); and
- Sending out news releases to media outlets.

⁵ An EA was originally proposed for the Mathilda Avenue Improvements Project; however, later in the project development process, it was determined that no federal funding would be pursued to construct the project and that no federal approvals or environmental permits were needed. As a result, the project sponsors and the CEQA lead agency determined no NEPA clearance would be pursued.



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Figure 4
Potential Construction Staging Areas
 Mathilda Avenue Improvements at SR 237 and US 101 Project

- During this review period, a public meeting will be held to share information about the Project and to receive comments on the Draft EIR from interested parties. All formal comments will be addressed and responded to in the published Final EIR (anticipated January 2017).

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Chapter 3 – Affected Environment

3.1 Study Area

The study area for the purposes of this analysis comprises the four census tracts in the 2010 U.S. Census located adjacent to the Project area (census tracts 5046.02, 5048.03, 5090.00, and 5091.02). **Figure 5** depicts the study area and shows the location of the census tracts in relation to the Project. Generally, this study area represents the geographical extent of the community adjacent to the Project area, and the area in which any potential Project effects on the community may occur.

3.2 Existing Land Use

Within the City of Sunnyvale, Mathilda Avenue is a six-lane divided roadway between US 101 and SR 237. Mathilda Avenue is a moderately developed arterial roadway with residential development primarily east of the Project area and commercial and industrial uses primarily west of the Project area (refer to **Figure 6**). The northern portion of the Project area, to both sides of Mathilda Avenue and north of SR 237, includes a hotel, the Moffett Place re-development area, the former Onizuka Air Force Station (currently under development), and Sunnyvale Fire Station #5. The Sunnyvale Fire Station #5 is to be relocated as part of a separate project, and prior to construction of the Project. The Moffett Federal Airfield is located just to the west of the western-most point of the Project area, adjacent to the SR 237/US 101 interchange. The Project area is served by two VTA LRT stations, Moffett Park and Lockheed Martin, which are located within the Project area and serve the business district north of SR 237. In addition, VTA operates a local bus service with four bus stops on Mathilda Avenue. Refer to **Figure 7** for existing land uses within the Project area.

3.2.1 Sunnyvale

As described above, land uses along the Project area in the City of Sunnyvale generally consist of commercial and single-family residential uses. The single-family residential uses are concentrated on the east end of the Project area, while the commercial uses are concentrated on the west end of the Project area.

The Project is consistent with *Plan Bay Area*, the regional transportation plan (ABAG and MTC 2013), the City of Sunnyvale's General Plan (General Plan), the *City of Sunnyvale Moffett Park Specific Plan*, and the *City of Sunnyvale 2006 Bicycle Plan* and *Santa Clara Countywide Bicycle Plan* (Santa Clara County 2008). *Plan Bay Area* identifies the need for improvements to the 237/Mathilda Avenue and US 101/Mathilda Avenue interchanges, which are consistent with the Project. The General Plan was updated in July 2011 and guides the City's growth and change through 2025. Specifically, the purpose of the General Plan is to provide guiding goals, policies, and direction for physical development in the City so that the City successfully emerges as a vibrant, innovative, and attractive community in which both residents and businesses can thrive. The General Plan designates a large portion of the Project area as Low Density Residential, High Density Residential, Industry, and Industrial Intensification. The General Plan designates the Project area as a potential growth area including office, industrial, and mixed uses. Enhancements envisioned as part of the General Plan include gateway improvements at SR 237, US 101, and Mathilda Avenue at US 101.

The City of Sunnyvale prepared the *Moffett Park Specific Plan* in 2013 that includes a portion of the Project area, north of SR 237. The purpose of this Specific Plan is to maximize Moffett Park

development with corporate headquarters, office, and research/development facilities of high technology companies that will represent the next wave of economic growth in Silicon Valley. The Specific Plan also identifies three sub-districts that the City plans for enhancement: MP-TOD (parcels within 0.25 mile of an existing LRT station), MP-I (industrial areas beyond 0.25 mile of an existing transit station), and MP-C (provides support for commercial services). The Project area is within each of the sub-districts. Enhancements envisioned as part of the Specific Plan include additional arterial connections to the Plan area, localized roadway improvements, and intersection improvements.

The *City of Sunnyvale 2006 Bicycle Plan* lists goals that include facilitating bicycling during the transportation planning process and accommodating bicycle needs in future roadway and land development projects. The *Santa Clara Countywide Bicycle Plan* provides policy framework that includes providing bicycle/pedestrian connections to commercial and residential areas. As such, bicycle and pedestrian improvements included in the Project would be consistent with both the City and County bicycle plans.

3.3 Community Characteristics

3.3.1 Demographic Profile

Data for the census tracts and the City of Sunnyvale were gathered to present a demographic profile of the community. Table 3-1 summarizes the make-up of the population in the Project study area.

Table 3-1. Population of Census Tracts in Project Study Area

| Geography/ Census Tract (CT) | Total Population | Hispanic or Latino | White | Black or African American | American Indian and Alaska Native | Asian | Native Hawaiian and Other Pacific Islander | Some Other Race | Two or More Races |
|------------------------------------|---------------------|--------------------------|---------------|---------------------------------|---|--------------|--|-----------------------|-------------------------|
| CT 5091.02 | 4,900 | 468 | 1,692 | 157 | 0 | 2,756 | 0 | 35 | 260 |
| CT 5090.00 | 8,386 | 4,236 | 5,301 | 342 | 15 | 1,485 | 126 | 906 | 211 |
| CT 5048.03 | 5,793 | 663 | 1,954 | 225 | 0 | 3,309 | 0 | 101 | 204 |
| CT 5046.02 | 1,835 | 1,045 | 1,053 | 23 | 10 | 453 | 0 | 274 | 22 |
| <i>Study Area Total</i> | <i>20,914</i> | <i>6,412</i> | <i>10,000</i> | <i>747</i> | <i>25</i> | <i>8,003</i> | <i>126</i> | <i>1,316</i> | <i>697</i> |
| City of Sunnyvale | 145,921 | 26,268 | 70,035 | 2,886 | 363 | 60,528 | 942 | 5,620 | 5,547 |

Source: U.S. Census Bureau, 2010-2014 American Community Survey 5-Year Estimates⁶

*Data are based on a sample and are subject to sampling variability.

⁶ American Community Survey data was used as 2010 Census data is over five years old and American Community Survey data is based on the Census data, but is an ongoing statistical survey that samples a small percentage of the population every year.

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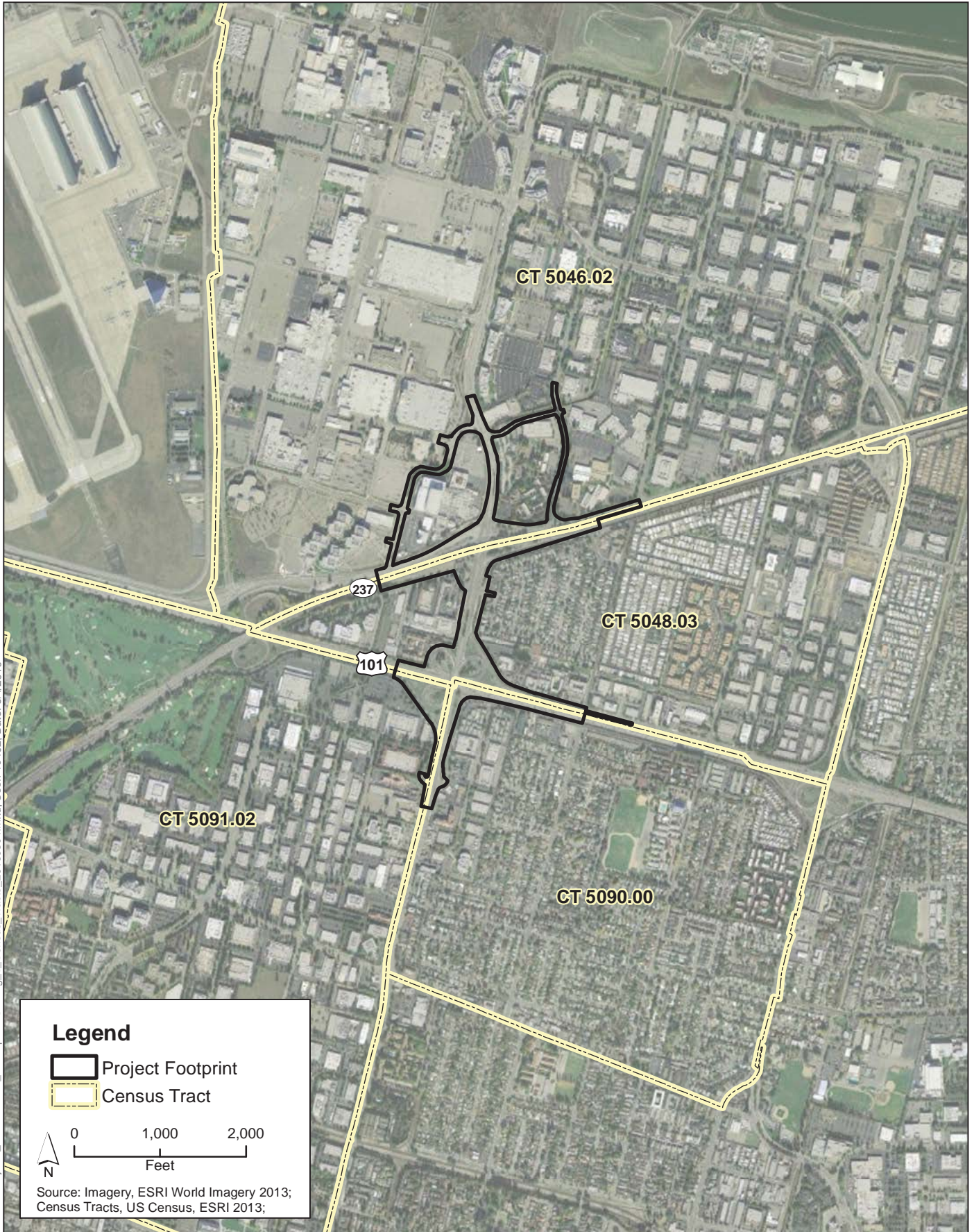


Figure 5
Study Area Limits and Census Tracts
Mathilda Avenue Improvements at SR 237 and US 101 Project

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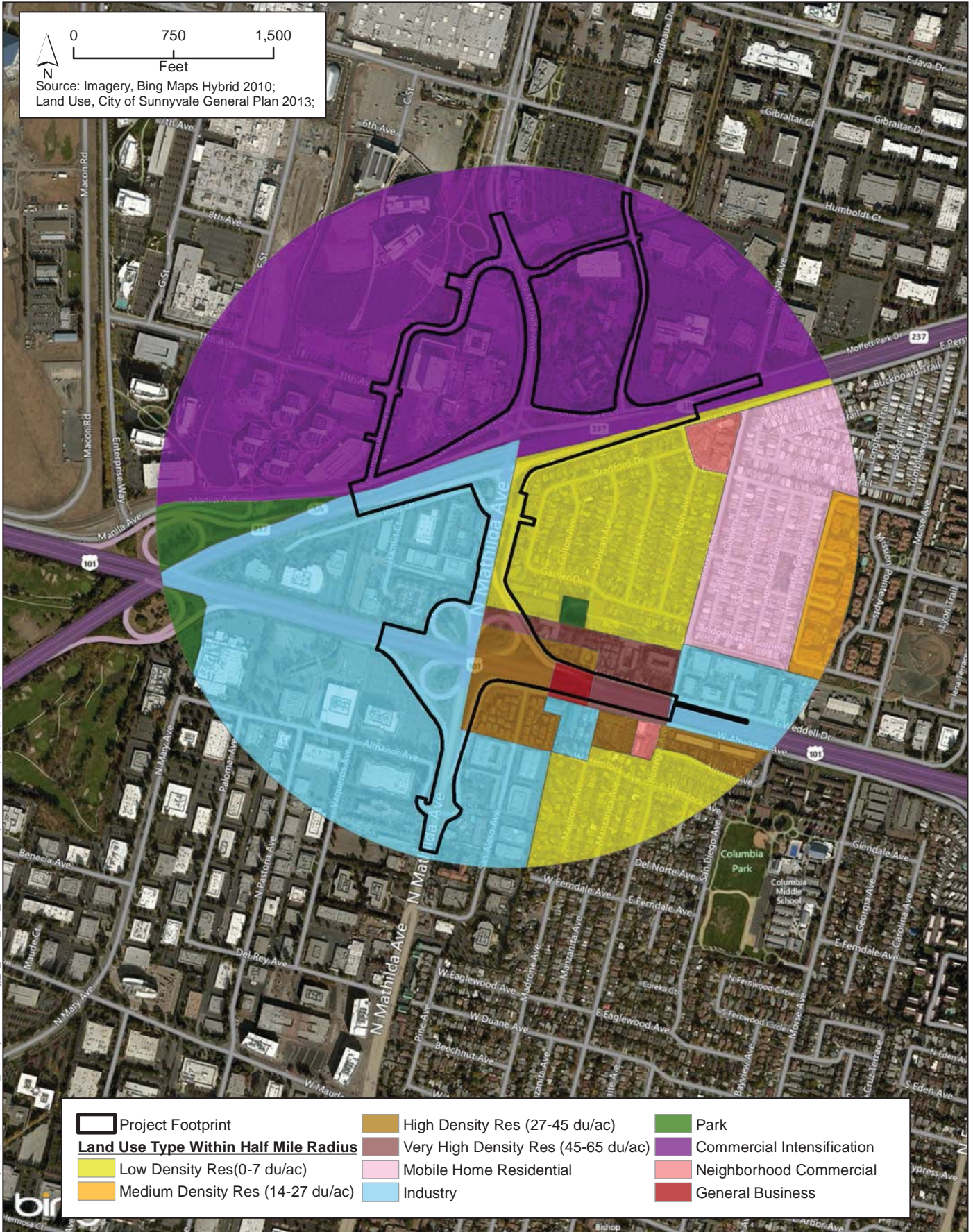


Figure 6
Study Area Land Uses
Mathilda Avenue Improvements at SR 237 and US 101 Project



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Figure 7
Existing Land Uses
 Mathilda Avenue Improvements at SR 237 and US 101 Project

Table 3-2 summarizes the income statics for the population in the Project study area.

Table 3-2. Income Data for Census Tracts in Project Study Area

| Geography/ Census Tract (CT) | Total Population | Median Household Income | Per Capita Income | Percentage of Population with Income Below Poverty Level | Number of Population with Income Below Poverty Level¹ |
|---|-----------------------------|--|------------------------------|---|---|
| CT 5091.02 | 4,900 | \$119,938 | \$63,149 | 0% | 0 |
| CT 5090.00 | 8,386 | \$73,333 | \$29,393 | 7.3% | 612 |
| CT 5048.03 | 5,793 | \$100,458 | \$52,208 | 5.3% | 307 |
| CT 5046.02 | 1,835 | \$76,705 | \$29,929 | 9.5% | 174 |
| <i>Study Area Total</i> | <i>20,914</i> | <i>x</i> | <i>x</i> | <i>5.2%</i> | <i>1,093</i> |
| City of Sunnyvale | 145,921 | \$103,257 | \$48,203 | 4.8% | 7,004 |

Source: U.S. Census Bureau, 2010-2014 American Community Survey 5-Year Estimates

¹Rounded to the nearest whole number.

*Data are based on a sample and are subject to sampling variability.

x = data not available

3.3.2 Neighborhood Characteristics

Within the study area, Mathilda Avenue is a major local arterial roadway that provides access to US 101 and SR 237 in the City. The study area can generally be characterized as suburban, commercial, and industrial in character. The eastern side of the Project study area is predominantly single-family residential (between US 101 and SR 237) and commercial land uses with several industrial land uses along US 101. The western side of the Project area is predominantly industrial and commercial land uses, including several hotels, an office building, and a warehouse.

3.3.3 Community Facilities

Community facilities within a ¼ mile of the Project area include the Lockheed Martin and Moffett Park LRT stations, four churches, four parks, a community center, three schools and a college. Table 3-3 summarizes community facilities near the Project area and **Figure 8** identifies the location of the facilities relative to the Project area.

Table 3-3. Project Area Land Uses and Community Facilities

| Community Facility | Distance from Project Area* | Corresponding Identification Number on Figure 8 |
|--|------------------------------------|--|
| Foothill De Anza Community College | Within Project Area | 2 |
| John W. Christian Greenbelt | 0.05 miles | 15 |
| The Rock Church | 0.08 miles | 5 |
| Lockheed Martin LRT Station | 0.10 miles | 3 |
| Orchard Gardens Park | 0.10 miles | 4 |
| Columbia Park | 0.15 miles | 14 |
| Moffett Park LRT Station | 0.20 miles | 1 |
| Seven Seas Park | 0.20 miles | 6 |
| New Hope International Church | 0.20 miles | 7 |
| The 1 st Morning Light Chinese Christian Church | 0.20 miles | 8 |
| Iranian Assembly of God Church | 0.20 miles | 9 |
| Columbia Neighborhood Center | 0.20 miles | 10 |
| Madrone School | 0.20 miles | 11 |
| Spark Charter School | 0.25 miles | 12 |
| Columbia Middle School | 0.25 miles | 13 |

Source: Google Earth Pro 2013.

*As measured from the nearest Project boundary.

**John W. Christian Greenbelt and Columbia Park are identified with polygons on Figure 8.

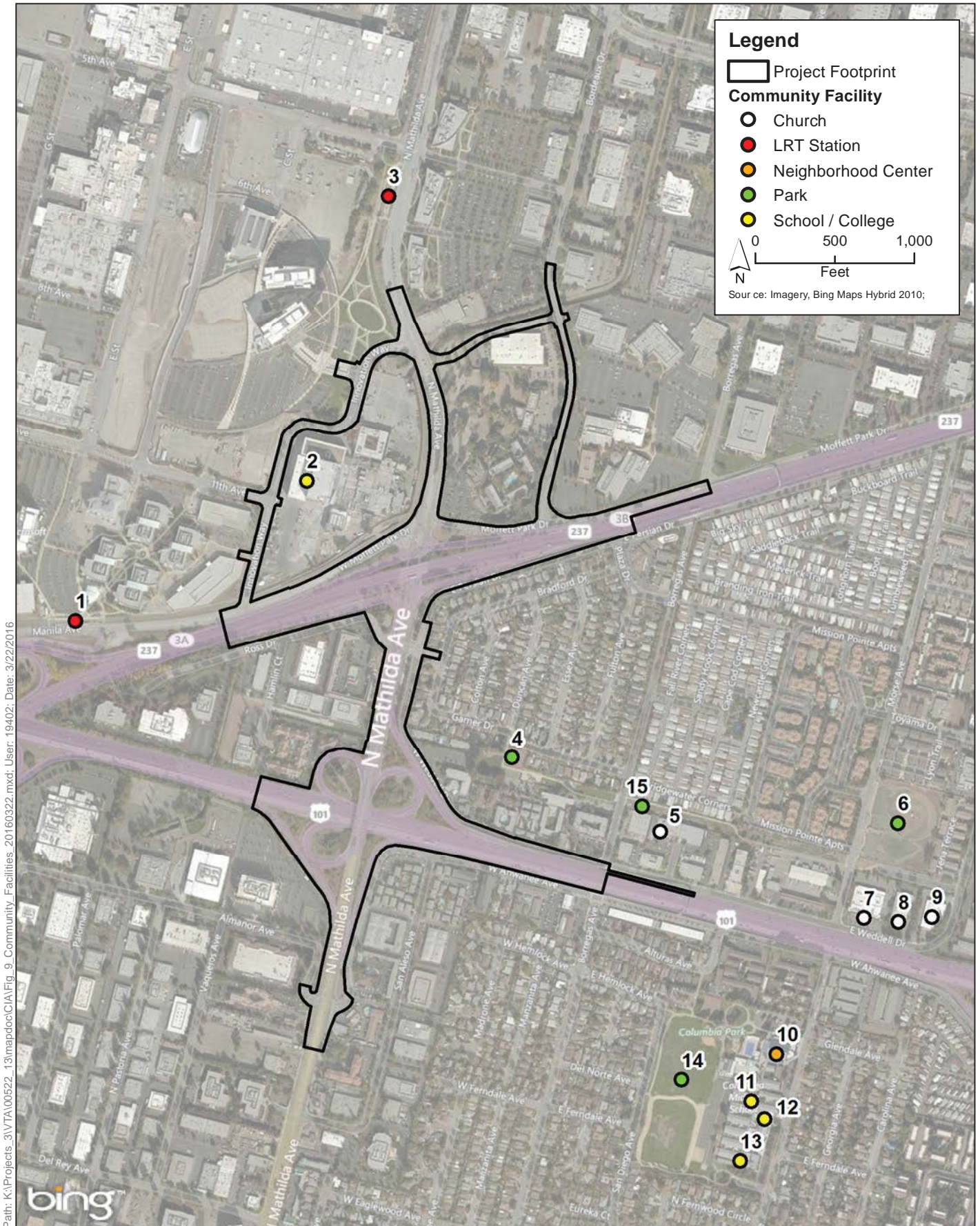
Emergency Services

Other than Sunnyvale Fire Station #5, there are no emergency service provider facilities located within a ½ mile of the Project area. Table 3-4 lists the City's emergency service providers and their proximity to the Project area.

Table 3-4. Emergency Service Facilities

| Facility Name | Address | Distance from the Project Area |
|---|-------------------------------|---------------------------------------|
| Police | | |
| Department of Public Safety-Sunnyvale Police Department | 700 All American Way | 1.6 miles |
| Fire | | |
| Sunnyvale Fire Station #1 | 171 N. Mathilda Avenue | 1.0 mile |
| Sunnyvale Fire Station #2 | 795 E. Arques Avenue | 1.3 miles |
| Sunnyvale Fire Station #3 | 910 Ticonderoga Drive | 3.0 miles |
| Sunnyvale Fire Station #4 | 996 S. Wolfe Road | 2.8 miles |
| Sunnyvale Fire Station #5 | 11120 Innovation Way | Within Project Area |
| Sunnyvale Fire Station #6 | 1282 N. Lawrence Station Road | 1.7 miles |

Sources: Google Earth Pro, 2013; City of Sunnyvale, 2015.



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Figure 8
Community Facilities
Mathilda Avenue Improvements at SR 237 and US 101 Project

Chapter 4 – Impact Analysis

The following discussion is intended to describe the potential impacts on the community that may result from construction and operation of the Project. The Project features that have the highest potential to result in impacts are described as follows.

Construction Impacts: Construction activities would require temporary construction easements and include activities related to: utility relocations; installation of stormwater treatment facilities; enhanced lighting; ramp reconfiguration; overhead signage replacement; and removal, modification, or installation of traffic signals. In addition, short-term lane and ramp closures are anticipated. Refer to Section 4.1.1, Impacts Common to all Build Alternatives for further discussion on construction activities.

Operation Impacts: A permanent partial ROW acquisition of the Sheraton Hotel would occur under both the Build Alternatives. The Build Alternatives were designed to reduce existing traffic congestion and improve mobility for all users in the Project area. As reported in the Traffic Operations Analysis Report (Fehr and Peers 2016), in most cases, both Build Alternatives show a reduction in average travel time and an increase in average travel speed on Mathilda Avenue in 2018 (opening year) when compared to No Build conditions. An overall reduction in peak hour delay and queuing on local streets and freeway ramps is also seen with Both Build Alternatives compared to the No Build Alternative.

Build Alternative 1 would result in a northbound delay reduction of approximately 6 minutes during the morning (8:00 AM) and evening (5:00 PM) peak hours. In the southbound direction, Build Alternative 1 would reduce delays by over 0.5 minutes in the morning peak hour and increase travel times by approximately 1 minute during the evening peak hour.

Build Alternative 2 would result in a northbound delay reduction of over 3.5 minutes and 5.5 minutes during the morning and evening peak hours, respectively. In the southbound direction, Build Alternative 2 would reduce delays by over 1.5 minutes and 3.5 minutes during the morning and evening peak hour, respectively.

The following sections address potential impacts to land use, community cohesion, local community facilities and services, and required ROW acquisitions and temporary construction easements.

4.1 Land Use Impacts

Potential land use impacts associated with the Project would be related to the following issues:

- The compatibility of the Project with existing and planned land uses.
- The consistency of the Project with state, regional, and local plans and programs.
- The type and number of property acquisitions required for the Project.

Potential land use impacts are discussed below.

4.1.1 Impacts Common to all Build Alternatives

Each Build Alternative would result in changes at the same locations that would include the removal of ramps; modification and widening of existing ramps; traffic signal removal, modification, or installation; roadway improvements; reconfiguring Moffett Park Drive; and intersection improvements.

Construction Impacts

Construction of either Build Alternative would take approximately one year and would require traffic control for a period of approximately seven to eight months. Long term closures of freeway mainline shoulders, and freeway on- and off-ramp shoulders are expected, as are short term closures of freeway lanes, ramps, and local roads. Detours, traffic shifts, and lane restriping would be utilized to maintain access and improve worker safety. As such, extensive delays are not anticipated; however, efforts will be made to further minimize the potential for delays through traffic management measures that will be defined in the TMP (to be prepared prior to construction), which would be implemented to provide residents, businesses, motorists, transit users, and emergency service providers with advance notice of construction activities and durations, temporary closures, detours, and access issues during construction.

The Project would require temporary construction easements and would result in a partial permanent ROW acquisition; however, no residential or business relocations would be required. Construction work along curbs, such as sidewalk and crosswalk alterations, would result in inconveniences to adjacent businesses and properties; however, all businesses would remain open and accessible during construction. In addition, the forthcoming TMP would provide bicyclists and pedestrians with alternative paths during construction, and signs would be posted to direct bicyclists and pedestrians to intersections where they may cross.

Operation Impacts

Under both of the Build Alternatives, the Project would be compatible with existing land uses, as the SR 237/Mathilda Avenue and the US 101/Mathilda Avenue interchanges are existing primary access points on the state highway system for the City. The Project would retain existing transportation land uses for Project elements, including traffic signal removal, modification, or installation, and bicycle and pedestrian enhancements. One partial permanent ROW acquisition would occur as a result of the Project; however, no relocations of buildings and structures are anticipated. Accordingly, no changes in land use or zoning are anticipated as part of the Project.

Plan Bay Area and the City's General Plan identify SR 237, US 101, and Mathilda Avenue at US 101 as locations in need of gateway improvements. In addition, the *Moffett Park Specific Plan* identifies Mathilda Avenue as a major arterial roadway that requires traffic congestion relief, particularly at the SR 237 and US 101 interchanges. The bicycle and pedestrian improvements are also consistent with the City and County bicycle plans. As such, the Project would be consistent with the expressed goals of these planning documents.

4.1.2 Impacts Specific to Alternative 1

There would be no impacts specific to Alternative 1.

4.1.3 Impacts Specific to Alternative 2

There would be no impacts specific to Alternative 2.

4.2 Community Impacts

Potential community impacts associated with the Project would be related to the following issues:

- Dividing an established community or neighborhood.
- Altering a community or neighborhood to a point that it no longer maintains its cohesion or character.
- Restricting access or otherwise altering the way in which a community uses its facilities.
- Acquiring or displacing community serving businesses and displacing residents.

4.2.1 Community Character and Cohesion

Income data and demographic information from Section 3.3, *Community Characteristics*, demonstrate that 4.8 percent of the population in the City of Sunnyvale is below poverty level and 5.2 percent of the population in the Study Area is below the poverty level. Furthermore, the City of Sunnyvale has a 52.0 percent minority population, while the Study Area has a 52.2 percent minority population.

Construction

The Project would be constructed almost entirely within existing City of Sunnyvale and Caltrans' ROW. While some temporary construction easements may be required for curb removal and utility relocation work (refer to Section 4.4, *Right-of-Way Acquisitions*), access to local neighborhoods, facilities, and businesses along the Project area would be maintained throughout construction.

Impacts resulting from the Project involve construction-related disruptions associated with operation of construction equipment in the area, partial and/or complete lane and ramp closures, construction work conducted along sidewalks and pedestrian crossings, noise and vibration, light and glare, and construction emissions. These impacts would be temporary, amounting to inconveniences to motorists, bicyclists, and pedestrians in the vicinity of construction activities.

Because through traffic, bicycle, and pedestrian circulation would be maintained in each direction during construction, Project construction would not result in any new barriers that would impede community interaction. Impacts related to construction would be localized to the maximum extent possible so that at any given time construction impacts would affect only a small portion of the Project area. Accordingly, construction would have no effect on long-term community character and cohesion beyond typical temporary construction impacts described above. Furthermore, a TMP would be developed in cooperation with the City of Sunnyvale, Santa Clara County, and Caltrans prior to construction. Bicyclists and pedestrians would be provided with alternative paths during construction, signs would be posted to direct bicyclists and pedestrians to intersections where they may cross, and access to local businesses in the Project area would be maintained.

Construction activities associated with both of the Build Alternatives would result in some temporary disruptions to businesses because construction equipment and construction-related noise, dust, and traffic would be noticeable to patrons of businesses in the vicinity of construction work.

However, implementation of Caltrans' standard specification and measures to control dust during construction would help to minimize air quality impacts from construction activities. Additionally, as described in the Noise Study Report (ICF International 2016) developed for the Project, vibration-reducing construction measures to limit groundborne vibration at nearby structures and residences would be used to minimize any exposure of persons to or generation of excessive groundborne vibration or groundborne noise levels. Further, noise-reduction construction practices would be implemented to minimize any temporary or periodic increase in ambient noise levels in the Project vicinity so that it would not result in a substantial increase above existing levels.

As described above and in Section 4.4, *Right-of-Way Acquisitions*, temporary construction easements that may be required would not result in the displacement of any people, housing, or businesses. Access to any housing or businesses in the Project area potentially affected by construction activities would be maintained at all times, and construction work is not anticipated to result in effects severe enough to disrupt regular business.

Operation of the Project

The proposed changes under the Project would improve access and mobility to the SR 237/Mathilda Avenue and US 101/Mathilda Avenue interchanges, and along Mathilda in between both interchanges. The Project would provide enhanced bicycle facilities including a Class I bikeway between Bordeaux Drive and Mathilda Avenue, and Class II and Class III bikeways between Mathilda Avenue and Innovation Way based on available pavement widths. Under both of the Build Alternatives, Moffett Park Drive access on the east side of Mathilda Avenue would be closed, replaced with a Class I bikeway, and traffic would be shifted to Bordeaux Drive and Innovation Way. However, Moffett Park Drive access west of Mathilda Avenue would remain open. A continuous sidewalk would be provided on the east side of Mathilda Avenue within the Project limits, with crosswalks, curb ramps, and pedestrian countdown signals at each intersection. The new crosswalks at the reconfigured ramp intersections would be signalized. The Project area would also include enhanced lighting and updated overhead signage. Accordingly, Project implementation would have beneficial impacts to the cohesion of the communities along the Project area.

As described in the Noise Study Report (ICF International 2016), the Project would not result in a significant increase in ambient noise levels. Further, as described in the Air Quality Study Report (ICF International 2016) developed for the Project, in 2018, Build Alternatives 1 and 2 would result in decreases in all pollutants compared to existing conditions. The Project would not expose sensitive receptors (i.e., schools, residences, parks) to substantial pollutant concentrations, nor would the Project create objectionable odors affecting a substantial number of people.

Impacts Specific to Alternative 1

There would be no impacts specific to Alternative 1.

Impacts Specific to Alternative 2

There would be no impacts specific to Alternative 2.

4.3 Community Facilities

4.3.1 Impacts Common to all Build Alternatives

Construction Period

The Project could affect access to community facilities and businesses during construction primarily related to operation of construction equipment, partial and/or complete lane and ramp closures, noise and vibration, light and glare, and dust. Because Project construction activities would be temporary, no long-term or permanent adverse effect on nearby community facilities is expected to result. To minimize impacts during construction, Caltrans and VTA will regularly inform the community about construction activities through implementation of a TMP. Construction activities would be coordinated with local police and fire departments to ensure that emergency service and response times remain unaffected during construction. The TMP would require coordination and development of alternate emergency response routes as needed. Similarly, the TMP would require maintenance of emergency access to all properties throughout the construction period.

Operation of the Project

Because the Project would operate within the existing transportation ROW and none of the community facilities or businesses would be relocated as a result of any Build Alternative, no long-term operational effects on identified community facilities or businesses would occur. Updated overhead signage would be installed to inform motorists of the approaching on- and off-ramps associated with the Project. Emergency vehicles would be unrestricted in their ability to access any property along the Project area. Since the Project would not remove any parking within the Project area, there would be no adverse effects attributable to loss of parking.

4.3.2 Impacts Specific to Alternative 1

There would be no impacts specific to Alternative 1.

4.3.3 Impacts Specific to Alternative 2

There would be no impacts specific to Alternative 2.

4.4 Right-of-Way Acquisitions

Conceptual engineering has been completed for the Project Build Alternatives. When a preferred alternative is selected, preliminary and final engineering will begin. Conceptual engineering provides sufficient information to determine if full or partial property acquisitions are necessary, however, it is possible that the location of all the temporary and permanent construction easements may change as design is refined. Depending on sidewalk widths and property lines, temporary construction easements may be required in the northern portion of the Project area to modify the traffic signal along Moffett Park Drive where the Project is outside of the transportation ROW. Both Build Alternatives would require partial acquisition of the Sheraton Hotel at 1108 North Mathilda Avenue. This partial acquisition would not affect any buildings associated with the property, but would close access to the Sheraton Hotel along Moffett Park Drive. The hotel would still be accessible along North Mathilda Avenue and Bordeaux Drive. Access to all properties within the Project area would be maintained during construction. Tables 4-1 and 4-2 list potential ROW

acquisitions and temporary construction easements required for construction of each Build Alternative. **Figures 9a and 9b** show the location of the potential ROW acquisitions and temporary construction easements.

Table 4-1. Build Alternative 1 Right-of-Way Requirements

| Assessor Parcel Number (APN) | Property Owner | Temporary Construction Easement (TCE) | Public Access Easement | Partial Fee Take | Other Easements |
|--|--|---------------------------------------|------------------------|--------------------|----------------------|
| 204-01-013 | PSS Enterprises Inc. 776 N. Mathilda Ave. Sunnyvale, CA 94085 | 200 square feet (sf)/ 0.005 acre (ac) | | | - |
| 110-08-025 | Pappas, Louis G and Effie 502 Ross Dr. Sunnyvale, CA 94089 | 324 sf/ 0.007 ac | | | - |
| 110-27-025 | W2005 New Century Hotel Portfolio LP 1108 N. Mathilda Ave. Sunnyvale, CA 94089 | 11,293 sf/ 0.259 ac | | 2,383 sf/ 0.055 ac | - |
| N/A Moffett Park Dr East of Mathilda | City of Sunnyvale 456 W. Olive Ave. Sunnyvale, CA 94086 | - | | | 43,774 sf/ 1.005 ac |
| N/A Innovation Way | Foothill De Anza Community College 12345 El Monte Road Los Altos Hills, CA 94022 | - | 170,875 sf/ 3.923 ac | | 170,875 sf/ 3.923 ac |
| N/A Innovation Way | Moffett Place LLC 1183 Borregas Ave Sunnyvale, CA 94089 | | 41,226 sf/ 0.946 ac | | 41,226 sf/ 0.946 ac |
| N/A Moffett Park Dr West of Mathilda | City of Sunnyvale 456 W. Olive Ave Sunnyvale, CA 94086 | | | | 4,798 sf/ 0.11 ac |

Table 4-2. Build Alternative 2 Right-of-Way Requirements

| Assessor Parcel Number (APN) | Property Owner | Temporary Construction Easement (TCE) | Public Access Easement | Partial Fee Take | Other Easements |
|--|--|---------------------------------------|------------------------|--------------------|----------------------|
| 204-01-013 | PSS Enterprises Inc. 776 N. Mathilda Ave. Sunnyvale, CA 94085 | 200 square feet (sf)/ 0.005 acre (ac) | | | - |
| 110-08-025 | Pappas, Louis G and Effie 502 Ross Dr. Sunnyvale, CA 94089 | 324 sf/ 0.007 ac | | | - |
| 110-27-025 | W2005 New Century Hotel Portfolio LP 1108 N. Mathilda Ave. Sunnyvale, CA 94089 | 11,373 sf/ 0.261 ac | | 2,779 sf/ 0.064 ac | - |
| N/A Moffett Park Dr East of Mathilda | City of Sunnyvale 456 W. Olive Ave. Sunnyvale, CA 94086 | - | | | 30,849 sf/ 0.708 ac |
| N/A Innovation Way | Foothill De Anza Community College 12345 El Monte Road Los Altos Hills, CA 94022 | - | 170,875 sf/ 3.923 ac | | 170,875 sf/ 3.923 ac |
| N/A Innovation Way | Moffett Place LLC 1183 Borregas Ave Sunnyvale, CA 94089 | | 41,226 sf/ 0.946 ac | | 41,226 sf/ 0.946 ac |

Utility relocation may also require some temporary construction easements, and potentially permanent easements, in addition to the ROW requirements presented in Tables 4-1 and 4-2. However, temporary or permanent easements as a result of utility relocation would be minimal and would not result in displacements of residences or businesses.

Implementation of any of the Build Alternatives would not affect any existing housing; therefore, no replacement housing would be necessary. Implementation of any of the Build Alternatives would not affect any existing businesses; therefore, no business relocations would be necessary.

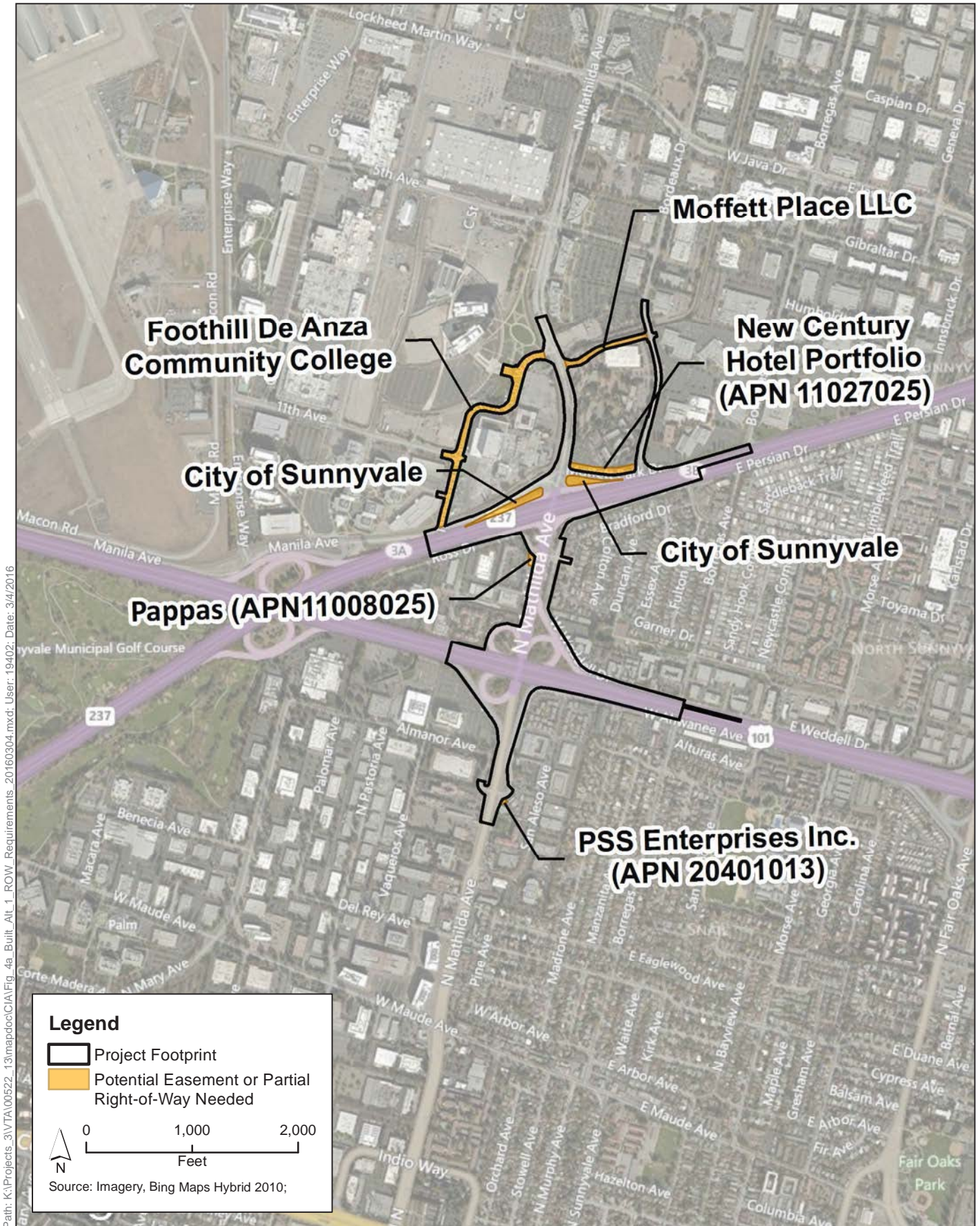
Impacts Specific to Alternative 1

ROW impacts related to Build Alternative 1 are included in Table 4-1 and shown in Figure 9a. Impacts are comparable to Build Alternative 2.

Impacts Specific to Alternative 2

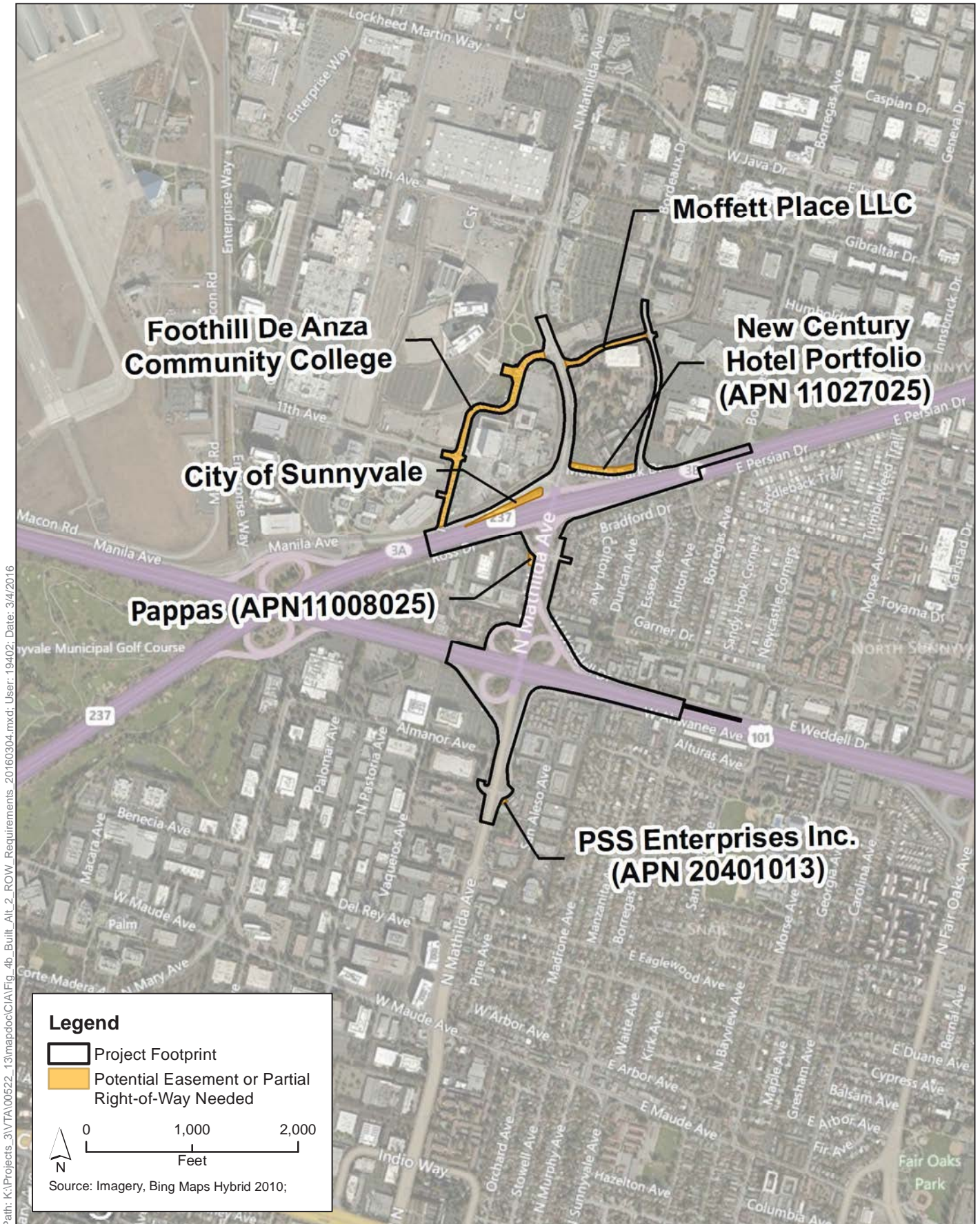
ROW impacts related to Build Alternative 2 are included in Table 4-2 and shown in Figure 9b. Impacts are comparable to Build Alternative 1.

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Figure 9a
Right-of-Way Requirements (Build Alternative 1)
 Mathilda Avenue Improvements at SR 237 and US 101 Project



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Figure 9b
Right-of-Way Requirements (Build Alternative 2)
 Mathilda Avenue Improvements at SR 237 and US 101 Project

Chapter 5 – Avoidance, Minimization, and/or Mitigation

Avoidance, minimization, and/or mitigation measures proposed for air quality, noise, and traffic would result in minimizing and/or mitigating potential impacts related to the surrounding community. These measures include:

- A TMP would be developed in cooperation with the City of Sunnyvale, Santa Clara County, and Caltrans prior to construction. A component of the TMP would include public outreach. Efforts would be made to regularly inform the community about construction activities through notices, press releases, and the use of changeable message signs.
- Implementation of Caltrans' standard specification and measures to control dust during construction would help to minimize air quality impacts from construction activities.
- Vibration-reducing construction measures to limit groundborne vibration at nearby structures and residences would be used to minimize any exposure of persons to or generation of excessive groundborne vibration or groundborne noise levels.
- Noise-reduction construction practices would be implemented to minimize any temporary or periodic increase in ambient noise levels in the Project vicinity so that it would not result in a substantial increase above existing levels.

The above measures would serve to reduce any construction-related impacts to the community within the Project area and no mitigation specific to community impacts is required.

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Chapter 6 – Conclusion

The primary purpose of the Project is to improve traffic operations on Mathilda Avenue through the US 101 and SR 237 interchanges. Overall, the Project is needed to address several issues in the Project area, including roadway deficiencies, lack of or discontinuous bicycle and pedestrian access, improvement of local roadway and freeway ramp operations, and provision of access to current and future economic development.

The percentage of the population living below the poverty level is 4.8 percent in the City of Sunnyvale and 5.2 percent in the Project study area. Furthermore, the City of Sunnyvale has a 52.0 percent minority population, while the Study Area has a 52.2 percent minority population. The Project would not result in long-term adverse impacts on the population or communities within the Project study area. Generally, the only adverse impacts resulting from the Project would be temporary and during the construction period as a result of temporary disruptions to businesses because construction equipment and construction-related noise, dust, and traffic would be noticeable to patrons of businesses in the vicinity of construction work. Implementation of Caltrans' standard specification and measures to control dust during construction would help to minimize air quality impacts from construction activities. Vibration-reducing construction measures to limit groundborne vibration at nearby structures and residences would be used to minimize any exposure of persons to or generation of excessive groundborne vibration or groundborne noise levels. Further, noise-reduction construction practices would be implemented to minimize any temporary or periodic increase in ambient noise levels in the Project vicinity so that it would not result in a substantial increase above existing levels. A TMP would be implemented to minimized traffic impacts during construction.

The majority of the Project would be constructed within existing Caltrans and City of Sunnyvale ROW, requiring only one partial permanent ROW acquisition from the Sheraton Hotel at 1108 North Mathilda Avenue. Businesses and residences in the Project vicinity could experience temporary impacts resulting from increased dust and noise, diminished access, and general inconveniences during the construction period; however, these impacts would be temporary. These impacts would be further minimized through implementation of a TMP.

The Project would be consistent with the local general plans and specific plans and would be compatible with surrounding land uses. The Project would not result in an adverse impact on the public services and community facilities in the Project corridor. The Project would not result in a significant increase in ambient noise levels. The Project would not expose sensitive receptors (i.e., schools, residences, parks) to substantial pollutant concentrations, nor would the Project create objectionable odors affecting a substantial number of people. Upon completion of construction, the Project would result in beneficial impacts on the community by easing existing congestion and providing enhanced pedestrian and bicycle access, improved connection to community centers and businesses. Both Build Alternatives show a reduction in average travel time and an increase in average travel speed on Mathilda Avenue in 2018 (opening year) when compared to No Build conditions.

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Chapter 7 – References

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Appendix A

Public Meetings Held

The Project was presented at the following meetings. A summary of each meeting is provided below.

| Meeting | Date | Location | Parties in attendance | Summary |
|---|-----------------|---|---|--|
| Sunnyvale City Council Study Session | June 10, 2014 | Sunnyvale City Council 456 West Olive Avenue, Sunnyvale | Sunnyvale City Councilmembers, City of Sunnyvale, VTA, WMH Corporation, members of the public | <p>The Project was presented at the Sunnyvale City Council and described the Project location, background, purpose, funding, development process, alternatives considered, challenges, and the DDI alternative. Comments from the public included:</p> <ul style="list-style-type: none"> • A request to incorporate Complete Streets concepts into design; • Concern about long traffic signal cycles with the DDI alternative; • A request for more details on accommodation of bicycles; • Concern about construction impacts to businesses near Mathilda Avenue and US 101; and • Support of all alternatives presented. |
| Public Scoping Meeting and Open House (flyer and fact sheets attached) | August 27, 2015 | Columbia Middle School 739 Morse Avenue, Sunnyvale | Caltrans District 4 staff, VTA, WMH Corporation, City of Sunnyvale, members of the public | <p>The Project was presented at a public scoping meeting and open house. The meeting provided an opportunity for the public to learn more about the Project and to provide input on the scope of the improvements. Twenty-one total comments were received: 19 were from members of the public, one comment letter was received from the California Transportation Commission, and one comment letter was received from the County of Santa Clara. Comments included:</p> <ul style="list-style-type: none"> • General safety concerns about pedestrian and bicycle access; • Concern about impeding company bus traffic; • Concern about long traffic signal cycles and too many stop lights; • Concern about air quality from traffic congestion; • Support of VTA increasing bus and LRT transit options; • A request to submit a Complete Streets checklist; • A request to not close Moffett Park Drive; and • Concern that closing the Moffett Park Drive connection would force bicyclists onto SR 237. |

| | | | | |
|--|----------------------------|---|--|---|
| VTA Bicycle and Pedestrian Committee | October 7, 2015 | VTA River Oaks Campus Conference Room B-104 3331 North First Street, San Jose | Caltrans District 4 staff; VTA; City of Sunnyvale; WMH Corporation; Bicycle, Pedestrian Advisory Committee | The Project was presented to the Bicycle and Pedestrian Committee on October 7, 2015. |
| Public Meeting during Public Comment Period of the Draft EIR | Anticipated in summer 2016 | TBD | Pending | Pending |

Mathilda Avenue Improvements at SR 237 and US 101 Project

- Receive a project overview and schedule.
- Receive a summarized project description.
- Give your comments on the environmental issues that will be discussed in the environmental document.

Thursday, August 27, 2015

5:30 p.m. - 7:00 p.m.

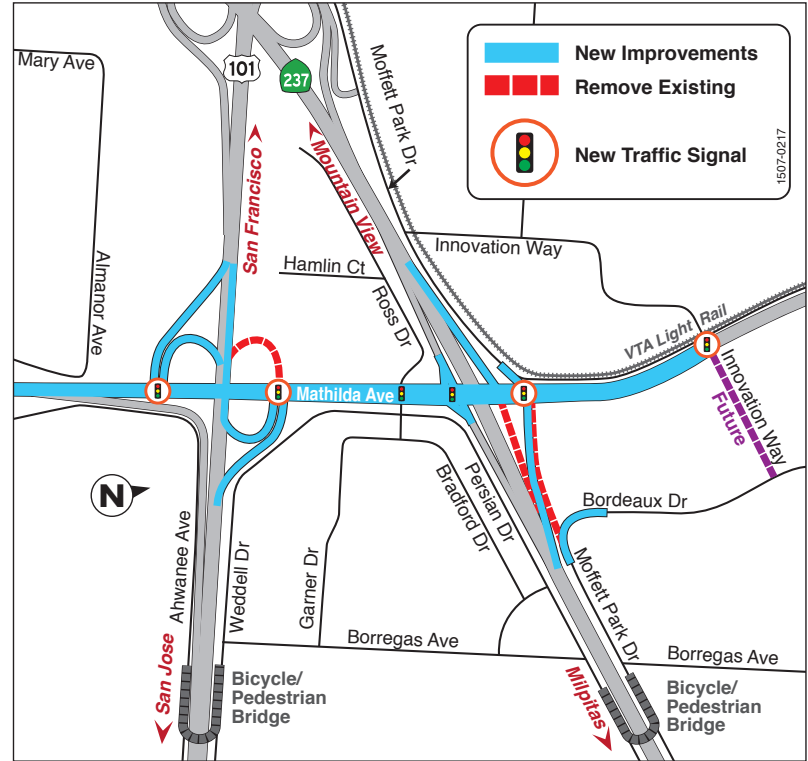
Columbia Middle School - Staff Lounge
739 Morse Avenue
Sunnyvale, CA 94085

Take VTA Bus Lines: 22, 26, 55, 62, and 522

For more information, please contact VTA Community Outreach at (408) 321-7575. The deadline for receiving comments on the project scope is September 15, 2015, by 5 p.m. Comments can be sent by email to MathildaAve@vta.org or by mail to:

VTA Environmental Programs and
Resources Management
Attn: Lani Ho
3331 North First Street, Bldg. B-2
San Jose, CA 95134-1927

Si desea más información en su idioma, por favor comuníquese con el Programa de Alcance a la Comunidad de VTA al (408) 321-7575.



Nếu quý vị muốn thông tin đã được dịch sang tiếng Việt, xin liên lạc Ban Tiếp Ngoại Cộng Đồng của VTA tại số (408) 321-7575.





SANTA CLARA

Valley Transportation Authority

3331 North First Street • San Jose, CA 95134-1927

PRESORTED
STANDARD
U.S. POSTAGE
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PERMIT NO. 589
SAN JOSE, CA

**Learn about the Mathilda Avenue
Improvements at SR 237 and US 101 Project
at a Public Scoping Meeting/Open House
for the Environmental Impact Report/
Environmental Assessment.**

We Want to Hear From You!

Come learn about the Mathilda Avenue improvements at SR 237 and U.S. 101 at a Public Scoping Meeting for the Environmental Impact Report.

The purpose of the project is to reduce congestion on Mathilda Avenue, improve mobility for all travel modes, and provide better access to local destinations.

Thursday, August 27

Columbia Middle School (Staff Lounge)
739 Morse Avenue, Sunnyvale 94085
5:30 p.m. to 7 p.m.

VTA Bus Line 55 is within walking distance of this location

The deadline for receiving comments on the project scope is 5 p.m. on September 15. For more information, please contact VTA Community Outreach at (408) 321-7575. Comments can be sent by email to MathildaAve@vta.org or by mail to:

VTA Environmental Programs and Resources Management, Attn: Lani Ho
3331 North First Street, Bldg. B-2
San Jose, CA 95134-1927

VTA's Upgraded IVR Coming Soon

To provide even better customer service, we will be making significant improvements to our automated route information phone system. New features include the ability to look up route times by bus stop number, text-to-speech functionality in English and Spanish, and more! The menu will change slightly, so remember to listen carefully when you call VTA Customer Service.

Need a Hand? Just Ask!

In response to new ADA rules, VTA will begin to further accommodate passengers with disabilities using bus and light rail services by making reasonable modifications to operating policies, practices, and procedures upon request. Reasonable modifications may include helping passengers insert money into fare boxes, allowing passengers to eat, drink or take medicine aboard a transit vehicle to avoid a medical problem, and permitting passengers to board separately from their mobility devices when the passenger can control the movement of the device.

Passengers may request modifications in advance or at the time they are needed. Passengers are not required to say "Reasonable Modification" when asking for an accommodation. VTA staff will work with passengers to find an alternative approach to accommodate their accessibility needs if a request for a policy, practice, or procedural modification cannot be fulfilled.

To make a request for a reasonable accommodation, please contact VTA Customer Service. Visit vta.org/reasonablemod for more information.

Help Us Enhance Your Walking Experience

VTA would like to learn how your walk to the bus stop or train station could be improved. Your answers will help us create a **Pedestrian Access to Transit Plan**. We will use this plan to work with cities on improving pedestrian access to bus stops and train stations. Please take a moment to complete the survey at vta.org/pedestrian-plan.

National Night Out

Join VTA at this year's National Night Out on Tuesday, August 4. National Night Out is a crime and drug prevention event that is sponsored nationally by the National Association of Town Watch and co-sponsored by local organizations.

This year is the 36th anniversary of this event with over 37 million people across the country expected to participate. VTA will be participating in National Night Out at the **Mayfair Community Center, 2039 Kammerer Avenue, San Jose from 4 p.m. to 7 p.m.**

Learn about safety and city services and all the transportation options available to the community. More than 20 public agencies and non-profit groups will be available to share their information.

Don't miss this once-a-year event and come celebrate our community.

This location is served by VTA Bus Lines 22, 70, and 77.

Convivio Comunitario Nacional

Únase con VTA para participar en el Convivio Comunitario Nacional el martes, 4 de agosto. El Convivio Comunitario es un evento para ayudar a prevenir el crimen y abuso de drogas y es patrocinado a nivel nacional por "National Association of Town Watch" y copatrocinado por organizaciones locales.

Este evento se ha celebrado durante los últimos 36 años y se espera que participen más de 37 millones de personas. VTA estará presente en el Centro Comunitario Mayfair, 2039 Kammerer Avenue en San José de 4 p.m. a 7 p.m.

Aprenda acerca de la seguridad y los servicios que ofrece la ciudad de San José, además de todas las opciones que hay disponibles para la comunidad. Habrá más de 20 agencias públicas y agencias no lucrativas que estarán disponibles para compartir información.

¡No se pierda este evento ya que es sólo una vez al año!

Tome las líneas de autobús de VTA 22, 70, o 77, para llegar a este evento.

39th Almaden Valley Art & Wine Festival

Presented by the Almaden Valley Women's Club, the annual Almaden Valley Art & Wine Festival will be held in beautiful Almaden Lake Park, on Sunday, September 20, from 10 a.m. to 6 p.m. Admission is free.

Voted one of the best festivals in San Jose, the Almaden Valley Art & Wine Festival features a large selection of local artisans, entertainment by popular bands throughout the day on our main stage, boutique wines from Northern California

vineyards, a variety of food offerings to taste including gourmet food trucks, a Kids-Zone with crafts, carnival games, and rides, souvenir wine and beer glasses, a silent auction, and much more.

Festival attendees are encouraged to use public transit and ride bicycles – please contact VTA for your customized trip plan.

This location is served by VTA Light Rail and Bus Line 64.

Free Admission

Los Gatos

Fiesta de Artes

August Sat 8 & Sun 9 2015 10 a.m. - 6 p.m.

Food Trucks • Wine • Art • Live Music • Kids Zone

110 E. Main Street
Civic Center in Downtown Los Gatos

Buses from the Winchester Light Rail Station
Parking at the Los Gatos High School
408.395.8016 • www.lgfiesta.org

VTA Customer Service Call Center(408) 321-2300

From 650 area code and South Santa Clara County toll area.(800) 894-9908

- Listen to recorded route and schedule information
 - 24 hours a day in English and Spanish
- Speak with an Information Service Representative
 - Weekdays: 6 a.m. – 7 p.m., Saturday: 7:30 a.m. – 4 p.m.

Hearing Impaired TTY only(408) 321-2330

VTA Website vta.org

VTA Downtown Customer Service Center
55-A West Santa Clara St., San Jose, CA 95113
Weekdays: 9 a.m. – 6 p.m., closed weekends and most holidays

VTA River Oaks Administrative Offices
3331 N. First St., San Jose, CA 95134
Weekdays: 8 a.m. – 4:30 p.m., closed weekends

VTA Take-One

August 2015

Take VTA to Art & Wine Festivals

What's Inside:

- New ADA Reasonable Modifications
- San Jose Jazz Festival
- National Night Out
- Art & Wine Festivals in Mountain View and Almaden
- Silicon Valley Pride

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Mountain View Art & Wine Festival

September 12 and 13
10 a.m. to 6 p.m.

Festival insiders know the Mountain View Art & Wine Festival is the crême de la crême on the Bay Area festival scene. Voted “Best Festival in the South Bay” multiple times by readers of *Metro* and still hitting on all cylinders better than ever, this year’s 44th annual festival promises to be a “festival like no other.”

Come experience an authentic and moveable feast for the senses:

- The cool, vibrant, multicultural Castro Street vibe
- An all-new premium wine tasting pavilion – “Wine Haven, Taste of the Mountains Passport Days”
- Exceptional handcrafted work by 600 of America’s top artists and craft makers
- Stellar live music on stage and street throughout downtown plus the return of mega-hit “Salsa Sunday”
- Fabulous food and drink

- The Comcast Pigskin Party Lounge with giant screen TV
- Artisan specialty food purveyors
- Home and garden exhibits
- Health and wellness displays
- An organic and green products showcase
- Tons of fun and games for kids with ultra-thrilling bungee jumping, roll-on-water “waterballerz” and other amazing attractions
- An affordable, sun-splashed, memorable, leisure-filled weekend



Widely considered one of America’s top art festivals, huge throngs of art lovers are expected to pour onto Castro Street in Silicon Valley’s epicentre for this “Cultural Community Celebration” presented by the Chamber of Commerce Mountain View. Admission is free.

This location is served by VTA Light Rail (exit at the Mountain View Transit Center) and VTA Bus Lines 22, 35, and 522.

San Jose Jazz Summer Fest

August 7 to August 9

The San Jose Jazz Festival started on one stage in 1990 and has grown into one of the nation’s most important music festivals, featuring 100+ performances of the best in jazz, blues, R&B, funk, New Orleans, zydeco, and more. In recent years, the Fest has become renowned for its top-flight Latin artists, presented on stages throughout the event. Summer Fest is not just a place to sit and listen; the 12 indoor and outdoor stages provide a variety of experiences and music. The Fest’s centerpiece is the Kaiser Permanente Main Stage located in the Plaza de

Cesar Chavez Park, fronting the Fairmont San Jose, but the tight footprint of the Fest makes it easy to sample everything the Fest has to offer. You’ll also want to take part in “Big Easy Parade” on Saturday.

There’s something for everyone and, even with its awesome scale and breadth, the Fest has remained one of the most affordable events of its kind. And there’s more than just music—the Fest is the perfect summer experience, with fantastic weather, great food, wine, and microbrews; music-themed film screenings and a jazz mass; a family fun zone with great activities for the kids and evening activities for the grown-ups like Fest+ concerts and a free club crawl.

VTA is excited to partner with the San Jose Jazz for the Summer Fest and encourage you to use public transportation in traveling to and from the festival.

For more information about the Summer Fest, visit jazzfest.sanjosejazz.org.



Chacho’s Taco Festival

Love tacos? Don’t miss Chacho’s Annual Taco Festival at St. James Park on Saturday, August 15 from 11 a.m. to 8 p.m. Enjoy live music, food trucks, and yummy tacos!

You’ll get to see the number one taco eating champion at the Taco Eating Contest. Last year’s winner ate 101 tacos in eight minutes during the festival. That’s about one taco every five seconds! Don’t miss the exciting competition and delicious tacos in downtown San Jose.

Log on chachostacofestival.com for ticket and event information.



This location is served by VTA Light Rail (exit at St. James Light Rail Station) and VTA Bus Lines 22, 23, 66, 72, 73, 82, 181, 323, and 522.

Second Harvest Food Bank – Access Made Easy

Sadly, many community members in Santa Clara County are unsure of where or when they will find their next meal. That’s why Second Harvest Food Bank of Santa Clara and San Mateo Counties has launched an innovative new texting program to connect hungry families to the nutritious food they need to thrive. Those who need food assistance can now get help from Second Harvest in three ways.

1. Text “GetFood” to “97779” (for Vietnamese, text “Free”; for Spanish, text “ComidaYa”); standard text messaging rates apply.

2. Call Second Harvest’s Food Connection multilingual hotline at (800) 984-3663.
3. Visit SHFB.org/getfood.

SHFB Food Connection Specialists can connect families and individuals to the CalFresh application assistance and free food programs through community partners.



Summer Happenings in August

Hop on board a VTA bus or light rail and check out these happening events in Santa Clara County!

The Tamale Festival

Saturday & Sunday, August 1 and 2
9 a.m. to 6 p.m.

sjtamalefest.com

Emma Prusch Farm Park, San Jose
Take VTA Bus Lines 12, 22, 25, and 77.

Thursday Night Live

Thursday, August 6, 5:30 p.m. to 8:30 p.m.

mountainview.gov/depts/cs/events/thursdaynight-live.asp

Castro Street at Dana Street
Downtown Mountain View

Take VTA Light Rail or Bus Line 35 or 52 to this event. VTA Bus Lines 22 and 522 are also available on El Camino Real.

4th Annual Silicon Valley Food and Art Festival

Sunday, August 30, 1:30 p.m. to 5:30 p.m.

svfoodart.org

Cupertino Quinlan Center, Cupertino
Take VTA Bus Lines 23, 25, 54, and 55.

Palo Alto Festival of the Arts

Saturday & Sunday, August 22 and 23
10 a.m. to 6 p.m.

mlaproductions.com/PaloAlto/

Downtown Palo Alto (University Avenue)
Take VTA Bus Lines 22, 35, or 522.

Italian Family Festa

Saturday & Sunday, August 29 and 30
11 a.m. to 8 p.m. (Sat); 11 a.m. to 6 p.m. (Sun)

italianfamilyfestasj.org

Guadalupe River Park, San Jose
Take VTA Light Rail or VTA Bus Lines 22, 63, 64, 68, 181, or 522.



Celebrate Silicon Valley Pride

Silicon Valley Pride is hosting a high-tech festival to celebrate Lesbian, Gay, Bisexual, and Transgender Pride with a parade and all-day events in downtown San Jose.

The parade and festival on Saturday, August 30, will spotlight the youth of our community with strong engagement from the Gay/Straight Alliance Network. The parade kicks off the celebration and begins at 10 a.m. from Market Street and ends at the festival grounds. The festival follows at noon on Almaden Boulevard, between San Carlos and Park Avenue.

The Adobe Stage will entertain festival goers with live bands, international singing sensations, and top DJs. Don’t miss the fun!

Visit svpride.com for more information and to purchase tickets. This event is made possible thanks to the generous support of Adobe, Alaska Airlines, and the many sponsors and community allies.

This location is served by VTA Light Rail (exit at the Convention Center Station) and VTA Bus Lines 22, 23, 63, 64, 66, 68, 72, 73, 82, 181, 323, 522, and DASH.

TỜ THÔNG TIN: Đường cao tốc

Cải thiện Đại lộ Mathilda Avenue tại SR 237 và US 101

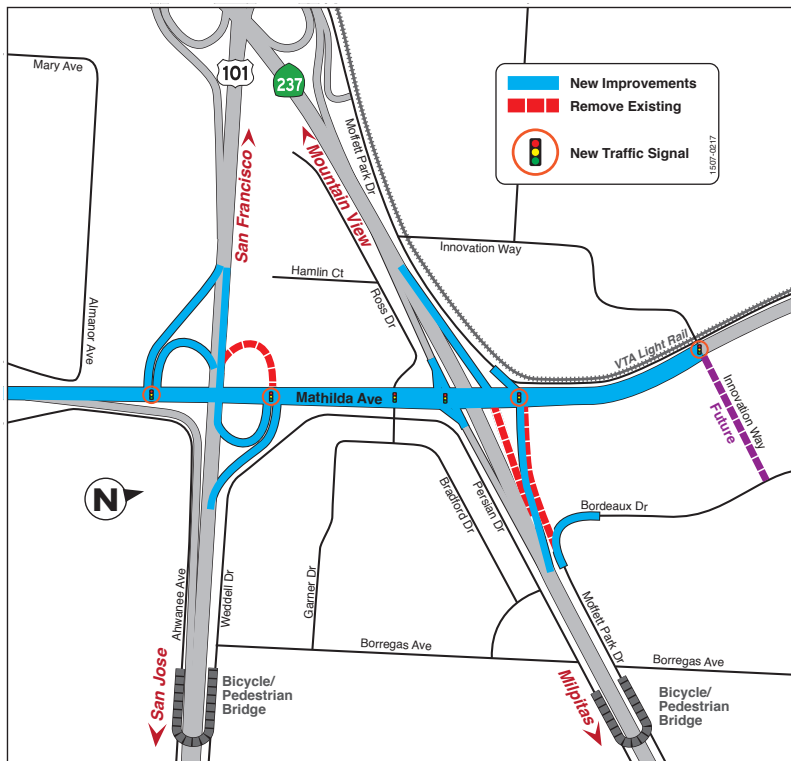
Tổng quan

Dự án đề xuất cải thiện Đại lộ Mathilda Avenue ở thành phố Sunnyvale từ Đại lộ Almanor Avenue đến đường Innovation Way, bao gồm cải thiện các dốc thoải lên xuống tại các giao lộ đường tiểu bang 237 / Đại lộ Mathilda Avenue và US 101 / Đại lộ Mathilda Avenue.

Cải thiện cụ thể bao gồm sửa đổi các dốc thoải lên xuống; loại bỏ, bổ sung, và lắp hệ thống tín hiệu tại các nút giao thông; cung cấp các làn đường rẽ trái mới, và sửa đổi để cải thiện việc tiếp cận của xe đạp và người đi bộ.

Mục tiêu

Để giảm tắc nghẽn trên Đại lộ Mathilda Avenue, cải thiện tính cơ động cho tất cả các hình thức đi lại, và cung cấp đường đi tốt hơn tới các điểm đến trong toàn thành phố Sunnyvale.



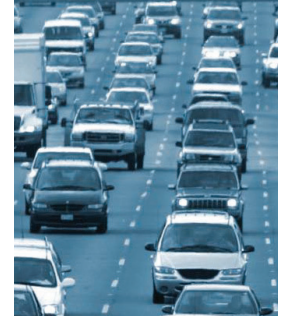
Lịch trình dự án

| | |
|-----------------------|-----------------|
| Phê chuẩn môi trường: | Giữa 2017 |
| Hoàn thành thiết kế: | Đầu 2018 |
| Thi công dự án: | Sẽ được công bố |

Liên hệ với chúng tôi

Nếu bạn có bất kỳ câu hỏi về việc Cải thiện Đại lộ Mathilda Avenue dự án SR 237 và US 101, xin vui lòng gọi cho Ban Tiếp Ngoại Cộng đồng VTA tại (408) 321-7575, (TTY) cho những người khiếm thính (408) 321-2330. Bạn cũng có thể ghé thăm chúng tôi trên web tại www.vta.org/mathildaimprovements, hoặc gửi email cho chúng tôi tại community.outreach@vta.org.

Đối tác tài trợ Dự án



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FACT SHEET: *Mga Highway*

Mga Pagpapahusay sa Mathilda Avenue sa SR 237 at US 101

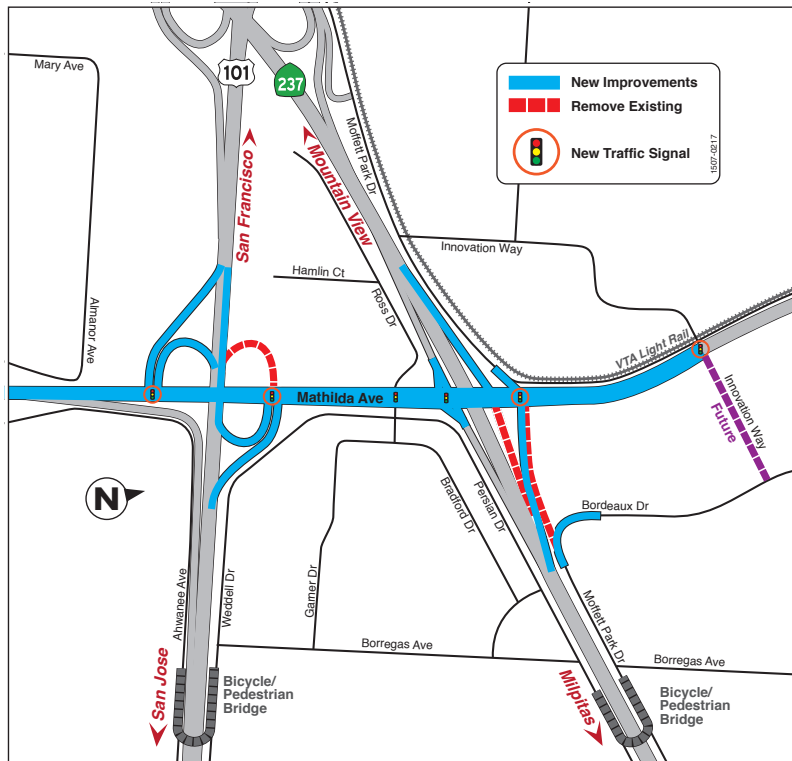
Pangkalahatang-ideya

Iminumungkahi ng Proyekto na pahasayin ang Mathilda Avenue sa Lungsod ng Sunnyvale mula Almanor Avenue hanggang sa Innovation Way, kabilang ang mga pagpapahusay sa on- at off-ramp sa mga interchange ng State Route 237/Mathilda Avenue at US 101/Mathilda Avenue.

Kabilang sa mga ispesipikong pagpapahusay ang modipikasyon sa mga on- at off-ramp; pag-alis, pagdaragdag at paglalagay ng signal sa mga interseksyon; paglalagay ng mga bagong linya para sa left-turn at modipikasyon sa pinahusay na linya para sa bisikleta at pedestrian.

Layunin

Upang bawasan ang pagsisikip ng trapiko sa Mathilda Avenue, pahasayin ang daloy ng lahat ng uri ng transportasyon at magbigay ng mas mahusay na access sa mga lokal na destinasyon sa buong lungsod ng Sunnyvale.



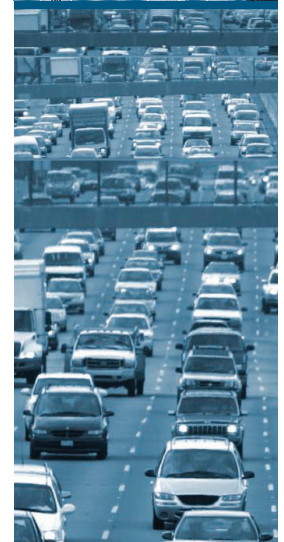
Iskedyul ng Proyekto

| | |
|----------------------------|-------------------------|
| Pag-apruba sa Kapaligiran: | Kalagitnaan ng 2017 |
| Pagkumpleto sa Disenyo: | Mga Unang Buwan ng 2018 |
| Konstruksyon sa Proyekto: | Iaunusyo |

Paano Kami Makokontak

Kung mayroon kang anumang mga katanungan tungkol sa Proyekto na Mga Pagpapahusay sa Mathilda Avenue sa SR 237 at US 101, mangyaring tumawag sa Community Outreach Department ng VTA sa (408) 321-7575, (TTY) para sa may kahirapan sa pandinig (408) 321-2330. Maaari mo rin kaming bisitahin sa web sa www.vta.org/mathildaimprovements, o mag-email sa amin sa community.outreach@vta.org.

Mga Kasama sa Pagpopondo ng Proyekto



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HOJA DE DATOS: Carreteras

Mejoras a Mathilda Avenue en la intersección de SR 237 y US 101

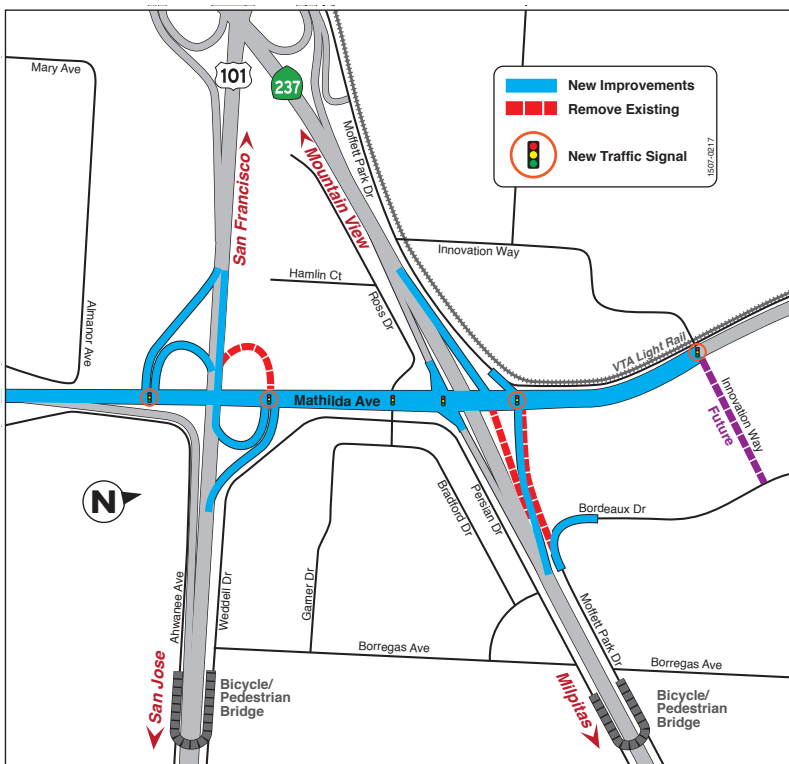
Visión general

El Proyecto propone mejorar Mathilda Avenue en la Ciudad de Sunnyvale desde Almanor Avenue hasta Innovation Way, incluyendo mejoras a las rampas de entrada y salida en los pasos a desnivel SR 237/Mathilda Avenue y US 101/Mathilda Avenue.

Las mejoras específicas incluyen modificaciones a las rampas de entrada y salida; remoción, adición y señalización de las intersecciones; provisión de nuevos carriles para vuelta a la izquierda, y modificaciones para mejorar el acceso de bicicletas y peatones.

Objetivo

Reducir la congestión vial en Mathilda Avenue, mejorar la movilidad para todo tipo de viaje, y proporcionar un mejor acceso a los destinos locales en toda la ciudad de Sunnyvale.



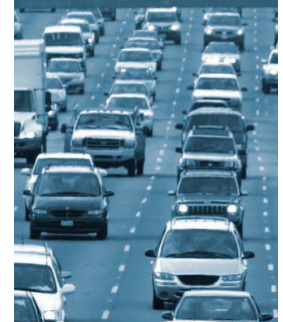
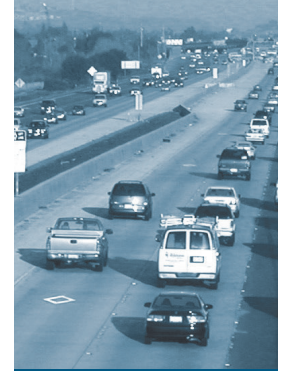
Calendario del proyecto

| | |
|----------------------------|-------------------|
| Aprobación ambiental: | Mediados de 2017 |
| Terminación del diseño: | Principio de 2018 |
| Construcción del proyecto: | Por anunciarse |

Cómo comunicarse con nosotros

Si tiene preguntas sobre el Proyecto de mejoras de Mathilda Avenue en la intersección de SR 237 y US 101, llame al Programa de Extensión a la Comunidad de VTA al (408) 321-7575, TTY para los que tienen incapacidad auditiva al (408) 321-2330. Usted puede visitarnos también en la red en www.vta.org/mathildaimprovements, o enviarnos un correo electrónico a community.outreach@vta.org.

Socios de financiamiento del proyecto



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기본 정보: 고속도로

237번 주도(SR)와 101번 국도 마틸다 애비뉴 개선 (Mathilda Avenue Improvements) 프로젝트

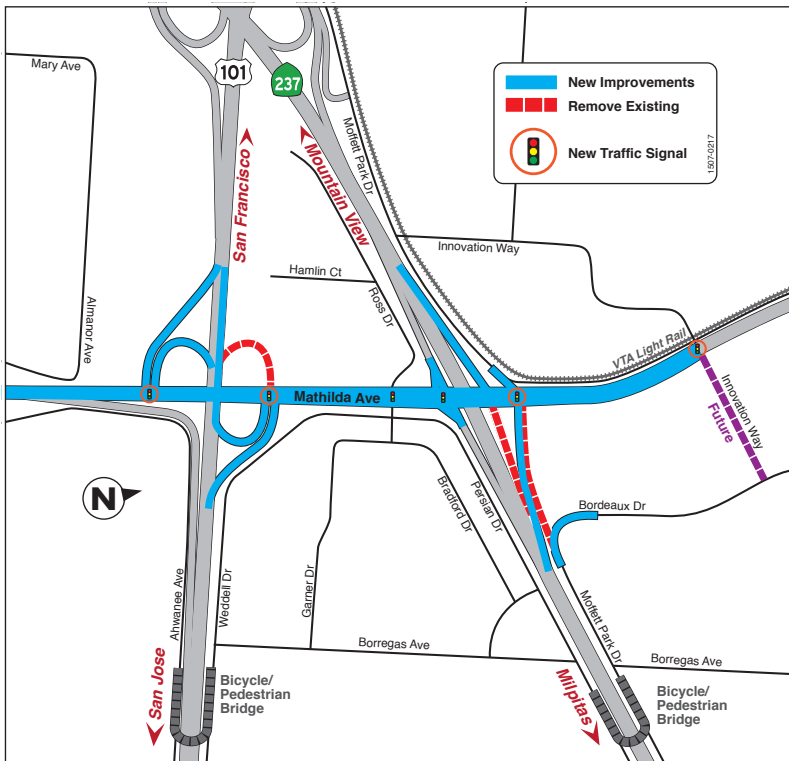
개요

이번 프로젝트에서는 237번 주도/마틸다 애비뉴와 101번 국도/마틸다 애비뉴 인터체인지의 진출입로 포함, 알마노 애비뉴(Almanor Avenue)에서 이노베이션 웨이(Innovation Way)까지의 서니베일(Sunnyvale)시 마틸다 애비뉴의 개선 작업이 제안되었습니다.

구체적인 개선 사항은 진출입로 변경, 교차로 제거/추가/신호 설치, 좌회전 차선 신설 및 자전거와 보행자 접근성 개선 등입니다.

목표

프로젝트의 목표는 마틸다 애비뉴의 교통 정체 감소, 교통 수단의 이동성 개선 및 서니베일 시 전체 로컬 지역에 대한 접근성 향상 등입니다.



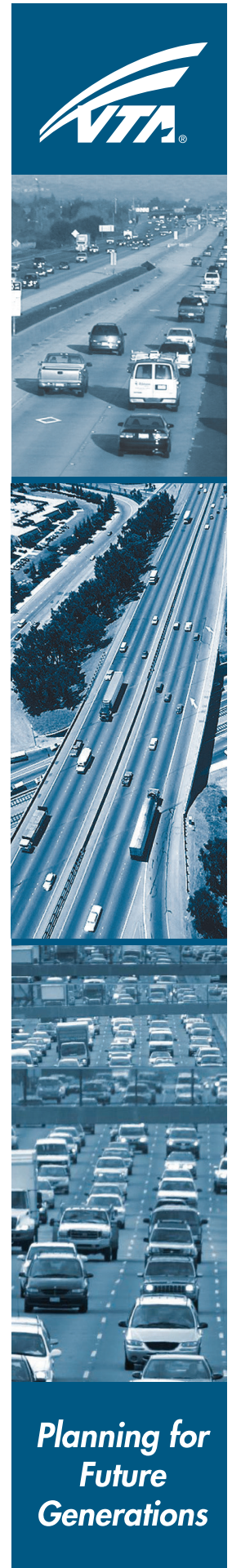
프로젝트 일정

환경 승인: 2017년 중반
 설계 완료: 2018년 초반
 공사: 추후 공지

문의처

237번 주도와 101번 국도의 마틸다 애비뉴 개선 프로젝트에 관해 더 자세한 정보를 원하시는 경우, VTA 지역봉사부 (408) 321-7575로 연락 주십시오. 청각 장애가 있으신 분들을 위해 TTY 모드 (408) 321-2330 도 제공하고 있습니다. 또한, 관련 웹페이지(www.vta.org/mathildaimprovements)를 확인하시거나, 이메일 (community.outreach@vta.org)로도 연락가능합니다.

프로젝트 기금 후원 파트너



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情况说明: 高速公路

对 237 号州道及 101 高速公路 Mathilda Avenue 路段的修

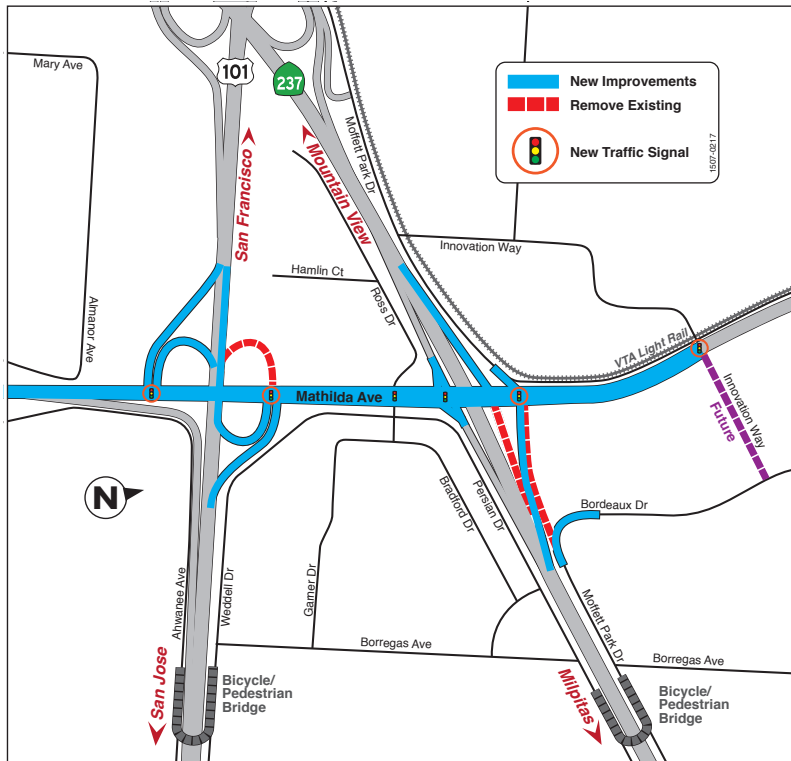
概况

这一项目提议修缮 Sunnyvale 市 Almanor Avenue 与 Innovation Way 之间的 Mathilda Avenue 路段，包括修缮 237 号州道/ Mathilda Avenue 及 101 高速公路/ Mathilda Avenue 的高速公路上下坡道。

具体内容包括：高速公路上下坡道改建；去除或增加交叉路口，在交叉路口安装交通信号；提供新的左转车道、改善自行车及行人的通行。

目

减缓 Mathilda Avenue 路面交拥挤状况，使所有交通方式运行畅通，使 Sunnyvale 市的交通更为便利。



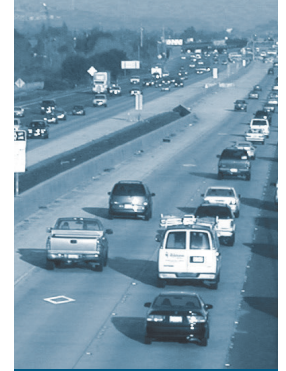
目时间表

| | |
|-------|---------|
| 环保审批: | 2017 年中 |
| 完成设计: | 2018 年初 |
| 项目施工: | 待公布 |

如何联系我

如果您对于 237 号州道及 101 高速公路 Mathilda Avenue 路段的修缮项目有任何问题，请打电话给 VTA 社区外展部。电话是：(408) 321-7575，TTY 听障者专线是 (408) 321-2330。您也可以访问我们的网站 www.vta.org/mathildaimprovements，或发电子邮件至 community.outreach@vta.org。

提供资金的合作伙伴



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FACT SHEET: **Highways**

Mathilda Avenue Improvements at SR 237 and US 101

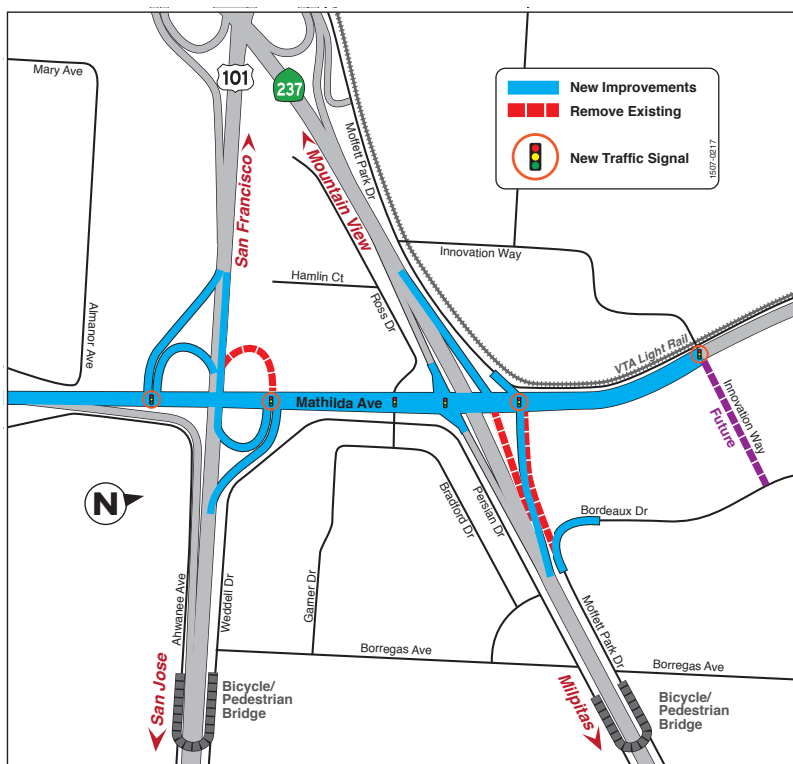
Overview

The Project proposes to improve Mathilda Avenue in the City of Sunnyvale from Almanor Avenue to Innovation Way, including on- and off-ramp improvements at the State Route 237/ Mathilda Avenue and U.S. 101/Mathilda Avenue interchanges.

Specific improvements include modification to on- and off-ramps; removal, addition, and signalization of intersections; provision of new left-turn lanes, and modification for improved bicycle and pedestrian access.

Objective

To reduce congestion on Mathilda Avenue, improve mobility for all travel modes, and provide better access to local destinations throughout the City of Sunnyvale.



Project Schedule

| | |
|-------------------------|-----------------|
| Environmental Approval: | Mid 2017 |
| Design Completion: | Early 2018 |
| Project Construction: | To be announced |

How to Reach Us

If you have any questions about the Mathilda Avenue Improvements at SR 237 and US 101 Project, please call VTA's Community Outreach Department at (408) 321-7575, (TTY) for the hearing-impaired (408) 321-2330. You may also visit us on the web at www.vta.org/mathildaimprovements, or email us at community.outreach@vta.org.

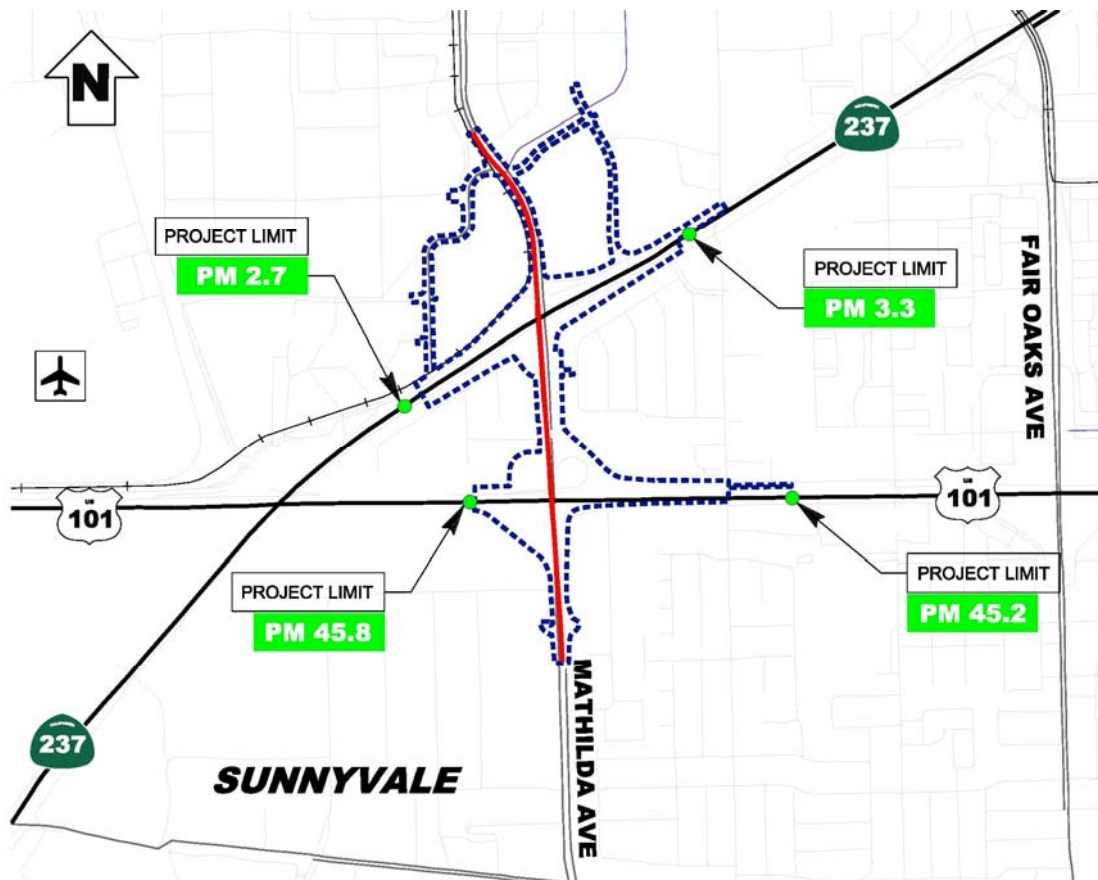
Project Funding Partners



Initial Site Assessment

for the

MATHILDA AVENUE IMPROVEMENTS AT SR 237 AND US 101 PROJECT



Prepared for:

Santa Clara Valley Transportation Authority

California Department of Transportation
District 4

Prepared by:

BASELINE Environmental Consulting

Dated: October 2015

For individuals with sensory disabilities, this document is available in Braille, in large print, on audiocassette, or on computer disk. To obtain a copy in one of these alternative formats, please write to Caltrans, Attn: Elizabeth White, Office of Environmental Planning, 111 Grand Avenue, Oakland, CA 94623-0660; or call (510) 286-6233 (voice); or use the California Relay Service TTY number, (800) 735-2929.

Initial Site Assessment

for the

MATHILDA AVENUE IMPROVEMENTS AT SR 237 AND US 101 PROJECT

on Mathilda Avenue from Almanor Avenue to Innovation Way; on SR 237 from 0.3 mile south of US 101/SR 237 Junction to 0.3 mile east of Mathilda Avenue Undercrossing; and on US 101 from 0.5 mile south of Mathilda Avenue to SR 237/US 101/SR 237 Junction in City of Sunnyvale, in Santa Clara County

SCL-237-PM 2.7/3.3; SCL-101-PM 45.2/45.8
EA 04-4H2900/Project ID 0413000204

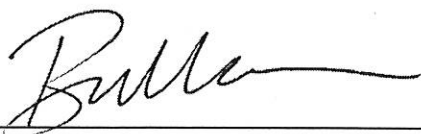
October 2015

U.S. DEPARTMENT OF TRANSPORTATION
STATE OF CALIFORNIA

and

Cooperating Agency: Santa Clara Valley Transportation Authority

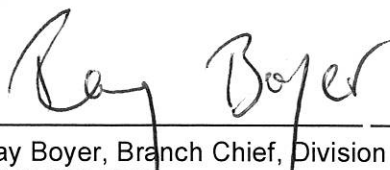
Prepared By:



Date: 12/21/2015

Bruce Abelli-Amen, Principal
(510) 420-8686
BASELINE Environmental Consulting

Approved By:



Date: 1-7-16

Ray Boyer, Branch Chief, Division of Environmental Planning & Engineering
(510) 286-5668
California Department of Transportation, District 4

Statement of Compliance: Produced in compliance with National Environmental Policy Act (NEPA) and California Environmental Quality Act (CEQA) requirements, as appropriate, to meet the level of analysis and documentation that has been determined necessary for this Project.

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INITIAL SITE ASSESSMENT

Mathilda Avenue Improvements at SR 237 and US 101 Project

EXECUTIVE SUMMARY

BASELINE Environmental Consulting (“BASELINE”) conducted this Initial Site Assessment (ISA) for the “Mathilda Avenue Improvements at SR 237 and US 101 Project” (Project). The Project proposes to improve Mathilda Avenue in the City of Sunnyvale from Almanor Avenue to Innovation Way, including on- and off-ramp improvements at the State Route 237/Mathilda Avenue and U.S. Highway 101/Mathilda Avenue interchanges (Figure 1). Two Build Alternatives, Build Alternative 1 and Build Alternative 2, are being considered for the Project (Figures 2a and 2b). Project improvements for both Build Alternatives would include reconfiguration of existing roadways and intersections, new bicycle and pedestrian facilities, utility relocations, new stormwater treatment facilities, new safety lighting, ramp metering modifications, modification of overhead signage, and a new retaining wall.

The purpose of this ISA was to identify and evaluate the level of risk associated with hazardous materials, hazardous waste, and/or contamination within the Project limits that could potentially result from the proposed construction activities and/or operations. This ISA has identified low and medium risks associated with the following hazardous material concerns:

- Potential aerially-deposited lead in exposed shallow soils – **Medium Risk**
- Potential groundwater impacts from a regional chlorinated solvent plume (Sites 1, 2, and 4 through 7 on Table 3 and Figure 6) – **Low Risk**
- Potential groundwater impacts from residual petroleum hydrocarbons release at Shell (Site 9 on Table 3 and Figure 6) – **Low Risk**
- Potential groundwater impacts from residual petroleum hydrocarbons released at Wolco Oil Co. (Site 11 on Table 3 and Figure 6) – **Low Risk**
- Potential groundwater impacts from chlorinated solvents, methylene chloride, and metals potentially released at Circo Inc (Site 12 on Table 3 and Figure 6) – **Low Risk**
- Potential groundwater impacts from residual petroleum hydrocarbons released at Moffet Park Auto Center (Site 14 on Table 3 and Figure 6) – **Low Risk**
- Potential arsenic and organochlorine pesticides in shallow soils across the entire Project site from historical agriculture (Figure 5) – **Low Risk**
- Potential naturally-occurring asbestos in fill embankments – **Low Risk**
- Potential lead-based paint and asbestos-containing materials on US 101 overpass – **Low Risk**
- Potential metals in drainage swale and catch basin sediments from stormwater runoff – **Low Risk**
- Potential lead and chromium in yellow thermoplastic and yellow paint striping and markings on roadways – **Low Risk**

- Petroleum hydrocarbons, metals, and high pH in asphalt and Portland-cement concrete grindings – **Low Risk**

Risk levels associated with hazardous material concerns identified within the Project limits are summarized for each Build Alternative in Matrix 1, below. The associated risks identified in this ISA would generally apply equally to each Build Alternative.

MATRIX 1: Summary of Risk Levels for each Build Alternative

| Hazardous Materials Concern | Risk Level | Media Affected | Primary Contaminants of Concern | Build Alternatives | |
|---|------------|-----------------------|---|--------------------|---|
| | | | | 1 | 2 |
| Aerially-Deposited Lead | Medium | Soil | Lead | X | X |
| Hazardous Materials Release Sites* | Low | Groundwater | Petroleum Hydrocarbons, Chlorinated Solvents, Methylene Chloride, and/or Metals | X | X |
| Agricultural Pesticides | Low | Soil | Arsenic and Organochlorine Pesticides | X | X |
| Naturally-Occurring Asbestos | Low | Soil | Asbestos | X | X |
| Lead-Based Paint and Asbestos-Containing Material | Low | Construction Material | Lead and Asbestos | X | X |
| Drainage Swales and Catch Basins | Low | Soil | Metals | X | X |
| Yellow Thermoplastic/Paint Striping and Markings | Low | Construction Material | Lead and Chromium | X | X |
| Asphalt and Portland-Cement Concrete Grindings | Low | Construction Material | Petroleum Hydrocarbons and Metals | X | X |

* Five potential groundwater plumes that pose a risk to the Project are identified in Section 5.

Once a preferred Build Alternative has been chosen and areas of excavation and pavement disturbance are determined, BASELINE recommends performing a Preliminary Site Investigation (PSI) to investigate hazardous materials concerns related to soil, groundwater, and construction materials on the Project site, as identified in this ISA. All environmental investigations for the Project should be performed in accordance with a Workplan approved by Caltrans, and the findings should be provided to the Project contractors to incorporate into their Health and Safety and Hazard Communication programs. Project construction should be conducted under a project-specific Construction Risk Management Plan to protect construction workers, the general public, and the environment from hazardous materials in soil, groundwater, and/or construction materials identified in the PSI and/or undocumented sources.

INITIAL SITE ASSESSMENT

Mathilda Avenue Improvements at SR 237 and US 101 Project

1. INTRODUCTION

The California Department of Transportation (Caltrans), in cooperation with the Santa Clara Valley Transportation Authority (VTA) and the City of Sunnyvale, is proposing the “Mathilda Avenue Improvements at SR 237 and US 101 Project” (Project) to improve Mathilda Avenue in the City of Sunnyvale from Almanor Avenue to Innovation Way, including on- and off-ramp improvements at the State Route (SR) 237/Mathilda Avenue and U.S. Highway 101 (US 101)/Mathilda Avenue interchanges. On SR 237, the Project limits are from 0.3 miles east of the US 101/SR 237 interchange (post mile [PM] 2.7) to 0.3 miles east of the Mathilda Avenue undercrossing (PM 3.3). On US 101, the Project limits are from 0.5 miles south of Mathilda Avenue overcrossing (PM 45.2) to 0.3 miles south of SR 237/US 101 interchange (PM 45.8). The total length of the Project on Mathilda Avenue is approximately 1 mile. Figure 1 shows the location of the Project.

The purpose of this Initial Site Assessment (ISA) is to identify and evaluate the level of risk associated with hazardous materials, hazardous waste, and/or contamination within the Project limits that could potentially result from the proposed construction activities and/or operations. This assessment was prepared by BASELINE Environmental Consulting (BASELINE) with review and approval by Caltrans.

2. PROJECT DESCRIPTION

This section describes the purpose and scope of the proposed Project.

2.1 Purpose and Need

The primary purpose of the Project is to improve traffic operations on Mathilda Avenue through the US 101 and SR 237 interchanges. Specifically, the goals and objectives of the Project are to:

- Reduce congestion and improve traffic operations along Mathilda Avenue and at the SR 237/Mathilda Avenue and US 101/Mathilda Avenue interchanges.
- Improve mobility for all travel modes in the area including motor vehicles, transit, bicycles, and pedestrians.
- Provide standard crosswalks and sidewalks along Mathilda Avenue, improving access to local destinations such as Moffett Park, the VTA Light Rail Transit (LRT) stations, and downtown Sunnyvale.

The Project is needed for the following reasons:

- Regional growth and new local development combined with inefficient roadway operations has resulted in substantial traffic congestion on Mathilda Avenue.
- Efficient access for all travel modes into and out of downtown Sunnyvale and development to the north of SR 237 is critical to a healthy and sustainable economy. Congestion on Mathilda Avenue adversely affects the economic vitality of the City of Sunnyvale.

Overall, the Project is needed to address several issues in the Project area including roadway deficiencies, lack of or discontinuous bicycle and pedestrian access, improvement of local roadway and freeway ramp operations, and provision of access to current and future economic development.

2.2 Project Description and Alternatives

The Project alternatives that were developed to meet the purpose and need of the Project include Alternative 1 (Figure 2a), Alternative 2 (Figure 2b), and the No-Build Alternative. Under the No-Build Alternative, no changes would be made to the existing local roadways or freeway system within the Project limits. No construction activities would occur, and there would be no change in the operations of the existing facilities.

The design features of the two Build Alternatives include reconfiguration of the US 101 and SR 237 interchanges with Mathilda Avenue. The Build Alternatives include design variations for reconfigured roadways and intersections, and construction of new signalized intersections. Proposed improvements included in the Build Alternatives south of Ross Drive on Mathilda Avenue and at the US 101 interchange, are identical. This includes new bicycle and pedestrian facilities, utility relocations, new storm water treatment facilities, new safety lighting, ramp metering modifications, modification of overhead signage, and a new retaining wall. Unique improvements, north of Ross Drive on Mathilda Avenue, primarily include improvements related to construction of a diverging diamond interchange¹ under Build Alternative 2 (Figure 3).

2.2.1 Roadway Improvements

The Build Alternatives would consist of the following roadway improvements:

- Provide three continuous through lanes in each direction of Mathilda Avenue.
- Remove northbound US 101 loop off-ramp and shift traffic to northbound US 101 diagonal off-ramp.

¹ A diverging diamond interchange, also called a double crossover diamond interchange, is a type of diamond interchange where traffic briefly crosses over to the left (opposite) side of the roadway, guided by traffic signals at each crossover. This allows vehicles to turn left onto freeway on-ramps without stopping and without conflicting with through traffic. The signals at ramp terminal intersections can be operated with two signal phases (a signal phase allows for traffic at an intersection to cycle through specific movements for each direction) instead of three.

- Realign and widen northbound ramps and signalize ramp intersection with Mathilda Avenue, and construct left-turn lane on southbound Mathilda Avenue to access northbound US 101 loop on-ramp.
- Realign southbound US 101 off-ramp and loop on-ramp and signalize ramp intersection with Mathilda Avenue.
- Modify Mathilda Avenue / Ross Drive signal intersection.
- Close Moffett Park Drive between Bordeaux Drive and Mathilda Avenue, replace with a Class I bikeway (as described below), and shift traffic to Bordeaux Drive and Innovation Way.²
- Remove westbound SR 237 ramp signal intersection. Realign westbound SR 237 off-ramp opposite Moffett Park Drive and modify signal intersection.
- Build Alternative 1 would modify westbound SR 237 ramps to provide a diamond configuration (see Figure 2a).
- Build Alternative 2 would modify Mathilda Avenue and SR 237 ramps to provide a diverging diamond configuration (see Figure 2b and Figure 3). Eastbound Moffett Park Drive between Innovation Way and Mathilda Way would be diverted to Innovation Way to access Mathilda Avenue.

2.2.2 Bicycle and Pedestrian Facilities

Enhanced bicycle and pedestrian facilities would be provided. Bicycle improvements on Mathilda Avenue would consider both Class II and Class III bikeways³, based on available pavement widths within the project limits, and would connect to the existing Class III bikeway north of Innovation Way and Class I bikeway on the Sunnyvale West Channel. Bicycle improvements on Moffett Park Drive would consist of a Class I bikeway between Bordeaux Drive and Mathilda Avenue. Between Mathilda Avenue and Innovation Way, Class II and Class III bikeways would be considered based on available pavement widths within the project limits. A continuous sidewalk would be provided on the east side of Mathilda Avenue within the project limits with crosswalks, curb ramps, and pedestrian countdown signals at each intersection. The new crosswalks at the reconfigured ramp intersections would be signalized.

3. METHODOLOGY

As shown in Figure 1, the limits of the Project site include all areas that could potentially be disturbed during construction of the proposed improvements. BASELINE performed this assessment in accordance with Chapter 10 of the Caltrans *Environmental Handbook* (Caltrans, 2015a) to support the preliminary engineering and environmental review of the Project. As required by Caltrans, potential sources of contamination within the Project limits were identified as Recognized Environmental Conditions⁴ (RECs) in accordance with ASTM

² Innovation Way would be extended from Mathilda Avenue to Bordeaux Drive by the Moffett Place development project.

³ Class I bikeway is a bicycle path. Class II bikeway is a bicycle lane. Class III bikeway is bicycle route [Source: Highway Design Manual Index 1002.1]

⁴ RECs are defined in ASTM E1527-13 as “the presence or likely presence of any hazardous substances or petroleum products in, on, or at a property: (1) due to release to the environment; (2) under conditions indicative

International's (20013) Standard Practice Method E1527-13, *Standard Practice for Environmental Site Assessments: Phase I Environmental Assessment Process*. The scope of services for this ISA included review and evaluation of the physical setting, historical land uses, environmental records, and previous environmental investigations, as well as a site reconnaissance. A completed ISA checklist for the Project is included as Appendix A.

3.1 Recognized Environmental Conditions

In accordance with ASTM 1527-13, standard data sources were reviewed to identify sites associated with hazardous materials within 1 mile of the Project. The data sources included a site reconnaissance, United States Geological Survey (USGS) topographic maps, historical aerial photographs, environmental records derived from regulatory agency databases, and previous environmental investigations. Based on the review of data sources, potential sites of concern were further evaluated to identify releases of hazardous materials that could result in a REC in connection with the Project site. Risk levels associated with identified RECs were then assessed for each Build Alternative in accordance with the Caltrans *Environmental Handbook*.

3.2 Other Environmental Concerns

Based on the Caltrans *Environmental Handbook* and BASELINE's previous experience working on similar transportation infrastructure projects, other environmental concerns that could pose a risk to the Project, but are not considered RECs under ASTM 1527-13, were evaluated. These environmental concerns include the following: agricultural pesticides; aerially-deposited lead (ADL); naturally-occurring asbestos; lead-based paint and asbestos-containing materials; metals in soils from non-point source stormwater runoff; yellow traffic stripes and pavement markers; and asphalt-concrete and Portland-cement grindings. Following the evaluation of other environmental concerns, associated risk levels were assessed for each Build Alternative in accordance with the Caltrans *Environmental Handbook*.

4. REVIEW OF DATA SOURCES

This section describes the review of the physical setting, site reconnaissance, historical land uses, environmental records, and previous environmental investigations in the Project vicinity.

4.1 Physical Setting

The regional topography slopes gradually to the north-northeast with elevations ranging from about 20 to 40 feet (NAVD 88) along Mathilda Avenue (USGS, 2015) (Figure 4). The Project is generally underlain by Holocene alluvium (Graymer, R.W, et al., 2006). The Project crosses one waterway, Sunnyvale West Channel, near the intersection of Moffett Park Drive and Innovation

of a release to the environment; or (3) under conditions that pose a material threat of a future release to the environment." According to ASTM E1527-13, the term "REC" is not intended to include de minimis conditions that generally do not present a threat to human health or the environment and that generally would not be the subject of an enforcement action if brought to the attention of appropriate governmental agencies.

Way and the intersection of Mathilda Avenue and Innovation Way. The Sunnyvale West Channel generally drains north (Figure 4), eventually discharging into the San Francisco Bay.

Ambient groundwater level data were reviewed from the State Water Resources Control Board's (SWRCB) (2015) *GeoTracker* database for monitoring wells at two leaking underground storage tank (LUST) sites near the Project: the Texaco site at 724 Mathilda Avenue and the Professional Center site at 102 Persian Drive. Depth to groundwater generally ranges from about 7 to 15 feet below ground surface and groundwater generally flows to the north-northeast at both of the LUST sites. Based on the regional topography and previously measured groundwater levels, groundwater is expected to flow to the north-northeast across the Project site.

4.2 Site Reconnaissance

On 28 August 2015, BASELINE conducted a site reconnaissance to identify evidence of potential hazardous materials releases on the Project site and on adjoining properties. Evidence of potential hazardous materials releases could include on-site waste disposal, apparent odors, stained or discolored surfaces, and stressed or damaged vegetation. A windshield site reconnaissance was conducted for the entire Project alignment by Cem Atabek from BASELINE. Current land uses adjacent to Mathilda Avenue generally included residential, commercial, and industrial properties. Evidence of potential hazardous materials releases on or adjacent to the Project was not observed.

4.3 Historical Land Use Records

BASELINE reviewed historical land use records for the Project and surrounding area to identify potential sources of hazardous materials that may have resulted in a REC in connection with the Project. Historical land uses in the Project vicinity were determined by reviewing historical aerial photographs between 1939 and 2012 (EDR, 2015). The aerial photographs were geocoded and imported into a Geographic Information System (GIS) to spatially analyze land use developments relative to the Project location. The aerial photographs reviewed for this ISA are included in Appendix B.

As early as 1939 until as late as 1956, large portions of the Project site and surrounding area were being used for agriculture. During this time period, several agricultural structures (e.g., homesteads and barns) appeared to be located on portions of the Project site. In 1956, a large barn or warehouse structure appeared to be located at the current intersection of Ross Drive and Mathilda Avenue (Figure 5). By 1968, the current roadway/highway alignments for Mathilda Avenue, SR 237, and US 101 were constructed through the Project site, and adjacent land uses had been redeveloped as residential, commercial, and industrial properties. By the early 1990s, a portion of the VTA LRT line was constructed adjacent to Moffett Park Drive and the segment of Mathilda Avenue north of SR 237 on the Project site (EDR, 2015). The current land uses on and adjacent to the Project site have not changed significantly since the late 1960s.

4.4 Environmental Records

BASELINE reviewed environmental records that were reasonably ascertainable⁵ from standard sources⁶ to identify RECs in connection with the Project site. Standard environmental record sources for State-registered aboveground storage tank (AST) sites were not reviewed, because the records were not reasonably ascertainable. All facilities that have registered ASTs are required to submit information annually to the California Environmental Reporting System (CERS). Information about facilities stored in the CERS database is not currently available to the public.

The United States Coast Guard maintains the federal government's *National Response Center* database (formerly the ERNS database), which lists all reported hazardous materials releases or spills in quantities greater than the reportable quantities codified in 40 CFR Parts 302 and 355. The United States Environmental Protection Agency (USEPA) oversees facilities that generate, transport, store, treat, and/or dispose of hazardous waste as defined by the Resource Conservation and Recovery Act (RCRA). In California, the SWRCB and Department of Toxic Substances Control (DTSC) oversee the cleanup of contaminated properties. The SWRCB and DTSC also oversee the State's underground storage tank (UST) program and permitted hazardous waste facilities, respectively, to minimize the potential threat of future hazardous materials releases. The environmental record sources reviewed for this ISA were derived from the United States Coast Guard *National Response Center* database (Center for Effective Government, 2015), USEPA (2015) *RCRAInfo* database, SWRCB (2015) *GeoTracker* database, and DTSC (2015) *EnviroStor* database. A summary of the environmental record sources reviewed is provided on Table 1.

Site information from each record source was imported into a GIS program to spatially analyze sites within the minimum search distances defined by ASTM E1527-13 relative to the boundary of the Project site (Table 1). The spatial analysis identified one permitted UST facility and seven small-quantity RCRA generators adjacent to the Project site (Table 2). The spatial analysis identified 42 hazardous materials release sites within 1 mile of the Project site (Table 3).

4.5 Previous Environmental Investigations

Based on ascertainable data, previous environmental investigations have not been performed on the Project site. Numerous environmental investigations have been performed at hazardous materials release sites within 1 mile of the Project site identified during the review of environmental records. The findings of the previous environmental investigations at sites of potential concern are summarized below.

⁵ Information that is 1) publically available, 2) obtainable from its source within reasonable time and cost restraints, and 3) practically reviewable (ASTM 1527-13).

⁶ Defined in Section 8 of ASTM 1527-13.

5. EVALUATION OF RECOGNIZED ENVIRONMENTAL CONDITIONS

The review of environmental records identified seven small-quantity RCRA generators adjacent to the Project site. One of the seven RCRA generators referred to as “Shell Stn” was also identified as a permitted UST facility referred to as “Shell Oil Self-Serve” (Table 2). Two of the seven RCRA generators referred to as “Shell Stn” and “Pacific Bell” were also identified as known hazardous materials release sites referred to as “Shell” and “Pacific Bell”, which are discussed further, below. Hazardous materials releases have not been reported at the other five RCRA generator facilities; therefore, these facilities are not expected to pose a threat of affecting environmental conditions beneath the Project site.

The review of environmental records identified 42 sites with known hazardous materials releases within 1 mile of the Project site (Table 3 and Figure 6). Two release sites were identified within the boundaries of the Project site (Sites 16 and 17 on Table 3), nine release sites were identified on properties adjacent to the Project site, and six active release sites were identified hydrologically upgradient (to the south-southwest) of the Project site (Sites 1 through 17 on Table 3). Pending further evaluation, these 17 release sites were identified as sites of potential concern that could result in a REC in connection with the Project and are discussed further, below. The other 25 release sites (Sites 18 through 42 on Table 3) are not expected to pose a threat of affecting environmental conditions beneath the Project site because the cases are closed (i.e., cleanup is complete) or a pathway for contaminant migration onto the Project site does not exist (i.e., the site is downgradient).

Available information for the 17 release sites of potential concern was reviewed to determine if there are any RECs in connection with the Project. Groundwater quality data was screened against the San Francisco Bay Regional Water Quality Control Board’s (Regional Water Board’s) (2013) Environmental Screening Levels (ESLs) where groundwater is a potential drinking water resource. The 17 release sites of potential concern identified during the review of environmental records are discussed, below.

5.1 Regional Chlorinated Solvent Plume

Seven release sites of potential concern located south of US 101 and west of Mathilda Avenue are associated with a regional groundwater plume(s) of chlorinated solvents: California Microwave (Site 1), 645/675 Almanor, et al (Site 2), Litton Applied Technology (Site 3), Siemens Microelectronics Inc. (Site 4), Eaton & Signetics (Site 5), Zymos (Site 6), and Maxim Integrated Products Inc. (Site 7) (Table 3 and Figure 6). Numerous sources of chlorinate solvent releases have been identified as contributing to the regional groundwater impacts. The primary contaminants of concern (COCs) are tetrachloroethylene (PCE), trichloroethylene (TCE), and cis-1,2-Dichloroethene (cis-1,2-DCE).

The Regional Water Board is currently overseeing groundwater investigation and cleanup activities at all of the sites except Litton Applied Technology (Site 3) and Maxim Integrated Products Inc. (Site 7). The groundwater beneath Litton Applied Technology (Site 3) has been impacted primarily by cis-1,2-DCE that migrated onto the site from an upgradient source;

therefore, the Regional Water Board (1996) issued a letter for no further action related to the investigation and cleanup of contaminated groundwater at the site. Maxim Integrated Products Inc. (Site 7) is a former RCRA generator that the DTSC has listed as an inactive Corrective Action site requiring investigation of potential hazardous materials releases. However, the site is also referred to as “Zymos” (Site 6), which is currently being regulated by the Regional Water Board. For this assessment, Maxim Integrated Products and Zymos are considered the same site.

The extent of the regional chlorinated solvent plume(s) has not been defined. As shown in Figure 6, the closest monitoring well to the Project site that is associated with the chlorinated solvent plume, LF37A, is located approximately 200 feet west of the Project site near the entrance to the US 101 southbound off-ramp. Based on the most recent sampling event in 2007, concentrations of TCE and cis-1,2-DCE were reported at 44 micrograms per liter ($\mu\text{g/L}$) and 41 $\mu\text{g/L}$ in monitoring well LF37A, respectively (Environ International Corporation, 2007). These concentrations exceed the current Regional Water Board (2013) groundwater ESLs for TCE and cis-1,2-DCE of 5.0 $\mu\text{g/L}$ and 6.0 $\mu\text{g/L}$, respectively. Chlorinated solvents from the regional plume(s) could potentially extend beneath the Project site at concentrations exceeding the groundwater ESLs.

5.2 Leaking Underground Storage Tank sites

Six of the release sites of potential concern were identified as LUST sites with Regional Water Board oversight for investigation and/remediation, as described further, below.

5.2.1 Thrifty #165

In 1983, a release of petroleum hydrocarbons was reported from LUSTs at the former Thrifty #165 (Site 8 on Table 3 and Figure 6), which was located adjacent to the southern terminus of the Project. The primary COC was total petroleum hydrocarbons as gasoline (TPHg). In 1996, a case closure letter was issued for the site after remediation had reduced TPHg concentrations in groundwater to 71 $\mu\text{g/L}$ (Santa Clara Valley Water District, 1996), which is below the current Regional Water Board (2013) groundwater ESL of 100 $\mu\text{g/L}$; therefore, residual petroleum hydrocarbon contamination from the site (if any) would not be expected to impact the Project.

5.2.2 Shell

In 1984, a release of petroleum hydrocarbons was reported from LUSTs at Shell (Site 9 on Table 3 and Figure 6), which is located adjacent to the southern terminus of the Project. The primary COCs were TPHg, benzene, toluene, ethylbenzene, total xylenes (BTEX), and methyl tert-butyl ether (MTBE). In 2004, a case closure letter was issued for the site; however, residual petroleum hydrocarbon contamination remained on the site. As shown in Figure 6, the closest monitoring well to the Project site, S-7, was located on the Project site. Based on the most recent sampling event in 2002, a concentration of MTBE was reported at 9.6 $\mu\text{g/L}$ in monitoring well S-7 (County of Santa Clara Department of Environmental Health, 2004a), which exceeds the current Regional Water Board (2013) groundwater ESL of 5.0 $\mu\text{g/L}$; therefore, residual petroleum hydrocarbon contamination from the site (if any) could potentially extend beneath the Project site at concentrations exceeding the groundwater ESLs.

5.2.3 Pace Distributors

In 1990, a release of petroleum hydrocarbons was reported from a LUST at Pace Distributors (Site 10 on Table 3 and Figure 6), which is located adjacent to the southern terminus of the Project. Relatively low concentrations of TPHg and BTEX were reported in groundwater below the current Regional Water Board (2013) groundwater ESLs. In 1991, a case closure letter was issued for the site (Regional Water Board, 1991). Residual petroleum hydrocarbon contamination from the site (if any) would not be expected to impact the Project.

5.2.4 Wolco Oil Co. (Borregas)

In 1984, a release of petroleum hydrocarbons was reported from LUSTs at Wolco Oil Co. (Borregas) (Site 11 on Table 3 and Figure 6), which was located near the US 101 southbound on-ramp. The primary COCs were TPHg, total petroleum hydrocarbons as diesel (TPHd), BTEX, and MTBE. A petroleum hydrocarbon plume migrated north from the site and extended beneath the Project site. In 2004, a case closure letter was issued for the site; however, residual petroleum hydrocarbons remained beneath the site. As shown in Figure 6, monitoring well B10 was located on the Project site. Based on the most recent sampling events in 2001 and 2003, concentrations of TPHg, benzene, and MTBE were reported at 250 µg/L, 12 µg/L, and 21 µg/L, respectively, in monitoring well B10 (County of Santa Clara Department of Environmental Health, 2004b). These concentrations exceed the current Regional Water Board (2013) groundwater ESLs for TPHg, benzene, and MTBE of 100 µg/L, 1.0 µg/L, and 5.0 µg/L, respectively. Residual petroleum hydrocarbon contamination from the site (if any) could potentially extend beneath the Project site at concentrations exceeding the groundwater ESLs.

5.2.5 Pacific Bell

In 1996, a release of petroleum hydrocarbons was reported from a LUST at Pacific Bell (Site 13 on Table 3 and Figure 6), which is located adjacent to the north terminus of the Project. The primary COC was TPHd. In 1997, a case closure letter was issued for the site (DTSC, 2015). Since groundwater generally flows to the north-northeast (see Section 4.1, *Physical Setting*), residual petroleum hydrocarbon contamination (if any) would not be expected to migrate beneath the Project.

5.2.6 Moffet Park Auto Center

In 1988, a release of petroleum hydrocarbons was reported from LUSTs at Moffet Park Auto Center (Site 14 on Table 3 and Figure 6), which is located adjacent to the north terminus of the Project. The primary COCs were TPHg, BTEX, and MTBE. In 2000, a case closure letter was issued for the site; however, residual petroleum hydrocarbons remained beneath the site. As shown in Figure 6, monitoring well MW-1-R2 was located about 30 feet from the Project site. Based on the most recent sampling event in 2000, concentrations of TPHg, benzene, ethylbenzene, and total xylenes were reported at 2,300 µg/L, 2.6 µg/L, 190 µg/L, and 46 µg/L, respectively, in monitoring well MW-1-R2 (Santa Clara Valley Water District, 2000). These concentrations exceed the current Regional Water Board (2013) groundwater ESLs for TPHg, benzene, ethylbenzene, and total xylenes of 100 µg/L, 1.0 µg/L, 30 µg/L, and 20 µg/L,

respectively. Residual petroleum hydrocarbon contamination from the site (if any) could potentially extend beneath the Project site at concentrations exceeding the groundwater ESLs.

5.3 Corrective Action Site

Circo Inc. (Site 12 on Table 3 and Figure 6) is a former RCRA generator that the DTSC has listed as an inactive Corrective Action site requiring investigation of potential hazardous materials releases. The facility formerly manufactured printed circuit boards using organic solvents, cleaners, strippers, acids, caustics, cyanide, and metal plating solutions. In 1983, concentrations of methylene chloride, trans-1,2,-dichloroethene, TCE, and zinc were reported in a groundwater sample collected beneath a sump at 60 µg/L, 47 µg/L, 9 µg/L, and 470 µg/L, respectively (Ecology and Environment, Inc., 1990). These concentrations exceed the current Regional Water Board (2013) groundwater ESLs for methylene chloride, trans-1,2,-dichloroethene, TCE, and zinc of 5.0 µg/L, 10 µg/L, 5.0 µg/L, and 81 µg/L, respectively. The groundwater analytical results indicate that a hazardous materials release may have occurred on the property. Based on review of the DTSC (2015) *EnviroStor Database*, it does not appear that additional investigations were conducted to further evaluate the potential source and extent of groundwater contamination. Groundwater impacted by solvents and/or metals from the site (if any) could potentially extend beneath the Project site at concentrations exceeding the groundwater ESLs.

5.4 Military Cleanup Site

The former Onizuka AFS – Onizuka Air Force Station (Site 15 on Table 3 and Figure 6) operated from 1960 to 2010. The 19.6-acre station was located adjacent to and northwest of the Project at the intersection of Mathilda Ave and Moffett Park Drive. A fuel tank farm consisting of five 50,000-gallon jet fuel ASTs and two 10,000-gallon jet fuel ASTs was located on the southeast portion of the site. In 1987, approximately 1,600 gallons of jet fuel (JP-5) was released from one of the ASTs. Impacted soils were excavated and disposed offsite. In 1996, groundwater samples were collected from monitoring well MW-J2 in the tank farm area (Figure 6) and analyzed for JP-5 and semi-volatile organic compounds (SVOCs). Concentrations of JP-5 were reported as high as 96.1 µg/L. The Regional Water Board does not have an ESL for JP-5. However, it should be noted that the carbon range for TPHd analyzed by USEPA Method 8015M is C9 to C25, which generally includes the carbon range for JP-5 (C9 to C16). The reported concentration of JP-5 was below the current Regional Water Board (2013) groundwater ESL for TPHd of 100 µg/L. Concentrations of SVOCs were not reported above the laboratory reporting limits (Radian International LLC, 1996). The Regional Water Board closed the case in 1997. Residual jet fuel contamination from the site (if any) would not be expected to impact the Project site.

5.5 ERNS Incidents

Two ERNS incidents involving the releases of gasoline from tanker trucks appear to have occurred on the Project site.⁷ In 2012, ERNS Incident ID 1026923 involved the releases of

⁷ ERNS incident locations are reported according to the nearest cross street and typically do not include a street address or coordinates.

approximately 100 gallons of gasoline from an open valve on a tanker truck on Mathilda Avenue near the intersection of US 101 (Site 16 on Table 3 and Figure 6). Nearby storm drains were blocked with sand bags and the spill on the roadway was cleaned up (Center for Effective Government, 2015). In 1994, ERNS Incident ID 239305 involved the release of approximately 1,685 gallons of gasoline from a Shell Oil Company tanker truck that was overturned after being struck by another vehicle on US 101 north near the intersection of Mathilda Avenue (Site 17 on Table 3 and Figure 6). Impacted soils were reportedly removed for cleanup (Center for Effective Government, 2015). Additional regulatory requirements for cleanup were not reported at either release site; therefore, it is not expected that the chemical quality of soil and/or groundwater on the Project site is impacted by the former ERNS incidents.

6. EVALUATION OF OTHER ENVIRONMENTAL CONCERNS

Based on the Caltrans *Environmental Handbook* and BASELINE's previous experience working on similar transportation infrastructure projects, other environmental concerns that could pose a risk to the Project, but are not considered RECs under ASTM 1527-13, are described further, below.

6.1 Aerially-Deposited Lead

Lead alkyl compounds were first added to gasoline in the 1920s. Beginning in 1973, the USEPA ordered a gradual phase out of lead from gasoline that significantly reduced the prevalence of leaded gasoline by the mid-1980s. Prior to the 1970s, the USEPA estimated that vehicles emitted approximately 75 percent of the lead consumed in leaded gasoline as particulate matter in the exhaust (DTSC, 2004). As a result, shallow soils within approximately 30 feet of the edge of pavement in highway corridors have the potential to be contaminated with ADL from historical car emissions prior to the elimination of lead in gasoline (DTSC, 2009a).

Based on a review of historical aerial photographs (see Section 4.3), the intersections of US 101 and SR 237 with Mathilda Avenue were constructed in the late 1960s, which was before the full phase-out of lead in gasoline. Therefore, exposed shallow soils on the Project site within approximately 30 feet of the edge of pavement could be contaminated with ADL.

On 1 July 2009, the DTSC issued a variance to Caltrans (Caltrans/DTSC ADL Variance), allowing the reuse of some lead-affected soils for construction projects within the Caltrans rights-of-way (DTSC, 2009b). The Caltrans/DTSC ADL Variance allows Caltrans to reuse soils containing total lead at concentrations up to 3,397 milligrams per kilogram, or soluble lead at concentrations up to 150 milligrams per liter within the Project construction area and the Caltrans right-of-way, subject to certain restrictions and reporting requirements. The most recent extension of the Caltrans/DTSC ADL Variance will expire on 31 October 2015. Caltrans is currently negotiating the terms of a new variance with DTSC to be issued after 31 October 2015; however, it is currently unknown if DTSC will grant a new variance after the expiration date (Caltrans, 2015b).

6.2 Agricultural Pesticides

Prior to 1950, inorganic pesticides that contained elevated concentrations of metals, such as arsenic, were commonly used in California agriculture. After 1950, organochlorine pesticides (OCPs) were commonly used in California agriculture until about the mid-1970s. Arsenic from inorganic pesticides and residues from OCPs used in the past have the potential to persist for many decades in shallow soils and can affect human health and the environment (DTSC, 2008). Since the Project site was used for agriculture as early as 1939 (see Section 4.3), shallow soils beneath the Project site may be contaminated with arsenic and/or OCPs. However, the mixing of soils during excavation and grading activities for construction of the existing roadway and highway alignments through the Project site in the late 1960s may have reduced the concentration of residual pesticides in soils (if any). Therefore, the risk of encountering elevated concentrations of residual pesticides is expected to be low.

6.3 Naturally-Occurring Asbestos

Geologic mapping from the USGS does not show any areas of rock likely to contain naturally-occurring asbestos (ultramafic rock) on the Project site (Van Gosen, B.S., and J.P. Clinkenbeard, 2011). Based on the USGS mapping, naturally-occurring asbestos in bedrock at the Project site would not be expected to be a potential hazard during development of the Project. However, previous Caltrans projects in Santa Clara County have identified naturally-occurring asbestos in soil imported for embankment fill. Therefore, asbestos could potentially be present in embankment fill materials on the Project site.

6.4 Lead-Based Paint and Asbestos-Containing Materials

The US 101 overpass structure on the Project site may be coated with lead-based paint and/or asbestos-containing materials. Lead and asbestos are state-recognized carcinogens, and lead is a reproductive toxicant (California Environmental Protection Agency, 2012). Modification of the bridge barriers and sign structure on US 101 for the Project could pose a risk of releasing lead particles and asbestos fibers into the environment (if present).

6.5 Drainage Swales and Catch Basins

Metals from nonpoint runoff sources, such as urban developments, vehicle tires, and brake pads, can accumulate in catch basins and drainage swales over time. Sediments in catch basins and exposed soils in drainage swales on the Project site could contain elevated concentrations of metals and pose a risk to human health and the environment, if disturbed.

6.6 Yellow Traffic Striping and Pavement Markers

Lead chromate has been used in yellow thermoplastic and yellow paint for traffic striping and pavement markers for many years and as recently as 1996 in Caltrans District 4 where the Project is located. The residue that may be produced from the yellow thermoplastic and yellow paint during road improvement activities may contain lead and chromium concentrations that could produce toxic fumes when heated. The debris produced during the removal of yellow

thermoplastic and yellow paint may need to be disposed of as a California and/or federal hazardous waste if the concentrations of lead or chromium exceed applicable hazardous waste thresholds for total or soluble concentrations of those metals. If lead and chromium concentrations are unknown (i.e., previous residue testing has not been conducted), Caltrans Standard Special Provision 14-11.07 requires that yellow traffic striping and pavement markers be managed as an assumed hazardous waste by implementing a Lead Compliance Plan and testing the residues for hazardous-waste classification prior to off-site disposal (Caltrans, 2012).

6.7 Asphalt and Portland-Cement Concrete

Grindings of asphalt concrete (AC) and Portland-cement concrete (PCC) have a relatively high pH and may contain metals and petroleum hydrocarbons that can impact stormwater runoff and threaten surface water bodies. In accordance with guidance from the Regional Water Board, Caltrans projects may reuse AC and PCC grindings as roadway sub-base, backfill material, and compacted surface in a maintenance/work yard (Regional Water Board, 2007). Non-road base reuse scenarios must be reviewed by the Regional Water Board on a case-by-case basis. Surplus AC and PCC grindings generated from Project implementation and not re-used along the Project alignment may be transported to an aggregate recycling facility or a construction and demolition waste disposal facility.

7. ASTM 1527-13 DATA GAPS

The ASTM E1527-13 requires the identification of data gaps, along with actions taken to address these gaps, and an opinion as to whether these gaps are significant. A data gap may result from a lack of or inability to obtain information during any of the activities required by ASTM E1527-13. In particular, review of reasonably ascertainable historical land use information from the first developed land use to the present that does not provide sufficient detail to assess potential land use changes at five year intervals may be considered a data gap. Data gaps identified during the preparation of this ISA are described, below.

7.1 Historical Land Use Review

The time intervals between some of the historical land use records exceeded 5 years. These data gaps are not considered significant because the land uses were relatively consistent between the extended time intervals.

7.2 Environmental Records Review

Standard environmental record sources associated with State-registered ASTs were not reviewed, because the records were not reasonably ascertainable. This exclusion does not pose a significant data gap because the management of hazardous materials within or adjacent to the Project site would not constitute a REC.

8. ASTM 1527-13 DEVIATIONS

The purpose of this ISA was not to qualify the Project applicant for landowner liability protections associated with commercial real estate transactions under the Comprehensive Environmental Response, Compensation, and Liability Act (CERCLA). As a result, the following deviations from ASTM E1527-13, which are intended to meet or exceed the federal requirements for landowner liability protections under CERCLA, do not have a significant effect on the findings or conclusions of this ISA:

- The Project site is not a single contiguous commercial parcel, as assumed in ASTM E1527-13, and therefore a title search to identify potential environmental liens and activity and use limitations associated with commercial parcels was not conducted;
- Interviews with past, present, and prospective owners or operators who are likely to have material information regarding the potential for contamination at the Project site were not conducted, because such persons could not be identified; and
- Interviews with State or local government regulatory agency officials regarding the potential for contamination in the Project vicinity were not conducted, because any information obtained would likely duplicate information already reviewed from Federal, State, and local regulatory agency environmental records.

9. CONCLUSIONS

In accordance with the Caltrans *Environmental Handbook*, the levels of risk associated with RECs and other environmental concerns identified within the Project limits that could potentially affect proposed Project construction activities and/or operations are described further, below. Risks are categorized as either “low”, “medium”, or “high” based on the expected impact to the cost, scope, and schedule of a transportation project.

A high-risk condition typically involves crossing a site or property impacted by a known or suspected hazardous materials release, such as a landfill or railroad yard. A high-risk condition can potentially eliminate a build alternative; therefore, high-risk conditions require early investigation to support cost estimates, risk assessments, and adjustments to the project schedule during the Project Initiation Document phase.

A medium-risk condition typically involves the management of hazardous materials (e.g., ADL in soil) that require additional investigation, but is not expected to eliminate a build alternative and/or have a significant effect on the project scope, cost, and schedule. Site investigations for medium-risk conditions should be performed during the Project Approval and Environmental Document phase.

A low-risk condition typically includes the management of hazardous materials (e.g., lead-based paint on bridge structures) that may require additional investigation (if necessary), but the effect on the project scope, cost, and schedule can be reasonably estimated based on available information and/or is considered negligible. Site investigations for low-risk conditions can be

performed when convenient and may be delayed until the Plans, Specifications, and Estimates phase if there is sufficient time to complete the investigations.

9.1 Risk Analysis for Recognized Environmental Conditions

We have performed this ISA in conformance with the scope and limitations of ASTM E1527-13 for the Project, located along Mathilda Avenue in the City of Sunnyvale from Almanor Avenue/Ahwanee Avenue to Innovation Way. Any exceptions to, or deletions from, this practice are described in Section 8 of this report. In accordance with ASTM E1527-13 and the Caltrans *Environmental Handbook*, this assessment has identified the following five RECs and associated risk levels for hazardous materials, hazardous waste, and/or contamination on the Project site that could potentially affect proposed construction activities and/or operations:

- Potential groundwater impacts from a regional chlorinated solvent plume (Sites 1, 2, and 4 through 7 on Table 3 and Figure 6) – **Low Risk**
- Potential groundwater impacts from residual petroleum hydrocarbons at Shell (Site 9 on Table 3 and Figure 6) – **Low Risk**
- Potential groundwater impacts from residual petroleum hydrocarbons at Wolco Oil Co. (Site 11 on Table 3 and Figure 6) – **Low Risk**
- Potential groundwater impacts from solvents and metals potentially released at Circo Inc. (Site 12 on Table 3 and Figure 6) – **Low Risk**
- Potential groundwater impacts from residual petroleum hydrocarbons at Moffet Park Auto Center (Site 14 on Table 3 and Figure 6) – **Low Risk**

These RECs were all identified as a low risk, because the costs associated with managing impacted groundwater (if any) encountered during Project construction (e.g., dewatering) can be reasonable estimated and would not be expected to affect the scope and schedule of the Project.

9.2 Risk Analysis for Other Environmental Conditions

This assessment has also identified the following environmental concerns and associated risk levels on the Project site that are considered outside the standard scope of ASTM E1527-13:

- Potential ADL in exposed shallow soils – **Medium Risk**
- Potential arsenic and OCPs in shallow soils across the entire Project site from historical agriculture (Figure 5) – **Low Risk**
- Potential naturally-occurring asbestos in fill embankments – **Low Risk**
- Potential lead-based paint and asbestos-containing materials on US 101 overpass – **Low Risk**
- Potential metals in drainage swale and catch basin sediments from stormwater runoff – **Low Risk**
- Potential lead and chromium in yellow thermoplastic and yellow paint striping and markings on roadways – **Low Risk**
- Petroleum hydrocarbons, metals, and high pH in AC and PCC grindings – **Low Risk**

Shallow soils potentially impacted by ADL was identified as a medium risk because additional investigation is necessary to determine the potential effects on the Project cost, scope, and schedule. Potential pesticides (arsenic and OCPs) in shallow soils were identified as a low risk because concentrations (if any) are expected to have been reduced by previous excavation and grading activities; therefore, the risk of encountering elevated concentrations of residual pesticides is expected to be low. A low level of risk was identified for potential naturally-occurring asbestos in fill embankments and metals in drainage swales and catch basins because the area of impact would be limited and the occurrence of these environmental conditions is not very common for transportation projects. A low level of risk was also identified for hazardous materials on the US 101 overpass and in roadway materials because the effect on the project scope, cost, and schedule would not be considered significant and can be reasonably estimated.

9.3 Risk Analysis Summary for Build Alternatives

Risk levels associated with the hazardous materials concerns identified within the Project limits are summarized for each Build Alternative in Matrix 1, below. The associated risks identified in this ISA would generally apply equally to each Build Alternative.

MATRIX 1: Summary of Risk Levels for each Build Alternative

| Hazardous Materials Concern | Risk Level | Media Affected | Primary Contaminants of Concern | Build Alternatives | |
|---|------------|-----------------------|---|--------------------|---|
| | | | | 1 | 2 |
| Aerially-Deposited Lead | Medium | Soil | Lead | X | X |
| Hazardous Materials Release Sites* | Low | Groundwater | Petroleum Hydrocarbons, Chlorinated Solvents, Methylene Chloride, and/or Metals | X | X |
| Agricultural Pesticides | Low | Soil | Arsenic and OCPs | X | X |
| Naturally-Occurring Asbestos | Low | Soil | Asbestos | X | X |
| Lead-Based Paint and Asbestos-Containing Material | Low | Construction Material | Lead and Asbestos | X | X |
| Drainage Swales and Catch Basins | Low | Soil | Metals | X | X |
| Yellow Thermoplastic/Paint Striping and Markings | Low | Construction Material | Lead and Chromium | X | X |
| Asphalt and Portland-Cement Concrete Grindings | Low | Construction Material | Petroleum Hydrocarbons and Metals | X | X |

* Five potential groundwater plumes that pose a risk to the Project are identified in Section 5.

10. RECOMMENDATIONS

This sections describes BASELINE's recommendations for performing a Preliminary Site Investigation (PSI) and a Construction Risk Management Plan (CRMP).

10.1 Preliminary Site Investigation

Once a preferred Build Alternative has been chosen and areas of excavation and pavement disturbance are determined, a PSI should be performed prior to construction to investigate hazardous materials concerns related to soil, groundwater, and construction materials on the Project site, as identified in this ISA. Additional investigation may be required to fully evaluate potential hazardous materials issues if concerns are identified during the PSI. All environmental investigations for the Project should be performed in accordance with a Workplan approved by Caltrans. The Workplan should include procedures for collecting and analyzing representative samples from the following areas on the Project site that could be disturbed during proposed construction:

- Shallow exposed soils potentially impacted by ADL within 30 feet of Mathilda Avenue and the SR 237 and US 101 on- and off-ramps;
- Groundwater potentially impacted by hazardous materials release sites (see Section 9.1);
- Shallow soils along the entire Project alignment potentially impacted by arsenic and OCPs from former agriculture;
- Soil embankments near bridges and ramps potentially impacted by naturally-occurring asbestos.
- Shallow sediments in drainage swales and catch basins potentially impacted by metals from stormwater runoff;
- Lead-based paint and asbestos-containing materials on the US 101 overpass structure; and
- Yellow traffic stripes and pavement markings potentially containing lead and chromium.

All environmental investigations for the Project should be provided to the Project contractors to incorporate into their Health and Safety and Hazard Communication programs.

10.2 Hazardous Materials Management and Disposal

Project construction should be conducted under a project-specific CRMP to protect construction workers, the general public, and the environment from hazardous materials identified in the PSI and/or undocumented sources. The CRMP should incorporate the soil and groundwater analytical data from the PSI to ensure that soil and groundwater are stored, managed, and disposed of in a manner protective of human health and the environment, and in accordance with applicable laws and regulations. To address potential groundwater contamination concerns, the CRMP should require all groundwater from dewatering of excavations, if any, to be stored in a tank(s) during construction activities and characterized prior to disposal or recycling. This would be in addition to the pre-characterization of groundwater quality during the PSI.

The CRMP should also address the possibility of encountering undocumented sources of contamination in the subsurface by including measures for identifying, testing, and managing soil and groundwater suspected of containing hazardous materials that have not previously been identified at the Project site. The CRMP should describe required worker health and safety provisions for all workers potentially exposed to hazardous materials in accordance with State and Federal worker safety regulations and designate personnel responsible for implementation of the CRMP.

The CRMP should describe procedures for reusing AC and PCC grindings on-site in accordance with the Regional Water Board's guidelines for Caltrans' projects or transporting off-site for recycling or disposal. In accordance with Caltrans Standard Special Provision 14-11.03, the CRMP should include a Lead Compliance Plan for managing soil with hazardous waste concentrations of ADL (if any) based on the findings of the PSI. In accordance with Caltrans Standard Special Provision 14-11.07, the Lead Compliance Plan should also describe procedures for managing yellow paint striping and markings on existing roadways with either assumed or known hazardous waste concentrations of lead and/or chromium.

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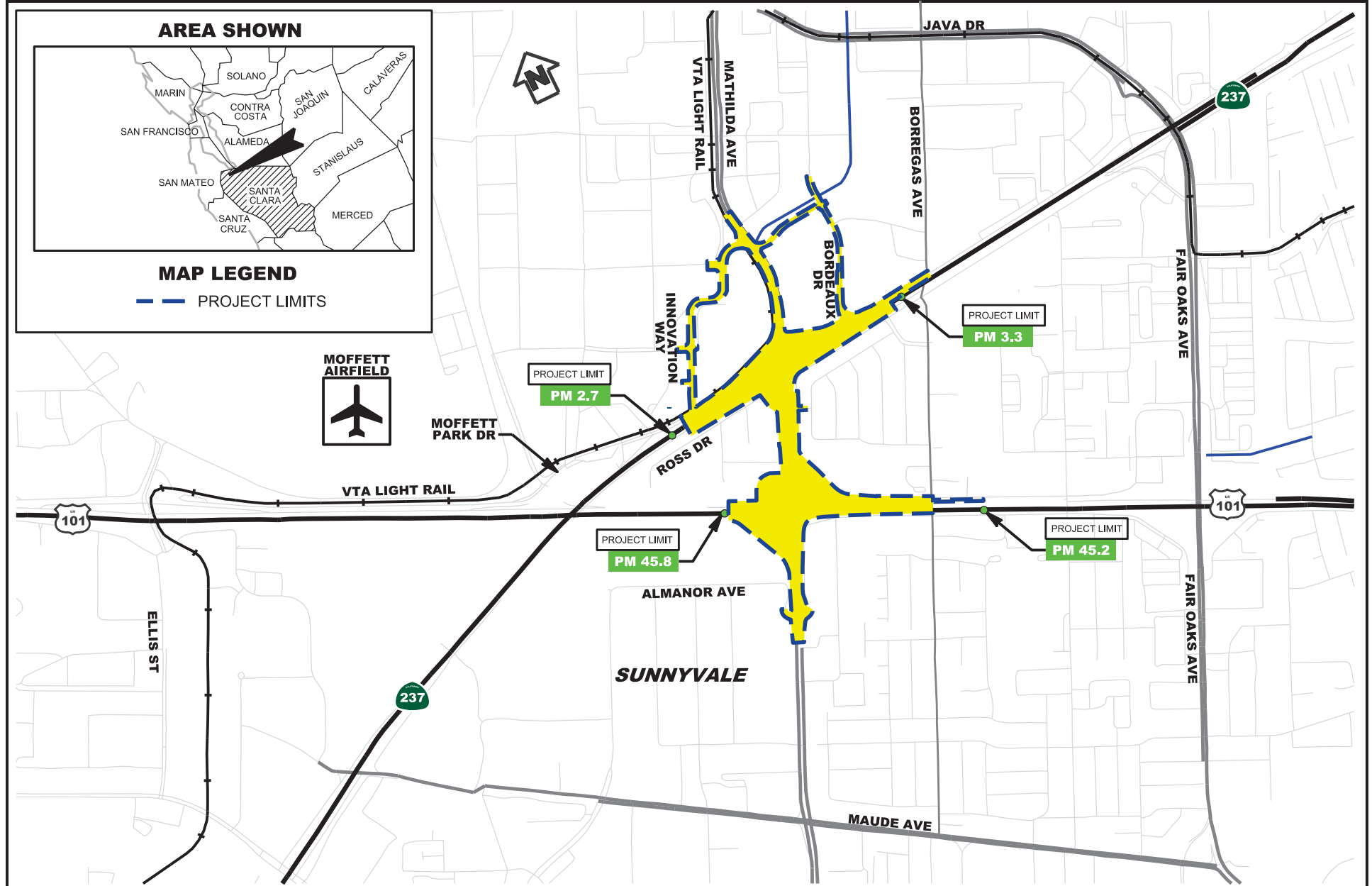
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FIGURES

Project Location

Figure 1



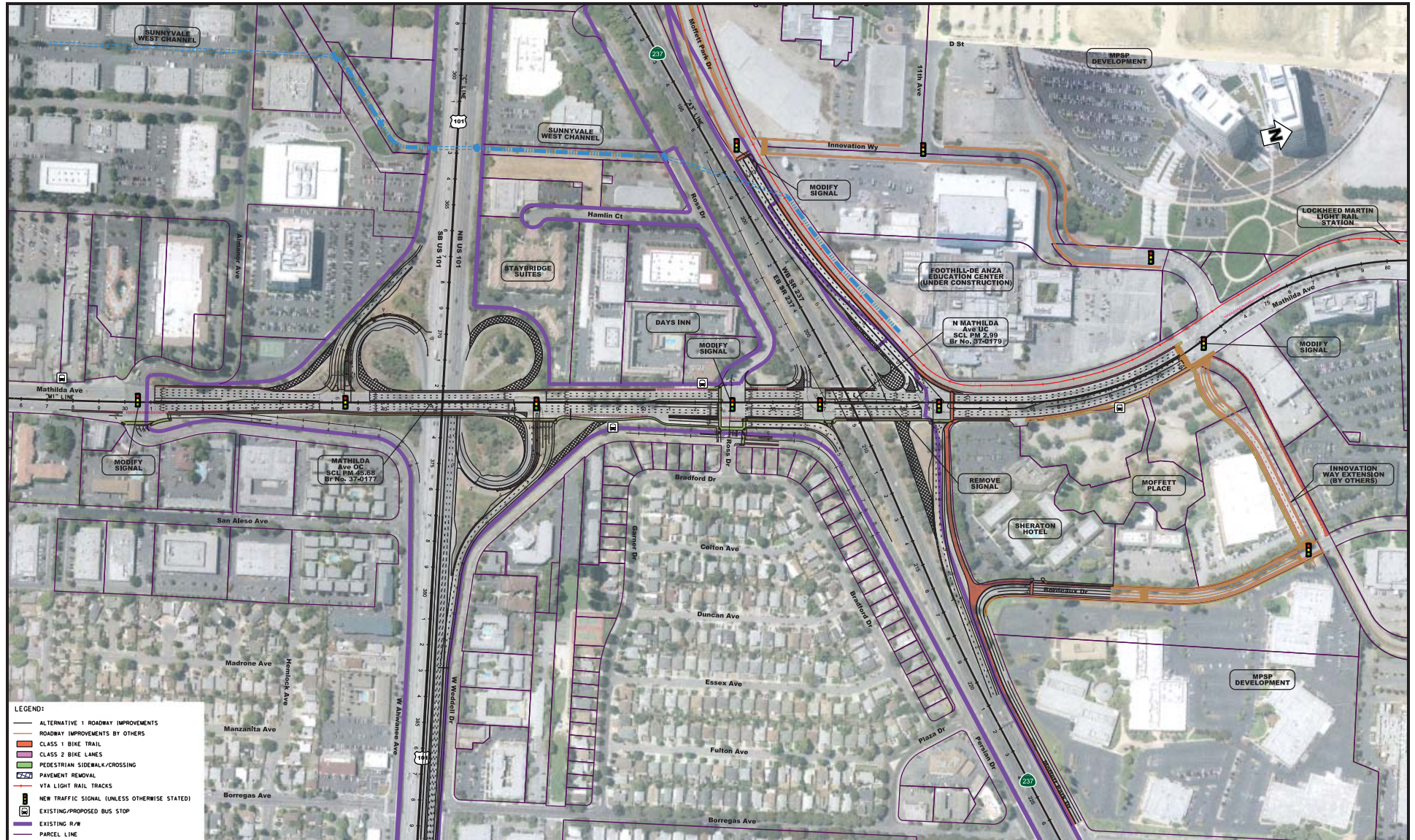
Source: WMH, 2015

Mathilda Avenue Improvements at SR 237 and US 101 Project

Note: Not to Scale

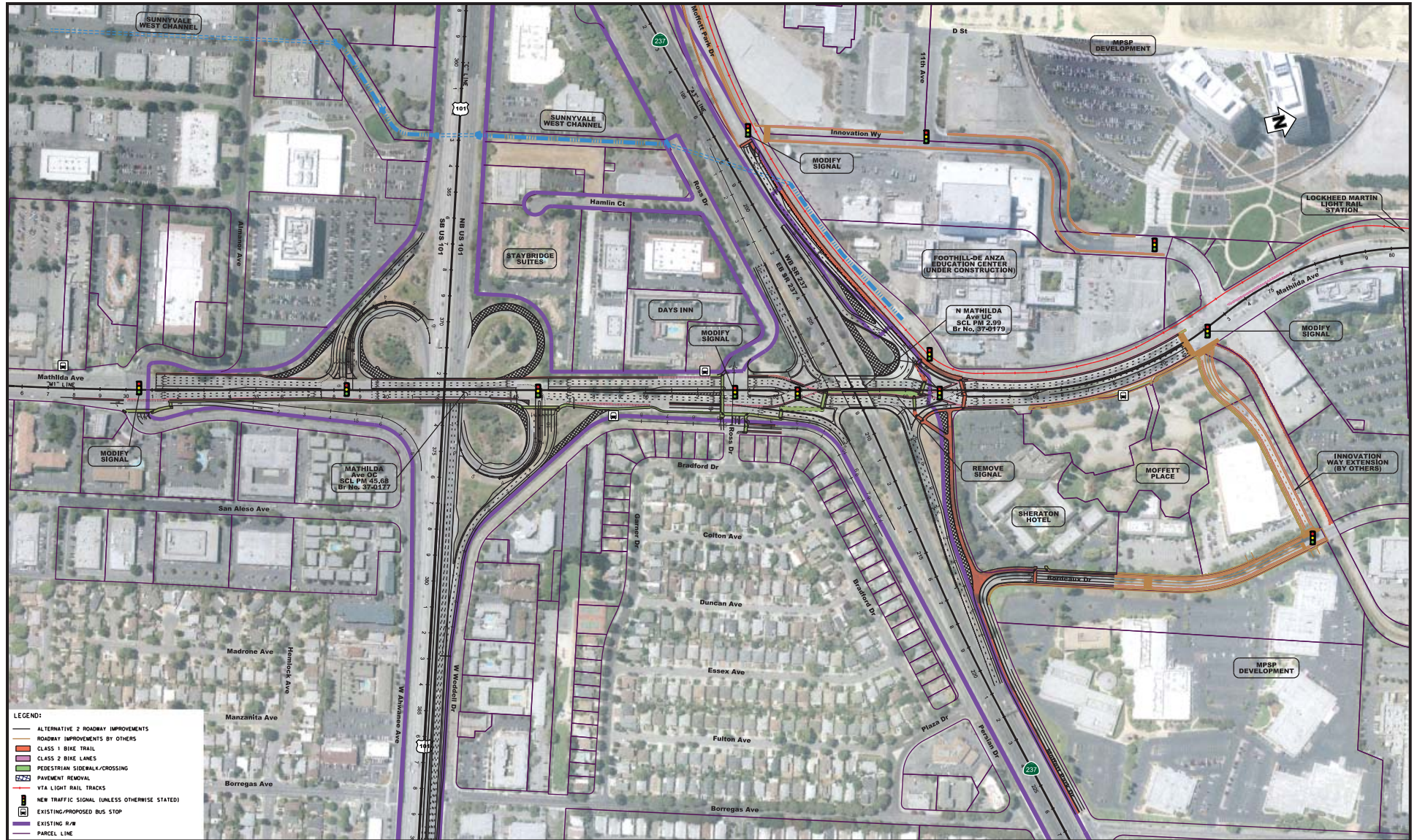
Build Alternative 1

Figure 2a



Mathilda Avenue Improvements at SR 237 and US 101 Project



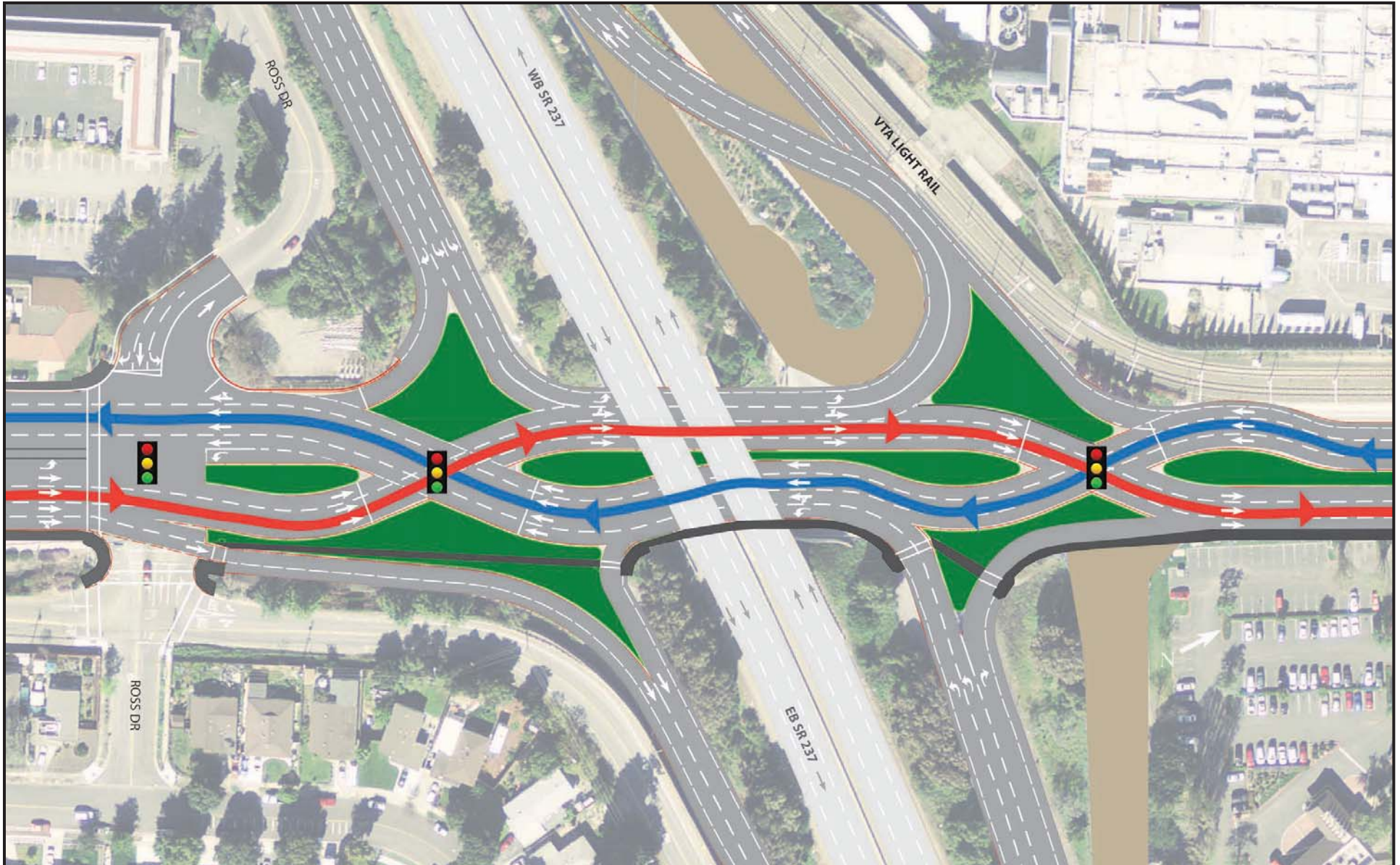


Mathilda Avenue Improvements at SR 237 and US 101 Project



Diverging Diamond Interchange Illustration

Figure 3

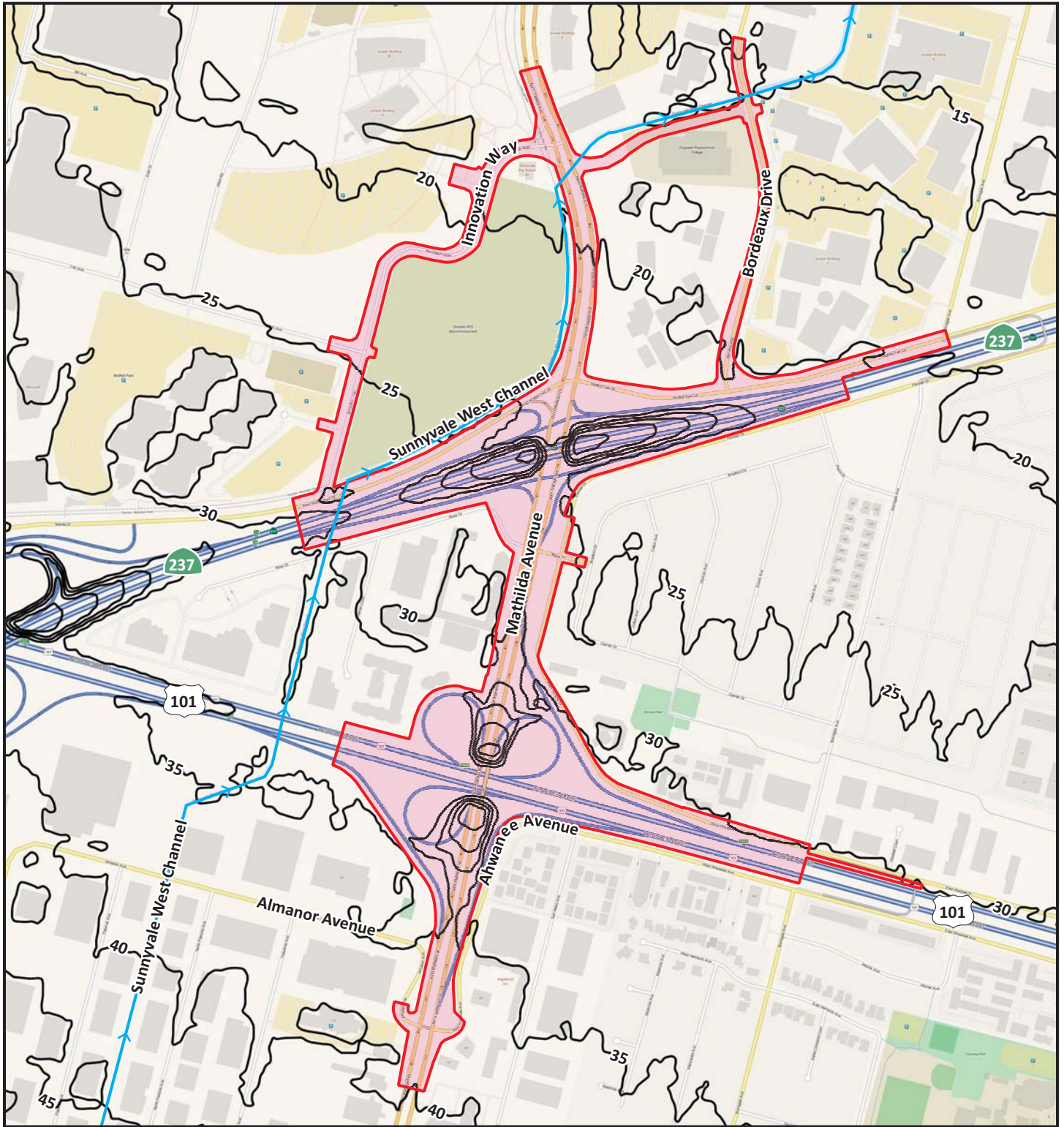


Source: WMH, 2015


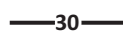

Mathilda Avenue Improvements at SR 237 and US 101 Project



Note: Not to Scale



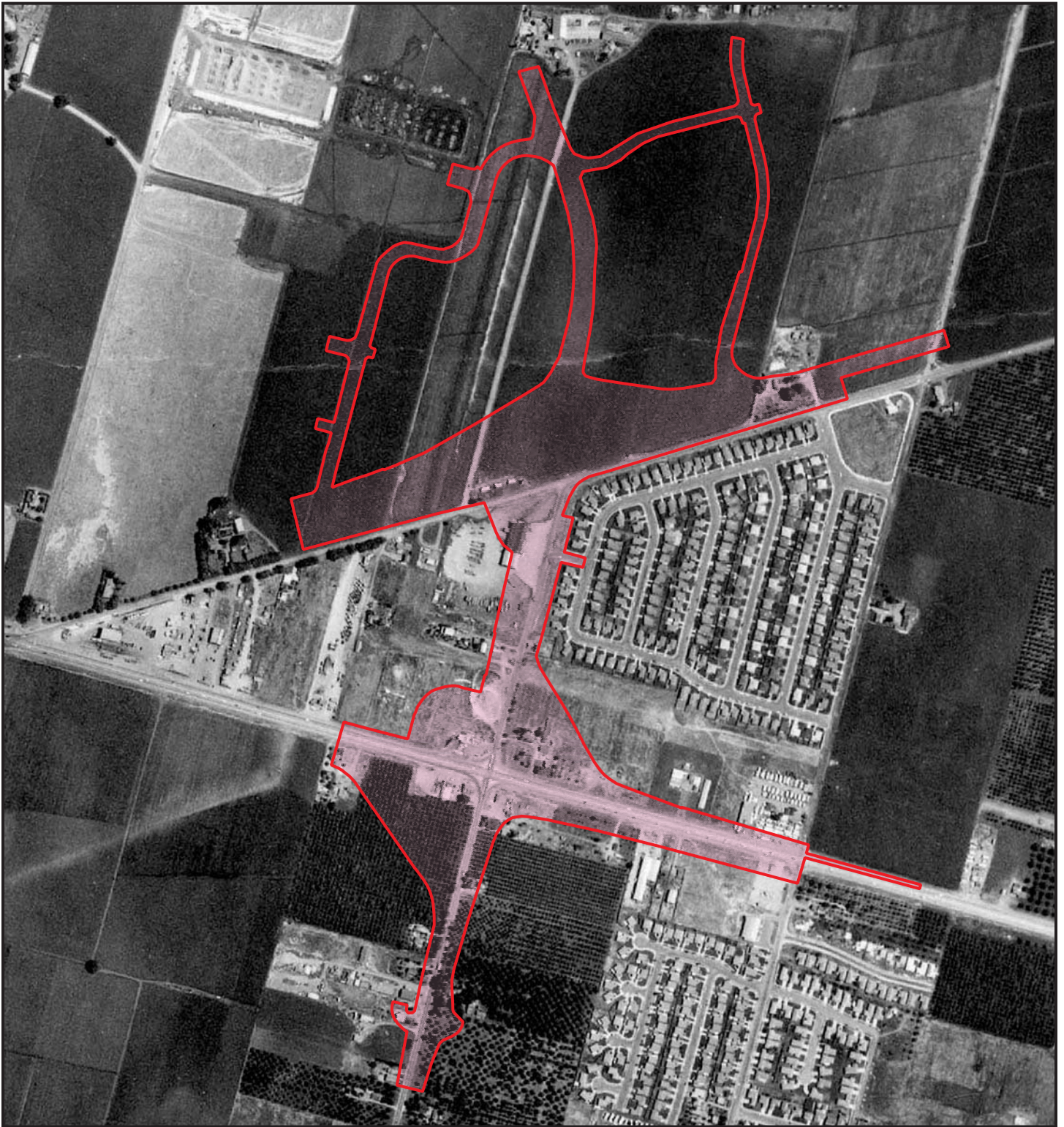
Legend

-  Project Limits
-  30 Surface Elevation Contour (feet, NAVD 88)
-  Surface Water Flow Direction

Base: MapQuest OpenStreetMap, 2015
Source: Surface Elevation Contours (USGS, 2015)

Mathilda Avenue Improvements at SR 237 and US 101 Project





Legend

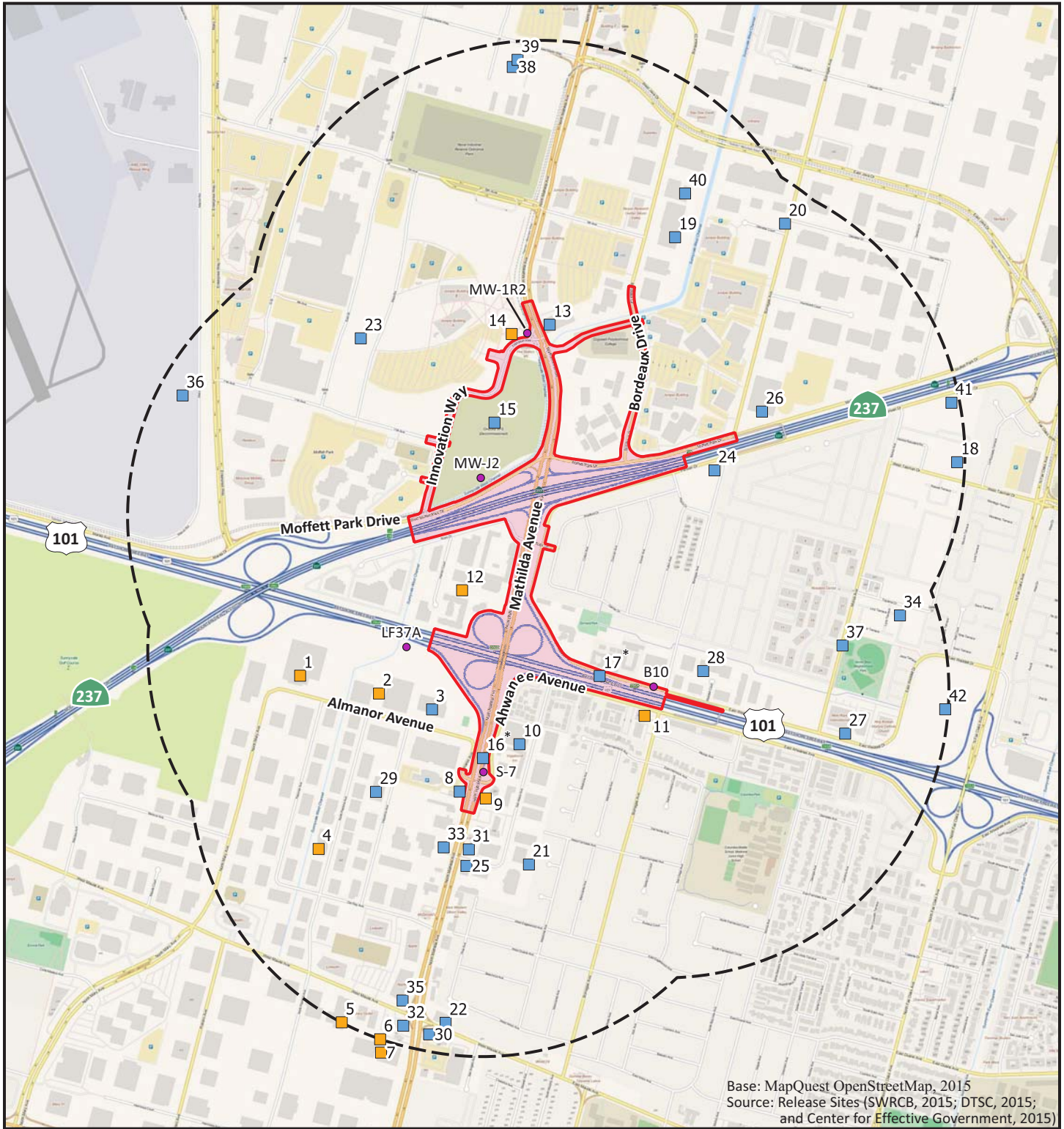
 Project Limits

Note: Aerial Photograph from 1956.

Base: EDR, 2015

**Mathilda Avenue Improvements
at SR 237 and US 101 Project**





Base: MapQuest OpenStreetMap, 2015
 Source: Release Sites (SWRCB, 2015; DTSC, 2015; and Center for Effective Government, 2015)

Legend

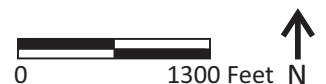
- Project Limits
- 0.5-mile Buffer
- Release Site with Potential Impact
- Release Site with No Impact
- Monitoring Well

Notes: Site information and Project impact determinations are summarized in Table 3 and Section 5.

The review of environmental records identified 42 sites with known hazardous materials releases within 1 mile of the Project site. The farthest hazardous materials release site (Site 7) was located approximately 0.5 miles from the Project.

* The location of Sites 16 and 17 are approximate.

Mathilda Avenue Improvements at SR 237 and US 101 Project



TABLES

Table 1: Summary of Environmental Records Reviewed

| Environmental Record Source | Search Distance | Reference | Record Source Description |
|--------------------------------------|------------------------|------------------------|---|
| ERNS Incidents | On | U.S. Coast Guard, 2015 | Toxic chemical spills and other accidents reported to the National Response Center database (formerly called the ERNS database). |
| Permitted USTs | On or Adjacent | SWRCB, 2015 | Facilities/sites that have a current permit to operate a UST(s) issued by the local permitting agency. |
| Hazardous Waste Facilities | On or Adjacent | DTSC, 2015 | Facilities/sites that were required to obtain a permit or have received a hazardous waste facility permit from the DTSC or U.S. EPA. |
| RCRA Facilities | On or Adjacent | USEPA, 2015 | Facilities/sites that generate, transport, store, treat and/or dispose of hazardous waste as defined by the Resource Conservation and Recovery Act. |
| Cleanup Program Site (formerly SLIC) | 0.5 mile | SWRCB, 2015 | Contaminated sites generally not associated with petroleum USTs with Regional Water Board oversight for investigation and/or remediation. |
| Evaluation | 0.5 mile | DTSC, 2015 | Suspected, but unconfirmed, contaminated sites that need or have gone through a limited investigation and assessment process. |
| FUDS | 0.5 mile | DTSC, 2015 | Military facilities that were FUDS with confirmed or unconfirmed releases and where DTSC is involved in investigation and/or remediation. |
| HWP / BZP Evaluation | 0.5 mile | DTSC, 2015 | Significant hazardous waste properties (HWPs) and border zone properties (BZPs) located within 2,000 feet of a significant HWP. |
| Land Disposal Site | 0.5 mile | SWRCB, 2015 | Regulated waste management units (e.g., waste piles, surface impoundments, and landfills) that discharge waste to land for treatment, storage and disposal. |
| LUST Cleanup Site | 0.5 mile | SWRCB, 2015 | Sites contaminated from leaking USTs with Regional Water Board oversight for investigation and/or remediation. |
| Military Evaluation | 0.5 mile | DTSC, 2015 | Closed and open military facilities with confirmed or unconfirmed releases with DTSC oversight for investigation and/or remediation. |
| Military Cleanup Site | 0.5 mile | SWRCB, 2015 | Military UST sites, Military Privatized sites, and Military Cleanup sites with Regional Water Board oversight for investigation and/or remediation. |
| School | 0.5 mile | DTSC, 2015 | Proposed and existing school sites that are being evaluated by DTSC for possible hazardous materials contamination. |
| Voluntary Cleanup | 0.5 mile | DTSC, 2015 | Sites with either confirmed or unconfirmed releases, and the project proponents have requested DTSC oversight for investigation and/or remediation. |
| Corrective Action | 1.0 mile | DTSC, 2015 | Investigation or cleanup activities at RCRA or state-only permitted hazardous waste facilities. |
| Expedited Remedial Action Program | 1.0 mile | DTSC, 2015 | High-priority and high potential risk sites requiring expedited cleanup with DTSC oversight. This is currently a pilot program. |
| Federal Superfund | 1.0 mile | DTSC, 2015 | Sites where the USEPA proposed, listed, or delisted a site on the NPL. |
| State Response | 1.0 mile | DTSC, 2015 | High-priority and high potential risk sites requiring cleanup with DTSC oversight. |

Table 1: Summary of Environmental Records Reviewed

Notes:

Search distances are defined by ASTM E1527-05 and are relative to the boundary of the Project site.

Land use restrictions for contaminated properties are reported by both the SWRCB and DTSC under the status of an environmental record.

SWRCB = State Water Resources Control Board

DTSC = Department of Toxic Substances Control

RCRA = Resource Conservation and Recovery Act

FUDS = Formerly Used Defense Sites

NPL = National Priorities List

USEPA = United States Environmental Protection Agency

UST = Underground Storage Tank

SLIC = Spills, Leaks, Investigation, and Cleanup

Table 2: Summary of Environmental Records for Hazardous Materials Facilities

| Site Name | Address | Facility Type |
|-----------------------------------|--------------------------------|-------------------------------|
| Shell Oil Self-Serve | 776 N Mathilda Ave, Sunnyvale | Permitted UST |
| Shell Stn | 776 N Mathilda, Sunnyvale | Small-Quantity RCRA Generator |
| Sunnyvale Auto Body | 505 Almanor Ave, Sunnyvale | Small-Quantity RCRA Generator |
| Nimbus Software Svcs | 520 Almanor Ave, Sunnyvale | Small-Quantity RCRA Generator |
| Sirenza Microdevices | 522 Almanor Ave, Sunnyvale | Small-Quantity RCRA Generator |
| Applied Chemical Laboratories Inc | 526 Almanor Ave, Sunnyvale | Small-Quantity RCRA Generator |
| Pacific Auto Electric | 105 West Weddell, Sunnyvale | Small-Quantity RCRA Generator |
| Pacific Bell | 1140 North Mathilda, Sunnyvale | Small-Quantity RCRA Generator |

Notes:

UST = underground storage tank

RCRA = Resource Conservation and Recovery Act

All sites are located adjacent to the Project.

Site name, address, and status information (including spellings) are derived directly from the regulatory databases.

Small-quantity RCRA generators are facilities that generate more than 100 kilograms, but less than 1,000 kilograms, of hazardous waste per month.


Table 3: Summary of Environmental Records for Hazardous Materials Release Sites

| Site ID | Site Name | Address | Status | Project Impact Determination | Environmental Record Source | | | | | | | |
|---------|--|--|--------------------------------|------------------------------|-----------------------------|-------------------|---------------|------------|--------------------|-------------------|-----------------------|-------------------|
| | | | | | Cleanup Program Site | Corrective Action | ERNS Incident | Evaluation | Land Disposal Site | LUST Cleanup Site | Military Cleanup Site | Voluntary Cleanup |
| 1 | California Microwave | 985 Almanor Ave, Sunnyvale | Open - Inactive | Potential Impact | X | | | | | | | |
| 2 | 645/675 Almanor, et al | 645/675 Almanor Ave, Sunnyvale | Open - Verification Monitoring | Potential Impact | X | | | | | | | |
| 3 | Litton Applied Technology | 525 Almanor Ave, Sunnyvale | Completed - Case Closed | No Impact | X | | | | | | | |
| 4 | Siemens Microelectronics Inc | 639 North Pastoria Ave, Sunnyvale | Open - Remediation | Potential Impact | X | | | | | | | |
| 5 | Eaton & Signetics | 680 West Maude Ave, Sunnyvale | Open - Remediation | Potential Impact | X | | | | | | | |
| 6 | Zymos | 477 Mathilda Ave N, Sunnyvale | Open - Inactive | Potential Impact | X | | | | | | | |
| 7 | Maxim Integrated Products Inc | 477 No Mathilda Ave, Sunnyvale | Inactive - Needs Evaluation | Potential Impact | | X | | | | | | |
| 8 | Thrifty #165 | 773 N Mathilda Ave, Sunnyvale | Completed - Case Closed | No Impact | | | | | | X | | |
| 9 | Shell | 776 N Mathilda Ave, Sunnyvale | Completed - Case Closed | Potential Impact | | | | | | X | | |
| 10 | Pace Distributors | 828 W Ahwanee Ave, Sunnyvale | Completed - Case Closed | No Impact | | | | | | X | | |
| 11 | Wolco Oil Co. (Borregas) | 883 Borregas Ave, Sunnyvale | Completed - Case Closed | Potential Impact | | | | | | X | | |
| 12 | Circo Inc | 940 Hamlin Court, Sunnyvale | Inactive - Needs Evaluation | Potential Impact | | X | | | | | | |
| 13 | Pacific Bell | 1140 N Mathilda Ave, Sunnyvale | Completed - Case Closed | No Impact | | | | | | X | | |
| 14 | Moffet Park Auto Center | 1135 N Mathilda Ave, Sunnyvale | Completed - Case Closed | Potential Impact | | | | | | X | | |
| 15 | Onizuka AFS - Onizuka Air Force Station | 1080 Innovation Way, Sunnyvale | Completed - Case Closed | No Impact | | | | | | | X | |
| 16 | ERNS Incident ID 1026923 | Mathilda Ave near US 101 | Remediation Completed | No Impact | | | X | | | | | |
| 17 | ERNS Incident ID 239305 | US 101 North near Mathilda Ave Exit | Remediation Completed | No Impact | | | X | | | | | |
| 18 | ESL Inc. | 425 Tasman Drive, Sunnyvale | Completed - Case Closed | No Impact | X | | | | | | | |
| 19 | DII Orbit Semiconductor (Former) | 1230 Bordeaux Dr, Sunnyvale | Completed - Case Closed | No Impact | X | | | | | | | |
| 20 | Pan American Savings | 165 Gibraltar Ct, Sunnyvale | Completed - Case Closed | No Impact | X | | | | | | | |
| 21 | Ampex - Sunnyvale | 728 San Aleso, Sunnyvale | Completed - Case Closed | No Impact | X | | | | | | | |
| 22 | Data General Corp | 433 North Mathilda Ave, Sunnyvale | Completed - Case Closed | No Impact | X | | | | | | | |
| 23 | Lockheed Sunnyvale - Plant One Facility - Building 109 USTs | 1111 Lockheed Way, Sunnyvale | Completed - Case Closed | No Impact | X | | | | | | | |
| 24 | Professional Center | 102 W. Persian Drive, Sunnyvale | Completed - Case Closed | No Impact | | | | | | X | | |
| 25 | Quality Tune-Up #2 | 696 N Mathilda Ave, Sunnyvale | Completed - Case Closed | No Impact | | | | | | X | | |
| 26 | Moffett Park Dr Mccandless | 215 Moffett Park Drive, Sunnyvale | Completed - Case Closed | No Impact | | | | | | X | | |
| 27 | Direct Delivery Service | 925 Morse Ave, Sunnyvale | Completed - Case Closed | No Impact | | | | | | X | | |
| 28 | Sunnyvale Valve & Fitting Co | 929 Weddell Ct, Sunnyvale | Completed - Case Closed | No Impact | | | | | | X | | |
| 29 | Micromask Inc | 716 Pastoria Ave N, Sunnyvale | Completed - Case Closed | No Impact | | | | | | X | | |
| 30 | Exxon #7-3669 | 498 N Mathilda Ave, Sunnyvale | Completed - Case Closed | No Impact | | | | | | X | | |
| 31 | Texaco | 724 N. Mathilda Avenue, Sunnyvale | Completed - Case Closed | No Impact | | | | | | X | | |
| 32 | Unocal #4315 | 499 N. Mathilda Ave., Sunnyvale | Completed - Case Closed | No Impact | | | | | | X | | |
| 33 | T & J Garage | 755 Mathilda Ave N, Sunnyvale | Completed - Case Closed | No Impact | | | | | | X | | |
| 34 | Specialty Garbage & Refuse | 438 Toyama Dr, Sunnyvale | Completed - Case Closed | No Impact | | | | | | X | | |
| 35 | Shell - 505 N. Mathilda | 505 N Mathilda Ave, Sunnyvale | Completed - Case Closed | No Impact | | | | | | X | | |
| 36 | Cang Former Civil Engineering Storage Yard | 680 Macon Road, Stop 20, Mountain View | Completed - Case Closed | No Impact | | | | | | | X | |
| 37 | Morse Park | 1010 to 1024 Morse Avenue, Sunnyvale | Certified | No Impact | | | | | | | | X |
| 38 | Lockheed Sunnyvale - A Parent | 1111 Lockheed Martin Way, Sunnyvale | Open - Site Assessment | No Impact | X | | | | | | | |
| 39 | Lockheed Sunnyvale - Process Wastewater Treatment And Reclamation Facility | 1111 Lockheed Martin, Sunnyvale | Open | No Impact | | | | | X | | | |
| 40 | Orbit Semiconductor | 1230 Bordeaux Drive, Sunnyvale | Inactive - Needs Evaluation | No Impact | | | X | | | | | |

Table 3: Summary of Environmental Records for Hazardous Materials Release Sites

| Site ID | Site Name | Address | Status | Project Impact Determination | Environmental Record Source | | | | | | | |
|---------|-------------------|---|------------------------|------------------------------|-----------------------------|-------------------|---------------|------------|--------------------|-------------------|-----------------------|-------------------|
| | | | | | Cleanup Program Site | Corrective Action | ERNS Incident | Evaluation | Land Disposal Site | LUST Cleanup Site | Military Cleanup Site | Voluntary Cleanup |
| 41 | 460 Persian Drive | 460 Persian Drive, Sunnyvale | Active | No Impact | | | | | | | | X |
| 42 | Raintree | 520 and 592 East Weddell Drive, Sunnyvale | Open - Site Assessment | No Impact | X | | | | | | | |

Key:

 Light blue shading indicates that groundwater contamination from the release site could potentially impact the Project.

Notes:

Site name, address, and status information (including spellings) are derived directly from the regulatory databases.

Site locations are shown on Figure 6.

Project impact determinations are evaluated under Section 5.

APPENDICES

APPENDIX A
ISA CHECKLIST

Initial Site Assessment (ISA) Checklist

Project Information

District 04 County SCL Route 237; 101 Post Mile 2.7/3.3; 45.2/45.8 EA 4H2900

Description: Mathilda Avenue Improvements at SR 237 and US 101 Project

Is the project on the HW Study Minimal-Risk Projects List (HW1)? No

Project Manager Dina El-Tawansy phone # 510-286-7236.

Project Engineer Tim Lee, WMH Corporation phone # 415-806-7500.

Project Screening

Attach the project location map to this checklist to show location of all known and/or potential HW sites identified. See Figures 1 and 6 of the ISA report

1. Project Features:

New R/W? Yes

Excavation? Yes

Railroad Involvement? Yes

Structure demolition/modification? Yes

Subsurface utility relocation? Yes

2. Project Setting:

Rural or Urban: Urban

Current land uses: Transportation

Adjacent land uses: Residential, commercial, and industrial

3. Check federal, State, and local environmental and health regulatory agency records as necessary, to see if any known hazardous waste site is in or near the project area. If a known site is identified, show its location on the attached map and attach additional sheets, as needed, to provide pertinent information for the proposed project.

See Table 3, Figure 6, and Section 5 of the ISA report.

4. Field Inspection – Date: 8/27/15

STORAGE STRUCTURES / PIPELINES: The Project Area of Potential Effect may potentially include the following structures noted below:

Underground tanks No

Surface tanks No

Sumps No

Ponds No

Drums No

Basins Yes (next to on- and off-ramps)

Transformers Yes

Landfill No

Other None

CONTAMINATION: (spills, leaks, illegal dumping, etc.)

Surface staining No

Oil sheen No

(continued)

Odors **No**

Vegetation damage **No**

Other **No**

HAZARDOUS MATERIALS: (asbestos, lead, etc.)

Buildings **No**

Spray-on fireproofing **No**

Pipe wrap **No**

Friable tile **No**

Acoustical plaster **No**

Serpentine **None mapped in Project vicinity**

Paint **Yes (Yellow striping and pavement markings)**

Other **None**

5. Additional record search, as necessary, of subsequent land uses that could have resulted in a hazardous waste site.

Potential arsenic and organochlorine pesticides from former agriculture. See Section 6.2 of the ISA report.

6. Other comments and/or observations:

Refer to Executive Summary of the ISA report.

ISA Determination

Does the project have potential hazardous waste involvement? **Yes**

If there is known or potential hazardous waste involvement, is additional ISA work needed before task orders can be prepared for the Investigation? **No.**

A brief memo should be prepared to transmit the ISA conclusions to the Project Manager and Project Engineer. **Executive Summary of the ISA report provided to the Project Manager and Project Engineer.**

ISA Conducted by: **Patrick Sutton, BASELINE Environmental Consulting** Date: **October 2015**

APPENDIX B
HISTORICAL LAND USE RECORDS



Mathilda Avenue Improvements

N MATHILDA AVE

Sunnyvale, CA 94089

Inquiry Number: 4379572.1

August 13, 2015

The EDR Aerial Photo Decade Package



6 Armstrong Road, 4th Floor
Shelton, Connecticut 06484
Toll Free: 800.352.0050
www.edrnet.com

EDR Aerial Photo Decade Package

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Date EDR Searched Historical Sources:

Aerial Photography August 13, 2015

Target Property:

N MATHILDA AVE

Sunnyvale, CA 94089

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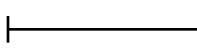


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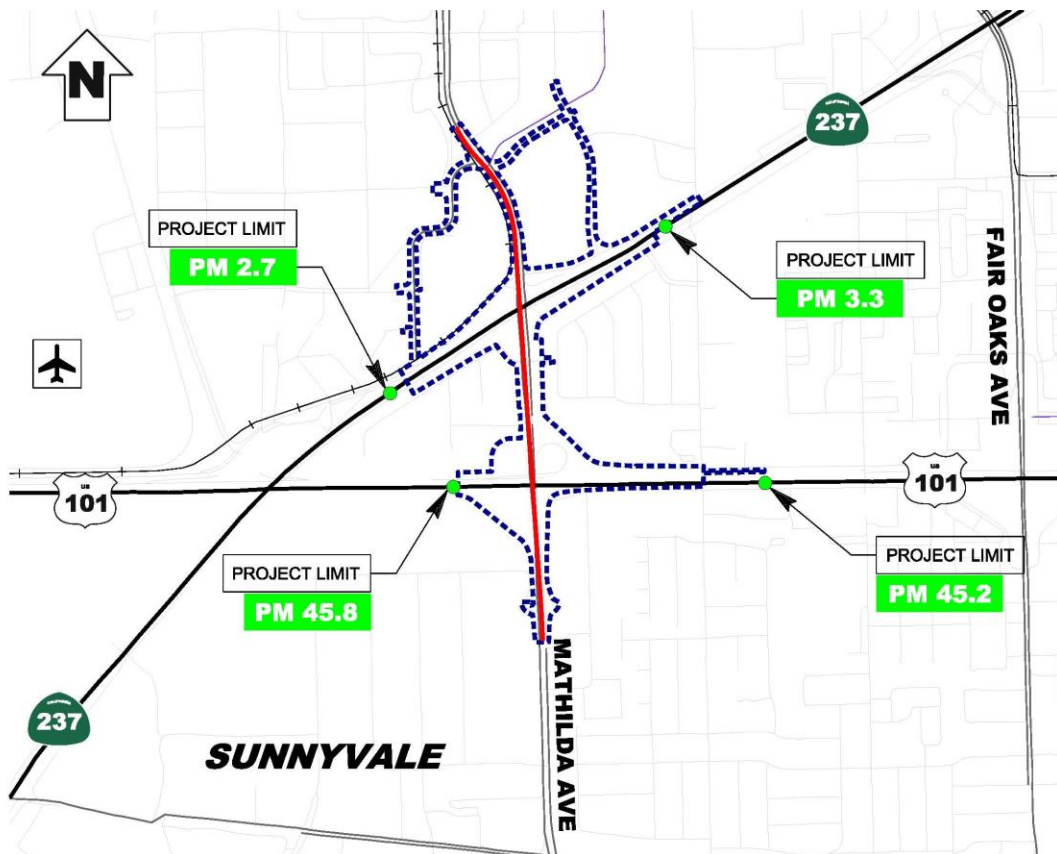


Natural Environment Study

Minimal Impact

for the

MATHILDA AVENUE IMPROVEMENTS AT SR 237 AND US 101 PROJECT



Prepared for:

Santa Clara Valley Transportation Authority

**California Department of Transportation
District 4**

Prepared by:

ICF International

Dated: February 2016

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Natural Environment Study

Minimal Impact

for the

MATHILDA AVENUE IMPROVEMENTS AT SR 237 AND US 101 PROJECT

on Mathilda Avenue from Almanor Avenue to Innovation Way, on SR 237 from 0.3 mile south of US 101/SR 237 junction to 0.3 mile east of Mathilda Avenue undercrossing, and on US 101 from 0.5 mile south of Mathilda Avenue to SR 237/US 101/SR 237 junction in the City of Sunnyvale, Santa Clara County


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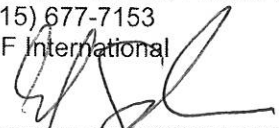
February 2016


U.S. DEPARTMENT OF TRANSPORTATION
STATE OF CALIFORNIA

and

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Statement of Compliance: Produced in compliance with California Environmental Quality Act (CEQA) requirements, as appropriate, to meet the level of analysis and documentation that has been determined necessary for this project.

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Summary

The Mathilda Avenue Improvements at SR 237 and US 101 Project (Project) is located in Sunnyvale, Santa Clara County, California (Figure 1). The purpose of the Project is to reduce congestion and improve traffic operations on Mathilda Avenue at State Route (SR) 237 and U.S. Highway 101 (US 101) while improving mobility for all travel modes in the area. The scope and scale of the Project is intended to provide locally scaled transportation improvements in the near term that address multiple existing deficiencies.

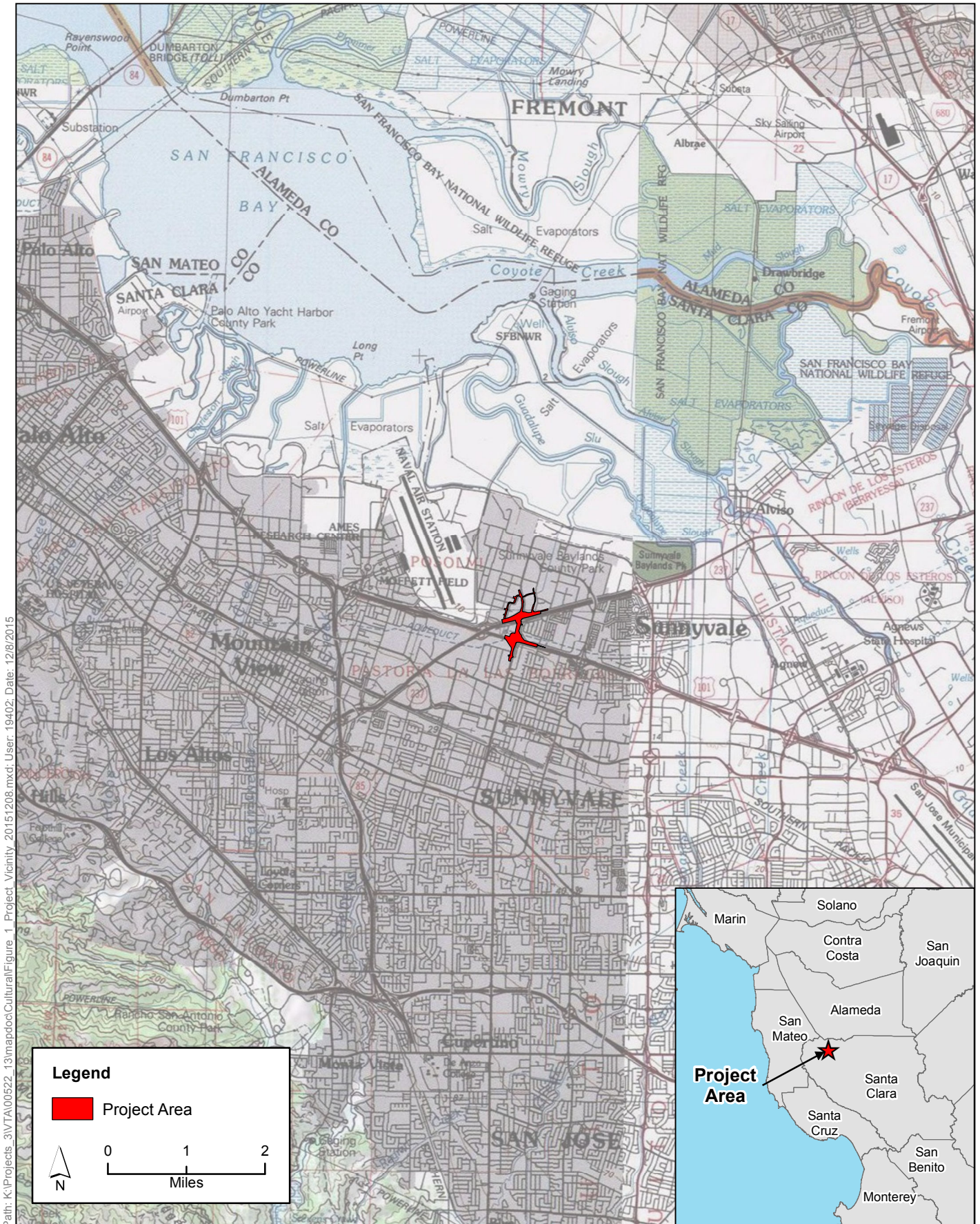
The purpose of this Natural Environment Study – Minimal Impacts (NES-MI) is to evaluate the potential for the Project to affect sensitive biological resources, including, but not limited to, special-status species and natural habitats.

ICF International (ICF) reviewed online resources on the U.S. Fish and Wildlife Service, California Department of Fish and Wildlife, and California Native Plant Society websites to identify potential special-status botanical and wildlife resources found on the Project site. Based on the results, it was determined that six special-status plant species and 27 special-status wildlife species have the potential to occur in the Project region. Field surveys were conducted on March 6 and July 29, 2015. The purposes of field surveys were to identify vegetation and cover types within the Project site and assess habitat suitability for special-status species. Based on the results of the field surveys, the Project would have no effect on habitats and natural communities of special concern and no effect on special-status plant species because of the high degree of development and routine human activity within the Project footprint.

By causing nesting and reproductive failure from high disturbance levels, construction of the Project could affect nesting birds and/or raptors that are protected by the Migratory Bird Treaty Act. If feasible, trees would be removed during the non-nesting season, September 1 to January 31. Otherwise, preconstruction surveys would be conducted during the nesting season, February 1 to August 31, to ensure that no active bird nests are present prior to tree removal. If active nests are identified, then buffers would be established until nesting is completed.

A wetlands assessment was conducted concurrently with the field surveys described above. The wetlands assessment identified culverted portions of a concrete-lined flood control channel and open stormwater drainage ditches within the Biological Study Area (BSA), which is bounded by the Project limits. The flood control channel (Sunnyvale West Channel) was identified as potentially subject to both federal and state jurisdiction because it drains directly to a navigable water (San Francisco Bay) via Guadalupe Slough. The stormwater drainage ditches are presumed to be non-jurisdictional because they were constructed in uplands and drain runoff from uplands. The Project is not expected to affect the Sunnyvale West Channel and, therefore, would not require a Clean Water Act Section 404 permit or Section 401 water quality certification or waste discharge requirement. Approximately 626 trees occur in the BSA. The California Department of Transportation (Caltrans) and Santa Clara Valley Transportation Authority (VTA) are exempt from local tree protection ordinances. However, the trees provide aesthetic and other benefits to the community and may provide habitat or food sources for local wildlife; therefore, trees impacted by the Project will be replaced at ratios that are commensurate with the size of the tree to be removed, as described in Chapter 4.

Invasive plant species are present throughout much of the Project work limits. To minimize the introduction and spread of additional invasive plant species within project boundaries as well as lands adjacent to the Project, the City of Sunnyvale or its contractor shall implement best management practices to the greatest extent practicable when disturbing soil and removing or disposing of invasive plant material.



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Figure 1
Project Vicinity
Mathilda Avenue Improvements at SR 237 and US 101

Chapter 1 – Introduction

1.1 Project History

The SR 237/Mathilda Avenue and US 101/Mathilda Avenue interchanges are primary access points on the state highway system for the City of Sunnyvale and important local destinations, such as downtown Sunnyvale, the Sunnyvale Caltrain station to the south, and an expanding high-tech business district to the north. The Project is also located within the “Golden Triangle,” an area bordered by US 101, SR 237, and Interstate (I) 880 that includes parts of Sunnyvale, Santa Clara, North San Jose, and Milpitas. The Golden Triangle is named for the high concentration of employment centers within this area. US 101, SR 237, and I-880 are heavily used commute corridors to destinations within and beyond the Golden Triangle.

1.1.1 MATHILDA AVENUE

Within the Project area, Mathilda Avenue is a six-lane divided local roadway. Mathilda Avenue serves as the main access route to residential communities on the east side of Mathilda Avenue and is the only access route to the landlocked area within the US 101/SR 237/Mathilda Avenue triangle via Ross Drive. Mathilda Avenue is also one of City of Sunnyvale’s designated truck routes for trucks over three tons in weight. The speed limit is 45 miles per hour (mph) and on-street parking is prohibited within the Project area. Approximately 45,000 vehicles travel on Mathilda Avenue south of SR 237 on an average weekday.

1.1.2 SR 237

SR 237 is an east-west freeway, starting at SR 82 (El Camino Real) in the City of Mountain View and ending approximately 11 miles to the east at I-680 in the City of Milpitas. Within the Project area, SR 237 provides two mixed-flow lanes in each direction. On eastbound SR 237, a high-occupancy vehicle (HOV) lane is provided east of Mathilda Avenue and becomes an HOV/express lane from east of Zanker Road to the eastbound SR 237/northbound I-880 direct connector ramp. On westbound SR 237, there is an HOV/express lane beginning at the southbound I-880/westbound SR 237 direct connector ramp that becomes an HOV lane from North First Street to just east of Fair Oaks Avenue. Within the Project area, auxiliary lanes are provided in each direction between US 101 and Mathilda Avenue on SR 237. There is also an auxiliary lane on westbound SR 237 between Fair Oaks Avenue and Mathilda Avenue. SR 237 is a link for trucking between the southern part of the San Francisco Peninsula and the East Bay, providing the first connection south of the Dumbarton Bridge. SR 237 east of Mathilda Avenue currently carries approximately 90,000 vehicles daily.

The SR 237/Mathilda Avenue interchange is a full “tight” diamond interchange that accommodates all ramp movements, with access to and from east and westbound SR 237. All ramp termini are signalized. The westbound SR 237 on-ramp has existing ramp metering equipment installed; however, there is no existing ramp metering equipment installed for the eastbound SR 237 on-ramp.

1.1.3 US 101

Within the Project area, US 101 provides three mixed-flow lanes plus one HOV lane in each direction, while an auxiliary lane is also provided in the southbound direction between SR 237

and Mathilda Avenue. US 101 south of Mathilda Avenue currently carries approximately 154,000 vehicles daily.

The Moffett Park Drive/US 101 northbound on-ramp is a one-lane on-ramp located along Moffett Park Drive west of the Mathilda Avenue/Moffett Park Drive intersection. This on-ramp merges with the westbound SR 237 off-ramp that connects to northbound US 101. The ramp terminus is signalized, and the on-ramp is not metered.

The US 101/Mathilda Avenue interchange is a partial cloverleaf interchange with access to all but two movements: southbound Mathilda Avenue to northbound US 101 and southbound US 101 to northbound Mathilda Avenue. None of the ramp termini are signalized; however, all of the on-ramps are metered.

1.1.4 TRANSIT FACILITIES IN THE PROJECT AREA

Two VTA light-rail transit (LRT) stations, Moffett Park and Lockheed Martin, are located within the Project area and serve the business district north of SR 237. VTA also operates a local bus service with four bus stops on Mathilda Avenue. The Sunnyvale Caltrain Station is located in downtown Sunnyvale, adjacent to West Evelyn Avenue.

1.1.5 PROJECT PURPOSE AND NEED

The primary purpose of the Project is to improve traffic operations on Mathilda Avenue through the US 101 and SR 237 interchanges. Due to the close proximity of the SR 237 and US 101 interchanges (less than one mile), modification of one interchange would affect the other.

Specifically, the purposes of the Project are to:

- Reduce congestion and improve traffic operations along Mathilda Avenue and at the SR 237/Mathilda Avenue and US 101/Mathilda Avenue interchanges.
- Improve mobility for all travel modes in the area, including motor vehicles, transit, bicycles, and pedestrians.
- Provide standard crosswalks and sidewalks along Mathilda Avenue, improving access to local destinations such as Moffett Park, the VTA LRT stations, and downtown Sunnyvale.

The Project is needed for the following reasons:

- Regional growth and new local development combined with inefficient roadway operations, have resulted in substantial traffic congestion on Mathilda Avenue.
- Efficient access for all travel modes into and out of downtown Sunnyvale and development to the north of SR 237 is critical to a healthy and sustainable economy. Congestion on Mathilda Avenue adversely affects the economic vitality of the City of Sunnyvale.

Overall, the Project is needed to address several issues in the Project area, including roadway deficiencies, lack of or discontinuous bicycle and pedestrian access, local roadway and freeway ramp operations, and current and future economic development.

1.1.6 PROJECT LOCATION

The Project is located in the City of Sunnyvale in Santa Clara County, California (Figure 1). On SR 237, the Project limits are from 0.3 mile east of the US 101/SR 237 interchange (post mile [PM] 2.7) to 0.3 mile east of the Mathilda Avenue undercrossing (PM 3.3). On US 101, the Project limits are from 0.5 mile south of the Mathilda Avenue overcrossing (PM 45.2) to 0.3 mile south of SR 237/US 101 interchange (PM 45.8) (Figure 2). The Project limits include approximately 0.4-mile of Innovation Way and a new road that would connect Mathilda Avenue to Bordeaux Drive; this new road will be completed by the Moffett Place Project prior to the Mathilda Avenue Improvements at SR 237 and US 101 Project. The Project occurs in a sectionless area within Township 6 South, Ranges 2 and 1 West in the Mountain View U.S. Geological Survey (USGS) 7.5-minute series topographic quadrangle.

The Biological Study Area (BSA) for the project is based on the Project limits (Figure 2).

1.2 Project Description

The Project alternatives that were developed to meet the purpose and need of the Project include Alternative 1, Alternative 2, and the No-Build Alternative. Under the No-Build Alternative, no changes would be made to the existing local roadway or freeway ramps within the Project limits. No construction activities would occur, and there would be no change in the operation of existing facilities.

The design features of the two build alternatives include reconfiguration of the US 101 and SR 237 interchanges at Mathilda Avenue. The build alternatives include design variations for reconfigured roadways and intersections as well as the construction of new signalized intersections. Proposed improvements included in the build alternatives south of Ross Drive along Mathilda Avenue and at the US 101 interchange are identical. These improvements include new bicycle and pedestrian facilities, utility relocations, new stormwater treatment facilities, enhanced lighting, ramp metering modifications, overhead signage modifications, and a new retaining wall. Unique improvements of the build alternatives occur north of Ross Drive along Mathilda Avenue primarily related to construction of a diverging diamond interchange (DDI)¹ under Build Alternative 2.

1.2.1 ROADWAY IMPROVEMENTS

The build alternatives would consist of the following roadway improvements:

- Provide three continuous through lanes in each direction on Mathilda Avenue.
- Remove northbound US 101 loop off-ramp and shift traffic to northbound US 101 diagonal off-ramp.
- Realign and widen northbound US 101 ramps and signalize ramp intersection with Mathilda Avenue, and construct left-turn lane on southbound Mathilda Avenue to access northbound US 101 loop on-ramp.

¹ A diverging diamond interchange (DDI) , also called a double crossover diamond (DCD) interchange, is a type of diamond interchange where traffic briefly crosses over to the left (opposite) side of the roadway, guided by traffic signals at each crossover. This allows vehicles to turn left onto freeway on-ramps without stopping and without conflicting with through traffic. The signals at ramp terminal intersections can be operated with two signal phases (phases when a traffic signal allows for traffic at an intersection to cycle through specific movements for each direction) instead of three.

- Realign southbound US 101 off-ramp and loop on-ramp and signalize ramp intersection with Mathilda Avenue.
- Modify Mathilda Avenue/Ross Drive signal intersection.
- Close Moffett Park Drive between Bordeaux Drive and Mathilda Avenue, replace with a Class I bikeway (as described below), and shift traffic to Bordeaux Drive and Innovation Way.²
- Remove westbound SR 237 ramp signal intersection. Realign westbound SR 237 off-ramp opposite Moffett Park Drive and modify signal intersection.
- Build Alternative 1 would modify westbound SR 237 ramps to provide a diamond configuration.
- Build Alternative 2 would modify Mathilda Avenue and SR 237 ramps to provide a diverging diamond configuration. Eastbound Moffett Park Drive between Innovation Way and Mathilda Avenue would be diverted to Innovation Way to access Mathilda Avenue.

1.2.2 BICYCLE AND PEDESTRIAN FACILITIES

Enhanced bicycle and pedestrian facilities would be provided. Bicycle improvements on Mathilda Avenue would consist of both Class II and Class III bikeways³, based on available pavement widths within the Project limits, and connect to the existing Class III bikeway north of Innovation Way and the Class I bikeway on the Sunnyvale West Channel. Bicycle improvements on Moffett Park Drive would consist of a Class I bikeway between Bordeaux Drive and Mathilda Avenue. Between Mathilda Avenue and Innovation Way, Class II and Class III bikeways would be considered, based on available pavement widths within the Project limits. A continuous sidewalk would be provided on the east side of Mathilda Avenue within the Project limits with crosswalks, curb ramps, and pedestrian countdown signals at each intersection. The new crosswalks at the reconfigured ramp intersections would be signalized.

1.2.3 UTILITY RELOCATIONS

The following utility companies have known facilities within the project limits: Pacific Gas & Electric (PG&E) gas and electric service, AT&T telephone service, Comcast cable and internet service, Verizon, San Francisco Public Utilities Commission (SFPUC) Hetch-Hetchy Aqueduct, VTA light rail electric and communication services, and City of Sunnyvale water line, recycled water line, storm drain and sanitary sewer services.

The build alternatives would include utility relocations, as necessary, to construct the above-described improvements. Build Alternative 1 would require relocation of Verizon telecommunication lines and relocation of a City of Sunnyvale recycled water line along the current alignment of Moffett Park Drive east of Mathilda Avenue. Build Alternative 2 would require relocation of a six-foot PG&E underground gas line and a 12kV PG&E underground electrical line along the current alignment of Moffett Park Drive west of Mathilda Avenue. Both Build Alternatives could require adjustments to three PG&E electrical pole wires to accommodate ramp modifications at the Mathilda Avenue/US 101 interchange. Utility covers would be adjusted to grade in areas of pavement rehabilitation.

² Innovation Way would be extended from Mathilda Avenue to Bordeaux Drive by the Moffett Place Project.

³ Class I bikeway is a bicycle path. Class II bikeway is a bicycle lane. Class III bikeway is bicycle route (Source: Highway Design Manual, Index 1002.1).

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Legend

- Biological Study Area
- Roadwork within this section to be constructed by a project other than the Mathilda Avenue Improvements at SR 237 and US 101 Project

* Depending on traffic data (still being gathered)

0 250 500
Feet

Source: Imagery; NAIP 2014

Figure 2
Biological Study Area
Mathilda Avenue Improvements at SR 237 and US 101 Project

1.2.4 STORMWATER TREATMENT

The proposed interchange ramp modifications are expected to result in the fill or removal of existing ditches, modification or relocation of existing longitudinal drainage structures, and construction of new drainage structures. The build alternative's drainage design would maintain existing drainage patterns; however, during construction, temporary drainage facilities may be required to redirect runoff from construction areas.

The stormwater treatment facilities for both build alternatives may include biofiltration strips, biofiltration swales, bioretention basins, and/or detention basins within the state right-of-way near the on- and off-ramps and on city streets.

1.2.5 ENHANCED LIGHTING

The build alternatives would both provide enhanced lighting to improve roadway visibility for drivers during nighttime hours. Overhead lighting would be maintained or installed at all ramps. The lights would either be supported on a cast-in-drilled-hole pile, with a typical diameter of 2.5 feet and depth of five feet, or mounted on a structure above grade.

1.2.6 RAMP METERING

Ramp metering facilities already exist at the northbound US 101 loop on-ramp, southbound US 101 ramps, and the westbound SR 237 on-ramp. Because these ramps would be modified and realigned under both build alternatives, the affected ramp metering equipment would also be modified.

1.2.7 OVERHEAD SIGNAGE

Updated overhead signs in each direction on SR 237 and US 101 would inform motorists of the approaching on- and off-ramps associated with the Project. The overhead sign structure mounted to the Mathilda Avenue overcrossing on northbound US 101 would be removed because it applies to the existing loop off-ramp, which is being relocated and integrated as both a west and east Mathilda Avenue access route from northbound US 101. The northbound US 101 off-ramp sign would be impacted by the off-ramp widening, therefore, it would be removed and replaced just south of the Borregas Pedestrian Overcrossing.

1.2.8 LIGHT-RAIL FACILITIES

VTA LRT facilities that cross the Moffett Park Drive/Innovation Way and Mathilda Avenue/Innovation Way intersections would be coordinated with traffic signal modifications, which would be location specific. The final locations for new traffic signals would be determined during design.

1.2.9 CONSTRUCTION AND STAGING AREAS

Construction of the build alternatives would take approximately 250 working days. A combination of day and night work is anticipated. Weekend work is not anticipated. Short-term lane and ramp closures would be necessary to facilitate construction. A Traffic Management Plan would be implemented during construction to minimize and prevent delay and inconvenience to the traveling public. Staging/laydown areas for equipment and materials would be needed during

Project construction. Construction staging areas would be located within the state right-of-way adjacent to Mathilda Avenue.

Potential locations include:

- Within the northbound US 101 loop off-ramp,
- Between the northbound US 101 diagonal off-ramp and northbound loop on-ramp,
- Within the southbound US 101 loop on-ramp,
- Between the southbound US 101 loop on-ramp and diagonal off-ramp, and
- Between the westbound SR 237 ramps and Moffett Park Drive.

Chapter 2 – Methods

2.1 Regulatory Requirements

Potentially applicable federal and state regulations for biological resources are described below.

2.1.1 FEDERAL REGULATIONS

Federal Endangered Species Act

The federal Endangered Species Act (ESA) is administered by U.S. Fish and Wildlife Service (USFWS) and National Marine Fisheries Service (NMFS). In general, NMFS is responsible for protection of ESA-listed marine species and anadromous fishes, whereas other listed species are under USFWS jurisdiction. *Endangered* refers to species, subspecies, or distinct population segments that are in danger of extinction through all or a significant portion of their range; *threatened* refers to species, subspecies, or distinct population segments that are likely to become endangered in the near future. Section 9 of the ESA is relevant to the proposed Project and is summarized below.

Endangered Species Act Prohibitions (Section 9)

Section 9 of ESA prohibits the take of any fish or wildlife species that has been listed under the ESA as endangered. Take of threatened species is also prohibited under Section 9, unless otherwise authorized by federal regulations. Take, as defined by ESA, means “to harass, harm, pursue, hunt, shoot, wound, kill, trap, capture, or collect or to attempt to engage in any such conduct.” Harm is defined as “any act that kills or injures the species, including significant habitat modification.” In addition, Section 9 prohibits removing, digging up, cutting, and maliciously damaging or destroying federally listed plants on sites that are under federal jurisdiction. Section 9 does not prohibit take of federally listed plants on sites that are not under federal jurisdiction.

Migratory Bird Treaty Act

The federal Migratory Bird Treaty Act (MBTA) (16 United States Code [USC] 703) enacts the provisions of treaties between the United States, Great Britain, Mexico, Japan, and the Soviet Union (now Russia) and authorizes the U.S. Secretary of the Interior to protect and regulate the taking of migratory birds. It protects migratory birds, their occupied nests, and their eggs (16 USC 703, 50 Code of Federal Regulations [CFR] 21, 50 CFR 10). Most actions that result in taking or in permanent or temporary possession of a protected species constitute violations of the MBTA. Examples of permitted actions that do not violate the MBTA are the possession of a hunting license to pursue specific game birds, legitimate research activities, display in zoological gardens, banding, and other similar activities. USFWS is responsible for overseeing compliance with the MBTA, and the U.S. Department of Agriculture’s (USDA’s) Animal Damage Control Officer makes recommendations on related animal protection issues.

Clean Water Act

The federal Clean Water Act (CWA) was enacted as an amendment to the federal Water Pollution Control Act of 1972, which outlined the basic structure for regulating discharges of pollutants to

waters of the United States. The CWA serves as the primary federal law to protect the quality of the nation's surface waters, including lakes, rivers, and coastal wetlands.

The CWA empowers the U.S. Environmental Protection Agency (EPA) to set national water quality standards and effluent limitations. It also includes programs for addressing both point-source and nonpoint-source pollution. Point-source pollution is pollution that originates or enters surface waters at a single, discrete location, such as an outfall structure or an excavation or construction site. Nonpoint-source pollution originates over a broader area and includes urban contaminants in stormwater runoff and sediment loading from upstream areas. The CWA operates on the principle that all discharges into the nation's waters are unlawful, unless specifically authorized by a permit; permit review is the CWA's primary regulatory tool.

The sections below provide additional details on specific sections of the CWA.

Permits for Fill Placement in Waters and Wetlands (Section 404)

CWA Section 404 regulates the discharge of dredged and fill materials into waters of the United States. *Waters of the United States* refers to oceans, bays, rivers, streams, lakes, ponds, and wetlands, including any or all of the following:

- Areas within the ordinary high-water mark of a stream, including non-perennial streams with a defined bed and bank and any stream channel that conveys natural runoff, even if it has been realigned; and
- Seasonal and perennial wetlands, including coastal wetlands.

In *Solid Waste Agency of Northern Cook County v. Army Corps of Engineers*, 521 U.S. 159 (2001), the Court held that the provision of the CWA, which requires discharging fill material into navigable waters to obtain a permit from the U.S. Army Corps of Engineers (USACE), does not extend to isolated wetlands. In the consolidated cases *Rapanos v. United States* and *Carabell v. United States*, 126 S. Ct. 2208 (2006) (referred to as the Rapanos decision), the Court reviewed the USACE definition of waters of the United States and whether or not it extended out to tributaries of traditional navigable waters (TNW) or wetlands adjacent to those tributaries. Guidance issued by EPA and USACE on the Rapanos decision provides that agencies will assert jurisdiction over non-navigable, not relatively permanent tributaries and their adjacent wetlands where such tributaries and wetlands have a significant nexus to a traditional navigable water.

Applicants must obtain a permit from USACE for all discharges of dredged or fill material into waters of the United States, including adjacent wetlands, before proceeding with a proposed activity. USACE may issue either an individual permit, evaluated on a case-by-case basis, or a general permit, evaluated at a program level for a series of related activities. General permits are preauthorized and issued to cover multiple instances of similar activities that are expected to cause only minimal adverse environmental effects. Nationwide permits (NWP) are a type of general permit to cover particular fill activities. Each NWP specifies particular conditions that must be met for the NWP to apply to a particular project.

Compliance with CWA Section 404 requires compliance with several other environmental laws and regulations. USACE cannot issue an individual permit or verify the use of a general permit until the requirements of the National Environmental Policy Act (NEPA), the ESA, and the National Historic Preservation Act (NHPA) have been met. In addition, the USACE cannot issue or verify

any permit until a water quality certification or a waiver of certification has been issued pursuant to CWA Section 401.

Permits for Stormwater Discharge (Section 402)

CWA Section 402 regulates construction-related stormwater discharges to surface waters through the National Pollutant Discharge Elimination System (NPDES) program, administered by EPA. In California, the State Water Resources Control Board is authorized by EPA to oversee the NPDES program through the Regional Water Quality Control Boards (RWQCBs) (see the related discussion under “Porter-Cologne Water Quality Control Act,” below). The project area is under the jurisdiction of the San Francisco Bay RWQCB.

The NPDES Construction General Permit is required for projects that disturb more than one acre of land. The NPDES Construction General Permit process requires the applicant to file a public notice of intent (NOI) to discharge stormwater and prepare and implement a stormwater pollution prevention plan (SWPPP). The SWPPP includes a site map and a description of proposed construction activities. In addition, it describes the best management practices (BMPs) that would be implemented to prevent soil erosion and the discharge of other construction-related pollutants (e.g., petroleum products, solvents, paints, cement) that could contaminate nearby water resources. Permittees are required to conduct before, during, and post-storm monitoring and annual reporting to ensure that BMPs are correctly implemented and effective in controlling the discharge of construction-related stormwater pollutants.

Water Quality Certification (Section 401)

Under CWA Section 401, applicants for a federal license or permit to conduct activities that may result in the discharge of a pollutant into waters of the United States must obtain certification from the state in which the discharge would originate or, if appropriate, from the interstate water pollution control agency with jurisdiction over affected waters at the point where the discharge would originate. Therefore, all projects that have a federal component and may affect state water quality (including projects that require federal agency approval, such as issuance of a Section 404 permit) must also comply with CWA Section 401.

For each of the above sections of the CWA, if the Project would result in impacts on waters of the United States or waters of the state, the Project applicant would obtain and comply with the applicable federal and state permits, and all conditions that are attached to those permits would be implemented as part of the Project. The permit conditions would be clearly identified in the construction plans and specifications and monitored during and after construction to ensure compliance.

2.1.2 STATE REGULATIONS

California Endangered Species Act

The California Endangered Species Act (CESA) prohibits the take of endangered and threatened species; however, habitat destruction is not included in the state’s definition of take. Section 2090 of CESA requires state agencies to comply with endangered species protection and recovery and to promote conservation of these species. The California Department of Fish and Wildlife (CDFW) administers the act and authorizes take through Section 2081 agreements (except for species that are designated as fully protected). CDFW can adopt a federal biological opinion as a state biological opinion under California Fish and Game Code (CFG) Section 2095. In addition, CDFW

can write a consistency determination for species that are both federally and state listed if CDFW determines that the avoidance, minimization, and compensation measures will ensure no take of species.

Porter-Cologne Water Quality Control Act

California Water Code Section 13260 requires “any person discharging waste, or proposing to discharge waste, in any region that could affect the waters of the state to file a report of discharge (an application for waste discharge requirements).” Under the Porter-Cologne Act definition, waters of the state are “any surface water or groundwater, including saline waters, within the boundaries of the state.” Although all waters of the United States that are within the borders of California are also waters of the state, the reverse is not true. Therefore, California retains authority to regulate discharges of waste into any waters of the state, regardless of whether USACE has concurrent jurisdiction under CWA Section 404. If USACE determines that a wetland is not subject to regulation under Section 404, CWA Section 401 water quality certification is not required. However, the RWQCB may impose waste discharge requirements (WDRs) if fill material is placed into waters of the state.

California Fish and Game Code

Several sections of the CFGC apply to the proposed Project and are described herein (i.e., CFGC Sections 3503, 3503.5, 3511, and 3513).

CFGC 3503 prohibits the destruction of bird nests. Section 3503.5 prohibits the killing of raptor species and destruction of raptor nests.

The CFGC provides protection from take for a variety of species, referred to as fully protected species. CFGC 3511 lists fully protected birds and prohibits take of these species. The code defines take as “hunt, pursue, catch, capture, or kill, or attempt to hunt, pursue, catch, capture, or kill.” Except for take related to scientific research, all take of fully protected birds is prohibited.

CFGC 3513 prohibits the take or possession of any migratory non-game bird, as designated in the MBTA, or any part of such migratory non-game bird, except as provided by rules and regulations adopted by the Secretary of the Interior under provisions of the MBTA.

California Native Plant Protection Act

The California Native Plant Protection Act (CNPPA) of 1977 prohibits importation of rare and endangered plants into California, take of rare and endangered plants, and the sale of rare and endangered plants. The CESA defers to the CNPPA, which ensures that state-listed plant species are protected when state agencies are involved in projects that are subject to CEQA. In this case, plants that are listed as rare under the CNPPA are not protected under CESA but rather under CEQA.

2.1.3 LOCAL REGULATIONS

City of Sunnyvale Tree Preservation

The City of Sunnyvale regulates the protection, installation, removal and long term management of significantly sized trees on private property within the city and city owned golf courses and

parks (Sunnyvale Municipal Code 19.94). The City's Planning Department considers a tree protected if it meets the following specifications:

- Any single trunk tree 38 inches or greater in circumference at breast height (4.5 feet above grade) or 12 inches or greater in diameter at breast height (DBH), and
- Any multi-trunk tree that has at least one trunk 38 inches or greater in circumference at breast height or multi-trunk measurements added together that equal at least 113 inches.

Water Resources Protection Ordinance (06-1)

The Water Resources Protection Ordinance was adopted by a Water Resources Protection Collaborative, which is made up of representatives from the Santa Clara Valley Water District, cities and towns within Santa Clara County, the Guadalupe-Coyote Resource Conservation District, the RWQCB, and various community stakeholder interests. Its purpose is to protect the water resources managed by the District by providing a set of model guidelines and standards for land uses along stream corridors and regulate access to and use of the District's facilities and easements.

2.2 Studies Required

Biological resources and potential impacts on such resources due to the Project were identified through a literature and database review, correspondence with USFWS, and reconnaissance field surveys. Based on the information collected, ICF determined that the following studies would be required to document natural resources in the biological study area (BSA; defined in Chapter 3, Results: Environmental Setting):

- Botanical field survey to identify plant communities, trees, and suitable habitat for special-status plant species;
- General habitat assessment for special-status wildlife species; and
- Delineation of waters of the United States.

2.2.1 LITERATURE AND DATABASE REVIEW

To prepare for the field surveys and evaluate whether special-status species or other sensitive biological resources (e.g., wetlands) could occur in the BSA and vicinity, biologists reviewed the following:

- California Native Plant Society's (CNPS's) *Inventory of Rare and Endangered Plants of California* (California Native Plant Society 2015) (Appendix A);
- California Natural Diversity Database (CNDDDB) records search for the U.S. Geological Survey (USGS) 7.5-minute Mountain View quadrangle (CDFW 2015) (Appendix B); and
- USFWS list of threatened and endangered species for the Mathilda Avenue Improvements at SR 237 and US 101 Project (USFWS 2016) (Appendix C);

Based on information from the above sources, ICF developed lists of special-status species and natural communities of special concern that could be present in the Project vicinity. Figures 3a and 3b present the results of a 2-mile CNDDDB record search around the BSA for special-status

plants and wildlife. All biological resources are evaluated for their potential to occur within the BSA in Chapter 3 of this NES-MI.

2.3 Personnel and Survey Dates

ICF biologists surveyed the BSA in March and July 2015. Methods for documenting botanical, wildlife, and wetland resources are described below.

2.3.1 BOTANICAL RESOURCES

ICF botanists Amy May and Torrey Edell conducted botanical surveys on March 6 and July 29, 2015, by walking through the accessible portions of the BSA and identifying all plant species encountered. During the botanical field surveys, vegetation communities were identified and mapped, and trees were identified and recorded. Results of these surveys are presented in Chapters 3 and 4.

2.3.2 WILDLIFE RESOURCES

ICF wildlife biologist Eric Christensen conducted a reconnaissance-level survey of the BSA and immediately adjacent areas on March 6, 2015. The survey was conducted on foot with binoculars to ensure thorough visual coverage. Observations of habitat conditions and wildlife species were recorded in field notes. Results of the survey are presented in Chapters 3 and 4.

2.3.3 DELINEATION OF WATERS OF THE UNITED STATES

Concurrently with the botanical and wildlife surveys described above, ICF biologists identified features that could be considered jurisdictional waters of the United States by USACE. Details regarding the methods used in the survey and the results are presented in the wetlands assessment in Appendix D. All waters of the United States identified in the wetlands assessment also are assumed to be subject to state jurisdiction.

2.3.4 LIMITATIONS THAT MAY INFLUENCE RESULTS

Access to the Mathilda Avenue overpass above US 101 was largely limited due to the traffic traveling on US 101. The underside of the overpass was viewed from the side of US 101 with binoculars during the survey, but not all areas of the overpass were able to be visually inspected. At the time of the delineation fieldwork in 2015, California was in a historic drought. However, factors that would be affected, including hydrophytic vegetation and wetland hydrology, were evident and identifiable. Therefore, there were no other limitations with regard to the survey for biological resources, or wetland and non-wetland waters in the BSA.

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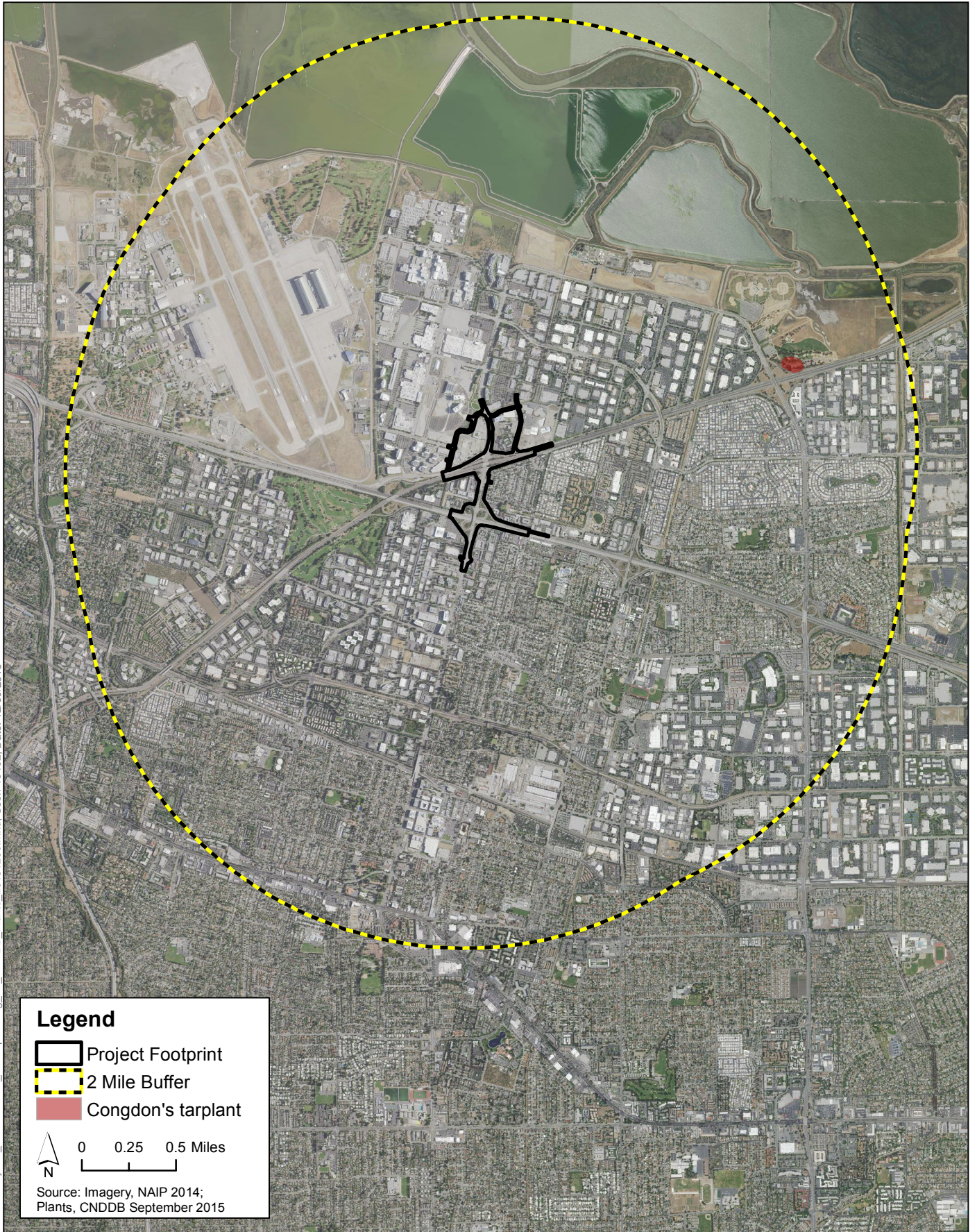


Figure 3a
Plant Occurrences within 2 Miles of the Project Footprint

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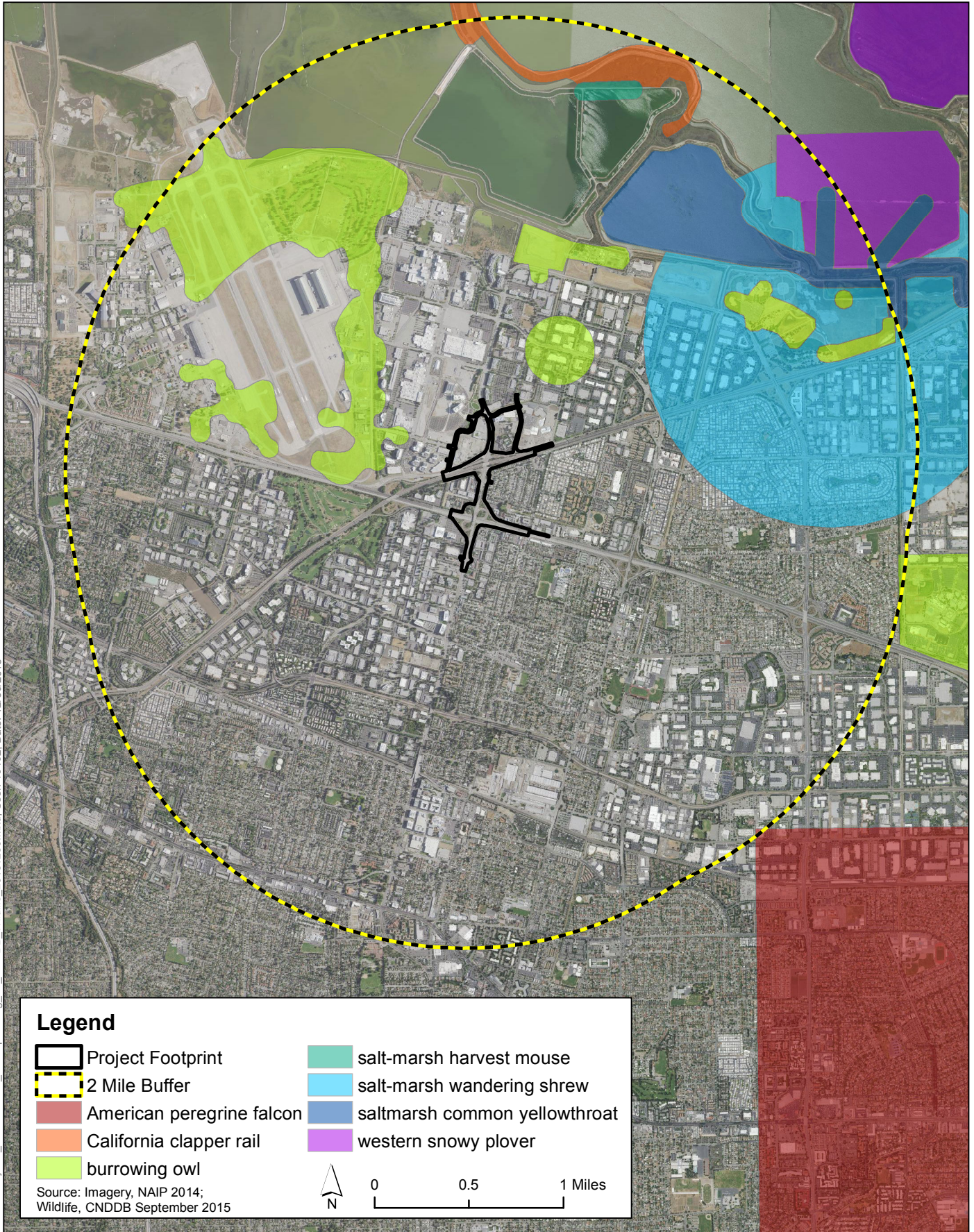


Figure 3b
Wildlife Occurrences within 2 Miles of the Project Footprint

Chapter 3 – Results: Environmental Setting

3.1 Description of the Existing Biological and Physical Conditions

This section includes a description of biological and physical conditions present in the Biological Study Area (BSA).

3.1.1 BIOLOGICAL STUDY AREA

The BSA for the Project is approximately 63 acres in size and includes areas that would be directly impacted during construction as well as adjacent areas that could be indirectly impacted (e.g., aquatic features susceptible to construction-related runoff, habitat for nesting birds that could be disturbed) (Figure 2). On SR 237, the BSA, which is equivalent to the Project limits, extends from 0.3 mile east of the US 101/SR 237 interchange (PM 2.7) to 0.3 mile east of the Mathilda Avenue undercrossing (PM 3.3). On US 101, the BSA extends from 0.5 mile south of Mathilda Avenue overcrossing (PM 45.2) to 0.3 mile south of SR 237/US 101 interchange (PM 45.8). The BSA includes approximately 0.4-mile of Innovation Way and a new road that would connect Mathilda Avenue to Bordeaux Drive; this new road will be completed by the Moffett Place Project prior to the Mathilda Avenue Improvements at SR 237 and US 101 Project. The total length of the Project on Mathilda Avenue is approximately one mile.

3.1.2 PHYSICAL CONDITIONS

The BSA is located in the San Francisco Bay Area, which is characterized by warm, dry summers and mild, wet winters, with most of the rainfall occurring between November and March. The BSA has an estimated mean annual temperature of 59 degrees Fahrenheit and an estimated mean annual precipitation of 15.71 inches (USDA, Natural Resources Conservation Service 2015). Vegetation is adapted to this Mediterranean climate, and the landscape is a mosaic of drought-adapted tree, shrub, and grassland communities. Elevations in the BSA range from approximately 15 feet above mean sea level in low-lying areas to 40 feet above mean sea level on raised highway ramps (Google Earth Pro 2015). Topography within the BSA is relatively flat, with a gentle downward slope from US 101 to SR 237.

The Sunnyvale West Channel occurs within the northwestern area of the BSA and provides flood control protection to the surrounding communities. Water flows through the channel to the San Francisco Bay via Guadalupe Slough. The Sunnyvale West Channel is assumed to be subject to USACE jurisdiction under Section 404 of the CWA because of its direct hydrologic connection to the Bay. While the Channel is located within the BSA, the construction of the proposed road that will connect Mathilda Avenue with Bordeaux Drive, which will affect the Channel, is part of the Moffet Place Project. The Mathilda Avenue Improvements at SR 237 and US 101 Project will not affect the Sunnyvale West Channel, as the Project proposes the construction of traffic signals and striping for bicycle lanes within the Mathilda Avenue-Bordeaux Drive connector road after its construction. Stormwater drainage ditches run parallel to Mathilda Avenue and occur along cloverleaves and other ingress/egress ramps to and from US 101 and SR 237 and Mathilda Avenue within the BSA. The ditches drain stormwater runoff during rain events, but flow does not persist after rain events. These ditches were constructed in upland areas to drain the adjacent roads and highway segments, and ultimately drain into the municipal stormwater system. Therefore, the stormwater drainage ditches are not considered to be subject to USACE jurisdiction or state jurisdiction.

3.1.3 BIOLOGICAL CONDITIONS

Two land cover types occur in the BSA: developed and landscaped (Figure 4). The developed land cover type consists of the existing paved Mathilda Avenue, on- and off-ramps from US 101 and SR 237, other existing roads, parking lots, and residential and commercial development. The landscaped cover type comprises the remainder of the BSA (15 acres) and is described under *Vegetation Communities*, below.

Vegetation Communities

Landscaped vegetation is typically planted and consists of non-native, ornamental plant species and/or cultivars of native plant species that may or not be regularly maintained or managed. Although not considered a natural vegetation community, landscaped vegetation can provide habitat and food sources for wildlife. Common plant species in the landscaped vegetation in the BSA include purple lantana (*Lantana montevidensis*), Peruvian pepper (*Schinus molle*), deodar cedar (*Cedrus deodara*), gum trees (*Eucalyptus* sp.), southern magnolia (*Magnolia grandiflora*), white Lady Banks rose (*Rosa banksiae*), and olive (*Olea europaea*), to name a few. Ground cover in the landscaped cover type consists primarily of ruderal species, including oat (*Avena* sp.), ripgut grass (*Bromus diandrus*), summer mustard (*Hirschfeldia incana*), Italian thistle (*Carduus pycnocephalus* subsp. *pycnocephalus*), bristly ox-tongue (*Helminthotheca echioides*), smilo grass (*Stipa miliaceae* var. *miliaceae*), and prickly lettuce (*Lactuca serriola*).

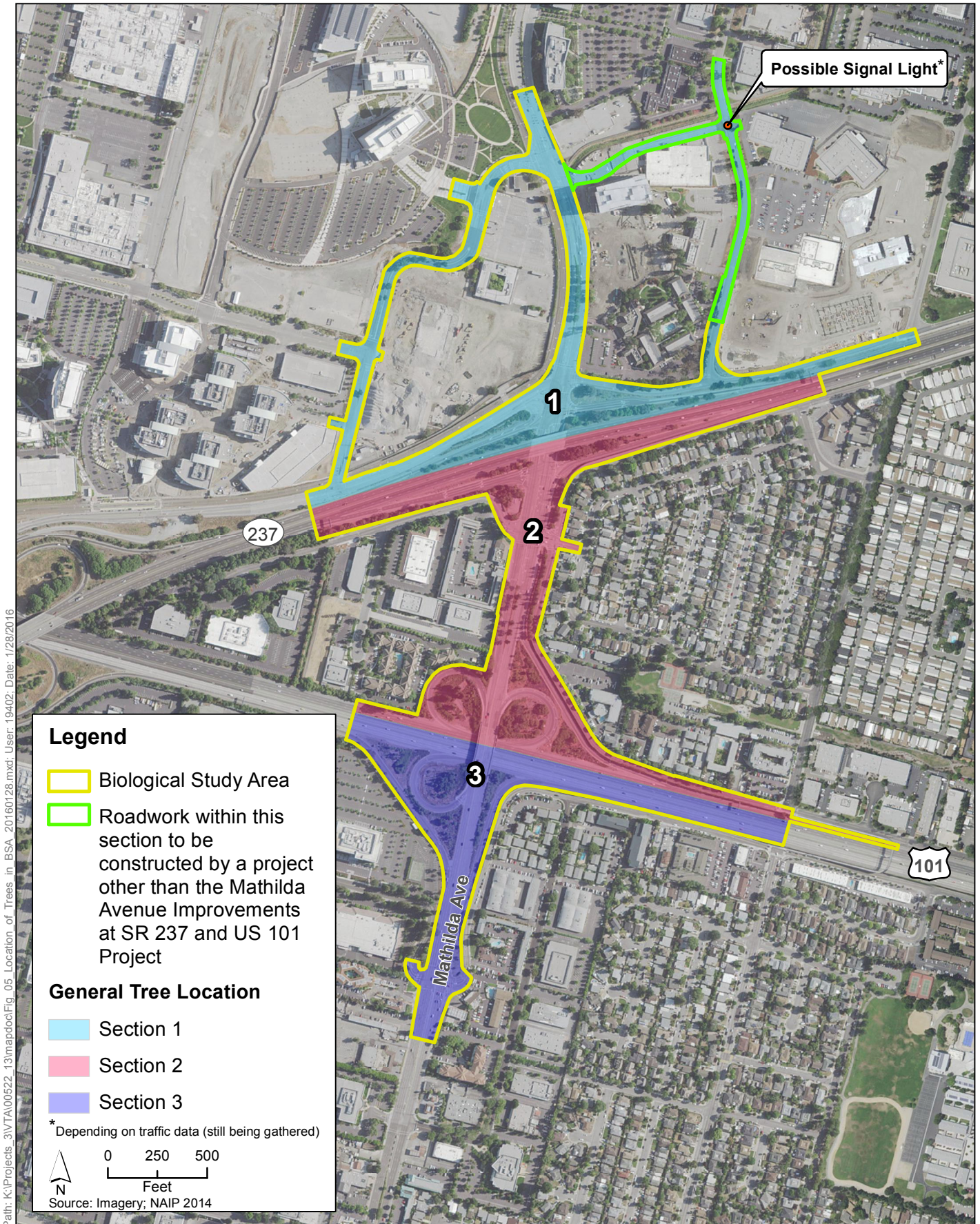
Trees

Trees in the BSA occur within the landscaped cover type and consist mostly of non-native species. Table 1 includes a list of all 626 trees identified within the BSA and their approximate DBH. Refer to Figure 5 for the general locations of the identified trees.

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Figure 4
Land Cover Types within the BSA
Mathilda Avenue Improvements at SR 237 and US 101 Project



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Figure 5
General Location of Trees within the Biological Study Area
 Mathilda Avenue Improvements at SR 237 and US 101 Project

Table 1. Trees in the BSA

| Common Name* | Scientific Name | Number of Trees | DBH | General Location |
|--------------------------|---------------------------------|-----------------|--------|--|
| ash | <i>Fraxinus</i> sp. | 7 | 2–6 | Project limits north of SR 237, including Moffett Park Drive (Figure 5, Section 1) |
| ash, autumn purple | <i>Fraxinus americana</i> | 1 | 8 | |
| ash, velvet | <i>Fraxinus velutina</i> | 1 | 2–6 | |
| blackwood acacia | <i>Acacia melanoxyton</i> | 2 | 2–8 | |
| Bradford pear | <i>Pyrus calleryana</i> | 13 | 8–12 | |
| camphor tree | <i>Cinnamomum camphora</i> | 2 | 4–8 | |
| Chinese elm | <i>Ulmus parvifolia</i> | 5 | 2–8 | |
| Chinese elm | <i>Ulmus parvifolia</i> | 3 | 16 | |
| Chinese pistache | <i>Pistacia chinensis</i> | 1 | 6–10 | |
| coast redwood* | <i>Sequoia sempervirens</i> | 27 | 4–12 | |
| crape myrtle | <i>Lagerstroemia</i> sp. | 6 | 2–6 | |
| crape myrtle | <i>Lagerstroemia</i> sp. | 4 | 6–8 | |
| gum | <i>Eucalyptus</i> sp. | 1 | 20–30 | |
| gum, blue | <i>Eucalyptus globulus</i> | 1 | 14–18 | |
| gum, blue | <i>Eucalyptus globulus</i> | 3 | 20–30 | |
| gum, red | <i>Eucalyptus camaldulensis</i> | 8 | 30 | |
| gum, silver dollar | <i>Eucalyptus polyanthemos</i> | 2 | 30 | |
| Italian stone pine | <i>Pinus pinea</i> | 19 | 50–100 | |
| oak, coast live* | <i>Quercus agrifolia</i> | 10 | 6–10 | |
| oak, southern live | <i>Quercus virginiana</i> | 32 | 4–10 | |
| oak, southern live | <i>Quercus virginiana</i> | 1 | 30 | |
| Peruvian pepper | <i>Schinus molle</i> | 9 | 16–30 | |
| purple-leaf plum | <i>Prunus cerasifera</i> | 6 | 6–10 | |
| sheoak | <i>Casuarina</i> sp. | 1 | 6–10 | |
| sheoak | <i>Casuarina</i> sp. | 1 | 30–50 | |
| unknown ornamental | — | 1 | 6 | |
| ash | <i>Fraxinus</i> sp. | 4 | 6–12 | Adjacent to Mathilda Avenue between SR 237 and US 101 (Figure 5, Section 2) |
| ash, autumn purple | <i>Fraxinus americana</i> | 2 | 8 | |
| blackwood acacia | <i>Acacia melanoxyton</i> | 5 | 4–10 | |
| California black walnut* | <i>Juglans californicus</i> | 11 | 8–16 | |
| Chinese elm | <i>Ulmus parvifolia</i> | 5 | 6–10 | |
| Chinese pistache | <i>Pistacia chinensis</i> | 23 | 8–12 | |
| Chinese pistache | <i>Pistacia chinensis</i> | 1 | 20 | |
| Chinese privet | <i>Ligustrum lucidum</i> | 19 | 6–10 | |

| Common Name* | Scientific Name | Number of Trees | DBH | General Location |
|---------------------|---------------------------------|-----------------|-------|---|
| coast redwood* | <i>Sequoia sempervirens</i> | 27 | 20–40 | Adjacent to Mathilda Avenue between SR 237 and US 101 (Figure 5, Section 2) |
| crimson bottlebrush | <i>Callistemon citrinus</i> | 2 | 6–10 | |
| deodar cedar | <i>Cedrus deodara</i> | 16 | 12–20 | |
| deodar cedar | <i>Cedrus deodara</i> | 17 | 20–30 | |
| gum | <i>Eucalyptus</i> sp. | 7 | 14–18 | |
| gum, blue | <i>Eucalyptus globulus</i> | 19 | 12–30 | |
| gum, red | <i>Eucalyptus camaldulensis</i> | 1 | 20 | |
| Italian cypress | <i>Cupressus sempervirens</i> | 1 | 8–12 | |
| Lombardy poplar | <i>Populus nigra</i> | 9 | 16–26 | |
| oak, coast live* | <i>Quercus agrifolia</i> | 5 | 4–10 | |
| oak, southern live | <i>Quercus virginiana</i> | 34 | 4–10 | |
| Peruvian pepper | <i>Schinus molle</i> | 15 | 20–30 | |
| Peruvian pepper | <i>Schinus molle</i> | 28 | 8–16 | |
| pine | <i>Pinus</i> sp. | 6 | 6–10 | |
| pine, Canary Island | <i>Pinus canariensis</i> | 9 | 16–24 | |
| purple-leaf plum | <i>Prunus cerasifera</i> | 8 | 6–10 | |
| silk oak | <i>Grevillea robusta</i> | 12 | 12–18 | |
| southern magnolia | <i>Magnolia grandiflora</i> | 3 | 8–14 | |
| unknown ornamental | <i>Prunus</i> sp. | 5 | 8–12 | |
| wax myrtle | <i>Myrica cerifera</i> | 7 | 8–12 | |
| western redbud* | <i>Cercis occidentalis</i> | 1 | 4–8 | |
| blackwood acacia | <i>Acacia melanoxylon</i> | 2 | 6–10 | |
| camphor tree | <i>Cinnamomum camphora</i> | 7 | 10–20 | |
| Chinese elm | <i>Ulmus parvifolia</i> | 10 | 10–20 | |
| Chinese pistache | <i>Pistacia chinensis</i> | 6 | 8–12 | |
| gum, red | <i>Eucalyptus camaldulensis</i> | 1 | 10–20 | |
| London plane | <i>Platanus acerifolia</i> | 4 | 10–20 | |
| purple-leaf plum | <i>Prunus cerasifera</i> | 7 | 8–12 | |
| red maple | <i>Acer rubrum</i> | 3 | 8–12 | |
| silver birch | <i>Betula pendula</i> | 2 | 16 | |

| Common Name* | Scientific Name | Number of Trees | DBH | General Location |
|--------------------------|-----------------------------|-----------------|-------|---|
| ash | <i>Fraxinus</i> sp. | 1 | 6–12 | Project limits south of US 101 (Figure 5, Section 3) |
| ash, autumn purple | <i>Fraxinus americana</i> | 1 | 10 | |
| blackwood acacia | <i>Acacia melanoxylon</i> | 3 | 6–10 | |
| California black walnut* | <i>Juglans californicus</i> | 3 | 8–16 | |
| Chinese elm | <i>Ulmus parvifolia</i> | 8 | 6–10 | |
| Chinese pistache | <i>Pistacia chinensis</i> | 12 | 4–8 | |
| Chinese privet | <i>Ligustrum lucidum</i> | 3 | 6–10 | |
| crape myrtle | <i>Lagerstroemia</i> sp. | 18 | 4–8 | |
| deodar cedar | <i>Cedrus deodara</i> | 17 | 12–20 | |
| gum | <i>Eucalyptus</i> sp. | 3 | 12–20 | |
| oak, southern live | <i>Quercus virginiana</i> | 12 | 8–14 | |
| olive | <i>Olea europaea</i> | 2 | 6–10 | |
| Peruvian pepper | <i>Schinus molle</i> | 20 | 16–30 | |
| pine | <i>Pinus</i> sp. | 1 | 6–10 | |
| southern magnolia | <i>Magnolia grandiflora</i> | 1 | 16 | |
| unknown ornamental | <i>Prunus</i> sp. | 10 | 6–12 | |
| Total | | 626 | | |
| * Native species | | | | |

Invasive Plant Species

Invasive plant species include species that have been designated as federal noxious weeds by USDA, species that have been listed as pests by the California Department of Food and Agriculture (CDFA), and other invasive plants that have been designated by the California Invasive Plant Council (Cal-IPC). Roads, highways, and related construction projects are some of the principal dispersal pathways for invasive plant species. The introduction and spread of invasive plants adversely affect natural plant communities by displacing native plant species that provide shelter and forage for wildlife species. Table 2 identifies invasive plant species identified in the BSA.

Table 2. Invasive Plant Species Identified in the BSA

| Species | CDFA | Cal-IPC |
|---|------|----------|
| blackwood acacia (<i>Acacia melanoxylon</i>) | — | Limited |
| bristly ox-tongue (<i>Helminthotheca echioides</i>) | — | Limited |
| California burclover (<i>Medicago polymorpha</i>) | — | Limited |
| edible fig (<i>Ficus carica</i>) | — | Moderate |
| English ivy (<i>Hedera helix</i>) | — | High |
| fennel (<i>Foeniculum vulgare</i>) | — | High |
| gum, blue (<i>Eucalyptus globulus</i>) | — | Limited |
| gum,red (<i>Eucalyptus camaldulensis</i>) | — | Limited |
| Italian thistle (<i>Carduus pycnocephalus</i>) | C | Moderate |
| oat (<i>Avena</i> sp.) | — | Moderate |
| olive (<i>Olea europaea</i>) | — | Limited |
| Peruvian pepper tree (<i>Schinus molle</i>) | — | Limited |
| ripgut brome (<i>Bromus diandrus</i>) | — | Moderate |
| Russian thistle (<i>Salsola tragus</i>) | C | Limited |
| soft chess (<i>Bromus hordeaceus</i>) | — | Limited |
| summer mustard (<i>Hirschfeldia incana</i>) | — | Moderate |

Notes: The California Department of Food and Agriculture (CDFA) and California Invasive Plant Council (Cal-IPC) lists assign ratings that reflect CDFA and Cal-IPC views of the statewide importance of the pest, the likelihood that eradication or control efforts would be successful, and the present distribution of the pest in the state. These ratings are guidelines that indicate the most appropriate action to take against a pest under general circumstances. The Cal-IPC species list is more inclusive than the CDFA list.

The CDFA category indicated in the table is defined as follows:
C: State-endorsed holding action and eradication only when found in a nursery; action to retard spread outside nurseries at the discretion of the county agricultural commissioner.

The Cal-IPC categories indicated in the table are defined as follows:
High: Species with severe ecological impacts, high rates of dispersal and establishment, and usually wide distribution.
Moderate: Species with substantial and apparent ecological impacts, moderate to high rates of dispersal, and limited to widespread distribution; establishment dependent on disturbance.
Limited: Species with minor ecological impacts, low to moderate rates of invasion, and limited distribution; locally persistent and problematic.

Aquatic Resources

No naturally occurring aquatic resources, such as wetlands, streams, or sloughs, are present in the BSA. A concrete-lined flood control channel (the Sunnyvale West Channel) is culverted underneath SR 237 and Mathilda Avenue where it intersects with the BSA and it eventually drains to Guadalupe Slough approximately 2 miles northeast of the BSA. This channel is not identified in Figure 4 of the NES-MI; however, it is identified in Figure 4 of the Project's wetlands assessment (Appendix D).

Habitat Connectivity

The BSA is largely developed, with undeveloped areas having been landscaped with predominantly non-native species. The BSA does not possess any characteristics (e.g., riparian vegetation, stream/creek) that facilitate habitat connectivity for migratory and/or local wildlife species and is not located within a known wildlife corridor. The presence of US 101 and SR 237, as well as the existing Mathilda Avenue and arterial streets, isolate the BSA from the surrounding landscape.

Regional Species and Habitats and Natural Communities of Concern

Regional species and habitats and natural communities of concern are generally the species, habitats and/or resources that are included in published regional lists maintained by entities such as CDFW, USFWS and CNPS. Tables 3 and 4 list special-status plant and wildlife species, respectively, which are known or have the potential to occur in the general Project vicinity. These species were identified through the CNPS *Inventory of Rare and Endangered Plants* (2015) (Appendix A), the CNDDDB records search (2015) (Appendix B), species lists provided by USFWS (2016) (Appendix C), and habitat observations during the March and July field surveys.

Table 3. Special-Status Plant Species Known or with Potential to Occur in the Project Region

| Scientific and Common Names | Status ^a Federal/ State/ CNPS | Geographic Distribution | General Habitat Description | Blooming Period | Habitat Present/ Absent | Rationale | Effect Finding for Federally Listed Species |
|--|--|--|--|-----------------|-------------------------|--|---|
| <i>Astragalus tener</i> var. <i>tener</i> Alkali milk-vetch | -/-1B.2 | Southern Sacramento Valley, northern San Joaquin Valley, east San Francisco Bay Area | Playas, on adobe clay in valley and foothill grassland, vernal pools on alkaline soils; 1–200 feet | Mar–June | A | Playas, valley and foothill grassland, vernal pools, and adobe clay and alkaline soils not present in the BSA. Not observed during March or July 2015 surveys. | Not applicable. |
| <i>Centromadia parryi</i> ssp. <i>congdonii</i> Congdon's tarplant | -/-1B.1 | East San Francisco Bay Area, Salinas Valley, Los Osos Valley | Alkaline soils in annual grassland, on lower slopes, flats, and swales (sometimes on saline soils); below 755 feet | May–Oct (Nov) | A | Alkaline and saline soils not present in the BSA. Not observed during March or July 2015 surveys. | Not applicable. |
| <i>Chloropyron maritimum</i> ssp. <i>palustre</i> Point Reyes bird's-beak | -/-1B.2 | Coastal Northern California, from Humboldt to Santa Clara County; Oregon | Coastal salt marsh; below 33 feet | June–Oct | A | Coastal salt marsh not present in the BSA. Not observed during March or July 2015 surveys. | Not applicable. |
| <i>Eryngium aristulatum</i> var. <i>hooveri</i> Hoover's button-celery | -/-1B.1 | South San Francisco Bay Area; South Coast Ranges in Alameda, San Benito, Santa Clara, and San Luis Obispo Counties | Vernal pools; 9–148 feet | July (Aug) | A | Vernal pools not present in BSA. Not observed during March or July 2015 surveys. | Not applicable. |
| <i>Stuckenia filiformis</i> ssp. <i>alpina</i> Slender-leaved pondweed | -/-2B.2 | Scattered locations in California: Contra Costa, El Dorado, Lassen, Merced, Mono, Modoc, Mariposa, Placer, Santa Clara, and Sierra Counties; Arizona, Nevada, Oregon, Washington | Freshwater marsh, shallow emergent wetlands and freshwater lakes, drainage channels; 984–7,054 feet | May–July | A | Freshwater marsh, shallow emergent wetlands, freshwater lakes not present in BSA. Not observed during March or July 2015 surveys. | Not applicable. |

| Scientific and Common Names | Status ^a Federal/ State/ CNPS | Geographic Distribution | General Habitat Description | Blooming Period | Habitat Present/ Absent | Rationale | Effect Finding for Federally Listed Species |
|--|--|---|--|-----------------|-------------------------|--|---|
| <i>Suaeda californica</i> California seablite | FE/-/1B.1 | Morro Bay, San Luis Obispo County, and San Francisco and Contra Costa Counties; historically found in the south San Francisco Bay | Margins of tidal salt marsh; below 49 feet | July–Oct | A | Tidal salt marsh not present in BSA. Not observed during March or July 2015 surveys. | No effect – no habitat available within project limits. |

^a Status explanations:

Federal

FE = listed as *endangered* under the Endangered Species Act (ESA)
 – = no listing

State

– = no listing

California Native Plant Society (CNPS)

1A = List 1A species: presumed extinct in California
 1B = List 1B species: rare, threatened, or endangered in California and elsewhere
 2 = List 2 species: rare, threatened, or endangered in California but more common elsewhere

CNPS Code Extensions:

0.1 = seriously endangered in California (more than 80 percent of occurrences threatened/high degree and immediacy of threat)
 0.2 = fairly endangered in California (20–80 percent of occurrences threatened)

Table 4. Special-Status Wildlife Species Known or with Potential to Occur in the Project Region

| Common Name Scientific Name | Legal Status (Federal/State /Other) ^a | General Habitat Description | Habitat Present/ Absent | Rationale | Effect finding for Federally Listed Species |
|---|--|--|-------------------------------|--|---|
| Invertebrates | | | | | |
| <i>Callophrys mossii bayensis</i> San Bruno elfin butterfly | FE/- | North-facing slopes and ridges that face the Pacific Ocean, from 600 to 1,100 feet that support <i>Sedum spathulifolium</i> , its host plant. | A | No suitable slopes or ridges that face the Pacific Ocean present in the BSA. No <i>Sedum spathulifolium</i> observed in the BSA during March or July 2015 surveys. | No effect – no suitable habitat within the BSA. |
| <i>Euphydryas editha bayensis</i> Bay checkerspot butterfly | FT/- | Native grasslands on outcrops of serpentine soil; California plantain and owl's clover are host plants | A | No suitable native grasslands on outcrops of serpentine soil present in the BSA. | No effect – no suitable habitat within the BSA. |
| <i>Lepidurus packardii</i> Vernal pool tadpole shrimp | FE/- | Found in vernal pools and ephemeral stock ponds | A | No suitable vernal pool or ephemeral stock pond habitat in the BSA. | No effect – no suitable habitat within the BSA. |
| Amphibians | | | | | |
| <i>Ambystoma californiense</i> California tiger salamander | FT/ST | Small ponds, lakes, or vernal pools in grasslands and oak woodlands for larvae; rodent burrows, rock crevices, or fallen logs for cover for adults and for summer dormancy | A | No suitable aquatic breeding or upland (rodent burrow complexes within uplands) habitat in the BSA. | No effect – no suitable habitat within the BSA. |
| <i>Rana draytonii</i> California red-legged frog | FT/SSC | Permanent and semipermanent aquatic habitats, such as creeks and coldwater ponds, with emergent and submergent vegetation; may aestivate in rodent burrows or cracks during dry periods | A | No suitable aquatic breeding or upland habitat (rodent burrow complexes) in the BSA. | No effect – no suitable habitat within the BSA. |
| Birds | | | | | |
| <i>Agelaius tricolor</i> (nesting colony) Tricolored blackbird | —/SSC | Nests in dense colonies in emergent marsh vegetation, such as tules and cattails, or upland sites with blackberries, nettles, thistles, and grainfields; habitat must be large enough to support 50 pairs; probably requires water at or near the nesting colony | A | No suitable marsh habitat in the BSA. | Not applicable. |

| Common Name Scientific Name | Legal Status (Federal/State /Other) ^a | General Habitat Description | Habitat Present/ Absent | Rationale | Effect finding for Federally Listed Species |
|---|--|--|--|---|---|
| <i>Athene cunicularia</i> burrowing owl | —/SSC | Level, open, dry, heavily grazed or low-stature grassland or desert vegetation to forage in with available burrows for refuge and nesting | A | No suitable level, open, dry, heavily grazed, or low-stature grassland or desert vegetation with available rodent burrows in the BSA. | Not applicable. |
| <i>Charadrius alexandrinus nivosus</i> western snowy plover | FT/SSC | Coastal beaches above the normal high-tide limit in flat, open areas with sandy or saline substrates; vegetation and driftwood are usually sparse or absent | A | No suitable coastal beach habitat in the BSA. | No effect – no suitable habitat within the BSA. |
| <i>Circus cyaneus</i> northern harrier | —/SSC | Grasslands, meadows, marshes, and seasonal and agricultural wetlands; nests on the ground within a thicket of vegetation | P (foraging) / A (nesting) | No suitable grassland, meadow, marsh, or wetland habitat in the BSA. Known to occur within 2 miles of BSA (CDFW 2015) but not expected to nest because of ongoing disturbance and lack of suitable nesting substrate. Individuals may occasionally forage in undeveloped open areas within BSA. | Not applicable. |
| <i>Coccyzus americanus occidentalis</i> western yellow-billed cuckoo | FT/SE | Wide, dense riparian forests with a thick understory of willows for nesting; sites with a dominant cottonwood overstory are preferred for foraging; may avoid valley-oak riparian habitats where scrub jays are abundant | A | No suitable riparian habitat in the BSA. | No effect – no suitable habitat within the BSA. |
| <i>Falco peregrinus</i> American peregrine falcon | —/FP | Near wetlands, lakes, rivers, or other water; on cliffs, banks, dunes, mounds; also, human-made structures | A | No suitable wetland, lake, riparian, or cliff habitat in the BSA. Unlikely to occur on buildings surrounding Project site because of the high level of human activity/disturbance | Not applicable. |
| <i>Geothlypis trichas sinuosa</i> San Francisco (=salt marsh) common yellowthroat | —/SSC | Freshwater marshes in summer and salt or brackish marshes in fall and winter; requires tall grasses, tules, and willow thickets for nesting and cover | A | No suitable marsh or riparian habitat in the BSA. | Not applicable. |

| Common Name Scientific Name | Legal Status (Federal/State /Other)^a | General Habitat Description | Habitat Present/ Absent | Rationale | Effect finding for Federally Listed Species |
|---|--|--|--|--|--|
| <i>Laterallus jamaicensis coturniculus</i> California black rail | —/ST | Tidal salt marshes associated with dense pickleweed; also occurs in brackish or freshwater marshes at low elevations | A | No suitable marsh habitat in the BSA. | Not applicable. |
| <i>Melospiza melodia pusillula</i> Alameda song sparrow | —/SSC | Tidal marshes dominated by pickleweed; nests in tall vegetation (gumplant) or dense stands of pickleweed | A | No suitable tidal salt marsh habitat in the BSA. | Not applicable. |
| <i>Rallus longirostris obsoletus</i> California clapper rail | FE/— | Restricted to tidal salt marshes; usually associated with dense pickleweed and abundant tidal channels | A | No suitable tidal salt marsh habitat in the BSA. | No effect – no suitable habitat within the BSA. |
| <i>Sternula antillarum</i> (=Sterna, =albifrons) browni California least tern | FE/SE | Nests on sandy, upper ocean beaches, and occasionally uses mudflats; forages on adjacent surf line, estuaries, or the open ocean | A | No suitable nesting or foraging habitat in the BSA. | No effect – no suitable habitat within the BSA. |
| Mammals | | | | | |
| <i>Antrozous pallidus</i> pallid bat | —/SSC/ WBWG-High | Occurs throughout California, primarily at lower and mid-level elevations in a variety of habitats, from desert to coniferous forest; most closely associated with oak, yellow pine, redwood, and giant sequoia habitats in Northern California and oak woodland, grassland, and desert scrub in Southern California. Daytime roosts include rock outcrops, mines, caves, hollow trees, buildings, and bridges. Extremely intolerant of urban development. | A | Extirpated from the Santa Clara Valley floor (D. Johnston, pers. comm.) | Not applicable. |
| <i>Corynorhinus townsendii</i> Townsend's big-eared bat | —/SCT, SSC/ WBWG-High | Roosts in caves, tunnels, mines, and dark attics of abandoned buildings; very sensitive to disturbances; may abandon roost after one on-site visit. | A | No suitable roosting habitat in the BSA, due to the species' sensitivity to disturbance and the presence of routine vehicular disturbance. | Not applicable. |

| Common Name Scientific Name | Legal Status (Federal/State /Other) ^a | General Habitat Description | Habitat Present/ Absent | Rationale | Effect finding for Federally Listed Species |
|--|--|---|-------------------------------|--|---|
| <i>Lasiurus cinereus</i> hoary bat | —/—/MBWG- Medium | Roosts in trees, typically within forests | A | No suitable native tree habitat in the BSA. Vehicular disturbance reduces the likelihood of the species roosting within the BSA. | Not applicable. |
| <i>Reithrodontomys raviventris</i> salt marsh harvest mouse | FE/SE, FP | Tidal salt marshes with dense pickleweed and fat hen with sufficient high-tide cover in adjacent uplands | A | No suitable tidal salt marsh habitat in the BSA. | No effect – no suitable habitat within the BSA. |
| <i>Sorex vagrans halicoetes</i> salt marsh wandering shrew | —/SSC | Mid-elevation salt marsh habitats with dense pickleweed; requires driftwood and other objects for nesting cover | A | No suitable tidal salt marsh habitat in the BSA. | Not applicable. |
| Fish | | | | | |
| <i>Acipenser medirostris</i> green sturgeon | FT/— | Ocean water, bays, and estuaries while not spawning; spawns in the mainstem of freshwater rivers with connections to marine habitat and suitable deep pools | A | No suitable ocean, bay, estuary, river, or deep-pool habitat in the BSA. | No effect – no suitable habitat within the BSA. |
| <i>Hypomesus transpacificus</i> delta smelt | FT/SE | Occurs in estuary habitat in the Delta where fresh and brackish water mix, in the salinity range of 2 to 7 parts per thousand (Moyle 2002) | A | No suitable estuary habitat in the BSA. | No effect – no suitable habitat within the BSA. |
| <i>Oncorhynchus kisutch</i> Coho salmon – central California coast | FE/— | Occurs in coastal streams with water temperatures < 15°C; needs cool, clear water with instream cover; spawns in tributaries to large rivers or streams that are directly connected to the ocean (Moyle 2002) | A | No suitable coastal streams or large rivers that are directly connected to the ocean in the BSA. | No effect – no suitable habitat within the BSA. |
| <i>Oncorhynchus mykiss</i> Central California Coastal steelhead, Central Valley steelhead critical habitat, Central California coastal steelhead | FT/— | An anadromous fish that spawns and spends a portion of its life in inland streams, typically maturing in the open ocean | A | No suitable stream or ocean habitat in the BSA. | No effect – no suitable habitat within the BSA. |
| <i>Oncorhynchus tshawytscha</i> Central Valley Chinook salmon | FT (spring run) /— FE (winter run)/— | An anadromous fish that spawns and spends a portion of its life in inland streams, typically maturing in the open ocean | A | No suitable stream or ocean habitat in the BSA. | No effect – no suitable habitat within the BSA. |

| Common Name Scientific Name | Legal Status (Federal/State /Other) ^a | General Habitat Description | Habitat Present/ Absent | Rationale | Effect finding for Federally Listed Species |
|---|--|--|-------------------------------|---|---|
| <i>Spirinchus thaleichthys</i> longfin smelt | Candidate for federal listing/ST, SSC | Bay, estuary, Humboldt Bay, Gulf of the Farallones, San Francisco Bay, San Pablo Bay, and the Sacramento (from upstream of Rio Vista) and San Joaquin River Delta (from Cache Slough and Medford Island) through Suisun Bay and Suisun Marsh | A | No suitable bay, estuary, gulf, river delta, or marsh habitat in the BSA. | No effect – no suitable habitat within the BSA. |
| <p>Notes:</p> <p>^a Status codes</p> <p>— = no status</p> <p>FE = listed as <i>endangered</i> under the federal Endangered Species Act</p> <p>FT = listed as <i>threatened</i> under the federal Endangered Species Act</p> <p>PD = proposed for delisting under the federal Endangered Species Act</p> <p>SE = listed as <i>endangered</i> under the California Endangered Species Act</p> <p>ST = listed as <i>threatened</i> under the California Endangered Species Act</p> <p>SCT = candidate for listing as <i>threatened</i> under the California Endangered Species Act</p> <p>SSC = California Species of Special Concern</p> <p>FP = California fully protected species</p> <p>WBWG = Western Bat Working Group conservation priority (high or medium)</p> | | | | | |

For the purpose of this NES-MI, special-status species include the following:

- Species listed or proposed for listing as threatened or endangered under the federal ESA (50 CFR 17.11 [listed animals], 50 CFR 17.12 [listed plants], and various notices in the *Federal Register* [FR] [proposed species]).
- Species that are candidates for possible future listing as threatened or endangered under the federal ESA (73 FR 75176, December 10, 2008).
- Species listed or proposed for listing by the state of California as threatened or endangered under CESA (14 California Code of Regulations [CCR] 670.5).
- Species that meet the definitions of rare or endangered under CEQA (State CEQA Guidelines Section 15380).
- Plants listed as rare under CNPPA (CFGF Section 1900 et seq.).
- Plants considered by CNPS to be “rare, threatened, or endangered in California” (2009).
- Plants listed by CNPS as plants about which more information is needed to determine their status and plants of limited distribution, which may be included as special-status species on the basis of local significance or recent biological information.
- Animals designated as California Species of Special Concern by CDFW.
- Animal species that are fully protected in California (CFGF Sections 3511 [birds], 4700 [mammals], 5050 [amphibians and reptiles], and 5515 [fish]).

Special-Status Plant Species

Based on the CNDDDB search results (CNDDDB 2015), the CNPS inventory (CNPS 2015), and the USFWS list (USFWS 2016) for the Project region, it was determined that six special-status plant species have the potential to occur in the Project region (Table 3). Suitable habitat is not present for any of these plant species in the BSA because of the large proportion of the BSA that is developed or landscaped.

Special-Status Wildlife Species

Based on the CNDDDB search results and the USFWS list for the Project region, 27 special-status wildlife species were identified as potentially occurring in the Project region. After completing field surveys and reviewing information on species distribution and habitat requirements, the biologists determined that 26 of the 27 species are not expected to occur in the BSA because it lacks suitable habitat and/or is outside the species’ known range (Table 4). Individual northern harriers (California Species of Special Concern) may occasionally forage over undeveloped portions of the BSA but are not expected to nest due to the lack of habitat (i.e., marsh or grassland with dense ground cover) and high disturbance levels.

Other Protected or Managed Biological Resources

Other protected or managed biological resources include Western Bat Working Group (WBWG) priority bat species and nesting birds.

Western Bat Working Group Priority Species

The WBWG maintains a regional priority matrix for western bat species (WBWG 2015). The matrix is intended to provide states, provinces, federal land management agencies, and interested organizations and individuals with a better understanding of the overall status of individual bat species throughout their western North American ranges. In light of this information, the importance of a single region or multiple regions to the viability and conservation of each species becomes more apparent. The matrix also provides a means for prioritizing and focusing on population monitoring, research, conservation actions, and the efficient use of the limited funding and resources that are currently devoted to bats.

The WBWG matrix indicates that pallid bat is a high-priority species in California. The high-priority designation indicates that the species is imperiled or at high risk of imperilment (WBWG 2015). This bat is also a California Species of Special Concern (see above). The underside of the overpass was inaccessible during ICF's site visits because of the high volume of traffic on US 101, but pallid bat is not expected to occur under the overpass due to the lack of species' incompatibility with urban development (Desert Renewable Energy Conservation Plan 2012, Technology Associates 2009), the species having been extirpated from the Santa Clara Valley floor due to extensive development (D. Johnston, pers. comm.), the urban character of the BSA, and the background level of routine vehicular and human disturbance. Further, there was no observation of bat guano and staining under the overpass during the field survey.

Nesting Birds and Raptors

Native migratory birds and raptors have the potential to nest in trees and shrubs in the BSA. Swallows and black phoebes have the potential to nest under the highways in the BSA. Although these species are not considered special-status wildlife species, their occupied nests and eggs are protected by CFGC Sections 3503 and 3503.5 and the MBTA.

Chapter 4 – Results: Biological Resources, Discussion of Impacts and Mitigation

4.1 Habitats and Natural Communities of Special Concern

Natural communities of special concern are those that are regulated by federal, state, or local laws, or have limited distributions. Examples include natural communities considered highly imperiled by CDFW and tracked in the CNDDDB, jurisdictional waters of the United States and/or state (including wetlands), and riparian habitats.

No natural communities of special concern are identified in the CNDDDB (CDFW 2015) as occurring within the BSA. Northern coastal salt marsh is a natural community of special concern that occurs within the 7.5-minute USGS Mountain View quadrangle CNDDDB search radius, but this community does not occur within the BSA. The only vegetation community identified in the BSA is landscaped vegetation, which is not considered highly imperiled by CDFW.

The Sunnyvale West Channel is a partially concrete-lined flood control channel occurring within the BSA that ultimately connects to the Guadalupe Slough, which flows into the southern portion of San Francisco Bay. Because it has a direct connection with a TNW of the United States (San Francisco Bay), the Sunnyvale West Channel is a non-wetland water of the United States subject to USACE jurisdiction and also is a water of the state subject to San Francisco Bay RWQCB jurisdiction. However, where this feature occurs in the BSA it is culverted underground and thus would not be considered a sensitive natural community.

The Project will not impact any sensitive natural communities and no mitigation would be necessary.

4.2 Special-status Species

As described above, no special-status plant or wildlife species are expected to occur in the BSA due to a lack of soil types or suitable habitat. The Project will not impact any special-status plant or wildlife species.

4.3 Other Protected or Managed Biological Resources

This section includes a description of nesting birds, trees, and invasive plant species present in the BSA.

4.3.1 NESTING BIRDS

As mentioned in Chapter 2, under Regulatory Requirements, nesting birds and raptors are protected by the MBTA and CFGC (Sections 3503 [bird nests], 3503.5 [raptors], 3511 [fully protected bird species], and 3513 [migratory birds]).

The trees and shrubs within the undeveloped portions of the BSA provide suitable nesting substrate for numerous bird species that are protected by the MBTA and CFGC. No active nests were observed during the March 2015 survey, but an inactive cliff swallow (*Petrochelidon*

pyrrhonota) nest was observed under the northern portion of the Mathilda Avenue overpass above US 101. This species could nest under the overpass in the future.

Vegetation clearing, ground disturbance, and construction-generated noise and vibration could result in direct or indirect mortality of nesting birds through crushing, parental abandonment of young, reduced fitness, reduction in number of available prey, and degradation or loss of habitat. Removal of trees or other vegetation could result in the destruction of active bird nests. Birds that nest on existing structures within or near the BSA could be disturbed by the demolition or modification of these structures (particularly the Mathilda Avenue overpass above US 101). As mentioned above, one inactive cliff swallow nest was observed attached to a vertical support column below the Mathilda Avenue overpass above US 101 and the species could nest under the overpass in the future. Implementation of avoidance and minimization measures, described below, would avoid or reduce impacts on nesting migratory birds in the BSA.

Avoidance and Minimization Efforts

To avoid impacts on nesting bird species such as cliff swallow, construction activity within 100 feet of all bridges will be scheduled to avoid the avian nesting season (February 1 through August 31, or earlier than August 31 if surveys determine that swallows have completed nesting for the season). Construction disturbance during the breeding season could result in the incidental loss of eggs or nestlings, either directly through the destruction or disturbance of active nests or indirectly by causing the abandonment of nests. With implementation of avoidance practices for nesting birds, this type of impact would not be considered substantial for either colonial nesters or other bird species that could potentially nest in or adjacent to the Project disturbance area due to the local and regional abundances of these species and/or the low magnitude of the potential impact of the Project to these species. However, the following measures will be implemented to ensure that Project activities comply with the MBTA and California Fish and Game Code.

- **Avoidance of Nesting Bird Season.** To the extent feasible, Project activities should be scheduled outside the avian nesting season to avoid impacts to nesting birds (including raptors) protected under the MBTA and California Fish and Game Code. The nesting season for most birds in Santa Clara County typically extends from February 1 through August 31, although some raptors may nest as early as January 1.
- **Pre-construction/Pre-disturbance Surveys for Nesting Birds.** If it is not possible to schedule Project activities between September 1 and January 1, then pre-construction surveys for nesting birds will be conducted by a qualified biologist to ensure that no nests will be disturbed during Project implementation. These surveys will be conducted no more than 48 hours prior to the initiation of Project activities. During this survey, a qualified biologist will inspect all potential nesting habitats (e.g., trees, shrubs, and overpasses) within 300 feet of impact areas for raptor nests and within 100 feet of impact areas for nests of non-raptors. If an active nest (i.e., a nest with eggs or young, or any completed raptor nest attended by adults) is found sufficiently close to work areas to be disturbed by these activities, the biologist, in consultation with CDFW, will determine the extent of a disturbance-free buffer zone to be established around the nest (typically 300 feet for raptors and 50–100 feet for other species), to ensure that no nests of species protected by the MBTA and California Fish and Game Code will be disturbed during Project implementation.
- **Nest Deterrence.** If Project activities will not be initiated until after the start of the nesting season, potential nesting substrate (e.g., bushes, trees, structures, and other vegetation) that is scheduled to be removed by the Project, if any, may be removed prior to the start of the nesting season (e.g., prior to January 1) to reduce the potential for initiation of nests.

4.3.2 TREES

Approximately 626 trees were identified in the BSA (Table 1). Many of the trees within the BSA meet the size requirements to be considered protected by the City of Sunnyvale, according to Sunnyvale Municipal Code 19.94; however, VTA and Caltrans are not subject to the City's tree ordinance or protection policies.

A conservative estimate of the total number of trees in the BSA (626), of which a lesser number could be affected, has been provided in this NES-MI. Damage to or removal of any trees will be avoided to the maximum extent practicable. The majority of these existing trees will be unaffected by the Project's construction or operation. The intent of the City of Sunnyvale's tree preservation ordinance is to maintain the benefits to the community provided by trees, including keeping public rights-of-way cooler in the summer, providing aesthetic value, and removing air pollutants, to name a few. Damage to and/or removal of trees reduces these benefits to the community. Additionally, trees provide habitat and food sources to local wildlife.

Avoidance and Minimization Efforts

To the maximum extent practicable, damage to or removal of trees will be avoided by the Project. If trees need to be removed or are damaged as a result of the Project, they will be replaced within the Project corridor, to the extent feasible. Native trees with a DBH of less than 12 inches will be replaced at a 2:1 ratio. Native trees with a DBH of 12 inches or more will be replaced at a 3:1 ratio. If urban trees (nonnatives and ornamentals) are replaced with native trees, a reduced mitigation ratio of 1:1 for all trees smaller than 12 inches DBH, and 2:1 for all trees with a DBH of 12 inches or more, will be implemented. These trees will be irrigated and maintained for a period of not less than 3 years. If trees cannot be replaced at the stated ratios within the Project corridor, in-lieu fees will be paid to an appropriate fund so that trees can be planted elsewhere within the City of Sunnyvale limits.

4.4 Invasive Species

As discussed in Chapter 3, the introduction and spread of invasive plants adversely affect natural plant communities by displacing native plant species that provide shelter and forage for wildlife.

Table 2 names 16 invasive plant species identified in the BSA. Infestation of the BSA by these species is confined to the ruderal ground cover of the landscaped vegetation community because the landscaped vegetation is surrounded by development (Figure 2).

The landscaped vegetation is not considered a sensitive natural community and the BSA is entirely within a developed area; therefore, the Project is not likely to contribute to the spread of invasive species to sensitive natural communities in adjacent lands. Further, numerous invasive species already occur within the BSA; therefore, the BSA itself is not as sensitive to the introduction of other invasive species compared with areas that lack invasive species. The Project does have the potential to spread invasive plant species to uninfested areas outside the Project limits if plants removed during construction are not disposed of or transported correctly.

4.4.1 AVOIDANCE AND MINIMIZATION EFFORTS

To minimize introduction and spread of non-native invasive plant species, the following avoidance and minimization efforts will be implemented by the Project:

- Prior to construction, Project disturbance areas infested with invasive plant species will be identified, mapped and cleared of vegetation. All vegetative material will be incinerated off-site or disposed of in a landfill, taking care to prevent any seed dispersal during the process;
- During construction, vehicles and all equipment will be washed (including wheels, undercarriages, and bumpers) before and after entering the Project area. Vehicles will be cleaned at existing construction yards or legally operating car washes. In addition, tools such as chainsaws, hand clippers, pruners, etc., will be washed before and after entering the Project work area; and
- Following Project implementation, areas where vegetation was removed within the BSA will be either hydroseeded with native seed from a local source or planted with landscaping vegetation and properly maintained per Caltrans standards to reduce the risk of non-native invasive species establishment. Native species and/or drought-tolerant plants should be used in landscaping to the extent practicable.

Chapter 5 – Conclusions and Regulatory Determination

5.1 Federal Endangered Species Act Consultation Summary

ICF biologists obtained a USFWS list of threatened and endangered species potentially occurring in the BSA vicinity on January 6, 2016. In addition, ICF queried the CNDBB and CNPS online inventory for special-status plant and wildlife species occurrences in the BSA vicinity, including federally listed species, prior to field surveys. Based on the results of the database query and the results of the surveys, no federally listed species are expected to occur in the BSA due to its location within a dense urban environment and consequent lack of suitable habitat. As such, consultation with the USFWS and/or NMFS pursuant to the ESA is not required.

5.2 Wetland and Non-Wetland Waters Summary

The Sunnyvale West Channel is culverted underground at two locations in the BSA. This feature is identified in the wetlands assessment (Appendix D) as a water of the United States that is subject to USACE jurisdiction (this determination is subject to verification by the USACE). This feature is also assumed to be a water of the state that is subject to jurisdiction by the San Francisco Bay RWQCB. Because the Project will not impact this channel, no federal or state permits are required and no mitigation is necessary. Cumulative impacts to wetland and non-wetland waters within the BSA are not anticipated.

5.3 Invasive Species

The Project has limited potential to spread invasive plant species. Implementation of avoidance and minimization efforts described in Chapter 4 would reduce the introduction and spread of invasive plant species to or from the Project area. Therefore, the Project is ***not expected to result in an increase*** of invasive plant species within and adjacent to the Project's boundaries. Due to the limited potential of invasive plant species to spread within the BSA and adjacent land, cumulative impacts are not likely.

5.4 Other Protected or Managed Biological Resources

5.4.1 NESTING BIRDS

Project activities and the removal of trees or other vegetation could result in direct or indirect impacts on nesting birds through mortality due to nest destruction, parental abandonment of young, reduced fitness, reduction in number of available prey, and degradation or loss of habitat. Implementation of the avoidance and minimization measures described in Chapter 4 would avoid or reduce impacts on nesting birds in the BSA. Thus, the Project is ***not likely to impact*** nesting birds. The BSA is relatively developed, it is subject to routine vehicular and human disturbance, and the majority of trees within it are not native and/or have been planted as landscape cover. Further, implementation of the avoidance and minimization measures described in Chapter 4 would avoid impacts to nesting birds. Similar nesting bird avoidance measures are expected to be implemented by other projects in the surrounding region. For these reasons, the project is not anticipated to have a cumulative impact to nesting birds in the region.

5.4.2 TREES

The Project will avoid damage to and removal of trees to the greatest extent practicable; however, tree trimming and removal may need to occur within the Project limits. No tree removal permit would be required because VTA and Caltrans are not subject to local tree ordinances or tree removal permit requirements. Nonetheless, if trimming or removal of any trees is determined to be necessary to construct the Project, the loss of trees will be mitigated by replacing trees within the Project corridor at ratios described in Chapter 4. Thus, the Project is ***not expected to have substantial impact*** on trees within the BSA. Since, the project is not expected to have a substantial impact on trees in the region, cumulative impacts are not anticipated.

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Memorandum

| | |
|-----------------|---|
| Date: | January 28, 2016 |
| To: | Lani Lee Ho (VTA), Sajeeni DeAlwis-Mima (VTA) |
| Cc: | Tim Lee (WMH), Christine Fukasawa (ICF), Karin Bouler (ICF) |
| From: | Peter Hardie INCE (ICF), Eric Moskus (ICF) |
| Subject: | Mathilda Avenue Improvements at SR-237 and US 101 Project CEQA only Significance Threshold |

Introduction

This memo discusses CEQA noise significance thresholds in the context of the CEQA-only noise study that is being prepared for the Mathilda Avenue Improvements at SR-237 and US 101 Project (Project).

The Protocol dated May 2011 provides direction for how a Noise Study Report (NSR) which is subject to CEQA only (where a Federal Nexus does not trigger the requirements of CFR 772) should be evaluated and presented. The guidance in Protocol states “Under CEQA, a determination must be made as to whether the proposed Project will result in significant adverse environmental effects (i.e., significant environmental impacts). A significant environmental effect under CEQA generally is defined as a substantial or potentially substantial adverse change in the physical environment.” (See Protocol page 37). A more detailed discussion of substantial adverse change will be addressed as follows.

The primary purpose of this memo is to describe the requirement in the Protocol that discuss the identification of a substantial increase (i.e., what noise level increase during the design-year (2040), relative to the existing (2013) [or no-build] condition would signify as a substantial increase).

Background

The Protocol, as discussed above, directs a CEQA-only NSR to identify the relative increase in noise level between the design-year build condition and the existing condition. The Protocol specifically states: “A significant environmental effect under CEQA generally is defined as a substantial or potentially substantial adverse change in the physical environment.” The protocol also states, “Section 15125 of the State CEQA Guidelines states that this environmental setting normally will constitute the baseline physical conditions by which a lead agency determines whether an impact is significant. Because CEQA focuses on comparisons to the existing conditions baseline, Caltrans determines the significance of noise impacts under CEQA based on a comparison of design-year with-Project conditions to the existing

conditions baseline.” (See Protocol page 37). The design-year no-build condition can be used to show the Project-only contribution relative to the design-year build condition in some cases. As the NSR only identifies the relative increase between these time periods, it is not within the purview of the analyst to document a significance determination within the NSR. The significance determination is left to be discussed and determined in the Environmental Document (ED). As such the relative increase must be defined for the purposes of CEQA significance.

The Protocol states, “No single numerical threshold is used on all projects. In the past, Caltrans definition for a substantial increase in noise (defined in the Protocol as a 12 dB increase between existing and design-year with-Project conditions) has been used. This 12 dB increase should not necessarily be used for all projects. There could be cases where an increase less than 12 dB would approach significance (such as a quiet rural environment) or where a 12 dB increase would not necessarily be deemed significant (noisy urban environment.) It is important to note as well that a 3 dBA difference is generally the point at which the human ear will perceive a difference in noise level.”

The absolute future noise level predicted is also a key factor in determining significance. If two people are speaking, 67 dBA is the approximate noise level that would interfere with human speech. Therefore, if the absolute future noise level is less than 67 dBA that may be a factor in determining that the noise impact is less than significant. Lastly, in determining significance under CEQA, it is important to take into account the setting of the impact. According to State CEQA Guidelines, Section 15064(b), an ironclad definition of significant effect is not always possible because the significance of an activity may vary with the setting.” (See Protocol page 38).

Research into the defined significance thresholds for CEQA-only NSR’s identified two other sources: the US 101 Express Lanes Project ED and the City of Sunnyvale’s General Plan. A more detailed discussion of these two documents is provided in the Discussion section, as follows.

Discussion

The Protocol is in essence leaving the CEQA determination open to interpretation. The discussion above refers to a 12 dB increase (design-year build condition relative to the existing condition), which is Caltrans interpretation of a substantial increase to satisfy the requirements of CFR 772. The Protocol also discusses that a 12 dB increase may not be applicable for all situations when judging CEQA significance. The determination of a substantial increase should be judged relative to the environment where the project is taking place. For instance, similar to the FTA Noise and Vibration Manual’s Increase in Cumulative Noise Level (see page 3-6 of the FTA Noise and Vibration Manual [Figure 1 as follows]) when a project area has a generally low ambient noise level, the relative project increase (design-year build condition relative to the existing condition) can be larger. This is shown by in the attached figure where an existing noise exposure of 40 dBA correlates to a project noise exposure increase of 10 dB before a moderate impact has occurred. Comparatively an existing noise exposure of 50 dBA would allow for a 5 dB increase before a moderate impact would occur. As such, a 12 dB increase (the Caltrans threshold for substantial increase for NEPA) may not be appropriate in an urban environment. A more conservative increase (i.e. less than an increase of 12 dB) may be appropriate.

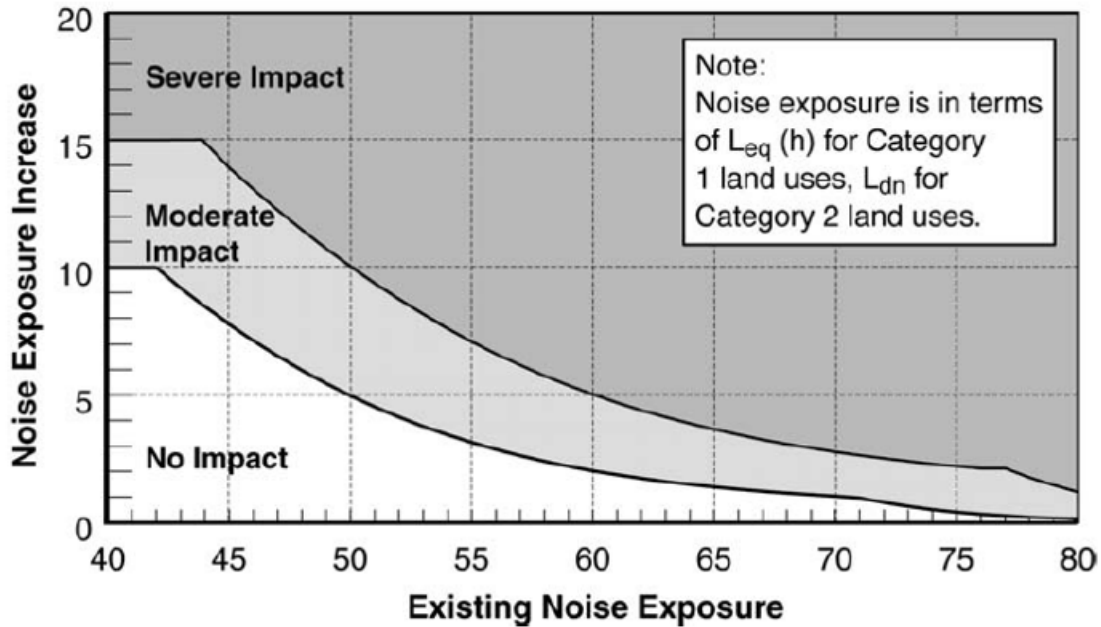


Figure 1. Increase in Cumulative Noise Levels Allowed by Criteria (Land Use Cat. 1 & 2)

Source: FTA Manual, Figure 3-2.

Table 1, attached to this memorandum, shows the preliminary predicted noise increases at 30 modeling locations between the design-year build condition and the existing condition. With inclusion of Alternative 1, the design-year noise levels relative to the existing condition increase no more than 2 dB. With inclusion of Alternative 2, the design-year noise levels relative to the existing condition increase no more than 3 dB. It is important to note that the threshold of perception for noise increases is generally considered 3 dB. It is also important to note, that 5 dB increase in noise levels is considered readily perceptible and that a 10 dB increase is considered a doubling of the loudness of the noise level.

With respect to the responsibility for identifying the threshold by which a substantial increase should be judged, the Protocol states, “The determination of CEQA significance therefore is left to the Project Development Team (PDT) for each project because the team is the most knowledgeable about the specifics of the project area and is in the best position to make the significance determination.”

Other Sources

US-101 Express Lanes Project:

Noise analysis of the US 101 Express Lane Project (on US 101 between Morgan Hill and Palo Alto, crossing through the Project area) was conducted in 2013. Per the November 2014 IS/MND prepared for that project, a 0-3 dbA increase in noise levels was not considered a substantial project related noise level increase. This project's noise impact significance (refer to Section 2.2.7.5 of the IS/MND) was evaluated based on the difference between the existing baseline noise level and the build noise level. The analysis found that the difference ranged from 0-3 dbA, and stated that an increase of 3 dbA is considered to be barely detectable to the human ear. As such, under CEQA it was found that changes in traffic noise from the project were considered to not result in a significant impact.

It should be noted that this project was a joint NEPA/CEQA IS-MND/EA and that Federal Funding was allocated to this project. As such, the noise analysis referred to the FTA Protocol definition of noise impact (an increase of 12 dbA or more), and did not set a separate CEQA-only noise significance threshold.

City of Sunnyvale General Plan:

The City of Sunnyvale's General Plan (refer to page 6-27) discusses a threshold by which to analyze significance:

“Generally, a three dBA Ldn or greater change in noise level is considered “significant” because it can be noticed by the human ear. Most homes will continue to have acceptable noise levels in the future. For individual roadway projects, potential noise impacts are evaluated on a case-by-case basis. Despite the traffic noise, noise levels are considered “normally acceptable” for most homes today and most homes will continue to have normally acceptable noise levels in the future.”

This is the threshold for CEQA significance that would generally be included in a CEQA document with no Caltrans oversight. The caveat that should be pointed out here is that the threshold is established in Ldn. Ldn is a 24 hour metric that establishes “penalties” for noise that is produced during a specific time period, (specifically noise levels between the hours of 10:00 PM and 7:00 AM). The traffic noise model analysis for this Project is analyzed in peak hour ($L_{eq}[1hr]$). These two different metrics are not directly correlative.

Conclusion

In conclusion, the threshold of significance for a substantial increase for the proposed Project should be discussed and identified by the PDT as they are the most knowledgeable about the Project, the relative Project environment, and the overall Project design. The specifics included within this memo should guide the PDT to a decision which will be applicable and defensible for the purposes of analysis of the Mathilda Avenue Improvements at SR-237 and US 101 Project and in the ED.



Table 1 – Preliminary Predicted Traffic Noise Levels

| | Measurement Location | Existing Noise Level $L_{eq}(h)$, dBA | Design-Year 2040 Noise Level without Project, $Leq(h)$, dBA | Design-Year Noise Level with Project (Alt 1), $Leq(h)$, dBA | Design-Year Noise Level with Project (Alt 2), $Leq(h)$, dBA | Design-Year 2040 (Alt 1) Noise Level with Project minus No Project Conditions $Leq(h)$, dBA | Design-Year 2040 (Alt 2) Noise Level with Project minus No Project Conditions $Leq(h)$, dBA | Design-Year 2040 (Alt 1) Noise Level with Project minus Existing Conditions $Leq(h)$, dBA | Design-Year 2040 (Alt 2) Noise Level with Project minus Existing Conditions $Leq(h)$, dBA |
|------|----------------------|--|--|--|--|--|--|--|--|
| M-1 | -- | 73 | 74 | 74 | 74 | 0 | 0 | 1 | 1 |
| M-2 | -- | 66 | 67 | 67 | 67 | 0 | 0 | 1 | 1 |
| M-3 | -- | 63 | 64 | 64 | 64 | 0 | 0 | 1 | 1 |
| M-4 | -- | 67 | 69 | 69 | 69 | 0 | 0 | 2 | 2 |
| M-5 | -- | 63 | 64 | 64 | 64 | 0 | 0 | 1 | 1 |
| M-6 | ST-1 | 71 | 73 | 72 | 72 | -1 | -1 | 1 | 1 |
| M-7 | ST-2 | 66 | 68 | 68 | 68 | 0 | 0 | 2 | 2 |
| M-8 | -- | 59 | 60 | 60 | 60 | 0 | 0 | 1 | 1 |
| M-9 | -- | 56 | 56 | 56 | 56 | 0 | 0 | 0 | 0 |
| M10 | -- | 58 | 59 | 59 | 59 | 0 | 0 | 1 | 1 |
| M-11 | -- | 57 | 58 | 58 | 58 | 0 | 0 | 1 | 1 |
| M-12 | -- | 60 | 61 | 61 | 61 | 0 | 0 | 1 | 1 |
| M-13 | ST-3 | 68 | 69 | 69 | 69 | 0 | 0 | 1 | 1 |
| M-14 | -- | 60 | 61 | 61 | 61 | 0 | 0 | 1 | 1 |
| M-15 | -- | 60 | 61 | 61 | 61 | 0 | 0 | 1 | 1 |
| M-16 | -- | 63 | 64 | 64 | 64 | 0 | 0 | 1 | 1 |
| M-17 | -- | 62 | 64 | 64 | 64 | 0 | 0 | 2 | 2 |
| M-18 | ST-5 | 64 | 65 | 65 | 65 | 0 | 0 | 1 | 1 |
| M-19 | -- | 63 | 64 | 64 | 64 | 0 | 0 | 1 | 1 |
| M-20 | -- | 59 | 61 | 61 | 61 | 0 | 0 | 2 | 2 |

Mathilda Avenue Improvements at SR-237 and US 101 CEQA only NSR

January 28, 2016

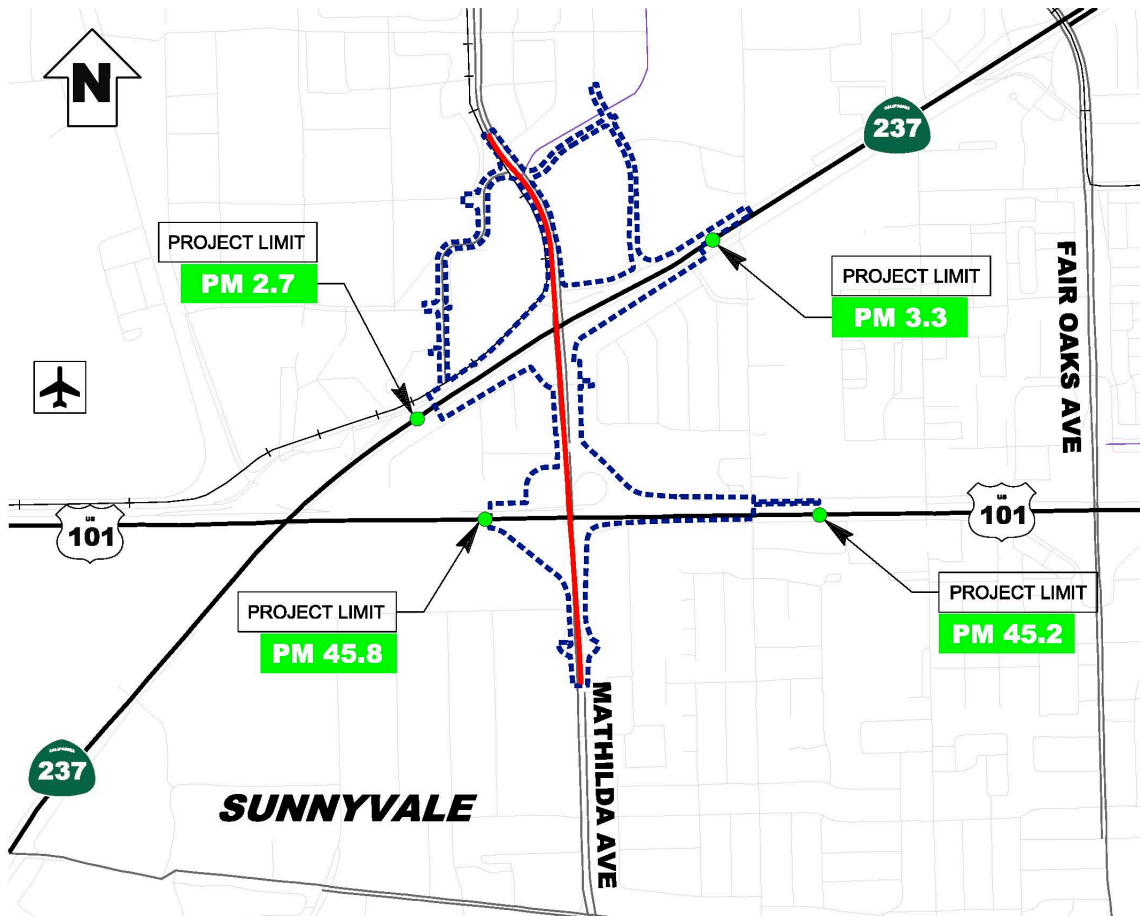
Page 2 of 6

| | Measurement Location | Existing Noise Level $L_{eq}(h)$, dBA | Design-Year 2040 Noise Level without Project, $Leq(h)$, dBA | Design-Year Noise Level with Project (Alt 1), $Leq(h)$, dBA | Design-Year Noise Level with Project (Alt 2), $Leq(h)$, dBA | Design-Year 2040 (Alt 1) Noise Level with Project minus No Project Conditions $Leq(h)$, dBA | Design-Year 2040 (Alt 2) Noise Level with Project minus No Project Conditions $Leq(h)$, dBA | Design-Year 2040 (Alt 1) Noise Level with Project minus Existing Conditions $Leq(h)$, dBA | Design-Year 2040 (Alt 2) Noise Level with Project minus Existing Conditions $Leq(h)$, dBA |
|------|----------------------|--|--|--|--|--|--|--|--|
| M-21 | -- | 67 | 68 | 68 | 68 | 0 | 0 | 1 | 1 |
| M-22 | ST-4 | 65 | 66 | 66 | 66 | 0 | 0 | 1 | 1 |
| M-23 | ST-6 | 64 | 65 | 66 | 65 | 1 | 0 | 2 | 1 |
| M-24 | -- | 68 | 69 | 69 | 69 | 0 | 0 | 1 | 1 |
| M-25 | -- | 65 | 67 | 67 | 67 | 0 | 0 | 2 | 2 |
| M-26 | ST-7 | 66 | 67 | 67 | 67 | 0 | 0 | 1 | 1 |
| M-27 | -- | 67 | 68 | 68 | 68 | 0 | 0 | 1 | 1 |
| M-28 | ST-8 | 68 | 69 | 69 | 69 | 0 | 0 | 1 | 1 |
| M-29 | -- | 60 | 62 | 61 | 61 | -1 | -1 | 1 | 1 |
| M-30 | ST-9 | 68 | 70 | 70 | 71 | 0 | 1 | 2 | 3 |

Paleontological Identification Report

for the

MATHILDA AVENUE IMPROVEMENTS AT SR 237 AND US 101 PROJECT



Prepared for:

Santa Clara Valley Transportation Authority
California Department of Transportation
District 4

Prepared by:

ICF, International

Dated: December 2015

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Paleontological Identification Report

for the

MATHILDA AVENUE IMPROVEMENTS AT SR 237 AND US 101 PROJECT

on Mathilda Avenue from Almanor Avenue to Innovation Way; on SR 237 from 0.3 mile south of US 101/SR 237 Junction to 0.3 mile east of Mathilda Avenue Undercrossing; and on US 101 from 0.5 mile south of Mathilda Avenue to SR 237/US 101/SR 237 Junction in City of Sunnyvale, in Santa Clara County


SCL-237-PM 2.7/3.3; SCL-101-PM 45.2/45.8
EA 04-4H2900/Project ID 0413000204

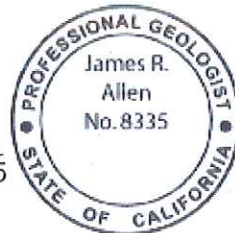
December 2015

U.S. DEPARTMENT OF TRANSPORTATION
STATE OF CALIFORNIA

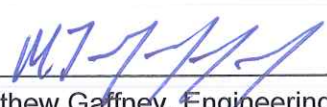
and

Cooperating Agency: Santa Clara Valley Transportation Authority


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Date: 12/23/15

Statement of Compliance: Produced in compliance with California Environmental Quality Act (CEQA) requirements, as appropriate, to meet the level of analysis and documentation that has been determined necessary for this project.

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- 3: DIVERGING DIAMOND INTERCHANGE ILLUSTRATION**
- 4: PROJECT AREA GEOLOGIC MAP**

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1.0 PURPOSE OF STUDY

The purpose of this Paleontological Identification Report (PIR) is to document the presence of paleontological resources within the Mathilda Avenue Improvements at SR 237 and US 101 Project alignment in Santa Clara County, California. The California Department of Transportation (Caltrans) is the lead agency under the California Environmental Quality Act (CEQA).

This PIR was prepared in accordance with the Caltrans Standard Environmental Reference (SER), Volume 1, Chapter 8, *Paleontology* (Caltrans 2014) and follows guidelines set by the Society of Vertebrate Paleontologists, where feasible. The PIR serves as an initial screening to assess whether Project-related ground disturbance would take place in geologic units that have a high potential to contain sensitive paleontological resources.

PIR preparation included a windshield survey and reviews of literature and maps. The literature and maps were used to identify geologic units in the Project area, the potential for those geologic units to contain fossils, and the types of fossils that may be in or adjacent to the Project area. This PIR was prepared by James R. Allen, Professional Geologist (PG) of ICF International with review and final approval by Caltrans.

2.0 PROJECT DESCRIPTION

2.1 Introduction

Caltrans, in cooperation with the Santa Clara Valley Transportation Authority (VTA) and the City of Sunnyvale, is proposing the “Mathilda Avenue Improvements at SR 237 and US 101 Project” (Project) to improve Mathilda Avenue in the City of Sunnyvale from Almanor Avenue to Innovation Way, including on- and off-ramp improvements at the State Route (SR) 237/Mathilda Avenue and U.S. Highway 101 (US 101)/Mathilda Avenue interchanges. On SR 237, the Project limits are from 0.3 miles east of the US 101/SR 237 interchange (post mile [PM] 2.7) to 0.3 miles east of the Mathilda Avenue undercrossing (PM 3.3). On US 101, the Project limits are from 0.5 miles south of Mathilda Avenue overcrossing (PM 45.2) to 0.3 miles south of SR 237/US 101 interchange (PM 45.8). The total length of the Project on Mathilda Avenue is approximately one mile. Figure 1 shows the location of the Project.

2.2 Purpose and Need

The primary purpose of the Project is to improve traffic operations on Mathilda Avenue through the US 101 and SR 237 interchanges. Specifically, the goals and objectives of the Project are to:

- Reduce congestion and improve traffic operations along Mathilda Avenue and at the SR 237/Mathilda Avenue and US 101/Mathilda Avenue interchanges.
- Improve mobility for all travel modes in the area including motor vehicles, transit, bicycles, and pedestrians.
- Provide standard crosswalks and sidewalks along Mathilda Avenue, improving access to local destinations such as Moffett Park, the VTA Light Rail Transit (LRT) stations, and downtown Sunnyvale.

The Project is needed for the following reasons:

- Regional growth and new local development combined with inefficient roadway operations has resulted in substantial traffic congestion on Mathilda Avenue.

- Efficient access for all travel modes into and out of downtown Sunnyvale and development to the north of SR 237 is critical to a healthy and sustainable economy. Congestion on Mathilda Avenue adversely affects the economic vitality of the City of Sunnyvale.

Overall, the Project is needed to address several issues in the Project area including roadway deficiencies, lack of or discontinuous bicycle and pedestrian access, improvement of local roadway and freeway ramp operations, and provision of access to current and future economic development.

2.3 Build Alternatives

The Project alternatives that were developed to meet the purpose and need of the Project include Alternative 1, Alternative 2, and the No-Build Alternative (refer to Figure 2). Under the No-Build Alternative, no changes would be made to the existing local roadways or freeway system within the Project limits. No construction activities would occur, and there would be no change in the operations of the existing facilities.

The design features of the Build Alternatives include reconfiguration of the US 101 and SR 237 interchanges with Mathilda Avenue. The Build Alternatives include design variations for reconfigured roadways and intersections, and construction of new signalized intersections. Proposed improvements included in the Build Alternatives to the south of Ross Drive along Mathilda Avenue and at the US 101 interchange, are identical. These improvements include new bicycle and pedestrian facilities, utility relocations, new storm water treatment facilities, new safety lighting, ramp metering modifications, modification of overhead signage, and a new retaining wall. Unique improvements of the Build Alternatives occur to the north of Ross Drive on Mathilda Avenue and primarily include improvements related to construction of a diverging diamond interchange (DDI)¹ under Build Alternative 2 (Figure 3).

Roadway Improvements

The Build Alternatives would consist of the following roadway improvements:

- Provide three continuous through lanes in each direction of Mathilda Avenue;
- Remove northbound US 101 loop off-ramp and shift traffic to northbound US 101 diagonal off-ramp;
- Realign and widen northbound ramps and signalize ramp intersection with Mathilda Avenue, and construct left-turn lane on southbound Mathilda Avenue to access northbound US 101 loop on-ramp;
- Realign southbound US 101 off-ramp and loop on-ramp and signalize ramp intersection with Mathilda Avenue;
- Modify Mathilda Avenue / Ross Drive signal intersection;
- Close Moffett Park Drive between Bordeaux Drive and Mathilda Avenue, replace with a Class I bikeway (as described below), and shift traffic to Bordeaux Drive and Innovation Way;²

¹ A diverging diamond interchange (DDI), also called a double crossover diamond interchange (DCD) is a type of diamond interchange where traffic briefly crosses over to the left (opposite) side of the roadway, guided by traffic signals at each crossover. This allows vehicles to turn left onto freeway on-ramps without stopping and without conflicting with through traffic. The signals at ramp terminal intersections can be operated with two signal phases (phases when a traffic signal allows for traffic at an intersection to cycle through specific movements for each direction) instead of three.

² Innovation Way would be extended from Mathilda Avenue to Bordeaux Drive by the Moffett Place development project.

- Remove westbound SR 237 ramp signal intersection. Realign westbound SR 237 off-ramp opposite Moffett Park Drive and modify signal intersection;
- Build Alternative 1 would modify westbound SR 237 ramps to provide a diamond configuration (see Figure 2a); and
- Build Alternative 2 would modify Mathilda Avenue and SR 237 ramps to provide a diverging diamond configuration (see Figure 2b and Figure 3). Eastbound Moffett Park Drive between Innovation Way and Mathilda Way would be diverted to Innovation Way to access Mathilda Avenue.

Bicycle and Pedestrian Facilities

Enhanced bicycle and pedestrian facilities would be provided. Bicycle improvements on Mathilda Avenue would consider both Class II and Class III bikeways³, based on available pavement widths within the project limits, and would connect to the existing Class III bikeway north of Innovation Way and Class I bikeway on the Sunnyvale West Channel. Bicycle improvements on Moffett Park Drive would consist of a Class I bikeway between Bordeaux Drive and Mathilda Avenue. Between Mathilda Avenue and Innovation Way, Class II and Class III bikeways would be considered based on available pavement widths within the project limits. A continuous sidewalk would be provided on the east side of Mathilda Avenue within the project limits with crosswalks, curb ramps, and pedestrian countdown signals at each intersection. The new crosswalks at the reconfigured ramp intersections would be signalized.

3.0 REGULATORY SETTING

Paleontology is a natural science focused on the study of ancient animal and plant life as it is preserved in the geologic record as fossils.

3.1 State Regulations and Policies

Under California law, paleontological resources are protected by CEQA.

California Environmental Quality Act

CEQA, Chapter 1, Section 21002 states:

It is the policy of the state that public agencies should not approve projects as proposed if there are feasible alternatives or feasible mitigation measures available which would substantially lessen the significant environmental effects of such projects, and that the procedures required are intended to assist public agencies in systematically identifying both the significant effects of proposed projects and the feasible alternatives or feasible mitigation measures which will avoid or substantially lessen such significant effects.

The CEQA Guidelines (Article 1, Section 15002(a)(3)) state that CEQA is intended to:

Prevent significant, avoidable damage to the environment by requiring changes in projects through the use of alternatives or mitigation measures when the governmental agency finds the changes to be feasible.

³ Class I bikeway is a bicycle path. Class II bikeway is a bicycle lane. Class III bikeway is bicycle route [Source: Highway Design Manual Index 1002.1]

Public Resources Code Section 5097.5

Public Resources Code Section 5097.5 prohibits “knowing and willful” excavation, removal, destruction, injury, and defacement of paleontological features on public lands, except where the agency with jurisdiction has granted express permission. For the purposes of this code section, public lands are defined as including lands under state, county, city, district, or public authority jurisdiction, or the jurisdiction of a public corporation.

California Code of Regulations

California Code of Regulations (Title 14, Division 3, Chapter 1, *Natural Resources, Department of Parks and Recreation*) addresses paleontological resources. Specifically, Section 4307, subdivision a, prohibits destruction, disturbance, mutilation, and removal of geological materials and paleontological features on State Parks lands, although rockhounding is permitted. This is defined in Section 4301 as recreational gathering of naturally occurring “stones and minerals” found on the undisturbed ground surface and panning for gold in natural stream gravels, and presumably includes recreational collection of some types of fossil materials.

4.0 METHODOLOGY

Evaluation of paleontological resources along the Project alignment was based on review of the following materials.

- Project information, including the Project area of potential effect (APE) map and information on anticipated depth of excavation.
- Geologic mapping by Wentworth et al. (1999) and Brabb et al. (1998).
- Information on lithology and fossil content from the published geologic and paleontological literature.
- A search of the University of California, Berkeley Museum of Paleontology’s (UCMP’s) online collections database.
- Air photo inspection of the Project alignment.
- Windshield survey on September 6, 2015.
- Familiarity with area geology and fossil resources from prior projects evaluation of paleontological sensitivity/potential following the methods outlined in Chapter 8 of the Caltrans SER.

The SER, Chapter 8, briefly equates the significance of paleontological resources with their scientific importance, and recognizes that both concepts apply to individual fossil species, to fossil assemblages, and to geologic units as a whole. The SER offers two definitions of *significance*.

- **National** – This definition reflects language in legislation establishing the National Natural Landmark Program. The general definition used in the SER, Chapter 8 refers to “an area of national significance (as defined under 36 CFR 62) that contains an outstanding example of fossil evidence of the development of life on earth.”
- **Scientific** – The SER recognizes that definitions of scientific significance may vary between agencies and between practitioners, but follows the usage established in work done for a landmark Caltrans project in the Cajon Pass area by identifying the term *significant* as generally applying to identified sites and deposits containing fossils (individual or assemblages) that are unique or unusual, diagnostically or stratigraphically important, and add to the existing body of stratigraphic, taxonomic, or regional knowledge. Particular importance is attached to undisturbed fossil materials found in their original context, because of their potential utility in stratigraphy, tectonics, geomorphology, paleoclimatology, and to the understanding of relationships between

aquatic and terrestrial species and “evolution in general.” Because of their rarity, terrestrial vertebrate fossils are generally assigned greater significance. As applied to the entirety of a geologic unit, the SER’s definition of *significance* reflects the “research potential” of the unit’s known or suspected fossil content. Because actual fossil content is typically not known until after grading/excavation begins, decisions about the management of paleontological resources must be based on assessed potential rather than known content. Potential is evaluated based on the criteria presented below in Table 1. Consistent with prevailing practice in paleontological resources management (Society of Vertebrate Paleontology Conformable Impact Mitigation Guidelines Committee 1995, revised 2010), the Caltrans process considers a geologic unit that contains significant paleontological resources anywhere within its geographic extent as having the same high potential everywhere it occurs.

Caltrans uses the tripartite scale shown in Table 1 to rank the sensitivity or potential for a particular geologic unit to contain paleontological resources.

Table 1 – Caltrans Definitions of Paleontological Potential

| Caltrans Sensitivity Designation | Characteristics of Geologic Units in this Category |
|---|--|
| High Potential (High Sensitivity) | <p>This category consists of rock units known to contain significant vertebrate, invertebrate, or plant fossils anywhere within their geographic extent, including sedimentary rock units that are suitable for the preservation of fossils, as well as some volcanic and low-grade metamorphic rock units.</p> <p>This category includes rock units with the potential to contain:</p> <ul style="list-style-type: none"> ▪ Abundant vertebrate fossils; ▪ A few significant vertebrate, invertebrate, or plant fossils that may provide new and significant taxonomic, phylogenetic, ecological, and/or stratigraphic data; ▪ Areas that may contain datable organic remains older than Recent; ▪ Areas that may contain unique new vertebrate deposits, traces, and/or trackways; and ▪ Fossiliferous deposits with very limited geographic extent or an uncommon origin (e.g., tar pits and cave deposits). |
| Low Potential (Low Sensitivity) | <p>This category includes sedimentary rock units* that</p> <ul style="list-style-type: none"> ▪ Are potentially fossiliferous, but have not yielded significant fossils in the past; ▪ Have not yet yielded fossils, but have the potential to contain fossil remains; or ▪ Contain common and/or widespread invertebrate fossils of species whose taxonomy, phylogeny, and ecology are well understood. <p><i>*Note that sedimentary rocks expected to contain vertebrate fossils are considered highly sensitive, because vertebrates are generally rare and found in more localized strata.</i></p> |
| No Potential (No Sensitivity) | <p>This category includes rock units of intrusive igneous origin, most extrusive igneous rocks, and moderate- to high-grade metamorphic rocks.</p> |

Source: California Department of Transportation 2014 (Accessible: <http://www.dot.ca.gov/ser/vol1/sec3/physical/Ch08Paleo/chap08paleo.htm>)

5.0 GEOLOGICAL SETTING

The Project alignment is located in the northern Santa Clara Valley, in the California Coast Ranges geomorphic province of northern California. The Coast Ranges are characterized by a sub-parallel series of rugged, northwest-trending mountain ranges and valleys reflecting relatively young uplift associated with the active Pacific–North American plate boundary system (Norris and Webb, 1990; Atwater, 1988; Buising and Walker, 1995; Wakabayashi, 1999; Allen, 2003). The Santa Clara Valley lies between two of these ranges – the Santa Cruz Mountains and the Diablo Range – and is widely considered to represent the onland continuation of the same topographic depression that contains San Francisco Bay (Sedlock, 1995; Iwamura, 1995). The Bay Block is bounded on the west by a complex zone of reverse and dextral faults generally aligned with the Santa Cruz Mountains range front and including the Monte Vista, Berrocal, Shannon, Sargent, and Carnadero faults; and on the east by the dominantly dextral strike-slip southern Hayward and Calaveras faults and related structures (Helley and Wesling 1990, Wagner et al. 1990, Dibblee 2006).

The Project alignment follows the western margin of the Santa Clara Valley within the San Francisco Bay structural block (Buising and Walker, 1995; Wakabayashi, 1999; Allen, 2003), in the central portion of the Coast Ranges geomorphic province of California. Geologically, the project area is underlain by alluvial and fluvial deposits consisting of clay, silt, sand, and gravel. These deposits range in age from Holocene Alluvium and Pleistocene Older Alluvium to the Pliocene–Pleistocene Santa Clara Formation. Holocene deposits conceal Pleistocene deposits at depth. These deposits, both Holocene and Pleistocene, contain paleontological resources. Geologic mapping indicates that the Project is underlain by Holocene alluvium (Graymer et al., 2006) with an average thickness of about 55 feet (Helley, E.J., 1990).

6.0 STUDY RESULTS

The results of the literature and map review of geologic units in the vicinity of the Project are described in this section.

As shown in Figure 4, Project Area Geologic Map, the Project alignment is entirely situated on sediments of Holocene age alluvial fan deposits, fine facies (Qhff) (Geology, Knudsen et al 2006). The windshield survey on September 6, 2015 resulted in no observation of any outcrops within the Project area; therefore, visual inspection of outcroppings was not possible. Holocene strata are underlain at varying unknown depths by older sedimentary materials, including predominantly alluvial strata of Pleistocene age, underlain in turn by the older Santa Clara Formation and its regional equivalents, which presumably rest on bedrock at depth (Iwamura 1995, Stanley et al. 2002). All of these units consist of varying proportions of clay, silt, sand, and gravel. In general, deposits are coarser near the range fronts and along former stream channels, with finer grained materials accumulated in overbank, floodplain, and basin settings on the valley floor (Helley and Wesling 1990, Wentworth et al. 1999, Brabb et al. 2000). Deposits are generally fine toward the Bay margin (California Department of Water Resources 1967).

6.1 Paleontological Sensitivity

This section discusses the paleontological sensitivity of the Holocene deposits within the Project area, shown in Figure 4. These resources may be encountered by deep excavations and boring or auger activities. The data is derived from an on-line University of California Museum of Paleontology search on September 7, 2015; and reviews at the U.S. Geological Survey and San Jose State Martin Luther King Jr., Library on September 8 and 9, 2015.

Fossils that have been recovered in Holocene deposits of the Santa Clara Formation were actually found to be of the Pleistocene-age, and, therefore, there was a clear miss-mapping of the area previously

(University of California Museum of Paleontology 2005). These fossils are: Rancholabrean (early Pleistocene) Columbian mammoth (*Mammuthus columbi*), pollen, fresh water snails (associated with Qpa or the Santa Clara Formation). Other fossils found in Qpa or Santa Clara Formation, which underlie the Holocene deposits, are: bison (*Bison latifrons* and *Bison* sp.) and mammoth of an unidentified species (*Mammuthus* sp.), freshwater mollusc fossils (Brabb et al. 2000), fern *Pteris calabazensis*, alder (*Alnus merriami*), sarvisberry, (*Amelanchier* sp.), incense cedar (*Calocedrus* sp.), buckthorn (*Ceanothus chaneyi*), mountain-mahogany (*Cercocarpus cuneatus*), pine (*Pinus* sp.), chokecherry (*Prunus merriami*), oak (*Quercus hannibali*) and currant (*Ribes stanfordianum*). Invertebrates include gastropods, *Fluminicola sanmateoensis* and *Parapholix durhami*. Vertebrates include horses (*Equus* spp.); and bison (*Bison latifrons*), bony fish, and unidentified mammalian remains of Pleistocene age.

Quaternary Holocene Alluvial Fan Deposits, Fine Facies

Quaternary Holocene Alluvial Fan Deposits, Fine Facies (Qhff) are recognized by the United States Department of the Interior and the United States Geological Survey as being of recent to less than 11,800 years old (Geology, Knudsen et al 2006). Recent sedimentary deposits, such as those of Holocene age, are generally considered too young geologically to contain significant paleontological resources. Therefore, the Holocene deposits encompassing the Project area have a low potential to contain significant paleontological resources.

7.0 SUMMARY

The Project is situated on Holocene surficial deposits that are typically associated with non-fossil-bearing material due to age. Because of their relative rarity, and their potential to provide geochronologic information, vertebrate fossils are considered significant wherever they occur (Society of Vertebrate Paleontology Conformable Impact Mitigation Guidelines Committee 1995), and the Santa Clara Valley area is no exception. Vertebrate materials in Holocene-mapped strata of the Santa Clara Valley are of particular interest and significance because, to date, the only vertebrate find documented from these units is the mammoth, which, as discussed above, is not actually of Holocene age; additional finds would have the potential to further clarify the stratigraphic and chronologic questions raised by the mammoth find. Although invertebrate and plant fossils are often considered less inherently significant than vertebrate remains (e.g., Society of Vertebrate Paleontology Conformable Impact Mitigation Guidelines Committee 1995, revised 2010), in this context, we also consider invertebrate and plant materials in Holocene-identified strata as potentially significant and are of particular interest because of their potential to provide additional geochronologic information bearing on the accuracy of age attributions in published geologic mapping.

The Project would not involve deep construction excavation into the native Holocene deposits for either Build Alternative. The No Build Alternative, likewise, would have no effect or negative impacts to paleontological resources. The majority of Project work, and all Project staging, would occur within the area already disturbed and consists largely of changing existing lanes and flows of traffic. The Project focuses on minor modifications and improvements requiring minimal and superficial ground disturbance. Project activities would, therefore, have little to no potential to encounter or impact paleontological resources.

7.1 Recommendations

No further paleontological study for the Project is necessary, as impacts to non-renewable paleontological resources are lacking for this Project.

8.0 PREPARER

This report was prepared by James R. Allen, Master of Science (CA-PG-8355). Mr. Allen has over 17 years of private, State, and Federal professional project experience in Paleontological Resources Management, laboratory work, geotechnical, environmental science and geology, coupled with groundwater studies, monitoring, and sampling. Mr. Allen has three years of experience conducting USGS laboratory work (grain size analysis, moisture content, stream gaging), and 14 years of private sector geotechnical work (core logging, mapping, groundwater studies), mapping geologic quadrangles for the California Geological Survey, fault trenching/core/soil logging, and environmental hazardous material clean-up work. In addition, Mr. Allen has teaching experience at San Jose State and San Francisco State universities. His experience includes extensive field work of mapping, sampling and locating, report writing, project management, managing work crews in the field for paleontology, hazardous material site remediation projects, geotechnical residential and commercial, general geological investigations, CEQA-NEPA compliance report writing for protected paleontological, biological, and archeological resources, soil and rock core/hallow-stem auger logging, cone penetration test observation, construction observation, foundation inspections, dam, bridge and tunnel geotechnical investigations, landslide mapping and repair observation and project management work. He conducted geologic mapping for the California Geological Survey as well as for private sector projects, paleoseismic trenching on numerous Bay Area faults, test-pit logging, extensive soil and core logging, groundwater sampling, site characterization, resources assessments, sensitivity reporting, and information searches. In addition, he is experienced in laboratory work processing sand, soil, and rock sampling, provided petrographic thin section analysis reports, soil density testing and compaction lab and field analysis on numerous projects, sample excavation and preparation, and monitoring and mitigation. He has authored and co-authored dozens of professional and research publications focused on the seismic activity, paleontology, and geological background of California.

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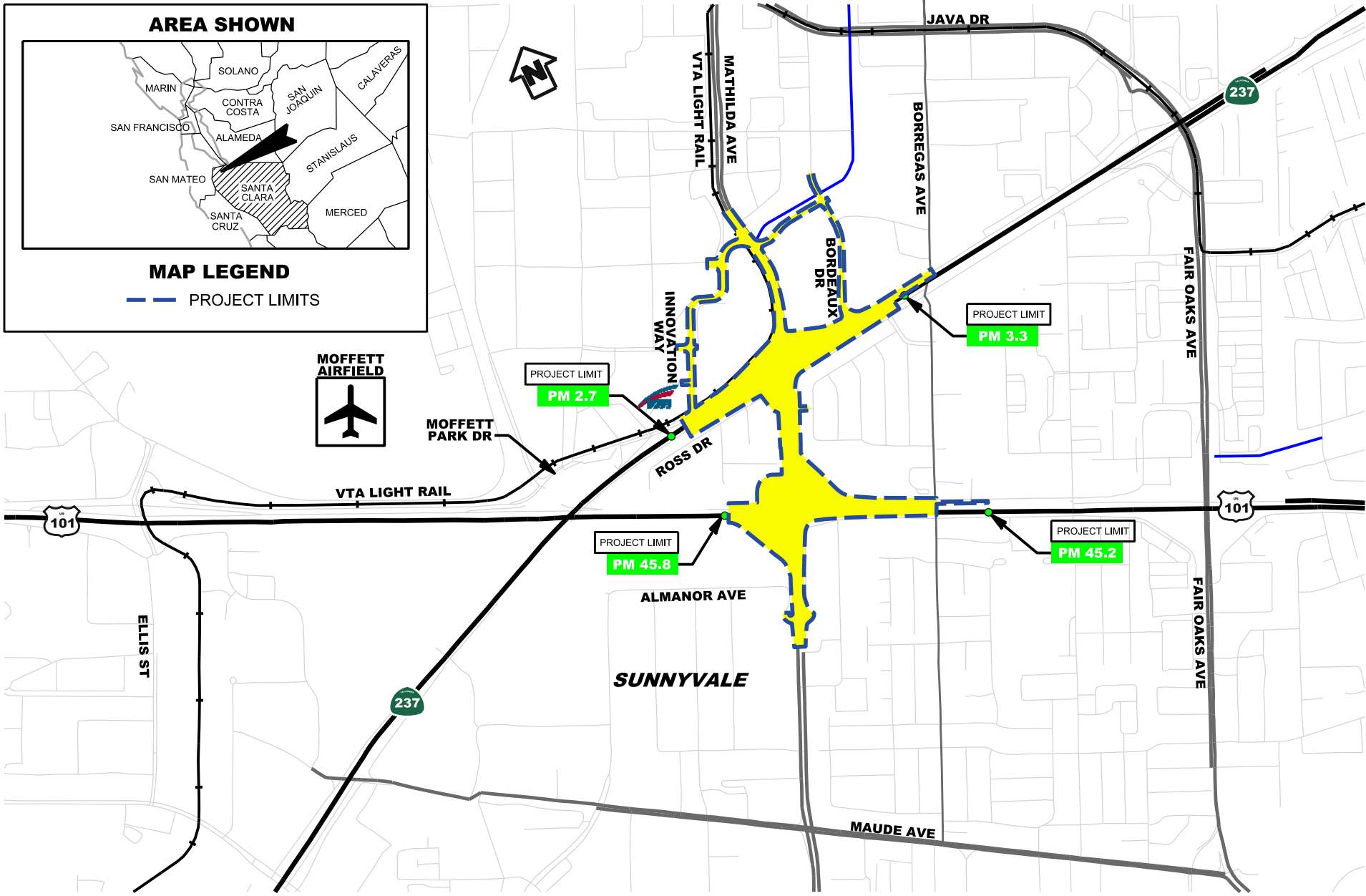
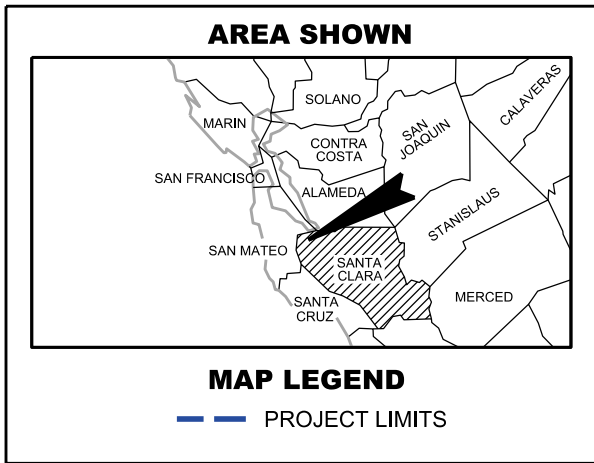
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Figures

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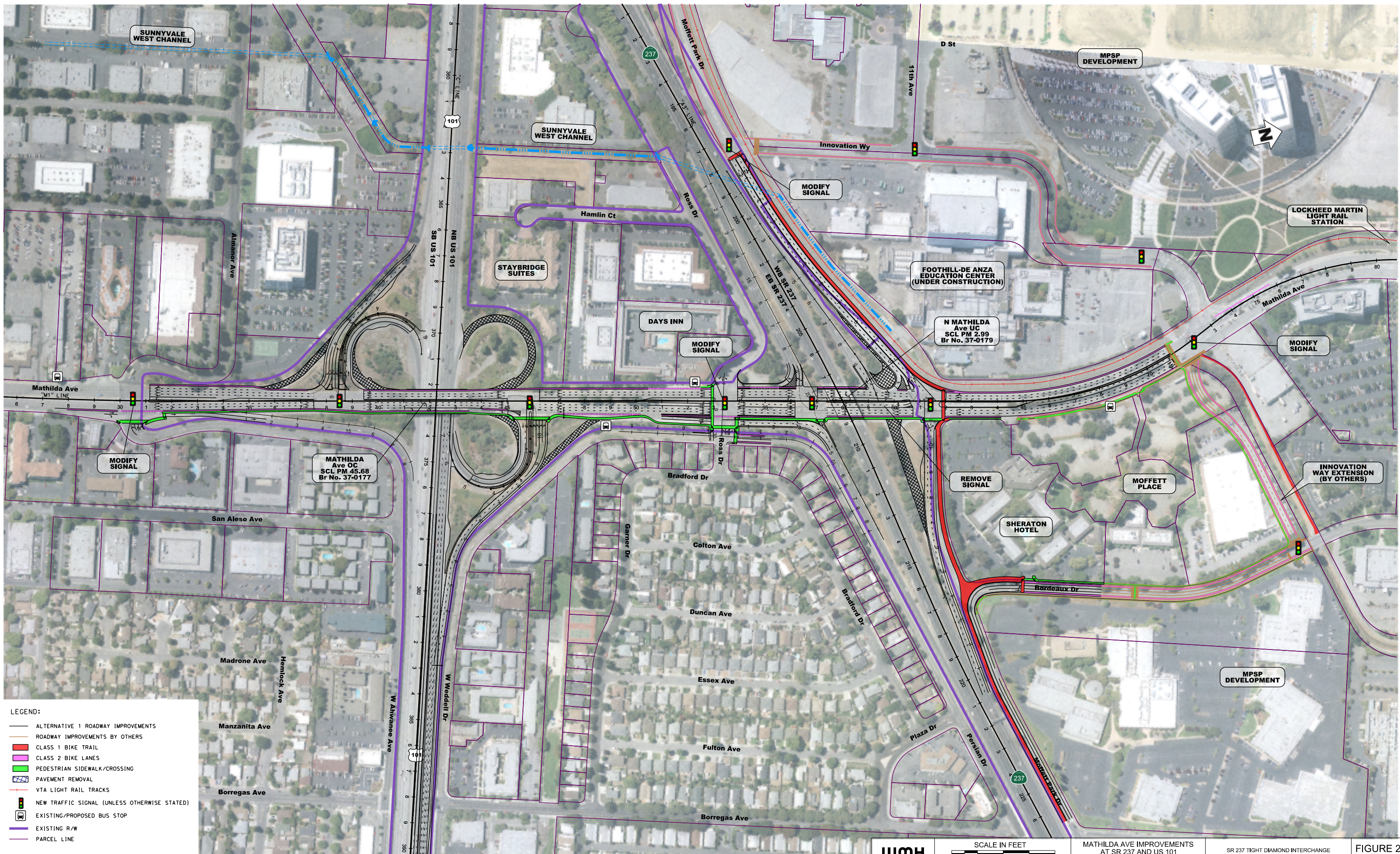


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WMH

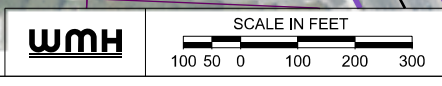
Mathilda Avenue Improvement at SR 237 and US 101

PROJECT LOCATION MAP

Figure
1



- LEGEND:**
- ALTERNATIVE 1 ROADWAY IMPROVEMENTS
 - ROADWAY IMPROVEMENTS BY OTHERS
 - CLASS 1 BIKE TRAIL
 - CLASS 2 BIKE LANES
 - PEDESTRIAN SIDEWALK/CROSSING
 - PAVEMENT REMOVAL
 - VTA LIGHT RAIL TRACKS
 - 🚦 NEW TRAFFIC SIGNAL (UNLESS OTHERWISE STATED)
 - 🚌 EXISTING/PROPOSED BUS STOP
 - EXISTING R/W
 - PARCEL LINE

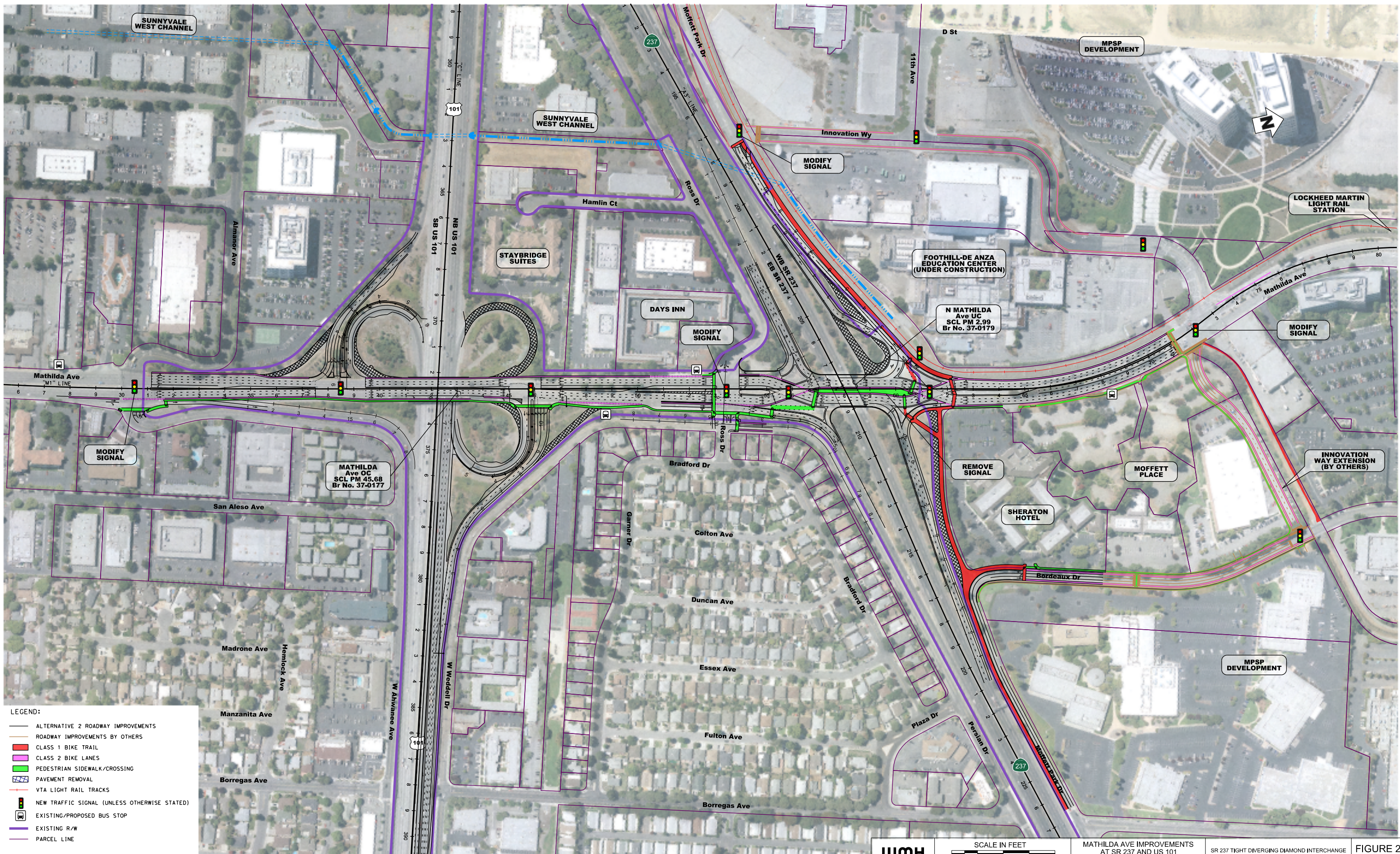


MATHILDA AVE IMPROVEMENTS
AT SR 237 AND US 101
SCL 237 - PM 2,7/3,3
SCL 101 - PM 45,4/45,8

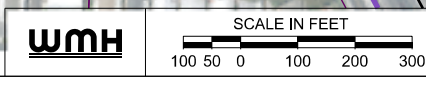
SR 237 TIGHT DIAMOND INTERCHANGE
AND US 101 FULL PAR-CLO INTERCHANGE

FIGURE 2a
NOV 2015

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PLN



- LEGEND:**
- ALTERNATIVE 2 ROADWAY IMPROVEMENTS
 - ROADWAY IMPROVEMENTS BY OTHERS
 - CLASS 1 BIKE TRAIL
 - CLASS 2 BIKE LANES
 - PEDESTRIAN SIDEWALK/CROSSING
 - PAVEMENT REMOVAL
 - VTA LIGHT RAIL TRACKS
 - 🚦 NEW TRAFFIC SIGNAL (UNLESS OTHERWISE STATED)
 - 🚌 EXISTING/PROPOSED BUS STOP
 - EXISTING R/W
 - PARCEL LINE

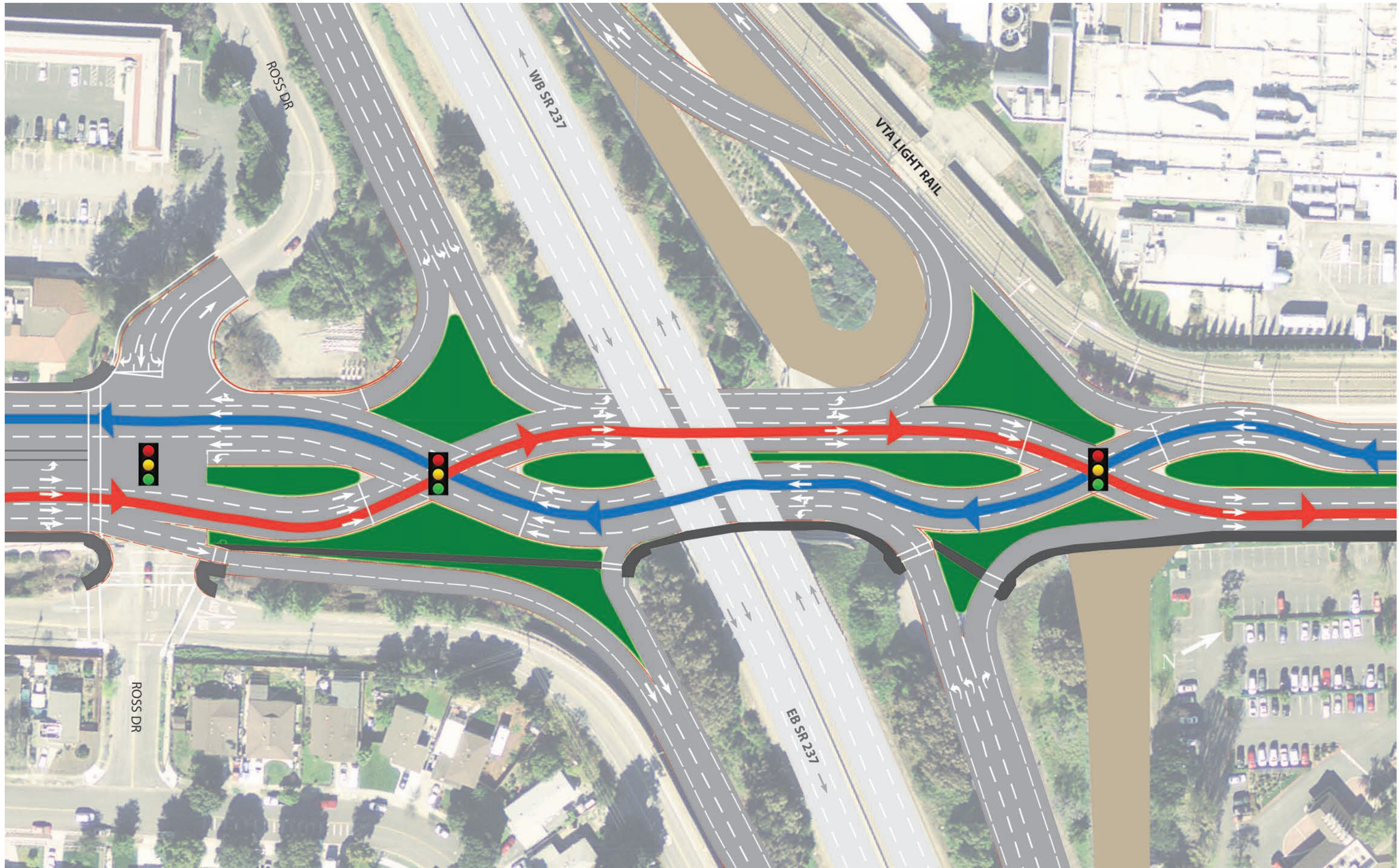


MATHILDA AVE IMPROVEMENTS
AT SR 237 AND US 101
SCL 237 - PM 2,7/3,3
SCL 101 - PM 45,4/45,8

SR 237 TIGHT DIVERGING DIAMOND INTERCHANGE
AND US 101 FULL PAR-CLO INTERCHANGE

FIGURE 2b
NOV 2015

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NOT TO SCALE

MATHILDA AVE IMPROVEMENTS
 AT SR 237 AND US 101
 SCL 237 - PM 2.7/3.3
 SCL 101 - PM 4.5/4.5.8

DIVERGING DIAMOND
 INTERCHANGE (DDI) ILLUSTRATION

FIGURE 3
 JULY 2015

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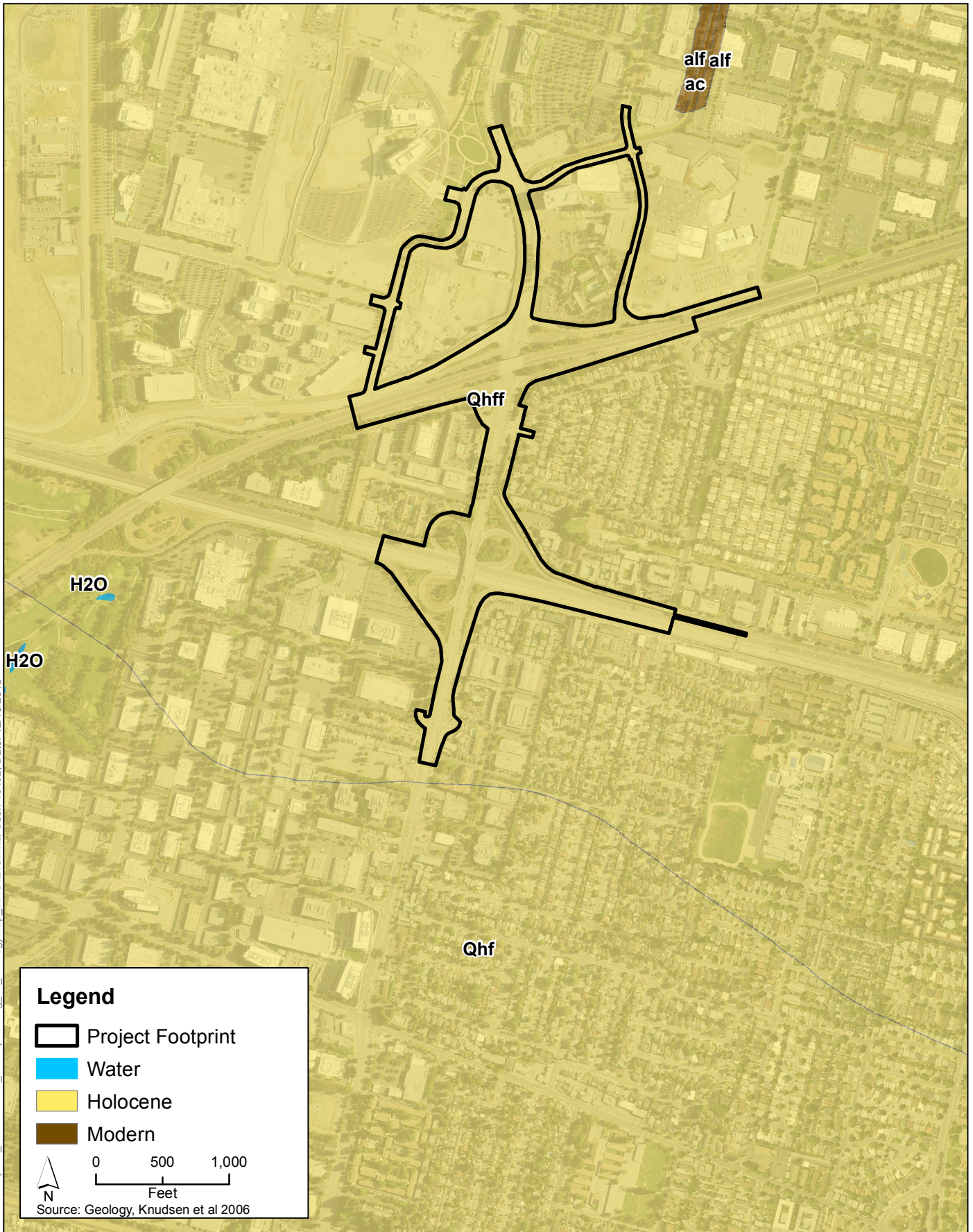
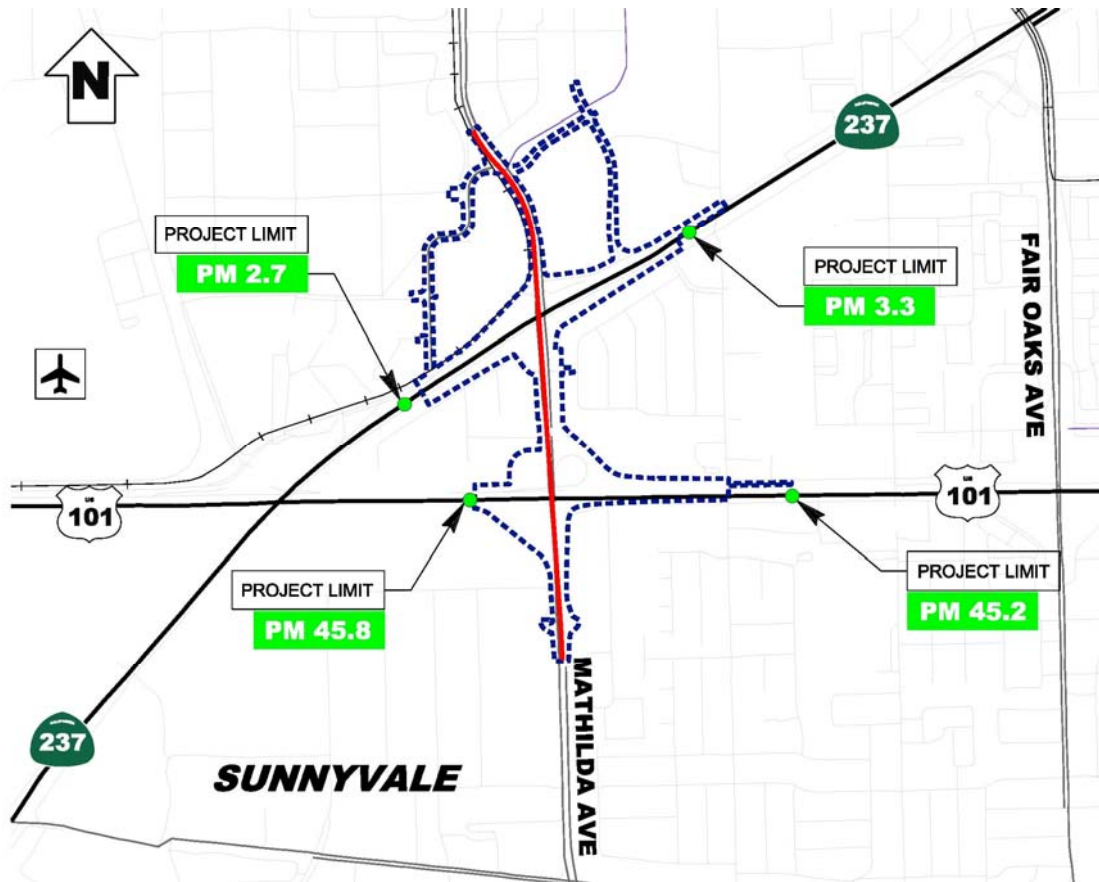


Figure 4
Project Area Geologic Map
Mathilda Avenue Improvements at SR 237 and US 101 Project

PRELIMINARY GEOLOGICAL ASSESSMENT

for the

MATHILDA AVENUE IMPROVEMENTS AT SR 237 AND US 101 PROJECT



Prepared for:

Santa Clara Valley Transportation Authority
California Department of Transportation
District 4

Prepared by:
BASELINE Environmental Consulting

Dated: October 2015

For individuals with sensory disabilities, this document is available in Braille, in large print, on audiocassette, or on computer disk. To obtain a copy in one of these alternative formats, please write to Caltrans, Attn: Chris Riden, Office of Geotechnical Design – West , 111 Grand Avenue, Oakland, CA 94623-0660; or call (510) 622-8757 (voice); or use the California Relay Service TTY number, (800) 735-2929.

PRELIMINARY GEOLOGICAL ASSESSMENT

for the

MATHILDA AVENUE IMPROVEMENTS AT SR 237 AND US 101 PROJECT
on Mathilda Avenue from Almanor Avenue to Innovation Way; on SR 237 from 0.3 mile south of US 101/SR 237 Junction to 0.3 mile east of Mathilda Avenue Undercrossing; and on US 101 from 0.5 mile south of Mathilda Avenue to SR 237/US 101/SR 237 Junction in City of Sunnyvale, in Santa Clara County

SCL-237-PM 2.7/3.3; SCL-101-PM 45.2/45.8
EA 04-4H2900/Project ID 0413000204

October 2015

U.S. DEPARTMENT OF TRANSPORTATION
STATE OF CALIFORNIA

and

Cooperating Agency: Santa Clara Valley Transportation Authority

Prepared By:  Date: 12/21/2015

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California Department of Transportation, District 4

Statement of Compliance: Produced in compliance with National Environmental Policy Act (NEPA) and California Environmental Quality Act (CEQA) requirements, as appropriate, to meet the level of analysis and documentation that has been determined necessary for this Project.

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PRELIMINARY GEOLOGICAL ASSESSMENT FOR THE MATHILDA AVENUE IMPROVEMENTS AT SR 237 AND US 101 PROJECT

EXECUTIVE SUMMARY

BASELINE Environmental Consulting (“BASELINE”) conducted this Preliminary Geological Assessment for the “Mathilda Avenue Improvements at SR 237 and US 101 Project” (Project). The Project proposes to improve Mathilda Avenue in the City of Sunnyvale from Almanor Avenue to Innovation Way, including on- and off-ramp improvements at the State Route 237/Mathilda Avenue and U.S. Highway 101/Mathilda Avenue interchanges (Figure 1). Two Build Alternatives, Build Alternative 1 and Build Alternative 2, are being considered for the Project (Figures 2a and 2b). Project improvements for both Build Alternatives would include reconfiguration of existing roadways and intersections, new bicycle and pedestrian facilities, utility relocations, new stormwater treatment facilities, new safety lighting, ramp metering modifications, modification of overhead signage, and a new retaining wall.

The purpose of this Preliminary Geological Assessment was to describe existing geological, seismic, and mineral resource conditions in the Project vicinity, evaluate related hazards that could impact proposed construction activities and/or operations, and provide preliminary recommendations for mitigation. As summarized in Matrix 1, below, the potentially significant Project impacts identified in the assessment were associated with soil erosion, expansive soils, corrosive soils, seismic shaking, and liquefaction; the impacts apply to both of the Build Alternatives. These hazards could affect the structural integrity of Project structures, such as new pavement, retaining walls, overhead sign foundations, and utility relocations, as well as traffic operations.

MATRIX 1: Summary of Impacts for each Build Alternative

| Impact | Build Alternatives | |
|-----------------------|--------------------|---|
| | 1 | 2 |
| Soil Erosion | X | X |
| Expansive Soils | X | X |
| Corrosive Soils | X | X |
| Surface Fault Rupture | | |
| Seismic Shaking | X | X |
| Seismic Liquefaction | X | X |
| Seismic Landslides | | |
| Mineral Resources | | |

Note: X = impact

Once a preferred Build Alternative has been chosen, BASELINE recommends performing a site-specific geotechnical investigation to evaluate geologic and seismic hazards identified in this report and to provide detailed design measures that comply with Caltrans' standards for construction. In addition, development and implementation of Best Management Practices during construction and operation is recommended to minimize soil erosion in accordance with National Pollutant Discharge Elimination System permits.

PRELIMINARY GEOLOGICAL ASSESSMENT FOR THE MATHILDA AVENUE IMPROVEMENTS AT SR 237 AND US 101 PROJECT

1. INTRODUCTION

The California Department of Transportation (Caltrans), in cooperation with the Santa Clara Valley Transportation Authority (VTA) and the City of Sunnyvale, is proposing the “Mathilda Avenue Improvements at SR 237 and US 101 Project” (Project) to improve Mathilda Avenue in the City of Sunnyvale from Almanor Avenue to Innovation Way, including on- and off-ramp improvements at the State Route (SR) 237/Mathilda Avenue and U.S. Highway 101 (US 101)/Mathilda Avenue interchanges. On SR 237, the Project limits are from 0.3 miles east of the US 101/SR 237 interchange (post mile [PM] 2.7) to 0.3 miles east of the Mathilda Avenue undercrossing (PM 3.3). On US 101, the Project limits are from 0.5 miles south of Mathilda Avenue overcrossing (PM 45.2) to 0.3 miles south of SR 237/US 101 interchange (PM 45.8). The total length of the Project on Mathilda Avenue is approximately 1 mile. Figure 1 shows the location of the Project.

The purpose of this Preliminary Geological Assessment was to document existing geological, seismic, and mineral resource conditions in the Project vicinity, evaluate related hazards that could impact proposed construction activities and/or operations, and provide preliminary recommendations for mitigation. This assessment was prepared by BASELINE Environmental Consulting with review and approval by Caltrans.

2. PROJECT DESCRIPTION

This section describes the purpose and scope of the proposed Project.

2.1 Purpose and Need

The primary purpose of the Project is to improve traffic operations on Mathilda Avenue through the US 101 and SR 237 interchanges. Specifically, the goals and objectives of the Project are to:

- Reduce congestion and improve traffic operations along Mathilda Avenue and at the SR 237/Mathilda Avenue and US 101/Mathilda Avenue interchanges.
- Improve mobility for all travel modes in the area including motor vehicles, transit, bicycles, and pedestrians.
- Provide standard crosswalks and sidewalks along Mathilda Avenue, improving access to local destinations such as Moffett Park, the VTA Light Rail Transit (LRT) stations, and downtown Sunnyvale.

The Project is needed for the following reasons:

- Regional growth and new local development combined with inefficient roadway operations has resulted in substantial traffic congestion on Mathilda Avenue.
- Efficient access for all travel modes into and out of downtown Sunnyvale and development to the north of SR 237 is critical to a healthy and sustainable economy. Congestion on Mathilda Avenue adversely affects the economic vitality of the City of Sunnyvale.

Overall, the Project is needed to address several issues in the Project area including roadway deficiencies, lack of or discontinuous bicycle and pedestrian access, improvement of local roadway and freeway ramp operations, and provision of access to current and future economic development.

2.2 Project Description and Alternatives

The Project alternatives that were developed to meet the purpose and need of the Project include Alternative 1 (Figure 2a), Alternative 2 (Figure 2b), and the No-Build Alternative. Under the No-Build Alternative, no changes would be made to the existing local roadways or freeway system within the Project limits. No construction activities would occur, and there would be no change in the operations of the existing facilities.

The design features of the two Build Alternatives include reconfiguration of the US 101 and SR 237 interchanges with Mathilda Avenue. The Build Alternatives include design variations for reconfigured roadways and intersections, and construction of new signalized intersections. Proposed improvements included in the Build Alternatives south of Ross Drive on Mathilda Avenue and at the US 101 interchange, are identical. This includes new bicycle and pedestrian facilities, utility relocations, new storm water treatment facilities, new safety lighting, ramp metering modifications, modification of overhead signage, and a new retaining wall. Unique improvements, north of Ross Drive on Mathilda Avenue, primarily include improvements related to construction of a diverging diamond interchange¹ under Build Alternative 2 (Figure 3).

2.2.1 Roadway Improvements

The Build Alternatives would consist of the following roadway improvements:

- Provide three continuous through lanes in each direction of Mathilda Avenue.
- Remove northbound US 101 loop off-ramp and shift traffic to northbound US 101 diagonal off-ramp.

¹ A diverging diamond interchange, also called a double crossover diamond interchange, is a type of diamond interchange where traffic briefly crosses over to the left (opposite) side of the roadway, guided by traffic signals at each crossover. This allows vehicles to turn left onto freeway on-ramps without stopping and without conflicting with through traffic. The signals at ramp terminal intersections can be operated with two signal phases (a signal phase allows for traffic at an intersection to cycle through specific movements for each direction) instead of three.

- Realign and widen northbound ramps and signalize ramp intersection with Mathilda Avenue, and construct left-turn lane on southbound Mathilda Avenue to access northbound US 101 loop on-ramp.
- Realign southbound US 101 off-ramp and loop on-ramp and signalize ramp intersection with Mathilda Avenue.
- Modify Mathilda Avenue / Ross Drive signal intersection.
- Close Moffett Park Drive between Bordeaux Drive and Mathilda Avenue, replace with a Class I bikeway (as described below), and shift traffic to Bordeaux Drive and Innovation Way.²
- Remove westbound SR 237 ramp signal intersection. Realign westbound SR 237 off-ramp opposite Moffett Park Drive and modify signal intersection.
- Build Alternative 1 would modify westbound SR 237 ramps to provide a diamond configuration (see Figure 2a).
- Build Alternative 2 would modify Mathilda Avenue and SR 237 ramps to provide a diverging diamond configuration (see Figure 2b and Figure 3). Eastbound Moffett Park Drive between Innovation Way and Mathilda Way would be diverted to Innovation Way to access Mathilda Avenue.

2.2.2 Bicycle and Pedestrian Facilities

Enhanced bicycle and pedestrian facilities would be provided. Bicycle improvements on Mathilda Avenue would consider both Class II and Class III bikeways³, based on available pavement widths within the project limits, and would connect to the existing Class III bikeway north of Innovation Way and Class I bikeway on the Sunnyvale West Channel. Bicycle improvements on Moffett Park Drive would consist of a Class I bikeway between Bordeaux Drive and Mathilda Avenue. Between Mathilda Avenue and Innovation Way, Class II and Class III bikeways would be considered based on available pavement widths within the project limits. A continuous sidewalk would be provided on the east side of Mathilda Avenue within the project limits with crosswalks, curb ramps, and pedestrian countdown signals at each intersection. The new crosswalks at the reconfigured ramp intersections would be signalized.

3. METHODOLOGY

As shown in Figure 1, the limits of the Project site include all areas that could potentially be disturbed during construction of the proposed improvements. BASELINE performed this assessment in accordance Chapter 7 of the Caltrans *Environmental Handbook* (Caltrans, 2015a) to support the preliminary engineering and environmental review of the Project. The scope of services for this Preliminary Geological Assessment included review of documents, databases, maps, and geospatial data from Caltrans, the United States Geological Survey (USGS), the United States Department of Agriculture (USDA), and the California Geological Survey (CGS) to

² Innovation Way would be extended from Mathilda Avenue to Bordeaux Drive by the Moffett Place development project.

³ Class I bikeway is a bicycle path. Class II bikeway is a bicycle lane. Class III bikeway is bicycle route [Source: Highway Design Manual Index 1002.1]

describe existing conditions and identify known or potential hazards in the Project vicinity. These hazards were then evaluated to determine potential impacts related to each Build Alternative. Preliminary mitigation measures were then formulated for the Build Alternatives.

4. EXISTING CONDITIONS AND HAZARDS

This section describes the physical setting, geologic hazards, seismic hazards, and mineral resources in the Project vicinity.

4.1 Physical Setting

The Project site is located in the Coast Ranges Geomorphic Province of northern California. The regional structure of the Coast Ranges consists of northwest-trending folds and faults associated with the San Andreas Fault Zone. As a result, northwest-trending ranges of low mountains and intervening valleys dominate this region. The elevation profile of the Project site is relatively flat and varies from about 20 to 40 feet (NAVD 88) along Mathilda Avenue (USGS, 2015) (Figure 4). Geologic mapping indicates that the Project is generally underlain by Holocene alluvium (Graymer et al., 2006) with an average thickness of about 55 feet (Helley, E.J., 1990).

The Bay Area has a Mediterranean climate characterized by wet winters and dry summers. The annual average rainfall reported at the San Jose International Airport approximately 5 miles southeast of the Project is about 12 inches (Western Regional Climate Center, 2015). The Project site is located in the Santa Clara Valley that drains north toward the San Francisco Bay. The Project crosses one waterway, Sunnyvale West Channel, near the intersection of Moffett Park Drive and Innovation Way and the intersection of Mathilda Avenue and Innovation Way. The Sunnyvale West Channel generally drains north (Figure 4), eventually discharging into the San Francisco Bay.

Ambient groundwater level data were reviewed from the State Water Resources Control Board's (2015) *GeoTracker* database for monitoring wells at two leaking underground storage tank sites near the Project: the Texaco site at 724 Mathilda Avenue and the Professional Center site at 102 Persian Drive. Depth to groundwater generally ranges from about 7 to 15 feet below ground surface and groundwater generally flows to the north-northeast at both of the sites. Based on the regional topography and previously measured groundwater levels, groundwater is expected to flow to the north-northeast across the Project site.

4.2 Geologic Hazards

Soil survey data was reviewed from the USDA, Natural Resources Conservation Service (NRCS), to identify and evaluate existing soil conditions and geologic hazards in the Project vicinity. The entire Project site is underlain by Urbanland-Hangerone complex, which is a combination of native alluvium, disturbed soils, and imported fill materials. Descriptions of the soil features (e.g., thickness, permeability, and corrosion potential) are included in Appendix A. Potential

geologic hazards of concern include soil erosion, expansion, and corrosion. Soil survey information related to geologic hazards are discussed further, below.

4.2.1 Soil Erosion Hazards

Erosion is the detachment, movement, and redistribution of soil particles by forces of water, wind, and/or gravity. On the Project site, erosion from rain and stormwater runoff are the dominant natural erosion processes. The rate of soil erosion during a rain event is a function of the slope, vegetative cover, and soil properties. The primary soil properties that influence the erodibility of a soil are texture, structure, organic matter content, and permeability. The collective influence of these soil properties on the erodibility of a soil is described by the soil-erodibility factor (K) (USDA, 1997).

Soils with K factors between about 0.25 and 0.4 are moderately susceptible to water erosion and K factors greater than 0.4 are highly susceptible to water erosion (Institute of Water Research, Michigan State University, 2002). The Hangerone component of soils on the Project site have properties that are moderately susceptible to water erosion with K factors as high as 0.37 (USDA NRCS, 2015). The extent of fill materials on the Project site and their susceptibility to water erosion has not been evaluated. The overall susceptibility of soils to erosion often increases during excavation and grading activities as vegetative cover is removed and/or local gradients and slope lengths are increased.

4.2.2 Expansive Soil Hazards

Expansive soils are characterized by the potential for shrinking and swelling as the moisture content of the soil decreases and increases, respectively. Shrink-swell potential is influenced by the amount and type of clay minerals present and can be measured by the percent change of the soil volume, which is known as the “linear extensibility.” Linear extensibility values ranging from about 6 to 9 percent have a high expansion potential and values exceeding 9 percent have a very high expansion potential. Soils mapped within 45 inches below ground surface on the Project site have high to very high expansion potentials with liner extensibility values ranging from 6 to 12 percent (USDA NRCS, 2015).

4.2.3 Corrosive Soil Hazards

Uncoated subsurface steel and concrete structures are susceptible to corrosion based on the moisture content, texture, acidity, electrical conductivity, and sulfate and sodium content of the soil. Soils mapped on the Project site have a high potential to corrode uncoated steel and a moderate potential to corrode concrete (USDA NRCS, 2015).

4.3 Seismic Hazards

The Project site is located in the San Francisco Bay Area, which includes numerous active faults identified by the CGS under the Alquist-Priolo Earthquake Fault Zoning Act. Caltrans defines a fault as “active” if it has ruptured in the late-Quaternary (the last 750,000 years). This definition is broader than that used by CGS, which defines an active fault as one that has ruptured in the

Holocene (the last 11,000 years). Potential seismic hazards associated with active faults include surface fault rupture, seismic shaking, liquefaction, and landslides.

According to the current *Caltrans Fault Database* (Caltrans, 2012a), the closest active faults to the Project site are the Cascade and Silver Creek faults located about 3.9 miles southwest and 4.5 miles northeast of the Project site, respectively (Figure 5). Since these faults are considered active by Caltrans, they are further evaluated in this assessment; however, it should be noted CGS has not documented evidence of movement within the last 750,000 years along these faults (Jennings and Bryant, 2010). Other active faults identified in the *Caltrans Fault Database* that are located within 10 miles of the Project site include the Monte Vista-Shannon, San Andreas, and Hayward faults (Figure 5).

4.3.1 Surface Fault Rupture Hazards

Surface rupture occurs when the ground surface is broken due to fault movement during an earthquake. The location of surface rupture generally occurs along an existing (usually active) fault trace. As described in Caltrans guidelines (Caltrans, 2007a), areas susceptible to surface fault rupture are delineated by the CGS Alquist-Priolo Earthquake Fault Zones and/or are located near fault traces shown on the *1996 Caltrans California Seismic Hazard Map* (which is now superseded by the *Caltrans Deterministic PGA Map* [Caltrans, 2007b]). The CGS Alquist-Priolo Earthquake Fault Zones have up to about a ¼-mile buffer around the surface traces of faults that have been active within Holocene time (the last 11,000 years). The *Caltrans Deterministic PGA Map* contains less detail than the mapped CGS Alquist-Priolo Earthquake Fault Zones, but includes traces of faults that have been active since the late-Quaternary time (the last 750,000 years) and are capable of producing an earthquake with a moment magnitude⁴ of 6.0 or greater. As shown on Figure 5, the closest active fault to the Project site is the Cascade fault located about 3.9 miles southwest of the Project.

4.3.2 Seismic Ground Shaking Hazards

Seismic ground shaking generally refers to all aspects of motion of the earth's surface resulting from an earthquake, and is normally the major cause of damage in seismic events. The extent of ground shaking is controlled by the magnitude and intensity of the earthquake, distance from the epicenter, and local geologic conditions. The magnitude of a seismic event is a measure of the energy released by an earthquake; it is assessed by seismographs that measure the amplitude of seismic waves. The intensity of an earthquake is a subjective measure of the perceptible effects of a seismic event at a given point. The Modified Mercalli Intensity scale (MMI) is the most commonly used scale to measure the subjective effects of earthquake intensity in values ranging from I to XII. Intensity can also be quantitatively measured using strong motion seismographs that record the peak ground acceleration (PGA) in terms of percent of acceleration force of gravity (%g). Descriptions of the MMI scale and PGA equivalents are summarized in Table 1.

⁴ The amount of energy that is released during an earthquake.

According to the current *Caltrans Fault Database* (Caltrans, 2012), the maximum moment magnitude (M_{Max}) for the largest reasonable earthquake expected along active faults within about 10 miles of the Project site ranges from 6.4 to 8.0 (Table 2). BASELINE used *Caltrans ARS Online V2.3.06* (Caltrans, 2015b) to estimate preliminary PGA values at the center of the Project site associated with the M_{Max} earthquake from nearby active faults. Since the Project site is located on Holocene alluvium, preliminary PGA values were estimated by BASELINE assuming near surface soils with an average shear wave velocity of 270 meters per second. As summarized in Table 2, the preliminary PGA estimated at the center of the Project site for the M_{Max} earthquake along active faults within 10 miles of the Project site ranged from 56 to 72%g, which can result in severe to violent ground shaking.

4.3.3 Seismic Liquefaction Hazards

Liquefaction is the temporary transformation of loose, saturated, granular sediments to a fluid-like state as a result of seismic ground shaking. In the process, the soil undergoes transient loss of strength, which commonly causes ground displacement such as sand boils, settlement, and lateral spreading. CGS has developed Seismic Hazard Zone Maps that delineate areas susceptible to liquefaction that require additional investigation to determine the extent and magnitude of potential ground failure. According to CGS (2006), the Project site is located within a Seismic Hazard Zone for liquefaction.

4.3.4 Seismic Landslide Hazards

Landslides can occur as either rapid movement of large masses of soil or imperceptibly slow movement of soils on slopes. The primary factors influencing the stability of a slope are the nature of the underlying soil or bedrock and the geometry of the slope (height and steepness). Landslides are generally triggered by rainfall, excavation, or seismic activities. The CGS Seismic Hazard Zone Maps delineate areas susceptible to seismically-induced landslides that require additional investigation to determine the extent and magnitude of potential ground failure. According to CGS (2006), the Project site is not located within a Seismic Hazard Zone for seismically-induced landslides.

4.4 Mineral Resource Hazards

In compliance with the Surface Mining and Reclamation Act, CGS has designated mineral resources in areas within California subject to irreversible land uses that would preclude mineral extraction. Land has been classified by the State Geologist into Mineral Resource Zones (MRZs) based on geologic and economic factors. The MRZs include classifications for construction materials, industrial and chemical mineral materials, metallic and rare minerals, and non-fluid mineral fuels. The mapping of MRZs is intended to help identify and preserve significant mineral deposits for future use. The entire Project site is classified as MRZ-1 (Kohler-Antablin, 1996), which indicates that significant mineral deposits are not likely present (Figure 6).

The California Department of Conservation, Division of Oil, Gas, and Geothermal Resources (DOGGR) regulates oil, gas, and geothermal drilling activities and assists in locating and

reviewing the status of wells located near or beneath proposed improvements. The closest DOGGR well is mapped about 12 miles northeast of the Project site (Figure 6). No oil, gas, or geothermal wells were mapped on or adjacent to the Project site (DOGGR, 2015).

5. EVALUATION OF IMPACTS

This section evaluates the potential impacts of geologic and seismic hazards, as well as mineral resources, associated with both construction and operation of the Build Alternatives. As summarized in Matrix 1, below, there are no impacts specific to one of the individual Build Alternatives.

MATRIX 1: Summary of Impacts for each Build Alternative

| Impact | Build Alternatives | |
|-----------------------|--------------------|---|
| | 1 | 2 |
| Soil Erosion | X | X |
| Expansive Soils | X | X |
| Corrosive Soils | X | X |
| Surface Fault Rupture | | |
| Seismic Shaking | X | X |
| Seismic Liquefaction | X | X |
| Seismic Landslides | | |
| Mineral Resources | | |

Note: X = impact

5.1 Geologic Impacts

5.1.1 *Soil Erosion Impacts*

Soils mapped on the Project site have properties that are moderately susceptible to water erosion. Project construction activities, such as grading and excavation, could significantly impact the stability of existing soils and increase the overall potential for soil erosion across the Project site. During Project construction, erosion could cause significant impacts related to sedimentation in storm drains, loss of top soils, gullies on slopes, and undermining of engineered fills beneath foundations or roadways. Long-term significant impacts to the Project could include undercutting of roadways by uncontrolled stormwater runoff.

5.1.2 *Expansive Soil Impacts*

Soils mapped within 45 inches of the ground surface on the Project site have a high to very high expansion potential. Project structures (e.g., new pavement and retaining walls) and utilities built in expansive soils could be significantly impacted by seasonal shrink-swell effects.

5.1.3 Corrosive Soil Impacts

Soils mapped on the Project site have a high potential to corrode uncoated steel and a moderate potential to corrode concrete. Corrosive soils could significantly impact Project structures (e.g., retaining walls) and underground utilities containing steel that are not properly protected.

5.2 Seismic Impacts

1.1.1 Surface Fault Rupture Impacts

The Project site is not located within a mapped Alquist-Priolo Earthquake Fault Zone and is not near an active fault trace shown on the *Caltrans Deterministic PGA Map* (Figure 5); therefore, impacts from surface fault rupture would not be expected on the Project site.

5.2.1 Seismic Ground Shaking Impacts

Based on estimates of preliminary PGA values associated with M_{Max} earthquakes along nearby active faults (Table 2), the Project site could experience severe to violent ground shaking (VIII to IX on the MMI scale). Significant seismic shaking damages could include rupturing of underground pipelines, and cracking and distortion of pavement, walls, and foundations. These potential impacts are present under existing conditions; however, new pavement, retaining walls, and foundations for overhead signs proposed under the Project could significantly increase the risk of structural damage if not properly designed.

5.2.2 Seismic Liquefaction Impacts

The Project site is located within a Seismic Hazard Zone for liquefaction. Potential liquefaction could result in surface impacts to the Project site (e.g., sand boils, settlement, or lateral spreading). Such impacts could affect the structural integrity of roadways and bridges and damage underground utilities. These potential impacts are present under existing conditions; however, new Project construction could significantly increase the risk of structural damage if not properly designed.

5.2.3 Seismic Landslide Impacts

The Project site is not located within a Seismic Hazard Zone for seismically-induced landslides; therefore, landslides would not be expected to impact the Project site.

5.3 Mineral Resource Impacts

Significant mineral resources (including oil, gas, or geothermal) have not been mapped on or adjacent to the Project site. Therefore, the Project would not be expected to impact existing or potential mineral resources.

6. MITIGATION OF IMPACTS

This section presents preliminary recommendations to mitigate all identified impacts related to geologic and seismic hazards to levels equal to or better than existing conditions.

6.1 Mitigation of Geologic Hazards

During subsequent engineering phases for the chosen Build Alternative, a geotechnical investigation should be performed by a professional engineer or geologist to document and further evaluate potential soil expansion and corrosion hazards near proposed improvements (e.g., retaining walls). Based on the findings of the investigation, specific recommendations that comply with Caltrans' standards for construction should be made for the Project design.

Construction, operation, and maintenance of the chosen Build Alternative should implement erosion and sediment control measures in accordance with the *National Pollutant Discharge Elimination System* permits.

6.2 Mitigation of Seismic Hazards

During subsequent engineering phases for the chosen Build Alternative, a geotechnical investigation should be performed by a professional engineer or geologist to document and further evaluate liquefaction and seismic shaking hazards near proposed improvements (e.g., retaining walls). Based on findings of the investigation, specific recommendations that comply with Caltrans' standards for construction should be made for the Project design.

7. CONCLUSIONS

Geologic and seismic hazards that could impact or be impacted by construction and operation of the Build Alternatives include soil erosion, expansive soils, corrosive soils, seismic ground shaking, and liquefaction. These hazards could affect the structural integrity of Project structures, such as new pavement, new retaining walls, and potential utility relocations, as well as traffic operations. A site-specific geotechnical investigation is recommended to document and evaluate geologic and seismic hazards identified in this report and to provide detailed design measures for the Project design of the chosen Build Alternative that complies with Caltrans' standards for construction. In addition, development and implementation of BMPs during construction and operation are recommended to minimize soil erosion.

8. QUALIFICATIONS OF PREPARERS

This report was prepared by Patrick Sutton from BASELINE under the direct supervision of a professional geologist, Bruce Abelli-Amen. Patrick Sutton is an environmental engineer with over 10 years of experience preparing technical reports related to geology, hydrogeology, air quality, and hazardous materials. Bruce Abelli-Amen is a principal of BASELINE and has over 25 years of experience preparing and reviewing technical documents. The resumes for BASELINE staff are included Appendix B.

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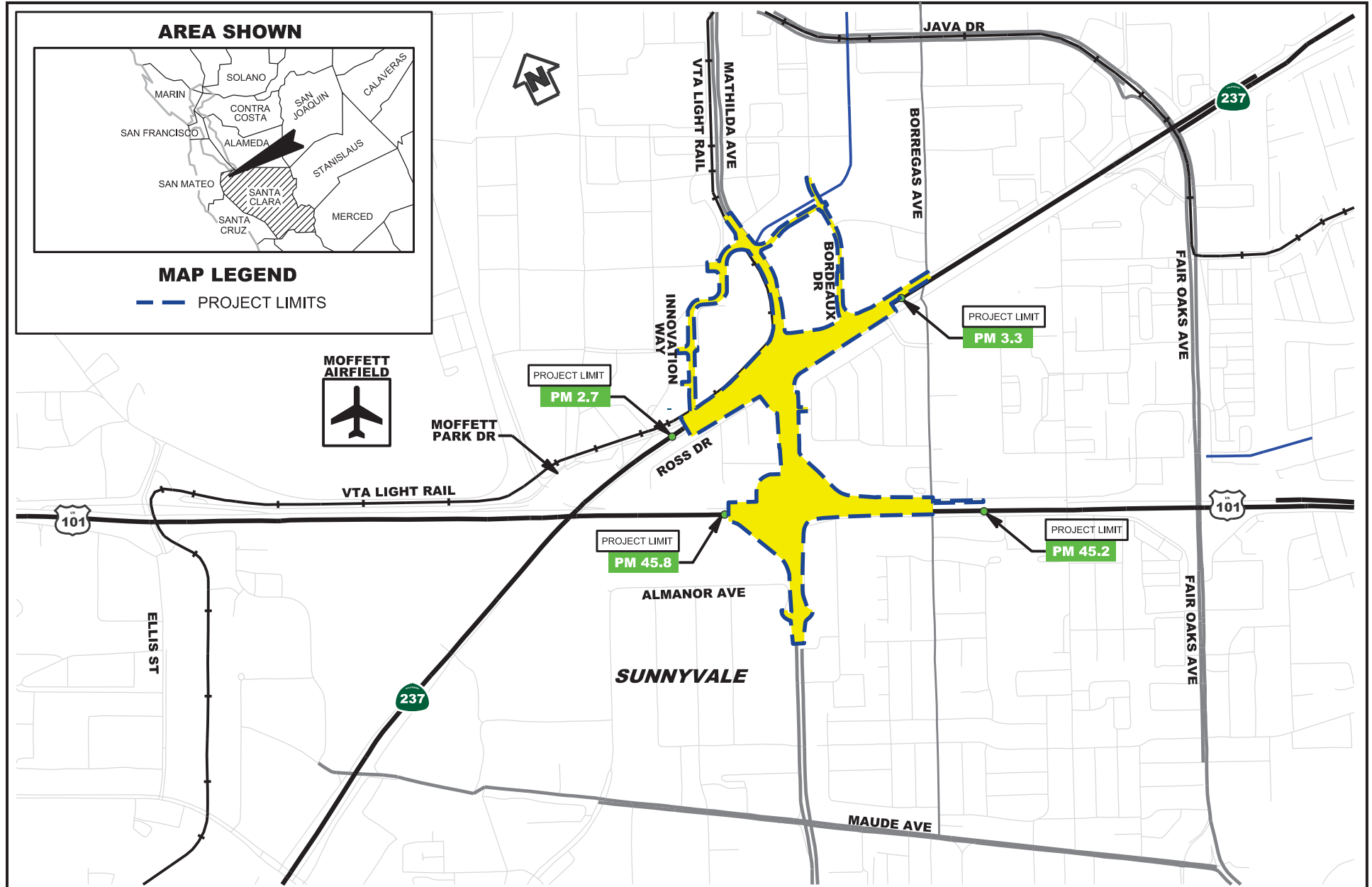
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FIGURES

Project Location

Figure 1



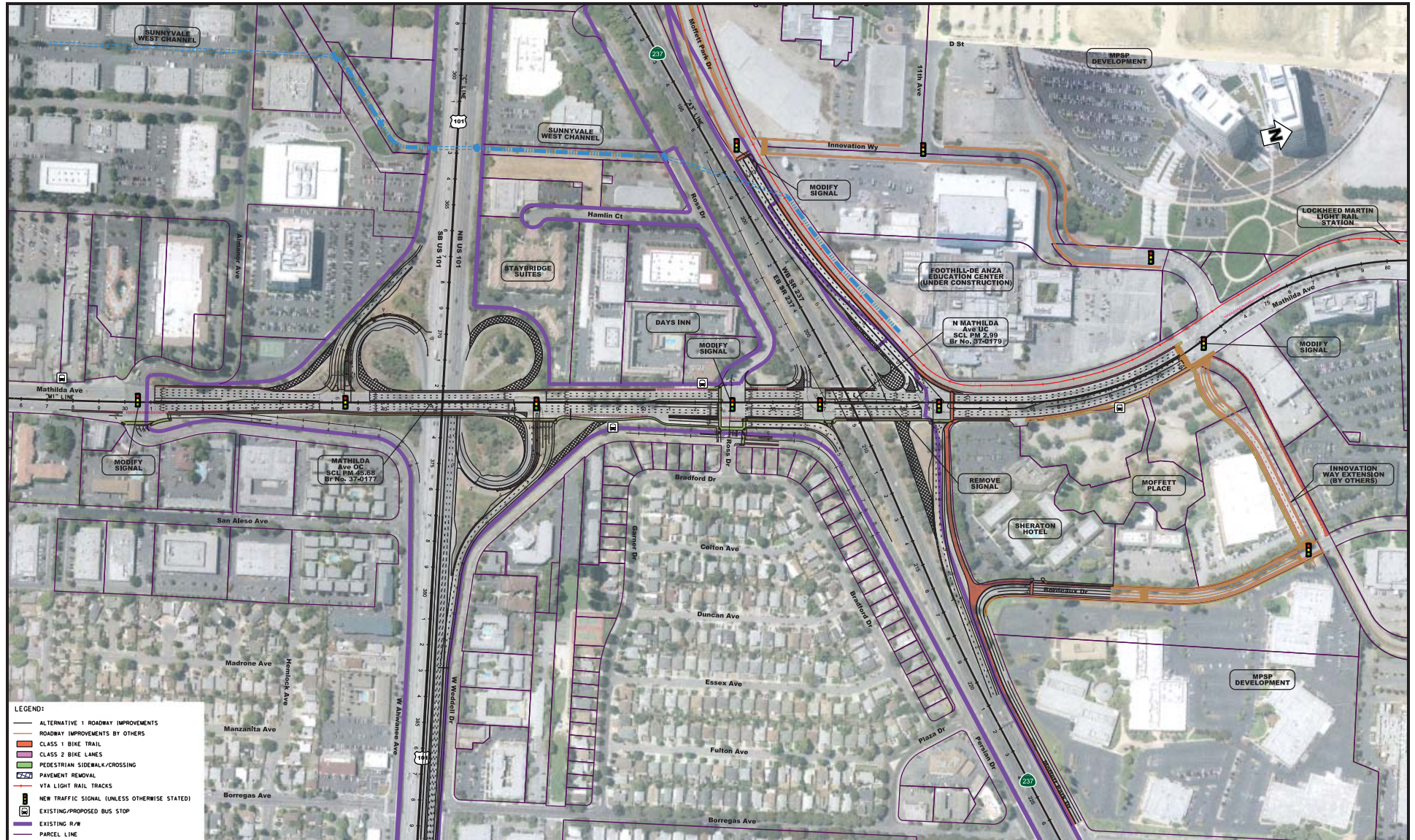
Source: WMH, 2015

Mathilda Avenue Improvements at SR 237 and US 101 Project

Note: Not to Scale

Build Alternative 1

Figure 2a

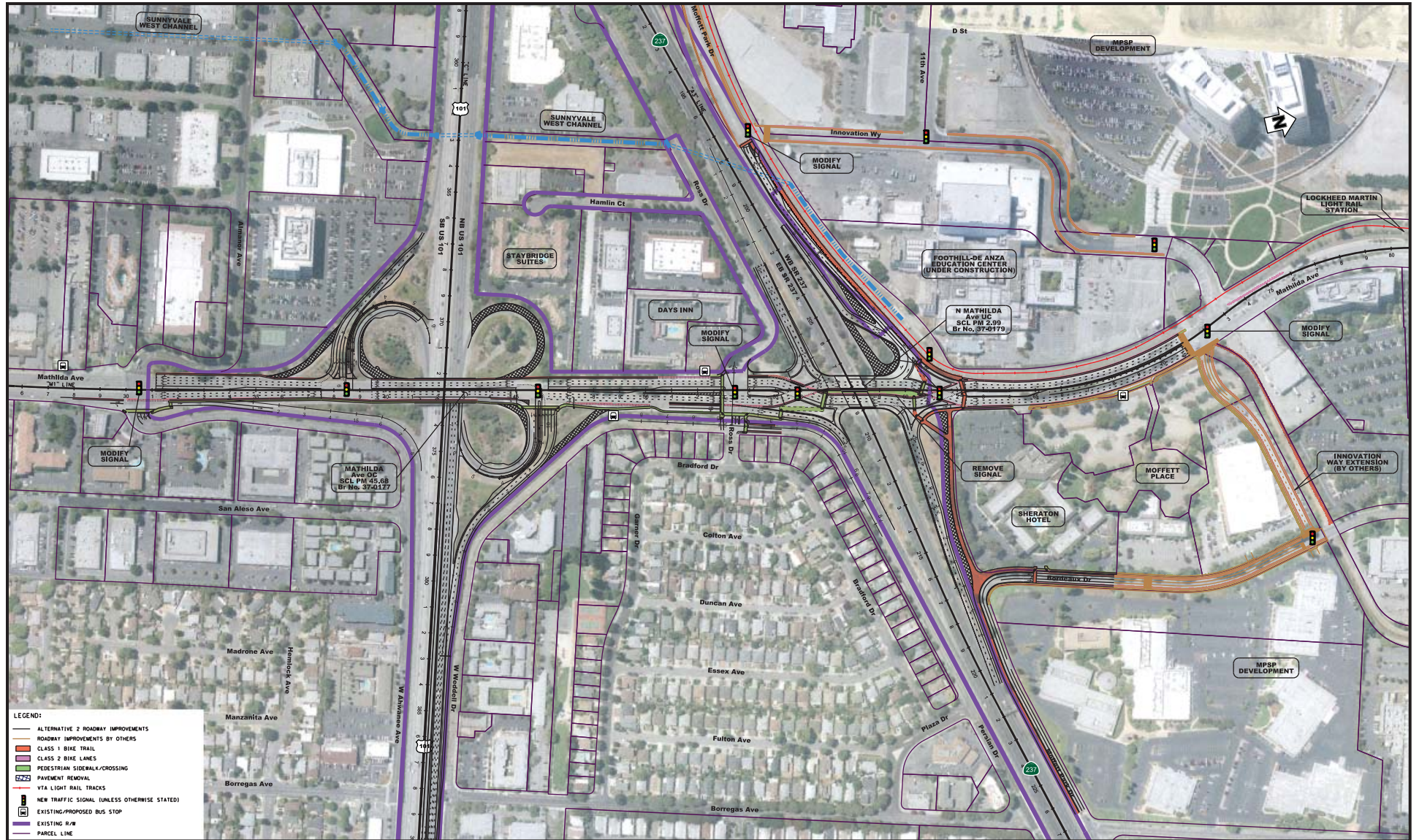


Mathilda Avenue Improvements at SR 237 and US 101 Project



Build Alternative 2

Figure 2b

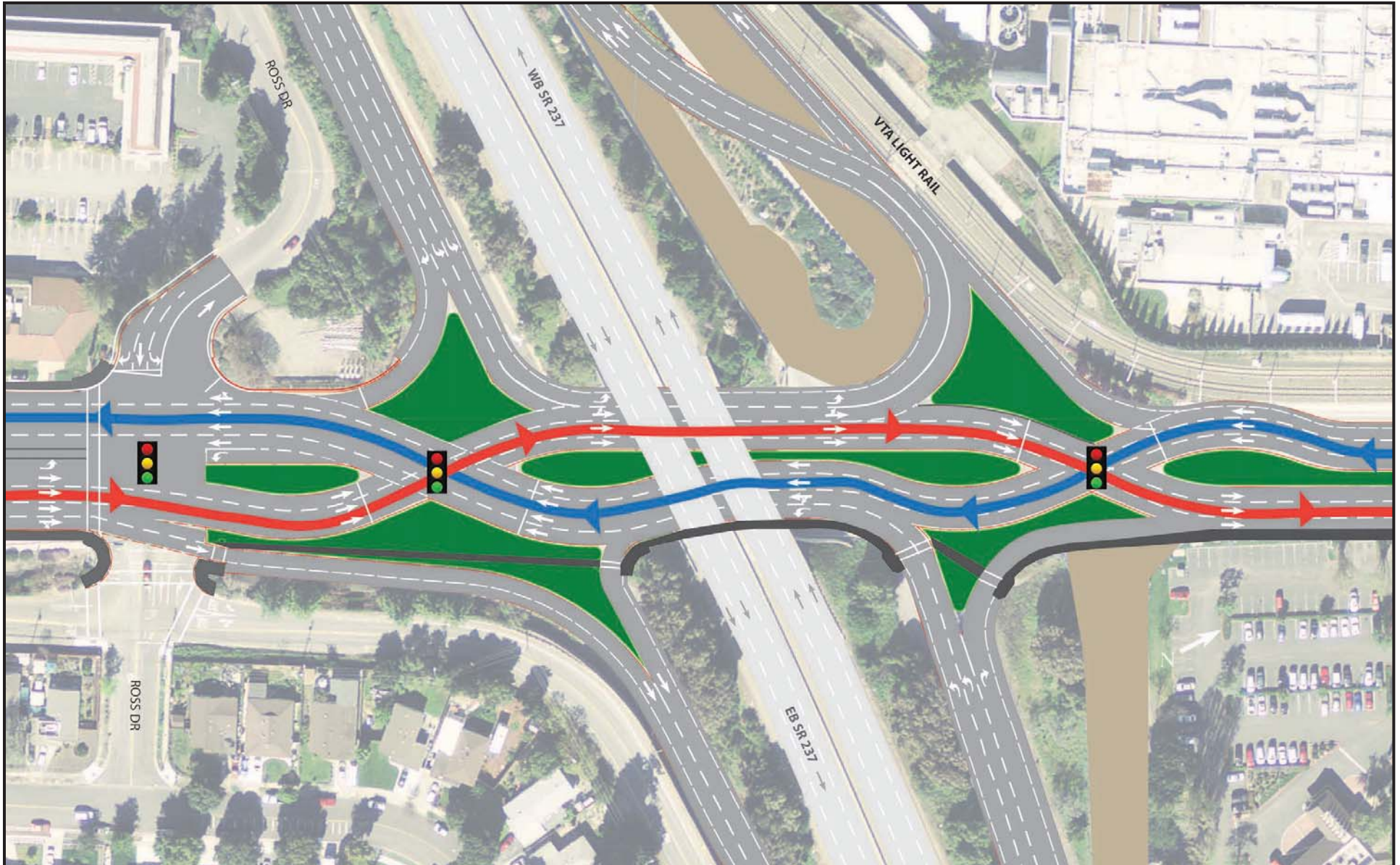


Mathilda Avenue Improvements at SR 237 and US 101 Project



Diverging Diamond Interchange Illustration

Figure 3

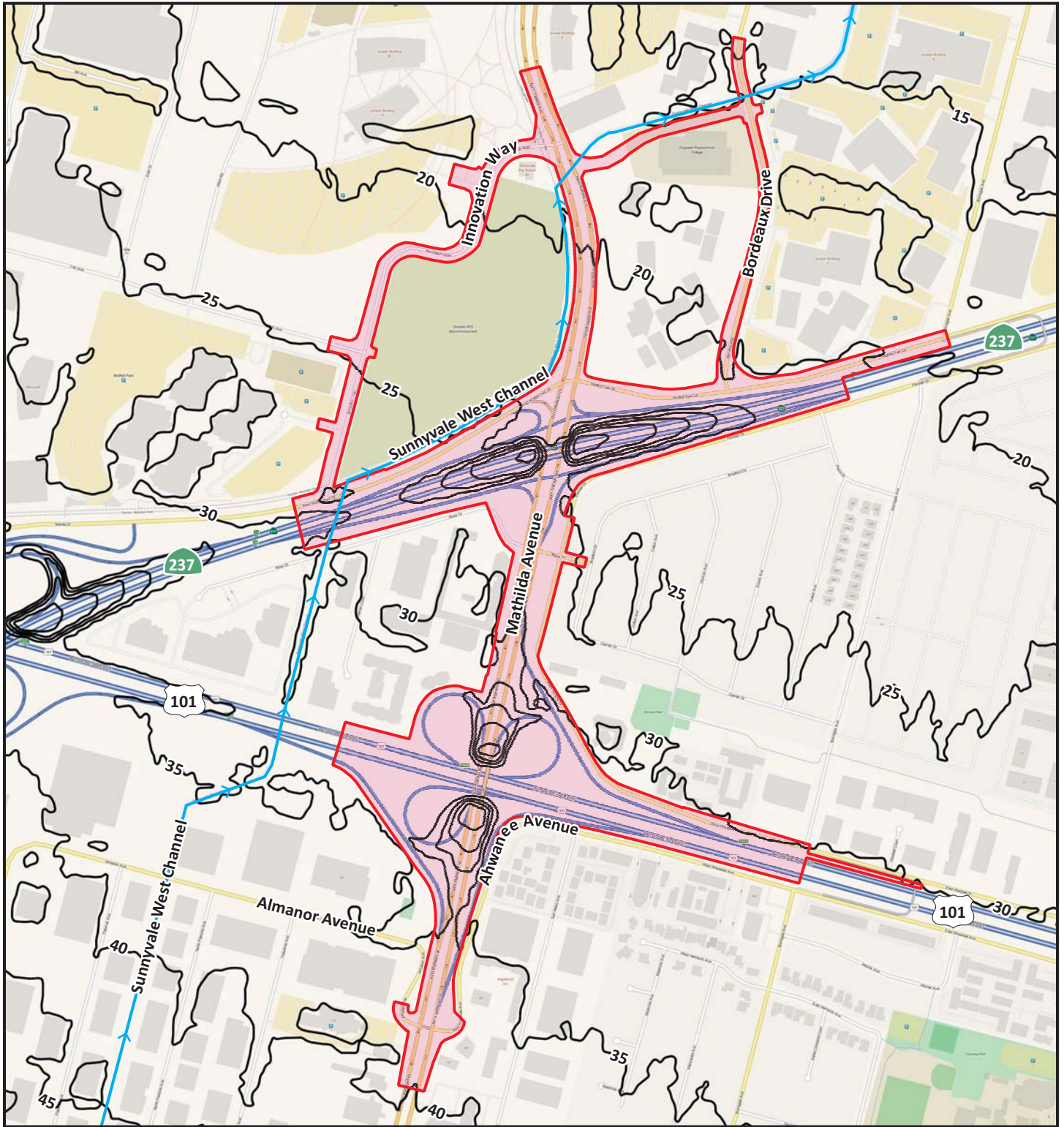


Source: WMH, 2015


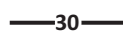

Mathilda Avenue Improvements at SR 237 and US 101 Project



Note: Not to Scale



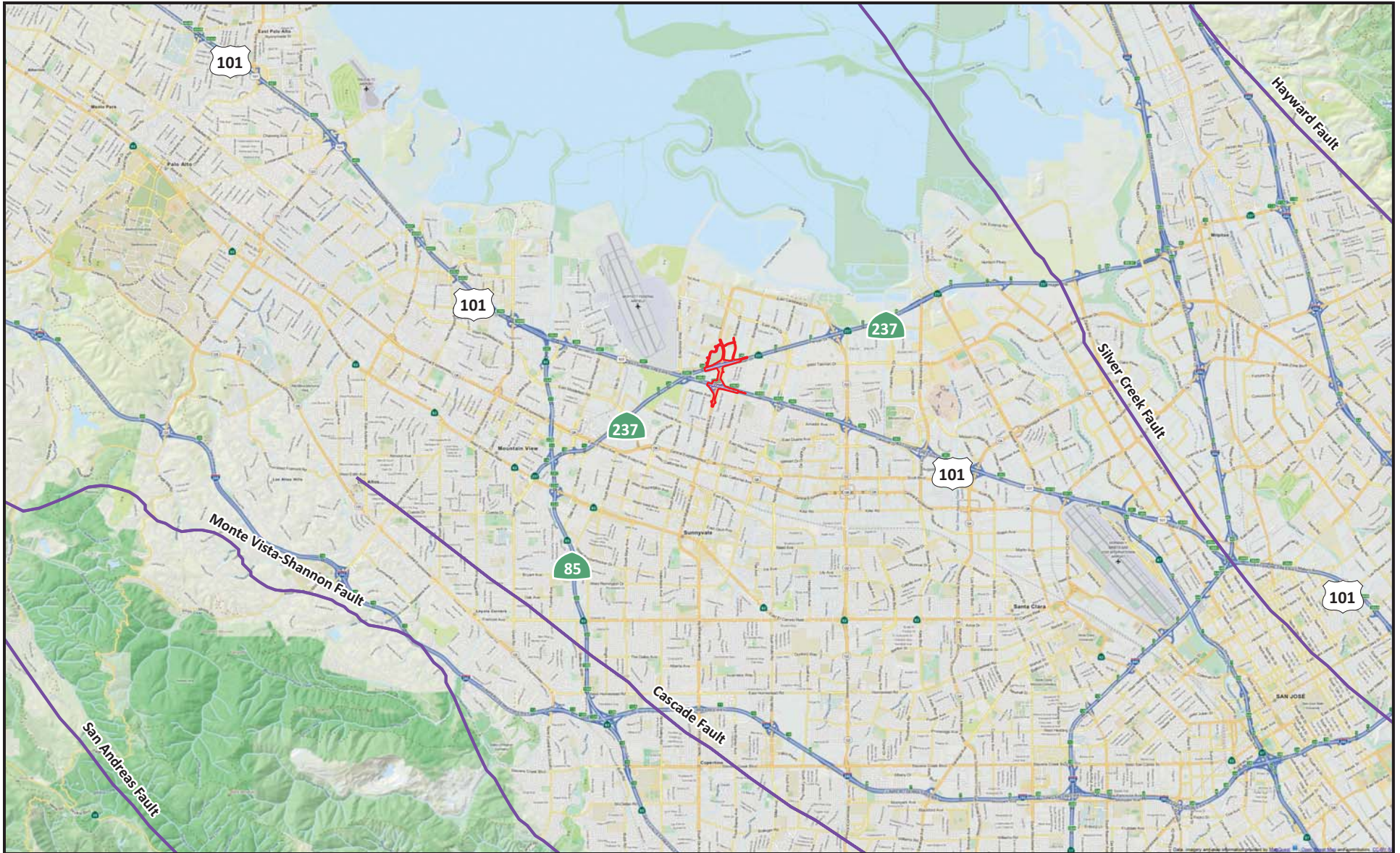
Legend

-  Project Limits
-  —30— Surface Elevation Contour (feet, NAVD 88)
-  —> Surface Water Flow Direction

Base: MapQuest OpenStreetMap, 2015
Source: Surface Elevation Contours (USGS, 2015)

Mathilda Avenue Improvements at SR 237 and US 101 Project



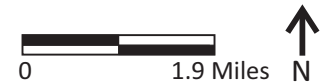


Base: MapQuest OpenStreetMap, 2015
Source: Active Faults (Caltrans, 2012a)

Legend

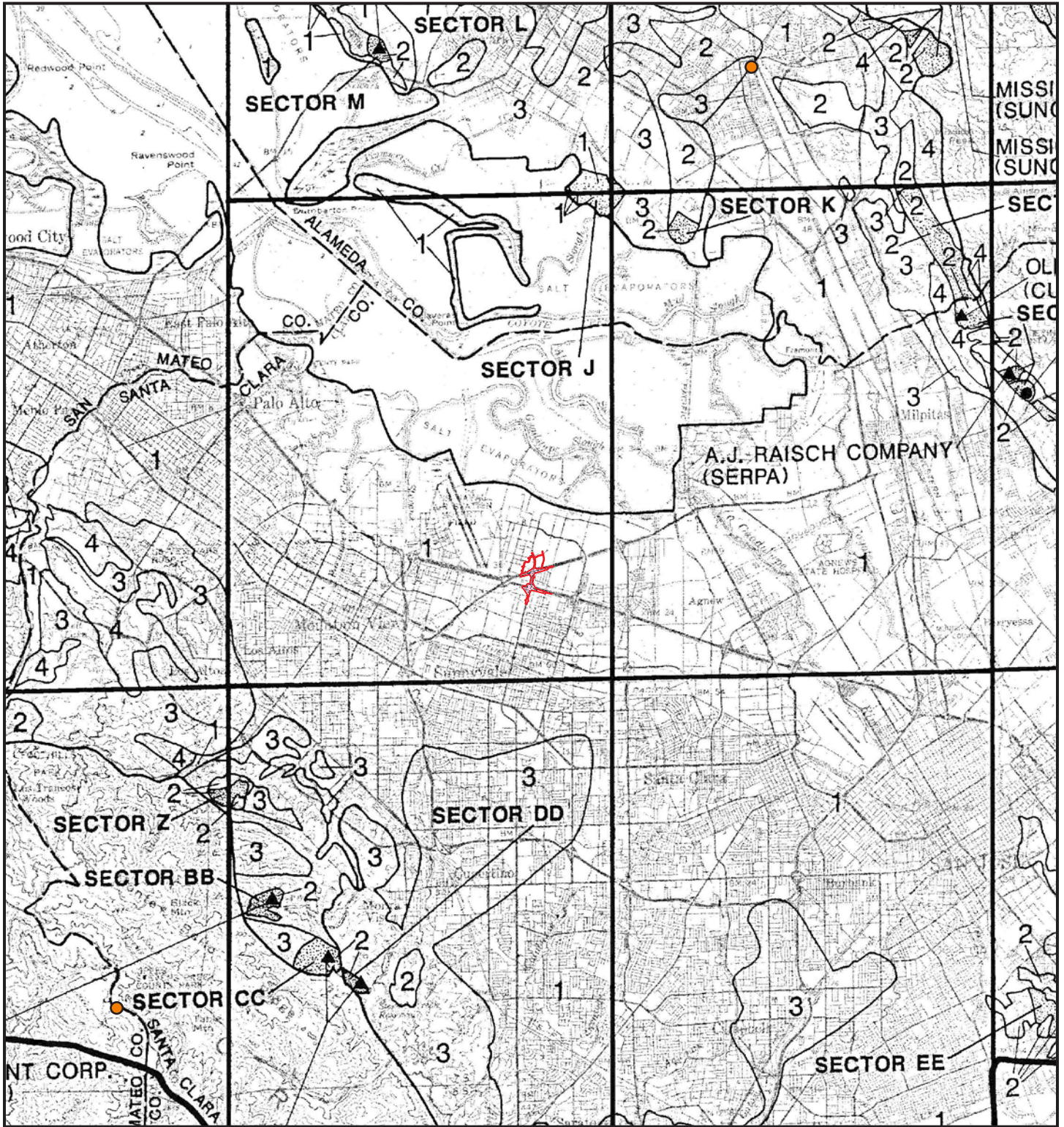
-  Project Limits
-  Active Fault

**Mathilda Avenue Improvements
at SR 237 and US 101 Project**



Mineral Resource Zones and DOGGR Wells

Figure 6

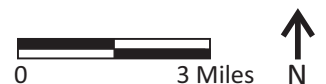


Legend

- Project Limits
- California Department of Conservation, Division of Oil, Gas, and Geothermal Resources (DOGGR) Well

Source: Mineral Resource Zones (Kohler-Antablin, 1996)
DOGGR Wells (DOGGR, 2015)

Mathilda Avenue Improvements at SR 237 and US 101 Project



TABLES

TABLE 1: Modified Mercalli Intensity Scale

| MMI Scale | PGA ¹ (%g) | Perceived Shaking | Description of Ground Motion Intensity ² |
|-----------|-----------------------|-------------------|---|
| I | <0.17 | None | Not felt except by a very few under especially favorable circumstances. |
| II | 0.17-1.4 | Weak | Felt only by a few persons at rest, especially on upper floors of buildings. Delicately suspended objects may swing. |
| III | 0.17-1.4 | Weak | Felt quite noticeably indoors, especially on upper floors of buildings, but many people do not recognize it as an earthquake. Standing motor cars may rock slightly. Vibration like passing of truck. Duration estimated. |
| IV | 1.4-3.9 | Light | During the day felt indoors by many, outdoors by few. At night some awakened. Dishes, windows, doors disturbed; walls make cracking sound. Sensation like heavy truck striking building. Standing motor cars rocked noticeably. |
| V | 3.9-9.2 | Moderate | Felt by nearly everyone, many awakened. Some dishes, windows, etc., broken; a few instances of cracked plaster; unstable objects overturned. Disturbances of trees, poles, and other tall objects sometimes noticed. Pendulum clocks may stop. |
| VI | 9.2-18 | Strong | Felt by all, many frightened and run outdoors. Some heavy furniture moved; a few instances of fallen plaster or damaged chimneys. Damage slight. |
| VII | 18-34 | Very Strong | Everybody runs outdoors. Damage negligible in building of good design and construction; slight to moderate in well-built ordinary structures; considerable in poorly built or badly designed structures; some chimneys broken. <u>Noticed by persons driving motor cars.</u> |
| VIII | 34-65 | Severe | Damage slight in specially designed structures; considerable in ordinary substantial buildings, with partial collapse; great in poorly built structures. Panel walls thrown out of frame structures. Fall of chimneys, factory stacks, columns, monuments, walls. Heavy furniture overturned. Sand and mud ejected in small amounts. Changes in well water. Persons driving motor cars disturbed. |
| IX | 65-124 | Violent | Damage considerable in specially designed structures; well-designed frame structures thrown out of plumb; great in substantial buildings, with partial collapse. Buildings shifted off foundations. Ground cracked conspicuously. <u>Underground pipes broken.</u> |
| X | >124 | Extreme | Some well-built wooden structures destroyed; most masonry and frame structures destroyed with foundations; ground badly cracked. Rails bent. Landslides considerable from river banks and steep slopes. Shifted sand and mud. <u>Water splashed (slopped) over banks.</u> |
| XI | >124 | Extreme | Few, if any, (masonry) structures remain standing. Bridges destroyed. Broad fissures in ground. Underground pipelines completely out of service. Earth slumps and land slips in soft ground. <u>Rails bent greatly.</u> |
| XII | >124 | Extreme | Damage total. Practically all works of construction are damaged greatly or destroyed. Waves seen on ground surface. Lines of sight and level are distorted. |

Notes

MMI = Modified Mercalli Intensity; %g = percent of acceleration force of gravity

¹ Wald, D.J., Quitoriano, V., Heaton, T.H., and Kanamori, H., 1999. *Relationship between Peak Ground Acceleration, Peak Ground Velocity, and Modified Mercalli Intensity in California. Earthquake Spectra, V. 15, no. 3, p. 557-564.*

² United States Geological Survey, 2014. *The Modified Mercalli Intensity Scale .*

<http://earthquake.usgs.gov/learn/topics/mercalli.php>. Accessed 6 May.

TABLE 2: Summary of Parameters used to Estimated Ground Shaking Hazards

| Active Fault Name | Distance (miles) | M _{max} | PGA (%g) | MMI Scale | Perceived Shaking |
|---------------------|------------------|------------------|----------|-----------|-------------------|
| Cascade | 3.9 | 6.7 | 72 | IX | Violent |
| Silver Creek | 4.5 | 6.9 | 71 | IX | Violent |
| Monte Vista-Shannon | 5.4 | 6.4 | 60 | VIII | Severe |
| Hayward | 8.4 | 7.3 | 56 | VIII | Severe |
| San Andreas | 9.7 | 8 | 61 | VIII | Severe |

Notes

M_{Max} = maximum moment magnitude

PGA = peak ground acceleration

%g = percent of acceleration force of gravity

MMI = Modified Mercalli Intensity

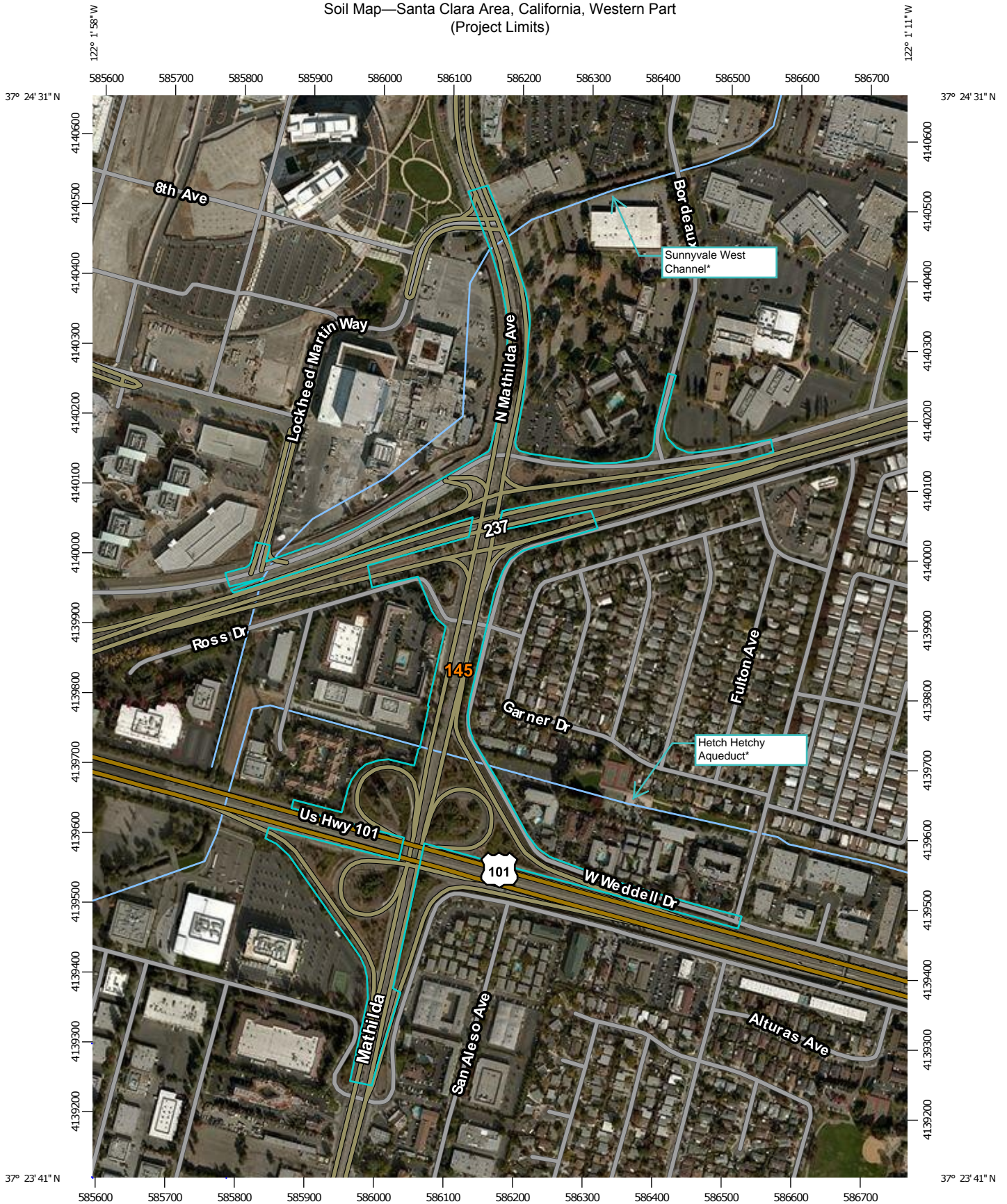
Ground shaking hazards estimated using Caltrans ARS Online V2.3.06 (Caltrans, 2015b).

The relationship between the MMI scale and PGA values are summarized in Table 1.

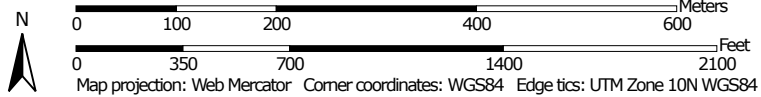
APPENDICES

APPENDIX A
USDA SOIL SURVEY DATA

Soil Map—Santa Clara Area, California, Western Part
(Project Limits)



Map Scale: 1:7,550 if printed on A portrait (8.5" x 11") sheet.




Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 10N WGS84


* Label inserted by BASELINE Environmental Consulting.


MAP LEGEND

Area of Interest (AOI)

 Area of Interest (AOI)

Soils

 Soil Map Unit Polygons

 Soil Map Unit Lines

 Soil Map Unit Points

Special Point Features



Blowout



Borrow Pit



Clay Spot



Closed Depression



Gravel Pit



Gravelly Spot



Landfill



Lava Flow



Marsh or swamp



Mine or Quarry



Miscellaneous Water



Perennial Water



Rock Outcrop



Saline Spot



Sandy Spot



Severely Eroded Spot



Sinkhole



Slide or Slip



Sodic Spot



Spoil Area



Stony Spot



Very Stony Spot



Wet Spot



Other



Special Line Features

Water Features



Streams and Canals

Transportation



Rails



Interstate Highways



US Routes



Major Roads



Local Roads

Background



Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
Web Soil Survey URL: <http://websoilsurvey.nrcs.usda.gov>
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Santa Clara Area, California, Western Part
Survey Area Data: Version 3, Sep 18, 2014

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Oct 26, 2010—Nov 3, 2013

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

| Santa Clara Area, California, Western Part (CA641) | | | |
|--|---|--------------|----------------|
| Map Unit Symbol | Map Unit Name | Acres in AOI | Percent of AOI |
| 145 | Urbanland-Hangerone complex, 0 to 2 percent slopes, drained | 36.8 | 100.0% |
| Totals for Area of Interest | | 36.8 | 100.0% |

Santa Clara Area, California, Western Part

145—Urbanland-Hangerone complex, 0 to 2 percent slopes, drained

Map Unit Setting

National map unit symbol: 1nszw

Elevation: 0 to 220 feet

Mean annual precipitation: 14 to 24 inches

Mean annual air temperature: 57 to 61 degrees F

Frost-free period: 275 to 325 days

Farmland classification: Not prime farmland

Map Unit Composition

Urban land: 70 percent

Hangerone, drained, and similar soils: 25 percent

Minor components: 5 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Urban Land

Setting

Landform: Basin floors

Landform position (three-dimensional): Talf

Down-slope shape: Linear

Across-slope shape: Linear

Parent material: Disturbed and human-transported material

Description of Hangerone, Drained

Setting

Landform: Basin floors

Landform position (three-dimensional): Talf

Down-slope shape: Linear

Across-slope shape: Linear, convex

Parent material: Alluvium derived from metamorphic and sedimentary rock and/or alluvium derived from metavolcanics

Typical profile

A1 - 0 to 9 inches: clay

A2 - 9 to 17 inches: clay

Bw - 17 to 27 inches: clay

Bk - 27 to 35 inches: clay

Ck - 35 to 45 inches: clay loam

C - 45 to 72 inches: gravelly loam

2Ab - 72 to 89 inches: clay

Properties and qualities

Slope: 0 to 2 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Poorly drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat):

Moderately low to moderately high (0.06 to 0.20 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Calcium carbonate, maximum in profile: 25 percent

Gypsum, maximum in profile: 2 percent

Salinity, maximum in profile: Nonsaline to slightly saline (0.2 to 4.0 mmhos/cm)

Sodium adsorption ratio, maximum in profile: 5.0

Available water storage in profile: Moderate (about 8.3 inches)

Interpretive groups

Land capability classification (irrigated): 2s

Land capability classification (nonirrigated): 3s

Hydrologic Soil Group: C

Minor Components

Bayshore

Percent of map unit: 2 percent

Landform: Basin floors

Landform position (three-dimensional): Talf

Down-slope shape: Linear

Across-slope shape: Linear

Clear lake

Percent of map unit: 2 percent

Landform: Basin floors

Landform position (three-dimensional): Talf

Down-slope shape: Linear

Across-slope shape: Linear

Embarcadero

Percent of map unit: 1 percent

Landform: Basin floors

Landform position (three-dimensional): Talf

Down-slope shape: Linear

Across-slope shape: Linear

Data Source Information

Soil Survey Area: Santa Clara Area, California, Western Part

Survey Area Data: Version 3, Sep 18, 2014

Physical Soil Properties

This table shows estimates of some physical characteristics and features that affect soil behavior. These estimates are given for the layers of each soil in the survey area. The estimates are based on field observations and on test data for these and similar soils.

Depth to the upper and lower boundaries of each layer is indicated.

Particle size is the effective diameter of a soil particle as measured by sedimentation, sieving, or micrometric methods. Particle sizes are expressed as classes with specific effective diameter class limits. The broad classes are sand, silt, and clay, ranging from the larger to the smaller.

Sand as a soil separate consists of mineral soil particles that are 0.05 millimeter to 2 millimeters in diameter. In this table, the estimated sand content of each soil layer is given as a percentage, by weight, of the soil material that is less than 2 millimeters in diameter.

Silt as a soil separate consists of mineral soil particles that are 0.002 to 0.05 millimeter in diameter. In this table, the estimated silt content of each soil layer is given as a percentage, by weight, of the soil material that is less than 2 millimeters in diameter.

Clay as a soil separate consists of mineral soil particles that are less than 0.002 millimeter in diameter. In this table, the estimated clay content of each soil layer is given as a percentage, by weight, of the soil material that is less than 2 millimeters in diameter.

The content of sand, silt, and clay affects the physical behavior of a soil. Particle size is important for engineering and agronomic interpretations, for determination of soil hydrologic qualities, and for soil classification.

The amount and kind of clay affect the fertility and physical condition of the soil and the ability of the soil to adsorb cations and to retain moisture. They influence shrink-swell potential, saturated hydraulic conductivity (K_{sat}), plasticity, the ease of soil dispersion, and other soil properties. The amount and kind of clay in a soil also affect tillage and earthmoving operations.

Moist bulk density is the weight of soil (oven-dry) per unit volume. Volume is measured when the soil is at field moisture capacity, that is, the moisture content at 1/3- or 1/10-bar (33kPa or 10kPa) moisture tension. Weight is determined after the soil is dried at 105 degrees C. In the table, the estimated moist bulk density of each soil horizon is expressed in grams per cubic centimeter of soil material that is less than 2 millimeters in diameter. Bulk density data are used to compute linear extensibility, shrink-swell potential, available water capacity, total pore space, and other soil properties. The moist bulk density of a soil indicates the pore space available for water and roots. Depending on soil texture, a bulk density of more than 1.4 can restrict water storage and root penetration. Moist bulk density is influenced by texture, kind of clay, content of organic matter, and soil structure.

Saturated hydraulic conductivity (Ksat) refers to the ease with which pores in a saturated soil transmit water. The estimates in the table are expressed in terms of micrometers per second. They are based on soil characteristics observed in the field, particularly structure, porosity, and texture. Saturated hydraulic conductivity (Ksat) is considered in the design of soil drainage systems and septic tank absorption fields.

Available water capacity refers to the quantity of water that the soil is capable of storing for use by plants. The capacity for water storage is given in inches of water per inch of soil for each soil layer. The capacity varies, depending on soil properties that affect retention of water. The most important properties are the content of organic matter, soil texture, bulk density, and soil structure. Available water capacity is an important factor in the choice of plants or crops to be grown and in the design and management of irrigation systems. Available water capacity is not an estimate of the quantity of water actually available to plants at any given time.

Linear extensibility refers to the change in length of an unconfined clod as moisture content is decreased from a moist to a dry state. It is an expression of the volume change between the water content of the clod at 1/3- or 1/10-bar tension (33kPa or 10kPa tension) and oven dryness. The volume change is reported in the table as percent change for the whole soil. The amount and type of clay minerals in the soil influence volume change.

Linear extensibility is used to determine the shrink-swell potential of soils. The shrink-swell potential is low if the soil has a linear extensibility of less than 3 percent; moderate if 3 to 6 percent; high if 6 to 9 percent; and very high if more than 9 percent. If the linear extensibility is more than 3, shrinking and swelling can cause damage to buildings, roads, and other structures and to plant roots. Special design commonly is needed.

Organic matter is the plant and animal residue in the soil at various stages of decomposition. In this table, the estimated content of organic matter is expressed as a percentage, by weight, of the soil material that is less than 2 millimeters in diameter. The content of organic matter in a soil can be maintained by returning crop residue to the soil.

Organic matter has a positive effect on available water capacity, water infiltration, soil organism activity, and tilth. It is a source of nitrogen and other nutrients for crops and soil organisms.

Erosion factors are shown in the table as the K factor (Kw and Kf) and the T factor. Erosion factor K indicates the susceptibility of a soil to sheet and rill erosion by water. Factor K is one of six factors used in the Universal Soil Loss Equation (USLE) and the Revised Universal Soil Loss Equation (RUSLE) to predict the average annual rate of soil loss by sheet and rill erosion in tons per acre per year. The estimates are based primarily on percentage of silt, sand, and organic matter and on soil structure and Ksat. Values of K range from 0.02 to 0.69. Other factors being equal, the higher the value, the more susceptible the soil is to sheet and rill erosion by water.

Erosion factor Kw indicates the erodibility of the whole soil. The estimates are modified by the presence of rock fragments.

Erosion factor Kf indicates the erodibility of the fine-earth fraction, or the material less than 2 millimeters in size.

Erosion factor T is an estimate of the maximum average annual rate of soil erosion by wind and/or water that can occur without affecting crop productivity over a sustained period. The rate is in tons per acre per year.

Wind erodibility groups are made up of soils that have similar properties affecting their susceptibility to wind erosion in cultivated areas. The soils assigned to group 1 are the most susceptible to wind erosion, and those assigned to group 8 are the least susceptible. The groups are described in the "National Soil Survey Handbook."

Wind erodibility index is a numerical value indicating the susceptibility of soil to wind erosion, or the tons per acre per year that can be expected to be lost to wind erosion. There is a close correlation between wind erosion and the texture of the surface layer, the size and durability of surface clods, rock fragments, organic matter, and a calcareous reaction. Soil moisture and frozen soil layers also influence wind erosion.

Reference:

United States Department of Agriculture, Natural Resources Conservation Service. National soil survey handbook, title 430-VI. (<http://soils.usda.gov>)

Report—Physical Soil Properties

| Physical Soil Properties—Santa Clara Area, California, Western Part | | | | | | | | | | | | | | |
|---|-----------|------------|------------|------------|--------------------|----------------------------------|--------------------------|----------------------|------------------|-----------------|-----|---|------------------------|------------------------|
| Map symbol and soil name | Depth | Sand | Silt | Clay | Moist bulk density | Saturated hydraulic conductivity | Available water capacity | Linear extensibility | Organic matter | Erosion factors | | | Wind erodibility group | Wind erodibility index |
| | | | | | | | | | | Kw | Kf | T | | |
| | <i>In</i> | <i>Pct</i> | <i>Pct</i> | <i>Pct</i> | <i>g/cc</i> | <i>micro m/sec</i> | <i>In/In</i> | <i>Pct</i> | <i>Pct</i> | | | | | |
| 145— Urbanland- Hangerone complex, 0 to 2 percent slopes, drained | | | | | | | | | | | | | | |
| Urban land | — | — | — | — | — | — | — | — | — | | | | | |
| Hangerone, drained | 0-9 | -21- | -38- | 27-42- 45 | 1.40-1.45 -1.50 | 1.40-3.00-4.00 | 0.17-0.19-0. 21 | 6.0- 7.5- 9.0 | 1.0- 2.0- 4.0 | .28 | .28 | 5 | 4 | 86 |
| | 9-17 | -16- | -34- | 27-51- 55 | 1.40-1.45 -1.50 | 1.40-3.00-4.00 | 0.17-0.19-0. 21 | 6.0- 7.5- 9.0 | 0.8- 1.1- 2.0 | .24 | .24 | | | |
| | 17-27 | -16- | -34- | 35-50- 60 | 1.35-1.40 -1.45 | 0.42-1.00-1.40 | 0.14-0.15-0. 16 | 9.0-10.5-12.0 | 0.8- 1.1- 2.0 | .24 | .24 | | | |
| | 27-35 | -19- | -38- | 35-44- 60 | 1.35-1.40 -1.45 | 0.42-1.00-1.40 | 0.14-0.15-0. 16 | 9.0-10.5-12.0 | 0.5- 0.9- 1.5 | .28 | .28 | | | |
| | 35-45 | -25- | -42- | 30-34- 60 | 1.35-1.40 -1.45 | 0.42-1.00-1.40 | 0.14-0.15-0. 16 | 9.0-10.5-12.0 | 0.4- 0.6- 0.8 | .37 | .37 | | | |
| | 45-72 | -44- | -32- | 20-24- 35 | 1.60-1.65 -1.70 | 42.00-50.00-14 1.00 | 0.05-0.06-0. 07 | 0.0- 3.0- 9.0 | 0.1- 0.3- 0.5 | .10 | .20 | | | |
| | 72-89 | -22- | -29- | 20-49- 50 | 1.45-1.50 -1.55 | 4.00-10.00-14.0 0 | 0.15-0.18-0. 20 | 3.0- 6.0- 9.0 | 0.1- 0.1- 0.3 | .20 | .20 | | | |

Data Source Information

Soil Survey Area: Santa Clara Area, California, Western Part
Survey Area Data: Version 3, Sep 18, 2014

Soil Features

This table gives estimates of various soil features. The estimates are used in land use planning that involves engineering considerations.

A *restrictive layer* is a nearly continuous layer that has one or more physical, chemical, or thermal properties that significantly impede the movement of water and air through the soil or that restrict roots or otherwise provide an unfavorable root environment. Examples are bedrock, cemented layers, dense layers, and frozen layers. The table indicates the hardness and thickness of the restrictive layer, both of which significantly affect the ease of excavation. *Depth to top* is the vertical distance from the soil surface to the upper boundary of the restrictive layer.

Subsidence is the settlement of organic soils or of saturated mineral soils of very low density. Subsidence generally results from either desiccation and shrinkage, or oxidation of organic material, or both, following drainage. Subsidence takes place gradually, usually over a period of several years. The table shows the expected initial subsidence, which usually is a result of drainage, and total subsidence, which results from a combination of factors.

Potential for frost action is the likelihood of upward or lateral expansion of the soil caused by the formation of segregated ice lenses (frost heave) and the subsequent collapse of the soil and loss of strength on thawing. Frost action occurs when moisture moves into the freezing zone of the soil. Temperature, texture, density, saturated hydraulic conductivity (Ksat), content of organic matter, and depth to the water table are the most important factors considered in evaluating the potential for frost action. It is assumed that the soil is not insulated by vegetation or snow and is not artificially drained. Silty and highly structured, clayey soils that have a high water table in winter are the most susceptible to frost action. Well drained, very gravelly, or very sandy soils are the least susceptible. Frost heave and low soil strength during thawing cause damage to pavements and other rigid structures.

Risk of corrosion pertains to potential soil-induced electrochemical or chemical action that corrodes or weakens uncoated steel or concrete. The rate of corrosion of uncoated steel is related to such factors as soil moisture, particle-size distribution, acidity, and electrical conductivity of the soil. The rate of corrosion of concrete is based mainly on the sulfate and sodium content, texture, moisture content, and acidity of the soil. Special site examination and design may be needed if the combination of factors results in a severe hazard of corrosion. The steel or concrete in installations that intersect soil boundaries or soil layers is more susceptible to corrosion than the steel or concrete in installations that are entirely within one kind of soil or within one soil layer.

For uncoated steel, the risk of corrosion, expressed as *low*, *moderate*, or *high*, is based on soil drainage class, total acidity, electrical resistivity near field capacity, and electrical conductivity of the saturation extract.

For concrete, the risk of corrosion also is expressed as *low*, *moderate*, or *high*. It is based on soil texture, acidity, and amount of sulfates in the saturation extract.

Report—Soil Features

| Soil Features—Santa Clara Area, California, Western Part | | | | | | | | | |
|---|--------------------|--------------------|--------------|-----------|-----------------|-----------------|----------------------------|-------------------|----------|
| Map symbol and soil name | Restrictive Layer | | | | Subsidence | | Potential for frost action | Risk of corrosion | |
| | Kind | Depth to top | Thickness | Hardness | Initial | Total | | Uncoated steel | Concrete |
| | | <i>Low-RV-High</i> | <i>Range</i> | | <i>Low-High</i> | <i>Low-High</i> | | | |
| | | <i>In</i> | <i>In</i> | | <i>In</i> | <i>In</i> | | | |
| 145—Urbanland-Hangerone complex, 0 to 2 percent slopes, drained | | | | | | | | | |
| Urban land | Manufactured layer | - 0- | — | Indurated | 0 | 24-79 | None | | |
| Hangerone, drained | | — | — | | 0 | 24-79 | None | High | Moderate |

Data Source Information

Soil Survey Area: Santa Clara Area, California, Western Part
 Survey Area Data: Version 3, Sep 18, 2014

APPENDIX B

QUALIFICATIONS OF PREPARERS

Bruce Abelli-Amen, P.G., C.Hg.

Principal Certified Hydrogeologist

M.S., Environmental Systems, Applied Geology, Humboldt State University, 1988
B.A., Geological Sciences, UC Santa Barbara
40-hour OSHA training, 1985
Certified Hydrogeologist No. 96, 1995
Professional Geologist No. 5593, 1993
25 years of experience



Recent Projects

- Yolo County Central Landfill Soil Borrow Site EIR, Project Manager
- New Irvington Tunnel EIR, Hetch Hetchy Water Conveyance System, SFPUC, EIR and Groundwater Project Manager
- Port of San Francisco, Municipal Stormwater Program Manager
- SFPUC Westside Groundwater Basin Monitoring Program Manager
- City Place EIR, Santa Clara, Project Manager for Geology, Groundwater Hydrology and Water Quality, and Hazardous Materials sections.
- Doyle Drive Replacement Project, San Francisco, Technical Lead on Hydrology and Water Quality and Groundwater Monitoring
- Apple Campus EIR, Cupertino, Project Manager for Geology, Hazards, and Hydrology EIR sections

Bruce Abelli-Amen is a Principal, Certified Hydrogeologist, and a CEQA project manager. He also manages hazardous materials investigations. He has experience in all phases of CEQA and NEPA projects, including managing large multi-disciplinary teams of specialists in the preparation of Expanded Initial Studies, Mitigated Negative Declarations, and Environmental Impact Reports and Statements. He has managed CEQA projects for landfill decommissioning, new wastewater treatment plants, mining projects, mixed-use developments, and major water conveyance infrastructure projects.

He also has experience with construction management and permitting, which provides useful insights into the development of feasible and practical mitigation measures for identified significant CEQA impacts. He is currently leading the Groundwater Management Program during construction of the SFPUC's New Irvington Tunnel between Sunol Valley and Fremont.

He is also currently assisting the Port of San Francisco with their NPDES compliance programs (both the Industrial General Permit and the Phase II MS4 General Permit. Under this program, BASELINE collects stormwater runoff samples, updates the Port's website with current content, assists with education and outreach, and completes annual reports.

He has designed and implemented groundwater aquifer tests and remediation systems for the cleanup of contaminated shallow groundwater aquifers. He has managed numerous UST investigations and is familiar with local, state, and federal regulatory requirements for such investigations. He has experience managing large-scale soil and groundwater remediation projects. He has supervised soil excavation, bioremediation, and backfill operations.

What Our Clients Say:

Bruce Abelli-Amen's performance for the Port of San Francisco is excellent. Bruce is client-focused, anticipates my project needs, and offers creative solutions if problems arise. The BASELINE team has consistently provided great service and most importantly, there are no surprises! I know that I will get a topnotch product. – Shannon Alford, Port of San Francisco

Patrick Sutton

Environmental Engineer

M.S., Civil and Environmental Engineering,
University of California – Davis

B.S., Environmental Science,
Dickinson College

10 years of experience



Recent Projects

- I-680 Northbound HOV/Express Lane Project, Manager for the Caltrans Initial Site Assessment and Preliminary Geological Assessment.
- Yolo County Central Landfill Soil Borrow Site EIR, Technical Lead for Air Quality, Climate Change, Geology, Hazardous Materials, Hydrology, Mineral Resources, and Paleontology.
- Mountain View General Plan EIR, Technical Lead for Hazardous Materials.
- New Irvington Tunnel Project, Water Resource Database Manager for over 40 domestic water supply wells.

Recent Publications

- Sutton, P.T. and T.R Ginn, 2014. Sustainable in-well vapor stripping: A design, analytical model, and pilot study for groundwater remediation. Journal of Contaminant Hydrology. 171 32-41.
- ASTM D6771-15 (Under Review), Standard Practice Low-Flow Purging and Sampling for Wells Used for Groundwater Quality Investigations. ASTM International.

Patrick Sutton is an environmental engineer. He has prepared numerous CEQA evaluations for air quality, climate change, geology, paleontology, hazardous materials, and water quality related to residential, commercial, and industrial projects, as well as large infrastructure developments. Mr. Sutton has also prepared many Phase I Environmental Site Assessments in accordance with ASTM standards and Initial Site Assessments and Preliminary Site Investigations in accordance with Caltrans requirements. His proficiency in a wide range of technical software (Microsoft Access, GIS, air quality and groundwater models, and graphics design) allows him to thoroughly and efficiently assess and mitigate environmental concerns.

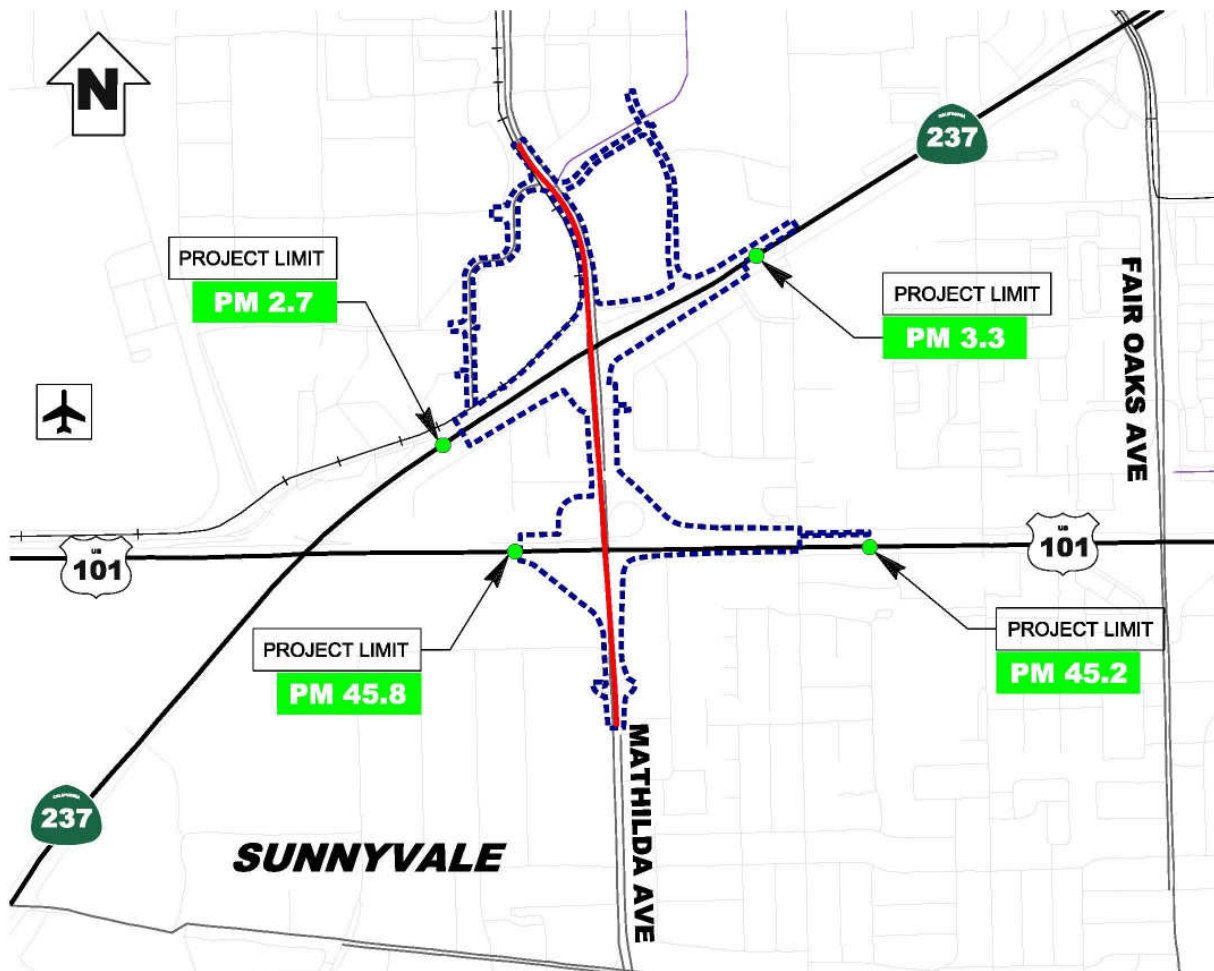
Mr. Sutton has worked as a field technician for hazardous waste sites, and managed state-funded and privately-financed soil and groundwater remediation projects. Remediation projects have included service stations, landfills, drycleaners, railroads, and other commercial properties impacted by hazardous materials releases. As a current member of ASTM, Mr. Sutton is revising the standard for low-flow purging and sampling commonly applied during environmental investigations to improve estimates of contaminant concentrations in groundwater.

In 2014, Mr. Sutton designed and modeled a sustainable in-well vapor stripping system to remove chlorinated solvents from groundwater, and to provide an affordable alternative to conventional remediation technologies. In cooperation with the Central Valley Regional Water Quality Control Board, a successful pilot test of the technology was implemented at a dry cleaner site in Sonora, California. Mr. Sutton has also supervised the installation and maintenance of a variety of remediation systems, such as air sparge and soil vapor extraction, enhanced bioremediation, permanganate injection, and groundwater extraction. Through his work associated with assessing, investigating, and remediating hazardous materials in the subsurface, he has developed an excellent perspective on how to satisfy both regulatory and technical requirements to properly manage hazardous material concerns.

SUMMARY OF FLOODPLAIN ENCROACHMENT

for the

MATHILDA AVENUE IMPROVEMENTS AT SR 237 AND US 101 PROJECT



Prepared for:

Santa Clara Valley Transportation Authority

**California Department of Transportation
District 4**

Prepared by:
WRECO

Dated: December 2015

For individuals with sensory disabilities, this document is available in Braille, in large print, on audiocassette, or on computer disk. To obtain a copy in one of these alternative formats, please write to Caltrans, Attn: Elizabeth White, Office of Environmental Planning, 111 Grand Avenue, Oakland, CA 94623-0660; or call (510) 286-6233 (voice); or use the California Relay Service TTY number, (800) 735-2929.

Overview

This memo was prepared by WRECO for the California Department of Transportation, District 4. The purpose of this memo is to examine and analyze the existing Federal Emergency Management Agency (FEMA) floodplains within the limits of the “Mathilda Avenue Improvements at SR 237 and US 101 Project,” document any potential impacts or encroachments upon these floodplains, and recommend any avoidance, minimization, or mitigation that may be required. The Floodplain Evaluation Report Summary is provided in Appendix A. Technical Information for Location Hydraulic Study is provided in Appendix B.

1. INTRODUCTION

The California Department of Transportation (Caltrans), in cooperation with the Santa Clara Valley Transportation Authority (VTA) and the City of Sunnyvale, is proposing the “Mathilda Avenue Improvements at SR 237 and US 101 Project” (Project) to improve Mathilda Avenue in the City of Sunnyvale from Almanor Avenue to Innovation Way, including on- and off-ramp improvements at the State Route (SR) 237/Mathilda Avenue and U.S. Highway 101 (US 101)/Mathilda Avenue interchanges. On SR 237, the Project limits are from 0.3 miles east of the US 101/SR 237 interchange (post mile [PM] 2.7) to 0.3 miles east of the Mathilda Avenue undercrossing (PM 3.3). On US 101, the Project limits are from 0.3 miles south of Mathilda Avenue overcrossing (PM 45.2) to 0.3 miles south of SR 237/US 101 interchange (PM 45.8). The total length of the Project on Mathilda Avenue is approximately one (1) mile. Figure 1 shows the location of the Project, and Figure 2 shows the vicinity of the Project.

1.1 *Project Description and Alternatives*

The Project alternatives that were developed to meet the purpose and need of the Project include Alternative 1, Alternative 2, and the No-Build Alternative (refer to Figure 3 and Figure 4). Under the No-Build Alternative, no changes would be made to the existing local roadways or freeway system within the Project limits. No construction activities would occur, and there would be no change in the operations of the existing facilities.

The design features of the two (2) Build Alternatives include reconfiguration of the US 101 and SR 237 interchanges with Mathilda Avenue. The Build Alternatives include design variations for reconfigured roadways and intersections, and construction of new signalized intersections. Proposed improvements included in the Build Alternatives south of Ross Drive on Mathilda Avenue and at the US 101 interchange, are identical. This includes new bicycle and pedestrian facilities, utility relocations, new storm water treatment facilities, new safety lighting, ramp metering modifications, modification of overhead signage, and a new retaining wall. Unique improvements, north of Ross Drive on Mathilda Avenue, primarily include improvements related to construction of a diverging diamond interchange (DDI)¹ under Build Alternative 2 (Figure 4).

¹ A diverging diamond interchange (DDI), also called a double crossover diamond interchange (DCD), is a type of diamond interchange where traffic briefly crosses over to the left (opposite) side of the roadway, guided by traffic signals at each crossover. This allows

Roadway Improvements

The Build Alternatives would consist of the following roadway improvements:

- Provide three continuous through lanes in each direction of Mathilda Avenue
- Remove northbound US 101 loop off-ramp and shift traffic to northbound US 101 diagonal off-ramp
- Realign and widen northbound ramps and signalize ramp intersection with Mathilda Avenue, and construct left-turn lane on southbound Mathilda Avenue to access northbound US 101 loop on-ramp
- Realign southbound US 101 off-ramp and loop on-ramp and signalize ramp intersection with Mathilda Avenue
- Modify Mathilda Avenue / Ross Drive signal intersection
- Close Moffett Park Drive between Bordeaux Drive and Mathilda Avenue, replace with a Class I bikeway (as described below), and shift traffic to Bordeaux Drive and Innovation Way.²
- Remove westbound SR 237 ramp signal intersection. Realign westbound SR 237 off-ramp opposite Moffett Park Drive and modify signal intersection
- Build Alternative 1 would modify westbound SR 237 ramps to provide a diamond configuration (see Figure 3)
- Build Alternative 2 would modify Mathilda Avenue and SR 237 ramps to provide a diverging diamond configuration (see Figure 4). Eastbound Moffett Park Drive between Innovation Way and Mathilda Way would be diverted to Innovation Way to access Mathilda Avenue

Bicycle and Pedestrian Facilities

Enhanced bicycle and pedestrian facilities would be provided. Bicycle improvements on Mathilda Avenue would consider both Class II and Class III bikeways³, based on available pavement widths within the project limits, and would connect to the existing Class III bikeway north of Innovation Way and Class I bikeway on the Sunnyvale West Channel. Bicycle improvements on Moffett Park Drive would consist of a Class I bikeway between Bordeaux Drive and Mathilda Avenue. Between Mathilda Avenue and Innovation Way, Class II and Class III bikeways would be considered based on available pavement widths within the project limits. A continuous sidewalk would be provided on the east side of Mathilda Avenue within the project limits with crosswalks, curb ramps, and pedestrian countdown signals at each intersection. The new crosswalks at the reconfigured ramp intersections would be signalized.

vehicles to turn left onto freeway on-ramps without stopping and without conflicting with through traffic. The signals at ramp terminal intersections can be operated with two signal phases (a signal phase allows for traffic at an intersection to cycle through specific movements for each direction) instead of three.

² Innovation Way would be extended from Mathilda Avenue to Bordeaux Drive by the Moffett Place development project.

³ Class I bikeway is a bicycle path. Class II bikeway is a bicycle lane. Class III bikeway is bicycle route [Source: Highway Design Manual Index 1002.1]

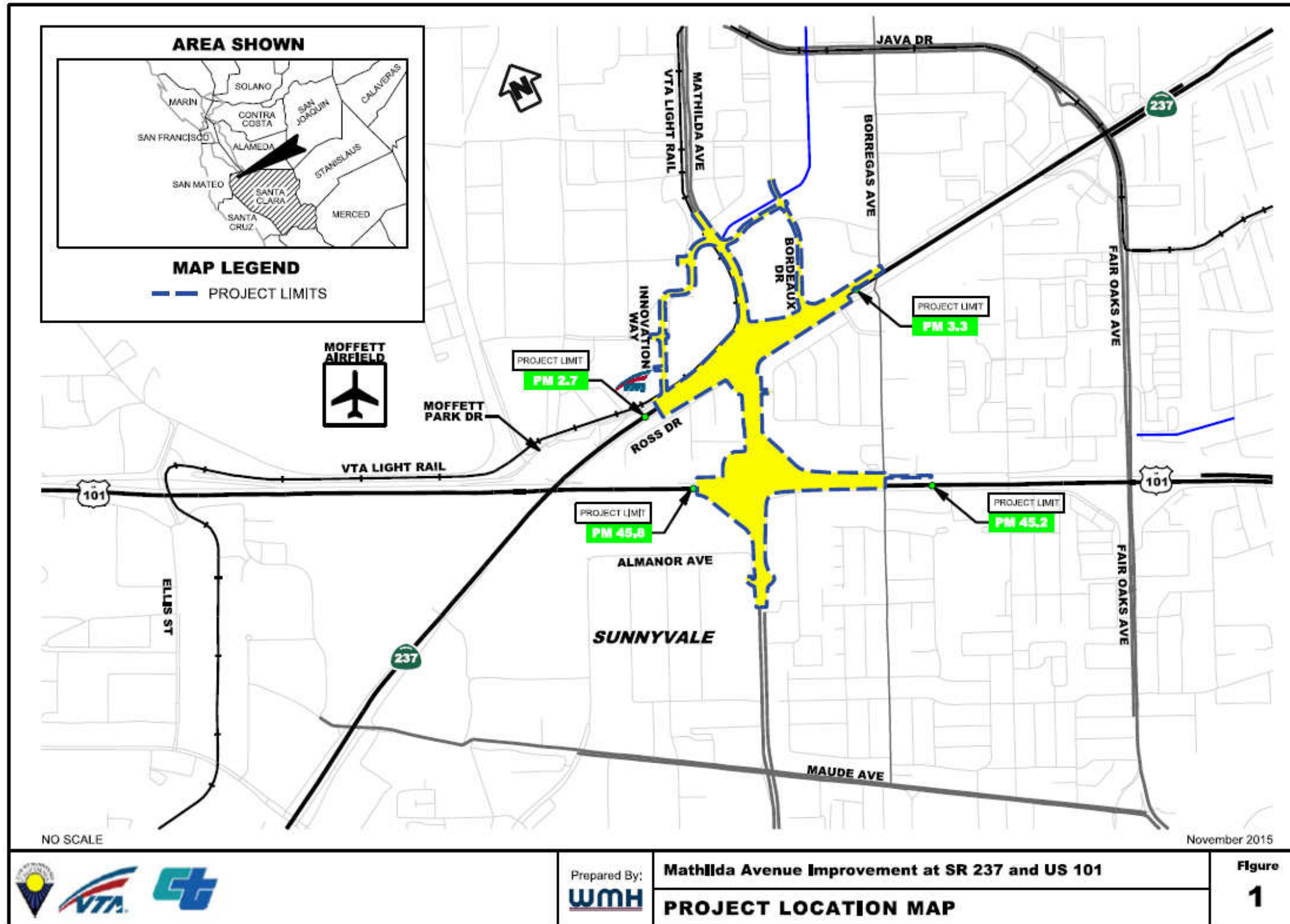


Figure 1. Project Location Map

Source: WMH Corporation

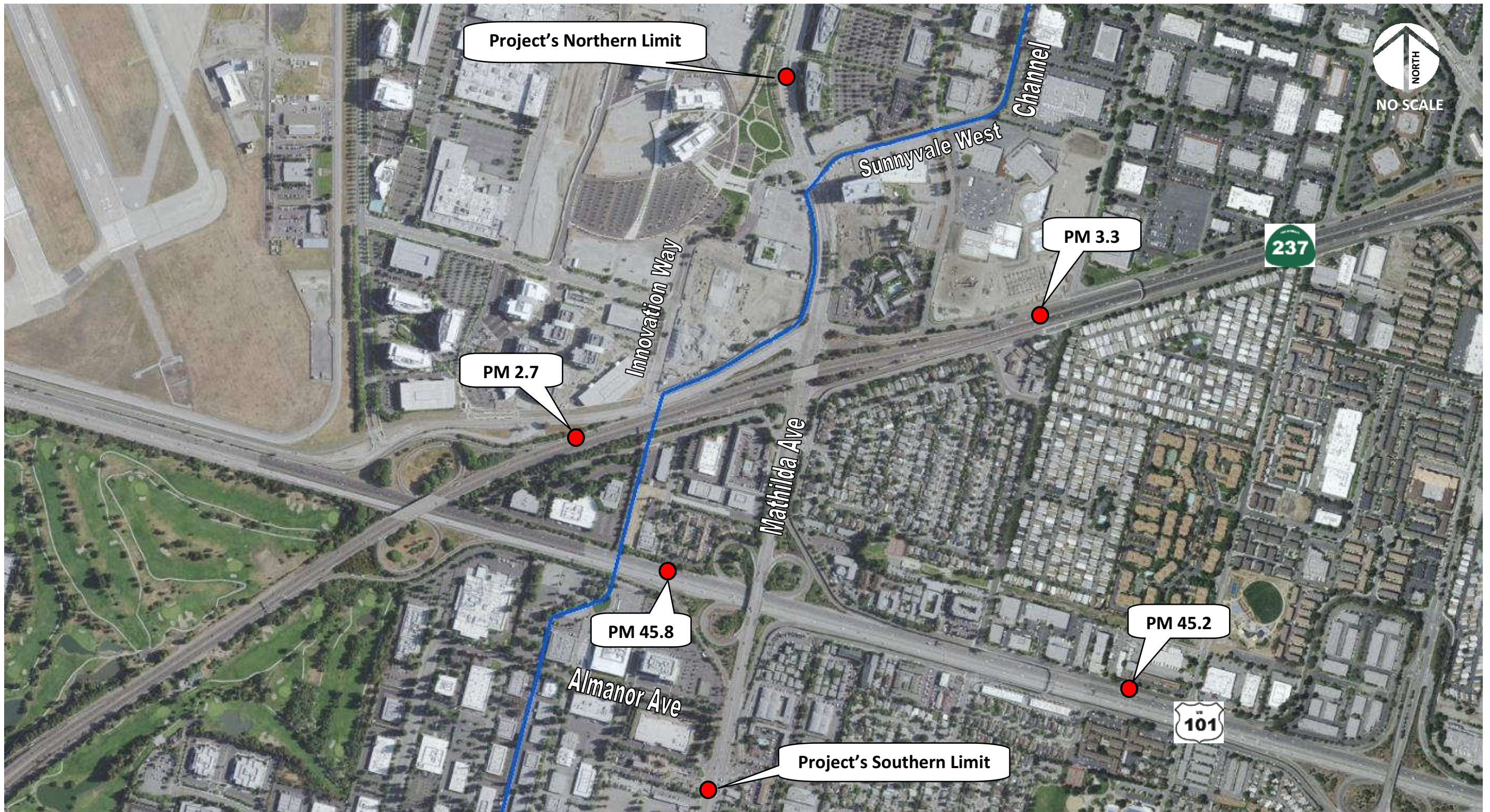
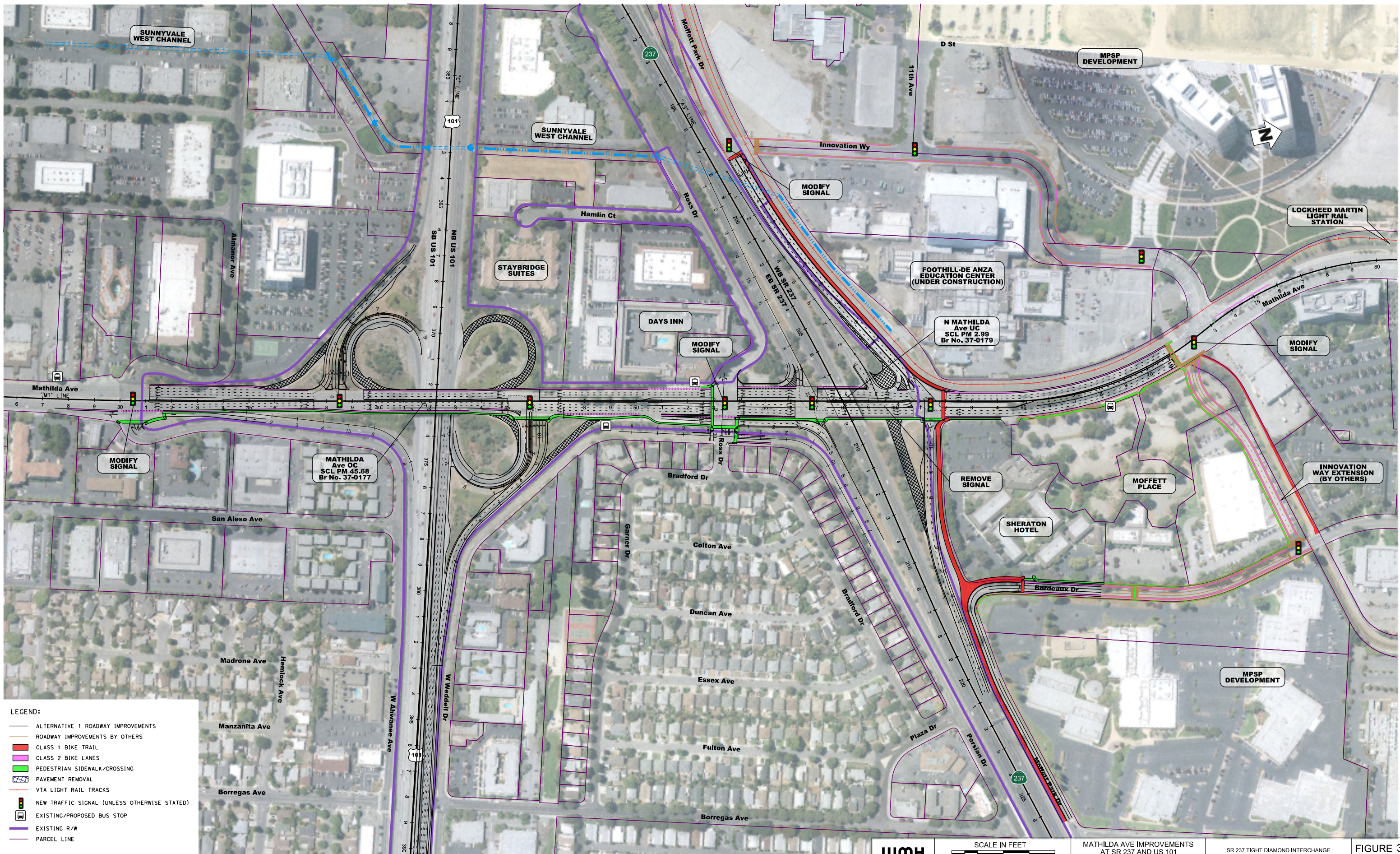
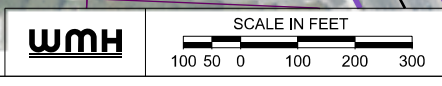


Figure 2. Project Vicinity Map

Source: Caltrans, Environmental System Research Institute (ESRI) and Santa Clara Valley Water District (SCVWD)



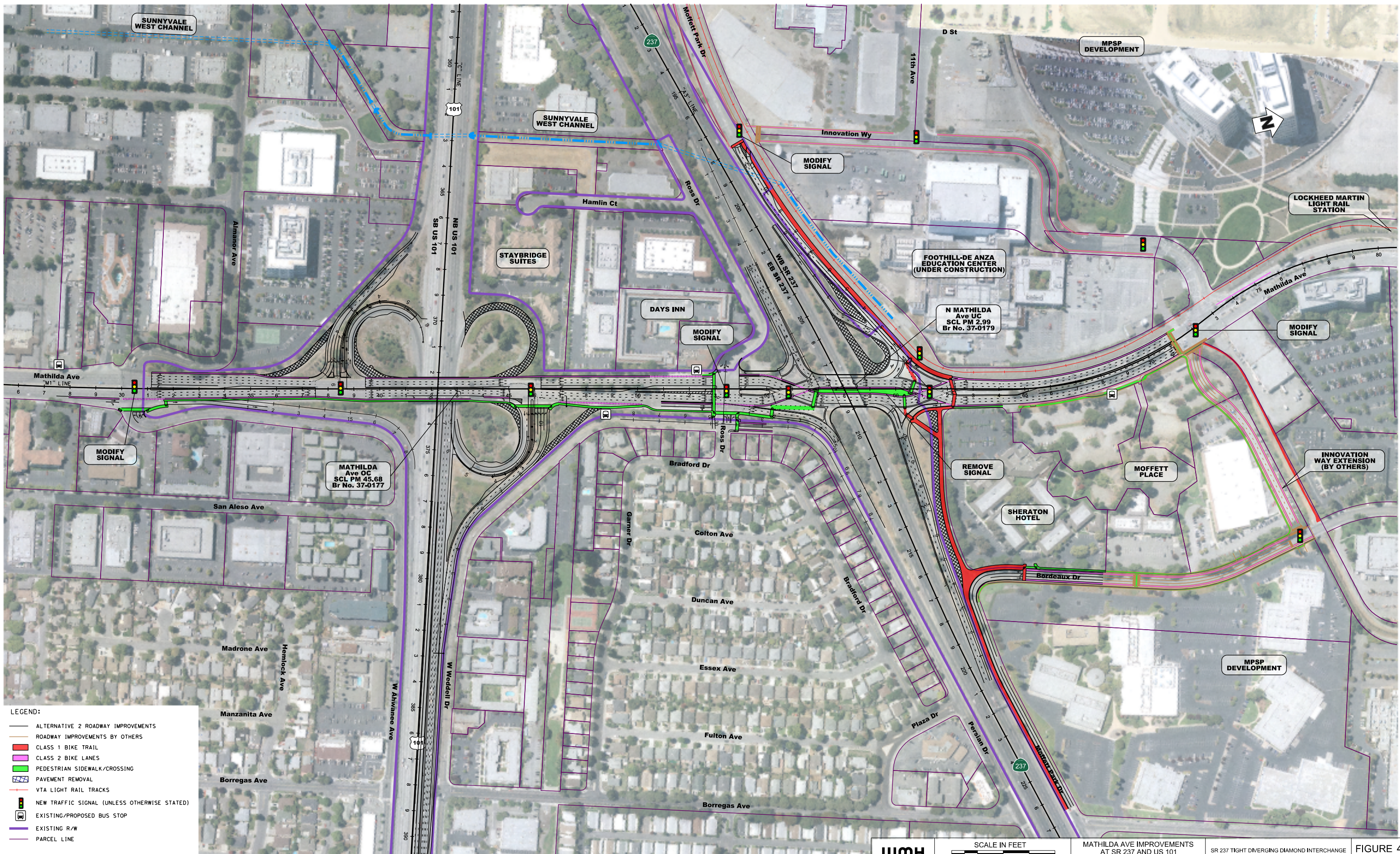
- LEGEND:**
- ALTERNATIVE 1 ROADWAY IMPROVEMENTS
 - ROADWAY IMPROVEMENTS BY OTHERS
 - CLASS 1 BIKE TRAIL
 - CLASS 2 BIKE LANES
 - PEDESTRIAN SIDEWALK/CROSSING
 - PAVEMENT REMOVAL
 - VTA LIGHT RAIL TRACKS
 - NEW TRAFFIC SIGNAL (UNLESS OTHERWISE STATED)
 - EXISTING/PROPOSED BUS STOP
 - EXISTING R/W
 - PARCEL LINE



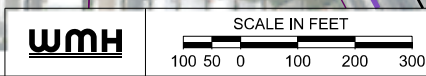
MATHILDA AVE IMPROVEMENTS
AT SR 237 AND US 101
SCL 237 - PM 2,7/3,3
SCL 101 - PM 45,4/45,8

SR 237 TIGHT DIAMOND INTERCHANGE
AND US 101 FULL PAR-CLO INTERCHANGE

FIGURE 3
NOV 2015



- LEGEND:**
- ALTERNATIVE 2 ROADWAY IMPROVEMENTS
 - ROADWAY IMPROVEMENTS BY OTHERS
 - CLASS 1 BIKE TRAIL
 - CLASS 2 BIKE LANES
 - PEDESTRIAN SIDEWALK/CROSSING
 - PAVEMENT REMOVAL
 - VTA LIGHT RAIL TRACKS
 - 🚦 NEW TRAFFIC SIGNAL (UNLESS OTHERWISE STATED)
 - 🚌 EXISTING/PROPOSED BUS STOP
 - EXISTING R/W
 - PARCEL LINE



MATHILDA AVE IMPROVEMENTS
AT SR 237 AND US 101
SCL 237 - PM 2,7/3,3
SCL 101 - PM 45,4/45,8

SR 237 TIGHT DIVERGING DIAMOND INTERCHANGE
AND US 101 FULL PAR-CLO INTERCHANGE

FIGURE 4
NOV 2015

1.2 Project Background

The SR 237/Mathilda Avenue and US 101/Mathilda Avenue interchanges are primary access points on the state highway system to the City of Sunnyvale and important local destinations such as downtown Sunnyvale, the Sunnyvale Caltrain Station to the south, and an expanding high-tech business district to the north. The Project is also located within the “Golden Triangle,” an area bordered by US 101, SR 237, and Interstate 880 (I-880) that includes parts of Sunnyvale, Santa Clara, North San Jose, and Milpitas. The Golden Triangle is named for the high concentration of employment centers, and US 101, SR 237, and I-880 are heavily used commute corridors to destinations within and beyond the Golden Triangle.

1.3 Regulatory Setting

This section summarizes the regulatory requirements associated with the floodplain that are mandated at federal, state, and local levels.

1.3.1 Executive Order 11988

Executive Order 11988 (Floodplain Management) directs all federal agencies to avoid, to the extent possible, long- and short-term adverse impacts associated with the occupancy and modification of floodplains, and to avoid direct and indirect support of floodplain development wherever there is a practicable alternative. Requirements for compliance are outlined in Title 23, Code of Federal Regulations, Part 650, Subpart A (23 CFR 650A) titled “Location and Hydraulic Design of Encroachment on Floodplains.”

If the preferred alternative involves significant encroachment onto the floodplain, the final environmental document (final Environmental Impact Statement or Finding of No Significant Impact) must include:

- The reasons why the proposed action must be located in the floodplain,
- The alternatives considered and why they were not practicable, and
- A statement indicating whether the action conforms to applicable State or local floodplain protection standards.

1.3.2 California’s National Flood Insurance Program

FEMA is the nationwide administrator of the National Flood Insurance Program (NFIP), which is a program that was established by the National Flood Insurance Act of 1968 to protect lives and property, and to reduce the financial burden of providing disaster assistance. Under the NFIP, FEMA has the lead responsibility for flood hazard assessment and mitigation, and it offers federally backed flood insurance to homeowners, renters, and business owners in communities that choose to participate in the program. FEMA has adopted the 100-year floodplain as the base flood standard for the NFIP. FEMA is also concerned with construction that would be within a 500-year floodplain for proposed projects that are considered “critical actions,” which are defined as any activities where even a slight chance of flooding is too great. FEMA issues Flood Insurance Rate Maps (FIRMs)

for communities that participate in the NFIP. These FIRMs present delineations of flood hazard zones.

In California, nearly all of the State's flood-prone communities participate in the NFIP, which is locally administered by the California Department of Water Resources' (DWR) Division of Flood Management. Under California's NFIP, communities have a mutual agreement with the State and federal government to regulate floodplain development according to certain criteria and standards, which is further detailed in the NFIP.

The Project is located within FIRM number 06085C0045H, as shown in Figure 5.

1.3.3 Santa Clara County Floodplain Data

Typically, each county (or community) has a Flood Insurance Study (FIS), which is used to locally develop FIRMs and Base Flood Elevations (BFEs). Santa Clara County's effective FIS identifies special flood hazard areas and other flood areas within unincorporated and incorporated areas of the county.

The Project is covered by FIS numbers 06085CV001B, 06085CV002B, 06085CV003B, and 06085CV004B.

1.4 Design Standards

This section presents the design standards relevant to the chance of flooding.

1.4.1 FEMA Standards

The FEMA standards are employed for design, construction, and regulation to reduce flood loss and to protect resources. Two types of standards are often employed: design criteria and performance standards.

A design criterion or specified standard dictates that a provision, practice, requirement, or limit be met; e.g., using the 100-year flood and establishing floodway boundaries so as not to cause more than a 1-foot increase in flood stages.

A performance standard dictates that a goal is to be achieved, leaving it to the individual application as to how to achieve the goal; e.g., providing protection to the regulatory flood, keeping post-development stormwater runoff the same as pre-development, or maintaining the present quantity and quality of water in a wetland.

The 100-year flood and floodplain have been adopted as a common design and regulatory standard in the United States. The NFIP adopted it in the early 1970s, and it was adopted as a standard for use by all federal agencies with the issuance of Executive Order 11988. States or local agencies are free to impose a more stringent standard within their jurisdiction.

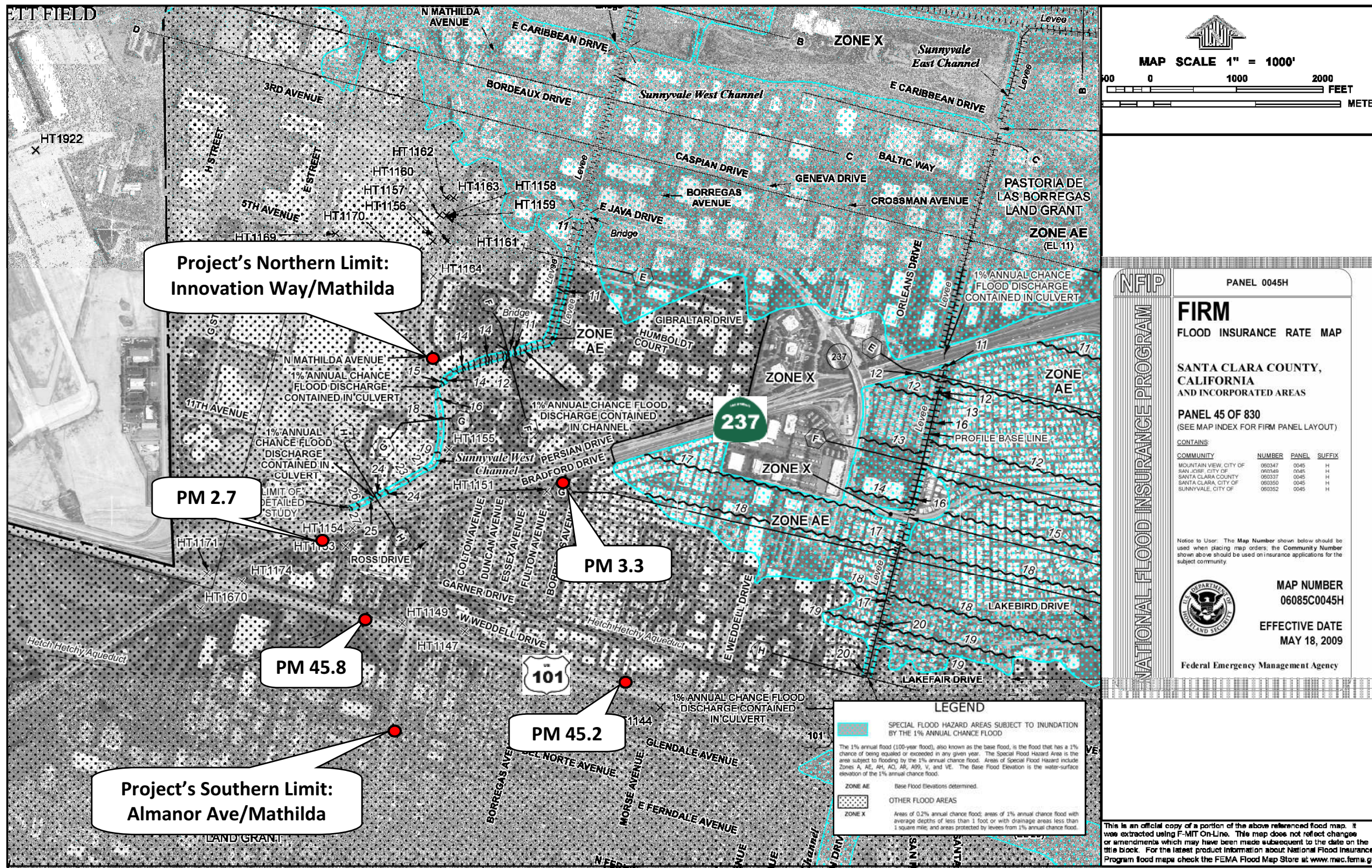


Figure 5. Flood Insurance Rate Map for the Project Area

Source: FEMA

2. AFFECTED ENVIRONMENT

This section describes the physical setting of the Project area. The Project limits cover approximately one mile along Mathilda Avenue between US 101 and SR 237 in the City of Sunnyvale, as well as the US 101 and SR 237 ramps and intersections with Mathilda Avenue.

2.1 Geographic Location

The geographic coordinates shown on the FEMA FIRMs and used in the FIS for Santa Clara County are referenced to the North American Datum of 1983 (NAD83).

2.2 Vertical Datum

The elevations shown in the FEMA FIRMs and FIS for Santa Clara County are referenced to the North American Vertical Datum of 1988 (NAVD88).

2.3 Creek, Stream, and River Crossings

Within the Project limits, Sunnyvale West Channel crosses SR 237 through a culvert at approximately PM 2.8 (see Figure 2). The channel also crosses Mathilda Avenue through a culvert approximately 100 feet south of Innovation Way. After crossing Mathilda Avenue, the channel becomes an open channel and flows northeast. Runoff from the Project is expected to be collected by the Caltrans or City of Sunnyvale stormwater drainage system instead of directly discharging to the channel at these crossings. Runoff from the Project would eventually discharge to San Francisco Bay. Figure 2 and Figure 6 show the location of the Sunnyvale West Channel within the Project vicinity.

2.4 Watershed Description

The Santa Clara Valley Urban Runoff Pollution Prevention Program (SCVURPPP) identifies the Project as being located within the Sunnyvale West Watershed (see Figure 7). The watershed has a drainage area of 7.6 square miles and is almost entirely urbanized.

The Sunnyvale West Channel is the receiving water body. The channel is approximately 3 miles in length. The channel originates from Maude Avenue as a concrete pipe culvert until it reaches Almanor Avenue in the northeastern direction. The channel becomes an earth-excavated channel from Almanor Avenue to Mathilda Avenue. The channel flows northeast to Guadalupe Slough via the Moffett Channel, and then ultimately drains to San Francisco Bay.

2.5 FEMA Floodplains

The FEMA FIRMs were researched for floodplain information. A Zone AE floodplain area is associated with Sunnyvale West Channel. FIRM number 06085C0045H identifies SR 237, US 101, and Mathilda Avenue in the Project limits as being within areas classified as shaded Zone X. The description of Zone AE in the Project vicinity is "1% annual chance flood discharge contained in channel." The description of shaded Zone X in this FIRM is "areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less

than 1 square mile; and areas protected by levees from 1% annual chance flood” (see Figure 5 and Figure 6 for the flood hazard areas).

Hydrologic Engineering Center data (HEC-2) for the Sunnyvale West Channel was obtained from the Santa Clara Valley Water District website. The results show that the 100-year flood is contained in the channel.

2.6 Traffic

The SR 237/Mathilda Avenue and US 101/Mathilda Avenue interchanges are primary access points on the state highway system for the City of Sunnyvale and important local destinations. US 101, SR 237, and I-880 are heavily used commute corridors to destinations within and beyond the Golden Triangle.

Mathilda Avenue is used for emergency supply and evacuation, emergency vehicle access, school buses, and mail delivery. Approximately 45,000 vehicles travel on Mathilda Avenue south of SR 237 on an average weekday, and traffic is projected to exceed 2,000 vehicles per hour during the AM and PM peak hours by 2040 per the Project Study Report-Project Development Support (WMH Corporation, 2015).

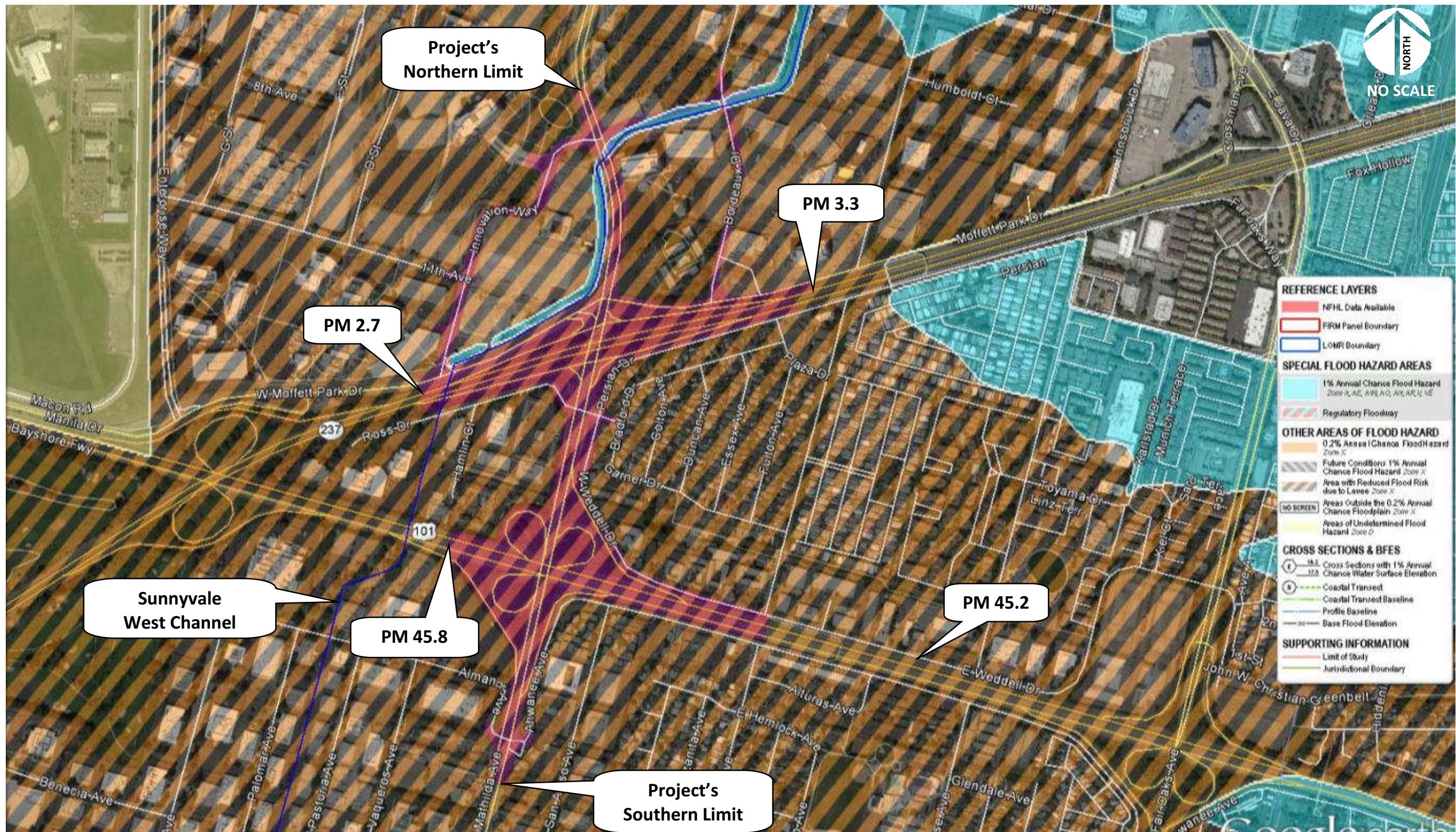


Figure 6. Stream and Floodplain in the Project Vicinity

Source: FEMA, Google Earth, Santa Clara County and WMH Corporation

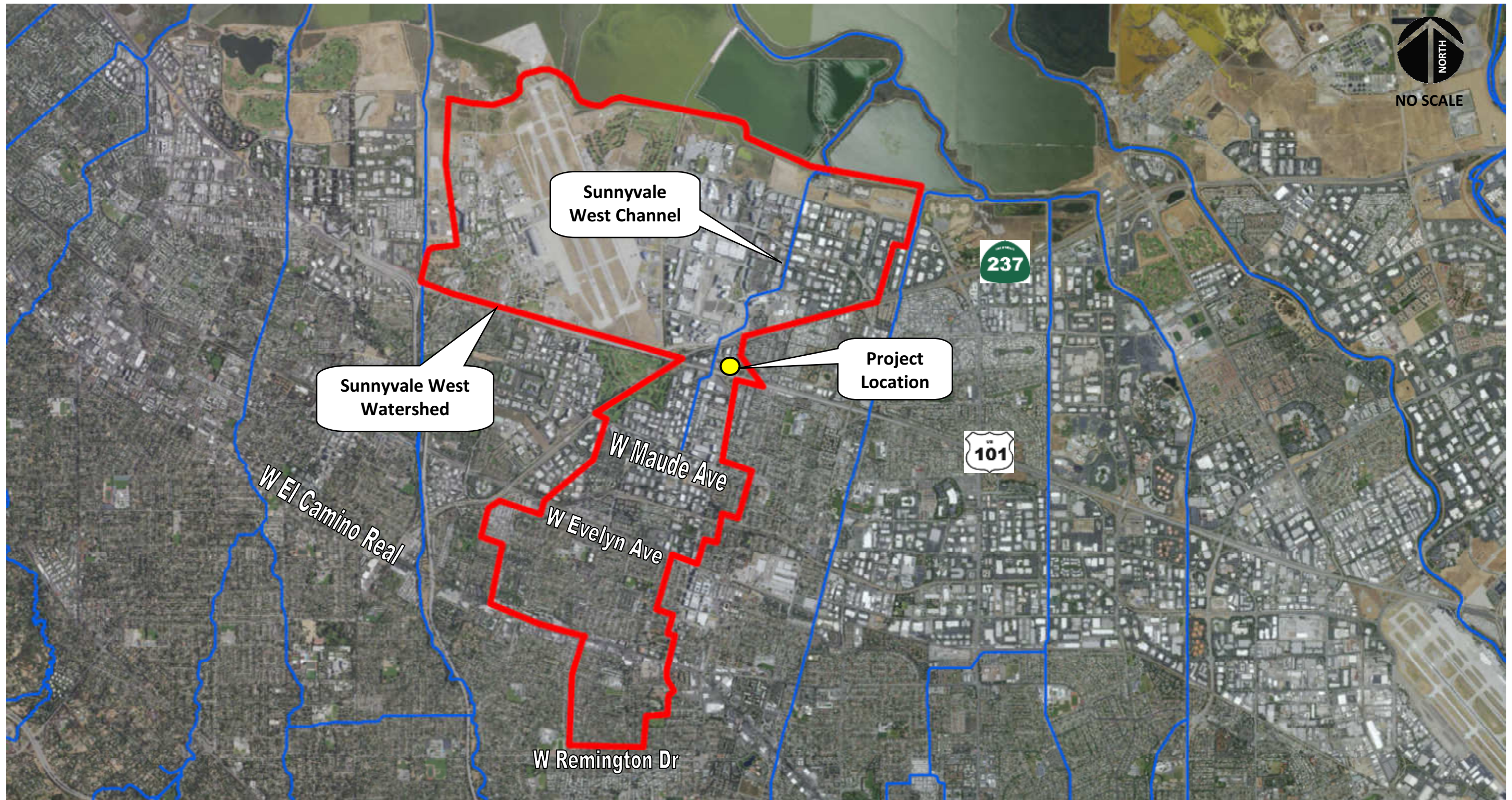


Figure 7. Sunnyvale West Watershed

Source: Santa Clara County

3. ENVIRONMENTAL CONSEQUENCES AND PROJECT IMPACTS

3.1 *Summary of Potential Encroachments*

The Federal Highway Administration (FHWA) defines a significant encroachment as a highway encroachment, and any direct support of likely development within the 100-year floodplain, that would involve one or more of the following construction or flood-related impacts: 1) significant potential for interruption or termination of a transportation facility that is needed for emergency vehicles or provides a community's only evacuation route; 2) a significant adverse impact on the natural and beneficial floodplain values; 3) support of probable incompatible floodplain development; or 4) longitudinal encroachments (1994).

3.1.1 Potential Traffic Interruptions

The Project's roadway improvements are outside of the 100-year floodplain. Practical detour routes are available, including on roads parallel to Mathilda Avenue, which would remain available during Project construction. Traffic interruptions are not anticipated.

3.1.2 Potential Impacts on Natural and Beneficial Floodplain Values

Natural and beneficial floodplain values include, but are not limited to: fish, wildlife, plants, open space, natural beauty, scientific study, outdoor recreation, agriculture, aquaculture, forestry, natural moderation of floods, water quality maintenance, and groundwater recharge.

Impacts to natural and beneficial floodplain values are not anticipated. The Project's roadway improvements are outside of the 100-year floodplain.

3.1.3 Support of Probable Incompatible Floodplain Development

As defined by the FHWA, the support of incompatible 100-year floodplain development will encourage, allow, serve, or otherwise facilitate incompatible 100-year floodplain development, such as commercial development or urban growth.

New access to undeveloped land would not be added with the Project improvements, and the Project would not support probable incompatible floodplain development.

3.1.4 Longitudinal Encroachments

As defined by the FHWA, a longitudinal encroachment is an action within the limits of the 100-year floodplain that is longitudinal to the normal direction of the floodplain. A longitudinal encroachment is "[a]n encroachment that is parallel to the direction of flow. Example: A highway that runs along the edge of a river is, usually considered a longitudinal encroachment." The requirement for consideration of avoidance alternatives must be included in a Location Hydraulic Study by including an evaluation and a discussion of the practicability of alternatives to any significant encroachment or any support of incompatible floodplain development.

Because the Project's roadway improvements are outside of the 100-year floodplain, and only minor improvements (e.g. signal modifications, restriping, etc.) are proposed within the Zone AE area, there are no longitudinal encroachments.

3.2 Risk Associated with Implementation of the Project

As defined by the FHWA, risk means the consequences associated with the probability of flooding attributable to an encroachment. It includes the potential for property loss and hazard to life during the service life of the bridge and roadway.

The potential risks associated with the implementation of the Project include a study of the following: 1) change in land use, 2) fill inside the floodplain, 3) change in the 100-year flood elevation, or 4) change in impervious surface area.

3.2.1 Change in Land Use

The Project would not result in changes to the existing land uses within the Project area or the surrounding areas. The Project proposes to improve the existing ramps and roadways; therefore, the area will remain a transportation corridor after Project completion. The areas surrounding the Project are currently developed with commercial and residential land uses, and the Project does not propose to change these land uses.

3.2.2 Fill Inside the Floodplain

The Project would result in fill; however, those cut and fill areas are not located within the 100-year floodplain, so no fill within the 100-year floodplain would result from the Project.

3.2.3 Change in the 100-Year Flood Elevation

No change in the 100-year flood elevation is expected as a result of the Project.

3.2.4 Change in Impervious Surface Area

Alternative 1 would add approximately 2 acres of impervious area, and Alternative 2 would add approximately 3 acres. However, given the size of the watershed (7.6-square-mile drainage area), the increase in impervious area from either alternative is not expected to impact the 100-year floodplain or 100-year flood elevations.

3.2.5 Summary of Risk

Based on the facts presented above, there is a low risk of floodplain impact associated with the Project.

4. AVOIDANCE, MINIMIZATION, AND/OR MITIGATION MEASURES

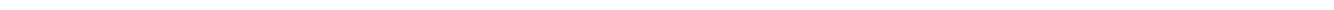
The Project would not result in floodplain impacts because all the major improvements in the Project are outside of the 100-year floodplain. The Project would increase the impervious area, but under either Build Alternative, the area would be small compared to the watershed and would not significantly increase flows or affect floodplain areas. In addition, downstream of the Sunnyvale

West Channel from Mathilda Avenue will be improved by the SCVWD proposed Sunnyvale East and West Channels Flood Protection Project. Therefore, no floodplain avoidance or minimization measures are considered, and mitigation measures are not required for this Project under either Build Alternative.

5. REFERENCES

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Appendix A Floodplain Evaluation Report Summary



FLOODPLAIN EVALUATION REPORT SUMMARY

Dist. 04 Co. SCL Rte. SR 237, US 101
P.M. 2.7/3.3, 45.2/45.8 EA: 04-4H2900 Bridge No. n/a
Federal-Aid Project Number: n/a

Limits:

On Mathilda Avenue, from Almanor Avenue to Innovation Way. On SR 237, from 0.3 miles south of the US 101/SR 237 Intersection (PM 2.7) to 0.3 miles east of the Mathilda Avenue overcrossing (PM 3.3). On US 101, from 0.3 miles south of Mathilda Avenue overcrossing (PM 45.2) to 0.3 miles south of SR 237/US 101 Interchange (PM 45.8).

Floodplain Description:

The Project is generally located within FEMA shaded Zone X. The FEMA FIRM has been identified this shaded Zone X areas as "areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood". The Zone AE areas associated with the Sunnyvale West Channel encompasses portions of the Innovation Way/Mathilda Avenue intersection, and has been identified in the FEMA FIRM as "1% annual chance flood discharge contained in culvert".

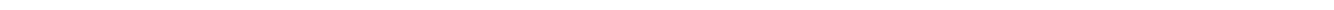
- | | No | Yes |
|---|----------|----------|
| 1. Is the proposed action a longitudinal encroachment of the base floodplain? | <u>X</u> | ___ |
| 2. Are the risks associated with the implementation of the proposed action significant? | <u>X</u> | ___ |
| 3. Will the proposed action support probable incompatible floodplain development? | <u>X</u> | ___ |
| 4. Are there any significant impacts on natural and beneficial floodplain values? | <u>X</u> | ___ |
| 5. Routine construction procedures are required to minimize impacts on the floodplain. Are there any special mitigation measures necessary to minimize impacts or restore and preserve natural and beneficial floodplain values? If yes, explain. | <u>X</u> | ___ |
| 6. Does the proposed action constitute a significant floodplain encroachment as defined in 23 CFR, Section 650.105(q). | <u>X</u> | ___ |
| 7. Are Location Hydraulic Studies that document the above answers on file? If not explain. | ___ | <u>X</u> |

PREPARED BY:

_____ *Date* _____
Local Agency/Consulting Project Engineer (*capital and 'on' system projects*)

_____ *Date* _____
Local Agency/Consulting Hydraulic Engineer (*local assistance projects*)

Appendix B Technical Information for Location Hydraulic Study



TECHNICAL INFORMATION FOR LOCATION HYDRAULIC STUDY

Dist. 04 Co. SCL Rte. SR 237, US 101
 P.M. 2.7/3.3, 45.2/45.8 EA: 04-4H2900 Bridge No. n/a
 Federal-Aid Project Number: n/a

Floodplain Description:

The Project is generally located within FEMA shaded Zone X. The FEMA FIRM has been identified this shaded Zone X areas as “areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood”. The Zone AE areas associated with the Sunnyvale West Channel encompasses portions of the Innovation Way/Mathilda Avenue intersection, and has been identified in the FEMA FIRM as “1% annual chance flood discharge contained in culvert”.

1. Description of Proposal (include any physical barriers i.e. concrete barriers, soundwalls, etc. and design elements to minimize floodplain impacts)

The Project proposes to reconfigure lanes on Mathilda Avenue and modify the US 101/Mathilda Avenue and SR 237/Mathilda Avenue interchanges. The proposed improvements included modification to on- and off-ramps; removal, addition, and signalization of intersections, provision of new left-turn lanes. In addition, the Project would include new bicycle and pedestrian facilities, utility relocations, new storm water treatment facilities, new safety lighting, ramp metering modifications, modification of overhead signage, and new retaining wall.

2. ADT: Current 45,000 Projected 48,000 (2040)

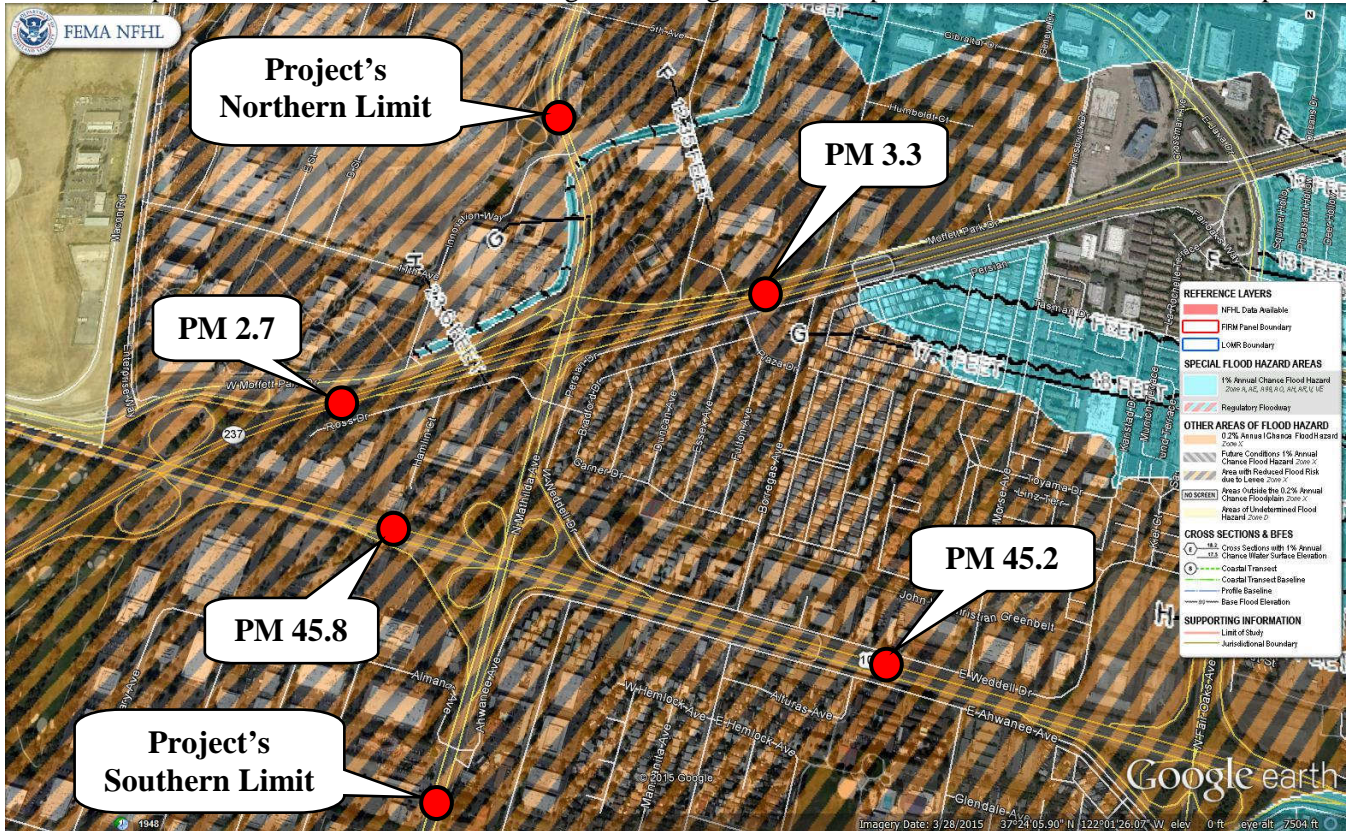
3. Hydraulic Data:

Base Flood: $Q_{100} =$ 360 cfs $WSE_{100} =$ 16 ft (NAVD 88)
 The flood of record, if greater than Q_{100} $Q =$ n/a cfs $WSE =$ _____
 Overtopping flood $Q =$ n/a cfs $WSE =$ _____

Are NFIP maps and studies available? NO _____ YES X

4. Is the highway location alternative within a regulatory floodway? NO X YES _____

5. Attach map with flood limits outlined showing all buildings or other improvements within the base floodplain.



Dist. 04 Co. SCL Rte. SR 237, US 101
 P.M. 2.7/3.3, 45.2/45.8 EA: 04-4H2900 Bridge No. n/a
 Federal-Aid Project Number: n/a

Potential Q100 backwater damages:

- A. Residences? NO X YES _____
- B. Other Bldgs? NO X YES _____
- C. Crops? NO X YES _____
- D. Natural and beneficial Floodplain values? NO X YES _____

"Natural and beneficial flood-plain values" shall include but are not limited to fish, wildlife, plants, open space, natural beauty, scientific study, outdoor recreation, agriculture, aquaculture, forestry, natural moderation of floods, water quality maintenance, and groundwater recharge.

6. Type of Traffic:

- A. Emergency supply or evacuation route? NO _____ YES X
- B. Emergency vehicle access? NO _____ YES X
- C. Practicable detour available? NO _____ YES X
- D. School bus or mail route? NO _____ YES X

7. Estimated duration of traffic interruption for 100-year event hours: n/a

8. Estimated value of Q100 flood damages (if any) – moderate risk level.

- A. Roadway \$ n/a
- B. Property \$ n/a
- Total \$ n/a

9. Assessment of Level of Risk Low X
 Moderate _____
 High _____

For High Risk projects, during design phase, additional Design Study Risk Analysis may be necessary to determine design alternative.

PREPARED BY:

Signature:

I certify that I have conducted a Location Hydraulic Study consistent with 23 CFR 650 and that the information summarized in items numbers 3, 4, 5, 7, and 9 of this form is accurate.

_____ Date _____
 Local Agency/Consulting Hydraulic Engineer (local assistance projects)

Is there any longitudinal encroachment, significant encroachment, or any support of incompatible Floodplain development? NO X YES _____

If yes, provide evaluation and discussion of practicability of alternatives in accordance with 23 CFR 650.113

Information developed to comply with the Federal requirement for the Location Hydraulic Study shall be retained in the project files.

I certify that item numbers 1, 2, 6 and 8 of this Location Hydraulic Study Form are accurate and will ensure that Final PS&E reflects the information and recommendations of said report:

_____ Date _____
 Local Agency/Consulting Project Engineer (local assistance projects)



Prepared by

FEHR & PEERS

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Mathilda Avenue Improvements at SR 237 and US 101

**Final
Traffic Operations
Analysis and Report**

Final

Traffic Operations Analysis Report: Mathilda Avenue Improvements between SR 237 and US 101 Project

**Prepared for:
VTA
Caltrans
City of Sunnyvale**

June 2016

SJ13-1460

FEHR  PEERS

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1. INTRODUCTION

The primary goal of the Mathilda Avenue at SR 237 and US 101 Project is to reduce congestion and improve traffic operations within project limits on Mathilda Avenue between SR 237 and US 101 while improving mobility for all travel modes in the area.

Regional growth, local development, and constrained geometrics have resulted in substantial traffic congestion on Mathilda Avenue, a main arterial roadway providing access into and out of downtown Sunnyvale and development to the north of SR 237. Without efficient access to these locations, the economic vitality and sustainability of Sunnyvale is adversely affected. Mathilda Avenue between SR 237 and US 101 currently carries approximately 2,500 and 2,700 vehicles during peak direction in the AM and PM peak hour, respectively. Traffic demand on SR 237 at Mathilda Avenue has increased in the past several years due to regional and local land use development. Continued growth in traffic demand in the study area would exacerbate congestion levels thereby adversely affecting mobility and safety. The purpose of this project is to reduce congestion and improve traffic operations on Mathilda Avenue between SR 237 and US 101 while considering enhanced mobility for all travel modes in the area. The scope and scale of the project is intended to provide locally-scaled transportation improvements in the near term that address multiple existing deficiencies in a cost-effective manner.

PURPOSE OF REPORT

The purpose of this Traffic Operations Analysis Report (TOAR) is to present existing and anticipated future transportation conditions for Mathilda Avenue at SR 237 and US 101. The results contained in this report serve as the basis for the traffic operations section of the Project Approval/Environmental Document (PA/ED) and associated Environmental Impact Report (EIR) being completed pursuant to the California Environmental Quality Act (CEQA). The Santa Clara Valley Transportation Authority (VTA) and the City of Sunnyvale are proceeding with an EIR for the following reasons:

- Under the Build Alternatives, traffic from the closure of Moffett Park Drive would be diverted to a new access point to be construction at Mathilda Avenue and Innovation Way. Based on the past studies, the Mathilda Avenue/Innovation Way intersection in the Year 2025 is predicted to operate at Level of Service (LOS) F in the PM peak hour. This intersection exceeds the Congestion Management Program threshold of LOS E and mitigation may not be feasible due to potential right-of-way impacts.
- Right-of-way concerns for the project include acquisition of a private road (Innovation Way) and loss of access to a private business (Sheraton Hotel).
- The project considers two Build Alternatives to be equally analyzed. One of the alternatives includes a diverging diamond-style interchange, an innovative design potentially subject to additional scrutiny.
- Under an EIR, a more robust public outreach process is required that will assure potential issues of concern by the public and other stakeholders are identified, documented, and considered in the analysis.



- The City has been challenged several times on the basis of CEQA adequacy in past project efforts, most notably the Mary Avenue Extension Project, which is located in the same general area as the project.
- The City of Sunnyvale is the local sponsor of the project, and the City Council has stated preference for an EIR.

The scope and scale of the project is intended to provide locally-scaled transportation improvements in the near term that address multiple existing deficiencies. The Santa Clara VTA, the City of Sunnyvale, and Caltrans District 4 are collaborating to advance this project through the approval process. Conditions are described for all travel modes, including automobiles, trucks, bicycles, pedestrians and surface transit. However, the primary focus of this report is on the expected automobile traffic operations that would result from implementation of the proposed project with bicycle and pedestrian facilities and transit services qualitatively discussed under Existing Conditions.

Prior to this TOAR, the project team completed the Alternatives Analysis and Project Initiation phases of the project. Caltrans approved the Project Study Report – Project Development Support (PSR / PDS) in February 2015.

PROJECT DESCRIPTION

The project is located within the City of Sunnyvale in Santa Clara County, California. The project proposes to improve local roadway operations on Mathilda Avenue in the City of Sunnyvale from Almanor Avenue and the US 101 / Mathilda Avenue interchanges. Two build alternatives are analyzed in this Report. Build Alternative 1 would modify westbound SR 237 ramps to provide a diamond configuration. Build Alternative 2 would modify Mathilda Avenue and SR237 ramps to provide a diverging diamond configuration.

The Build Alternatives would consist of the following roadway improvements:

- Provision of three continuous through lanes in each direction of Mathilda Avenue.
- Removal of the northbound US 101 loop off-ramp and shifting of traffic to the northbound US 101 diagonal off-ramp.
- Realignment and widening of the northbound ramps and signalize ramp intersection with Mathilda Avenue and construct a left-turn lane on southbound Mathilda Avenue to access the northbound US 101 on-ramp.
- Realignment of southbound US 101 off-ramp and loop on-ramp and signalization of the ramp intersection with Mathilda Avenue.
- Modification of the Mathilda / Ross Drive signalized intersection.
- Closure of Moffett park Drive between Bordeaux Drive and Mathilda Avenue and shifting traffic to Bordeaux Drive and Innovation Way.
- Removal of westbound SR 237 ramp signal intersection; realignment of westbound SR 237 off-ramp outside Moffett Park Drive and modification of the signalized intersection.



In general, proposed bicycle and pedestrian improvements in the project area would be consistent with the City of Sunnyvale 2006 Bicycle Plan and the Santa Clara Countywide Bicycle Plan (August 2008) and would include the following components:

- Upgrading existing pedestrian facilities to incorporate Americans with Disabilities Act (ADA) standards including curb ramps to all crosswalks.
- Incorporating pavement delineation with new crosswalk markings.
- Installation of pedestrian countdown signals.
- Realignment and signalizations of ramp termini to provide new pedestrian crossings, where feasible.
- Bicycle improvements on Moffett Park Drive would consist of a Class I bicycle path between Bordeaux Drive and Mathilda Avenue.
- Bicycle improvements on Mathilda Avenue will consider Class II bicycle lanes based on available pavement widths and provision of pedestrian facilities within the project limits, and would connect to the existing Class III bicycle route north of Innovation Way.

Under the No Build Alternative, no changes would be made to the existing local roadways or freeway system within the project limits.

REPORT ORGANIZATION

The report is organized into the following sections:

Data Collection and Analysis Methodology – Chapter 2 presents the study area, data collection and operational analysis methodologies.

Existing Conditions – Chapter 3 presents the existing physical and operational characteristics of the transportation system within the study area.

Travel Demand Forecasts – Chapter 4 presents future year (2018 and 2040) peak period traffic forecasts for the study area.

Year 2018 Traffic Operations Analysis – Chapter 5 presents year 2018 traffic operations analysis results.

Year 2040 Traffic Operations Analysis – Chapter 6 presents year 2040 traffic operations analysis results.

Traffic Analysis Summary – Chapter 7 presents an overall summary of the traffic operations analysis results.



2. DATA COLLECTION AND ANALYSIS METHODOLOGY

This chapter presents the study area, data collection and operational analysis methodologies. It is consistent with that presented in the updated final methodology memorandum dated August 2015 on study assumptions, methodologies and approach.

STUDY AREA

The study area is located within the City of Sunnyvale in Santa Clara County, California. It includes Mathilda Avenue between Almanor Avenue-Ahwanee Avenue and Fifth Avenue, including the interchanges at SR 237 and US 101. **Figure 1** illustrates the transportation analysis study area, which is generally bounded by Fifth Avenue to the north, Almanor Avenue-Ahwanee Avenue to the south, Fair Oaks Avenue to the east, and northbound US 101 on ramp at Moffett Park Drive to the west. This study evaluates the following intersections:

- 1) Mathilda Avenue/Fifth Avenue
- 2) Mathilda Avenue/Innovation Way
- 3) Mathilda Avenue/Moffett Park Drive/SR 237 WB Ramps
- 4) Mathilda Avenue/SR 237 EB Ramps
- 5) Mathilda Avenue/Ross Drive
- 6) Mathilda Avenue/US 101 NB Ramps (Build intersection)
- 7) Mathilda Avenue/US 101 SB Ramps (Build intersection)
- 8) Mathilda Avenue/Ahwanee Avenue-Almanor Avenue
- 9) US 101 NB On-Ramp/Moffett Park Drive
- 10) Innovation Way/Moffett Park Drive
- 11) Innovation Way/Eleventh Avenue (unsignalized)
- 12) Innovation Way/Juniper Networks Driveway (unsignalized)
- 13) Bordeaux Drive/Innovation Way (future intersection)

In addition, this study evaluates the following freeway mainline segments:

- 1) SR 237
 - a. Lawrence Expressway to Fair Oaks Avenue
 - b. Fair Oaks Avenue to Mathilda Avenue
 - c. Mathilda Avenue to US 101 Ramps
 - d. US 101 Ramps to Maude Avenue
- 2) US 101
 - a. Lawrence Expressway to Fair Oaks Avenue
 - b. Fair Oaks Avenue to Mathilda Avenue
 - c. Mathilda Avenue to SR 237 Ramps
 - d. SR 237 Ramps to Ellis Street





W:\San Jose N Drive\Projects\SJ13_Projects\SJ13_1460_Mathilda_Interchange\Graphics\ADOBE\Fig_1_Study_Intersections

- Study Intersections
- Freeway Study Segment



Figure 1
Vicinity Map
Mathilda Avenue Improvements

DATA COLLECTION

Extensive traffic and transportation data collection efforts were undertaken between 2013 and 2015 to determine existing peak hour traffic volumes, truck percentages, lane configurations, travel times throughout the corridor and mainline segments, and queues on key roadways within the study area. Existing and proposed pedestrian/bicycle facilities were identified and transit service information for routes within the area was also collected.

LOCAL STREET SYSTEM TRAFFIC DATA

Weekday intersection turning movement, pedestrian and bicycle counts were conducted during the morning (7:00 AM to 9:00 AM) and evening (4:00 PM to 7:00 PM) peak periods at six of the study intersections in November 2013. The remainder of the intersections use count data that was collected on the dates presented in **Table 2-1** during the morning and evening peak periods on a typical weekday. All counts were conducted while schools were in session.

TABLE 2-1: INTERSECTION COUNT DATES

| | Intersection | Count Date |
|----|---|-------------------|
| 1 | Mathilda Avenue/Fifth Avenue | 11/13/2013 |
| 2 | Mathilda Avenue/Innovation Way | 11/13/2013 |
| 3A | Mathilda Avenue/Moffett Park Drive | 2/12/2013 |
| 3B | Mathilda Avenue/SR 237 WB Ramps | 11/13/2013 |
| 4 | Mathilda Avenue/SR 237 EB Ramps | 11/13/2013 |
| 5 | Mathilda Avenue/Ross Drive | 2/12/2013 |
| 6 | Mathilda Avenue/US 101 NB Diagonal Off-Ramp | 11/13/2013 |
| | Mathilda Avenue/US 101 NB Loop Off-Ramp/On-Ramp | 11/13/2013 |
| 7 | Mathilda Avenue/US 101 SB Loop On-Ramp | 11/13/2013 |
| | Mathilda Avenue/US 101 SB Diagonal Off-Ramp/On-Ramp | 11/13/2013 |
| 8 | Mathilda Avenue/Ahwanee Avenue-Amanor Avenue | 2/13/2013 |
| 9 | US 101 NB On-Ramp/Moffett Park Drive | 2/12/2013 |
| 10 | Innovation Way/Moffett Park Drive | 11/18/2014 |
| 11 | Innovation Way/Eleventh Avenue (unsignalized) | 5/27/2015 |
| 12 | Innovation Way/Juniper Networks Driveway (unsignalized) | 5/27/2015 |
| 13 | Bordeaux Drive/Innovation Way (future intersection) | 5/27/2015 |

Source: Fehr & Peers, 2016.

Peak hour volumes, intersection controls, and lane configurations for the study intersections are shown in **Figure 2**. The peak hour volumes presented reflect minor adjustments to the raw traffic counts to ensure balanced vehicle trips between adjacent intersections.



The peak hour volumes presented reflect adjustments to the raw traffic counts to ensure balanced vehicle trips between closely spaced intersections. Intersection turning movement volumes were balanced among the study intersections for use in the Synchro/SimTraffic model. The ramp intersections were adjusted in the Synchro/SimTraffic model to account for peak hour traffic demand. The raw traffic count data is presented in **Appendix A**.

LOCAL STREET SYSTEM TRAVEL SPEED DATA

Travel speed data along the Mathilda Avenue corridor was obtained from GPS travel-time surveys on November 21, 2013. Travel speeds along Mathilda Avenue indicate excessive congestion among the closely spaced intersection on Mathilda Avenue near SR 237 in the morning and evening peak period.

For validation purposes along Mathilda Avenue, the GPS travel-time surveys were used to verify travel time and congestion along the Mathilda Avenue corridor in the model.

MAINLINE AND RAMP COUNTS

Year 2013 mainline counts and HOV percentages along US 101 and SR 237 were developed from the following sources and as seen in **Table 2-2**:

- US 101 Express Lanes Project – Existing Conditions and Model Calibration Report, dated January 16, 2013, prepared by DKS
- Phase II of the SR 237 Express Lanes Project – Existing Conditions Traffic Report, dated August 14, 2013, prepared by DKS
- Caltrans 2013 Census Data, received in September 2015

Ramp volumes were primarily based on the Caltrans 2013 census data received in September 2015 or based on traffic counts collected at the ramp terminal intersections from 7:00AM to 9:00AM and from 4:00PM to 7:00PM.



TABLE 2-2: STUDY AREA COUNT DATA SOURCES

| Data Source | Study Location |
|---|--|
| Intersection Turning Movement – February 2013, November 2013, May 2015 | All study intersections during the AM and PM peak periods. |
| Daily Volumes – November 2013 | Twenty-four hour tube counts were performed at the following locations: <ul style="list-style-type: none"> • Mathilda Avenue between Innovation Way and Moffett Park Drive • Mathilda Avenue between Ross Drive and US 101 • Mathilda Avenue between US 101 and Almanor Avenue-Ahwanee Avenue • Moffett Park Drive between Innovation Way and Mathilda Avenue • Moffett Park Drive between Mathilda Avenue and Bordeaux Drive |
| Mainline Counts/Bottlenecks – November 2013 | SR 237 mixed-flow and HOV lane counts were collected at the pedestrian over-crossing between the Mathilda Avenue and Fair Oaks Avenue interchanges. |
| US 101 Express Lanes Project | US 101 HOV percentages. US 101 northbound mainline count volume prior to the Lawrence Expressway ramps. |
| Caltrans 2013 Census Data | US 101 ramp counts between Lawrence Expressway and Ellis Street. US 101 southbound mainline count at the SR 237 interchange. |
| Phase II of the SR 237 Express Lanes Project | SR 237 freeway count/demand volumes prior to the Fair Oaks Avenue off-ramp (westbound) and prior to the Maude Avenue on-ramp (eastbound). |

Source: Fehr & Peers, 2016.

SR 237 Mainline and Ramp Volumes

SR 237 Count Volumes

Mainline traffic count volumes presented in Phase II of the SR 237 Express Lanes Study were used to determine Year 2013 mainline count volumes within the study area.

Traffic counts performed at the ramps as part of Phase II of the SR 237 Express Lanes Study was used at all ramp locations with the exception of the Mathilda Avenue ramps. Mathilda Avenue volumes were determined using the turning movement counts performed in November 2013 along the Mathilda Avenue corridor.

The raw traffic count data is presented in **Appendix A**.

SR 237 Demand Volumes

Year 2013 demand volumes along the SR 237 mainline were taken directly from Phase II of the SR 237 Express Lanes Study at the locations where counts performed (just west of the US 101 interchange for eastbound and just west of Lawrence Expressway for westbound). Ramp demand volumes were taken directly from Phase II of the SR 237 Express Lanes Study with the exception of the Mathilda Avenue ramps.

In order to determine the Year 2013 demand volume at the Mathilda Avenue ramps, the counts performed in November 2013 and the demand estimated in Phase II of the SR 237 Express Lanes Study were compared



to determine the appropriate demand. To be the most conservative along the Mathilda Avenue corridor, the maximum volume between these two sources was used as the estimated demand volume for the Mathilda Avenue ramps. Mainline volumes were then balanced upstream and downstream of the count location using the ramp demand volumes.

SR 237 mainline and ramp peak period demand volumes are shown on **Figure 3A** and **Figure 4A** for morning and evening peak hours, respectively. **Table 2-2** presents the data sources for the study area ramps and mainline segments.

US 101 Mainline and Ramp Volumes

US 101 Count Volumes

Caltrans provided Year 2013 traffic census counts at all of the ramps within the study area. This data was used at all ramp locations with the exception of the Mathilda Avenue ramps and the SR 237 interchange. Mathilda Avenue volumes were determined using the turning movement counts performed in November 2013 along the Mathilda Avenue corridor. In most cases, the turning movement counts resulted in higher ramp volumes than the census count data provided by Caltrans. The SR 237 interchange volumes were determined based on the traffic counts presented in Phase II of the SR 237 Express Lanes Study which uses counts from March-April 2013.

For southbound US 101 mainline, Caltrans also provided a 2013 traffic census count located just north of the SR 237 off-ramp. Mainline volumes at other mainline segments were estimated by subtracting off-ramp volumes and adding on-ramp volumes.

The US 101 Express Lanes Study presents Year 2011 traffic count data within the study area for northbound US 101. For northbound US 101 mainline, data from the US 101 Express Lanes study was used and a growth rate was applied. In order to be consistent with Year 2013 data used for other portions of US 101, a growth factor of 2.4 and 4.2 percent was applied to the Year 2011 AM and PM peak period traffic count data, respectively. These growth factors were derived by comparing 2011 counts from the US 101 Express Lanes Project, 2011 and 2013 Performance Measurement System (PeMS) data, and Caltrans 2013 census data for the AM and PM peak periods to account for average traffic growth rates between 2011 and 2013.

The raw traffic count data is presented in **Appendix A**.

US 101 Demand Volumes

Northbound AM and southbound PM mainline demand volumes were estimated by calculating the difference between the count and the demand presented in the US 101 Express Lanes Study and then applying that difference to the Year 2013 mainline count. This was done in order to account for queues that exist in these peak directions. Southbound AM and northbound PM mainline demand volumes were set equal to the count because Year 2013 observations showed there were no mainline queues in the non-peak directions.



Ramp demand volumes were estimated by calculating the difference between the count and the demand presented in the US 101 Express Lanes Study and then applying that difference to the Year 2013 count with the exception of the SR 237 interchange and the Mathilda Avenue ramps. In order to maintain consistency in volumes at the US 101/SR 237 interchange, the demand volumes at the SR 237 interchange were determined from Phase II of the SR 237 Express Lanes Study. These volumes were counted in 2013 as part of Phase II of the SR 237 Express Lanes Study. Demand was estimated using field observations performed for that analysis.

To determine the demand volume at the Mathilda Avenue ramps, the counts performed in November 2013 and the demand estimated in the US 101 Express Lanes Study were compared to determine the appropriate demand. To be the most conservative along the Mathilda Avenue corridor, the maximum volume between these two sources was used as the estimated demand volume for the Mathilda Avenue ramps. Mainline volumes were then balanced upstream and downstream of the count location using the ramp demand volumes.

US 101 mainline and ramp peak period demand volumes are shown on **Figure 3B** and **Figure 4B** for morning and evening peak hours, respectively. **Table 2-2** presents the data sources for the study area ramps and mainline segments.

Occupancy Data

High-occupancy vehicle (HOV) lanes exist along both directions of US 101 in the study area and on SR 237 in the eastbound direction starting approximately 700 feet east of the Mathilda Avenue on-ramp.

HOV percentages for US 101 were based on data presented in the US 101 Express Lanes Study.

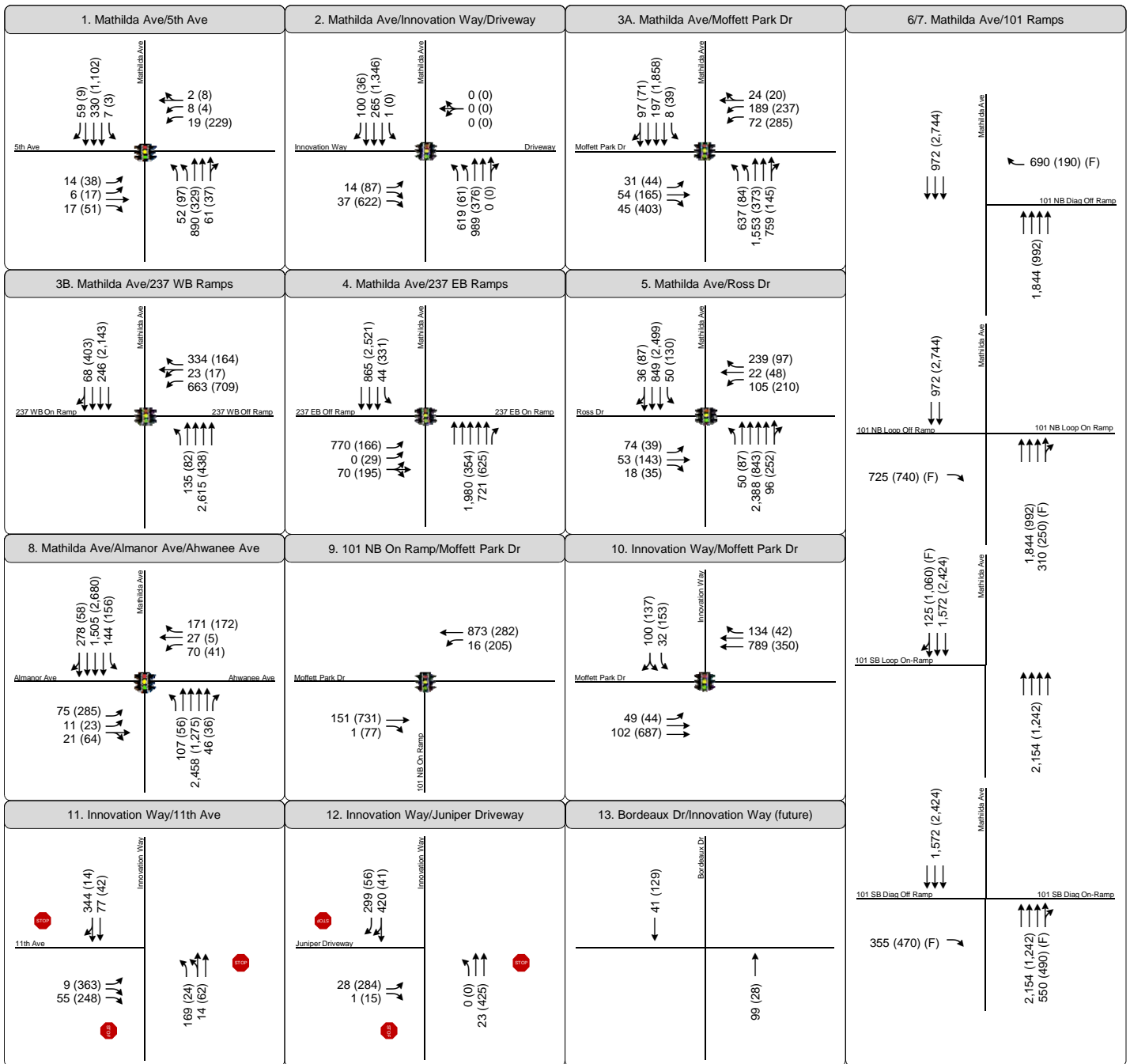
A mid-week manual AM and PM peak period (7:00 AM to 9:00 AM and 4:00 PM to 7:00 PM) traffic count was collected on November 13, 2013 at the pedestrian overcrossing between the Mathilda Avenue and Fair Oaks Avenue interchanges to determine HOV and mixed-flow volumes in queue along SR 237. The eastbound count indicates that HOVs represent eight and 26 percent of the morning and evening peak period traffic, respectively. **Table 2-3** summarizes the percent of traffic that travels within the HOV lanes for both freeways.

TABLE 2-3: MAINLINE AVERAGE PERCENT HOVS

| Segment | AM Peak Period Percentage (%) | PM Peak Period Percentage (%) |
|-------------------|-------------------------------|-------------------------------|
| Northbound US 101 | 17 | 13 |
| Southbound US 101 | 17 | 20 |
| Westbound SR 237 | No HOV | No HOV |
| Eastbound SR 237 | 8 | 26 |

Source: US 101 Express Lanes Project, January 2013; Fehr & Peers, November 2013.

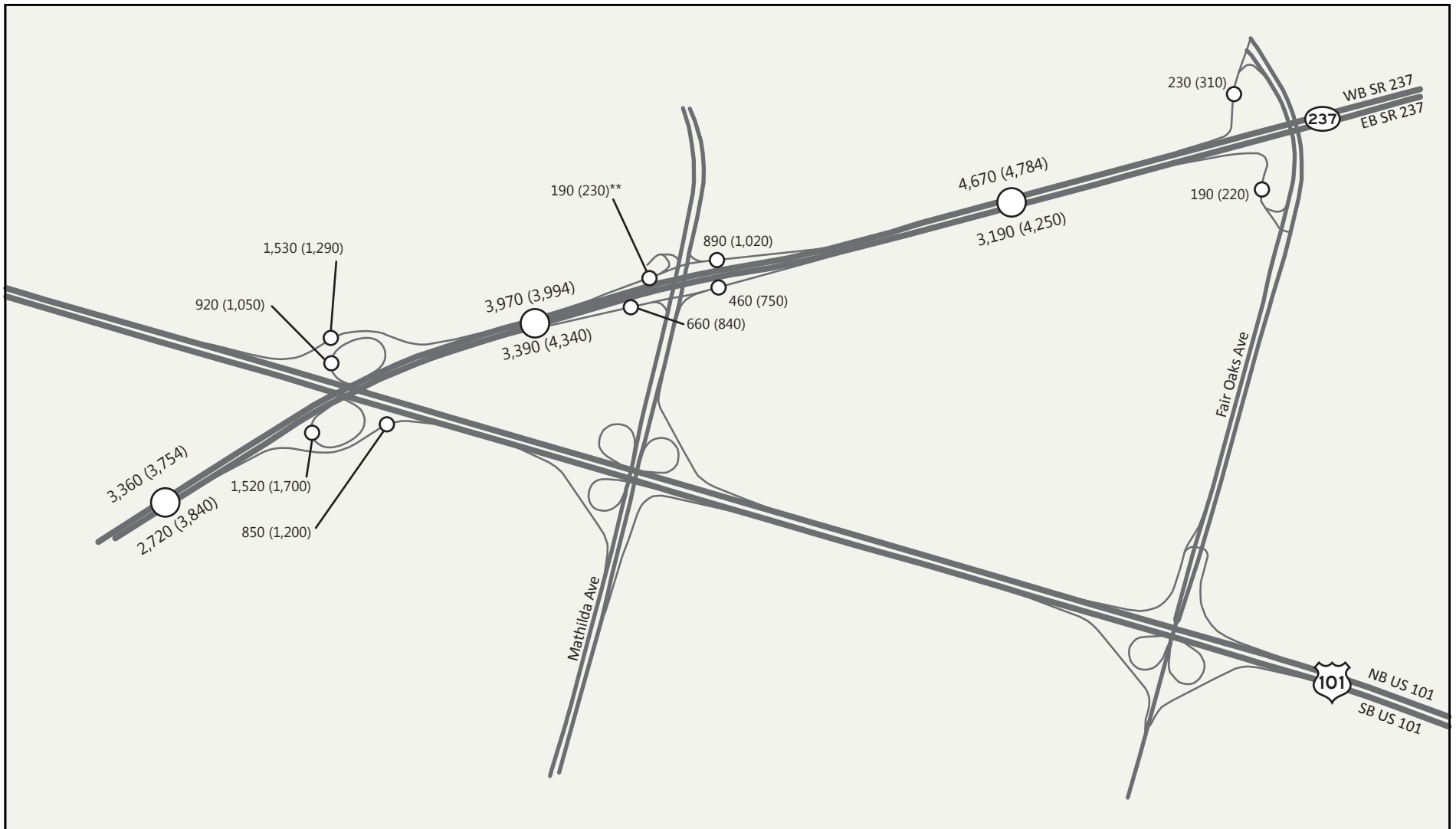




(##) - AM(PM) Peak Hour Demand Volumes
(F) - Unsignalized (free) Movement

Figure 2
Mathilda Interchange Project
Existing (2013) Intersection Demand Peak
Hour Volumes and Lane Configurations





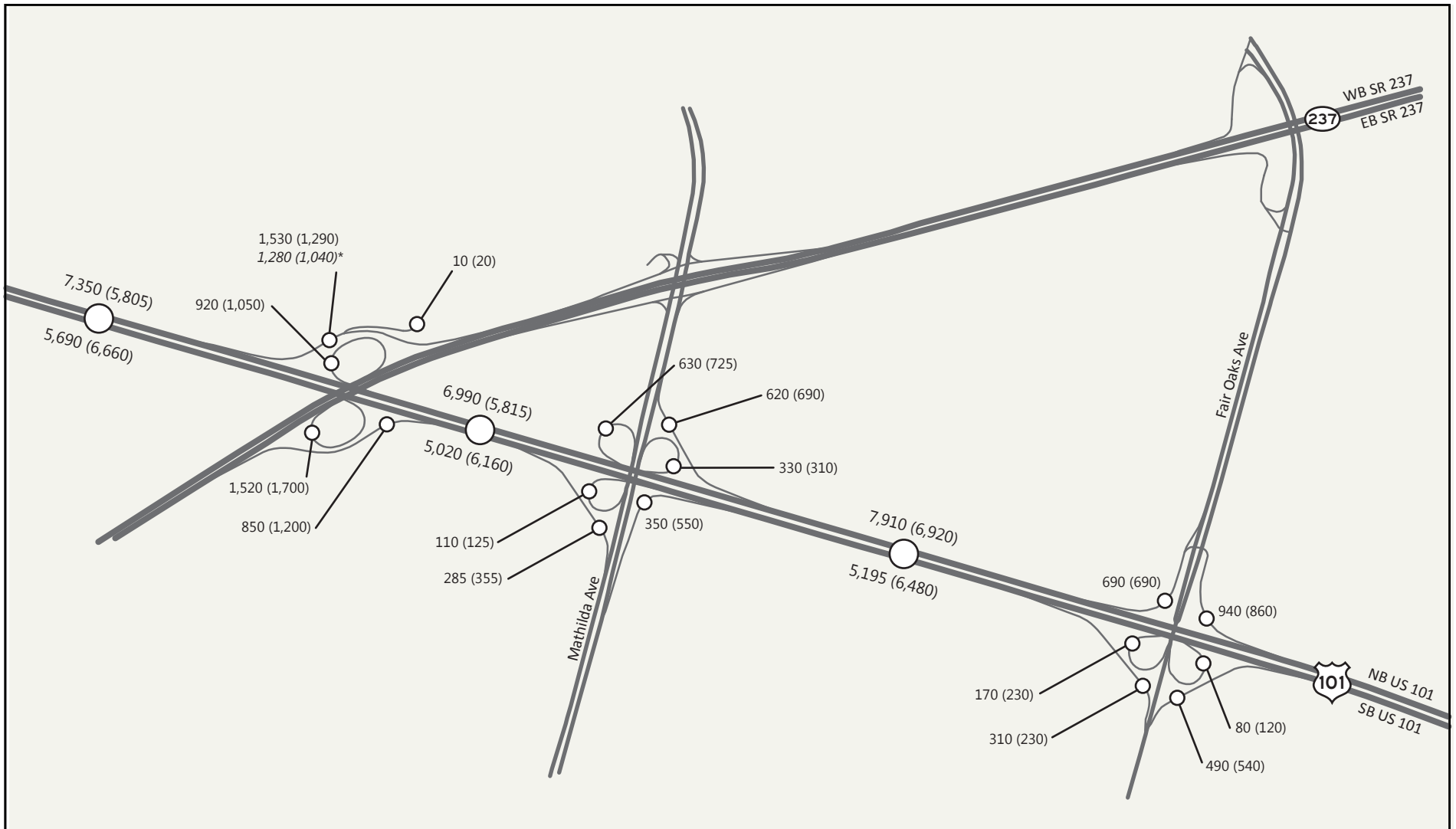
○ 7:00 AM (8:00 AM) Segment/Ramp Volume Location

** Ramp volume may not match ramp terminal intersection due to slip ramp form Moffett Park Drive.

Figure 3A

Mathilda Interchange Project
 Freeway and Ramp Demand Volumes - State Route 237
 Existing (2013) AM Peak Period





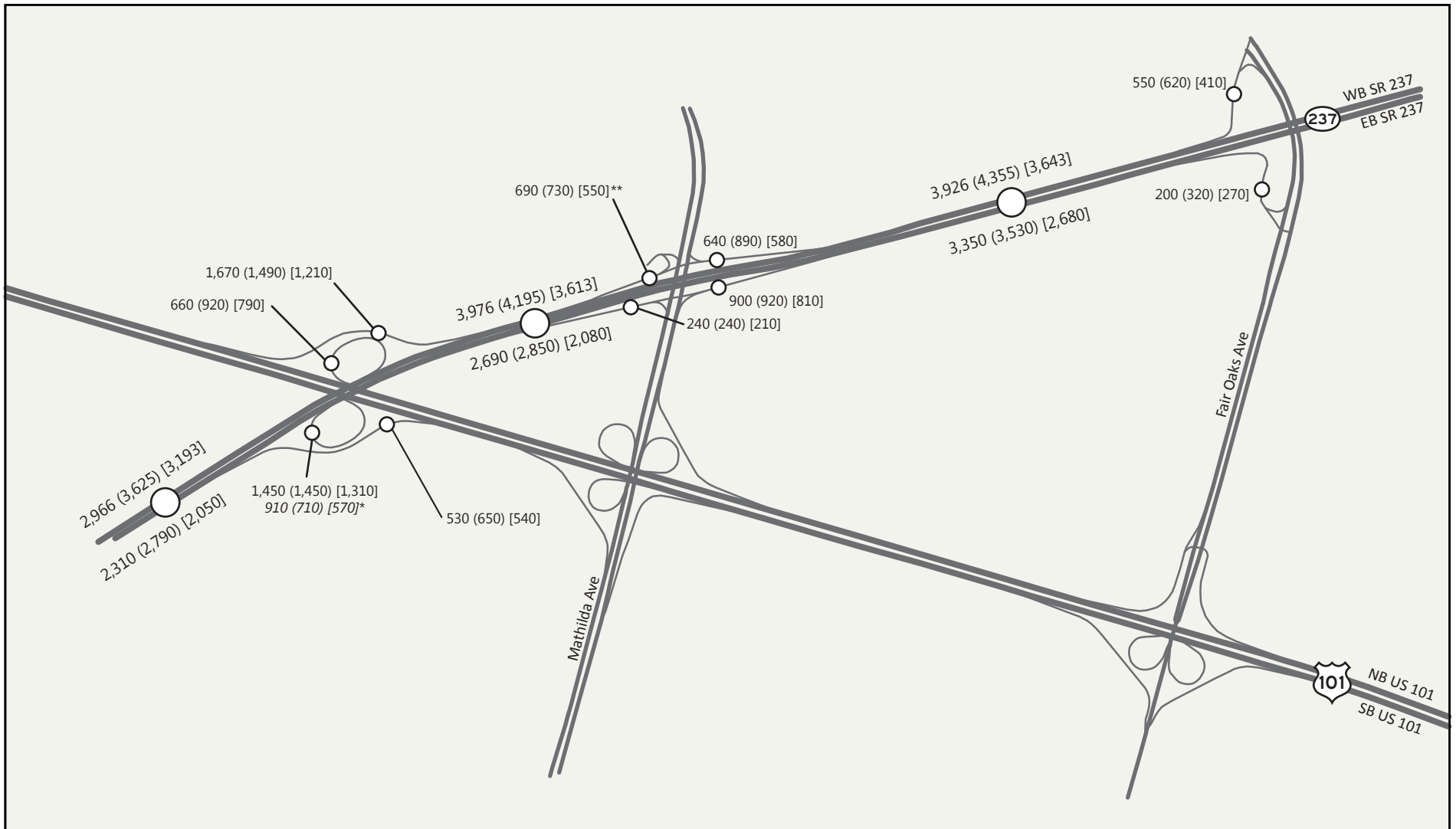
○ 7:00 AM (8:00 AM) Segment/Ramp Volume Location

* The constrained on-ramp demand is shown in italics and reflects the condition that not all of the off-ramp unconstrained demand is delivered downstream due to congestion.

Figure 3B

Mathilda Interchange Project
 Freeway and Ramp Demand Volumes - US Route 101
 Existing (2013) AM Peak Period





○ 4:00 PM (5:00 PM) [6:00 PM] Segment/Ramp Volume Location

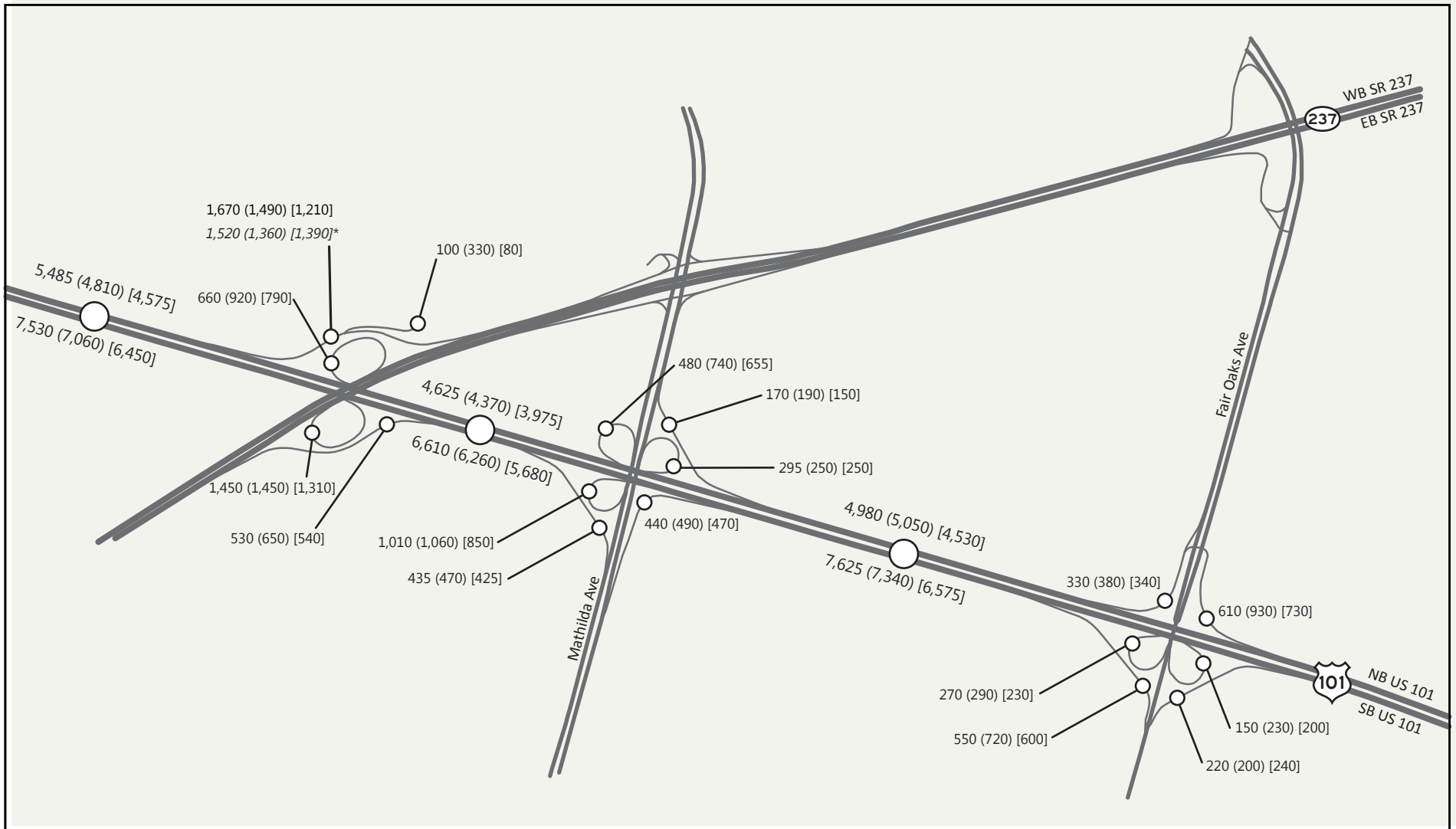
* The constrained on-ramp demand is shown in italics and reflects the condition that not all of the off-ramp unconstrained demand is delivered downstream due to congestion.

** Ramp volume may not match ramp terminal intersection due to slip ramp from Moffett Park Drive.

Figure 4A

Mathilda Interchange Project
 Freeway and Ramp Demand Volumes - State Route 237
 Existing (2013) PM Peak Period





○ 4:00 PM (5:00 PM) [6:00 PM] Segment/Ramp Volume Location

* The constrained on-ramp demand is shown in italics and reflects the condition that not all of the off-ramp unconstrained demand is delivered downstream due to congestion.

Figure 4B

Mathilda Interchange Project
 Freeway and Ramp Demand Volumes - US Route 101
 Existing (2013) PM Peak Period



MAINLINE TRAVEL SPEED DATA

Mainline travel speed data for the study corridor was obtained from both GPS travel-time surveys and the INRIX database. INRIX provides a traffic flow archive with the capability to capture speeds reported at the segment level for specific days and times of day. INRIX data is gathered from a variety of sources, including in-vehicle GPS systems, mobile smart phones, and roadway sensors.

Mainline travel speeds along the SR 237 and US 101 study corridors were obtained using the INRIX database for November 21, 2013. Fehr & Peers also performed AM and PM peak period floating-car travel time surveys on November 21, 2013 along both directions of SR 237 and US 101 within the study area. Fehr & Peers compared the INRIX speed data for November 21, 2013 to various other weekdays in November 2013 to confirm that bottlenecks and observed queues represent a typical weekday condition. Travel speeds along westbound SR 237 and northbound US 101 indicate that there was congestion during the morning peak period due to a downstream bottleneck on US 101 near the SR 85 and Shoreline Boulevard ramps that causes spillback onto US 101 and SR 237 within the study area. Observations indicate that vehicle queues occasionally also spill back onto westbound SR-237 during the morning peak period. Southbound US 101 experienced congestion during the PM peak period due to a downstream bottleneck at De La Cruz Boulevard and Trimble Road ramps that causes spillback on US 101 within the study area.

For validation purposes along SR 237, the travel time runs presented in Phase II of the SR 237 Express Lanes Study were used. The travel times presented in the express lanes report match the volumes presented in the report, which are the volumes that were used for purposes of this analysis. Although our travel times were used for comparison purposes with INRIX data, the travel time runs from Phase II of the SR 237 Express Lanes Study were used for FREQ validation because they were completed at the same time that mainline and ramp counts were conducted.

For validation purposes along US 101, the travel time runs performed between Lawrence Expressway and Ellis Street on November 21, 2013 were used.

Detailed speed and travel time data by segment for the AM and PM peak periods is provided in **Appendix B** and **Appendix C** for US 101 and SR 237, respectively. **Table 2-4** and **Table 2-5** provides peak period travel speed and time summaries for SR 237 and US 101 within the study area.



TABLE 2-4: EXISTING US 101 MAINLINE AVERAGE WEEKDAY TRAVEL TIMES AND SPEEDS

| Time Period | Northbound US 101 ¹ | | Southbound US 101 ² | |
|-----------------------|--------------------------------|---------------------|--------------------------------|---------------------|
| | Average Time (min:sec) | Average Speed (mph) | Average Time (min:sec) | Average Speed (mph) |
| AM Peak Period | | | | |
| 7:00 AM to 8:00 AM | 06:33 | 20 | 02:17 | 55 |
| 8:00 AM to 9:00 AM | 05:26 | 24 | 02:13 | 57 |
| PM Peak Period | | | | |
| 4:00 PM to 5:00 PM | N/A | N/A | 08:13 | 15 |
| 5:00 PM to 6:00 PM | 03:31 | 37 | 10:20 | 12 |
| 6:00 PM to 7:00 PM | 02:20 | 56 | 07:27 | 17 |

Notes:

1. Travel time and speed are reported between Fair Oaks Avenue and just north of SR 237 On-Ramp.
2. Travel time and speed are reported between just north of SR 237 and half way between Fair Oaks Avenue and Lawrence Expressway.

Source: Fehr & Peers, November 2013.

TABLE 2-5: EXISTING SR 237 MAINLINE AVERAGE WEEKDAY TRAVEL TIMES AND SPEEDS

| Time Period | Westbound SR 237 ¹ | | Eastbound SR 237 ² | |
|-----------------------|-------------------------------|---------------------|-------------------------------|---------------------|
| | Average Time (min:sec) | Average Speed (mph) | Average Time (min:sec) | Average Speed (mph) |
| AM Peak Period | | | | |
| 7:00 AM to 8:00 AM | 02:36 | 51 | 02:00 | 62 |
| 8:00 AM to 9:00 AM | 02:00 | 65 | 02:24 | 62 |
| PM Peak Period | | | | |
| 4:00 PM to 5:00 PM | 02:06 | 63 | 02:00 | 62 |
| 5:00 PM to 6:00 PM | 03:36 | 37 | 02:12 | 62 |
| 6:00 PM to 7:00 PM | 02:30 | 53 | 02:12 | 62 |

Notes:

1. Travel time and speed are reported between Lawrence Expressway On-Ramp and just west of US 101 On-Ramp. Observations indicate that AM peak period travel speeds on westbound SR 237 are occasionally lower than reported in this table, due to queue spillbacks from the downstream bottleneck on northbound US 101 at Shoreline Boulevard.
2. Travel time and speed are reported between west of US 101 Off-Ramp and Lawrence Expressway Off-Ramp.

Source: Phase II of the SR 237 Express Lanes, August 2013.

MATHILDA CORRIDOR TRAVEL SPEED DATA

Travel time surveys were performed on northbound and southbound Mathilda Avenue during the AM peak period and PM peak period on Tuesday, November 23, 2013. The surveys were collected using Global Positioning Systems (GPS) data logger units. **Table 2-6** presents the travel time for each direction and peak period. Based on the data collected, the peak direction is northbound in the AM peak period and southbound in the PM peak period. Travel time run information can be found in **Appendix D**.



TABLE 2-6: EXISTING MATHILDA AVENUE AVERAGE WEEKDAY TRAVEL TIMES AND SPEEDS¹

| Time Period | Northbound Mathilda Avenue | | Southbound Mathilda Avenue | |
|--------------|----------------------------|---------------------|----------------------------|---------------------|
| | Average Time (min:sec) | Average Speed (mph) | Average Time (min:sec) | Average Speed (mph) |
| AM Peak Hour | 04:17 | 23 | 04:12 | 20 |
| PM Peak Hour | 05:15 | 17 | 05:00 | 17 |

Notes:

1. Travel time and speed are reported between just north of San Aleso Avenue and just south of Java Drive.

Source: Fehr & Peers, 2013.

FIELD OBSERVATIONS

Field observations of traffic congestion and queues were conducted during the AM and PM peak periods in November 2013 while local schools were in session and during the same period that intersection traffic counts were collected. These field observations were supplemented by additional observations performed in July 2015 for the Mathilda Avenue corridor. Below is a summary of the major queues observed in the study area.

Mathilda Avenue Observations

In the morning peak period, majority of traffic was observed traveling northbound on Mathilda Avenue. The SR 237 westbound off-ramp was observed to queue beyond the turn pockets and the SR 237 eastbound ramp had queues that extended to approximately the end of the turn pockets. Moffett Park Drive had few queues except in the northbound direction which was observed to steadily have vehicles queued between the Moffett Park Drive and SR 237 Westbound Ramps intersections. No queues were observed at any of the US 101 ramps during the morning peak period. Despite the large volume of traffic traveling northbound, traffic queues that formed at the four closely spaced intersection surrounding the SR 237 ramps typically dissipated during the green phase of each signal cycle.

In the evening peak period, eastbound queues at Moffett Park Drive extended to the Innovation Way intersection. Majority of vehicles turned right onto southbound Mathilda Avenue and a smaller portion turned right onto westbound SR 237 ramps. Westbound Moffett Park Drive had queues that extended out of pocket. SR 237 ramps had some queues but generally did not experience the same volume as the morning peak period. At the intersection of Mathilda Avenue and Innovation Way, the eastbound queue extended past the Juniper Networks Driveway during cycles when VTA light rail was entering the intersection. The queue would remain around the Juniper Networks Driveway during all other cycles. Vehicles traveling southbound on Mathilda Avenue were observed to back up to Innovation Way occasionally. In the evening peak period, no excessive queue spillback was observed at the US 101 ramps.

US 101 Observations

In the northbound direction, traffic was observed to travel at less than free-flow speed in the morning throughout the study segments due to general congestion throughout the mainline. In the AM peak period,



a bottleneck was observed to begin north of the Ellis Street interchange and extend to south of the Lawrence Expressway interchange. No other on- or off-ramps were observed to cause excessive queuing onto the freeway mainline.

In the southbound direction, traffic was observed to travel at less than free-flow speed in the evening throughout the study segments due to general congestion throughout the mainline. In the PM peak period, a bottleneck that exists south of the study segments was observed to spill back throughout the study segments. The queues began to decrease after 6pm, but still remained throughout most of the study network. No other on- or off-ramps were observed to cause excessive queuing onto the freeway mainline.

SR 237 Observations

In the morning peak period, there was little to no congestion throughout the study segments. A majority of the congestion occurred in the westbound direction at the US 101 interchange. Vehicles attempting to merge into the backed-up US 101 northbound auxiliary lane caused excessive queues to back up past the Mathilda Avenue ramps. In addition, westbound SR 237 vehicles continuing past the US 101 interchange continued to travel slowly as the US 101 northbound loop on-ramp has very little merging distance and vehicles from the ramp are entering SR 237 at slower speeds.

In the evening peak period, the SR 237 eastbound mixed-flow lanes were observed to have some congestion east of the study mainline segments that continued to worsen later in the peak period, but was not observed to adversely affect the study mainline segments. The eastbound HOV lane was observed to move at free-flow speeds through the study segments. The westbound direction continued to see congestion starting at the US 101 northbound ramps that backed up to around the Mathilda Avenue ramps.

ROADWAY SYSTEM AND ANALYSIS METHODOLOGY

The traffic operations analysis methodologies and key assumptions for intersections and mainline facilities are described below.

INTERSECTIONS

Traffic operations for the study area were analyzed using the Synchro/SimTraffic 8.0 software program. Synchro/SimTraffic is based on procedures outlined in the Transportation Research Board's *2010 Highway Capacity Manual (HCM)*. Use of the SimTraffic simulation model allows the study area to be analyzed as an interconnected roadway network, which is useful to accurately analyze vehicle interactions along study roadways and to reflect potential vehicle queue impacts in the study area.

The SimTraffic models were validated to existing conditions using the criteria outlined in *Guidelines for Applying Traffic Micro-simulation Modeling Software* (California Department of Transportation, 2002) and additional validation criteria developed by Fehr & Peers. Chapter 3 contains more detailed information about the development of the simulation models and the calibration and validation process.



The analysis results include a descriptive term known as level of service (LOS). LOS is a measure of traffic operating conditions, which varies from LOS A (indicating free-flow traffic conditions with little or no delay) to LOS F (representing over-saturated conditions where traffic flows exceed design capacity resulting in long queues and delays). These ratings represent the perspective of drivers and are an indication of the comfort and convenience associated with driving.

The LOS is determined differently depending on the type of control at the intersection. For side-street stop-controlled intersections, the LOS rating is based on the weighted average control delay of the side-street. At all-way stop-controlled and signalized intersections, the LOS rating is based on the weighted average control delay of all movements measured in seconds per vehicle. Peak hour traffic volumes, lane configurations, and signal timing plans were used as inputs for the LOS calculations. **Table 2-7** summarizes the relationship between the average control delay per vehicle and LOS for signalized and unsignalized intersections. Results from SimTraffic were used to determine delay and LOS at all intersections.

Peak hour factors (PHF) used in the analysis were based on the results of the data collection effort. Global peak hour factors were determined for the study area by taking a weighted average of all of the study intersections. The global PHF was calculated at 0.92 for the AM peak hour and 0.95 for the PM peak hour.

TABLE 2-7: INTERSECTION LEVEL OF SERVICE THRESHOLDS

| Level of Service | Signalized Intersection Control Delay (sec/veh) ¹ | Unsignalized Intersection Control Delay (sec/veh) ¹ | General Description |
|------------------|--|--|--------------------------------------|
| A | 0 – 10.0 | 0 – 10.0 | Little to no congestion or delays. |
| B | 10.1 – 20.0 | 10.1 – 15.0 | Limited congestion. Short delays. |
| C | 20.1 – 35.0 | 15.1 – 25.0 | Some congestion with average delays. |
| D | 35.1 – 55.0 | 25.1 – 35.0 | Significant congestion and delays. |
| E | 55.1 – 80.0 | 35.1 – 50.0 | Severe congestion and delays. |
| F | > 80.0 | > 50.0 | Total breakdown with extreme delays. |

Notes:

1. Control delay includes initial deceleration delay, queue move-up time, stopped delay, and acceleration delay.

Source: 2010 Highway Capacity Manual, Transportation Research Board, 2010.

MAINLINE FACILITIES

The freeway mainline segments and ramp junction operations were analyzed using the FREQ macroscopic modeling software. FREQ is a freeway-modeling tool that evaluates basic mainline segments, weaving segments, HOV lanes, and ramp metering. The advantage of FREQ compared to the 2010 Highway Capacity Manual (HCM) method is that FREQ evaluates the corridor as a system and HCM evaluates the corridor's individual sections in isolation. FREQ accounts for traffic operations of one freeway section influencing the operations of adjacent sections. From a traffic engineering perspective, a calibrated/validated FREQ model is a better tool for estimating traffic operations than HCM and therefore was used for this study.



Freeway facility operations are also described with the term level of service. LOS is a qualitative description of traffic flow based on speed, travel time, delay, and freedom to maneuver, with six levels, ranging from LOS A (i.e., free-flow operating conditions) to LOS F (i.e., heavily congested, over-capacity conditions). LOS E represents “at-capacity” operations. When volumes exceed capacity, stop-and-go conditions result and operations are designated as LOS F. The service level for a freeway section is based on vehicle density expressed as passenger cars/lane/mile. **Table 2-8** presents a summary of the relationship between density and level of service for freeway sections and ramp junctions.

TABLE 2-8: FREEWAY LEVEL OF SERVICE CRITERIA

| Level of Service | Description | Basic Mainline Segment Density Criteria ¹ |
|------------------|---|--|
| A | Free-flow speeds prevail. Vehicles are almost completely unimpeded in their ability to maneuver within the traffic stream. | ≤ 11.0 |
| B | Free-flow speeds are maintained. The ability to maneuver with the traffic stream is only slightly restricted. | > 11.0 to 18.0 |
| C | Flow with speeds at or near free-flow speeds. Freedom to maneuver within the traffic stream is noticeably restricted, and lane changes require more care and vigilance on the part of the driver. | > 18.0 to 26.0 |
| D | Speeds decline slightly with increasing flows. Freedom to maneuver with the traffic stream is more noticeably limited, and the driver experiences reduced physical and psychological comfort. | > 26.0 to 35.0 |
| E | Operation at capacity. There are virtually no usable gaps within the traffic stream, leaving little room to maneuver. Any disruption can be expected to produce a breakdown with queuing. | > 35.0 to 45.0 |
| F | Represents a breakdown in flow. | > 45.0 |

Notes:

1. Density in passenger cars per mile per lane

Source: 2010 Highway Capacity Manual.

Corridor Measures of Effectiveness

It is often useful to supplement the individual segment analyses with system-wide performance measures such as vehicle miles of travel, average travel time, average travel speed, and vehicle hours of delay to obtain a better understanding of overall traffic operations. This information can be particularly useful when comparing project alternatives. Several Measures of Effectiveness (MOEs) computed by the FREQ models were used to quantify traffic operations of the US 101 and SR 237 corridors:

- **Vehicle Miles of Travel (VMT)** – is a measure of the total vehicle throughput of the corridor. This measure takes into consideration the actual volume served versus the demand and the trip lengths of those vehicles and travelers.
- **Average Travel Time (ATT)** – is a measure of the time it takes (on average) to travel from one end of a corridor to the other during the peak period. The travel time calculation considers the average delay throughout the corridor, vehicle queues, and friction caused by merging vehicles.



- **Average Travel Speed (ATS)** – is directly related to average travel time and the corridor length.
- **Vehicle Hours of Delay (VHD)** – is the total amount of delay incurred during the peak periods due to congestion and demand exceeding the capacity of the freeway.
- **Maximum Individual Vehicle Delay** – is the maximum delay in minutes experienced by an individual driver during the peak hour relative to driving the corridor under free-flow conditions.

Mainline Weaving Sections

Per Caltrans' requirements, the LOS for freeway weaving sections was also determined using the Leisch Method as outlined in Figure 504.7A in Caltrans' *Highway Design Manual* (HDM), 6th Edition. The Leisch Method calculates the LOS based on the service flow (passenger cars/ per hour/ per lane) through the weaving section.



3. EXISTING (2013) TRANSPORTATION CONDITIONS

This chapter describes the existing (2013) conditions of the roadway facilities, pedestrian and bicycle facilities, and transit service. It also presents existing traffic volumes and operations for the study intersections and freeway segments with the level of service.

EXISTING (2013) ROADWAY SYSTEM

As noted above, **Figure 1** illustrates the traffic study area, which is generally bounded by Fifth Avenue to the north, Almanor Avenue-Ahwanee Avenue to the south, Fair Oaks Avenue to the east, and northbound US 101 on ramp at Moffett Park Drive to the west. The following provides a brief description of the key facilities.

Mathilda Avenue is primarily a north-south six-lane divided arterial serving the downtown Sunnyvale area and Caltrain to the south and an expanding high-tech business community to the north. Within the study area, Mathilda Avenue serves as the main access to the residential communities on the east side of Mathilda Avenue and the only access to the landlocked area contained within the US 101/SR 237/Mathilda triangle with access through Ross Drive. Mathilda Avenue is one of the designated truck routes for trucks over three tons in weight in the City of Sunnyvale. The speed limit is 45 mph and on-street parking is prohibited in the study area. Approximately 45,000 vehicles travel on Mathilda Avenue south of SR 237 on an average weekday. Within the study area, sidewalks are located along the entire east side of Mathilda Avenue and on the west side of Mathilda Avenue north of Moffett Park Drive. There are no bicycle facilities on Mathilda Avenue within the study area.

State Route 237 is an east-west freeway/highway starting at SR 82 in the City of Mountain View and ending approximately 11 miles east at I-680 in the City of Milpitas. Within the study area, the SR 237 freeway provides two mixed-flow lanes in each direction and one additional auxiliary lane in each direction between US 101 and Mathilda Avenue. In addition, a High Occupancy Vehicle (HOV) lane is provided east of Mathilda Avenue in the eastbound direction and turns into an Express Lane to the east of the Zanker Road overpass. The westbound direction includes an Express Lane starting at the I-880 connector which then changes into an HOV lane at the North First Street overpass and ends just east of Fair Oaks Avenue. SR 237 east of Mathilda Avenue currently carries approximately 90,000 vehicles on a daily basis.

US 101 is primarily a north-south freeway that connects Northern California, southern Santa Clara County, and Southern California. Within Caltrans District 4, US 101 begins at the San Benito/Santa Clara County line (PM 0.0) and terminates at the Sonoma/Mendocino County line (PM 56.94). Within the study area, US 101 provides three mixed-flow lane plus one HOV lane in each direction, while an auxiliary lane is also provided in the southbound direction between SR 237 and Mathilda Avenue. US 101 south of Mathilda Avenue currently carries approximately 154,000 vehicles on a daily basis.

Innovation Way is a four-lane, north-south road serving the development in the northwest area of the Mathilda Avenue/SR 237 interchange. It connects Mathilda Avenue with West Moffett Park Drive and has



two lanes in each direction. The speed limit is 25 mph with on-street parking prohibited. Bicycle facilities are not provided on Innovation Way and sidewalks are provided for pedestrians along both sides of Innovation Way at the Mathilda Avenue intersection.

Moffett Park Drive runs parallel to SR 237 on the north side of the freeway. West of Mathilda Avenue, Moffett Park Drive has two lanes in each direction and runs parallel to the VTA light rail tracks. Moffett Park Drive has one lane in each direction east of Mathilda Ave. The intersection of Mathilda Avenue/Moffett Park Drive is closely spaced to the SR 237/Mathilda Avenue interchange. Given the existing geometry, the channelization of traffic from the westbound SR 237 off-ramp to West Moffett Park Drive is disallowed. Within the study area, the speed limit is 40 mph with on-street parking prohibited. There are generally no bicycle or pedestrian facilities on Moffett Park Drive throughout the study area; however, Class II bicycle lanes are present on Moffett Park Drive east of Bordeaux Drive.

Ross Drive is a two-lane undivided local street that provides the only access to businesses that lie within the Mathilda Avenue/SR 237/US 101 triangle. On the east side of Mathilda Avenue, Ross Drive provides access to a large residential area where there are buffered sidewalks throughout the development and crosswalks at stop-controlled intersections. There are no existing bicycle facilities on the east side of Ross Drive. The west side of Ross Drive does not provide any pedestrian or bicycle facilities. The Ross Drive/Mathilda Avenue intersection is closely spaced to the SR 237/Mathilda Avenue interchange. The speed limit is 25 mph with on-street parking prohibited.

Almanor Avenue is a two-lane street that runs parallel to US 101 connecting Mathilda Avenue to North Mary Avenue. The speed limit is 30 mph with on-street parking prohibited. There are no bicycle facilities along Almanor Avenue, and pedestrian facilities are limited to the west/south side of the roadway.

Ahwanee Avenue is two-lane arterial that runs parallel to US 101 connecting Mathilda Avenue to Fair Oaks Boulevard. The speed limit is 35 mph with on-street parking permitted along most parts of Ahwanee Avenue on the south side of the street. There are no bicycle facilities along Ahwanee Avenue, and pedestrian facilities are limited to the east/south side of the roadway.

Bordeaux Drive is a two-lane undivided local street that provides connection between Moffett Park Drive and Mathilda Avenue. A two-way left-turn lane (TWLTL) is provided between Moffett Park Drive and West Java Drive. There are no pedestrian facilities along Bordeaux Drive. While there is a shoulder that can accommodate bicyclists, it is not defined as a Class II bicycle facility.

EXISTING TRUCK ROUTES

There are several truck routes in the study area and nearby. Mathilda Avenue is a designated truck route between Sunnyvale-Saratoga Road and Caribbean Drive. Other truck routes in Sunnyvale nearby the study area also include the following:

- Caribbean Drive between Mathilda Avenue and Lawrence Expressway
- Java Drive between Mathilda Avenue and Fair Oaks Avenue
- Evelyn Avenue between Wolfe Road and Bernardo



- Fair Oaks Avenue between Evelyn Avenue and Arques Avenue
- Fair Oaks Avenue between SR 237 and US 101.

EXISTING (2013) FREEWAY INTERCHANGES

US 101 / Mathilda Avenue interchange is partially a Type F-2 configuration (partial cloverleaf) with access to all directions with the exception of two movements: southbound Mathilda Avenue to US 101 northbound and US 101 southbound to northbound Mathilda Avenue. For access to southbound US 101, there is a slip from northbound Mathilda Avenue and a loop ramp from southbound Mathilda Avenue. For access from southbound US 101, there is a slip ramp to southbound Mathilda Avenue. Access to northbound US 101 is provided via a loop ramp from northbound Mathilda Avenue and access from northbound US 101 is provided via a slip ramp to northbound Mathilda Avenue and a loop ramp for southbound Mathilda Avenue. The ramp termini are not signalized and the on-ramps are metered.

SR 237 / Mathilda Avenue interchange is a Type L-1 configuration (tight diamond) that provides full access to SR 237 and Mathilda Avenue. For access to and from westbound SR 237, there is a diagonal on-ramp and off-ramp controlled by a traffic signal at the intersection with Mathilda Avenue. For access to and from eastbound SR 237, there is also a diagonal on-ramp and off-ramp controlled by a traffic signal at the intersection with Mathilda Avenue. The westbound on-ramp has ramp metering facilities, but it is not turned on during the AM or PM peak period. The eastbound on-ramp does not have ramp metering facilities.

Moffett Park Drive / US 101 Northbound On-Ramp is a single-lane on-ramp located along Moffett Park Drive to the west of the Mathilda Avenue / Moffett Park Drive intersection. This on-ramp merges with the westbound SR 237 off-ramp that connects to northbound US 101. The ramp terminus is signalized, and the on-ramp is not metered.

EXISTING (2013) INTERSECTION TRAFFIC OPERATIONS

Existing intersection lane configurations, and signal timings were used to calculate levels of service for the study intersections during the AM and PM peak hours for Existing Conditions. The peak hour turning movement volumes were balanced throughout the network in order to run microsimulation. The results of the LOS analysis were calculated using SimTraffic 8.0 software and are presented in **Table 3-4**. LOS calculation sheets are presented in **Appendix E**.

INTERSECTION MODEL DEVELOPMENT

SimTraffic models were developed representing the existing AM and PM peak hour traffic conditions for the local streets. An extensive model calibration and validation process was followed to ensure that the modeled results are consistent with the observed conditions on the local streets.

The majority of model development was performed using Synchro before converting the network into the SimTraffic software. The Synchro models include all of the study intersections and were coded with the peak hour counts, posted speed limit, vehicle mix, and signal timings. Traffic signal timing and phasing



information for the signalized intersections were obtained from the respective agencies and municipalities (i.e., City of Sunnyvale and Caltrans). Additional detail such as turn pocket lengths and intersection spacing was coded into the model based on field observations and aerial photography. The following represents the initial SimTraffic parameters used in the modeling before calibration:

- Free flow speed = posted speed limit
- Left-turn turning speed = 15 mph
- Right-turn turning speed = 9 mph
- Vehicle lengths
 - Car 1 = 18 feet
 - Car 2 = 16 feet
- Vehicle Occurrence
 - Cars:
 - 50% Car 1
 - 50% Car 2
 - Heavy Vehicles:
 - 50% Single unit truck
 - 50% Semi truck 2
- Driver Behavior
 - Yellow phase reaction time for drivers 1-4 set equal to driver 5
 - Green phase reaction time for drivers 1-4 set equal to driver 5
 - Gap acceptance factor for drivers 1-4 set equal to driver 5
 - Mandatory/Positioning Distance Adjustment to be within 80%-125% range

Calibration

SimTraffic models reflecting existing field conditions require calibration to ensure that traffic volumes, queue lengths, and other operational observations are replicated satisfactorily. The final calibrations settings will be carried forward into the alternatives analysis of future year conditions (to be address in a subsequent technical memorandum).

The following calibration process was employed to determine if the model results were satisfactorily replicating the existing conditions:

1. Make a base model run with default parameters
2. Compare predicted and field-observed performance measures and assess differences
3. Assess differences between predicted and field-observed performance measures
4. Select reasonable model input changes to reduce differences
5. Make a new model run with selected input changes
6. Repeat process until predictions meet or exceed published criteria



Validation

Model validation is a process where the overall model traffic performance is verified against field measurements for traffic performance, such as traffic volumes, travel times, average speeds, queue lengths, and average delays.

Validation Criteria

The major validation criteria based on the *Guidelines for Applying Traffic Micro-simulation Modeling Software* used in this study are:

1. The model simulated total intersection volumes should be within five percent of the existing 2013 traffic volumes.
2. The simulation model should replicate noticeable field queues to the analyst's satisfaction.

Model Parameter Adjustments

The initial model runs did not replicate field traffic volumes or observed queues using the default analysis parameters. These model parameters were adjusted where appropriate to more closely match field-observed conditions. Driver aggressiveness factors were the most common adjustments made to the model.

These factors impact the vehicle headways and ultimately the saturation flow rates. Headways in urban areas with congested conditions are often lower than areas with un-congested conditions, resulting in higher saturation flow rates as drivers follow other vehicles more closely and drive more aggressively. The following model adjustments were made:

1. Mathilda Avenue / Fifth Avenue

- AM and PM – Changed southbound and eastbound right-turn speed to 15 MPH

2. Mathilda Avenue / Innovation Way

- AM and PM – Changed southbound and eastbound right-turn speed to 15 MPH

3A. Mathilda Avenue / Moffett Park Drive

- AM and PM – Adjusted northbound and southbound headway factors to 0.8
- AM and PM – Adjusted northbound mandatory and positioning distances
- AM and PM – Changed southbound right-turn speed to 15 MPH
- PM – Adjusted eastbound headway factor to 0.8
- PM – Adjusted mandatory and positioning distances
- PM – Changed eastbound right-turn speed to 20 MPH

3B. Mathilda Avenue / SR 237 Westbound Ramps



- AM and PM – Adjusted northbound, southbound, and westbound headway factors to 0.8
- AM and PM – Changed westbound left-turn speed to 25 MPH
- AM and PM – Adjusted westbound right-turn speed to 15 MPH
- AM – Adjusted westbound mandatory distance
- PM – Adjusted southbound mandatory distance
- PM – Adjusted southbound right-turn speed to 20 MPH

4. Mathilda Avenue / SR 237 Eastbound Ramps

- AM and PM – Adjusted northbound and southbound headway factors to 0.8
- AM and PM – Adjusted northbound mandatory and positioning distances
- AM and PM – Changed northbound right-turn speed to 35 MPH
- AM and PM – Changed eastbound right-turn speed to 15 MPH

5. Mathilda Avenue / Ross Drive

- AM and PM – Adjusted northbound and southbound headway factors to 0.8
- AM and PM – Adjusted northbound mandatory and positioning distances
- AM and PM – Changed northbound, southbound, eastbound, and westbound left-turn speeds to 20 MPH
- PM – Adjusted eastbound and westbound headway factors to 0.8
- PM – Adjusted southbound mandatory and positioning distances

8. Mathilda Avenue / Almanor Avenue-Ahwanee Avenue

- AM – Adjusted northbound headway factor to 0.8
- PM – Adjusted southbound mandatory and positioning distances

10. Innovation Way / Moffett Park Drive

- AM and PM – Changed southbound right-turn speed to 15 MPH

11. Innovation Way / Eleventh Avenue

- AM and PM – Changed eastbound right-turn speed to 15 MPH

Intersection Volume Validation Results

SimTraffic is a stochastic model where different random seed numbers generate different driver behaviors (e.g., accepting available gaps for turns, changing lanes, etc.) and system results. The *Guidelines for Applying Traffic Micro-simulation Modeling Software* recommends multiple runs to account for this stochastic nature of the model and to achieve confidence in the simulated results. Thus, all results presented in this section are the average of ten model runs with different seed numbers.



Table 3-1 presents the intersection volume validation results. Balanced demand volumes and balanced count volumes are both presented in **Table 3-1** to demonstrate that not all of the demand from the ramps is served, but the amount of traffic that is able to reach each intersection is being served. The SimTraffic model was run using demand volumes, but only the amount that was counted is actually being served.

As shown in **Table 3-1**, the total intersection model volumes at all intersections are within five percent of the counts during the AM peak hour. In the PM peak hour, only two intersections are not within the five percent of the counted volume due to lane utilization limitations of SimTraffic. In the field, it was observed that vehicles making an eastbound right-turn onto southbound Mathilda Avenue would use all available southbound lanes, enabling 10-12 vehicles to fill the southbound lanes between the SR 237 Westbound Ramps and Moffett Park Drive intersections. Due to the lane utilization limitations of SimTraffic, only about four vehicles per signal cycle are able to fill up the southbound lanes. Because of this, the eastbound queues was observed to be excessive in the SimTraffic model and spill back through Intersection #10 and #11. This causes the percent of demand served at Intersection #10 and #11 to be below the 95 percent threshold and the delay and LOS results to display slightly worse results than observed in the field. This SimTraffic limitation will be considered when presenting future conditions for No Build and Build Alternatives where the west leg of Moffett Park remains open conditions at this intersection. This limitation will not be a factor for Build Alternatives where the west leg of Moffett Park Drive is closed as a part of the project.

A detailed comparison by movement is included in **Appendix E**. With respect to traffic volumes, the models are considered sufficiently validated.



TABLE 3-1: MODEL VOLUME VALIDATION RESULTS SUMMARY

| Intersection | AM Peak Hour | | | | | PM Peak Hour | | | | |
|---|--------------------|---------------------|-------------------------|--------------------------------|---------------------------------|--------------------|---------------------|-------------------------|--------------------------------|---------------------------------|
| | Count ¹ | Demand ² | SimTraffic ³ | SimTraffic /Count ⁴ | SimTraffic /Demand ⁵ | Count ¹ | Demand ² | SimTraffic ³ | SimTraffic /Count ⁴ | SimTraffic /Demand ⁵ |
| 1 Mathilda Avenue / Fifth Avenue | 1,385 | 1,465 | 1,436 | 1.04 | 0.98 | 1,614 | 1,924 | 1,793 | 1.11 | 0.93 |
| 2 Mathilda Avenue / Innovation Way | 1,945 | 2,025 | 1,963 | 1.01 | 0.97 | 2,118 | 2,528 | 2,223 | 1.05 | 0.88 |
| 3A Mathilda Avenue / Moffett Park Drive | 3,586 | 3,666 | 3,528 | 0.98 | 0.96 | 3,163 | 3,724 | 3,329 | 1.05 | 0.89 |
| 3B Mathilda Avenue / SR 237 Westbound Ramps | 3,982 | 4,084 | 3,949 | 0.99 | 0.97 | 3,399 | 3,956 | 3,487 | 1.03 | 0.88 |
| 4 Mathilda Avenue / SR 237 Eastbound Ramps | 4,380 | 4,450 | 4,274 | 0.98 | 0.96 | 3,777 | 4,221 | 3,819 | 1.01 | 0.90 |
| 5 Mathilda Avenue / Ross Drive | 3,901 | 3,980 | 3,832 | 0.98 | 0.96 | 3,983 | 4,470 | 4,087 | 1.03 | 0.91 |
| 6 Mathilda Avenue / US 101 Northbound Ramps (project) | - | - | - | - | - | - | - | - | - | - |
| 7 Mathilda Avenue / US 101 Southbound Ramps (project) | - | - | - | - | - | - | - | - | - | - |
| 8 Mathilda Avenue / Almanor Avenue-Ahwanee Avenue | 4,870 | 4,913 | 4,927 | 1.01 | 1.00 | 4,851 | 4,851 | 4,611 | 0.95 | 0.95 |
| 9 US 101 Northbound On-Ramp / Moffett Park Drive | 1,041 | 1,041 | 1,009 | 0.97 | 0.97 | 1,234 | 1,295 | 1,200 | 0.97 | 0.93 |
| 10 Innovation Way / Moffett Park Drive | 1,206 | 1,206 | 1,170 | 0.97 | 0.97 | 1,336 | 1,413 | 1,278 | 0.96 | 0.90 |
| 11 Innovation Way / Eleventh Avenue | 668 | 668 | 648 | 0.97 | 0.97 | 681 | 753 | 734 | 1.08 | 0.98 |
| 12 Innovation Way / Juniper Networks Driveway | 771 | 771 | 758 | 0.98 | 0.98 | 721 | 821 | 756 | 1.05 | 0.92 |
| 13 Bordeaux Drive / Innovation Way (future) | 140 | 140 | 138 | 0.99 | 0.99 | 157 | 157 | 160 | 1.02 | 1.02 |

Notes: *Italics* indicate that the intersection did not meet the 95 percent volume served requirement.

1. Intersection count is the peak hour volume for all approaches to the intersection.
2. Intersection demand includes any unserved volume at each intersection and then is balanced among intersections.
3. Average served volumes based on ten SimTraffic runs.
4. Modeled traffic volume expressed as a ratio of **observed** traffic volume. For example: 1.00 indicates an exact replication of field conditions.
5. Modeled traffic volume expressed as a ratio of **demand** traffic volume. For example: 1.00 indicates all demand is served.

Source: Fehr & Peers, 2016.



Queues and Congestion Validation Results

Intersections are generally designed to accommodate 95th percentile queue lengths. The 95th percentile queue lengths for each of the study intersections are presented in **Table 3-2**. In general, the simulation models replicated observed queues to the analyst's satisfaction based on the field data listed in Chapter 2. A detailed summary by movement is included in **Appendix E**. With respect to traffic queue lengths, the models are considered validated.

TABLE 3-2: MODEL QUEUING ANALYSIS RESULTS

| Intersection | Movement ¹ | Available Storage ² | AM Peak Hour 95 th Percentile Queue (ft) | PM Peak Hour 95 th Percentile Queue (ft) |
|--|-----------------------|--------------------------------|--|--|
| 1. Mathilda Avenue / Fifth Avenue | NB-L | 425 | 75 | 125 |
| | NB-T | 1,150 | 275 | 150 |
| | SB-L | 225 | 50 | 50 |
| | SB-T | 1,375 | 125 | 1,050 |
| | SB-R | 225 | 25 | 150 |
| | EB-L | 625 | 50 | 75 |
| | EB-T | 625 | 25 | 25 |
| | EB-R | 625 | 25 | 50 |
| | WB-L | 925 | 50 | 500 |
| | WB-T | 75 | 50 | 75 |
| 2. Mathilda Avenue / Innovation Way | NB-L | 400 | 375 | 75 |
| | NB-T | 1,075 | 200 | 150 |
| | SB-L | 75 | 25 | 0 |
| | SB-T | 1,150 | 125 | 1,450 |
| | SB-R | 225 | 100 | 350 |
| | EB-L | 125 | 50 | 125 |
| | EB-R | 200 | 50 | 275 |
| 3. Mathilda Avenue / Moffett Park Drive / SR 237 Westbound Ramps | NB-L (MP) | 125 | 125 | 50 |
| | NB-L (237) | 200 | 150 | 225 |
| | NB-T | 325 | 400 | 200 |
| | SB-L (MP) | 175 | 50 | 75 |
| | SB-T | 1,200 | 200 | 1,275 |
| | EB-L (MP) | 350 | 50 | 900 |
| | EB-T (MP) | 1,100 | 125 | 1,400* |
| | EB-R (MP) | 1,100 | 50 | 625 |
| | WB-L (MP) | 300 | 125 | 325 |
| | WB-T (MP) | 650 | 250 | 250 |
| | WB-L (237) | 1,125 | 650 | 1,100 |
| WB-R (237) | 325 | 400 | 500 | |



TABLE 3-2: MODEL QUEUING ANALYSIS RESULTS

| Intersection | Movement ¹ | Available Storage ² | Peak Hour | |
|--|-----------------------|--------------------------------|--|--|
| | | | AM Peak Hour 95 th Percentile Queue (ft) | PM Peak Hour 95 th Percentile Queue (ft) |
| 4. Mathilda Avenue / SR 237 Eastbound Ramps | NB-T | 275 | 325 | 125 |
| | NB-R | 275 | 300 | 100 |
| | SB-L | 200 | 100 | 225 |
| | SB-T | 200 | 275 | 300 |
| | EB-L | 1,075 | 325 | 125 |
| | EB-LTR | 450 | 275 | 275 |
| 5. Mathilda Avenue / Ross Drive | NB-L | 150 | 100 | 150 |
| | NB-T | 2,200 | 950 | 450 |
| | SB-L | 125 | 125 | 200 |
| | SB-T | 250 | 275 | 350 |
| | EB-L | 650 | 150 | 250 |
| | EB-T | 75 | 100 | 125 |
| | EB-R | 50 | 75 | 75 |
| | WB-L | 75 | 300 | 925 |
| | WB-T | 75 | 125 | 125 |
| WB-R | 75 | 100 | 100 | |
| 6. Mathilda Avenue / US 101 NB Ramps** | N/A | N/A | N/A | N/A |
| 7. Mathilda Avenue / US 101 SB Ramps** | N/A | N/A | N/A | N/A |
| 8. Mathilda Avenue / Almanor Avenue-Ahwanee Avenue | NB-L | 375 | 325 | 125 |
| | NB-T | 675 | 675 | 325 |
| | NB-R | 75 | 75 | 75 |
| | SB-L | 125 | 225 | 200 |
| | SB-T | 2,200 | 575 | 1,225 |
| | EB-L | 350 | 100 | 250 |
| | EB-T | 125 | 75 | 125 |
| | WB-L | 250 | 125 | 100 |
| | WB-T | 625 | 150 | 75 |
| | WB-R | 75 | 125 | 100 |
| 9. US 101 Northbound On-Ramp / Moffett Park Drive | EB-T | 875 | 50 | 750 |
| | EB-R | 150 | 25 | 250 |
| | WB-L | 900 | 50 | 250 |
| | WB-T | 900 | 125 | 0 |



TABLE 3-2: MODEL QUEUING ANALYSIS RESULTS

| Intersection | Movement ¹ | Available Storage ² | Peak Hour | |
|--|-----------------------|--------------------------------|--|--|
| | | | AM Peak Hour 95 th Percentile Queue (ft) | PM Peak Hour 95 th Percentile Queue (ft) |
| 10. Innovation Way / Moffett Park Drive | SB-L | 525 | 50 | 200 |
| | SB-LTR | 525 | 100 | 325 |
| | EB-L | 225 | 75 | 275 |
| | EB-T | 900 | 75 | 975 |
| | WB-T | 975 | 325 | 150 |
| | WB-R | 225 | 125 | 25 |
| 11. Innovation Way / Eleventh Avenue | NB-L | 125 | 75 | 25 |
| | NB-LT | 500 | 75 | 75 |
| | SB-T | 775 | 150 | 75 |
| | EB-L | 125 | 50 | 125 |
| | EB-R | 1,150 | 50 | 100 |
| 12. Innovation Way / Juniper Driveway | NB-L | 125 | 25 | 50 |
| | NB-T | 900 | 50 | 25 |
| | SB-T | 300 | 250 | 100 |
| | SB-R | 300 | 175 | 100 |
| | EB-L | 300 | 50 | 1,000 |
| | EB-R | 300 | 25 | 250 |
| 13. Bordeaux Drive/Innovation Way*** | N/A | N/A | N/A | N/A |

Notes: **Bold** denotes locations where storage length is exceeded.

*Synchro/SimTraffic includes the vehicles stopped trying to enter the right-turn lane as queuing length for the through movement. Queuing is not observed in the field or in the SimTraffic simulation to queue back from the stop bar to the calculated queue length of 1,400 feet.

**Indicates intersection is signalized under Build 1 and Build 2 Alternatives, but operates as a free movement under the No Build Alternative.

***This intersection does not exist under Base Year Conditions (2013).

1. NB-northbound, SB-southbound, EB-eastbound, WB-westbound, L-left-turn movement, T-through movement, R-right-turn movement, (MP)-turn onto/from Moffett Park Drive, (237)-turn onto/from SR 237 WB Ramps.
2. Available storage lengths are provided on a "per lane" basis. For example, an available storage of 425 means each lane in the associated movement has a storage length of 425 feet.

Source: Fehr & Peers, 2016.

Peak Hour Travel Time Validation Results

Table 3-3 compares the observed peak hour travel times to the calibrated Mathilda Avenue model peak hour travel times for the study segments.



TABLE 3-3: MATHILDA AVENUE PEAK HOUR TRAVEL TIME VALIDATION RESULTS

| Peak Direction | Average Travel Time from Field Measurements (mm:ss) ¹ | Average Travel Time from SimTraffic Model (mm:ss) | Percent Difference |
|---|--|---|--------------------|
| Mathilda Avenue Northbound² | | | |
| AM Peak Hour | 04:17 | 06:35 | 54% |
| PM Peak Hour | 05:15 | 05:10 | -1% |
| Mathilda Avenue Southbound² | | | |
| AM Peak Hour | 04:12 | 05:40 | 35% |
| PM Peak Hour | 05:00 | 13:55 | 178% |

Notes:

- Travel time data was extracted from GPS travel time runs performed along Mathilda Avenue in November 2013 and confirmed through observations conducted by Fehr & Peers in November 2013.
- Travel time runs begin north of the San Aleso Avenue intersection and end south of the Lockheed Martin Way-Java Drive intersection.

Source: Fehr & Peers, 2016.

PEAK HOUR LEVEL OF SERVICE RESULTS

Existing intersection traffic operations were evaluated using the calibrated/validated SimTraffic models developed for the 14 study intersections. The simulation models were recorded for the AM and PM peak hours with a 15-minute seeding period. **Table 3-4** presents the simulated intersection level of service results for each of the study intersections and Fehr & Peers' analysis worksheets are presented in **Appendix E**.¹ As the simulation results show, all study intersections operate at LOS D or better during the AM and PM peak hours, except the following locations:

- Mathilda Avenue / Innovation Way (Intersection #2) – PM peak hour;
- Mathilda Avenue / Moffett Park Drive (Intersection #3) – PM peak hour;
- Mathilda Avenue / SR 237 Westbound Ramp (Intersection #4) – PM peak hour;
- Mathilda Avenue / Ross Drive (Intersection #6) – AM peak hour;
- US 101 Northbound On-Ramp / Moffett Park Drive (Intersection #10) – PM peak hour;
- Innovation Way / Moffett Park Drive (Intersection #11) – PM peak hour;
- Innovation Way / Juniper Networks Driveway (Intersection #13) – PM peak hour.

Operations at each of these intersection are discussed in more detail below.

¹ Please note that Synchro and SimTraffic worksheets are provided for the study intersection in **Appendix C** for informational purposes to present key modeling inputs including lanes, volumes, and signal timing. The results presented in **Table 3-4** are from the Fehr & Peers analysis worksheets, which are the average of ten SimTraffic model runs.



TABLE 3-4: EXISTING PEAK HOUR INTERSECTION ANALYSIS¹

| | Intersection | Traffic Control² | Peak Hour³ | Delay⁴ | LOS⁵ | Movements Operating at LOS F⁶ |
|----|---|------------------------------------|------------------------------|------------------------------|------------------------|--|
| 1 | Mathilda Avenue / Fifth Avenue | Signal | AM PM | 14.8 112.4 | B F | AM: N/A PM: SBL/T/R, WBL/T/R |
| 2 | Mathilda Avenue / Innovation Way | Signal | AM PM | 20.6 168.9 | C F | AM: N/A PM: SBT/R |
| 3 | Mathilda Avenue / Moffett Park Drive / SR 237 Westbound Ramps | Signal | AM PM | 131.0 286.7 | F F | AM: SBT, WBL (MPD), WBR (237) PM: NBL (237), SBL/T/R (MPD/237), EBL/T/R, WBL/T/R (237) |
| 4 | Mathilda Avenue / SR 237 Eastbound Ramps | Signal | AM PM | 30.1 20.3 | C B | AM: N/A PM: N/A |
| 5 | Mathilda Avenue / Ross Drive | Signal | AM PM | 94.6 46.7 | F D | AM: NBT/R PM: WBL/T/R |
| 6 | Mathilda Avenue / US 101 Northbound Ramps (project) | Slip Ramp | AM PM | N/A N/A | N/A N/A | N/A N/A |
| 7 | Mathilda Avenue / US 101 Southbound Ramps (project) | Slip Ramp | AM PM | N/A N/A | N/A N/A | N/A N/A |
| 8 | Mathilda Avenue / Almanor Avenue-Ahwanee Avenue | Signal | AM PM | 52.3 48.8 | D D | AM: SBL PM: SBL |
| 9 | US 101 Northbound On-Ramp / Moffett Park Drive ⁷ | Signal | AM PM | 4.6 65.6 | A E | AM: N/A PM: EBT |
| 10 | Innovation Way / Moffett Park Drive ⁷ | Signal | AM PM | 12.4 81.5 | B F | AM: N/A PM: EBL/T |
| 11 | Innovation Way / Eleventh Avenue | AWSC | AM PM | 7.7 6.8 | A A | AM: N/A PM: N/A |
| 12 | Innovation Way / Juniper Networks Driveway | AWSC | AM PM | 11.9 120.6 | B F | AM: N/A PM: NBT, EBL |
| 13 | Bordeaux Drive / Innovation Way (future) | N/A | AM PM | N/A N/A | N/A N/A | N/A N/A |

Notes: Results in **bold** represent unacceptable levels of service, N/A=not applicable.

- Results based on SimTraffic simulation of ten runs.
- Signal – signalized intersection, AWSC – all-way stop-controlled intersection, Free – uncontrolled intersection
- AM – morning peak hour, PM – evening peak hour
- Average control delay calculated using the *Highway Capacity Manual (HCM)* (Transportation Research Board, 2010) methodology and Synchro/SimTraffic 8.0 analysis software. For signalized and all-way stop-controlled intersections, average control delay is for the intersection, as a whole.
- For signalized and all-way stop-controlled intersections the LOS for the intersection as a whole is presented.
- NB-northbound, SB-southbound, EB-eastbound, WB-westbound, L-left turn movement, T-through movement, R-right turn movement, MPD-Moffett Park Drive, 237-SR 237 On/Off-Ramp.
- The delay and LOS during the PM peak hour for these intersections is worse than what was observed in the field due to limitation of SimTraffic described earlier in the chapter.

Source: Fehr & Peers, 2016.



Intersection #1 – Mathilda Avenue / Fifth Avenue

The Mathilda Avenue / Fifth Avenue intersection operates at LOS F during the PM peak hour due to the high levels of delay and congestion on the southbound through and eastbound right-turn approaches as vehicles travel toward the SR 237 and US 101 interchanges. In addition, the light rail causes additional delay for the eastbound right-turn approach.

Intersection #2 – Mathilda Avenue / Innovation Way (Signalized)

The Mathilda Avenue / Innovation Way intersection operates at LOS F during the PM peak hour due to high levels of delay and congestion on the southbound through and eastbound right-turn approaches as vehicles travel toward the SR 237 and US 101 interchanges. In addition, the light rail causes additional delay for the eastbound right-turn approach.

Intersection #3 – Mathilda Avenue / Moffett Park Drive / SR 237 Westbound Ramp (Signalized)

The Mathilda Avenue / Moffett Park Drive intersection operates at LOS F during the AM peak hour due to the high levels of delay and congestion traveling northbound on Mathilda Avenue from Mathilda Avenue and SR 237 Westbound Off-Ramp. Delay and congestion is also excessive in the PM peak hour (LOS F) due to the southbound through and eastbound right-turn approaches as vehicles travel toward the SR 237 and US 101 interchanges. The westbound left-turn approach also experiences a fair amount of delay, but the queues do not extend past the Bordeaux Drive intersection.

In the field, it was observed that vehicles making an eastbound right-turn onto southbound Mathilda Avenue would use all available southbound lanes enabling 10-12 vehicles to fill the southbound lanes between the SR 237 Westbound Ramps and Moffett Park Drive intersections. Due to the limitations of SimTraffic, only four vehicles per cycle are able to fill up the southbound lanes. Because of this, the eastbound queues was observed to be excessive in the SimTraffic model and spill back through Intersection #10 and #11.

Intersection #5 – Mathilda Avenue / Ross Drive (Signalized)

The Mathilda Avenue / Ross Drive intersection operates at LOS F during the AM peak hour due to high levels of delay and congestion on the northbound through, westbound right-turn, and eastbound left-turn approaches as vehicles travel toward the SR 237 interchange.

Intersection #9 – US 101 Northbound On-Ramp / Moffett Park Drive (Signalized)

The US 101 Northbound On-Ramp / Moffett Park Drive intersection operates at LOS E during the PM peak hour due to the high levels of delay and congestions on the eastbound through approach as vehicles travel toward Mathilda Avenue to access SR 237 and US 101 Southbound interchanges. The eastbound through experiences excessive queues that were not observed in the field due to the limitations of SimTraffic as described under Intersection #3 (3.3.2.2).



Intersection #10 – Innovation Way / Moffett Park Drive (Signalized)

The Innovation Way / Moffett Park Drive intersection operates at LOS F during the PM peak hour due to the high levels of delay and congestions on the eastbound through and southbound left-turn approaches as vehicles travel toward Mathilda Avenue to access SR 237 and US 101 interchanges. The eastbound through experiences excessive queues that were not observed in the field due to the limitations of SimTraffic as described under Intersection #3 (3.3.2.2).

Intersection #12 – Innovation Way / Juniper Networks Driveway (All-Way Stop-Controlled)

The Innovation Way / Juniper Networks Driveway intersection operates at LOS F during the PM peak hour due to high levels of delay and congestion on the eastbound left-turn and northbound through approaches as vehicles travel toward Mathilda Avenue to access the SR 237 and US 101 interchanges. This is a large all-way stop controlled intersection where vehicles queue back through the intersection during phases when light-rail pass through the Mathilda Avenue / Innovation Way intersection.

MATHILDA CORRIDOR TRAVEL TIME RUNS

Congested travel time was calculated using the SimTraffic arterial report and results can be found in **Table 3-5**. The results, which can be found in **Appendix D**, contains information about the speed and travel time for the Mathilda Avenue corridor between San Aleso Avenue and Java Drive.

TABLE 3-5: MATHILDA AVENUE TRAVEL TIMES¹

| Direction | Peak Hour | Free flow Travel Time (s) ² | Congested Travel Time (s) | Delay (s) |
|----------------------------|-----------|--|---------------------------|-----------|
| Mathilda Avenue Northbound | AM | 116.2 | 395.9 | 279.7 |
| | PM | 116.2 | 310.5 | 194.3 |
| Mathilda Avenue Southbound | AM | 116.2 | 339.6 | 223.4 |
| | PM | 116.2 | 835.2 | 719.0 |

Notes:

1. Travel time runs begin north of the San Aleso Avenue intersection and end south of the Lockheed Martin Way-Java Drive intersection (approximately 1.44 miles).
2. Free flow speed is calculated assuming a travel speed of 45 miles per hour.

Source: Fehr & Peers, 2016.

EXISTING (2013) FREEWAY MAINLINE OPERATIONS

The Existing Conditions operating conditions of US 101 and SR 237 were analyzed using the calibrated FREQ models. Existing peak hour levels of service from the FREQ models are presented in **Table 3-9** for US 101 freeway and **Table 3-10** for SR 237 freeway. **Appendix F** provides the FREQ analysis worksheets.

FREQ models representing northbound and southbound US 101 and eastbound and westbound SR 237 were developed to evaluate freeway mainline traffic operations during the weekday AM and PM peak



periods. Eight FREQ models were developed: US 101 Northbound AM and PM, US 101 Southbound AM and PM, SR 237 Eastbound AM and PM, SR 237 Westbound AM and PM. For the US 101 model, the study limits of the FREQ model extend between Shoreline Boulevard and SR 87 due to the length of observed queuing. The model was validated for a shorter section of the corridor including segments between Fair Oaks Avenue and just north of SR 237. The study limits for the SR 237 FREQ model extend between Lawrence Expressway and Maude Avenue.

Existing demand volumes and roadway lane configurations were used to develop the existing conditions models. These models were then calibrated so that the model queuing, travel times, and speeds were consistent with the observed queuing, travel times, and speeds. The models were then used to evaluate traffic operations and the corridor MOEs.

MAINLINE MODEL DEVELOPMENT

The number of lanes on the mainline and ramps were obtained from field observations, and distances between each ramp gore point were obtained from aerial photography. The traffic volume data was input in hourly time increments to account for traffic fluctuations during the peak periods with exception of the SR 237 WB models. The SR 237 WB models included 30-minute time slices in order to more accurately depict peak period queuing and speeds. The following represents the initial default parameters used in the modeling before calibration:

- Free flow speed = 65 miles per hour (mph)
- Speed delay curve = 30 mph
- Mainline capacity = 2,000 vehicles per hour per lane (vphpl)
- HOV lane capacity = 1,650 vphpl
- Ramp capacity for standard merge/diverge = 1,500 vphpl
- Ramp capacity for above-standard merge/diverge or lane add = 2,000 vphpl
- Auxiliary lane capacity = the minimum of the on-ramp or off-ramp peak hour volume

Calibration

FREQ models reflecting existing field conditions require calibration to ensure that traffic volumes, queue lengths, and other operational observations are replicated satisfactorily. The final calibrations settings will be carried forward into the alternatives analysis of future year conditions (to be address in a subsequent technical memorandum).

Based on the recommended calibration procedures presented in the FREQ *Freeway Analysis Manual* (June 30, 2009) the following calibration process was employed:

1. Make a base model run with default parameters
2. Compare predicted and field-observed performance measures



3. Assess differences between predicted and field-observed performance measures
4. Select reasonable model input changes to reduce differences
5. Make a new model run with selected input changes
6. Repeat process until predictions are acceptable

Validation

Model validation is a process where the overall model traffic performance is verified against field measurements for traffic performance, such as peak hour travel time, bottleneck locations and durations, and queues.

Validation Criteria

To determine if the model predictions were within acceptable tolerances, the following validation criteria were used from the *FREQ Freeway Analysis Manual*:

| <u>Criteria</u> | <u>Acceptable Targets</u> |
|-----------------------|---|
| Bottlenecks | Replicated by model at each location |
| Duration of queuing | Start and end times within 1 time increment |
| Queue length | Within 10 percent of actual length |
| Peak hour travel time | Within 10 percent of actual travel time |

Model Parameter Adjustments

The initial base model run with the default parameters did not result in the model replicating observed field conditions for the southbound PM and the northbound AM models. Specifically, the FREQ models did not replicate the field-observed bottlenecks and the travel times through the corridor were generally faster than measured in the field. A bottleneck is a mainline segment operating at capacity, or LOS E by definition, which results in upstream mainline queues. As recommended, reasonable model input changes were made to reduce the differences until the model replicated field observed conditions within acceptable targets.

Table 3-6 summarizes the changes made to the FREQ default parameters to achieve model validation.



TABLE 3-6: CHANGES TO FREQ PARAMETERS FOR MODEL CALIBRATION

| Parameter | Default | Calibrated | Reason for Change |
|--|-------------|--|--|
| Free Flow Speed | 65 mph | Varies between 60 mph and 65 mph | Changes made to reflect current design conditions and upstream bottlenecks. |
| Speed Delay Curve | 30 mph | No Change | --- |
| Mainline Capacity | 2,000 vphpl | US 101 - 1,960 vphpl; SR 237 EB – 2,200 vphpl | Changes made to reflect observed bottleneck and resulting queue length. The capacity was adjusted to demonstrate that a bottleneck does not form at this location, yet all of the demand volume is served as shown by the throughput count at the SR 237 pedestrian overcrossing and speed data at this location. |
| HOV Lane Capacity | 1,650 vphpl | No Change | --- |
| Ramp Capacity for Standard Merge/Diverge | 1,500 vphpl | No Change | --- |
| Ramp Capacity for Above-Standard Merge/Diverge | 2,000 vphpl | No Change | --- |
| Weaving Analysis | Disengaged | No Change | --- |

Source: Fehr & Peers, 2016.

Bottleneck Validation Results

Table 3-7 presents the validation results for the bottleneck locations. As shown in **Table 3-7**, the AM and PM models adequately reflect observed conditions.



TABLE 3-7: BOTTLENECK VALIDATION RESULTS

| Freeway / Direction / Peak Hour | Criteria | Observed ³ | FREQ Model | Difference |
|---------------------------------|--|--|--|------------|
| US 101 Northbound AM | Location A ¹ | Bottleneck develops north of study area limits. | Bottleneck develops north of study area limits. | None |
| | Queue length and duration | Entire study area is in queue between 7:00 AM and 9:00 AM as a result of a bottleneck outside the study area. The queue extends past the Fair Oaks Avenue Off-Ramp (queue extends beyond study area limits). | Entire study area is in queue between 7:00 AM and 9:00 AM as a result of a bottleneck outside the study area. The queue extends past the Fair Oaks Avenue Off-Ramp (queue extends beyond study area limits). | None |
| US 101 Southbound PM | Location A ² | Bottleneck develops south of study area limits. | Bottleneck develops south of study area limits. | None |
| | Queue length and duration | Entire study area is in queue between 4:00 PM and 6:00 PM as a result of a bottleneck outside the study area. The queue extends past the Ellis Street On-Ramp (queue extends beyond study area limits). Between 6:00 PM and 7:00 PM the queue recedes to about the SR 237 interchange (within the study area). | Entire study area is in queue between 4:00 PM and 6:00 PM as a result of a bottleneck outside the study area. The queue extends past the Ellis Street On-Ramp (queue extends beyond study area limits). Between 6:00 PM and 7:00 PM the queue recedes to about the SR 237 interchange (within the study area). | None |
| SR 237 Westbound AM | At US 101 Northbound Off-Ramp | Bottleneck develops at US 101 Off-Ramp location due to congestion on US 101 causing spillback onto SR 237. | Bottleneck develops at US 101 Off-Ramp location due to congestion on US 101 causing spillback onto SR 237. | None |
| | Queue length and duration | Queue spills back beyond the Mathilda Avenue interchange during the peak period. | Queue spills back beyond the Mathilda Avenue interchange during the peak period. | None |
| SR 237 Eastbound PM | No queue observed within the study segments. | | | |

Notes:

1. Bottleneck that develops during the AM peak period along NB US 101 is beyond the study area limits.
2. Bottleneck that develops during the PM peak period along SB US 101 is beyond the study area limits.
3. Queue length based on field observations, travel time runs, and INRIX travel speed databases. Queues extend to the general location denoted.

Source: Fehr & Peers, 2016.

Peak Hour Travel Time Validation Results

Table 3-8 compares the observed peak hour travel times to the calibrated FREQ model peak hour travel times for the study segments. As shown in **Table 3-8**, the AM and PM peak hour models were calibrated to within the acceptable 10 percent maximum deviation.



TABLE 3-8: PEAK HOUR TRAVEL TIME VALIDATION RESULTS

| Peak Direction | | Average Travel Time from Field Measurements (mm:ss) ¹ | Average Travel Time from FREQ Model (mm:ss) | Percent Difference |
|--------------------------|--------------|--|---|--------------------|
| US 101 Northbound | | | | |
| AM Peak Hour | 7:00-8:00AM | 06:33 | 06:29 | 1% |
| PM Peak Hour | 5:00-6:00 PM | 03:31 | 03:17 | 6% |
| US 101 Southbound | | | | |
| AM Peak Hour | 7:00-8:00AM | 02:17 | 02:06 | 8% |
| PM Peak Hour | 5:00-6:00 PM | 10:20 | 10:11 | 1% |
| SR 237 Westbound | | | | |
| AM Peak Hour | 7:00-8:00AM | 02:36 | 02:28 | 5% |
| PM Peak Hour | 5:00-6:00 PM | 03:36 | 03:39 | -2% |
| SR 237 Eastbound | | | | |
| AM Peak Hour | 8:00-9:00AM | 02:24 | 02:13 | 7% |
| PM Peak Hour | 5:00-6:00 PM | 02:12 | 02:07 | 4% |

Notes:

1. Travel time data was extracted from the Phase II of the SR 237 Express Lanes Study and GPS travel time runs performed along US 101 in November 2013 and confirmed through observations conducted by Fehr & Peers in November 2013.

Source: Fehr & Peers, 2016.

PEAK HOUR LEVEL OF SERVICE RESULTS

The existing operating conditions of US 101 and SR 237 were analyzed using the calibrated FREQ models. Existing study period levels of service from the FREQ model are presented in **Table 3-9** and US 101 and **Table 3-10** for SR 237. **Appendix F** provides the FREQ analysis worksheets.



TABLE 3-9: EXISTING US 101 PEAK HOUR LEVEL OF SERVICE BASED ON FREQ MODEL RESULTS

| Segment | Type | Number of Lanes | AM Peak Hour | | PM Peak Hour | |
|---|---------|------------------|---------------------------------|------------------|---------------------------------|------------------|
| | | | Density ¹ (vphpl) | LOS ² | Density ¹ (vphpl) | LOS ² |
| <i>US 101 Northbound</i> | | | <i>7AM-8AM</i> | | <i>5PM-6PM</i> | |
| Fair Oaks Off-Ramp | Diverge | 3 Mixed 1 HOV | 75.4 | F | 25.8 | C |
| Fair Oaks Off-Ramp to Fair Oaks On-Ramp | Basic | 3 Mixed 1 HOV | 68.1 | F | 21.5 | C |
| Fair Oaks On-Ramp | Merge | 3 Mixed 1 HOV | 53.8 | F | 23.4 | C |
| Fair Oaks On-Ramp to Mathilda NB Off Ramp | Basic | 3 Mixed 1 HOV | 55.6 | F | 23.4 | C |
| Mathilda NB Off-Ramp | Diverge | 3 Mixed 1 HOV | 57.3 | F | 23.4 | C |
| Mathilda NB Off-Ramp to Mathilda NB On-Ramp | Basic | 3 Mixed 1 HOV | 61.4 | F | 22.5 | C |
| Mathilda NB On-Ramp | Merge | 3 Mixed 1 HOV | 61.3 | F | 23.8 | C |
| Mathilda NB On-Ramp to Mathilda SB Off-Ramp | Basic | 3 Mixed 1 HOV | 61.5 | F | 23.8 | C |
| Mathilda SB Off-Ramp | Diverge | 3 Mixed 1 HOV | 61.7 | F | 23.8 | C |
| Mathilda SB Off-Ramp to SR 237 WB Off-Ramp | Basic | 3 Mixed 1 HOV | 66.1 | F | 20.3 | C |
| SR 237 WB Off-Ramp | Diverge | 3 Mixed 1 HOV | 70.1 | F | 20.3 | C |
| SR 237 WB Off-Ramp to SR 237 WB On-Ramp | Basic | 3 Mixed 1 HOV | 82.2 | F | 13.6 | F |
| SR 237 WB On-Ramp | Merge | 3 Mixed 1 HOV | 74.3 | F | 35.8 | F |
| SR 237 WB On-Ramp to Ellis | Basic | 3 Mixed 1 HOV | 76.9 | F | 59.8 | F |
| <i>US 101 Southbound</i> | | | <i>7AM-8AM</i> | | <i>5PM-6PM</i> | |
| Ellis On-Ramp to SR 237 EB Off-Ramp | Basic | 3 Mixed 1 HOV | 23.8 | C | 107.4 | F |
| SR 237 EB Off-Ramp | Diverge | 3 Mixed 1 HOV | 23.8 | C | 91.7 | F |
| SR 237 EB Off-Ramp to SR 237 EB On-Ramp | Basic | 3 Mixed 1 HOV | 17.0 | B | 158.2 | F |
| SR 237 EB On-Ramp | Merge | 3 Mixed 1 HOV | 15.7 | B | 181.7 | F |



TABLE 3-9: EXISTING US 101 PEAK HOUR LEVEL OF SERVICE BASED ON FREQ MODEL RESULTS

| Segment | Type | Number of Lanes | AM Peak Hour | | PM Peak Hour | |
|---|---------|-------------------------|---------------------------------|------------------|---------------------------------|------------------|
| | | | Density ¹ (vphpl) | LOS ² | Density ¹ (vphpl) | LOS ² |
| SR 237 EB On-Ramp to Mathilda Off-Ramp | Weave | 3 Mixed, 1 AUX 1 HOV | 15.7 | B | 186.2 | F |
| Mathilda Off-Ramp | Diverge | 3 Mixed 1 HOV | 15.7 | B | 182.8 | F |
| Mathilda Off-Ramp to Mathilda SB On-Ramp | Basic | 3 Mixed 1 HOV | 19.6 | C | 151.4 | F |
| Mathilda SB On-Ramp | Merge | 3 Mixed 1 HOV | 20.1 | C | 109.5 | F |
| Mathilda NB On-Ramp | Merge | 3 Mixed 1 HOV | 21.7 | C | 97.7 | F |
| Mathilda NB On-Ramp to Fair Oaks SB Off-Ramp | Basic | 3 Mixed 1 HOV | 21.7 | C | 102.6 | F |
| Fair Oaks SB Off-Ramp | Diverge | 3 Mixed 1 HOV | 21.7 | C | 97.1 | F |
| Fair Oaks SB Off-Ramp to Fair Oaks SB On-Ramp | Basic | 3 Mixed 1 HOV | 20.2 | C | 128.7 | F |
| Fair Oaks SB On-Ramp | Merge | 3 Mixed 1 HOV | 15.7 | B | 171.8 | F |
| Fair Oaks NB Off-Ramp | Diverge | 3 Mixed 1 HOV | 15.7 | B | 172.9 | F |
| Fair Oaks NB Off-Ramp to Fair Oaks NB On-Ramp | Basic | 3 Mixed 1 HOV | 20.6 | C | 126.8 | F |
| Fair Oaks NB On-Ramp | Merge | 3 Mixed 1 HOV | 22.8 | C | 117.5 | F |

Notes: **Bold** font indicates LOS F conditions. A segment may be designated LOS F even if the density is below the LOS F threshold if any portion of the segment is in queue.

1. Density presented in vehicles per hour per lane for the mixed-flow lanes.
2. LOS presented for the mixed-flow lanes.

Source: Fehr & Peers, 2016.



TABLE 3-10: EXISTING SR 237 PEAK HOUR LEVEL OF SERVICE BASED ON FREQ MODEL RESULTS

| Segment | Type | Number of Lanes | AM Peak Hour | | PM Peak Hour | |
|---|---------|------------------|---------------------------------|----------|---------------------------------|----------|
| | | | Density ¹ (vphpl) | LOS | Density ¹ (vphpl) | LOS |
| <i>SR 237 Westbound</i> | | | <i>7AM-8AM</i> | | <i>5PM-6PM</i> | |
| Lawrence On-Ramp to Crossman On-Ramp | Basic | 3 Mixed | 23.0 | C | 19.2 | B |
| Crossman On-Ramp | Merge | 3 Mixed | 24.5 | C | 22.1 | C |
| Crossman On-Ramp to Mathilda Off-Ramp | Basic | 3 Mixed | 24.5 | C | 47.9 | F |
| Mathilda Off-Ramp | Diverge | 3 Mixed | 27.1 | C | 55.0 | F |
| Mathilda Off-Ramp to Mathilda On-Ramp | Basic | 2 Mixed | 40.4 | E | 84.4 | F |
| Mathilda On-Ramp to US 101 NB Off-Ramp | Weave | 2 Mixed, 1 AUX | 48.4 | F | 53.3 | F |
| US 101 NB Off-Ramp to US 101 NB On-Ramp | Basic | 2 Mixed | 18.5 | B | 19.4 | B |
| US 101 NB On-Ramp | Merge | 2 Mixed | 26.7 | C | 28.2 | D |
| Maude Off-Ramp | Diverge | 2 Mixed | 26.7 | C | 28.2 | D |
| <i>SR 237 Eastbound</i> | | | <i>8AM-9AM</i> | | <i>5PM-6PM</i> | |
| Maude On-Ramp to US 101 SB Off-Ramp | Weave | 2 Mixed, 1 AUX | 19.7 | C | 14.3 | B |
| US 101 SB Off-Ramp to US 101 SB On-Ramp | Basic | 2 Mixed | 20.3 | C | 16.5 | B |
| US 101 SB On-Ramp | Merge | 2 Mixed, 1 AUX | 22.3 | C | 14.6 | B |
| US 101 SB On-Ramp to Mathilda Off-Ramp | Basic | 2 Mixed, 1 AUX | 22.3 | C | 14.6 | B |
| Mathilda Off-Ramp | Diverge | 2 Mixed, 1 AUX | 22.3 | C | 14.6 | B |
| Mathilda Off-Ramp to Mathilda On-Ramp | Basic | 2 Mixed | 29.0 | D | 20.1 | C |
| Mathilda On-Ramp | Merge | 2 Mixed | 38.7 | E | 29.4 | D |
| Mathilda On-Ramp to Start HOV Lane | Basic | 2 Mixed | 33.3 | D | 22.2 | C |
| Start HOV Lane to Persian Off-Ramp | Diverge | 2 Mixed 1 HOV | 33.3 | D | 22.2 | C |
| Persian Off-Ramp to Lawrence | Basic | 2 Mixed 1 HOV | 32.5 | D | 19.6 | C |

Notes: **Bold** font indicates LOS F conditions. A segment may be designated LOS F even if the density is below the LOS F threshold if any portion of the segment is in queue.

1. Density presented in vehicles per hour per lane for the mixed-flow lanes.

Source: Fehr & Peers, 2016.



Leisch Method Weaving Analysis

Auxiliary lanes are provided intermittently along US 101 and SR 237 in both directions within the study area. **Table 3-11** summarizes the peak hour mainline weaving operations at locations that provide an auxiliary lane using the Leisch Method.² The Leisch Method analysis was applied for the demand mainline and ramp volumes.

TABLE 3-11: EXISTING PEAK HOUR WEAIVING ANALYSIS BASED ON LEISCH METHOD

| Segment | Direction | Number of Lanes | AM Peak Hour LOS | PM Peak Hour LOS |
|---|-----------|--------------------------|--------------------|--------------------|
| US 101 | | | | |
| SR 237 EB on-ramp to Mathilda Avenue off-ramp | SB | 4 Mainline 1 Aux Lane | LOS C (8AM-9AM) | LOS D (4PM-5PM) |
| SR 237 | | | | |
| Mathilda Avenue on-ramp to US 101 NB off-ramp | WB | 2 Mainline 1 Aux Lane | LOS D (7AM-8AM) | LOS F (5PM-6PM) |
| US 101 on-ramp to Mathilda Avenue off-ramp | EB | 2 Mainline 1 Aux Lane | LOS E (8AM-9AM) | LOS B (5PM-6PM) |

Source: Fehr & Peers, 2016.

As the results show, the weave sections operate between LOS B and LOS F. **Appendix G** provides the Leisch analysis worksheets. These results differ from the FREQ results presented in **Table 3-9** and **Table 3-10** for the following reasons:

- FREQ is not a weaving analysis tool.
- Leisch Method uses default mainline capacities while FREQ models use calibrated capacities to reflect observed conditions.
- Leisch Method evaluates mainline segments in isolation so that bottlenecks and mainline queuing do not impact downstream or upstream traffic. FREQ models consider the effects of the bottlenecks and mainline queuing on the entire mainline system.

FREWAY SYSTEM PERFORMANCE

Existing hourly system-wide MOEs for the two-hour AM and three-hour PM peak period results are presented in **Table 3-12** through **Table 3-13**. **Appendix F** provides the FREQ analysis worksheets. Each of the MOEs is discussed below.

Vehicle Miles Traveled (VMT)

VMT represents the total distance traveled by all vehicles using the US 101 and SR 237 study corridors. VMT is the sum of the volume served for each segment multiplied by the length of each segment. The highest

² Procedures for Analysis and Design of Weaving Sections: A Users Guide. Jack E. Leisch, October 1985. The Leisch Method is one of the methodologies accepted by Caltrans for the analysis of freeway weaving sections.



VMT along the US 101 corridor occurs during the southbound PM peak period, while the lowest occurs during the southbound AM peak period. The highest VMT along the SR 237 corridor occurs during the westbound PM peak period, while the lowest occurs during the eastbound AM peak period.

Average Travel Time (ATT)

The Average Travel Time (ATT) for US 101 is longest in the southbound direction during the PM peak period, with an average time of 9 minutes and 29 seconds resulting in an average travel speed of 13 mph. The average travel speed along US 101 was about 20 mph during for the northbound AM peak period. SR 237 experienced the highest average travel time during the westbound PM peak period with a time of 2 minutes and 49 seconds. The lowest average travel time on SR 237 was eastbound in the PM peak period with a travel time of 2 minutes and 6 seconds.

Vehicle Delay

Vehicle delay is the amount of delay incurred during the peak period as a result of congestion and demand exceeding the capacity of a freeway segment. Vehicle delays were computed using the FREQ model output and are represented in units of vehicle-hours. For this study, vehicle delay is defined as the difference between the time it takes to travel a segment at a speed below the free-flow speed and the free-flow speed. It is important to note that this definition of vehicle delay is different from the definition used within the Mobility Performance Report (MPR) managed by Caltrans' Mobility Performance Reporting and Analysis Program. Vehicle delay in the MPR is defined as the time it takes to travel a segment at a recorded congested speed and the travel time at 35 mph (i.e., speeds above 35 mph are not considered congested).

As shown in **Table 3-12**, during the PM peak period the US 101 southbound direction experiences 1,695 vehicle-hours of delay compared to 662 vehicle-hours of delay for the northbound direction in the AM peak period. US 101 generally operates at free flow during the northbound PM and southbound AM study periods at 45 mph and 60 mph, respectively. **Table 3-13** shows that during the AM peak period, the SR 237 westbound direction experiences 41 vehicle-hours of delay compared to 11 vehicle-hours of delay for the eastbound direction during the PM peak period.



TABLE 3-12: EXISTING US 101 STUDY PERIOD MEASURES OF EFFECTIVENESS¹

| Measures of Effectiveness | AM Peak Period | PM Peak Period |
|--|----------------|----------------|
| Northbound | | |
| Vehicle Miles of Travel (vehicle-miles) | 20,110 | 24,630 |
| Average Travel Time (min:sec) ¹ | 06:25 | 02:52 |
| Average Travel Speed (mph) ¹ | 20 | 45 |
| Mainline Vehicle Delay (vehicle-hours) | 662 | 160 |
| Maximum Individual Vehicle Delay (min:sec) | 04:30 | 01:18 |
| Southbound | | |
| Vehicle Miles of Travel (vehicle-miles) | 17,800 | 28,150 |
| Average Travel Time (min:sec) | 02:07 | 09:29 |
| Average Travel Speed (mph) | 60 | 13 |
| Mainline Vehicle Delay (vehicle-hours) | 24 | 1,695 |
| Maximum Individual Vehicle Delay (min:sec) | 00:11 | 08:16 |

Notes:

1. Average Travel Time and Average Travel Speed differ from those presented in Table 2-4. Table 2-4 demonstrates the travel time and speed for each hour within the peak period and Table 3-12 demonstrates the travel time and speed for the peak period.
Source: Fehr & Peers, 2016.

TABLE 3-13: EXISTING SR 237 STUDY PERIOD MEASURES OF EFFECTIVENESS¹

| Measures of Effectiveness | AM Peak Period | PM Peak Period |
|--|----------------|----------------|
| Westbound | | |
| Vehicle Miles of Travel (vehicle-miles) | 18,560 | 23,060 |
| Average Travel Time (min:sec) ¹ | 02:22 | 02:49 |
| Average Travel Speed (mph) ¹ | 56 | 47 |
| Mainline Vehicle Delay (vehicle-hours) | 41 | 136 |
| Maximum Individual Vehicle Delay (min:sec) | 00:25 | 01:37 |
| Eastbound | | |
| Vehicle Miles of Travel (vehicle-miles) | 17,650 | 20,720 |
| Average Travel Time (min:sec) | 02:08 | 02:06 |
| Average Travel Speed (mph) | 62 | 63 |
| Mainline Vehicle Delay (vehicle-hours) | 12 | 11 |
| Maximum Individual Vehicle Delay (min:sec) | 00:10 | 00:04 |

Notes:

1. Average Travel Time and Average Travel Speed differ from those presented in Table 2-5. Table 2-5 demonstrates the travel time and speed for each hour within the peak period and Table 3-13 demonstrates the travel time and speed for the peak period.
Source: Fehr & Peers, 2016.



EXISTING (2013) TRANSIT SERVICE AND FACILITIES

The project area includes the Lockheed Martin and the Moffett Park light rail transit (LRT) stations, which are on the Mountain View to Winchester Avenue LRT line (Line 902) operated by the VTA. VTA also operates bus service in the area. **Figure 5** shows the existing transit service near the project site, which is described in detail below and summarized in **Table 3-14**. The table includes the origin and destination, the operating hours, the headways, and the average peak load factors for each route. The average peak load factor is a measure of resource utilization. It compares the supply of seats on a bus versus the average peak number of on-board passengers at any time during the peak period. For all-day service, the average peak load factor is based on the average over the entire day. A load factor of 1.0 would indicate that all seats are full.



TABLE 3-14: EXISTING TRANSIT SERVICE

| Route | From | To | Load Factor ¹ | Weekdays | | Weekends | |
|------------------------------------|--------------------------------|--------------------------------|--------------------------|-------------------------------------|-------------------------------------|------------------------------------|--------------------------------|
| | | | | Operating Hours | Peak Headway ² (minutes) | Operating Hours | Headway ² (minutes) |
| Bus Service (VTA) | | | | | | | |
| 32 | San Antonio Transit Center | Santa Clara Transit Center | 0.35 | 5:45 a – 8:03 p | 30 – 60 | 8:50 a – 5:51 p (Saturday Only) | 60 (Saturday Only) |
| 26 | Eastridge Transit Center | | 0.53 | 5:21 a – 11:49 p | 30 | 6:24 a – 10:45 p | 30 – 60 |
| 54 | De Anza College | | 0.45 | 6:01 a – 9:30 p | 30 | 7:58 a – 7:52 p | 45 – 60 |
| 120 | Fremont BART Station | | 0.69 | 6:12 a – 9:17 a 4:05 p – 7:10 p | AM: 6 SB Trips PM: 6 NB Trips | No Service | |
| 121 | Gilroy Transit Center | | 0.53 | 4:30 a – 9:17 a 3:00 p – 7:37 p | AM: 9 SB Trips PM: 9 NB Trips | No Service | |
| 122 | Santa Teresa LRT Station | Lockheed Martin Transit Center | 0.34 | 5:52 a – 6:45 a 4:48 p – 5:58 p | AM: 1 NB Trip PM: 1 SB Trip | No Service | |
| 321 | Great Mall/Main Transit Center | | 0.12 | 8:10 a – 8:46 a 5:50 p – 6:32 p | AM: 1 WB Trip PM: 1 EB Trip | No Service | |
| 328 | South San Jose | | 0.30 | 6:00 a – 8:40 a 4:55 p – 7:13 p | AM: 2 NB Trips PM: 2 SB Trips | No Service | |
| 826 (ACE) | ACE Great America Station | | N/A | 6:16 a – 9:38 a 3:11 p – 6:39 p | 4 WB Trips – AM 4 EB Trips – PM | No Service | |
| Mary/Moffett Area Caltrain Shuttle | Mountain View Caltrain Station | Alma Plaza | N/A | 7:05 a – 10:21 a 2:50 p – 6:30 p | AM: 4 NB Trips PM: 4 SB Trips | No Service | |
| Light Rail Service (VTA) | | | | | | | |
| 902 | Downtown Mountain View | Winchester | 0.42 | 5:06 a – 12:09 a | 15 | 6:02 a – 12:05 a | 30 |

Notes:

1. Average peak load factor is the ratio of the average peak number of on-board passengers aboard during the peak period to supply of seats.
2. Headways are defined as the time interval between two transit vehicles traveling in the same direction over the same route.

Source: VTA, January 2014.



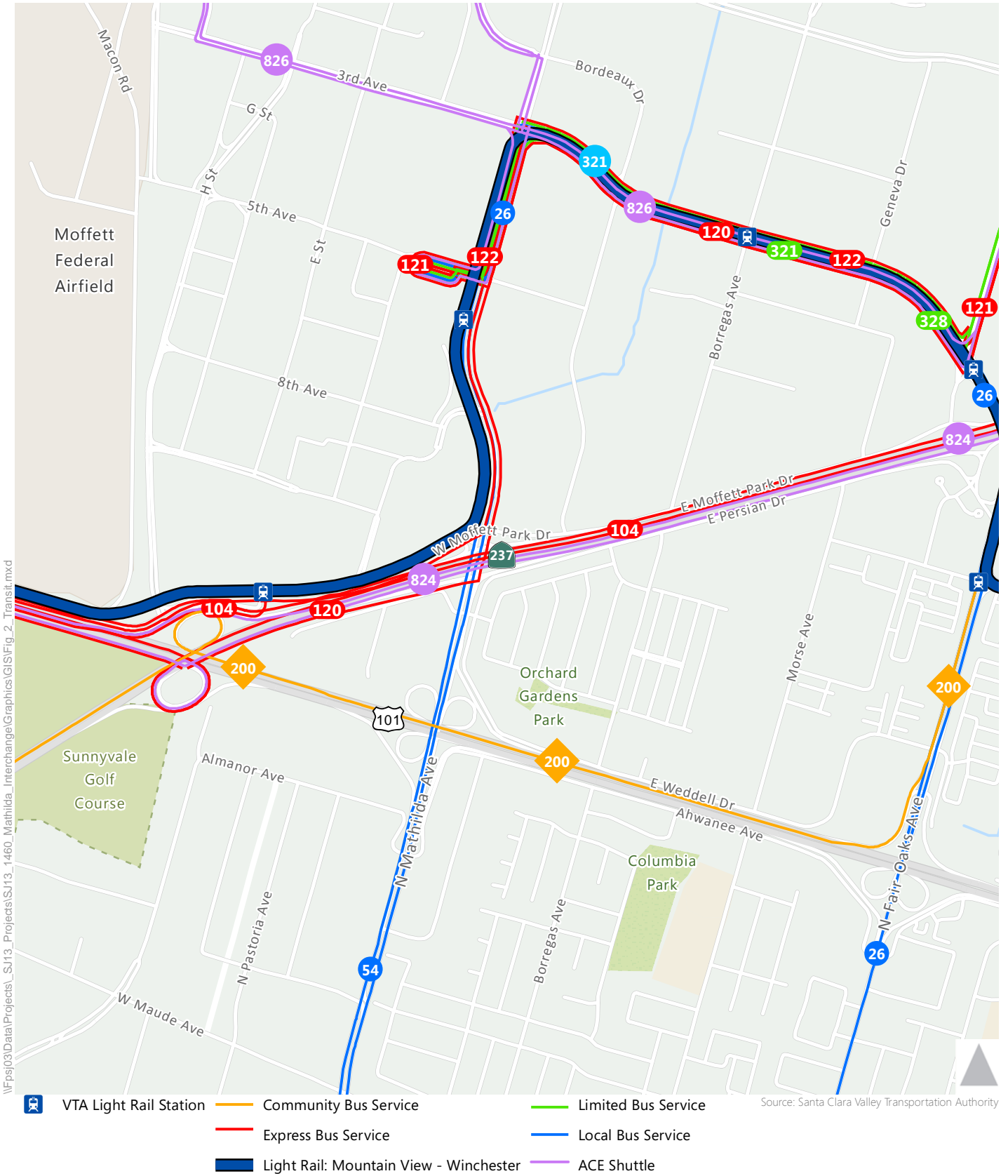


Figure 5
Existing Transit Service
Mathilda Avenue Improvements



VTA LRT AND LOCAL BUS ROUTES

The VTA Mountain View to Winchester Avenue LRT runs along Java Drive, Mathilda Avenue, Moffett Park Drive, and Manila Drive near the project. LRT Line 902 stops at the Lockheed Martin and the Moffett Park stations within the study area.

Bus Route 26 operates on Mathilda Avenue, Java Drive, and Fair Oaks Avenue. Route 26 provides service between the Eastridge Mall and Lockheed Martin/Moffett Park transit centers. Route 26 follows major arterials and travels through Sunnyvale, Cupertino, San Jose, and Campbell. Bus stops for Route 26 are provided at Java Drive and the Lockheed Martin/Moffett Park Transit Center.

Bus Route 54 operates on Mathilda Avenue, Java Drive, and Fair Oaks Avenue. Route 54 provides service between De Anza College and Sunnyvale/Fair Oaks Avenue. Bus stops for Route 54 are provided along Mathilda Avenue near Maude Avenue, Ahwanee Avenue, Ross Drive, and north of Moffett Park Drive at the Lockheed Martin/Moffett Park Transit Center.

Bus Route 32 operates on Central Expressway and Mathilda Avenue and can be used as a connection to Bus Route 54. Route 32 provides service between the San Antonio and Santa Clara transit centers. Route 32 follows major arterials and travels through Mountain View, Sunnyvale, and Santa Clara

EXPRESS AND LIMITED STOP BUS ROUTES

The VTA also runs several express bus routes and limited stop bus routes throughout the project area.

Bus Route 120 is an express bus route that operates on SR 237, Caribbean Drive, Java Drive, and Mathilda Avenue; it connects the Fremont BART Station to the Lockheed Martin Transit Center. Six Route 120 trips occur during each weekday peak period (to the project area in the morning and from it in the afternoon).

Bus Route 121 is an express bus route that operates on Lawrence Expressway, Caribbean Drive, Java Drive, and Mathilda Avenue; it connects the Gilroy Transit Center and Morgan Hill Caltrain Station to the Lockheed Martin Transit Center. Nine Route 121 trips occur during each weekday peak period (to the project area in the morning and from it in the afternoon).

Bus Route 122 is an express bus route that operates on US 101, Lawrence Expressway, Caribbean Drive, Java Drive, and Mathilda Avenue; it connects south the Santa Teresa LRT Station in San Jose to the Lockheed Martin Transit Center. One Route 122 trip occurs during each weekday peak period (away from the project area in the morning and to it in the afternoon).

Bus Route 321 is a limited stop bus route that operates on Lawrence Expressway, Caribbean Drive, Java Drive, and Mathilda Avenue; it connects the Great Mall Transit Center in Milpitas to the Lockheed Martin Transit Center. Two Route 321 trips occurs during each weekday peak period (away from the project area in the morning and to it in the afternoon).



Bus Route 328 is a limited stop bus route that operates on Lawrence Expressway, Caribbean Drive, Java Drive, and Mathilda Avenue; it connects south San Jose near Almaden Expressway to the Lockheed Martin Transit Center.

Additionally, *Bus Route 104* passes through the study area on US 101 and SR 237; it connects Palo Alto, Mountain View, Milpitas, and San Jose.

CALTRAIN AND ACE SHUTTLES

Caltrain provides intercity passenger rail service between San Francisco and San Jose, with extended service to Morgan Hill and Gilroy during weekday commute hours. Four *Mary/Moffett Area Caltrain Shuttle* runs connect the Mountain View Caltrain Station with office buildings in the Mary Avenue and Moffett Park areas. During weekday AM and PM commute periods, the Caltrain shuttle operates every 50 to 60 minutes on Mathilda Avenue with a stop near Ahwanee Avenue; there is another stop on Hamlin Court off Ross Drive. The Mountain View station is a designated express train station for Caltrain. Bus service between the Sunnyvale Caltrain Station and the Moffett Park area is provided by VTA Route 54. Additional private shuttles to the Moffett Park area from the Sunnyvale Caltrain Station are operated by local employers. These services are generally limited to the specific employer(s).

The *Altamont Corridor Express (ACE)* provides passenger rail service between Stockton and San Jose. The *ACE Red Line Shuttle (Route 826)* provides free shuttle service between buildings in the Moffett Park and the ACE Great America Station in Santa Clara. This shuttle operates on Mathilda Avenue north of the study area. Shuttle stops are provided at the Lockheed Martin/Moffett Park Transit Center. Four shuttle trips operate during each commute period with 60-minute headways in the morning and 30 to 80 minute headways in the evening.

LOCAL SHUTTLES

There are a number of local public and private shuttles specific to Moffett Park Area that provide service within Moffett Park and to surrounding neighborhoods and major transit facilities. The Moffett Park Business & Transportation Association provides information on available public shuttle programs to the tenants in Moffett Park.

EXISTING (2013) BICYCLE AND PEDESTRIAN FACILITIES

Pedestrian and bicycle volumes were collected at all study intersections in November 2013. Pedestrian and bicycle count worksheets are provided in **Appendix A**. There is moderate bicycle use along Moffett Park Drive during the peak hours; most other movements have only a few cyclists. Along Mathilda Avenue pedestrian volumes are low and due to the lack of pedestrian facilities on the project's frontage streets (Borregas Avenue, Bordeaux Drive, Moffett Park Drive) pedestrian activity is almost non-existent.



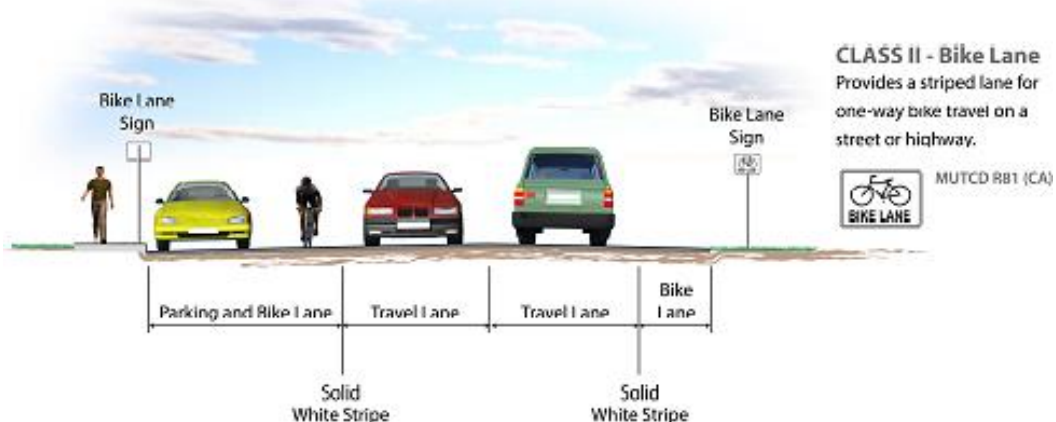
BICYCLE FACILITIES

Bikeway planning and design in California typically relies on guidelines and design standards established by California Department of Transportation (Caltrans) in the *Highway Design Manual* (Chapter 1000: Bikeway Planning and Design).

- Class I Bikeway (Bike Path) provides a completely separate right-of-way and is designated for the exclusive use of bicycles and pedestrians with vehicle and pedestrian cross-flow minimized. In general, bike paths serve corridors not served by streets and highways or where sufficient right-of-way exists to allow such facilities to be constructed away from the influence of parallel streets and vehicle conflicts.

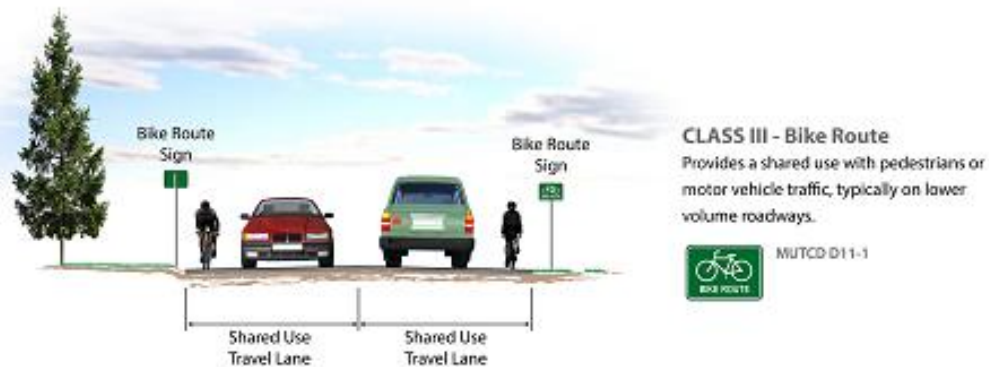


- Class II Bikeways (Bike Lanes) are lanes for bicyclists generally adjacent to the outer vehicle travel lanes. These lanes have special lane markings, pavement legends, and signage. Bicycle lanes are generally five (5) feet wide. Adjacent vehicle parking and vehicle/pedestrian cross-flow are permitted.

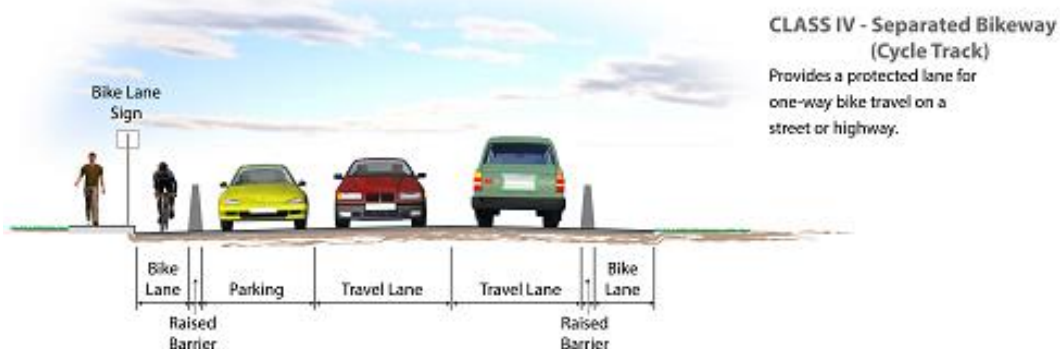


- Class III Bikeway (Bike Route) are designated by signs or pavement markings for shared use with pedestrians or motor vehicles, but have no separated bike right-of-way or lane striping. Bike routes serve either to: a) provide continuity to other bicycle facilities, or b) designate preferred routes through high demand corridors.





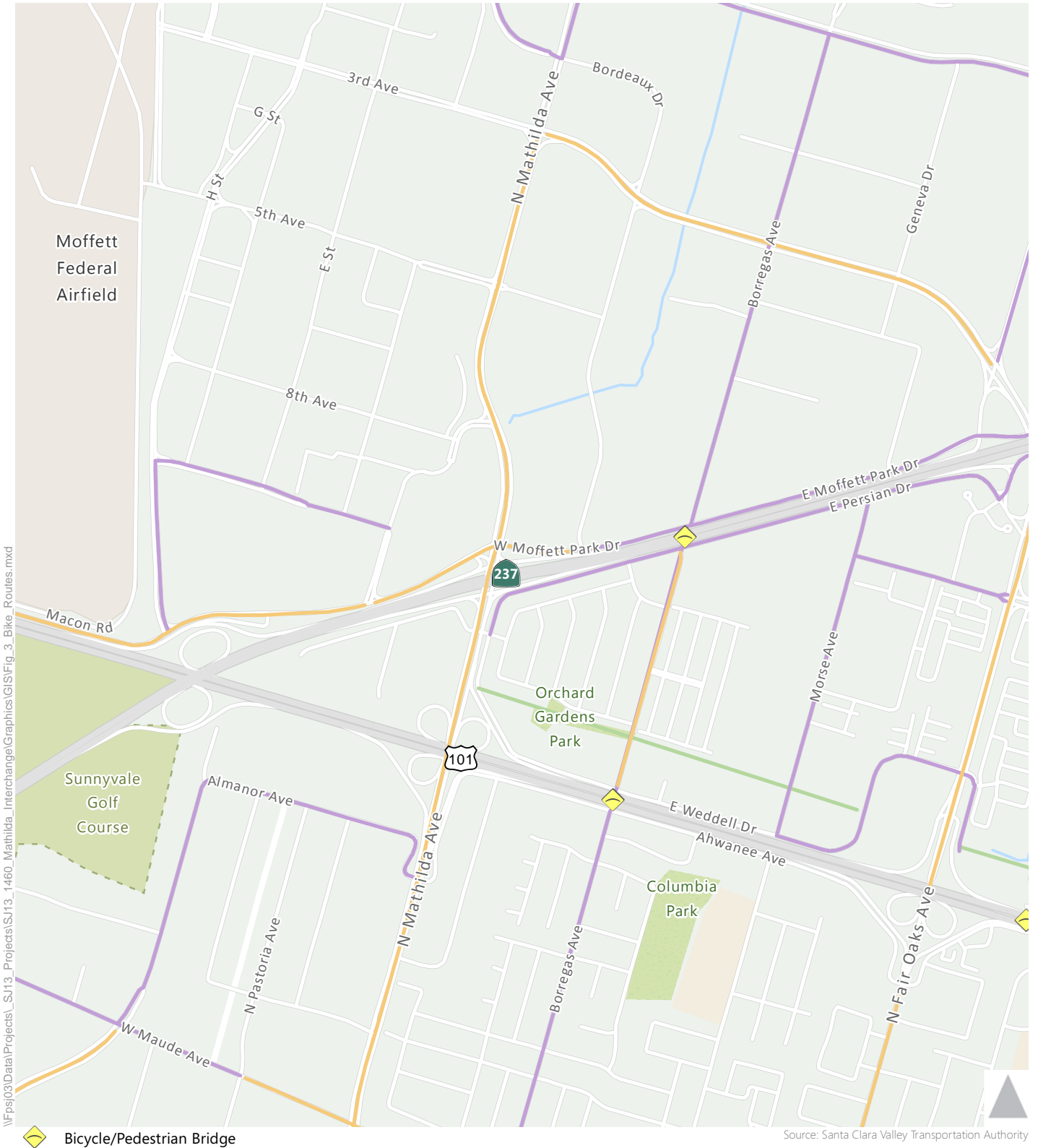
- Class IV Bikeways (Cycletracks or Protected Bike Lanes) provide a right-of-way designated exclusively for bicycle travel within a roadway and which are protected from other vehicle traffic with devices, including, but not limited to, grade separation, flexible posts, inflexible physical barriers, or parked cars



The VTA *Bicycle Technical Guidelines* (2012) recommend standards regarding bicycle facility dimension and provides supplemental information and guidance on when and how to better accommodate the many types of bicyclists. **Figure 6** shows the location of the existing bicycle facilities within the project study area. VTA has adopted the Santa Clara *Countywide Bicycle Plan* (CBP) in August 2008. The CBP guides the development of major bicycling facilities by identifying Cross County Bicycle Corridors and other projects of countywide or intercity significance. Several of these routes travel through the study area, including routes along Mary Avenue, Maude Avenue, Middlefield Road, Ellis Street, and Manila Drive/Moffett Park Drive.

Bicycle lanes are provided in both directions on both Bordeaux Drive (between Moffett Park Drive and Java Drive) and Borregas Avenue (between Moffett Park Drive and Caribbean Drive). Bicycle lanes are provided on Mathilda Avenue (north of Bordeaux Drive) and Moffett Park Drive (east of Bordeaux Drive). A bicycle route is designated on Mathilda Avenue from Bordeaux Drive to Innovation Way. A bicycle path extends from the north-east of the US 101/Mathilda Avenue interchange along the John W. Christian Greenbelt from Garner Drive to Morse Avenue, where it connects with existing Class II bike lanes along Weddell Drive. Multi-use Class I bicycle/pedestrian trails are provided along the San Francisco Bay Trail toward the north of the study area and the Calabazas Creek parallel and east of Lawrence Expressway along the eastern border of the City of Sunnyvale.





\\Fps03\Data\Projects\SJ13_P\Projects\SJ13_1460_Mathilda_Interchange\Graphics\GIS\Fig_3_Bike_Routes.mxd

Figure 6

Existing Bicycle Facilities
Mathilda Avenue Improvements





PEDESTRIAN FACILITIES

Pedestrian facilities consist of sidewalks, crosswalks, and pedestrian signals at signalized intersections. In the project area there are no sidewalks on Moffett Park Drive, Bordeaux Drive or Borregas Avenue, though the City has identified sidewalks on Moffett Park Drive as a future pedestrian improvement. Most study intersections include crosswalks and pedestrian signals on all approaches.

Sidewalks are provided on both sides of Mathilda Avenue between Fifth Avenue and Moffett Park Drive. South of Moffett Park Drive sidewalks are provided on the east side of Mathilda Avenue until Ross Drive. At the Mathilda Avenue/SR 237 interchange, north-south pedestrian movements are limited to the east side of Mathilda Avenue and east-west crossing of Mathilda Avenue is prohibited within the interchange area. Pedestrians crossing Mathilda (east-west) have to use the crosswalk on the north leg of the Mathilda Avenue/Moffett Park Drive intersection. Sidewalks continue on the east side of Mathilda Avenue from the SR 237 interchange to south of the US 101 interchange, at which point sidewalks continue on both sides of Mathilda Avenue.

A multi-use pedestrian/bicycle bridge crosses SR 237 and US 101 east of Mathilda Avenue providing a pedestrian/bicycle connection between Moffett Park to the north and the residential neighborhood to the south. There is currently an uncontrolled crosswalk located on the west leg of the Moffett Park Drive/Borregas Avenue intersection; however, there are currently no sidewalks connecting to the crosswalk at any point of the intersection.



EXISTING (2013) COLLISION HISTORY DATA

This section summarizes collision statistics for key mainline and arterials within the study area.

LOCAL STREET COLLISION HISTORY

Three years (January 2011 – December 2013) of collision data on local streets within the project study limits was provided by the City of Sunnyvale Division of Transportation and Traffic. **Table 3-15** and **Table 3-16** summarize the city collision data on local streets within the project study limits by analysis location and by collision type, respectively.

Table 3-15 shows that 86 of the 548 reported collisions during the time period were injury collisions.



TABLE 3-15: LOCAL STREET COLLISION DATA – JANUARY 2011 THROUGH DECEMBER 2013

| Location | Total Collisions | Collisions Involving Pedestrians | Collisions Involving Bicycles | Collisions Resulting in Injury | Collisions Resulting in Fatality |
|---|------------------|----------------------------------|-------------------------------|--------------------------------|----------------------------------|
| Moffett Park Dr. (Manila Dr. to Borregas Ave.)* | 30 | 0 | 3 | 7 | 0 |
| Mathilda Ave. (California Ave. to 5th Ave.)* | 274 | 1 | 3 | 42 | 0 |
| Moffett Park Dr./Borregas Ave. Intersection | 3 | 0 | 1 | 1 | 0 |
| Moffett Park Dr./Bordeaux Dr. Intersection | 1 | 0 | 0 | 0 | 0 |
| Moffett Park Dr./Enterprise Way Intersection | 1 | 0 | 0 | 0 | 0 |
| Moffett Park Dr./Innovation Way Intersection | 1 | 0 | 0 | 1 | 0 |
| Moffett Park Dr./Manila Dr. Intersection | 1 | 0 | 0 | 0 | 0 |
| Mathilda Ave./California Ave. Intersection | 20 | 0 | 0 | 3 | 0 |
| Mathilda Ave./Central Expressway Intersection | 5 | 0 | 0 | 0 | 0 |
| Mathilda Ave./Indio Way Intersection | 14 | 0 | 0 | 3 | 0 |
| Mathilda Ave./Maude Ave. Intersection | 30 | 1 | 1 | 2 | 0 |
| Mathilda Ave./Del Rey Ave. Intersection | 8 | 0 | 0 | 2 | 0 |
| Mathilda Ave./San Aleso Ave. Intersection | 8 | 0 | 0 | 2 | 0 |
| Mathilda Ave./Ahwanee Ave. Intersection | 26 | 0 | 0 | 1 | 0 |
| Mathilda Ave./US 101 SB On-Ramp Intersection | 2 | 0 | 0 | 0 | 0 |
| Mathilda Ave./US 101 NB On-Ramp Intersection | 1 | 0 | 0 | 0 | 0 |
| Mathilda Ave./Ross Dr. Intersection | 26 | 0 | 0 | 7 | 0 |
| Mathilda Ave./SR 237 EB Off-Ramp Intersection | 20 | 0 | 0 | 2 | 0 |
| Mathilda Ave./SR 237 Intersection | 35 | 0 | 0 | 5 | 0 |
| Mathilda Ave./SR 237 WB Ramps Intersection | 13 | 0 | 0 | 3 | 0 |
| Mathilda Ave./Moffett Park Dr. Intersection | 24 | 0 | 1 | 5 | 0 |
| Mathilda Ave./Innovation Way Intersection | 5 | 0 | 0 | 0 | 0 |

Notes:

*Indicates collisions along a roadway segment, not at an intersection.

Source: City of Sunnyvale collision data January 1, 2011 to December 31, 2013.



TABLE 3-16: LOCAL STREET COLLISION TYPES – JANUARY 2011 THROUGH DECEMBER 2013

| Collision Type | Total Percent (%) |
|-----------------|-------------------|
| Head-On | 1.4 |
| Sideswipe | 2.4 |
| Rear End | 8.7 |
| Broadside | 9.6 |
| Hit Object | 4.2 |
| Overturn | 0.7 |
| Auto/Pedestrian | 0.4 |
| Auto/Bicycle | 2.0 |
| Not Stated | 70.6 |
| Other | 0.0 |

Source: City of Sunnyvale collision data January 1, 2011 to December 31, 2013.

A total of 548 collisions were reported on the local streets within the project study limits over a three-year period including 86 injury accidents (see **Table 3-15**). The highest number of accidents occurred at the intersection of Mathilda Avenue and the SR 237 ramp intersection. The intersections of Mathilda Avenue/Moffett Park Drive, Mathilda Avenue/Ross Drive, and Mathilda Avenue/Maude Avenue, also had high numbers of collisions.

Rear-end and broadside type collisions that are generally due to driver inattention, unsafe speeds, and lane changing in traffic congestion, accounted for 18 percent of the accidents.

MAINLINE COLLISION HISTORY

Caltrans staff provided collision data for SR 237 and US 101 through the study area for the three-year period between January 2011 and December 2013 through their Traffic Accident Surveillance and Analysis System (TASAS Table B). **Table 3-17** and **Table 3-18** summarize the state collision data by collision type and analysis location, respectively. Collision rates along the mainline were higher during the three year period compared to the statewide average for similar facilities. Having a higher than average collision rate can result in additional delay due to lane blockages and police activity related to these collisions.

As shown on **Table 3-18**, seven locations along the study area ramps and mainline experienced total collision rates higher than the statewide average.



TABLE 3-17: FREEWAY COLLISION TYPES – JANUARY 2011 THROUGH DECEMBER 2013

| Code | Collision Type | SR 237 | | US 101 | |
|------|-----------------|--------------|-----------|--------------|-----------|
| | | Mainline (%) | Ramps (%) | Mainline (%) | Ramps (%) |
| A | Head-on | 0.0 | 6.7 | 0.0 | 4.3 |
| B | Sideswipe | 8.9 | 13.3 | 24.5 | 2.1 |
| C | Rear End | 78.6 | 43.3 | 55.8 | 25.5 |
| D | Broadside | 0.7 | 16.7 | 2.0 | 2.1 |
| E | Hit Object | 8.2 | 16.7 | 16.3 | 55.3 |
| F | Overturn | 2.2 | 3.3 | 1.4 | 10.7 |
| G | Auto-Pedestrian | 0.0 | 0.0 | 0.0 | 0.0 |
| H | Other | 0.7 | 0.0 | 0.0 | 0.0 |
| - | Not Stated | 0.7 | 0.0 | 0.0 | 0.0 |

Source: Caltrans TASAS data January 1, 2011 to December 31, 2013.



TABLE 3-18: FREEWAY COLLISION DATA – JANUARY 2011 THROUGH DECEMBER 2013

| Location Description | Number of Collisions | | | Actual Collision Rate (acc/million veh miles) | | | Average Collision Rate (acc/million veh miles) | | |
|---|----------------------|-------|-----|--|--------------|-------------|---|-------|------|
| | Total | Fatal | F+I | Total | Fatal | F+I | Total | Fatal | F+I |
| US 101 (PM 45.000 to 46.500) | 147 | 0 | 42 | 0.58 | 0.000 | 0.17 | 0.80 | 0.003 | 0.25 |
| US 101 (PM 45.544) NB off-ramp to NB Mathilda Ave. | 2 | 0 | 0 | 0.44 | 0.000 | 0.00 | 0.75 | 0.004 | 0.24 |
| US 101 (PM 45.631) SB on-ramp from NB Mathilda Ave. | 5 | 0 | 2 | 0.71 | 0.000 | 0.28 | 0.57 | 0.003 | 0.18 |
| US 101 (PM 45.644) NB on-ramp from NB Mathilda Ave. | 4 | 0 | 0 | 0.86 | 0.000 | 0.00 | 0.73 | 0.002 | 0.21 |
| US 101 (PM 45.721) SB on-ramp from SB Mathilda Ave. | 1 | 0 | 0 | 0.19 | 0.000 | 0.00 | 0.73 | 0.002 | 0.21 |
| US 101 (PM 45.734) NB off-ramp to SB Mathilda Ave. | 10 | 0 | 3 | 1.20 | 0.000 | 0.36 | 1.06 | 0.003 | 0.30 |
| US 101 (PM 45.821) SB off-ramp to SB Mathilda Ave. | 3 | 0 | 2 | 0.52 | 0.000 | 0.34 | 0.75 | 0.004 | 0.24 |
| US 101 (PM 46.111) SB off-ramp to EB SR 237 | 8 | 0 | 2 | 0.40 | 0.000 | 0.10 | 0.68 | 0.004 | 0.20 |
| US 101 (PM 46.154) NB off-ramp to WB SR 237 | 12 | 0 | 3 | 1.20 | 0.000 | 0.30 | 0.68 | 0.004 | 0.20 |
| US 101 (PM 46.156) 101/Seg NB on FR Frontage Rd | 0 | 0 | 0 | 0.00 | 0.000 | 0.00 | 0.41 | 0.000 | 0.13 |
| US 101 (PM 46.254) NB on FR WB 237/FRTGE Rd | 2 | 0 | 0 | 0.08 | 0.000 | 0.00 | 0.18 | 0.001 | 0.06 |
| SR 237 (PM M2.000 to R3.501) | 135 | 1 | 44 | 0.98 | 0.007 | 0.32 | 0.94 | 0.006 | 0.30 |
| SR 237 (PM M2.018) WB off-ramp to Maude/Middlefield | 2 | 0 | 1 | 0.35 | 0.000 | 0.17 | 1.01 | 0.003 | 0.35 |
| SR 237 (PM M2.055) EB on-ramp from Maude/Middlefield | 1 | 0 | 0 | 0.00 | 0.000 | 0.19 | 0.63 | 0.002 | 0.22 |
| SR 237 (PM 2.294) EB off-ramp to SB US 101 | 1 | 0 | 1 | 0.09 | 0.000 | 0.09 | 0.38 | 0.005 | 0.13 |
| SR 237 (PM 2.661) WB off-ramp to NB US 101 | 3 | 0 | 0 | 0.12 | 0.000 | 0.00 | 0.38 | 0.005 | 0.13 |
| SR 237 (PM 2.834) EB off-ramp to Mathilda Ave. | 2 | 0 | 1 | 0.33 | 0.000 | 0.17 | 1.01 | 0.003 | 0.35 |
| SR 237 (PM 2.841) WB on-ramp from Mathilda Ave. | 3 | 0 | 1 | 0.47 | 0.000 | 0.16 | 0.63 | 0.002 | 0.22 |
| SR 237 (PM 2.981) WB on-ramp from Moffett Park | 0 | 0 | 0 | 0.00 | 0.000 | 0.00 | 0.46 | 0.001 | 0.13 |
| SR 237 (PM 3.174) EB on-ramp from Mathilda Ave. | 4 | 0 | 2 | 0.41 | 0.000 | 0.20 | 0.63 | 0.002 | 0.22 |
| SR 237 (PM 3.181) WB off-ramp to Mathilda Ave. | 14 | 0 | 8 | 1.40 | 0.000 | 0.80 | 1.01 | 0.003 | 0.35 |

Notes: **Bold** text denotes locations that exceed the statewide average.

Source: Caltrans TASAS data January 1, 2011 to December 31, 2013.



Along US 101, 147 mainline and 47 ramp collisions were recorded over a three-year period. During this period there were 54 collisions resulting in injury and no recorded fatalities. Seventy-six percent of the accidents occurred on the freeway mainline. Rear end, sideswipe, and hit object collisions accounted for up to 97 percent of the mainline accidents. These types of collisions are commonly due to driver inattention, travel at unsafe speeds and unsafe lane changing maneuvers. For collisions that occurred on freeway ramps, hit object and rear end were the primary collision types, with percentages totaling 81 percent.

Within the study limits, 135 mainline and 30 ramp collisions were recorded along SR 237 over a three-year period including one fatal and 58 injury collisions. Eighty-two percent of collisions occurred on the mainline. Rear end type collisions, which are often due to driver inattention, unsafe speeds, and lane changing in traffic congestion, accounted for up to 78 percent of the mainline collisions. For the ramp collisions, rear end, broadside, and hit object were the primary collision types totaling 77 percent of all ramp collisions.

Table 3-18 shows that actual collision rates on this section of US 101 are less than the statewide average for similar highway facilities. However, accident rates on the northbound US 101 loop on-ramp from NB Mathilda Avenue and loop off-ramp to SB Mathilda Avenue and the southbound US 101 on-ramp from NB Mathilda Avenue exceed the statewide average for similar highway facilities.



4. TRAVEL DEMAND FORECASTS

A summary of the forecasting process and results is presented in this chapter. A detailed description of the traffic forecasting process is presented in the Final Travel Demand Forecasting Memorandum for this project and can be found in **Appendix H**.

ANALYSIS SCENARIOS

The Santa Clara Valley Transportation Authority (VTA) model was used to develop forecasts for the Mathilda Avenue Improvements between SR 237 and US 101 project. Existing demand volumes and steps taken to validate the VTA model within the project study area can be found in the model validation memorandum found in **Appendix H**. This memorandum presents peak hour and peak period traffic forecasts for the following scenarios:

- Opening Year (2018) No Build
- Opening Year (2018) With Build
 - Alternative 1 (SR 237 Modified Diamond Interchange)
 - Alternative 2 (SR 237 Diverging Diamond Interchange)
- Design Year (2040) No Build
- Design Year (2040) With Build
 - Alternative 1 (SR 237 Modified Diamond Interchange)
 - Alternative 2 (SR 237 Diverging Diamond Interchange)

Appendix I includes conceptual geometric layouts of Alternative 1 and Alternative 2.

FORECAST ASSUMPTIONS

The model horizon years are 2018 and 2040. The future land use changes and regional transportation improvement projects for the two horizon years are summarized in this section.

GROWTH RATE ASSUMPTIONS

The land use assumptions include ABAG regional growth projections found in the VTA model under 2020 and 2040.³ The annual growth rate in the project study area was verified and compared to the growth rate found in the City of Sunnyvale model. **Table 4-1** presents the annual growth rates by AM and PM peak hours found in the VTA model and used to develop future year forecasts. It also presents the annual growth rates found in the City of Sunnyvale model which was used to confirm the project area growth.

³ The Year 2020 VTA model land use was used to estimate Year 2018 land use.



TABLE 4-1: VTA AND CITY OF SUNNYVALE MODEL GROWTH RATES

| Model | Peak Hour | Annual Linear Growth Rate ¹ | |
|-------------------|-----------|--|----------|
| | | Inbound | Outbound |
| VTA | AM | 1.3% | 0.8% |
| | PM | 1.4% | 1.6% |
| City of Sunnyvale | AM | -0.2% | 0.9% |
| | PM | 1.2% | 2.0% |

Notes:

1. Growth rates were determined within a one mile radius of the project site as seen in **Appendix J**.

Source: Fehr & Peers, 2016.

Given that both models produce approximately the same amount of growth, the VTA model was deemed consistent with planned local land use changes and suitable for deriving future year travel demand forecasts.

ROADWAY NETWORK ASSUMPTIONS

The 2018 and 2040 roadway networks contain improvements in Santa Clara County's *Valley Transportation Plan (VTP) 2040* and coordination with City of Sunnyvale, VTA, and Caltrans staff.

2018 No Build

There are many freeway improvements planned in the vicinity of the Mathilda Avenue interchanges as seen in **Table 4-2** below. Express Lanes on SR 237 and US 101 are assumed to be partially completed by 2018 and fully completed by 2040 as are all of the ramp metering on both freeways. Ramp metering was also assumed completed by 2018. In terms of local roadway improvements, the Innovation Way extension between Mathilda Avenue and Bordeaux Drive is assumed to be completed with the Moffett Park development (currently under construction) and the Central Expressway auxiliary lanes are also assumed to be completed by 2018.

2040 No Build

In addition to the identified improvements under 2018, the Mary Avenue extension from its current location over US 101 and SR 237 to E Street on the north side is assumed to be completed by 2040. Freeway improvements included under 2040 include express lanes on SR 85, Lawrence Expressway / US 101 interchange improvements, and an auxiliary lane on US 101 southbound between Ellis Street and SR 237.



TABLE 4-2: ROADWAY NETWORK ASSUMPTIONS

| Improvement | Included in Network Year | |
|---|--------------------------|------|
| | 2018 | 2040 |
| Freeway/Ramp Improvements | | |
| SR 237 Eastbound Auxiliary Lanes – Mathilda Avenue to Fair Oaks Avenue | Yes | Yes |
| SR 237 Express Lanes – North First Street to Mathilda Avenue | Yes | Yes |
| SR 237 Express Lanes – Mathilda Avenue to SR 85 | No | Yes |
| US 101 Express Lanes – Whipple Avenue in San Mateo County to Cochrane Road in Morgan Hill (one lane in each direction) | Yes | Yes* |
| US 101 Express Lanes – Whipple Avenue in San Mateo County to Cochrane Road in Morgan Hill (two lanes in each direction) | No | Yes |
| US 101 Southbound Auxiliary Lane – Ellis Street and SR 237 | No | Yes |
| All freeway ramps metered on US 101 and SR 237 (includes widening of SR 237 EB on-ramp at Mathilda Avenue to two lanes) | Yes | Yes |
| SR 85 Express Lanes – US 101 to US 101 | No | Yes |
| Lawrence Expressway Ramp Improvements at SR 237 | No | Yes |
| Local Street Improvements | | |
| Central Expressway Auxiliary Lanes – Mary Avenue and Lawrence Expressway | Yes | Yes |
| Innovation Way Extension – Mathilda Avenue to Bordeaux Drive | Yes | Yes |
| Mary Avenue Extension – extended as a 4-lane street to E Street on the north side of SR 237 | No | Yes |
| Public Transit Improvements | | |
| BART Extension – Fremont Station to Berryessa Station | Yes | Yes |
| Bus Rapid Transit (BRT) along El Camino Real and Stevens Creek Boulevard | Yes | Yes |
| BART Extension – Berryessa Station through downtown San Jose to Santa Clara | No | Yes |
| Increase in VTA Light-Rail service frequencies | No | Yes |
| Caltrain Electrification – Tamien Station to San Francisco Transbay Station | No | Yes |

Notes:

*Express Lanes on US 101 will be expanded to two lanes in each direction by Year 2040.

Source: Valley Transportation Plan (VTP) 2040, Caltrans, VTA and City of Sunnyvale staff, Moffett Place EIR, Fehr & Peers, 2016.

With Build Alternatives

The 2018 and 2040 Build Alternative roadway networks were modified to reflect improvements that are part of the project alternatives. The Moffett Park Drive link between Mathilda Avenue and Bordeaux Drive was removed and the location of the SR 237 WB Off-Ramp was relocated to the current east leg of the Mathilda Avenue and Moffett Park Drive intersection. In addition, the US 101 NB Loop Off-Ramp was removed and links and turn penalties were adjusted to account for a full-access interchange at Mathilda Avenue and US 101. The roadway network surrounding the interchange will remain the same as No Build conditions.



TRAFFIC DEMAND FORECASTS

The model horizon years are 2018 and 2040; the Project Opening Year is 2018 and the Design Year is 2040.

2018 AND 2040 NO BUILD FORECASTS

Freeway mainline forecasts were developed using the difference method, which is a link-level adjustment procedure that adds the amount of growth projected by the model to the existing demand volumes. Future year intersection peak period hourly volumes were developed by using the existing relationships between the peak hour and peak period hourly volumes. The following presents the specific steps used to develop 2040 No Build intersection raw forecasts from the model:

- **Step 1** – Run the validated base year (2013) model to estimate existing AM and PM peak hour model traffic volumes.
- **Step 2** – Run the 2040 model to estimate AM and PM peak hour traffic forecasts.
- **Step 3** – Develop 2040 No Build raw forecasts using the maximum value of the following three formulas:
 1. 2040 Raw Forecasts = 2013 Peak Hour Demand Volume + (2040 Model Peak Hour Volume – Base Year Model Peak Hour Volume)
 2. 2040 Raw Forecasts = 2013 Peak Hour Demand Volume + 20
 3. Year 2040 Raw Forecasts = 2013 Peak Hour Demand Volume + (2013 Peak Hour Demand Volume * Annual Linear Growth Rate * Number of Years between 2040 and 2013)⁴
- **Step 4** – Check for reasonableness and make manual adjustments as necessary to ensure that volumes do not drop below existing levels or grow exponentially unless there is a specific reason. Also verify a balanced volume network.

Forecasts for 2018 were developed by applying linear interpolation between the 2013 existing demand volumes and 2040 demand volumes presented in this memorandum. Manual adjustments were made to account for the Mary Avenue extension which is not assumed to be completed by 2018.

2018 AND 2040 WITH BUILD FORECASTS

The project is a reconfiguration of an existing interchange and is not proposing to add capacity to US 101, SR 237, or to the surrounding roadway network system. Therefore, the project would not change overall travel demands compared to the No Build scenario, but is expected to change origin-destination patterns regarding the full-access interchange at Mathilda Avenue / US 101 and would result in a redistribution of traffic that reflects the proposed interchange modifications. As a result, the demand volumes into and out

⁴ Sub-Area is defined as a one-mile radius around the project study area between Almanor Avenue and 5th Avenue on Mathilda Avenue.



of the study area would be the same as the No Build conditions. Furthermore, the demand volumes at study intersections outside the interchange area (e.g. north on Mathilda Avenue) would also be the same as No Build Conditions.

The 2040 model was run with Build Alternative 1 geometry to estimate the traffic redistribution among the three interchanges (Mathilda Avenue/US 101, Mathilda Avenue/SR 237, and US 101/SR 237) due to the alternative ramp configurations. In addition, the 2040 model was run with Build Alternative 2 geometry in order to determine the traffic redistribution between the Mary Avenue extension and Mathilda Avenue with the closure of eastbound traffic at the Moffett Park Drive and Mathilda Avenue intersection. The information obtained for the Build Alternative 2 was only used for 2040 forecasts as the Mary Avenue extension is not assumed complete by 2018.

Manual adjustments were made to ensure reasonableness.

FINAL NO BUILD AND WITH BUILD 2018 AND 2040 DEMAND FORECASTS

Intersection Forecasts

A brief comparison between the City of Sunnyvale travel demand model and the VTA travel demand model shows that the City model experiences a larger shift in traffic from Mathilda Avenue to Mary Avenue with the Mary Avenue extension. In order to account for some of the expected effect the Mary Avenue extension will have on the Mathilda Avenue corridor, approximately 200 peak direction vehicles, as well as a small proportion of off-peak direction vehicles, were shifted from Mathilda Avenue to Mary Avenue under the 2040 forecasts.

Figure 7 and **Figure 8** present the 2018 and 2040 No Build intersection forecasts, respectively. **Figure 9** and **Figure 10** present the 2018 and 2040 Build Alternative 1 intersection forecasts, while **Figure 11** and **Figure 12** present the 2018 and 2040 Build Alternative 2 intersection forecasts.

US 101 and SR 237 Mainline and Ramp Forecasts

The AM and PM peak period freeway (mainline and ramp) 2018 and 2040 demand volumes are presented in **Appendix K**. Note that since the two Build Alternatives contain the same ramp reconfiguration of existing interchanges, there is no difference in freeway forecasts between Build Alternative 1 and Alternative 2. As a result only a single set of 2018 and 2040 Build demand volumes are presented.

The percentage of vehicles on the assumed on the high-occupancy toll (HOT) lanes are found in **Table 4-3**. These percentages were determined by taking the maximum of the percentage found in the VTA travel demand forecasting model and the HOV percentage assumed under existing conditions.



TABLE 4-3: FREEWAY MAINLINE HOT PERCENTAGE

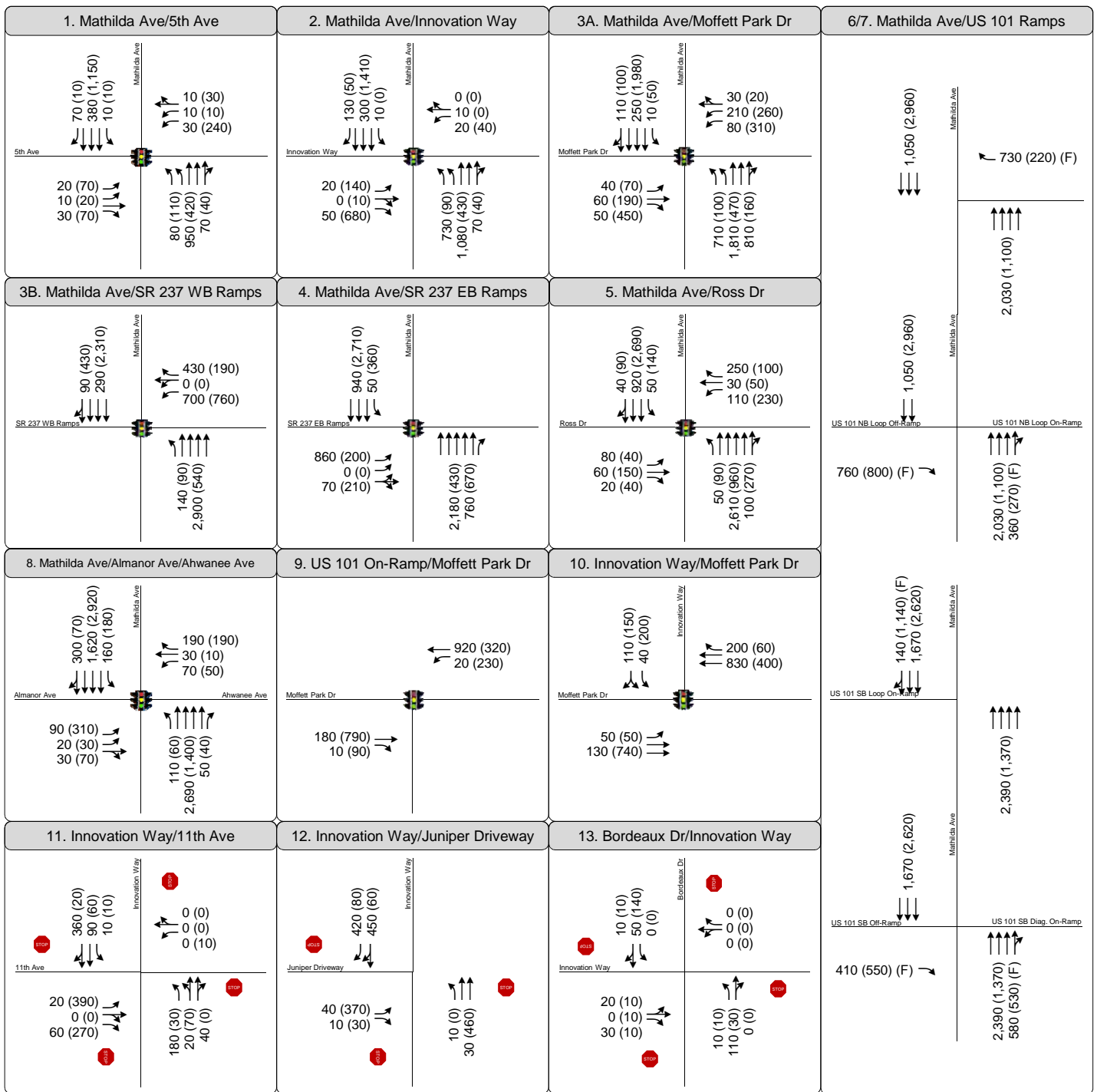
| Freeway Mainline | Peak Hour | HOT %¹ |
|-------------------------|------------------|--------------------------|
| US 101 Northbound | AM | 19% |
| | PM | 13% |
| US 101 Southbound | AM | 17% |
| | PM | 20% |
| SR 237 Westbound | AM | 26% |
| | PM | 16% |
| SR 237 Eastbound | AM | 25% |
| | PM | 26% |

Notes:

1. HOT volume is a percent of the total volumes presented in this memorandum.

Source: Fehr & Peers, 2016.

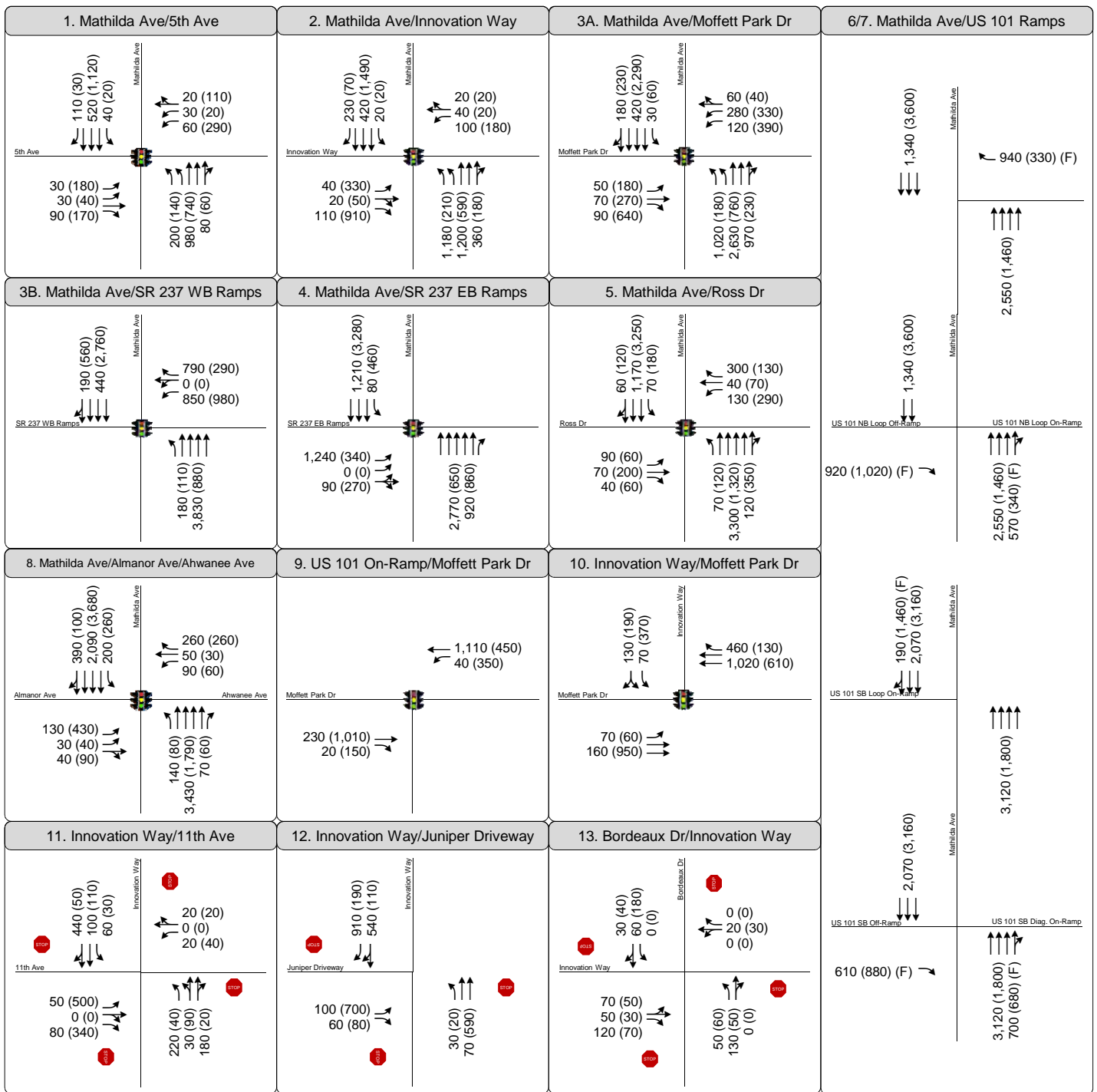




(##) - AM(PM) Peak Hour Demand Volumes
(F) - Unsignalized (free) Movement

Figure 7
Peak Hour Traffic Volumes
and Lane Configurations -
Mathilda Avenue - No Build 2018 Demand Volumes

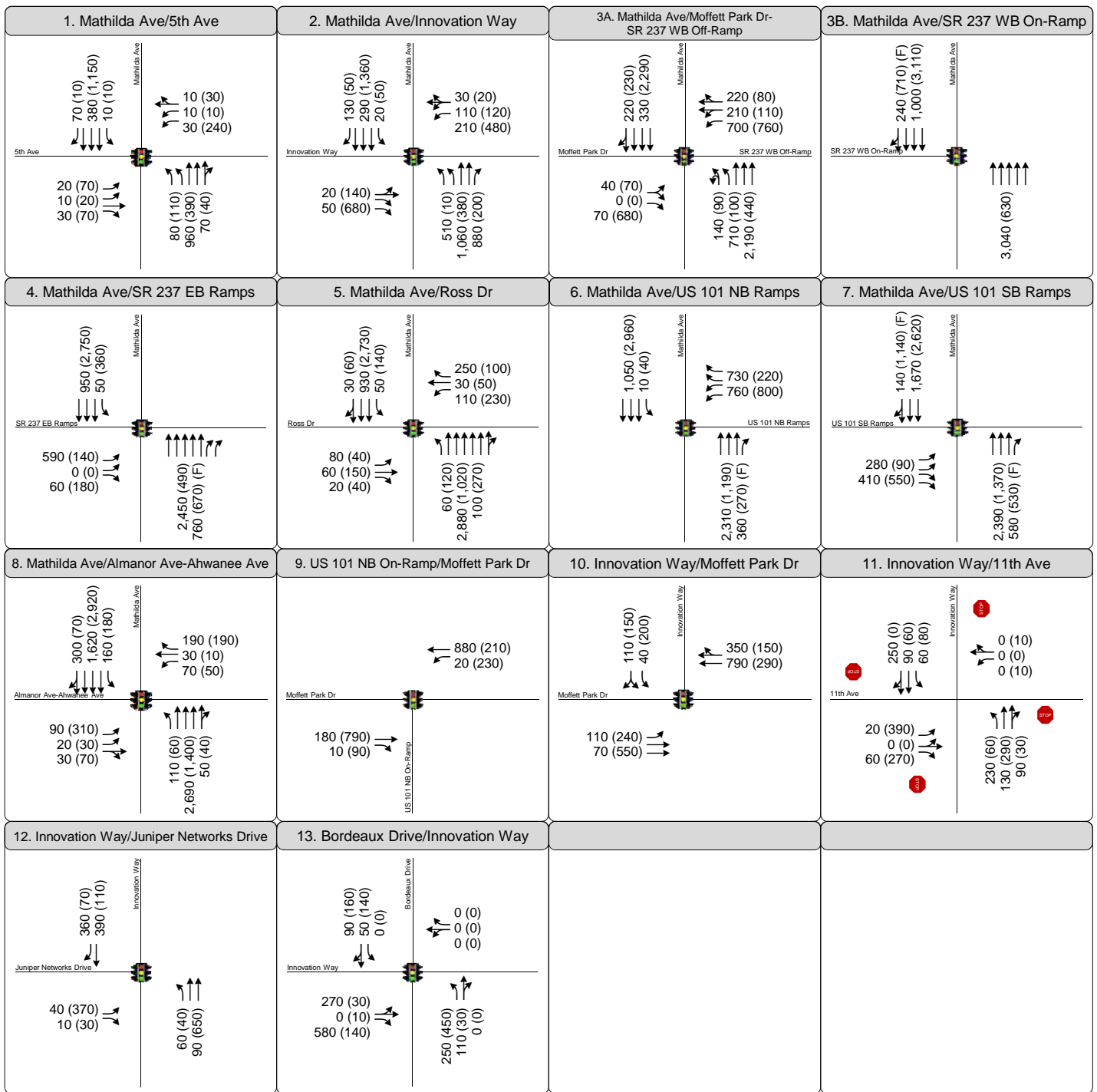




(##) - AM(PM) Peak Hour Demand Volumes
(F) - Unsignalized (free) Movement

Figure 8
Peak Hour Traffic Volumes
and Lane Configurations -
Mathilda Avenue - No Build 2040 Demand Volumes

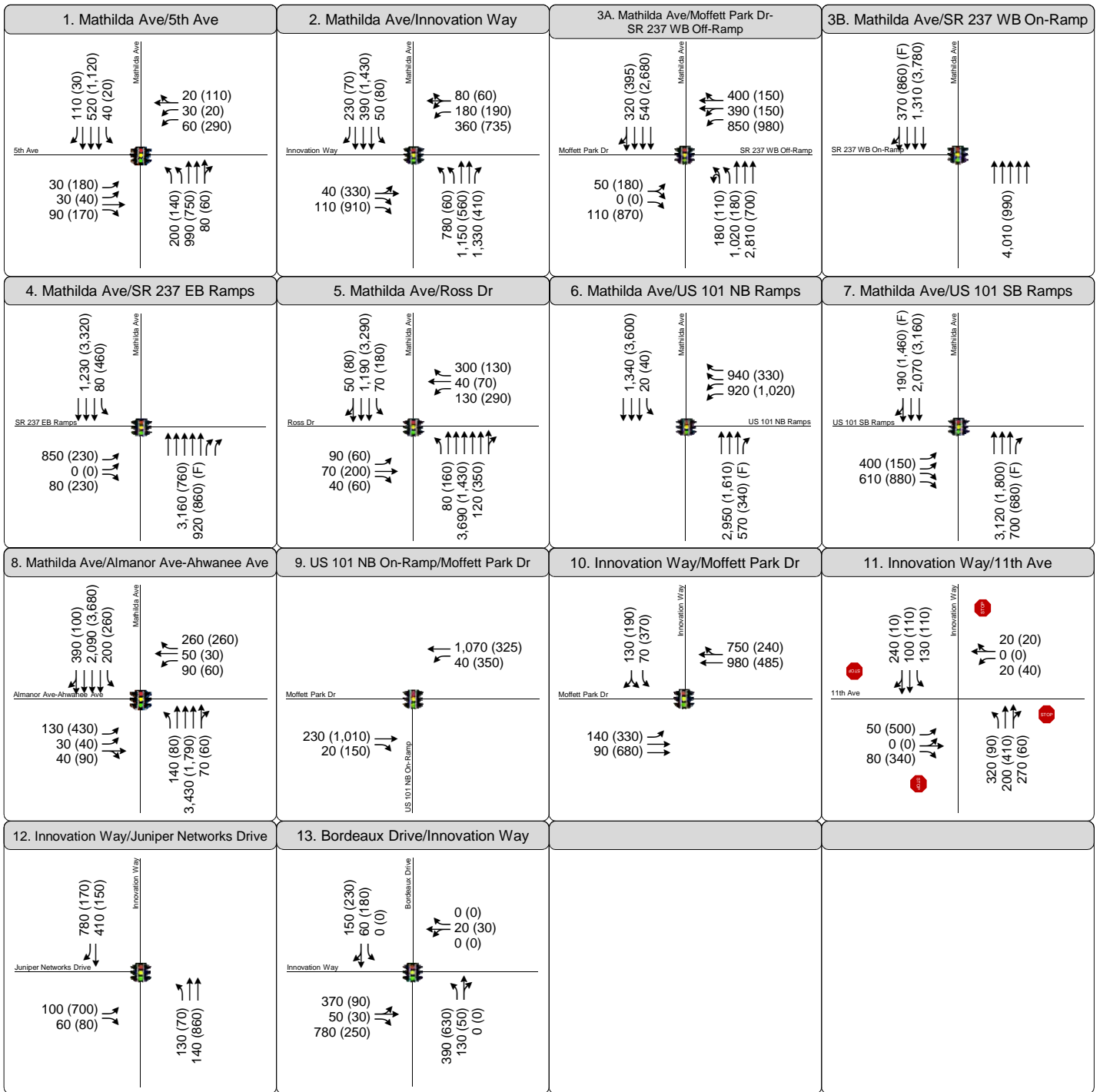




(##) - AM(PM) Peak Hour Demand Volumes
(F) - Unsignalized (free) Movement

Figure 9
Peak Hour Traffic Volumes
and Lane Configurations -
Mathilda Avenue - Build Alternative 1 2018 Demand Volumes

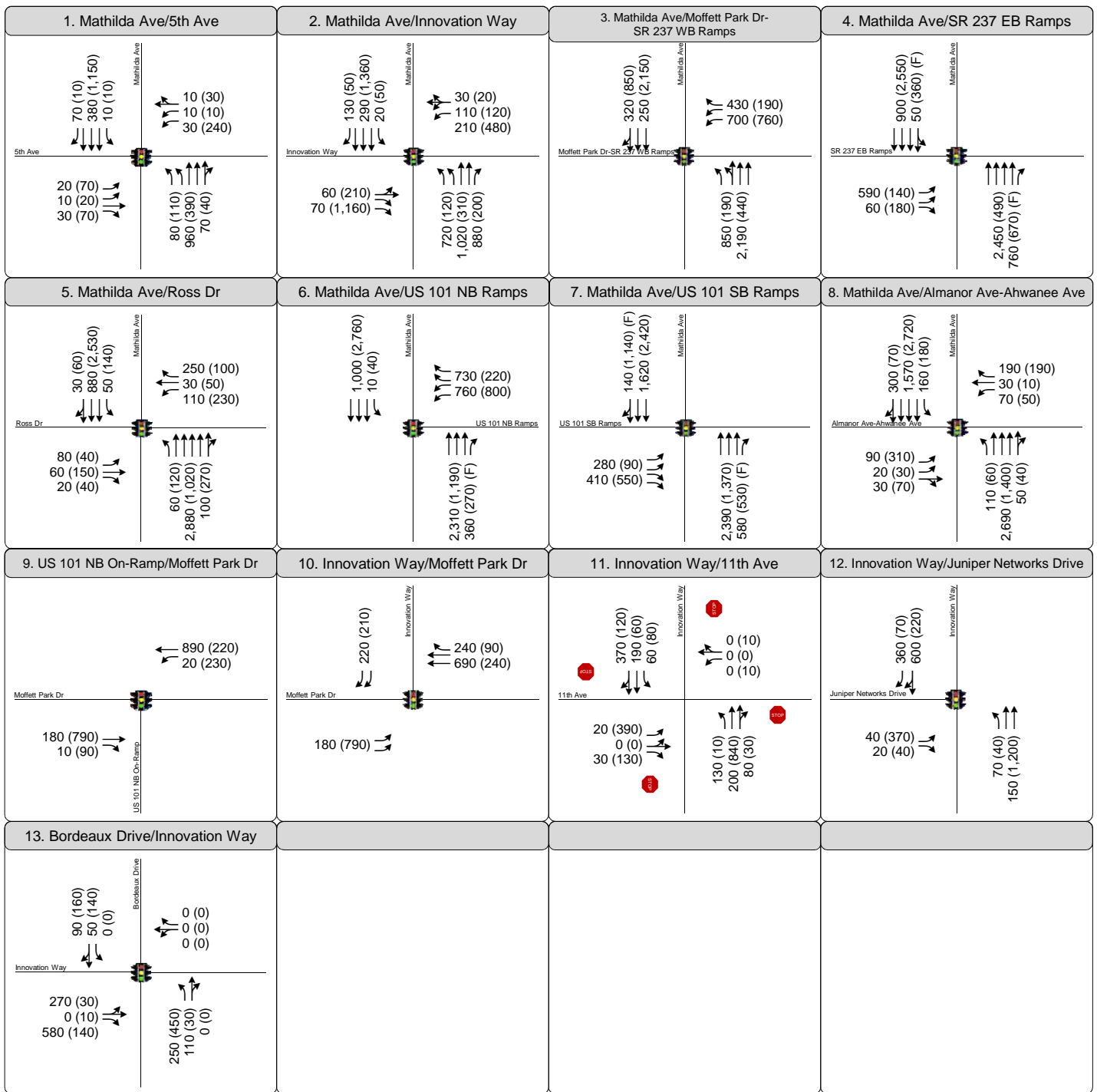




(##) - AM(PM) Peak Hour Demand Volumes
(F) - Unsignalized (free) Movement

Figure 10
Peak Hour Traffic Volumes
and Lane Configurations -
Mathilda Avenue - Build Alternative 1 2040 Demand Volumes

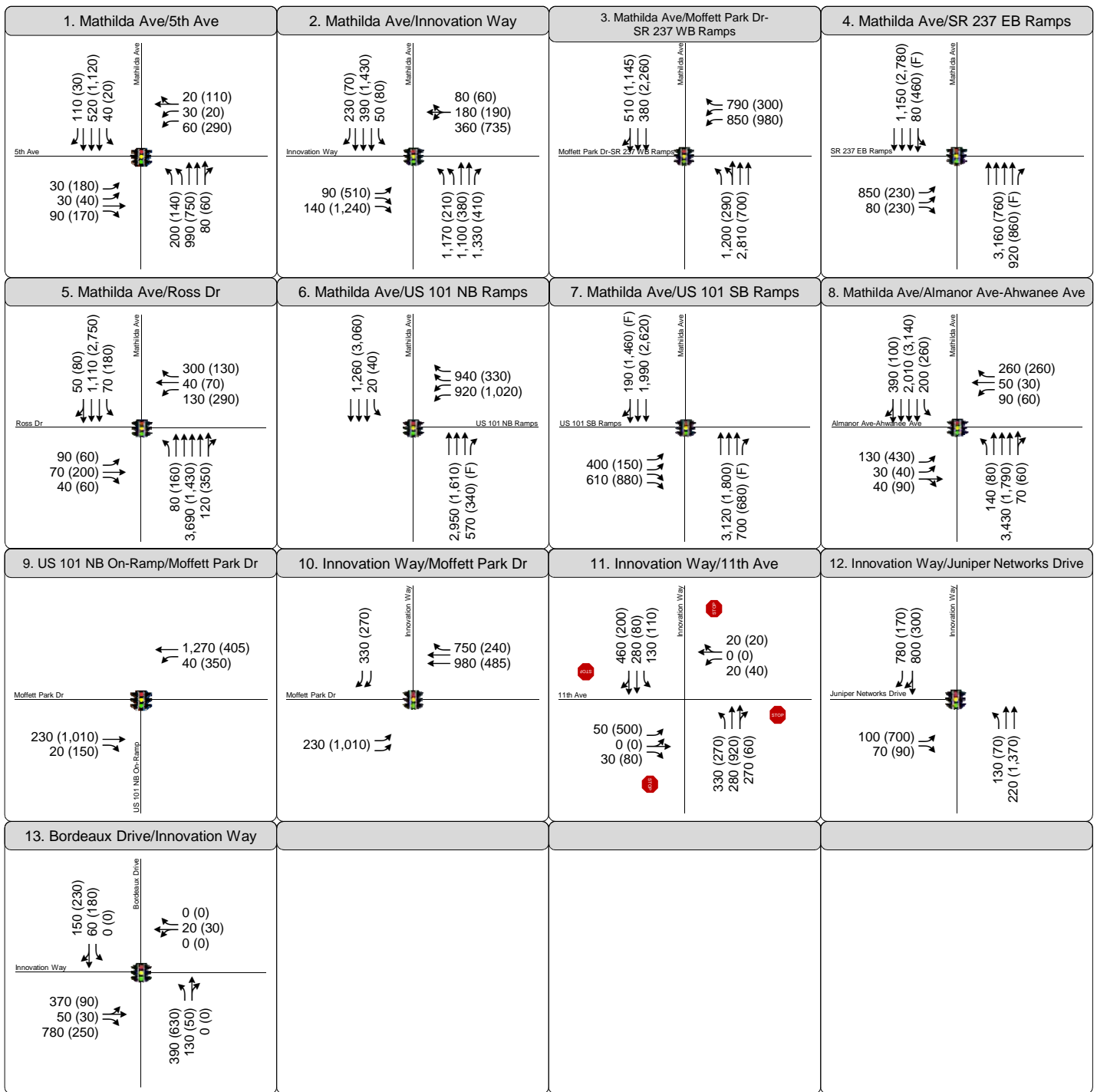




(##) - AM(PM) Peak Hour Demand Volumes
(F) - Unsignalized (free) Movement

Figure 11
Peak Hour Traffic Volumes
and Lane Configurations -
Mathilda Avenue - Build Alternative 2 2018 Demand Volumes





(##) - AM(PM) Peak Hour Demand Volumes
(F) - Unsignalized (free) Movement

Figure 12
Peak Hour Traffic Volumes
and Lane Configurations -
Mathilda Avenue - Build Alternative 2 2040 Demand Volumes



5. YEAR 2018 TRAFFIC OPERATIONS ANALYSIS

This chapter presents the results of the traffic operations analysis for year 2018, which is anticipated to be the opening year of the project. The analysis focuses on intersection and freeway operations for No Build and Build conditions. The process used to refine the traffic forecasts for the operations analysis is described, followed by the analysis results.

YEAR 2018 ROADWAY NETWORK ASSUMPTIONS

In order to conduct a traffic analysis that is consistent with CEQA guidelines and appropriate for preparation of an Environmental Document, it is necessary to develop reasonable assumptions about future infrastructure improvements. In the case of roadway infrastructure, an adequate environmental analysis requires that the analyst consider all major roadway improvements that are funded, as well as other reasonably foreseeable improvements that may have a direct effect on the project being studied. The roadway network assumptions for No Build and Build conditions are presented below.

Table 5-1 presents the intersection configuration under No Build, Alternative 1 and 2 at the major intersections being modified by the project. This information is useful in identifying locations where the project is substantially changing the intersection configuration and/or increasing capacity.

NO BUILD ASSUMPTIONS

Under this alternative, the existing facility would remain unchanged except for planned and programmed improvements including planned improvements at Mathilda Avenue and Innovation Way. This alternative does not meet the project Purpose and Need. Rather, it provides a basis for the analysis and evaluation of the Build Alternatives.

BUILD 1 ALTERNATIVE ASSUMPTIONS

The following section describes the Build Alternative 1 roadway and ramp configuration. The existing northbound US 101 loop off-ramp would be closed and traffic shifted to the northbound US 101 diagonal off-ramp. Northbound US 101 diagonal off-ramp and loop on-ramp would be realigned and widened to terminate at a new signalized intersection on Mathilda Avenue. Left-turn access from southbound Mathilda Avenue to northbound US 101 loop on-ramp would be provided. This new ramp configuration would provide full access to northbound US 101 by adding access to northbound US 101 from southbound on Mathilda Avenue.

The Southbound US 101 off-ramp and loop on-ramp would be realigned and widened to terminate at a new signalized intersection on Mathilda Avenue. Left-turn access from southbound US 101 off-ramp to northbound Mathilda Avenue would be provided. This new ramp configuration would provide full access to southbound US 101 by adding access to northbound on Mathilda Avenue from southbound US 101. The existing westbound SR 237 ramps would be realigned to accommodate local street improvements. The



westbound SR 237 off-ramp would be realigned with Moffett Park Drive on the west leg of the intersection and the signal at existing SR 237 westbound ramps would be removed. Moffett Park Drive access on the east side of Mathilda Avenue would be closed and traffic shifted to Bordeaux Drive and Innovation Way. Moffett Park Drive access west of Mathilda Avenue would remain open. Access to the westbound SR 237 on-ramp from northbound Mathilda Avenue would be accomplished with a U-turn movement at the new signalized intersection.

Three continuous through lanes would generally be provided in both directions on Mathilda Avenue through the interchanges. Pavement rehabilitation on Mathilda Avenue within the study limits would be considered.

Bicycle and Pedestrian Facilities

Enhanced bicycle and pedestrian facilities, and additional signage to improve wayfinding for freeway and local street access would be considered. A new Class II bicycle lane is proposed on both sides of Mathilda Avenue between Almanor Avenue and Innovation Way. The bicycle lanes would connect with the existing signed on-street bicycle route north of Innovation Way.

A new dedicated bicycle and pedestrian pathway, or a Class I bicycle facility, is proposed in both directions on Moffett Park Drive between Bordeaux Drive and Innovation Way. This bike facility would improve regional bicycle access through the study area and provide a dedicated connection across Mathilda Avenue connecting the east and west areas of the Moffett Business Park. The new Class I facility would also link with the north-south bikeway along Borregas Avenue to facilitate more convenient bicycle access from other parts of Sunnyvale.

Continuous sidewalks would be provided along both sides of Mathilda Avenue except on the west side of Mathilda between Ross Drive and Moffett Park Drive due to geometric constraints at the SR 237 Undercrossing structure. Crosswalks would be maintained at Ross Drive and Moffett Park Drive to allow pedestrians to cross Mathilda Avenue.

Collisions

Eliminating the northbound US 101 loop off-ramp and nonstandard weaving length with the northbound US 101 loop on-ramp, and signaling the southbound US 101 on-ramp termini are design features that could help reduce congestion related collisions. Actual collision rates on this section of SR 237 are greater than the statewide average for similar highway facilities. The westbound SR 237 off-ramp also exceeds the statewide average for similar highway facilities. Reconfiguring the Moffett Park Drive intersection and providing additional storage for queuing vehicles on the ramp may also contribute to a reduction in congestion related collisions.

BUILD 2 ALTERNATIVE ASSUMPTIONS

The following section describes the Build Alternative 2 roadway and ramp configuration. The existing SR 237 ramps would be realigned and widened to accommodate a diverging diamond interchange



configuration. Existing signal intersections on Mathilda Avenue at the SR 237 ramps and Moffett Park Drive would be removed. New signalized intersections would be constructed at realigned SR 237 ramp termini. Traffic on Mathilda Avenue would be shifted to the opposite side of the road between SR 237 ramp termini to facilitate left-turn movements. Moffett Park Drive access on the east side of Mathilda Avenue would be closed and traffic shifted to Bordeaux Drive and Innovation Way. West Moffett Park Drive would remain open for westbound traffic.

Improvements for the US 101 ramps would be similar to the other Build Alternative. Three to four continuous through lanes would be provided in both directions on Mathilda Avenue through the interchanges. Pavement rehabilitation on Mathilda Avenue within the study limits would be considered. Local street improvements would generally be similar to Alternative 1.

Bicycle and Pedestrian Facilities

Enhanced bicycle and pedestrian facilities, and additional signage to improve wayfinding for freeway and local street access would be considered. Bicycle and pedestrian facility improvements would be similar to Alternative 1, with a new Class I bicycle facility along Moffett Park Drive improving regional bicycle access providing a dedicated connection across Mathilda Avenue connecting the east and west areas of the Moffett Business Park. The Class I bicycle facility cross the diverging diamond interchange with a single-stage crossing for bicyclists and pedestrians.

Pedestrian access through the diverging diamond interchange would follow a route that would include travel in the median of Mathilda Avenue through the SR 237 interchange area. The specific route and dimensions of the sidewalk between Ross Drive and Moffett Park Drive will be considered and confirmed by detailed traffic analysis and geometric design studies conducted during the PA&ED phase.

Collisions

Similar to Build Alternative 1, eliminating the northbound US 101 loop off-ramp and nonstandard weaving section with the northbound US 101 loop on-ramp, and signalizing the southbound US 101 on-ramp termini could help reduce congestion related collisions. Actual collision rates on this section of SR 237 and the westbound SR 237 off-ramp are greater than the statewide average for similar highway facilities. The westbound SR 237 off-ramp also exceeds the statewide average for similar highway facilities. Reconfiguring the Moffett Park Drive intersection and providing additional storage for queuing vehicles could also help reduce congestion related collisions.



TABLE 5-1: INTERSECTION CONFIGURATION UNDER NO BUILD, ALTERNATIVE 1, AND ALTERNATIVE 2

| Intersection | Approach | No Build | Build 1 Alternative | Build 2 Alternative |
|---|-------------------------|--|--|--|
| 1: Mathilda Avenue/Fifth Avenue | NB | 2 left-turn lanes (425'), 2 through lanes, 1 shared through/right lane | Same as No Build | Same as No Build |
| | SB | 1 left-turn lane (250'), 3 through lanes, 1 right-turn lane (250') | Same as No Build | Same as No Build |
| | EB | 2 left-turn lanes (625'), 1 through lane, 1 right-turn lane (625') | Same as No Build | Same as No Build |
| | WB | 2 left-turn lanes (925'), 1 shared through/right lane | Same as No Build | Same as No Build |
| 2: Mathilda Avenue/Innovation Way | NB | 2 left-turn lanes (400'), 3 through lanes, 1 shared through/right lane | 2 left-turn lanes (700'), 2 through lanes, 1 right-turn lane (975') with overlap phase | 2 left-turn lanes (700'), 2 through lanes, 1 right-turn lane (975') with overlap phase |
| | SB | 1 left-turn lane (75'), 3 through lanes, 1 right-turn lane (225') | Same as No Build | Same as No Build |
| | EB | 1 left-turn lane (200'), 1 shared through/right lane, 1 right-turn lane | 1 shared left-turn/through lane, 2 right-turn lanes with overlap phase | 1 shared left-turn/through lane, 2 right-turn lanes with overlap phase |
| | WB | 1 left-turn lane (425'), 1 shared through/right lane | 1 left-turn lane (425'), 1 shared left/through/right lane | 1 left-turn lane (425'), 1 shared left/through/right lane |
| 3: Mathilda Avenue/Moffett Park Drive/SR 237 WB Ramps | NB | 2 left-turn lanes (125'), 2 through lanes, 1 shared through/right lane | 2 left-turn lanes (350'), 3 through lanes | 1 left-turn lane, 1 shared left-turn/through lane, 2 through lanes |
| | SB | 1 left-turn lane (175'), 3 through lanes, 1 shared through/right lane | 2 through lanes, 1 shared through/right lane | 2 through lanes, 1 shared through/right lane |
| | EB (Moffett Park) | 1 left-turn lane (350'), 1 through lane, 1 right-turn lane (1,100') with a second right-turn lane to a slip ramp | 1 shared left/right lane, 1 right-turn lane | EB Moffett Park Drive is eliminated |
| | WB (Moffett Park) | 2 left-turn lanes (300'), 1 shared through/right lane | WB Moffett Park Drive is eliminated | WB Moffett Park Drive is eliminated |
| | WB (SR 237 WB Off-Ramp) | 1 left-turn lane (1,125'), 1 through lane, 1 right-turn lane (325') | 1 left-turn lane (525'), 1 shared left/through lane, 1 shared through/right lane | 2 left-turn lanes (1,075'), 1 right-turn lane (550') |



TABLE 5-1: INTERSECTION CONFIGURATION UNDER NO BUILD, ALTERNATIVE 1, AND ALTERNATIVE 2

| Intersection | Approach | No Build | Build 1 Alternative | Build 2 Alternative |
|-------------------------------------|----------|---|---|---|
| 4: Mathilda Avenue/SR 237 EB Ramps | NB | 5 through lanes, 1 right-turn lane | 5 through lanes, 2 right-turn slip ramp lanes | 4 through lanes, 1 right-turn slip ramp lane |
| | SB | 1 left-turn lane (200'), 3 through lanes | 1 left-turn lane (325'), 3 through lanes | 1 shared left-turn/through lane, 3 through lanes |
| | EB | 2 left-turn lanes, 1 shared left/through/right lane (450') | 2 left-turn lanes, 1 right-turn lane (450') | 2 left-turn lanes, 1 right-turn lane (450') |
| 5: Mathilda Avenue/Ross Drive | NB | 1 left-turn lane (150'), 4 through lanes, 1 shared through/right lane | 1 left-turn lane (250'), 5 through lanes, 1 shared through/right lane | 1 left-turn lane (250'), 4 through lanes, 1 shared through/right lane |
| | SB | 1 left-turn lane (150'), 2 through lanes, 1 shared through/right lane | 1 left-turn lane (150'), 3 through lanes | 1 left-turn lane (225'), 3 through lanes |
| | EB | 1 left-turn lane, 1 through lane, 1 right-turn lane (50') | Same as No Build | Same as No Build |
| | WB | 1 left-turn lane (75'), 1 through lane, 1 right-turn lane (75') | Same as No Build | Same as No Build |
| 6: Mathilda Avenue/US 101 NB Ramps* | NB | Does not exist | 3 through lanes, 1 right-turn lane (710') | 3 through lanes, 1 right-turn lane (710') |
| | SB | Does not exist | 1 left-turn lane (350'), 3 through lanes | 1 left-turn lane (350'), 3 through lanes |
| | WB | Does not exist | 2 left-turn lanes, 2 right-turn lanes (400' & 100') | 2 left-turn lanes, 2 right-turn lanes (400' & 100') |
| 7: Mathilda Avenue/US 101 SB Ramps* | NB | Does not exist | 3 through lanes, 1 right-turn slip ramp lane | 3 through lanes, 1 right-turn slip ramp lane |
| | SB | Does not exist | 2 through lanes, 1 shared through/right lane | 2 through lanes, 1 shared through/right lane |
| | EB | Does not exist | 2 left-turn lanes (905'), 2 right-turn lanes (905') | 2 left-turn lanes (905'), 2 right-turn lanes (905') |



TABLE 5-1: INTERSECTION CONFIGURATION UNDER NO BUILD, ALTERNATIVE 1, AND ALTERNATIVE 2

| Intersection | Approach | No Build | Build 1 Alternative | Build 2 Alternative |
|--|----------|--|---|---|
| 8: Mathilda Avenue/Ahwanee Avenue-Almanor Avenue | NB | 1 left-turn lane (375'), 4 through lanes, 1 right-turn lane (75') | 1 left-turn lane (375'), 3 through lanes, 1 shared through/right lane (75') | 1 left-turn lane (375'), 3 through lanes, 1 shared through/right lane (75') |
| | SB | 1 left-turn lane (125'), 3 through lanes, 1 shared through/right lane | 1 left-turn lane (250'), 3 through lanes, 1 shared through/right lane | 1 left-turn lane (250'), 3 through lanes, 1 shared through/right lane |
| | EB | 2 left-turn lanes, 1 shared through/right lane (125') | Same as No Build | Same as No Build |
| | WB | 1 left-turn lane (250'), 1 through lane, 1 right-turn lane (75') | Same as No Build | Same as No Build |
| 9: US 101 NB On-Ramp/Moffett Park Drive | EB | 1 through lane, 1 right-turn lane (150') | Same as No Build | Same as No Build |
| | WB | 1 left-turn lane (850'), 1 through lane | Same as No Build | Same as No Build |
| 10: Innovation Way/Moffett Park Drive | SB | 1 left-turn lane (575'), 1 shared left/right lane | Same as No Build | 2 right-turn lanes |
| | EB | 1 left-turn lane (225'), 2 through lanes | Same as No Build | 2 left-turn lanes |
| | WB | 2 through lanes, 1 right-turn lane (225') | 1 through lane, 1 shared through/right lane | 2 through lane, 1 right-turn lane (200') |
| 11: Innovation Way/Eleventh Avenue | NB | 1 left-turn lane (125'), 1 shared left/through lane, 1 shared through/right lane | 1 left-turn lane (125'), 1 through lane, 1 shared through/right lane | 1 left-turn lane (125'), 1 through lane, 1 shared through/right lane |
| | SB | 1 left-turn lane (125'), 1 through lane, 1 shared through/right lane | Same as No Build | Same as No Build |
| | EB | 1 left-turn lane (100'), 1 shared through/right lane, 1 right-turn lane | 1 left-turn lane (100'), 1 shared left-turn/through lane, 1 right-turn lane | 1 left-turn lane (100'), 1 shared left-turn/through lane, 1 right-turn lane |
| | WB | 1 left-turn lane, 1 shared through/right-turn lane | Same as No Build | Same as No Build |



TABLE 5-1: INTERSECTION CONFIGURATION UNDER NO BUILD, ALTERNATIVE 1, AND ALTERNATIVE 2

| Intersection | Approach | No Build | Build 1 Alternative | Build 2 Alternative |
|---|----------|--|-----------------------------------|--|
| 12: Innovation Way/Juniper Networks Driveway* | NB | 1 left-turn lane (300'), 2 through lanes | Same as No Build | Same as No Build |
| | SB | 1 shared through/right lane, 1 right-turn lane | 1 through lane, 1 right-turn lane | 1 through lane, 1 shared through/right-turn lane |
| | EB | 1 left-turn lane (300'), 1 right-turn lane (300') | Same as No Build | Same as No Build |
| 13: Bordeaux Drive/Innovation Way* | NB | 1 left-turn lane (50'), 1 shared through/right lane | Same as No Build | Same as No Build |
| | SB | 1 left-turn lane, 1 shared through/right lane | Same as No Build | Same as No Build |
| | EB | 1 shared left/through lane, 1 right-turn lane (100') | Same as No Build | Same as No Build |
| | WB | 1 shared left/through lane, 1 right-turn lane (100') | Same as No Build | Same as No Build |

Notes:

*Indicates intersection is signalized under Build 1 and Build 2 Alternatives.

Source: Fehr & Peers and WMH, 2016.



CONSTRAINED VOLUME ANALYSIS APPROACH

The traffic forecasts presented in Chapter 4 are hourly demand volumes. Peak period congestion along US 101 and SR 237 is expected to worsen in the future, thus constraining the demand within the study area system. For local street operations the off-ramp demand volumes can result in an overestimate of the actual volume that would arrive at the US 101 and SR 237 interchanges when congestion is taken into consideration. Similarly, the on-ramp demand volumes can result in an overestimate of the actual volume that can access US 101 and SR 237. The traffic volumes used in the analysis are adjusted to account for congestion and are referred to as "constrained volumes". One of the limitations of using separate software analysis programs to perform the peak hour intersection analysis (Synchro/SimTraffic) and the peak period mainline analysis (FREQ) is that neither provides a seamless linkage with respect to constrained volumes. SimTraffic applies a stochastic modeling approach, while FREQ applies a deterministic modeling approach. To address these issues the following steps were undertaken:

- **Step 1** – Run initial set of FREQ models to determine constrained off-ramp volumes at the SR 237/US 101 interchange as well as at the Mathilda Avenue interchanges. The constrained Mathilda Avenue peak hour off-ramp volume was calculated by applying an adjustment factor to the peak hour demand forecast. The off-ramp adjustment factor = (upstream mainline segment constrained volume) ÷ (upstream mainline segment demand volume).
- **Step 2** – Run final set of SimTraffic models assuming the constrained off-ramp volume at the US 101 and SR 237 off-ramps calculated from Step 1. Once SimTraffic models are finalized, determine constrained volume at the on-ramps for the peak hour.
- **Step 3** – Run final set of FREQ models assuming constrained peak hour on-ramp volumes from Step 2.

This three-step approach was applied to the Year 2018 traffic operations analysis and Year 2040 traffic operations analysis summarized in Chapter 6.

YEAR 2018 INTERSECTION OPERATIONS

Year 2018 intersection traffic operations were evaluated using the calibrated/validated SimTraffic models developed for Existing Conditions. The simulation models were executed for the peak hour with a 30-minute seeding period. The following constrained volume factors were applied to the off-ramp demand volumes to account for congestion along US 101 and SR 237 (consistent with the three-step modeling approach described above):

- Westbound SR 237 off-ramp to Mathilda Avenue = 0.95 during the AM peak hour and 1.00 during the PM peak hour;
- Eastbound SR 237 off-ramp to Mathilda Avenue = 1.00 during the AM peak hour and 0.87 during the PM peak hour;
- Northbound US 101 off-ramp to Mathilda Avenue = 0.95 during the AM peak hour and 1.00 during the PM peak hour;



- Southbound US 101 off-ramp to Mathilda Avenue = 1.00 during the AM peak hour and 0.91 during the PM peak hour.

INTERSECTION DELAY, LOS, AND PERCENT DEMAND SERVED

Table 5-2 presents the Year 2018 simulated intersection level of service results and percent demand served for each of the study intersections under No Build and Build Alternatives (intersection queuing is described in the following section). Results in **bold** indicate locations operating at LOS F conditions. Analysis results worksheets are presented in **Appendix L**.⁵

No Build Conditions

As shown in **Table 5-2** the majority of study intersections are anticipated to operate at LOS F during the AM and/or PM peak hour under No Build conditions in the Year 2018. The percent demand served is on average 84 percent during the AM and PM peak hour. The low percent demand served is indicative of the projected traffic demand exceeding the capacity of the roadway system. The total vehicle hours of delay are estimated to be 1,319 in the AM peak hour and 1,504 in the PM peak hour.

Build 1 Alternative

Below is a brief summary of the operations at the study locations under Build 1 Alternative in the Year 2018 and how they compare to No Build conditions.

- *Mathilda Avenue/Fifth Avenue* – Intersection level of service is anticipated to remain unchanged (LOS B during the AM peak hour and LOS F during the PM peak hour). The overall intersection delay would also remain relatively unchanged (less than a 5 percent change) for the AM and PM peak hour. The percent demand served is anticipated to increase from 88 percent to 98 percent in the AM peak hour and decrease from about 86 percent to 80 percent in the PM peak hour. The decrease in PM percent demand served is due to queues from the downstream Mathilda Avenue/Innovation Way intersection that occasionally reach back to this intersection during the PM peak hour.
- *Mathilda Avenue/Innovation Way* – Intersection level of service is anticipated to remain unchanged (LOS D during the AM peak hour and LOS F during the PM peak hour). The overall intersection delay would also remain relatively unchanged (less than a 5 percent change) for the AM and PM peak hour. The percent demand served is anticipated to increase from 84 percent to 99 percent in the AM peak hour and decrease from about 80 percent to 77 percent in the PM peak hour. The slight decrease in PM percent demand served is due to additional traffic that will travel through this intersection due to the closure of Moffett Park Drive between Mathilda Avenue and Bordeaux Drive.
- *Mathilda Avenue/Moffett Park Drive/SR 237 Westbound Ramps* – Intersection level of service is anticipated to improve from LOS F to LOS D in the AM peak hour and remain unchanged at LOS F during the PM peak hour. Although the intersection would continue to operate at LOS F during

⁵ Please note that Synchro and SimTraffic worksheets are provided for the study intersections in **Appendix L** for informational purposes to present key modeling inputs including lanes, volumes, and signal timings. The results presented in **Table 5-2** are from SimTraffic analysis output.



the PM peak hour under Build 1 Alternative the overall intersection delay would be reduced by over 30 percent compared to No Build conditions. The improvement in the peak hours is a result of eliminating the westbound Moffett Park Drive approach which reduces the number of signal phases at this location. The percent demand served is anticipated to increase from 81 percent to 98 percent in the AM peak hour and decrease slightly from about 83 percent to 82 percent in the PM peak hour.

- *Mathilda Avenue/ SR 237 Eastbound Ramps* – Intersection level of service is anticipated to improve from LOS F to LOS C in the AM peak hour and worsen from LOS B to LOS C during the PM peak hour. The PM peak hour conditions worsen under the Build 1 Alternative due to a higher southbound left-turn/northbound through volume conflict that increases the southbound left-turn movement delay. The volume arriving on the northbound approach is over 140 vehicles greater under the Build 1 Alternative than No Build conditions. The percent demand served is anticipated to increase from 78 percent to 97 percent in the AM peak hour and from 84 percent to 86 percent in the PM peak hour.
- *Mathilda Avenue/ Ross Drive* – Intersection level of service is anticipated to improve from LOS F to LOS C in the AM peak hour and from LOS F to LOS D during the PM peak hour. The percent demand served is anticipated to increase from 75 percent to 98 percent in the AM peak hour and from 84 percent to 88 percent in the PM peak hour.
- *Mathilda Avenue/ US 101 Northbound Ramps (Build Conditions)* – This intersection is anticipated to operate at LOS D during the AM and PM peak hour. The percent demand served is estimated at 98 percent during the AM peak hour and 90 percent during the PM peak hour.
- *Mathilda Avenue/ US 101 Southbound Ramps (Build Conditions)* – This intersection is anticipated to operate at LOS C during the AM peak hour and LOS B during the PM peak hour. The percent demand served is estimated at 98 percent during the AM peak hour and 92 percent during the PM peak hour.
- *Mathilda Avenue/ Almanor Avenue-Ahwanee Avenue* – Intersection level of service is anticipated to remain unchanged (LOS F) during the AM peak hour and improve from LOS F to LOS C in the PM peak hour. Although the intersection would continue to operate at LOS F during the AM peak hour under Build 1 Alternative the overall intersection delay would be reduced by over 70 percent compared to No Build conditions. The percent demand served is anticipated to increase from 82 percent to 98 percent in the AM peak hour and from 87 percent to 94 percent in the PM peak hour.
- *US 101 Northbound On-Ramp/Moffett Park Drive* – Intersection level of service is anticipated to remain unchanged (LOS A) during the AM peak hour and improve from LOS E to LOS A in the PM peak hour. The improvement in LOS during the PM peak hour is due to the lane reconfiguration at Mathilda Avenue and Moffett Park Drive from one left-turn/through lane and one right-turn lane to one shared left-turn/right-turn lane and one right-turn lane. This creates larger queue storage and increased vehicular throughput at Mathilda Avenue which results in less queue spillback at the US 101 Northbound On-Ramp and Moffett Park Drive intersection. The percent demand served is anticipated to increase from 87 percent to 99 percent in the AM peak hour and from 80 percent to 93 percent in the PM peak hour.
- *Innovation Way/Moffett Park Drive* – Intersection level of service is anticipated to remain unchanged (LOS B) during the AM peak hour and during the PM peak hour (LOS F). Although the intersection would continue to operate at LOS F during the PM peak hour under Build 1 Alternative the overall intersection delay would be reduced by over 50 percent compared to No



Build conditions. The improvement in delay during the PM peak hour is due to two factors. First, the lane reconfiguration at Mathilda Avenue and Moffett Park Drive from one left-turn/through lane and one right-turn lane to one-shared left-turn/right-turn lane and one right-turn lane which increases the amount of right-turn storage and right-turn throughput. Second, the eastbound through volume at Mathilda Avenue/Moffett Park Drive under No Build Conditions is now diverted to Innovation Way which results in a portion of the eastbound through volume at Innovation Way / Moffett Park Drive being shifted to the eastbound left-turn movement. The percent demand served is anticipated to increase from 86 percent to 100 percent in the AM peak hour and from 78 percent to 88 percent in the PM peak hour.

- *Innovation Way/Eleventh Avenue* – Intersection level of service is anticipated to remain unchanged (LOS B) during the AM peak hour and during the PM peak hour (LOS F). Although the intersection would continue to operate at LOS F during the PM peak hour under Build 1 Alternative the overall intersection delay would be reduced by over 55 percent compared to No Build conditions. The percent demand served is anticipated to increase from 85 percent to 99 percent in the AM peak hour and decrease from 90 percent to 88 percent in the PM peak hour.
- *Innovation Way/Juniper Networks Driveway* – Intersection level of service is anticipated to remain unchanged (LOS B) during the AM peak hour and during the PM peak hour (LOS F). Although the intersection would continue to operate at LOS F during the PM peak hour under Build 1 Alternative the overall intersection delay would be reduced by over 24 percent compared to No Build conditions. The percent demand served is anticipated to increase from 83 percent to 100 percent in the AM peak hour and from 73 percent to 87 percent in the PM peak hour.
- *Bordeaux Drive/Innovation Way* – Intersection level of service is anticipated to worsen from LOS A to LOS B during the AM peak hour and from LOS B to LOS F during the PM peak hour. The proposed project design would result in an increase over 330 percent in traffic volume at this location during the PM peak hour. The percent demand served is anticipated to decrease from 100 percent to 99 percent in the AM peak hour and from 100 percent to 61 percent in the PM peak hour.

The Build 1 Alternative would improve traffic conditions at most of the study locations but also worsen some of the study locations for at least one peak hour. During the AM peak hour the total vehicle hours of delay would be reduced from 1,319 to 493 (63 percent reduction) and from 1,504 to 1,285 (15 percent reduction) during the PM peak hour. The reduction in overall vehicle hours of delay for the AM and PM peak hour indicates the Build 1 Alternative would provide an overall benefit to the traffic operations in the study area compared to No Build conditions.

Build 2 Alternative

Below is a brief summary of the operations at the study locations under Build 2 Alternative in Year 2018 and how they compare to No Build conditions.

- *Mathilda Avenue/Fifth Avenue* – Intersection level of service is anticipated to remain unchanged (LOS B during the AM peak hour and LOS F during the PM peak hour). The overall intersection delay would also remain relatively unchanged (less than a 5 percent change) for the AM and PM peak hour. The percent demand served is anticipated to increase from 88 percent to 96 percent in the AM peak hour and increase from about 86 percent to 87 percent in the PM peak hour.



- *Mathilda Avenue/Innovation Way* – Intersection level of service is anticipated to remain unchanged during the PM peak hour (LOS F), but decrease from LOS D to LOS E during the AM peak hour. The overall intersection delay would increase by approximately 25 seconds in the AM peak hour due to the vehicle volume that shifts from Moffett Park Drive to Innovation Way. The PM peak hour delay decreases by approximately 50 seconds due to the additional capacity provided by the DDI traveling southbound on Mathilda Avenue. The percent demand served is anticipated to increase from 84 percent to 95 percent in the AM peak hour and increase from about 80 percent to 83 percent in the PM peak hour.
- *Mathilda Avenue/Moffett Park Drive/SR 237 Westbound Ramps* – Intersection level of service is anticipated to improve from LOS F to LOS C in the AM peak hour and from LOS F to LOS E during the PM peak hour. The overall intersection delay would decrease by well over 265 seconds in the AM peak hour and 220 seconds in the PM peak hour. The reduction in peak hour delay is a result of the efficient signal timing as a results of the DDI and the closure of Moffett Park Drive to Mathilda Avenue. The percent demand served is anticipated to increase from 81 percent to 95 percent in the AM peak hour and increase from about 83 percent to 87 percent in the PM peak hour.
- *Mathilda Avenue/ SR 237 Eastbound Ramps* – Intersection level of service is anticipated to improve from LOS F to LOS D in the AM peak hour and worsen from LOS B to LOS E during the PM peak hour. The PM peak hour conditions worsen under the Build 2 Alternative due to the eastbound right-turn lane from the SR 237 off-ramp and the close proximity of Ross Drive to the DDI. The DDI is able to throughput a higher demand as shown by the increase in percent demand served in the PM peak hour from 85 percent to 89 percent, however, this then backs up at Ross Drive preventing vehicles from the off-ramp to enter Mathilda Avenue. The percent demand served in the AM peak hour increases from 84 percent to 89 percent.
- *Mathilda Avenue/ Ross Drive* – Intersection level of service is anticipated to remain at LOS F in the AM peak hour and improve from LOS F to LOS E during the PM peak hour. The percent demand served is anticipated to increase from 75 percent to 92 percent in the AM peak hour and from 84 percent to 90 percent in the PM peak hour.
- *Mathilda Avenue/ US 101 Northbound Ramps (Build Conditions)* – This intersection is anticipated to operate at LOS E during the AM peak hour and LOS D during the PM peak hour. The percent demand served is estimated at 95 percent during the AM peak hour and 92 percent during the PM peak hour.
- *Mathilda Avenue/ US 101 Southbound Ramps (Build Conditions)* – This intersection is anticipated to operate at LOS C during the AM peak hour and LOS B during the PM peak hour. The percent demand served is estimated at 95 percent during the AM peak hour and 93 percent during the PM peak hour.
- *Mathilda Avenue/ Almanor Avenue-Ahwanee Avenue* – Intersection level of service is anticipated to remain unchanged (LOS F) during the AM peak hour and improve from LOS F to LOS D in the PM peak hour. Although the intersection would continue to operate at LOS F during the AM peak hour under Build 1 Alternative the overall intersection delay would be reduced by over 145 seconds of delay compared to No Build conditions. The percent demand served is anticipated to increase from 82 percent to 95 percent in the AM peak hour and from 87 percent to 96 percent in the PM peak hour.
- *US 101 Northbound On-Ramp/Moffett Park Drive* – Intersection level of service is anticipated to remain unchanged (LOS A) during the AM peak hour and improve from LOS E to LOS D in the PM



peak hour. The percent demand served is anticipated to increase from 87 percent to 95 percent in the AM peak hour and from 80 percent to 93 percent in the PM peak hour.

- *Innovation Way/Moffett Park Drive* – Intersection level of service is anticipated to remain unchanged (LOS B) during the AM peak hour and during the PM peak hour (LOS F). Although the intersection would continue to operate at LOS F during the PM peak hour under Build 2 Alternative the overall intersection delay would be reduced by over 45 percent compared to No Build conditions. The percent demand served is anticipated to increase from 86 percent to 95 percent in the AM peak hour and from 78 percent to 86 percent in the PM peak hour.
- *Innovation Way/Eleventh Avenue* – Intersection level of service is anticipated to remain unchanged (LOS B) during the AM peak hour and during the PM peak hour (LOS F). Although the intersection would continue to operate at LOS F during the PM peak hour under Build 2 Alternative the overall intersection delay would be reduced by over 40 percent compared to No Build conditions. The percent demand served is anticipated to increase from 85 percent to 96 percent in the AM peak hour and decrease from 90 percent to 86 percent in the PM peak hour.
- *Innovation Way/Juniper Networks Driveway* – Intersection level of service is anticipated to remain unchanged (LOS B) during the AM peak hour and during the PM peak hour (LOS F). Although the intersection would continue to operate at LOS F during the PM peak hour under Build 2 Alternative the overall intersection delay would be reduced by more than 10 seconds compared to No Build conditions. The percent demand served is anticipated to increase from 83 percent to 96 percent in the AM peak hour and from 73 percent to 81 percent in the PM peak hour.
- *Bordeaux Drive/Innovation Way* – Intersection level of service is anticipated to worsen from LOS A to LOS E during the AM peak hour and from LOS B to LOS F during the PM peak hour. The proposed project design would result in an increase over 330 percent in traffic volume at this location during the PM peak hour. However the demand at this intersection is less than a fourth of the volume along Mathilda Avenue. The percent demand served is anticipated to decrease from 100 percent to 95 percent in the AM peak hour and from 100 percent to 83 percent in the PM peak hour.

The Build 2 Alternative would improve traffic conditions at most of the study locations but also worsen some of the study locations for at least one peak hour. During the AM peak hour the total vehicle hours of delay would be reduced from 1,319 to 773 (42 percent reduction) and from 1,504 to 1,107 (26 percent reduction) during the PM peak hour. The reduction in overall vehicle hours of delay for the AM and PM peak hour indicates the Build 2 Alternative would provide an overall benefit to the traffic operations in the study area compared to No Build conditions.



TABLE 5-2: YEAR 2018 PEAK HOUR INTERSECTION ANALYSIS¹

| | Intersection | Peak Hour ² | No Build | | | Build 1 Alternative | | | Build 2 Alternative | | |
|--------------------------------------|---|------------------------|--------------------|------------------|------------------------------|---------------------|------------------|------------------------------|---------------------|------------------|------------------------------|
| | | | Delay ³ | LOS ⁴ | % Demand Served ⁵ | Delay ³ | LOS ⁴ | % Demand Served ⁵ | Delay ³ | LOS ⁴ | % Demand Served ⁵ |
| 1 | Mathilda Avenue / Fifth Avenue ⁶ | AM | 17.4 | B | 87.8 | 17.1 | B | 97.5 | 15.8 | B | 95.8 |
| | | PM | 227.0 | F | 85.7 | 238.1 | F | 79.8 | 177.3 | F | 87.4 |
| 2 | Mathilda Avenue / Innovation Way ⁶ | AM | 42.1 | D | 83.5 | 44.1 | D | 98.7 | 69.7 | E | 94.6 |
| | | PM | 206.1 | F | 79.9 | 218.4 | F | 77.0 | 152.2 | F | 83.0 |
| 3 | Mathilda Avenue / Moffett Park Drive / SR 237 Westbound Ramps | AM | >300 | F | 80.5 | 53.1 | D | 98.2 | 32.5 | C | 94.8 |
| | | PM | >300 | F | 82.9 | 197.8 | F | 81.7 | 79.0 | E | 86.8 |
| 4 | Mathilda Avenue / SR 237 Eastbound Ramps | AM | 116.3 | F | 78.1 | 28.7 | C | 97.2 | 36.6 | D | 94.3 |
| | | PM | 19.4 | B | 84.3 | 29.0 | C | 85.9 | 56.4 | E | 88.7 |
| 5 | Mathilda Avenue / Ross Drive | AM | 285.7 | F | 74.6 | 31.6 | C | 97.7 | 98.6 | F | 92.5 |
| | | PM | 141.4 | F | 84.3 | 46.9 | D | 88.2 | 59.5 | E | 90.1 |
| 6 | Mathilda Avenue / US 101 Northbound Ramps (Build) | AM | N/A | N/A | N/A | 47.2 | D | 98.2 | 65.0 | E | 94.5 |
| | | PM | N/A | N/A | N/A | 47.8 | D | 90.3 | 52.3 | D | 91.9 |
| 7 | Mathilda Avenue / US 101 Southbound Ramps (Build) | AM | N/A | N/A | N/A | 20.7 | C | 97.8 | 33.7 | C | 94.4 |
| | | PM | N/A | N/A | N/A | 11.1 | B | 91.7 | 12.0 | B | 93.3 |
| 8 | Mathilda Avenue / Almanor Avenue-Ahwanee Avenue | AM | >300 | F | 82.3 | 83.1 | F | 97.6 | 152.1 | F | 95.1 |
| | | PM | 139.9 | F | 87.3 | 34.9 | C | 94.3 | 40.0 | D | 95.8 |
| 9 | US 101 Northbound On-Ramp / Moffett Park Drive | AM | 3.9 | A | 86.8 | 5.7 | A | 98.8 | 4.5 | A | 95.2 |
| | | PM | 63.0 | E | 80.0 | 8.7 | A | 93.3 | 35.2 | D | 93.4 |
| 10 | Innovation Way / Moffett Park Drive ⁶ | AM | 13.7 | B | 85.7 | 19.2 | B | 99.5 | 16.5 | B | 94.8 |
| | | PM | 190.5 | F | 78.4 | 90.7 | F | 87.6 | 105.7 | F | 86.4 |
| 11 | Innovation Way / Eleventh Avenue | AM | 10.5 | B | 85.0 | 11.8 | B | 98.5 | 12.1 | B | 96.4 |
| | | PM | 144.4 | F | 89.8 | 61.7 | F | 88.3 | 85.0 | F | 86.2 |
| 12 | Innovation Way / Juniper Networks Driveway | AM | 14.0 | B | 83.3 | 14.7 | B | 100.0 | 15.6 | B | 96.5 |
| | | PM | >300 | F | 72.8 | 227.0 | F | 87.0 | 288.3 | F | 81.1 |
| 13 | Bordeaux Drive / Innovation Way | AM | 3.2 | A | 100.0 | 12.7 | B | 99.1 | 57.4 | E | 94.7 |
| | | PM | 13.5 | B | 100.0 | >300 | F | 61.1 | >300 | F | 83.1 |
| Total Vehicle Hours of Delay (hours) | | AM | | 1,319 | | 493 | | 773 | | | |
| | | PM | | 1,504 | | 1,285 | | 1,107 | | | |



TABLE 5-2: YEAR 2018 PEAK HOUR INTERSECTION ANALYSIS¹

| Intersection | Peak Hour ² | No Build | | | Build 1 Alternative | | | Build 2 Alternative | | |
|------------------------------------|------------------------|--------------------|------------------|------------------------------|---------------------|------------------|------------------------------|---------------------|------------------|------------------------------|
| | | Delay ³ | LOS ⁴ | % Demand Served ⁵ | Delay ³ | LOS ⁴ | % Demand Served ⁵ | Delay ³ | LOS ⁴ | % Demand Served ⁵ |
| Network-wide Percent Demand Served | AM | | 89.0% | | | 99.3% | | | 94.8% | |
| | PM | | 85.8% | | | 89.9% | | | 91.8% | |

Notes: Results in **bold** represent unacceptable levels of service, N/A=not applicable.

1. Results based on SimTraffic simulation of five runs.
2. AM – morning peak hour, PM – evening peak hour
3. Average control delay calculated using the *Highway Capacity Manual (HCM)* (Transportation Research Board, 2010) methodology and Synchro/SimTraffic 8.0 analysis software. For signalized and all-way stop-controlled intersections, average control delay is for the intersection, as a whole.
4. For signalized and all-way stop-controlled intersections the LOS for the intersection as a whole is presented.
5. Modeled traffic volume expressed as a ratio of **demand** traffic volume. For example: 100% indicates all demand is served.
6. These intersections are coordinated with a light rail crossing. Under Year 2018, the headway in each direction is assumed to increase from 15 minutes to 12 minutes in each direction based on the VTA light-rail efficiency project currently underway.

Source: Fehr & Peers, 2016.



INTERSECTION 95TH PERCENTILE QUEUES

No Build 95th Percentile Queues

Table 5-3 presents the 2018 No Build peak hour 95th percentile queuing analysis results. Analysis results worksheets are presented in **Appendix L**. The projected traffic demand is anticipated to far exceed the available roadway capacity. As a result, vehicle queues will exceed available storage at most study locations and queues from one intersection will impact operations at adjacent intersections. During the AM peak hour, northbound Mathilda vehicle queues are expected to extend south past San Aleso Avenue. Due to the congestion on northbound Mathilda Avenue, particularly at the Ross Drive intersection, the US 101 northbound off-ramp queues would spill back onto the mainline. Additionally, the SR 237 westbound off-ramp vehicle queue is anticipated to extend back onto the mainline due to congestion at the ramp terminal.

During the PM peak hour, the projected high southbound traffic volumes on Mathilda Avenue and the close spacing between intersections near the SR 237 interchange would cause vehicle queues on southbound Mathilda Avenue to extend from SR 237 north past 5th Avenue. Eastbound Innovation Way and Moffett Park Drive are also expected to experience high delays and extensive queuing. Additionally, the SR 237 westbound off-ramp queues are expected to extend back to the freeway mainline due to congestion at the ramp terminal.

TABLE 5-3: YEAR 2018 NO BUILD QUEUING ANALYSIS RESULTS

| Intersection | Movement ¹ | Available Storage ² | AM Peak Hour 95 th Percentile Queue (ft) | PM Peak Hour 95 th Percentile Queue (ft) |
|-------------------------------------|-----------------------|--------------------------------|---|---|
| 1: Mathilda Avenue / Fifth Avenue | NB-L | 425 | 100 | 125 |
| | NB-T | 1,125 | 175 | 125 |
| | SB-L | 250 | 50 | 175 |
| | SB-T | 1,325 | 125 | 1,925 |
| | SB-R | 250 | 25 | 200 |
| | EB-L | 625 | 50 | 100 |
| | EB-T | 625 | 50 | 50 |
| | EB-R | 625 | 25 | 75 |
| | WB-L | 925 | 75 | 700 |
| 2: Mathilda Avenue / Innovation Way | WB-T | 75 | 75 | 100 |
| | NB-L | 400 | 375 | 75 |
| | NB-T | 975 | 325 | 150 |
| | NB-TR | 975 | 375 | 175 |
| | SB-L | 75 | 25 | 25 |
| | SB-T | 975 | 175 | 1,275 |
| | SB-R | 225 | 125 | 350 |
| | EB-L | 200 | 25 | 125 |
| | EB-TR | 200 | 50 | 50 |
| EB-R | 200 | 50 | 325 | |



TABLE 5-3: YEAR 2018 NO BUILD QUEUING ANALYSIS RESULTS

| Intersection | Movement ¹ | Available Storage ² | Peak Hour | |
|--|-----------------------|--------------------------------|--|--|
| | | | AM Peak Hour 95 th Percentile Queue (ft) | PM Peak Hour 95 th Percentile Queue (ft) |
| | WB-L | 425 | 25 | 75 |
| | WB-LTR | 225 | 25 | 75 |
| 3: Mathilda Avenue / Moffett Park Drive / SR 237 Westbound Ramps | NB-L (MP) | 125 | 50 | 50 |
| | NB-L (237) | 175 | 175 | 150 |
| | NB-T | 300 | 325 | 200 |
| | SB-L (MP) | 175 | 50 | 125 |
| | SB-T | 1,100 | 500 | 1,200 |
| | EB-L (MP) | 350 | 75 | 475 |
| | EB-T (MP) | 1,100 | 125 | 1,325 |
| | EB-R (MP) | 1,100 | 100 | 975 |
| | WB-L (MP) | 300 | 250 | 1,275 |
| | WB-T (MP) | 650 | 400 | 675 |
| | WB-L (237) | 1,125 | 1,300 | 4,675 |
| | WB-R (237) | 325 | 400 | 500 |
| 4: Mathilda Avenue / SR 237 Eastbound Ramps | NB-T | 275 | 325 | 100 |
| | NB-R | 275 | 375 | 200 |
| | SB-L | 200 | 100 | 175 |
| | SB-T | 200 | 225 | 225 |
| | EB-L | 1,025 | 2,900 | 125 |
| | EB-LTR | 450 | 650 | 200 |
| 5: Mathilda Avenue / Ross Drive | NB-L | 150 | 100 | 175 |
| | NB-T | 2,200 | 1,100 | 1,100 |
| | SB-L | 150 | 150 | 175 |
| | SB-T | 250 | 275 | 200 |
| | EB-L | 650 | 500 | 275 |
| | EB-T | 75 | 125 | 125 |
| | EB-R | 50 | 75 | 75 |
| | WB-L | 75 | 2,275 | 3,225 |
| | WB-T | 75 | 125 | 125 |
| WB-R | 75 | 100 | 100 | |
| 6. Mathilda Avenue/US 101 NB Ramps** | N/A | N/A | N/A ³ | N/A ⁴ |
| 7. Mathilda Avenue/US 101 SB Ramps** | N/A | N/A | N/A | N/A |



TABLE 5-3: YEAR 2018 NO BUILD QUEUING ANALYSIS RESULTS

| Intersection | Movement ¹ | Available Storage ² | AM Peak Hour | PM Peak Hour |
|--|-----------------------|--------------------------------|--|--|
| | | | 95 th Percentile Queue (ft) | 95 th Percentile Queue (ft) |
| 8: Mathilda Avenue / Almanor Avenue-Ahwanee Avenue | NB-L | 375 | 350 | 300 |
| | NB-T | 675 | >5,000 | 1,900 |
| | NB-R | 75 | 75 | 100 |
| | SB-L | 125 | 200 | 225 |
| | SB-T | 2,200 | 725 | 1,500 |
| | EB-L | 1,025 | 250 | 350 |
| | EB-T | 125 | 125 | 250 |
| | WB-L | 250 | 225 | 225 |
| | WB-T | 1,025 | 600 | 425 |
| 9: US 101 Northbound On-Ramp / Moffett Park Drive | WB-R | 75 | 150 | 150 |
| | EB-T | 850 | 50 | 1,100 |
| | EB-R | 150 | 25 | 425 |
| | WB-L | 850 | 50 | 250 |
| 10: Innovation Way / Moffett Park Drive | WB-T | 850 | 100 | 25 |
| | SB-L | 575 | 50 | 525 |
| | SB-LTR | 575 | 150 | 625 |
| | EB-L | 225 | 100 | 400 |
| | EB-T | 850 | 75 | 1,100 |
| | WB-T | 1,150 | 250 | 175 |
| 11: Innovation Way / Eleventh Avenue | WB-R | 225 | 125 | 50 |
| | NB-L | 125 | 50 | 25 |
| | NB-LT | 575 | 50 | 150 |
| | SB-T | 1,000 | 50 | 75 |
| | EB-L | 1,000 | 125 | 175 |
| 12: Innovation Way / Juniper Driveway | EB-R | 125 | 50 | 175 |
| | NB-L | 300 | 50 | 1,575 |
| | NB-T | 300 | 75 | 1,100 |
| | SB-T | 125 | 50 | 25 |
| | SB-R | 900 | 50 | 1,075 |
| | EB-L | 300 | 250 | 225 |
| | EB-R | 300 | 300 | 175 |
| 13: Bordeaux Drive / Innovation Way | NB-L | 325 | 50 | 50 |
| | NB-TR | 2,025 | 75 | 50 |
| | SB-L | 125 | 25 | 25 |
| | SB-TR | 725 | 50 | 75 |
| | EB-LT | 375 | 50 | 50 |
| | EB-R | 125 | 50 | 50 |
| | WB-LT | 125 | 25 | 25 |



TABLE 5-3: YEAR 2018 NO BUILD QUEUING ANALYSIS RESULTS

| Intersection | Movement ¹ | Available Storage ² | AM Peak Hour 95 th Percentile Queue (ft) | PM Peak Hour 95 th Percentile Queue (ft) |
|--------------|-----------------------|--------------------------------|---|---|
| | WB-R | 125 | 25 | 25 |

Notes: **Bold** denotes locations where storage length is exceeded.

**Indicates intersection is signalized under Build 1 and Build 2 Alternatives, but operates as a free movement under the No Build Alternative.

1. NB-northbound, SB-southbound, EB-eastbound, WB-westbound, L-left-turn movement, T-through movement, R-right-turn movement, (MP)-turn onto/from Moffett Park Drive, (237)-turn onto/from SR 237 WB Ramps.
2. Available storage lengths are provided on a "per lane" basis. For example, an available storage of 425 means each lane in the associated movement has a storage length of 425 feet.
3. Queuing at the US 101 northbound diagonal off-ramp was observed to extend onto the freeway mainline in the AM peak hour under Existing Conditions. This queuing is anticipated to worsen under Year 2018 No Build conditions.
4. Queuing at the US 101 northbound loop off-ramp was observed to extend onto the freeway mainline in the PM peak hour under Existing Conditions. This queuing is anticipated to worsen under Year 2018 No Build conditions.

Source: Fehr & Peers, 2016.

Build 1 95th Percentile Queues

Table 5-4 presents the Build 1 peak hour 95th percentile queuing analysis results. Analysis results worksheets are presented in **Appendix L**. The capacity enhancements at intersections on Mathilda Avenue and the realignment of the freeway ramps would improve traffic operations and reduce vehicle queue lengths compared to No Build conditions. The US 101 Northbound off-ramp and Southbound off-ramp queues are not anticipated to extend back to the freeway mainline under Build 1. During the AM peak hour, the SR 237 ramp terminal intersections would provide adequate vehicle storage to accommodate the 95th percentile queue lengths. Therefore, off-ramp queues are not expected to spill back to freeway mainline. During the PM peak hour, the realignment of the SR 237 ramps would reduce the SR 237 off-ramp queue lengths, but the westbound off-ramp queue is still anticipated to extend back to near the off-ramp gore point area and potentially onto the freeway mainline. Vehicle queues on southbound Mathilda Avenue and Innovation Way would still exist during the PM peak hour.

TABLE 5-4: YEAR 2018 BUILD 1 QUEUING ANALYSIS RESULTS

| Intersection | Movement ¹ | Available Storage ² | AM Peak Hour 95 th Percentile Queue (ft) | PM Peak Hour 95 th Percentile Queue (ft) |
|-----------------------------------|-----------------------|--------------------------------|---|---|
| 1: Mathilda Avenue / Fifth Avenue | NB-L | 425 | 100 | 125 |
| | NB-T | 1,125 | 200 | 125 |
| | SB-L | 250 | 50 | 175 |
| | SB-T | 1,325 | 125 | 2,125 |
| | SB-R | 250 | 25 | 175 |
| | EB-L | 625 | 50 | 100 |
| | EB-T | 625 | 25 | 50 |
| | EB-R | 625 | 25 | 75 |
| | WB-L | 925 | 75 | 225 |
| | WB-T | 75 | 75 | 100 |



TABLE 5-4: YEAR 2018 BUILD 1 QUEUING ANALYSIS RESULTS

| Intersection | Movement ¹ | Available Storage ² | Peak Hour | |
|--|-----------------------|--------------------------------|--|--|
| | | | AM Peak Hour 95 th Percentile Queue (ft) | PM Peak Hour 95 th Percentile Queue (ft) |
| 2: Mathilda Avenue / Innovation Way | NB-L | 400 | 325 | 25 |
| | NB-T | 975 | 525 | 225 |
| | NB-R | 975 | 650 | 150 |
| | SB-L | 75 | 75 | 150 |
| | SB-T | 975 | 150 | 1,300 |
| | SB-R | 225 | 125 | 350 |
| | EB-LT | 200 | 150 | 325 |
| | EB-R | 200 | 25 | 350 |
| | WB-L | 425 | 500 | 775 |
| WB-LTR | 225 | 275 | 250 | |
| 3: Mathilda Avenue / Moffett Park Drive / SR 237 Westbound Ramps | NB-L | 350 | 425 | 325 |
| | NB-T | 350 | 450 | 150 |
| | SB-T | 975 | 325 | 1,075 |
| | SB-TR | 975 | 425 | 1,125 |
| | EB-LR | 1,125 | 100 | 1,350 |
| | EB-R | 1,125 | 50 | 1,350 |
| | WB-L | 525 | 375 | 650 |
| | WB-LT | 1,225 | 375 | 1,300 |
| WB-TR | 1,225 | 375 | 275 | |
| 4: Mathilda Avenue / SR 237 Eastbound Ramps | NB-T | 275 | 150 | 100 |
| | NB-R | 275 | 50 | 125 |
| | SB-L | 325 | 275 | 350 |
| | SB-T | 350 | 375 | 475 |
| | EB-L | 1,025 | 550 | 150 |
| | EB-LT | 1,025 | 475 | 125 |
| | EB-R | 450 | 125 | 275 |
| 5: Mathilda Avenue / Ross Drive | NB-L | 150 | 225 | 250 |
| | NB-T | 700 | 725 | 475 |
| | SB-L | 150 | 125 | 150 |
| | SB-T | 250 | 275 | 275 |
| | EB-L | 650 | 125 | 100 |
| | EB-T | 75 | 150 | 275 |
| | EB-R | 50 | 50 | 100 |
| | WB-L | 75 | 125 | 125 |
| | WB-T | 75 | 350 | 900 |
| WB-R | 75 | 125 | 100 | |



TABLE 5-4: YEAR 2018 BUILD 1 QUEUING ANALYSIS RESULTS

| Intersection | Movement ¹ | Available Storage ² | Peak Hour | |
|--|-----------------------|--------------------------------|--|--|
| | | | AM Peak Hour 95 th Percentile Queue (ft) | PM Peak Hour 95 th Percentile Queue (ft) |
| 6: Mathilda Avenue / US 101 NB Ramps | NB-T | 575 | 525 | 275 |
| | NB-R | 575 | 175 | 50 |
| | SB-L | 375 | 50 | 225 |
| | SB-T | 700 | 325 | 700 |
| | WB-L | 1,025 | 400 | 150 |
| | WB-R | 1,025 | 175 | 125 |
| 7: Mathilda Avenue / US 101 SB Ramps | NB-T | 750 | 775 | 175 |
| | NB-R | 750 | 700 | 75 |
| | SB-T | 575 | 250 | 150 |
| | SB-TR | 575 | 300 | 325 |
| | EB-L | 1,050 | 225 | 100 |
| | EB-R | 1,050 | 25 | 25 |
| 8: Mathilda Avenue / Almanor Avenue-Ahwanee Avenue | NB-L | 375 | 425 | 150 |
| | NB-T | 750 | 1,225 | 350 |
| | NB-R | 75 | 325 | 325 |
| | SB-L | 125 | 350 | 300 |
| | SB-T | 750 | 525 | 425 |
| | EB-L | 1,025 | 125 | 300 |
| | EB-T | 125 | 100 | 225 |
| | WB-L | 250 | 150 | 100 |
| | WB-R | 75 | 125 | 100 |
| 9: US 101 Northbound On-Ramp / Moffett Park Drive | EB-T | 850 | 50 | 300 |
| | EB-R | 150 | 25 | 125 |
| | WB-L | 850 | 50 | 175 |
| | WB-T | 850 | 75 | 25 |
| 10: Innovation Way / Moffett Park Drive | SB-L | 575 | 50 | 525 |
| | SB-LTR | 575 | 175 | 600 |
| | EB-L | 225 | 150 | 350 |
| | EB-T | 850 | 50 | 625 |
| | WB-T | 1,150 | 275 | 150 |
| | WB-R | 225 | 350 | 200 |



TABLE 5-4: YEAR 2018 BUILD 1 QUEUING ANALYSIS RESULTS

| Intersection | Movement ¹ | Available Storage ² | AM Peak Hour | PM Peak Hour |
|---------------------------------------|-----------------------|--------------------------------|--|--|
| | | | 95 th Percentile Queue (ft) | 95 th Percentile Queue (ft) |
| 11: Innovation Way / Eleventh Avenue | NB-L | 125 | 100 | 75 |
| | NB-T | 575 | 125 | 200 |
| | SB-L | 175 | 75 | 75 |
| | SB-T | 1,000 | 50 | 50 |
| | SB-TR | 1,000 | 225 | 50 |
| | EB-L | 125 | 50 | 125 |
| | EB-LT | 300 | 25 | 900 |
| | EB-R | 300 | 75 | 1,050 |
| 12: Innovation Way / Juniper Driveway | NB-L | 125 | 150 | 200 |
| | NB-T | 900 | 100 | 825 |
| | SB-T | 300 | 125 | 225 |
| | SB-R | 300 | 150 | 100 |
| | EB-L | 150 | 100 | 2,325 |
| 13: Bordeaux Drive / Innovation Way | EB-R | 150 | 50 | 1,000 |
| | NB-L | 325 | 175 | 925 |
| | NB-TR | 2,025 | 75 | 800 |
| | SB-L | 125 | 25 | 25 |
| | SB-TR | 725 | 125 | 4,875 |
| | EB-LT | 375 | 275 | 75 |
| | EB-R | 125 | 150 | 100 |
| | WB-LT | 125 | 25 | 25 |
| WB-R | 125 | 25 | 25 | |

Notes: **Bold** denotes locations where storage length is exceeded.

1. NB-northbound, SB-southbound, EB-eastbound, WB-westbound, L-left-turn movement, T-through movement, R-right-turn movement, (MP)-turn onto/from Moffett Park Drive, (237)-turn onto/from SR 237 WB Ramps.
2. Available storage lengths are provided on a "per lane" basis. For example, an available storage of 425 means each lane in the associated movement has a storage length of 425.

Source: Fehr & Peers, 2016.

Build 2 95th Percentile Queues

Table 5-5 presents the Build 2 peak hour 95th percentile queuing analysis results. Analysis results worksheets are presented in **Appendix L**. Similar to Build 1, capacity enhancements on Mathilda Avenue and the realignment of freeway ramps would improve traffic operations and reduce queue lengths compared to No Build condition. Both the US 101 eastbound off-ramp and westbound off-ramp queues are not anticipated to extend back to the freeway mainline under Build 2. The SR 237 diverging diamond interchange configuration would substantially reduce the westbound off-ramp queue lengths to fit within the available storage distance on the ramp. However, this configuration would cause the SR 237 eastbound off-ramp queue to spill back to the freeway mainline in the PM peak hour due to the close proximity of Ross Drive and the right-turn-on-red limitations at the off-ramp which limits the number of right-turning



vehicles looking to access southbound Mathilda Avenue. Moreover, the closure of the Moffett Park Drive eastbound access to Mathilda Avenue would shift traffic to Innovation Way. As a result, the queue lengths on eastbound Innovation Way and Juniper Driveway are anticipated to increase compared to Build 1.

TABLE 5-5: YEAR 2018 BUILD 2 QUEUING ANALYSIS RESULTS

| Intersection | Movement ¹ | Available Storage ² | AM Peak Hour 95 th Percentile Queue (ft) | PM Peak Hour 95 th Percentile Queue (ft) |
|--|-----------------------|--------------------------------|--|--|
| 1: Mathilda Avenue / Fifth Avenue | NB-L | 425 | 100 | 125 |
| | NB-T | 1,150 | 200 | 125 |
| | SB-L | 225 | 50 | 150 |
| | SB-T | 1,375 | 125 | 1,450 |
| | SB-R | 225 | 25 | 200 |
| | EB-L | 625 | 75 | 125 |
| | EB-T | 625 | 50 | 75 |
| | EB-R | 625 | 25 | 75 |
| | WB-L | 925 | 75 | 675 |
| | WB-T | 75 | 50 | 100 |
| 2: Mathilda Avenue / Innovation Way | NB-L | 725 | 575 | 125 |
| | NB-T | 975 | 425 | 175 |
| | NB-R | 975 | 550 | 150 |
| | SB-L | 75 | 75 | 150 |
| | SB-T | 1,150 | 200 | 1,275 |
| | SB-R | 225 | 150 | 375 |
| | EB-LT | 200 | 200 | 350 |
| | EB-R | 200 | 25 | 350 |
| | WB-L | 425 | 850 | 800 |
| WB-LTR | 225 | 250 | 250 | |
| 3: Mathilda Avenue / Moffett Park Drive / SR 237 Westbound Ramps | NB-L | 150 | 150 | 25 |
| | NB-T | 400 | 450 | 175 |
| | SB-TR | 975 | 375 | 1,200 |
| | WB-L | 1,075 | 250 | 975 |
| | WB-R | 550 | 500 | 650 |
| 4: Mathilda Avenue / SR 237 Eastbound Ramps | NB-T | 150 | 275 | 200 |
| | NB-R | 150 | 25 | 75 |
| | SB-L | 175 | 0 | 50 |
| | SB-T | 400 | 325 | 400 |
| | EB-L | 1,075 | 325 | 1,975 |
| | EB-R | 450 | 25 | 1,575 |



TABLE 5-5: YEAR 2018 BUILD 2 QUEUING ANALYSIS RESULTS

| Intersection | Movement ¹ | Available Storage ² | Peak Hour | |
|--|-----------------------|--------------------------------|--|--|
| | | | AM Peak Hour 95 th Percentile Queue (ft) | PM Peak Hour 95 th Percentile Queue (ft) |
| 5: Mathilda Avenue / Ross Drive | NB-L | 250 | 275 | 250 |
| | NB-T | 700 | 825 | 600 |
| | SB-L | 225 | 125 | 200 |
| | SB-T | 225 | 175 | 225 |
| | EB-L | 650 | 150 | 125 |
| | EB-T | 75 | 475 | 275 |
| | EB-R | 50 | 50 | 100 |
| | WB-L | 75 | 125 | 125 |
| | WB-T | 75 | 3,925 | 1,400 |
| 6: Mathilda Avenue / US 101 NB Ramps | WB-R | 75 | 125 | 100 |
| | NB-T | 575 | 750 | 325 |
| | NB-R | 575 | 725 | 50 |
| | SB-L | 375 | 50 | 250 |
| | SB-T | 700 | 325 | 700 |
| | WB-L | 1,025 | 675 | 575 |
| 7: Mathilda Avenue / US 101 SB Ramps | WB-R | 1,025 | 450 | 425 |
| | NB-T | 750 | 875 | 200 |
| | NB-R | 750 | 850 | 100 |
| | SB-T | 575 | 125 | 250 |
| | SB-TR | 575 | 175 | 400 |
| | EB-L | 1,050 | 200 | 125 |
| 8: Mathilda Avenue / Almanor Avenue-Ahwanee Avenue | EB-R | 1,050 | 50 | 25 |
| | NB-L | 375 | 600 | 150 |
| | NB-T | 675 | 3,150 | 425 |
| | NB-TR | 200 | 300 | 350 |
| | SB-L | 275 | 325 | 325 |
| | SB-T | 750 | 550 | 450 |
| | EB-L | 1,025 | 125 | 275 |
| | EB-T | 125 | 100 | 200 |
| | WB-L | 250 | 150 | 100 |
| 9: US 101 Northbound On-Ramp / Moffett Park Drive | WB-T | 1,025 | 150 | 75 |
| | WB-R | 75 | 125 | 100 |
| | EB-T | 875 | 50 | 850 |
| | EB-R | 150 | 25 | 300 |
| | WB-L | 900 | 50 | 225 |
| | WB-T | 900 | 200 | 25 |



TABLE 5-5: YEAR 2018 BUILD 2 QUEUING ANALYSIS RESULTS

| Intersection | Movement ¹ | Available Storage ² | Peak Hour | |
|--|-----------------------|--------------------------------|--|--|
| | | | AM Peak Hour 95 th Percentile Queue (ft) | PM Peak Hour 95 th Percentile Queue (ft) |
| 10: Innovation Way / Moffett Park Drive | SB-R | 525 | 75 | 50 |
| | EB-L | 850 | 125 | 1,000 |
| | WB-T | 975 | 200 | 150 |
| | WB-TR | 975 | 250 | 125 |
| 11: Innovation Way / Eleventh Avenue | NB-L | 125 | 75 | 150 |
| | NB-T | 575 | 125 | 475 |
| | SB-L | 175 | 75 | 125 |
| | SB-T | 1,000 | 100 | 75 |
| | SB-TR | 1,000 | 250 | 150 |
| | EB-L | 125 | 50 | 175 |
| | EB-LT | 300 | 50 | 375 |
| 12: Innovation Way / Juniper Driveway | EB-R | 300 | 50 | 100 |
| | NB-L | 125 | 150 | 150 |
| | NB-T | 900 | 100 | 1,225 |
| | SB-T | 300 | 225 | 225 |
| | SB-TR | 300 | 175 | 125 |
| | EB-L | 150 | 100 | 3,875 |
| 13: Bordeaux Drive / Innovation Way | EB-R | 150 | 50 | 1,800 |
| | NB-L | 325 | 525 | 2,300 |
| | NB-TR | 2,025 | 675 | 1,150 |
| | SB-L | 125 | 25 | 25 |
| | SB-TR | 725 | 175 | 775 |
| | EB-LT | 375 | 325 | 75 |
| | EB-R | 125 | 150 | 100 |
| | WB-LT | 125 | 25 | 25 |
| WB-R | 125 | 25 | 25 | |

Notes: **Bold** denotes locations where storage length is exceeded.

1. NB-northbound, SB-southbound, EB-eastbound, WB-westbound, L-left-turn movement, T-through movement, R-right-turn movement, (MP)-turn onto/from Moffett Park Drive, (237)-turn onto/from SR 237 WB Ramps.
2. Available storage lengths are provided on a "per lane" basis. For example, an available storage of 425 means each lane in the associated movement has a storage length of 425.

Source: Fehr & Peers, 2016.

MATHILDA AVENUE AND INNOVATION WAY TRAVEL TIMES

Table 5-6 presents the average travel times and delays along the Mathilda Avenue corridor under No Build and Build conditions. Both of the build alternatives would reduce the average travel time and delays on Mathilda Avenue when compared to No Build conditions with the exception of the PM peak hour under the Build 1 Alternative.



The Build 1 Alternative would result in a northbound delay reduction of approximately 6 minutes during the AM and PM peak hours. In the southbound direction, the Build 1 Alternative would reduce delays by over 0.5 minutes in the AM peak hour and increase travel times by approximately 1 minute during the PM peak hour. The slight increase in southbound travel time during the PM peak hour is mostly concentrated north of the Innovation Way intersection. The higher westbound left-turn volumes on the Innovation Way extension take up additional queue storage south of the Mathilda Avenue / Innovation Way intersection for vehicles traveling southbound on Mathilda Avenue. This reduces the number of southbound through vehicles that are able to clear the intersection in a given signal cycle. This condition does not occur under the Build 2 Alternative because the diverging diamond reduces the southbound queue spillback from the SR 237 interchange.

Build 2 Alternative would result in a northbound delay reduction of over 3.5 minutes and 5.5 minutes during the AM and PM peak hour, respectively. In the southbound direction, Build 2 Alternative would reduce delays by over 1.5 minutes and 3.5 minutes during the AM and PM peak hour, respectively.

TABLE 5-6: YEAR 2018 MATHILDA AVENUE TRAVEL TIMES

| Direction | Peak Hour | Free flow Travel Time (s) ² | No Build | | Build 1 Alternative | | Build 2 Alternative | |
|----------------------------|-----------|--|---------------------------|-----------|---------------------------|-----------|---------------------------|-----------|
| | | | Congested Travel Time (s) | Delay (s) | Congested Travel Time (s) | Delay (s) | Congested Travel Time (s) | Delay (s) |
| Mathilda Avenue Northbound | AM | 116.2 | 737.8 | 621.6 | 346.7 | 230.5 | 508.2 | 392.0 |
| | PM | 116.2 | 736.2 | 620.0 | 341.6 | 225.4 | 406.1 | 289.9 |
| Mathilda Avenue Southbound | AM | 116.2 | 432.8 | 316.6 | 399.2 | 283.0 | 318.4 | 202.2 |
| | PM | 116.2 | 1056.0 | 939.8 | 1124.3 | 1008.1 | 836.4 | 720.2 |

Notes:

1. Travel time runs begin north of the San Aleso Avenue intersection and end south of the Lockheed Martin Way-Java Drive intersection (approximately 1.44 miles).
2. Free flow speed is calculated assuming a travel speed of 45 miles per hour.

Source: Fehr & Peers, 2016.

Table 5-7 presents the average travel times and delays along the Innovation Way corridor under No Build and Build conditions. The redistribution of traffic to this corridor under the build alternatives warrants a signal at the Innovation Way and Juniper Networks Driveway in order to increase output at the Mathilda Avenue and Innovation Way intersection. Due to the implementation of a signal at Innovation Way and Juniper Networks Driveway, the average travel time and delay along Innovation Way generally decreases when compared to No Build conditions. Build 1 Alternative would result in a slight northbound delay increase of around 10 seconds and a decrease of over 3.5 minutes during the AM and PM peak hour, respectively. In the southbound direction, the Build 1 Alternative would remain unchanged in the AM peak hour and decrease delay by over 1.5 minutes during the PM peak hour.

Build 2 Alternative would result in a northbound delay increase of around 15 seconds and a decrease of over 1 minute during the AM and PM peak hour, respectively. In the southbound direction, the Build 2 Alternative would decrease delay by about 10 seconds in the AM peak hour and by about 4 minutes during PM peak hour.



TABLE 5-7: YEAR 2018 INNOVATION WAY TRAVEL TIMES

| Direction | Peak Hour | Free flow Travel Time (s) ² | No Build | | Build 1 Alternative | | Build 2 Alternative | |
|---------------------------|-----------|--|---------------------------|-----------|---------------------------|-----------|---------------------------|-----------|
| | | | Congested Travel Time (s) | Delay (s) | Congested Travel Time (s) | Delay (s) | Congested Travel Time (s) | Delay (s) |
| Innovation Way Northbound | AM | 81.5 | 86.2 | 4.7 | 97.9 | 16.4 | 101.7 | 20.2 |
| | PM | 81.5 | 524.4 | 442.9 | 290.5 | 209.0 | 443.4 | 361.9 |
| Innovation Way Southbound | AM | 81.5 | 112.7 | 31.2 | 110.5 | 29.0 | 103.8 | 22.3 |
| | PM | 81.5 | 404.9 | 323.4 | 389.2 | 207.7 | 142.1 | 60.6 |

Notes:

1. Travel time runs begin at the Mathilda Avenue intersection and end at the Moffett Park Drive intersection (approximately 0.42 miles).
2. Free flow speed is calculated assuming a travel speed of 25 miles per hour.

Source: Fehr & Peers, 2016.

YEAR 2018 MAINLINE OPERATIONS

This section summarizes the mainline operations analysis for Year 2018 under No Build, Build 1 and Build 2 conditions using the calibrated/validated FREQ models developed under Existing Conditions. There are several projects identified in the Santa Clara Valley Transportation Plan (VTP) 2040 that could influence traffic operations on US 101 and SR 237 under Year 2018 Conditions. Below is a brief summary of the projects and how they were considered in the evaluation of the US 101 and SR 237 operations analysis under Year 2018 Conditions.

- *SR 237 Eastbound Auxiliary Lanes – Mathilda Avenue to Fair Oaks Avenue:* The SR 237 eastbound auxiliary lane between Mathilda Avenue and Fair Oaks Avenue is expected to be constructed by Year 2018.
- *SR 237 Express Lanes – North First Street to Mathilda Avenue:* The existing HOV lanes along SR 237 in both directions are expected to be converted to HOT lanes by the Year 2018. (The extended HOT lanes beyond Mathilda Avenue are not estimated to be completed by Year 2018, but are considered under Year 2040.)
- *US 101 Express Lanes – Whipple Avenue in San Mateo County to Cochrane Road in Morgan Hill (one lane in each direction):* The existing HOV lanes along US 101 in both directions are expected to be converted to HOT lanes by the Year 2018. (The addition of a second HOT lane in both directions is not estimated to be completed by Year 2018, but is considered under Year 2040.)
- *All freeway ramps metered on US 101 and SR 237 (includes widening of SR 237 EB on-ramp at Mathilda Avenue to two lanes):* Ramp metering is assumed to be installed and operating at all US 101 and SR 237 on-ramps by Year 2018. As part of this project, the Mathilda Avenue to SR 237 eastbound on-ramp is assumed to extend the existing two-lane ramp and meter two mixed-flow lanes. The specific design of the SR 237 eastbound on-ramp will be evaluated and finalized during the construction phase of the ramp metering system.



As discussed above, congestion on the local street system would constrain on-ramp demand volumes at the Mathilda Avenue interchanges during the peak hours. **Table 5-8** and **Table 5-9** presents the initial and constrained on-ramp volumes at the Mathilda Avenue/US 101 and Mathilda Avenue/SR 237 interchanges under the various alternatives. The initial demand volumes were replaced by the constrained volumes to determine US 101 and SR 237 traffic operations.

TABLE 5-8: YEAR 2018 AM ON-RAMP CONSTRAINED VOLUMES

| Alternative | Location from Mathilda | Initial FREQ Demand Volume | | Constrained Volume from SimTraffic (8AM-9AM) | Constrained FREQ Volume | |
|-------------|-------------------------|----------------------------|---------|--|-------------------------|---------|
| | | 7AM-8AM | 8AM-9AM | | 7AM-8AM | 8AM-9AM |
| No Build | SR 237 WB On | 210 | 250 | 194 | 160 | 194 |
| | SR 237 EB On | 510 | 810 | 575 | 360 | 575 |
| | US 101 NB On | 350 | 360 | 261 | 250 | 261 |
| | US 101 SB On (loop) | 120 | 140 | 126 | 110 | 126 |
| | US 101 SB On (diagonal) | 380 | 580 | 433 | 280 | 433 |
| Build 1 | SR 237 WB On | 210 | 240 | 240 | 210 | 240 |
| | SR 237 EB On | 510 | 810 | 798 | 500 | 798 |
| | US 101 NB On | 350 | 370 | 364 | 340 | 364 |
| | US 101 SB On (loop) | 120 | 140 | 133 | 110 | 133 |
| | US 101 SB On (diagonal) | 380 | 580 | 567 | 370 | 567 |
| Build 2 | SR 237 WB On | 210 | 240 | 225 | 200 | 225 |
| | SR 237 EB On | 510 | 810 | 744 | 470 | 744 |
| | US 101 NB On | 350 | 370 | 335 | 320 | 335 |
| | US 101 SB On (loop) | 120 | 140 | 124 | 110 | 124 |
| | US 101 SB On (diagonal) | 380 | 580 | 545 | 360 | 545 |

Source: Fehr & Peers, 2016.



TABLE 5-9: YEAR 2018 PM ON-RAMP CONSTRAINED VOLUMES

| Alternative | Location from Mathilda | Initial FREQ Demand Volume | | | Constrained Volume from SimTraffic (5PM-6PM) | Constrained FREQ Volume | | |
|-------------|-------------------------|----------------------------|---------|---------|--|-------------------------|---------|---------|
| | | 4PM-5PM | 5PM-6PM | 6PM-7PM | | 4PM-5PM | 5PM-6PM | 6PM-7PM |
| No Build | SR 237 WB On | 720 | 750 | 580 | 573 | 550 | 573 | 440 |
| | SR 237 EB On | 970 | 1030 | 860 | 886 | 830 | 886 | 740 |
| | US 101 NB On | 300 | 270 | 250 | 211 | 230 | 211 | 200 |
| | US 101 SB On (loop) | 1080 | 1140 | 910 | 982 | 930 | 982 | 780 |
| | US 101 SB On (diagonal) | 480 | 530 | 480 | 443 | 400 | 443 | 400 |
| Build 1 | SR 237 WB On | 680 | 710 | 550 | 560 | 540 | 560 | 430 |
| | SR 237 EB On | 970 | 1030 | 860 | 963 | 910 | 963 | 800 |
| | US 101 NB On | 340 | 310 | 280 | 307 | 340 | 307 | 280 |
| | US 101 SB On (loop) | 1080 | 1140 | 910 | 926 | 880 | 926 | 740 |
| | US 101 SB On (diagonal) | 480 | 530 | 480 | 530 | 480 | 530 | 480 |
| Build 2 | SR 237 WB On | 680 | 710 | 550 | 591 | 570 | 591 | 460 |
| | SR 237 EB On | 970 | 1030 | 860 | 970 | 910 | 970 | 810 |
| | US 101 NB On | 340 | 310 | 280 | 303 | 330 | 303 | 270 |
| | US 101 SB On (loop) | 1080 | 1140 | 910 | 956 | 910 | 956 | 760 |
| | US 101 SB On (diagonal) | 480 | 530 | 480 | 530 | 480 | 530 | 480 |

Source: Fehr & Peers, 2016.

PEAK HOUR LEVEL OF SERVICE

Table 5-10 and **Table 5-11** summarize the Year 2018 US 101 AM and PM peak hour density and LOS results, respectively, based on the FREQ model outputs. **Table 5-12** and **Table 5-13** summarize the Year 2018 SR 237 AM and PM peak hour density and LOS results, respectively, based on the FREQ model outputs. Locations in bold indicate LOS F operations. Results for the mixed-flow lanes are presented without parentheses while results for the high-occupancy toll (HOT) lanes are shown in parentheses. Detailed mainline analysis worksheets are presented in **Appendix M**. A more detailed discussion on peak hour level of service is presented after the analysis results tables.



TABLE 5-10: YEAR 2018 US 101 AM PEAK HOUR LEVEL OF SERVICE BASED ON FREQ MODEL RESULTS

| Segment | Type ¹ | # of Lanes | No Build | | Build Alternative 1 | | Build Alternative 2 | |
|--|-------------------|--------------------|-----------------------|-----------------|-----------------------|-----------------|-----------------------|-----------------|
| | | | Density ² | LOS | Density ² | LOS | Density ² | LOS |
| US 101 Northbound³ | | | | | | | | |
| Fair Oaks Off-Ramp | Diverge | 3 Mixed (1 HOT) | 74.0 (29.7) | F (D) | 73.7 (29.7) | F (D) | 73.6 (29.7) | F (D) |
| Fair Oaks Off-Ramp to Fair Oaks On-Ramp | Basic | 3 Mixed (1 HOT) | 67.9 (22.0) | F (C) | 67.5 (22.0) | F (C) | 67.4 (22.0) | F (C) |
| Fair Oaks On-Ramp | Merge | 3 Mixed (1 HOT) | 51.6 (26.4) | F (D) | 51.9 (26.4) | F (D) | 51.8 (26.4) | F (D) |
| Fair Oaks On-Ramp to Mathilda NB Off Ramp | Basic | 3 Mixed (1 HOT) | 54.3 (26.4) | F (D) | 54.7 (26.4) | F (D) | 54.5 (26.4) | F (D) |
| Mathilda NB Off-Ramp | Diverge | 3 Mixed (1 HOT) | 54.9 (26.4) | F (D) | 55.8 (26.4) | F (D) | 55.6 (26.4) | F (D) |
| Mathilda NB Off-Ramp to Mathilda NB On-Ramp | Basic | 3 Mixed (1 HOT) | 59.9 (21.8) | F (C) | 65.6 (20.1) | F (C) | 65.3 (20.1) | F (C) |
| Mathilda NB On-Ramp | Merge | 3 Mixed (1 HOT) | 59.9 (24.1) | F (C) | 65.6 (20.9) | F (C) | 65.4 (20.9) | F (C) |
| Mathilda NB On-Ramp to Mathilda SB Off-Ramp ⁵ | Basic | 3 Mixed (1 HOT) | 60.7 (24.1) | F (C) | 66.8 (20.9) | F (C) | 66.5 (20.9) | F (C) |
| Mathilda SB Off-Ramp ⁶ | Diverge | 3 Mixed (1 HOT) | 59.5 (24.1) | F (C) | N/A | N/A | N/A | N/A |
| Mathilda SB Off-Ramp to SR 237 WB Off-Ramp ⁶ | Basic | 3 Mixed (1 HOT) | 65.0 (20.7) | F (C) | N/A | N/A | N/A | N/A |
| SR 237 WB Off-Ramp | Diverge | 3 Mixed (1 HOT) | 66.5 (20.7) | F (C) | 70.0 (20.9) | F (C) | 69.8 (20.9) | F (C) |
| SR 237 WB Off-Ramp to SR 237 WB On-Ramp | Basic | 3 Mixed (1 HOT) | 81.1 (18.1) | F (C) | 85.1 (18.4) | F (C) | 84.9 (18.3) | F (C) |
| SR 237 WB On-Ramp | Merge | 3 Mixed (1 HOT) | 68.4 (22.0) | F (C) | 70.7 (24.2) | F (C) | 70.5 (24.1) | F (C) |
| SR 237 WB On-Ramp to Ellis | Basic | 3 Mixed (1 HOT) | 75.8 (22.0) | F (C) | 78.4 (24.2) | F (C) | 78.2 (24.1) | F (C) |



TABLE 5-10: YEAR 2018 US 101 AM PEAK HOUR LEVEL OF SERVICE BASED ON FREQ MODEL RESULTS

| Segment | Type ¹ | # of Lanes | No Build | | Build Alternative 1 | | Build Alternative 2 | |
|---|-------------------|---------------------------|----------------------|----------|----------------------|----------|----------------------|----------|
| | | | Density ² | LOS | Density ² | LOS | Density ² | LOS |
| US 101 Southbound⁴ | | | | | | | | |
| Ellis On-Ramp to SR 237 EB Off-Ramp | Weave | 3 Mixed, 1 AUX (1 HOT) | 18.8 (15.2) | C (B) | 18.8 (15.2) | C (B) | 18.8 (15.2) | C (B) |
| SR 237 EB Off-Ramp | Diverge | 3 Mixed, 1 AUX (1 HOT) | 18.8 (15.2) | C (B) | 18.8 (15.2) | C (B) | 18.8 (15.2) | C (B) |
| SR 237 EB Off-Ramp to SR 237 EB On-Ramp | Basic | 3 Mixed (1 HOT) | 17.9 (11.0) | B (A) | 18.8 (11.5) | C (B) | 18.8 (11.5) | C (B) |
| SR 237 EB On-Ramp | Merge | 3 Mixed, 1 AUX (1 HOT) | 16.4 (13) | B (B) | 17.1 (13.4) | B (B) | 17.1 (13.4) | B (B) |
| SR 237 EB On-Ramp to Mathilda Off-Ramp | Weave | 3 Mixed, 1 AUX (1 HOT) | 16.4 (13.0) | B (B) | 17.1 (13.4) | B (B) | 17.1 (13.4) | B (B) |
| Mathilda Off-Ramp | Diverge | 3 Mixed, 1 AUX (1 HOT) | 16.4 (13.0) | B (B) | 17.1 (13.4) | B (B) | 17.1 (13.4) | B (B) |
| Mathilda Off-Ramp to Mathilda SB On-Ramp | Basic | 3 Mixed (1 HOT) | 20.5 (12.3) | C (B) | 20.5 (12.3) | C (B) | 20.4 (12.3) | C (B) |
| Mathilda SB On-Ramp | Merge | 3 Mixed (1 HOT) | 20.9 (12.6) | C (B) | 20.9 (12.6) | C (B) | 20.9 (12.6) | C (B) |
| Mathilda NB On-Ramp | Merge | 3 Mixed (1 HOT) | 22.1 (13.3) | C (B) | 22.8 (13.5) | C (B) | 22.7 (13.5) | C (B) |
| Mathilda NB On-Ramp to Fair Oaks SB Off-Ramp | Basic | 3 Mixed (1 HOT) | 22.1 (13.3) | C (B) | 22.7 (13.5) | C (B) | 22.7 (13.5) | C (B) |
| Fair Oaks SB Off-Ramp | Diverge | 3 Mixed (1 HOT) | 22.1 (13.3) | C (B) | 22.7 (13.5) | C (B) | 22.7 (13.5) | C (B) |
| Fair Oaks SB Off-Ramp to Fair Oaks SB On-Ramp | Basic | 3 Mixed (1 HOT) | 20.8 (12.7) | C (B) | 21.1 (12.9) | C (B) | 21.1 (12.9) | C (B) |
| Fair Oaks SB On-Ramp | Merge | 3 Mixed, 1 AUX (1 HOT) | 16.2 (13.2) | B (B) | 16.5 (13.4) | B (B) | 16.4 (13.4) | B (B) |
| Fair Oaks NB Off-Ramp | Diverge | 3 Mixed, 1 AUX (1 HOT) | 16.2 (13.2) | B (B) | 16.5 (13.4) | B (B) | 16.4 (13.4) | B (B) |



TABLE 5-10: YEAR 2018 US 101 AM PEAK HOUR LEVEL OF SERVICE BASED ON FREQ MODEL RESULTS

| Segment | Type ¹ | # of Lanes | No Build | | Build Alternative 1 | | Build Alternative 2 | |
|---|-------------------|--------------------|----------------------|----------|----------------------|----------|----------------------|----------|
| | | | Density ² | LOS | Density ² | LOS | Density ² | LOS |
| Fair Oaks NB Off-Ramp to Fair Oaks NB On-Ramp | Basic | 3 Mixed (1 HOT) | 21.2 (13.0) | C (B) | 21.6 (13.3) | C (B) | 21.5 (13.2) | C (B) |
| Fair Oaks NB On-Ramp | Merge | 3 Mixed (1 HOT) | 23.8 (14.4) | C (B) | 24.3 (14.6) | C (B) | 24.2 (14.6) | C (B) |

Note: **Bold** font indicates LOS F conditions.

Locations marked with an asterisk () designate the end of bottleneck congestion. A segment may be designated LOS F even if the density is below the LOS F threshold if any portion of the segment is in queue.

1. Merge, diverge, and weave segments were not calculated differently from basic segments. All results are based on the density produced from FREQ. Weaving segments are further evaluated in the Mainline Weaving Analysis section of this report.
2. Density and LOS results shown as: mixed-flow lanes (HOT lane).
3. The AM peak hour for US 101 Northbound occurs between 7:00am and 8:00am.
4. The AM peak hour for US 101 Southbound occurs between 5:00pm and 6:00pm.
5. Due to the closure of the US 101 northbound loop off-ramp to southbound Mathilda Avenue, this freeway segment is assumed to extend from the Mathilda Avenue loop on-ramp to SR 237 westbound off-ramp.
6. These segments do not exist under both Build Alternatives due to the closure of the US 101 northbound loop off-ramp to southbound Mathilda Avenue.

Source: Fehr & Peers, 2016.



TABLE 5-11: YEAR 2018 US 101 PM PEAK HOUR LEVEL OF SERVICE BASED ON FREQ MODEL RESULTS

| Segment | Type ¹ | # of Lanes | No Build | | Build 1 Alternative | | Build 2 Alternative | |
|--|-------------------|--------------------|-----------------------|-----------------|-----------------------|-----------------|-----------------------|-----------------|
| | | | Density ² | LOS | Density ² | LOS | Density ² | LOS |
| US 101 Northbound³ | | | | | | | | |
| Fair Oaks Off-Ramp | Diverge | 3 Mixed (1 HOT) | 26.2 (11.6) | D (B) | 26.2 (11.6) | D (B) | 26.2 (11.6) | D (B) |
| Fair Oaks Off-Ramp to Fair Oaks On-Ramp | Basic | 3 Mixed (1 HOT) | 21.8 (9.8) | C (A) | 21.8 (9.8) | C (A) | 21.8 (9.8) | C (A) |
| Fair Oaks On-Ramp | Merge | 3 Mixed (1 HOT) | 24.2 (10.3) | C (A) | 24.2 (10.3) | C (A) | 24.2 (10.3) | C (A) |
| Fair Oaks On-Ramp to Mathilda NB Off Ramp | Basic | 3 Mixed (1 HOT) | 24.2 (10.3) | C (A) | 24.2 (10.3) | C (A) | 24.2 (10.3) | C (A) |
| Mathilda NB Off-Ramp | Diverge | 3 Mixed (1 HOT) | 17.8 (10.3) | B (A) | 17.8 (10.3) | B (A) | 17.8 (10.3) | B (A) |
| Mathilda NB Off-Ramp to Mathilda NB On-Ramp | Basic | 3 Mixed (1 HOT) | 23.0 (9.9) | C (A) | 19.2 (8.4) | C (A) | 19.2 (8.4) | C (A) |
| Mathilda NB On-Ramp | Merge | 3 Mixed (1 HOT) | 24.2 (10.1) | C (A) | 20.4 (8.8) | C (A) | 20.4 (8.8) | C (A) |
| Mathilda NB On-Ramp to Mathilda SB Off-Ramp ⁵ | Basic | 3 Mixed (1 HOT) | 24.2 (10.1) | C (A) | 20.4 (8.8) | C (A) | 20.4 (8.8) | C (A) |
| Mathilda SB Off-Ramp ⁶ | Diverge | 3 Mixed (1 HOT) | 24.3 (10.1) | C (A) | N/A | N/A | N/A | N/A |
| Mathilda SB Off-Ramp to SR 237 WB Off-Ramp ⁶ | Basic | 3 Mixed (1 HOT) | 20.1 (8.7) | C (A) | N/A | N/A | N/A | N/A |
| SR 237 WB Off-Ramp | Diverge | 3 Mixed (1 HOT) | 18.9* (8.7) | F (A) | 37.8* (8.8) | F (A) | 37.1* (8.8) | F (A) |
| SR 237 WB Off-Ramp to SR 237 WB On-Ramp | Basic | 3 Mixed (1 HOT) | 38.1* (7.0) | F (A) | 64.8 (7.2) | F (A) | 63.9 (7.2) | F (A) |
| SR 237 WB On-Ramp | Merge | 3 Mixed (1 HOT) | 53.8 (10.4) | F (A) | 73.1 (10.5) | F (A) | 72.4 (10.5) | F (A) |
| SR 237 WB On-Ramp to Ellis | Basic | 3 Mixed (1 HOT) | 72.2 (10.4) | F (A) | 92.3 (10.5) | F (A) | 91.5 (10.5) | F (A) |



TABLE 5-11: YEAR 2018 US 101 PM PEAK HOUR LEVEL OF SERVICE BASED ON FREQ MODEL RESULTS

| Segment | Type ¹ | # of Lanes | No Build | | Build 1 Alternative | | Build 2 Alternative | |
|---|-------------------|---------------------------|------------------------|-----------------|------------------------|-----------------|------------------------|-----------------|
| | | | Density ² | LOS | Density ² | LOS | Density ² | LOS |
| US 101 Southbound⁴ | | | | | | | | |
| Ellis On-Ramp to SR 237 EB Off-Ramp | Weave | 3 Mixed, 1 AUX (1 HOT) | 84.5 (24.7) | F (C) | 88.0 (24.7) | F (C) | 89.1 (24.7) | F (C) |
| SR 237 EB Off-Ramp | Diverge | 3 Mixed, 1 AUX (1 HOT) | 71.7 (24.7) | F (C) | 75.9 (24.7) | F (C) | 77.0 (24.7) | F (C) |
| SR 237 EB Off-Ramp to SR 237 EB On-Ramp | Basic | 3 Mixed (1 HOT) | 145.2 (18.0) | F (B) | 146.6 (18.3) | F (C) | 148.1 (18.3) | F (C) |
| SR 237 EB On-Ramp | Merge | 3 Mixed, 1 AUX (1 HOT) | 111.5 (19.5) | F (C) | 114.4 (19.9) | F (C) | 115.5 (19.9) | F (C) |
| SR 237 EB On-Ramp to Mathilda Off-Ramp | Weave | 3 Mixed, 1 AUX (1 HOT) | 115.6 (19.5) | F (C) | 118.9 (19.9) | F (C) | 120.0 (19.9) | F (C) |
| Mathilda Off-Ramp | Diverge | 3 Mixed, 1 AUX (1 HOT) | 111.6 (19.5) | F (C) | 114.3 (19.9) | F (C) | 115.4 (19.9) | F (C) |
| Mathilda Off-Ramp to Mathilda SB On-Ramp | Basic | 3 Mixed (1 HOT) | 143.0 (18.0) | F (C) | 145.7 (18.2) | F (C) | 147.1 (18.2) | F (C) |
| Mathilda SB On-Ramp | Merge | 3 Mixed (1 HOT) | 97.9 (20.7) | F (C) | 103.2 (20.7) | F (C) | 103.2 (20.8) | F (C) |
| Mathilda NB On-Ramp | Merge | 3 Mixed (1 HOT) | 87.9 (21.9) | F (C) | 88.0 (22.1) | F (C) | 88.4 (22.2) | F (C) |
| Mathilda NB On-Ramp to Fair Oaks SB Off-Ramp | Basic | 3 Mixed (1 HOT) | 92.2 (21.9) | F (C) | 93.3 (22.1) | F (C) | 93.7 (22.2) | F (C) |
| Fair Oaks SB Off-Ramp | Diverge | 3 Mixed (1 HOT) | 86.5 (21.9) | F (C) | 87.6 (22.1) | F (C) | 88.1 (22.2) | F (C) |
| Fair Oaks SB Off-Ramp to Fair Oaks SB On-Ramp | Basic | 3 Mixed (1 HOT) | 119.0 (20.3) | F (C) | 119.8 (20.6) | F (C) | 120.1 (20.7) | F (C) |
| Fair Oaks SB On-Ramp | Merge | 3 Mixed, 1 AUX (1 HOT) | 88.7 (21.2) | F (C) | 89.4 (21.5) | F (C) | 89.6 (21.6) | F (C) |
| Fair Oaks NB Off-Ramp | Diverge | 3 Mixed, 1 AUX (1 HOT) | 89.8 (21.2) | F (C) | 90.5 (21.5) | F (C) | 90.7 (21.6) | F (C) |



TABLE 5-11: YEAR 2018 US 101 PM PEAK HOUR LEVEL OF SERVICE BASED ON FREQ MODEL RESULTS

| Segment | Type ¹ | # of Lanes | No Build | | Build 1 Alternative | | Build 2 Alternative | |
|---|-------------------|--------------------|------------------------|-----------------|------------------------|-----------------|------------------------|-----------------|
| | | | Density ² | LOS | Density ² | LOS | Density ² | LOS |
| Fair Oaks NB Off-Ramp to Fair Oaks NB On-Ramp | Basic | 3 Mixed (1 HOT) | 116.9 (20.7) | F (C) | 117.6 (21.0) | F (C) | 118.0 (21.1) | F (C) |
| Fair Oaks NB On-Ramp | Merge | 3 Mixed (1 HOT) | 107.2 (21.4) | F (C) | 107.9 (21.6) | F (C) | 108.2 (21.7) | F (C) |

Note: **Bold** font indicates LOS F conditions.

Locations marked with an asterisk () designate the end of bottleneck congestion. A segment may be designated LOS F even if the density is below the LOS F threshold if any portion of the segment is in queue.

1. Merge, diverge, and weave segments were not calculated differently from basic segments. All results are based on the density produced from FREQ. Weaving segments are further evaluated in the Mainline Weaving Analysis section of this report.
2. Density and LOS results shown as: mixed-flow lanes (HOT lane).
3. The AM peak hour for US 101 Northbound occurs between 7:00am and 8:00am.
4. The AM peak hour for US 101 Southbound occurs between 5:00pm and 6:00pm.
5. Due to the closure of the US 101 northbound loop off-ramp to southbound Mathilda Avenue, this freeway segment is assumed to extend from the Mathilda Avenue loop on-ramp to SR 237 westbound off-ramp.
6. These segments do not exist under both Build Alternatives due to the closure of the US 101 northbound loop off-ramp to southbound Mathilda Avenue.

Source: Fehr & Peers, 2016.



TABLE 5-12: YEAR 2018 SR 237 AM PEAK HOUR LEVEL OF SERVICE BASED ON FREQ MODEL RESULTS

| Segment | Type ¹ | # of Lanes | No Build | | Build 1 Alternative | | Build 2 Alternative | |
|---|-------------------|--------------------|-----------------------|-----------------|-----------------------|-----------------|-----------------------|-----------------|
| | | | Density ² | LOS | Density ² | LOS | Density ² | LOS |
| SR 237 Westbound³ | | | | | | | | |
| Lawrence On-Ramp to Crossman On-Ramp | Basic | 2 Mixed (1 HOT) | 41.7 (19.3) | D (C) | 54.6 (19.3) | D (C) | 52.6 (19.3) | D (C) |
| Crossman On-Ramp | Merge | 2 Mixed (1 HOT) | 55.2 (19.3) | D (C) | 62.5 (19.3) | F (C) | 61.2 (19.3) | F (C) |
| Crossman On-Ramp to Mathilda Off-Ramp | Basic | 2 Mixed (1 HOT) | 65.0 (19.3) | F (C) | 71.2 (19.3) | F (C) | 70.2 (19.3) | F (C) |
| Mathilda Off-Ramp | Diverge | 3 Mixed | 57.1 | F | 60.8 | F | 60.2 | F |
| Mathilda Off-Ramp to Mathilda On-Ramp | Basic | 2 Mixed | 69.7 | F | 73.4 | F | 72.6 | F |
| Mathilda On-Ramp to US 101 NB Off-Ramp | Weave | 2 Mixed/1 AUX | 56.0 | F | 56.4 | F | 56.4 | F |
| US 101 NB Off-Ramp to US 101 NB On-Ramp | Basic | 2 Mixed | 18.5 | C | 18.5 | C | 18.5 | C |
| US 101 NB On-Ramp | Merge | 2 Mixed | 23.5 | C | 23.4 | C | 23.4 | C |
| Maude Off-Ramp | Diverge | 2 Mixed | 23.5 | C | 23.4 | C | 23.4 | C |
| SR 237 Eastbound⁴ | | | | | | | | |
| Maude On-Ramp to US 101 SB Off-Ramp | Weave | 2 Mixed/1 AUX | 22.0 | C | 22.0 | C | 22.0 | C |
| US 101 SB Off-Ramp to US 101 SB On-Ramp | Basic | 2 Mixed | 22.7 | C | 22.8 | C | 22.7 | C |
| US 101 SB On-Ramp | Merge | 2 Mixed/1 AUX | 28.9 | D | 23.9 | C | 23.9 | C |
| US 101 SB On-Ramp to Mathilda Off-Ramp | Basic | 2 Mixed/1 AUX | 28.9 | D | 23.9 | C | 23.9 | C |
| Mathilda Off-Ramp | Diverge | 2 Mixed/1 AUX | 28.9 | D | 23.9 | C | 23.9 | C |
| Mathilda Off-Ramp to Mathilda On-Ramp | Basic | 2 Mixed | 34.5 | D | 34.5 | D | 34.5 | D |



TABLE 5-12: YEAR 2018 SR 237 AM PEAK HOUR LEVEL OF SERVICE BASED ON FREQ MODEL RESULTS

| Segment | Type ¹ | # of Lanes | No Build | | Build 1 Alternative | | Build 2 Alternative | |
|--------------------------------------|-------------------|--------------------|----------------------|----------|----------------------|----------|----------------------|----------|
| | | | Density ² | LOS | Density ² | LOS | Density ² | LOS |
| Mathilda On-Ramp | Merge | 2 Mixed | 23.5 | C | 24.7 | C | 24.4 | C |
| Mathilda On-Ramp to Persian Off-Ramp | Basic | 2 Mixed (1 HOT) | 18.4 (15.5) | C (B) | 19.3 (16.4) | C (B) | 19.0 (16.1) | C (B) |
| Persian Off-Ramp to Lawrence | Basic | 2 Mixed (1 HOT) | 25.7 (15.5) | C (B) | 27.4 (16.4) | D (B) | 27.0 (16.1) | C (B) |

Note: **Bold** font indicates LOS F conditions.

Locations marked with an asterisk () designate the end of bottleneck congestion. A segment may be designated LOS F even if the density is below the LOS F threshold if any portion of the segment is in queue.

* Results are preliminary and subject to change pending FREQ model evaluation

1. Merge, diverge, and weave segments were not calculated differently from basic segments. All results are based on the density produced from FREQ. Weaving segments are further evaluated in the Mainline Weaving Analysis section of this report.
2. Density and LOS results shown as: mixed-flow lanes (HOT lane).
3. The AM peak hour for SR 237* Westbound occurs between 7:00am and 8:00am.
4. The AM peak hour for SR 237 Eastbound occurs between 8:00am and 9:00am.

Source: Fehr & Peers, 2016.



TABLE 5-13: YEAR 2018 SR 237 PM PEAK HOUR LEVEL OF SERVICE BASED ON FREQ MODEL RESULTS

| Segment | Type ¹ | # of Lanes | No Build | | Build 1 Alternative | | Build 2 Alternative | |
|---|-------------------|--------------------|----------------------|----------|----------------------|----------|----------------------|----------|
| | | | Density ² | LOS | Density ² | LOS | Density ² | LOS |
| SR 237 Westbound³ | | | | | | | | |
| Lawrence On-Ramp to Crossman On-Ramp | Basic | 2 Mixed (1 HOT) | 29.5 (10) | D (A) | 30.4 (10) | D (A) | 30.6 (10) | D (A) |
| Crossman On-Ramp | Merge | 2 Mixed (1 HOT) | 45.5 (10) | E (A) | 46.2 (10) | E (A) | 46.5 (10) | E (A) |
| Crossman On-Ramp to Mathilda Off-Ramp | Basic | 2 Mixed (1 HOT) | 50.9 (10) | E (A) | 51.5 (10) | E (A) | 51.7 (10) | E (A) |
| Mathilda Off-Ramp | Diverge | 3 Mixed | 47.4 | D | 48.1 | D | 48.2 | D |
| Mathilda Off-Ramp to Mathilda On-Ramp | Basic | 2 Mixed | 72.7 | F | 73.2 | F | 73.6 | F |
| Mathilda On-Ramp to US 101 NB Off-Ramp | Weave | 2 Mixed/1 AUX | 73.0 | F | 73.5 | F | 72.7 | F |
| US 101 NB Off-Ramp to US 101 NB On-Ramp | Basic | 2 Mixed | 19.2 | C | 19.4 | C | 19.6 | C |
| US 101 NB On-Ramp | Merge | 2 Mixed | 25.9 | C | 26.1 | D | 26.4 | D |
| Maude Off-Ramp | Diverge | 2 Mixed | 25.9 | C | 26.1 | D | 26.4 | D |
| SR 237 Eastbound⁴ | | | | | | | | |
| Maude On-Ramp to US 101 SB Off-Ramp | Weave | 2 Mixed, 1 AUX | 81.9 | F | 36.8* | F | 38.3* | F |
| US 101 SB Off-Ramp to US 101 SB On-Ramp | Basic | 2 Mixed | 129.6 | F | 88.4 | F | 89.9 | F |
| US 101 SB On-Ramp | Merge | 2 Mixed, 1 AUX | 75.4 | F | 61.0 | F | 61.4 | F |
| US 101 SB On-Ramp to Mathilda Off-Ramp | Weave | 2 Mixed, 1 AUX | 79.3 | F | 68.7 | F | 69.1 | F |
| Mathilda Off-Ramp | Diverge | 2 Mixed, 1 AUX | 83.3 | F | 76.5 | F | 76.8 | F |
| Mathilda Off-Ramp to Mathilda On-Ramp | Basic | 2 Mixed | 129.4 | F | 109.0 | F | 109.3 | F |



TABLE 5-13: YEAR 2018 SR 237 PM PEAK HOUR LEVEL OF SERVICE BASED ON FREQ MODEL RESULTS

| Segment | Type ¹ | # of Lanes | No Build | | Build 1 Alternative | | Build 2 Alternative | |
|--------------------------------------|-------------------|--------------------|------------------------|-----------------|------------------------|-----------------|------------------------|-----------------|
| | | | Density ² | LOS | Density ² | LOS | Density ² | LOS |
| Mathilda On-Ramp | Merge | 2 Mixed | 105.4 | F | 88.8 | F | 89.0 | F |
| Mathilda On-Ramp to Persian Off-Ramp | Diverge | 2 Mixed (1 HOT) | 102.2 (13.1) | F (B) | 81.5 (11.3) | F (B) | 81.7 (11.3) | F (B) |
| Persian Off-Ramp to Lawrence | Basic | 2 Mixed (1 HOT) | 147.5 (13.1) | F (B) | 116.3 (11.3) | F (B) | 116.5 (11.3) | F (B) |

Note: **Bold** font indicates LOS F conditions.

Locations marked with an asterisk () designate the end of bottleneck congestion. A segment may be designated LOS F even if the density is below the LOS F threshold if any portion of the segment is in queue.

1. Merge, diverge, and weave segments were not calculated differently from basic segments. All results are based on the density produced from FREQ. Weaving segments are further evaluated in the Mainline Weaving Analysis section of this report.
2. Density and LOS results shown as: mixed-flow lanes (HOT lane).
3. The PM peak hour for SR 237 Westbound occurs between 5:00pm and 6:00pm.
4. The PM peak hour for SR 237 Eastbound occurs between 5:00pm and 6:00pm.

Source: Fehr & Peers, 2016.



US 101 Northbound

AM Peak Hour

Under No Build conditions, a bottleneck would develop north of the study area at the SR 85 and Shoreline Boulevard ramps. The bottleneck results in upstream queuing that extends beyond the extents of the study segments. The study segments in queue would operate at LOS F. The northbound HOT lane is anticipated to operate at LOS C/D during the AM peak hour.

New bottlenecks are not anticipated to develop under the Build Alternatives. The general purpose lanes are anticipated to operate at the same level of service as No Build (LOS F) under both Build Alternatives. The northbound HOT lane is anticipated to operate at LOS C/D during the AM peak hour under the Build Alternatives.

PM Peak Hour

During the PM peak hour, a bottleneck would develop north of the study area at the SR 85 and Shoreline Boulevard ramps. This bottleneck exists for No Build and Build conditions. The bottleneck results in upstream queuing that extends to the SR 237 WB off-ramp. The general purpose lanes upstream of this bottleneck generally operate at LOS C/D under No Build conditions. The northbound HOT lane is anticipated to operate at LOS A/B during the PM peak hour.

Additional bottlenecks are not anticipated to develop under the Build Alternatives. The general purpose lanes upstream of this bottleneck are anticipated to operate at the same level of service as No Build (LOS C/D) under both Build Alternatives. The northbound HOT lane is anticipated to operate at LOS A/B during the PM peak hour under the Build Alternatives.

US 101 Southbound

AM Peak Hour

During the AM peak hour, there are no bottlenecks estimated to develop within the study area or spill back into the study area on US 101 southbound. The general purpose lanes operate at LOS B/C throughout the network under No Build conditions. The southbound HOT lane is anticipated to operate at LOS A/B during the AM peak hour.

New bottlenecks are not anticipated to develop under the Build Alternatives. The general purpose lanes are anticipated to operate at the same level of service as No Build (LOS C/D) under both Build Alternatives. The southbound HOT lane is anticipated to operate at LOS B during the AM peak hour under the Build Alternatives. The density on the general purpose lanes increases slightly between the SR 237 on-ramp and the Mathilda Avenue off-ramp due to the shift in traffic from SR 237 eastbound that now remains on US 101 southbound and exits at Mathilda Avenue. This shift in traffic does not adversely affect the results of the freeway density and LOS results.



PM Peak Hour

Under No Build conditions, a bottleneck would develop south of the study area at the De La Cruz Boulevard and SR 87 ramps. The bottleneck results in upstream queuing that extends beyond the extents of the study segments. The study segments in queue would operate at LOS F. The southbound HOT lane is anticipated to operate at LOS C during the PM peak hour.

New bottlenecks are not anticipated to develop under the Build Alternatives. The general purpose lanes are anticipated to operate at the same level of service as No Build (LOS F) under both Build Alternatives. The southbound HOT lane is anticipated to operate at LOS C during the PM peak hour under the Build Alternatives. The density on the general purpose lanes increases slightly between the SR 237 on-ramp and the Mathilda Avenue off-ramp due to the shift in traffic from SR 237 eastbound that now remains on US 101 southbound and exits at Mathilda Avenue. This shift in traffic does not adversely affect the results of the freeway density and LOS results.

SR 237 Westbound

AM Peak Hour

Under No Build conditions, a bottleneck would develop at the US 101 northbound off-ramp and spill back to east of the Mathilda Avenue off-ramp. The study segments in queue would operate at LOS F and are anticipated to operate at LOS C downstream of the US 101 Northbound off-ramp. The westbound HOT lane, which begins prior to the start of the study network and ends between the Mathilda Avenue and Fair Oaks Avenue ramps, is anticipated to operate at LOS C.

Additional bottlenecks are not anticipated to develop under the Build Alternatives. However, the No Build bottleneck that extends from US 101 northbound off-ramp to east of the Mathilda Avenue off-ramp is anticipated to extend slightly further to the Fair Oaks Avenue on-ramp under the Build Alternatives. Due to the local street improvements, more vehicles are able to access the on-ramp at Mathilda Avenue, therefore adding additional vehicles to the on-ramp. The general purpose lanes west of the bottleneck are anticipated to operate at the same level of service as No Build (LOS C) under both Build Alternatives. The westbound HOT lane is anticipated to operate at LOS C during the AM peak hour under the Build Alternatives.

PM Peak Hour

Under No Build conditions there are two bottlenecks that occur. The first bottleneck would develop at the US 101 northbound off-ramp with minimum spill back to within the Mathilda Avenue interchange. The congested study segments in queue would operate at LOS F and alleviate to LOS D. The second bottleneck would develop at the Mathilda Avenue off-ramp and spill back to west of the Lawrence Expressway on-ramp. The congested study segments in queue would operate at LOS E/F and improve to LOS D west of the Lawrence Expressway on-ramp. West of the Mathilda Avenue off-ramp the freeway segments operate at LOS C/D. The westbound HOT lane, which begins prior to the start of the study network and ends between the Mathilda Avenue and Fair Oaks Avenue ramps, is anticipated to operate at LOS A during the PM peak hour.



New bottlenecks are not anticipated to develop under the Build Alternatives. The general purpose lanes are anticipated to operate at the same level of service as No Build under both Build Alternatives. The general purpose lanes west of the US 101 interchange are anticipated to worsen from LOS C to LOS D, however, the change in density is 0.2 vehicles per hour per lane and is not anticipated to adversely affect freeway operations. The westbound HOT lane is anticipated to operate at LOS A during the PM peak hour under the Build Alternatives.

SR 237 Eastbound

AM Peak Hour

During the AM peak hour, there are no bottlenecks estimated to develop within the study area or spill back into the study area on SR 237 eastbound. The general purpose lanes operate at LOS C/D throughout the network under No Build conditions. The eastbound HOT lane, which starts at the Mathilda Avenue on-ramp, is anticipated to operate at LOS B during the AM peak hour.

New bottlenecks are not anticipated to develop under the Build Alternatives. The general purpose lanes are anticipated to operate at the same level of service as No Build (LOS C/D) under both Build Alternatives. The eastbound HOT lane is anticipated to operate at LOS B during the AM peak hour under the Build Alternatives. The density on the general purpose lanes decreases slightly between the US 101 on-ramp and the Mathilda Avenue off-ramp due to the shift in traffic from SR 237 eastbound to US 101 southbound and exits at Mathilda Avenue. There is also a slight increase in density east of the Mathilda Avenue on-ramp. Due to the increase in demand served along Mathilda Avenue, more vehicles are able to access the freeway on-ramp and an additional number of vehicles are estimated to enter the freeway under Build Conditions. This shift in traffic does not adversely affect the results of the freeway density and LOS results.

PM Peak Hour

Under No Build conditions, a bottleneck would develop east of the study area that most likely is due to the queue spillback from the I-880 ramps. The bottleneck results in upstream queuing that extends beyond the extents of the study segments. The study segments in queue would operate at LOS F. The southbound HOT lane is anticipated to operate at LOS B during the PM peak hour.

New bottlenecks are not anticipated to develop under the Build Alternatives. The general purpose lanes are anticipated to operate at the same level of service as No Build (LOS F) but at a lower density under both Build Alternatives. The significantly lower density under both Build Alternatives is due to the full access interchange at Mathilda Avenue and US 101. Vehicles traveling southbound on US 101 are able to remain on US 101 to access northbound Mathilda Avenue under both Build Alternatives instead of getting on SR 237 eastbound in order to access northbound Mathilda Avenue. The eastbound HOT lane is anticipated to operate at LOS B during the PM peak hour under the Build Alternatives.



FREEWAY SYSTEM PERFORMANCE

Year 2018 peak hour system-wide MOEs for the US 101 and SR 237 study corridors are presented in **Table 5-14** and **Table 5-15** for the peak hour and peak period, respectively. These MOEs reflect the overall US 101 operations between the Fair Oaks Avenue and the Ellis Street interchanges and SR 237 operations between the Fair Oaks Avenue and Maude Avenue interchanges. MOEs including average travel time and average speed are the most informative as they relate directly to the traveler experience on US 101 and SR 237 through the corridor. Detailed analysis worksheets are presented in **Appendix M**.

With the implementation of a full-access interchange at US 101 and Mathilda Avenue, there is a shift in some vehicular traffic from SR 237 to US 101. This results in a decrease in travel time, delay, and maximum individual delay along SR 237 eastbound in both the AM and PM peak hours. Consequently, the US 101 southbound segments see a slight increase in travel time, delay, and maximum delay. Due to the nature of the project, local street demand served will increase with the project and will put more traffic on the ramps as a result. The increase in on-ramp volume produces some additional delay along the SR 237 westbound network in the AM peak hour as see in **Table 5-14** and **Table 5-15**.

The US 101 northbound results indicate an increase in travel time and mainline vehicle delay with both Build Alternatives. This increase is due to the increase in demand served at the Mathilda Avenue / US 101 northbound ramp terminal intersection. Under the No Build Alternative, congestion along Mathilda Avenue prevents vehicles from accessing the US 101 northbound on-ramp. However, with both Build Alternatives, more of the demand volume on Mathilda Avenue is able to access the on-ramp, resulting in additional traffic entering US 101 in the northbound direction.



TABLE 5-14: YEAR 2018 PEAK HOUR MEASURES OF EFFECTIVENESS

| Scenario | Measure of Effectiveness | Peak Hour | No Build Conditions | Build 1 Alternative | | Build 2 Alternative | |
|-------------------|---|-----------|---------------------|---------------------|----------|---------------------|----------|
| | | | | Results | % Change | Results | % Change |
| US 101 Northbound | Vehicle Miles of Travel (vehicle-miles) | AM | 11,740 | 11,470 | -2.4% | 11,480 | -2.3% |
| | | PM | 9,770 | 9,480 | -3.1% | 9,480 | -3.1% |
| | Average Travel Time (min:sec) | AM | 6:27 | 7:06 | 9.2% | 7:04 | 8.7% |
| | | PM | 3:50 | 4:58 | 22.8% | 4:56 | 22.3% |
| | Average Travel Speed (mph) | AM | 20.1 | 18.2 | -10.4% | 18.3 | -9.8% |
| | | PM | 33.8 | 26.1 | -29.5% | 26.3 | -28.5% |
| | Mainline Vehicle Delay (vehicle-hours) ¹ | AM | 292 | 323 | 9.6% | 323 | 9.6% |
| | | PM | 102 | 159 | 35.8% | 158 | 35.4% |
| US 101 Southbound | Vehicle Miles of Travel (vehicle-miles) | AM | 10,740 | 10,940 | 1.8% | 10,920 | 1.6% |
| | | PM | 13,920 | 13,890 | -0.2% | 13,870 | -0.4% |
| | Average Travel Time (min:sec) | AM | 1:57 | 1:57 | 0.0% | 1:57 | 0.0% |
| | | PM | 8:11 | 8:22 | 2.2% | 8:28 | 3.3% |
| | Average Travel Speed (mph) | AM | 64.7 | 64.7 | 0.0% | 64.7 | 0.0% |
| | | PM | 15.4 | 15.1 | -2.0% | 14.9 | -3.4% |
| | Mainline Vehicle Delay (vehicle-hours) ¹ | AM | 1 | 1 | 0.0% | 1 | 0.0% |
| | | PM | 536 | 548 | 2.2% | 555 | 3.4% |
| SR 237 Westbound | Vehicle Miles of Travel (vehicle-miles) | AM | 11,470 | 11,360 | -1.0% | 11,370 | -0.9% |
| | | PM | 8,330 | 8,340 | 0.1% | 8,370 | 0.5% |
| | Average Travel Time (min:sec) | AM | 3:30 | 3:51 | 9.1% | 3:48 | 7.9% |
| | | PM | 3:36 | 3:38 | 0.9% | 3:38 | 0.9% |
| | Average Travel Speed (mph) | AM | 38.3 | 34.9 | -9.7% | 35.3 | -8.5% |
| | | PM | 37.3 | 36.9 | -1.1% | 36.9 | -1.1% |
| | Mainline Vehicle Delay (vehicle-hours) ¹ | AM | 60 | 70 | 14.3% | 70 | 14.3% |
| | | PM | 50 | 50 | 0.0% | 50 | 0.0% |
| SR 237 Eastbound | Vehicle Miles of Travel (vehicle-miles) | AM | 9,210 | 9,340 | 1.5% | 9,280 | 0.9% |
| | | PM | 7,780 | 8,890 | 12.5% | 8,880 | 12.4% |
| | Average Travel Time (min:sec) | AM | 2:16 | 2:14 | -1.5% | 2:13 | -2.3% |
| | | PM | 13:32 | 9:13 | -46.8% | 9:14 | -46.6% |
| | Average Travel Speed (mph) | AM | 59.1 | 60.0 | 1.5% | 60.4 | 2.2% |
| | | PM | 9.9 | 14.5 | 31.7% | 14.5 | 31.7% |
| | Mainline Vehicle Delay (vehicle-hours) ¹ | AM | 147 | 11 | -24.8% | 11 | -30.6% |
| | | PM | 513 | 384 | -33.7% | 384 | -33.7% |

Notes:

1. US 101 Northbound AM and PM peak hour is between 7:00AM and 8:00AM and 5:00PM to 6:00PM, respectively.
2. US 101 Southbound AM and PM peak hour is between 7:00AM and 8:00AM and 5:00PM to 6:00PM, respectively.
3. SR 237 Westbound AM and PM peak hour is between 7:00AM and 8:00AM and 5:00PM to 6:00PM, respectively.
4. SR 237 Eastbound AM and PM peak hour is between 8:00AM and 9:00AM and 5:00PM to 6:00PM, respectively.

Source: Fehr & Peers, 2016.



TABLE 5-15: YEAR 2018 PEAK PERIOD MEASURES OF EFFECTIVENESS

| Scenario | Measure of Effectiveness | Peak Hour | No Build Conditions | Build 1 Alternative | | Build 2 Alternative | |
|---|---|-----------|---------------------|---------------------|----------|---------------------|----------|
| | | | | Results | % Change | Results | % Change |
| US 101 Northbound | Vehicle Miles of Travel (vehicle-miles) | AM | 25,070 | 24,530 | -2.2% | 24,570 | -2.0% |
| | | PM | 30,250 | 29,860 | -1.3% | 29,830 | -1.4% |
| | Average Travel Time (min:sec) | AM | 6:37 | 7:20 | 9.8% | 7:18 | 9.4% |
| | | PM | 3:40 | 4:54 | 25.2% | 4:51 | 24.4% |
| | Average Travel Speed (mph) | AM | 19.6 | 17.7 | -10.7% | 17.7 | -10.7% |
| | | PM | 35.3 | 26.4 | -33.7% | 26.7 | -32.2% |
| Mainline Vehicle Delay (vehicle-hours) ¹ | AM | 672 | 763 | 11.9% | 763 | 11.9% | |
| | PM | 314 | 527 | 40.4% | 517 | 39.3% | |
| Maximum Individual Vehicle Delay (min:sec) | AM | 4:48 | 5:36 | 14.3% | 5:32 | 13.3% | |
| | PM | 3:10 | 5:45 | 44.9% | 5:36 | 43.5% | |
| US 101 Southbound | Vehicle Miles of Travel (vehicle-miles) | AM | 24,090 | 24,590 | 2.0% | 24,520 | 1.8% |
| | | PM | 36,350 | 36,330 | -0.1% | 36,280 | -0.2% |
| | Average Travel Time (min:sec) | AM | 2:02 | 2:03 | 0.8% | 2:03 | 0.8% |
| | | PM | 9:10 | 9:17 | 1.3% | 9:24 | 2.5% |
| | Average Travel Speed (mph) | AM | 62.0 | 61.5 | -0.8% | 61.5 | -0.8% |
| | | PM | 13.8 | 13.6 | -1.5% | 13.4 | -3.0% |
| Mainline Vehicle Delay (vehicle-hours) ¹ | AM | 17 | 21 | 19.0% | 19 | 10.5% | |
| | PM | 1569 | 1595 | 1.6% | 1611 | 2.6% | |
| Maximum Individual Vehicle Delay (min:sec) | AM | 0:10 | 0:13 | 23.1% | 0:12 | 16.7% | |
| | PM | 8:08 | 8:16 | 1.6% | 8:16 | 1.6% | |
| SR 237 Westbound | Vehicle Miles of Travel (vehicle-miles) | AM | 19,800 | 19,600 | -1.0% | 19,640 | -0.8% |
| | | PM | 25,210 | 25,240 | 0.1% | 25,330 | 0.5% |
| | Average Travel Time (min:sec) | AM | 3:46 | 4:02 | 6.6% | 3:60 | 5.8% |
| | | PM | 2:53 | 2:54 | 0.6% | 2:54 | 0.6% |
| | Average Travel Speed (mph) | AM | 35.6 | 33.3 | -6.9% | 33.6 | -6.0% |
| | | PM | 46.5 | 46.3 | -0.4% | 46.3 | -0.4% |
| Mainline Vehicle Delay (vehicle-hours) ¹ | AM | 220 | 240 | 8.3% | 240 | 8.3% | |
| | PM | 142 | 152 | 6.6% | 152 | 6.6% | |
| Maximum Individual Vehicle Delay (min:sec) | AM | 1:58 | 2:08 | 7.8% | 2:08 | 7.8% | |
| | PM | 1:32 | 1:34 | 2.1% | 1:35 | 3.2% | |
| SR 237 Eastbound | Vehicle Miles of Travel (vehicle-miles) | AM | 16,200 | 16,400 | 1.3% | 16,310 | 0.7% |
| | | PM | 19,740 | 21,020 | 6.1% | 21,020 | 6.1% |
| | Average Travel Time (min:sec) | AM | 2:13 | 2:12 | -0.8% | 2:12 | -0.8% |
| | | PM | 9:32 | 8:04 | -18.2% | 8:04 | -18.2% |
| | Average Travel Speed (mph) | AM | 60.4 | 60.9 | 0.8% | 60.9 | 0.8% |
| | | PM | 14.1 | 16.6 | 15.1% | 16.6 | 15.1% |
| Mainline Vehicle Delay (vehicle-hours) ¹ | AM | 20 | 17 | -16.3% | 16 | -20.6% | |
| | PM | 1124 | 751 | -49.5% | 757 | -48.3% | |
| Maximum Individual Vehicle Delay (min:sec) | AM | 0:13 | 0:10 | -20.0% | 0:10 | -20.0% | |
| | PM | 11:28 | 7:10 | -60.0% | 7:10 | -60.0% | |

Source: Fehr & Peers, 2016.



MAINLINE WEAVING ANALYSIS

Per Caltrans' requirements, **Table 5-16** summarizes the Year 2018 Leisch Method AM and PM peak hour mainline weaving analysis at the US 101/Mathilda Avenue and SR 237/Mathilda Avenue interchanges. The Leisch Method analysis was applied for the constrained mainline and ramp volumes as determined by the FREQ models. The Leisch Method has a limitation of 3,600 passenger cars per hour for weaving volumes and a weaving length of 6,000 feet. There are no segments that are outside of the provided parameters.

The SR 237 eastbound weaving section improves from an LOS F to LOS E in the AM peak hour under both Build Alternatives. In addition, the SR 237 westbound weaving section improves from an LOS F to an LOS E in the PM peak hour while the US 101 southbound weaving section decreases from an LOS D to LOS E in the PM peak hour with the given shift in traffic due to the full access interchange at US 101/Mathilda Avenue. **Appendix N** provides the Leisch analysis worksheets. These results differ from the FREQ results presented earlier due to the following reasons:

- Leisch Method uses default mainline capacities while the FREQ models use calibrated capacities to reflect observed conditions;
- Leisch Method evaluates mainline segments in isolation where bottlenecks and mainline queuing do not impact downstream or upstream traffic. FREQ models consider the effects of the bottlenecks and mainline queuing on the entire mainline system.

TABLE 5-16: YEAR 2018 PEAK HOUR WEAVING ANALYSIS BASED ON LEISCH METHOD

| Freeway | Location | Direction | Number of Lanes | No Build | Build 1 | Build 2 |
|-----------|---|-----------|-----------------------------------|----------|---------|---------|
| AM | | | | | | |
| US 101 | SR 237 EB on-ramp to Mathilda Avenue off-ramp | SB | 1 HOT 3 Mainline 1 Aux Lane | C | D | D |
| SR 237 | Mathilda Avenue on-ramp to US 101 NB off-ramp | WB | 2 Mainline 1 Aux Lane | D | D | D |
| | US 101 SB on-ramp to Mathilda Avenue off-ramp | EB | 2 Mainline 1 Aux Lane | F | E | E |
| PM | | | | | | |
| US 101 | SR 237 EB on-ramp to Mathilda Avenue off-ramp | SB | 1 HOT 3 Mainline 1 Aux Lane | D | E | E |
| SR 237 | Mathilda Avenue on-ramp to US 101 NB off-ramp | WB | 2 Mainline 1 Aux Lane | F | E | E |
| | US 101 SB on-ramp to Mathilda Avenue off-ramp | EB | 2 Mainline 1 Aux Lane | D | D | D |

Notes: **Bold** indicates weaving section operates at LOS F under un-congested conditions.

Source: Fehr & Peers, 2016.



6. YEAR 2040 TRAFFIC OPERATIONS ANALYSIS

This chapter presents the results of the traffic operations analysis for year 2040. The operations analysis for year 2040 focuses on intersection and freeway operations for No Build and Build conditions.

YEAR 2040 ROADWAY NETWORK ASSUMPTIONS

The local roadway network assumptions for Year 2040 No Build and Build Alternative scenarios are the same as those made for Year 2018 except for the following:

- *Mary Avenue Extension* – extended as a 4-lane street to E Street on the north side of SR 237: Mary Avenue, currently located west of Mathilda Avenue and south of US 101, is assumed to extend over the SR 237 and US 101 freeways and connect to E Street and 11th Avenue north of SR 237.

CONSTRAINED VOLUME ANALYSIS APPROACH

The same approach used to develop constrained volumes for Year 2018 was used to develop constrained volumes for Year 2040.

YEAR 2040 INTERSECTION OPERATIONS

Year 2040 intersection traffic operations were evaluated using the calibrated/validated SimTraffic models developed for Existing Conditions. The simulation models were executed for the peak hour with a 30-minute seeding period. The following constrained volume factors were applied to the off-ramp demand volumes to account for congestion along US 101 and SR 237 (consistent with the three-step modeling approach described above):

- Westbound SR 237 off-ramp to Mathilda Avenue = 0.79 during the AM peak hour and 0.84 during the PM peak hour;
- Eastbound SR 237 off-ramp to Mathilda Avenue = 0.90 during the AM peak hour and 0.83 during the PM peak hour;
- Northbound US 101 off-ramp to Mathilda Avenue = 0.84 during the AM peak hour and 0.84 during the PM peak hour;
- Southbound US 101 off-ramp to Mathilda Avenue = 0.85 during the AM peak hour and 0.65 during the PM peak hour.

INTERSECTION DELAY, LOS, AND PERCENT DEMAND SERVED

Table 6-1 presents the Year 2040 simulated intersection level of service results and percent demand served for each of the study intersections under No Build and Build Alternatives. Queuing results are included in



the following section. Intersection LOS results in **bold** indicate locations operating at LOS F conditions. Analysis results worksheets are presented in **Appendix O**.⁶

No Build Conditions

As shown in **Table 6-1** the majority of study intersections are anticipated to operate at LOS F during the AM and/or PM peak hour under No Build conditions in Year 2040. The percent demand served is on average 80 percent and 70 percent during the AM and PM peak hours, respectively. The low percent demand served is indicative of the projected traffic demand exceeding the capacity of the roadway system. The total vehicle hours of delay are estimated to be 2,989 in the AM peak hour and 3,830 in the PM peak hour.

Build 1 Alternative

Below is a brief summary of the operations at the study locations under Build 1 Alternative in Year 2040 and how they compare to No Build conditions.

- *Mathilda Avenue/Fifth Avenue* – Intersection level of service is anticipated to remain unchanged (LOS C during the AM peak hour and LOS F during the PM peak hour). The overall intersection delay is estimated to decrease slightly for the AM and PM peak hours. The percent demand served is anticipated to increase from 78 percent to 85 percent in the AM peak hour and increase from about 63 percent to 67 percent in the PM peak hour.
- *Mathilda Avenue/Innovation Way* – Intersection level of service is anticipated to remain unchanged (LOS F during the AM and PM peak hours). The overall intersection delay would also remain relatively unchanged (less than a 5 percent change) for the PM peak hour and decrease by approximately 30 second in the AM peak hour. The percent demand served is anticipated to increase from 67 percent to 79 percent in the AM peak hour and decrease from about 59 percent to 57 percent in the PM peak hour. The slight decrease in PM percent demand served is due to additional traffic that will travel through this intersection due to the closure of Moffett Park Drive between Mathilda Avenue and Bordeaux Drive.
- *Mathilda Avenue/Moffett Park Drive/SR 237 Westbound Ramps* – Intersection level of service is anticipated to remain unchanged (LOS F in the AM and PM peak hours). Although the intersection would continue to operate at LOS F under Build 1 Alternative, the overall intersection delay would be reduced by over 215 seconds in the AM peak hour and over 75 seconds in the PM peak hours compared to No Build conditions. The reduction in peak hour delay is a result of eliminating the westbound Moffett Park Drive approach which reduces the number of signal phases at this location. The percent demand served is anticipated to increase from 64 percent to 80 percent in the AM peak hour and decrease slightly from about 65 percent to 63 percent in the PM peak hour.
- *Mathilda Avenue/ SR 237 Eastbound Ramps* – Intersection level of service is anticipated to remain unchanged at LOS F in the AM peak hour and decrease from LOS C to LOS D in the PM peak hour. The PM peak hour conditions worsen under the Build 1 Alternative due to a higher southbound left-turn/northbound through volume conflict that increases the southbound left-

⁶ Please note that Synchro and SimTraffic worksheets are provided for the study intersections in **Appendix O** for informational purposes to present key modeling inputs including lanes, volumes, and signal timings. The results presented in **Table 5-2** are from SimTraffic analysis output.



turn movement delay. The volume arriving on the northbound approach is over 110 vehicles greater under the Build 1 Alternative than No Build conditions. The percent demand served is anticipated to increase from 60 percent to 77 percent in the AM peak hour and remain the same at 68 percent in the PM peak hour.

- *Mathilda Avenue/ Ross Drive* – Intersection level of service is anticipated to improve from LOS F to LOS E in the AM peak hour and remain unchanged at LOS F during the PM peak hour. Although the intersection would continue to operate at LOS F under Build 1 Alternative in the PM peak hour, the overall intersection delay would be reduced by over 50 seconds. The percent demand served is anticipated to increase from 55 percent to 80 percent in the AM peak hour and from 67 percent to 71 percent in the PM peak hour.
- *Mathilda Avenue/ US 101 Northbound Ramps (Build Conditions)* – This intersection is anticipated to operate at LOS F during the AM and PM peak hour. The percent demand served is estimated at 81 percent during the AM peak hour and 74 percent during the PM peak hour.
- *Mathilda Avenue/ US 101 Southbound Ramps (Build Conditions)* – This intersection is anticipated to operate at LOS D during the AM peak hour and LOS C during the PM peak hour. The percent demand served is estimated at 80 percent during the AM peak hour and 78 percent during the PM peak hour.
- *Mathilda Avenue/ Almanor Avenue-Ahwanee Avenue* – Intersection level of service is anticipated to remain unchanged (LOS F) during the AM peak hour and improve from LOS F to LOS E in the PM peak hour. Although the intersection would continue to operate at LOS F during the AM peak hour under Build 1 Alternative the percent demand served is anticipated to increase from 62 percent to 79 percent in the AM peak hour and from 68 percent to 84 percent in the PM peak hour.
- *US 101 Northbound On-Ramp/Moffett Park Drive* – Intersection level of service is anticipated to remain unchanged (LOS A) during the AM peak hour and decrease from LOS E to LOS F in the PM peak hour. The delay in the PM peak hour is estimated to increase by 20 seconds under the Build 1 Alternative. The various improvements along Mathilda Avenue as part of this project allow additional northbound and southbound traffic through the Mathilda Avenue corridor, but results in secondary congestion along eastbound Moffett Park Drive limiting the amount of traffic able to be served at Mathilda Avenue. The percent demand served is anticipated to increase from 75 percent to 86 percent in the AM peak hour and remain unchanged at 61 percent in the PM peak hour.
- *Innovation Way/Moffett Park Drive* – Intersection level of service is anticipated to increase from LOS B to LOS C during the AM peak hour and remain unchanged during the PM peak hour (LOS F). The percent demand served is anticipated to increase from 74 percent to 84 percent in the AM peak hour and remain unchanged at 60 percent in the PM peak hour.
- *Innovation Way/ Eleventh Avenue* – Intersection level of service is anticipated to remain unchanged (LOS B) during the AM peak hour and during the PM peak hour (LOS F). Although the intersection would continue to operate at LOS F during the PM peak hour under Build 1 Alternative the overall intersection delay would be reduced by over 40 percent compared to No Build conditions (see **Appendix O**). The percent demand served is anticipated to increase from 76 percent to 85 percent in the AM peak hour and slightly decrease from 59 percent to 58 percent in the PM peak hour.
- *Innovation Way/Juniper Networks Driveway* – Intersection level of service is anticipated to remain unchanged (LOS D) during the AM peak hour and during the PM peak hour (LOS F). Although the



intersection would continue to operate at LOS F during the PM peak hour under Build 1 Alternative the overall intersection delay would be reduced by over 24 percent compared to No Build conditions (see **Appendix O**). The percent demand served is anticipated to increase from 70 percent to 85 percent in the AM peak hour and from 50 percent to 52 percent in the PM peak hour.

- *Bordeaux Drive/Innovation Way* – Intersection level of service is anticipated to worsen from LOS A to LOS F during the AM and PM peak hours. The proposed project design would result in an increase over 260 and 190 percent in traffic volume at this location during the AM and PM peak hour, respectively. The percent demand served is anticipated to decrease from 100 percent to 75 percent in the AM peak hour and from 65 percent to 39 percent in the PM peak hour.

The Build 1 Alternative would improve traffic conditions at most of the study locations but also worsen some of the study locations for at least one peak hour. During the AM peak hour the total vehicle hours of delay would be reduced from 2,989 to 1,948 (35 percent reduction) and from 3,830 to 3,130 (18 percent reduction) during the PM peak hour. The reduction in overall vehicle hours of delay for the AM and PM peak hour indicates the Build 1 Alternative would provide an overall benefit to the traffic operations in the study area compared to No Build conditions.

Build 2 Alternative

Below is a brief summary of the operations at the study locations under Build 2 Alternative in Year 2040 and how they compare to No Build conditions.

- *Mathilda Avenue/Fifth Avenue* – Intersection level of service is anticipated to remain unchanged (LOS C during the AM peak hour and LOS F during the PM peak hour). The overall intersection delay would decrease by roughly 13 seconds in the AM peak hour and improve delay by 80 percent in the PM peak hour. The percent demand served is anticipated to increase from 78 percent to 84 percent in the AM peak hour and increase from about 63 percent to 70 percent in the PM peak hour.
- *Mathilda Avenue/Innovation Way* – Intersection level of service is anticipated to remain unchanged during the AM and PM peak hours (LOS F). The overall intersection delay would decrease 10 to 20 seconds of delay in the peak hours. The PM peak hour delay decreases by approximately 10 seconds due to the additional capacity provided by the DDI traveling southbound on Mathilda Avenue. The percent demand served is anticipated to increase from 67 percent to 77 percent in the AM peak hour and decrease slightly from about 59 percent to 56 percent in the PM peak hour. Queuing analysis results for this intersection are discussed in the following section.
- *Mathilda Avenue/Moffett Park Drive/SR 237 Westbound Ramps* – Intersection level of service is anticipated to remain unchanged at LOS F in the AM and PM peak hours. The overall intersection delay would decrease by approximately 80 percent in the AM and PM peak hours. The improvements in the peak hours is a result of the efficient signal timing as a results of the DDI and the closure of Moffett Park Drive to Mathilda Avenue. The percent demand served is anticipated to increase from 63 percent to 74 percent in the AM peak hour and increase from about 65 percent to 74 percent in the PM peak hour.



- *Mathilda Avenue/ SR 237 Eastbound Ramps* – Intersection level of service is anticipated to remain unchanged at LOS F during the AM peak hour and LOS C during the PM peak hour. The delay in the AM peak hour decreases by approximately 45 percent and the PM peak hour delay remains approximately the same. The percent demand served is anticipated to increase from 60 percent to 74 percent in the AM peak hour and from 68 percent to 72 percent in the PM peak hour.
- *Mathilda Avenue/ Ross Drive* – Intersection level of service is anticipated to remain at LOS F in the AM and PM peak hours. The delay in the AM peak hour is expected to decrease by over 60 percent. The percent demand served is anticipated to increase from 55 percent to 72 percent in the AM peak hour and from 67 percent to 72 percent in the PM peak hour.
- *Mathilda Avenue/ US 101 Northbound Ramps (Build Conditions)* – This intersection is anticipated to operate at LOS F during the AM and PM peak hours. The percent demand served is estimated at 75 percent during the AM peak hour and 74 percent during the PM peak hour.
- *Mathilda Avenue/ US 101 Southbound Ramps (Build Conditions)* – This intersection is anticipated to operate at LOS E during the AM and PM peak hours. The percent demand served is estimated at 73 percent during the AM peak hour and 76 percent during the PM peak hour.
- *Mathilda Avenue/ Almanor Avenue-Ahwanee Avenue* – Intersection level of service is anticipated to remain unchanged (LOS F) during the AM and PM peak hours. Although the intersection would continue to operate at LOS F during the AM peak hour under Build 2 Alternative the overall intersection delay would be reduced by approximately 4 percent of delay compared to No Build conditions in the AM peak hour and over 50 percent in the PM peak hour (see **Appendix O**). The percent demand served is anticipated to increase from 62 percent to 72 percent in the AM peak hour and from 68 percent to 79 percent in the PM peak hour.
- *US 101 Northbound On-Ramp/Moffett Park Drive* – Intersection level of service is anticipated to remain unchanged at LOS B during the AM peak hour and LOS F in the PM peak hour as a result of congestion along Innovation Way. The percent demand served is anticipated to increase from 75 percent to 81 percent in the AM peak hour and decrease from 61 percent to 53 percent in the PM peak hour.
- *Innovation Way/Moffett Park Drive* – Intersection level of service is anticipated to remain unchanged (LOS B) during the AM peak hour and during the PM peak hour (LOS F). The percent demand served is anticipated to increase from 74 percent to 79 percent in the AM peak hour and decrease from 61 percent to 53 percent in the PM peak hour.
- *Innovation Way/Eleventh Avenue* – Intersection level of service is anticipated to remain unchanged (LOS B) during the AM peak hour and during the PM peak hour (LOS F). Although the intersection would continue to operate at LOS F during the PM peak hour under Build 2 Alternative the overall intersection delay would be reduced by over 45 percent compared to No Build conditions. The percent demand served is anticipated to increase from 76 percent to 82 percent in the AM peak hour and decrease from 59 percent to 54 percent in the PM peak hour.
- *Innovation Way/Juniper Networks Driveway* – Intersection level of service is anticipated to remain unchanged (LOS D) during the AM peak hour and during the PM peak hour (LOS F). Although the intersection would continue to operate at LOS F during the PM peak hour under Build 2 Alternative the overall intersection delay would be reduced by roughly 50 percent compared to No Build conditions (see **Appendix O**). The Build 2 Alternative would result in an increase of over 160 percent in traffic volume at this location during the PM peak hour. The percent demand served is anticipated to increase from 70 percent to 79 percent in the AM peak hour and decrease from 50 percent to 42 percent in the PM peak hour.



- *Bordeaux Drive/Innovation Way* – Intersection level of service is anticipated to worsen from LOS A to LOS F during the AM and PM peak hours. The proposed project design would result in an increase of over 260 and 190 percent in traffic volume at this location during the AM and PM peak hour, respectively. However the demand at this intersection is less than a fourth of the volume along Mathilda Avenue. The percent demand served is anticipated to decrease from 100 percent to 73 percent in the AM peak hour and from 65 percent to 42 percent in the PM peak hour.

The Build 2 Alternative would improve traffic conditions at most of the study locations but also worsen some of the study locations for at least one peak hour. During the AM peak hour the total vehicle hours of delay would be reduced from 2,989 to 2,582 (14 percent reduction) and from 3,830 to 3,262 (15 percent reduction) during the PM peak hour. The reduction in overall vehicle hours of delay for the AM and PM peak hour indicates the Build 2 Alternative would provide an overall benefit to the traffic operations in the study area compared to No Build conditions.



TABLE 6-1: YEAR 2040 PEAK HOUR INTERSECTION ANALYSIS¹

| | Intersection | Peak Hour ² | No Build | | | Build 1 Alternative | | | Build 2 Alternative | | |
|--------------------------------------|---|------------------------|--------------------|------------------|------------------------------|---------------------|------------------|------------------------------|---------------------|------------------|------------------------------|
| | | | Delay ³ | LOS ⁴ | % Demand Served ⁵ | Delay ³ | LOS ⁴ | % Demand Served ⁵ | Delay ³ | LOS ⁴ | % Demand Served ⁵ |
| 1 | Mathilda Avenue / Fifth Avenue ⁶ | AM | 33.5 | C | 77.7 | 25.3 | C | 84.9 | 20.7 | C | 84.0 |
| | | PM | >300 | F | 63.3 | >300 | F | 66.9 | 117.9 | F | 69.5 |
| 2 | Mathilda Avenue / Innovation Way ⁶ | AM | 116.9 | F | 67.2 | 88.9 | F | 79.2 | 90.0 | F | 76.6 |
| | | PM | 222.0 | F | 59.0 | 220.9 | F | 56.8 | 209.0 | F | 55.9 |
| 3 | Mathilda Avenue / Moffett Park Drive / SR 237 Westbound Ramps | AM | >300 | F | 63.3 | 81.4 | F | 79.7 | 188.4 | F | 74.3 |
| | | PM | >300 | F | 65.0 | 221.4 | F | 62.5 | 94.4 | F | 73.8 |
| 4 | Mathilda Avenue / SR 237 Eastbound Ramps | AM | 257.7 | F | 59.7 | 142.3 | F | 76.9 | 133.0 | F | 73.8 |
| | | PM | 25.0 | C | 67.6 | 46.5 | D | 68.4 | 28.6 | C | 71.6 |
| 5 | Mathilda Avenue / Ross Drive | AM | >300 | F | 55.3 | 76.0 | E | 80.6 | 149.8 | F | 72.4 |
| | | PM | 200.0 | F | 67.1 | 148.3 | F | 71.2 | 149.0 | F | 71.8 |
| 6 | Mathilda Avenue / US 101 Northbound Ramps (Build) | AM | N/A | N/A | N/A | 87.9 | F | 81.1 | 95.6 | F | 75.3 |
| | | PM | | | | 112.6 | F | 74.1 | 127.7 | F | 74.1 |
| 7 | Mathilda Avenue / US 101 Southbound Ramps (Build) | AM | N/A | N/A | N/A | 42.0 | D | 79.6 | 61.1 | E | 73.2 |
| | | PM | | | | 29.0 | C | 78.3 | 66.5 | E | 75.5 |
| 8 | Mathilda Avenue / Almanor Avenue-Ahwanee Avenue | AM | >300 | F | 62.3 | >300 | F | 78.6 | >300 | F | 72.1 |
| | | PM | >300 | F | 67.9 | 71.5 | E | 83.9 | 219.4 | F | 79.0 |
| 9 | US 101 Northbound On-Ramp / Moffett Park Drive | AM | 3.4 | A | 75.2 | 4.9 | A | 85.5 | 3.7 | A | 81.1 |
| | | PM | 64.3 | E | 61.4 | 85.4 | F | 61.1 | 122.3 | F | 53.4 |
| 10 | Innovation Way / Moffett Park Drive ⁶ | AM | 14.2 | B | 73.6 | 24.8 | C | 83.6 | 19.8 | B | 79.0 |
| | | PM | 245.4 | F | 60.8 | 273.7 | F | 59.2 | 262.4 | F | 53.4 |
| 11 | Innovation Way / Eleventh Avenue | AM | 10.4 | B | 75.6 | 10.9 | B | 85.1 | 10.8 | B | 82.4 |
| | | PM | >300 | F | 59.2 | >300 | F | 57.7 | 294.5 | F | 54.4 |
| 12 | Innovation Way / Juniper Networks Driveway | AM | 34.2 | D | 69.7 | 31.4 | D | 84.5 | 53.4 | D | 78.8 |
| | | PM | >300 | F | 50.3 | >300 | F | 52.0 | >300 | F | 41.8 |
| 13 | Bordeaux Drive / Innovation Way (future) | AM | 4.7 | A | 100.0 | 130.2 | F | 75.5 | >300 | F | 72.9 |
| | | PM | 7.1 | A | 65.0 | >300 | F | 39.3 | >300 | F | 41.7 |
| Total Vehicle Hours of Delay (hours) | | AM | | 2,989 | | 1,948 | | 2,582 | | | |
| | | PM | | 3,830 | | 3,130 | | 3,262 | | | |



TABLE 6-1: YEAR 2040 PEAK HOUR INTERSECTION ANALYSIS¹

| Intersection | Peak Hour ² | No Build | | | Build 1 Alternative | | | Build 2 Alternative | | |
|------------------------------------|------------------------|--------------------|------------------|------------------------------|---------------------|------------------|------------------------------|---------------------|------------------|------------------------------|
| | | Delay ³ | LOS ⁴ | % Demand Served ⁵ | Delay ³ | LOS ⁴ | % Demand Served ⁵ | Delay ³ | LOS ⁴ | % Demand Served ⁵ |
| Network-wide Percent Demand Served | AM | | | 79.9% | | | 88.3% | | | 83.5% |
| | PM | | | 70.6% | | | 77.8% | | | 76.2% |

Notes: Results in **bold** represent unacceptable levels of service, N/A=not applicable.

1. Results based on SimTraffic simulation of five runs.
2. AM – morning peak hour, PM – evening peak hour
3. Average control delay calculated using the *Highway Capacity Manual (HCM)* (Transportation Research Board, 2010) methodology and Synchro/SimTraffic 8.0 analysis software. For signalized and all-way stop-controlled intersections, average control delay is for the intersection, as a whole.
4. For signalized and all-way stop-controlled intersections the LOS for the intersection as a whole is presented.
5. Modeled traffic volume expressed as a ratio of **demand** traffic volume. For example: 100% indicates all demand is served.
6. These intersections are coordinated with a light rail crossing. Under Year 2040, the headway in each direction is assumed to increase from 15 minutes to 12 minutes in each direction based on the light-rail efficiency project currently underway. In addition, the route from Mountain View to East San Jose is assumed complete and operates with 15 minute headways.

Source: Fehr & Peers, 2016.



INTERSECTION 95TH PERCENTILE QUEUES

No Build 95th Percentile Queues

Table 6-2 presents the 2040 No Build peak hour 95th percentile queuing analysis results. Analysis results worksheets are presented in **Appendix O**. The projected traffic demand in 2040 is anticipated to far exceed the available roadway capacity. As a result, vehicle queues will exceed available storage at most study locations and queues from one intersection will impact operations at adjacent intersections. During the AM peak hour, northbound Mathilda vehicle queues are expected to extend south past San Aleso Avenue. Due to morning congestion on northbound Mathilda Avenue, particularly at the Ross Drive intersection, the US 101 northbound diagonal off-ramp queues would spill back onto the mainline under No Build Conditions. The morning SR 237 eastbound and westbound off-ramp vehicle queue is also anticipated to extend back onto the mainline due to congestion at the ramp terminal. In addition, there are excessive queues observed traveling westbound on Moffett Park Drive during the AM peak hour.

During the PM peak hour, the projected high southbound traffic volumes on Mathilda Avenue and the close spacing between intersections near the SR 237 interchange would cause vehicle queues on southbound Mathilda Avenue to extend from SR 237 north past Lockheed Martin/Java Avenue. Queues are also anticipated in the northbound direction on Mathilda Avenue in the PM peak hour for vehicles attempted to turn onto the SR 237 Eastbound on-ramp and US 101 Northbound and Southbound on-ramps. Eastbound Innovation Way and Moffett Park Drive are also expected to experience high delays and extensive queuing that spills onto other local roadways. The SR 237 westbound off-ramp and US 101 northbound loop off-ramp queues are expected to extend back to the freeway mainline due to congestion at the ramp terminal.

TABLE 6-2: YEAR 2040 NO BUILD QUEUING ANALYSIS RESULTS

| Intersection | Movement ¹ | Available Storage ² | AM Peak Hour 95 th Percentile Queue (ft) | PM Peak Hour 95 th Percentile Queue (ft) |
|-----------------------------------|-----------------------|--------------------------------|--|--|
| 1. Mathilda Avenue / Fifth Avenue | NB-L | 425 | 125 | 125 |
| | NB-T | 1,125 | 175 | 150 |
| | SB-L | 250 | 100 | 250 |
| | SB-T | 1,325 | 375 | 4,225 |
| | SB-R | 250 | 100 | 275 |
| | EB-L | 625 | 50 | 225 |
| | EB-T | 625 | 50 | 75 |
| | EB-R | 625 | 100 | 275 |
| | WB-L | 925 | 125 | >5,000 |
| | WB-T | 75 | 100 | 100 |



TABLE 6-2: YEAR 2040 NO BUILD QUEUING ANALYSIS RESULTS

| Intersection | Movement ¹ | Available Storage ² | Peak Hour | |
|--|-----------------------|--------------------------------|--|--|
| | | | AM Peak Hour 95 th Percentile Queue (ft) | PM Peak Hour 95 th Percentile Queue (ft) |
| 2. Mathilda Avenue / Innovation Way | NB-L | 400 | 425 | 150 |
| | NB-T | 975 | 425 | 175 |
| | NB-TR | 975 | 375 | 275 |
| | SB-L | 75 | 125 | 100 |
| | SB-T | 975 | 875 | 1,200 |
| | SB-R | 225 | 350 | 350 |
| | EB-L | 200 | 100 | 175 |
| | EB-TR | 200 | 50 | 50 |
| | EB-R | 200 | 250 | 325 |
| | WB-L | 425 | 425 | 450 |
| | WB-LTR | 225 | 250 | 225 |
| 3. Mathilda Avenue / Moffett Park Drive / SR 237 Westbound Ramps | NB-L (MP) | 125 | 50 | 50 |
| | NB-L (237) | 175 | 175 | 150 |
| | NB-T | 300 | 325 | 275 |
| | SB-L (MP) | 175 | 75 | 100 |
| | SB-T | 1,100 | 1,200 | 1,250 |
| | EB-L (MP) | 350 | 75 | 400 |
| | EB-T (MP) | 1,100 | 150 | 1,175 |
| | EB-R (MP) | 1,100 | 100 | 1,150 |
| | WB-L (MP) | 300 | 1,500 | > 5,000 |
| | WB-T (MP) | 650 | 700 | 650 |
| 4. Mathilda Avenue / SR 237 Eastbound Ramps | WB-L (237) | 1,125 | 1,200 | > 5,000 |
| | WB-R (237) | 325 | > 5,000 | 475 |
| | NB-T | 275 | 325 | 100 |
| | NB-R | 275 | 250 | 200 |
| | SB-L | 200 | 150 | 175 |
| | SB-T | 200 | 175 | 225 |
| | EB-L | 1,025 | > 5,000 | 375 |
| 5. Mathilda Avenue / Ross Drive | EB-LTR | 450 | 575 | 400 |
| | NB-L | 150 | 100 | 200 |
| | NB-T | 2,200 | 1,100 | 1,100 |
| | SB-L | 150 | 100 | 175 |
| | SB-T | 250 | 225 | 250 |
| | EB-L | 650 | 1,000 | 400 |
| | EB-T | 75 | 125 | 125 |
| | EB-R | 50 | 75 | 75 |
| | WB-L | 75 | 3,600 | > 5,000 |
| WB-T | 75 | 125 | 150 | |



TABLE 6-2: YEAR 2040 NO BUILD QUEUING ANALYSIS RESULTS

| Intersection | Movement ¹ | Available Storage ² | Peak Hour | |
|--|-----------------------|--------------------------------|--|--|
| | | | AM Peak Hour 95 th Percentile Queue (ft) | PM Peak Hour 95 th Percentile Queue (ft) |
| | WB-R | 75 | 100 | 100 |
| 6. Mathilda Avenue/US 101 NB Ramps** | N/A | N/A | N/A ³ | N/A ⁴ |
| 7. Mathilda Avenue/US 101 SB Ramps** | N/A | N/A | N/A | N/A |
| 8. Mathilda Avenue / Almanor Avenue-Ahwanee Avenue | NB-L | 375 | 325 | 275 |
| | NB-T | 675 | >5,000 | >5,000 |
| | NB-R | 75 | 100 | 100 |
| | SB-L | 125 | 200 | 200 |
| | SB-T | 2,200 | 550 | 1,775 |
| | EB-L | 1,025 | 475 | 350 |
| | EB-TR | 125 | 225 | 300 |
| | WB-L | 250 | 375 | 400 |
| | WB-T | 1,025 | 1,175 | 1,025 |
| 9. US 101 Northbound On- Ramp / Moffett Park Drive | WB-R | 75 | 150 | 125 |
| | EB-T | 850 | 75 | 1,125 |
| | EB-R | 150 | 25 | 475 |
| | WB-L | 850 | 50 | 250 |
| | WB-T | 850 | 25 | 25 |
| 10. Innovation Way / Moffett Park Drive | SB-L | 575 | 50 | 575 |
| | SB-LTR | 575 | 175 | 575 |
| | EB-L | 225 | 100 | 425 |
| | EB-T | 850 | 75 | 1,050 |
| | WB-T | 1,150 | 200 | 400 |
| | WB-R | 225 | 200 | 125 |
| 11. Innovation Way / Eleventh Avenue | NB-L | 125 | 50 | 25 |
| | NB-LT | 575 | 75 | 300 |
| | SB-LT | 1,000 | 50 | 250 |
| | SB-TR | 1,000 | 125 | 350 |
| | EB-L | 125 | 75 | 200 |
| | EB-TR | 300 | 50 | >5,000 |
| | EB-R | 300 | 75 | >5,000 |
| | WB-L | 325 | 25 | 225 |
| WB-TR | 325 | 25 | 50 | |



TABLE 6-2: YEAR 2040 NO BUILD QUEUING ANALYSIS RESULTS

| Intersection | Movement ¹ | Available Storage ² | AM Peak Hour | PM Peak Hour |
|--|-----------------------|--------------------------------|--|--|
| | | | 95 th Percentile Queue (ft) | 95 th Percentile Queue (ft) |
| 12. Innovation Way / Juniper Driveway | NB-L | 125 | 75 | 175 |
| | NB-T | 900 | 175 | 1,100 |
| | SB-TR | 300 | 275 | 225 |
| | SB-R | 300 | 300 | 250 |
| | EB-L | 150 | 375 | >5,000 |
| | EB-R | 150 | 75 | 4,550 |
| 13. Bordeaux Drive / Innovation Way | NB-L | 325 | 75 | 50 |
| | NB-TR | 2,025 | 75 | 50 |
| | SB-L | 125 | 25 | 25 |
| | SB-TR | 725 | 75 | 75 |
| | EB-LT | 375 | 75 | 75 |
| | EB-R | 125 | 75 | 75 |
| | WB-LT | 125 | 25 | 25 |
| WB-R | 125 | 25 | 25 | |

Notes: **Bold** denotes locations where storage length is exceeded.

**Indicates intersection is signalized under Build 1 and Build 2 Alternatives, but operates as a free movement under the No Build Alternative.

1. NB-northbound, SB-southbound, EB-eastbound, WB-westbound, L-left-turn movement, T-through movement, R-right-turn movement, (MP)-turn onto/from Moffett Park Drive, (237)-turn onto/from SR 237 WB Ramps.
2. Available storage lengths are provided on a "per lane" basis. For example, an available storage of 425 means each lane in the associated movement has a storage length of 425 feet.
3. Queuing at the US 101 northbound diagonal off-ramp was observed to extend onto the freeway mainline in the AM peak hour under Existing Conditions. This queuing is anticipated to worsen under Year 2040 No Build conditions.
4. Queuing at the US 101 northbound loop off-ramp was observed to extend onto the freeway mainline in the PM peak hour under Existing Conditions. This queuing is anticipated to worsen under Year 2040 No Build conditions.

Source: Fehr & Peers, 2016.

Build 1 95th Percentile Queues

Table 6-3 presents the Year 2040 Build 1 peak hour 95th percentile queuing analysis results. Analysis results worksheets are presented in **Appendix O**. The capacity enhancements at intersections on Mathilda Avenue and the realignment of the freeway ramps would improve traffic operations and reduce vehicle queue lengths compared to No Build conditions. During the AM peak hour, the SR 237 westbound ramp terminal intersection would provide nearly adequate vehicle storage to accommodate the 95th percentile queue lengths along the off-ramp. However, the SR 237 eastbound off-ramp is anticipated to occasionally queue back onto the mainline during the morning peak hour. The US 101 southbound off-ramp queues are not anticipated to extend back to the freeway mainline under Build 1 compared to No Build. The US 101 northbound off-ramp is anticipated to occasionally queue back slightly onto the freeway (though only by approximately 300 feet). On the local streets, overall queuing is reduced along northbound and southbound Mathilda Avenue. The closure of westbound Moffett Park Drive shifts the queuing from Moffett Park Drive to Innovation Way and Bordeaux Drive on the east side of Mathilda Avenue.



During the PM peak hour, the realignment of the SR 237 ramps would reduce the SR 237 off-ramp queue lengths, but the 95th percentile westbound off-ramp queue is anticipated to extend onto the freeway mainline. The US 101 northbound off-ramp queue would also be reduced under the Build 1 Alternative but continue to occasionally back onto the freeway mainline. Vehicle queues on the local streets are expected mostly in the southbound direction along Mathilda Avenue. However, there is a northbound queue anticipated due to the increase in northbound volume by Year 2040 in the PM peak hour that results in congestion along northbound Mathilda Avenue. Eastbound Moffett Park Drive is still anticipated to have excessive queuing as stated under No Build Conditions, and queuing along Innovation Way east of Mathilda Avenue is anticipated to remain with the closure of westbound Moffett Park Drive. Vehicle queues on southbound Mathilda Avenue and Innovation Way would still exist during the PM peak hour.

TABLE 6-3: YEAR 2040 BUILD 1 QUEUING ANALYSIS RESULTS

| Intersection | Movement ¹ | Available Storage ² | AM Peak Hour 95 th Percentile Queue (ft) | PM Peak Hour 95 th Percentile Queue (ft) |
|--|-----------------------|--------------------------------|--|--|
| 1. Mathilda Avenue / Fifth Avenue | NB-L | 425 | 125 | 125 |
| | NB-T | 1,125 | 200 | 150 |
| | SB-L | 250 | 75 | 275 |
| | SB-T | 1,325 | 175 | 3,075 |
| | SB-R | 250 | 50 | 300 |
| | EB-L | 625 | 50 | 250 |
| | EB-T | 625 | 50 | 100 |
| | EB-R | 625 | 75 | 350 |
| | WB-L | 925 | 125 | 225 |
| | WB-T | 75 | 100 | 100 |
| 2. Mathilda Avenue / Innovation Way | NB-L | 400 | 700 | 75 |
| | NB-T | 975 | 1,350 | 300 |
| | NB-TR | 975 | 1,200 | 300 |
| | SB-L | 75 | 125 | 175 |
| | SB-T | 975 | 250 | 1,250 |
| | SB-R | 225 | 250 | 350 |
| | EB-LT | 200 | 225 | 350 |
| | EB-R | 200 | 50 | 325 |
| | WB-L | 425 | 800 | 775 |
| | WB-LTR | 225 | 250 | 250 |
| 3. Mathilda Avenue / Moffett Park Drive / SR 237 Westbound Ramps | NB-L | 350 | 475 | 350 |
| | NB-T | 350 | 500 | 175 |
| | SB-T | 975 | 700 | 1,100 |
| | SB-TR | 975 | 750 | 1,150 |
| | EB-LR | 1,125 | 125 | 1,200 |
| | EB-R | 1,125 | 75 | 1,200 |
| | WB-L | 525 | 550 | 625 |
| WB-LT | 1,225 | 750 | 1,250 | |



TABLE 6-3: YEAR 2040 BUILD 1 QUEUING ANALYSIS RESULTS

| Intersection | Movement ¹ | Available Storage ² | AM Peak Hour | PM Peak Hour |
|---|-----------------------|--------------------------------|--|--|
| | | | 95 th Percentile Queue (ft) | 95 th Percentile Queue (ft) |
| 4. Mathilda Avenue / SR 237 Eastbound Ramps | WB-TR | 1,225 | 775 | 325 |
| | NB-T | 275 | 275 | 300 |
| | NB-R | 275 | 50 | 300 |
| | SB-L | 325 | 325 | 375 |
| | SB-T | 350 | 400 | 475 |
| | EB-L | 1,025 | >5,000 | 275 |
| | EB-LT | 1,025 | 1,175 | 325 |
| | EB-R | 450 | 675 | 400 |
| 5. Mathilda Avenue / Ross Drive | NB-L | 150 | 350 | 350 |
| | NB-T | 700 | 825 | 850 |
| | SB-L | 150 | 275 | 200 |
| | SB-T | 250 | 125 | 300 |
| | EB-L | 650 | 125 | 125 |
| | EB-T | 75 | 225 | 400 |
| | EB-R | 50 | 100 | 125 |
| | WB-L | 75 | 125 | 4,500 |
| 6. Mathilda Avenue / US 101 NB Ramps | WB-T | 75 | 1,575 | >5,000 |
| | WB-R | 75 | 125 | 550 |
| | NB-T | 575 | 725 | 750 |
| | NB-R | 575 | 750 | 400 |
| | SB-L | 375 | 75 | 150 |
| | SB-T | 700 | 400 | 775 |
| | WB-L | 1,025 | 1,375 | 3,650 |
| | WB-R | 1,025 | 175 | 175 |
| 7. Mathilda Avenue / US 101 SB Ramps | NB-T | 750 | 925 | 775 |
| | NB-R | 750 | 1,025 | 750 |
| | SB-T | 575 | 300 | 275 |
| | SB-TR | 575 | 325 | 450 |
| | EB-L | 1,050 | 325 | 150 |
| | EB-R | 1,050 | 25 | 125 |



TABLE 6-3: YEAR 2040 BUILD 1 QUEUING ANALYSIS RESULTS

| Intersection | Movement ¹ | Available Storage ² | AM Peak Hour | PM Peak Hour |
|--|-----------------------|--------------------------------|--|--|
| | | | 95 th Percentile Queue (ft) | 95 th Percentile Queue (ft) |
| 8. Mathilda Avenue / Almanor Avenue-Ahwanee Avenue | NB-L | 375 | 500 | 300 |
| | NB-T | 750 | >5,000 | 700 |
| | NB-R | 75 | 325 | 375 |
| | SB-L | 125 | 350 | 325 |
| | SB-T | 750 | 550 | 375 |
| | EB-L | 1,025 | 150 | 425 |
| | EB-T | 125 | 125 | 275 |
| | WB-L | 250 | 200 | 150 |
| | WB-T | 1,025 | 350 | 225 |
| 9. US 101 Northbound On- Ramp / Moffett Park Drive | WB-R | 75 | 150 | 125 |
| | EB-T | 850 | 75 | 1,075 |
| | EB-R | 150 | 25 | 500 |
| | WB-L | 850 | 75 | 225 |
| 10. Innovation Way / Moffett Park Drive | WB-T | 850 | 25 | 25 |
| | SB-L | 575 | 75 | 575 |
| | SB-LTR | 575 | 200 | 575 |
| | EB-L | 225 | 175 | 450 |
| | EB-T | 850 | 75 | 975 |
| | WB-T | 1,150 | 350 | 250 |
| 11. Innovation Way / Eleventh Avenue | WB-R | 225 | 475 | 325 |
| | NB-L | 125 | 100 | 100 |
| | NB-T | 575 | 200 | 300 |
| | SB-L | 175 | 100 | 175 |
| | SB-T | 1,000 | 75 | 125 |
| | SB-TR | 1,000 | 175 | 175 |
| | EB-L | 125 | 75 | 150 |
| | EB-LT | 300 | 50 | >5,000 |
| | EB-R | 300 | 75 | 4,925 |
| | WB-L | 325 | 50 | 175 |
| 12. Innovation Way / Juniper Driveway | WB-TR | 325 | 50 | 50 |
| | NB-L | 125 | 175 | 150 |
| | NB-T | 900 | 375 | 750 |
| | SB-T | 300 | 250 | 225 |
| | SB-R | 300 | 225 | 150 |
| | EB-L | 150 | 200 | >5,000 |
| | EB-R | 150 | 75 | >5,000 |



TABLE 6-3: YEAR 2040 BUILD 1 QUEUING ANALYSIS RESULTS

| Intersection | Movement ¹ | Available Storage ² | AM Peak Hour | PM Peak Hour |
|--|-----------------------|--------------------------------|--|--|
| | | | 95 th Percentile Queue (ft) | 95 th Percentile Queue (ft) |
| 13. Bordeaux Drive / Innovation Way | NB-L | 325 | 350 | 900 |
| | NB-TR | 2,025 | 825 | 775 |
| | SB-L | 125 | 25 | 25 |
| | SB-TR | 725 | 400 | 4,800 |
| | EB-LT | 375 | 450 | 125 |
| | EB-R | 125 | 150 | 125 |
| | WB-LT | 125 | 75 | 125 |
| | WB-R | 125 | 25 | 25 |

Notes: **Bold** denotes locations where storage length is exceeded.

1. NB-northbound, SB-southbound, EB-eastbound, WB-westbound, L-left-turn movement, T-through movement, R-right-turn movement, (MP)-turn onto/from Moffett Park Drive, (237)-turn onto/from SR 237 WB Ramps.
2. Available storage lengths are provided on a "per lane" basis. For example, an available storage of 425 means each lane in the associated movement has a storage length of 425 feet.

Source: Fehr & Peers, 2016.

Build 2 95th Percentile Queues

Table 6-4 presents the Year 2040 Build 2 peak hour 95th percentile queuing analysis results. Analysis results worksheets are presented in **Appendix O**. Similar to Build 1, capacity enhancements on Mathilda Avenue and the realignment of freeway ramps would improve traffic operations and reduce queue lengths compared to No Build condition. During the AM peak hour, 95th percentile queue spillback onto the freeway mainline is expected at the US 101 northbound off-ramp and both SR 237 off-ramps. For a diverging diamond, it is recommended that the right-turns off of the freeway ramps be phased as no right-turn on red. For the SR 237 eastbound off-ramp queue spillback is caused by this right-turn-on-red limitation and the close proximity of the Ross Drive intersection which limits the storage capacity traveling southbound on Mathilda Avenue. The right-turn-on-red limitation also causes some queue spillback at the SR 237 westbound off-ramp. The high volume of northbound traffic along Mathilda Avenue causes the queue spillback onto the freeway mainline for the left-turn movement at the SR 237 eastbound off-ramp while the right-turn movement at the SR 237 westbound off-ramp experiences queuing due to the right-turn-on-red limitations. On the local streets, overall queuing is reduced along northbound and southbound Mathilda Avenue. The closure of westbound Moffett Park Drive shifts the queuing from Moffett Park Drive to Innovation Way and Bordeaux Drive on the east side of Mathilda Avenue.

During the PM peak hour, the realignment of the SR 237 off-ramps would eliminate queue spillback onto the freeway mainline. The US 101 northbound off-ramp queue would also be reduced under the Build 2 Alternative but continue to occasionally queue back onto the freeway mainline. Vehicle queues on the local streets are expected mostly in the southbound direction along Mathilda Avenue. However, there is a northbound queuing anticipated due to the ramp metering at the SR 237 eastbound on-ramp that spills back along Mathilda Avenue. The closure of eastbound Moffett Park Drive will shift the queuing from Moffett Park Drive to Innovation Way resulting in queuing on Innovation Way west of Mathilda Avenue. Queuing along Innovation Way east of Mathilda Avenue is anticipated to remain with the closure of the



westbound Moffett Park Drive. Vehicle queues on southbound Mathilda Avenue and Innovation Way would still exist during the PM peak hour.

TABLE 6-4: YEAR 2040 BUILD 2 QUEUING ANALYSIS RESULTS

| Intersection | Movement ¹ | Available Storage ² | AM Peak Hour 95 th Percentile Queue (ft) | PM Peak Hour 95 th Percentile Queue (ft) |
|--|-----------------------|--------------------------------|--|--|
| 1: Mathilda Avenue / Fifth Avenue | NB-L | 425 | 125 | 100 |
| | NB-T | 1,150 | 175 | 150 |
| | SB-L | 225 | 100 | 250 |
| | SB-T | 1,375 | 175 | 1,175 |
| | SB-R | 225 | 50 | 225 |
| | EB-L | 625 | 75 | 300 |
| | EB-T | 625 | 75 | 250 |
| | EB-R | 625 | 100 | 300 |
| | WB-L | 925 | 100 | 250 |
| | WB-T | 75 | 75 | 100 |
| 2: Mathilda Avenue / Innovation Way | NB-L | 725 | 900 | 300 |
| | NB-T | 975 | 1,025 | 175 |
| | NB-R | 975 | 1,200 | 275 |
| | SB-L | 75 | 150 | 175 |
| | SB-T | 1,150 | 300 | 1,300 |
| | SB-R | 225 | 275 | 375 |
| | EB-LT | 200 | 300 | 350 |
| | EB-R | 200 | 50 | 300 |
| | WB-L | 425 | 800 | 800 |
| | WB-LTR | 225 | 250 | 250 |
| 3: Mathilda Avenue / Moffett Park Drive / SR 237 Westbound Ramps | NB-L | 150 | 150 | 50 |
| | NB-T | 400 | 500 | 200 |
| | SB-T | 975 | 900 | 1,175 |
| | WB-L | 1,075 | 1,125 | 450 |
| | WB-R | 550 | 675 | 225 |
| 4: Mathilda Avenue / SR 237 Eastbound Ramps | NB-T | 150 | 275 | 200 |
| | NB-R | 150 | 25 | 50 |
| | SB-L | 175 | 25 | 50 |
| | SB-T | 400 | 300 | 375 |
| | EB-L | 1,075 | >5,000 | 175 |
| | EB-R | 450 | 600 | 300 |



TABLE 6-4: YEAR 2040 BUILD 2 QUEUING ANALYSIS RESULTS

| Intersection | Movement ¹ | Available Storage ² | Peak Hour | |
|--|-----------------------|--------------------------------|--|--|
| | | | AM Peak Hour 95 th Percentile Queue (ft) | PM Peak Hour 95 th Percentile Queue (ft) |
| 5: Mathilda Avenue / Ross Drive | NB-L | 250 | 300 | 250 |
| | NB-T | 700 | 800 | 800 |
| | SB-L | 225 | 100 | 200 |
| | SB-T | 225 | 200 | 175 |
| | EB-L | 650 | 125 | 125 |
| | EB-T | 75 | 1,775 | 350 |
| | EB-R | 50 | 75 | 125 |
| | WB-L | 75 | 125 | 125 |
| | WB-T | 75 | 5,000 | >5,000 |
| 6: Mathilda Avenue / US 101 NB Ramps | WB-R | 75 | 125 | 100 |
| | NB-T | 575 | 700 | 700 |
| | NB-R | 575 | 800 | 350 |
| | SB-L | 375 | 50 | 150 |
| | SB-T | 700 | 250 | 525 |
| | WB-L | 1,025 | 1,475 | 2,475 |
| 7: Mathilda Avenue / US 101 SB Ramps | WB-R | 1,025 | 425 | 500 |
| | NB-T | 750 | 875 | 925 |
| | NB-R | 750 | 975 | 1,050 |
| | SB-T | 575 | 225 | 700 |
| | SB-TR | 575 | 275 | 700 |
| | EB-L | 1,050 | 400 | 950 |
| 8: Mathilda Avenue / Almanor Avenue-Ahwanee Avenue | EB-R | 1,050 | 25 | 50 |
| | NB-L | 375 | 575 | 550 |
| | NB-T | 675 | >5,000 | >5,000 |
| | NB-TR | 200 | 300 | 325 |
| | SB-L | 275 | 375 | 375 |
| | SB-T | 750 | 525 | 550 |
| | EB-L | 1,025 | 150 | 450 |
| | EB-T | 125 | 125 | 1,000 |
| | WB-L | 250 | 200 | 225 |
| | WB-T | 1,025 | 275 | 450 |
| 9: US 101 Northbound On-Ramp / Moffett Park Drive | WB-R | 75 | 150 | 150 |
| | EB-T | 875 | 75 | 900 |
| | EB-R | 150 | 25 | 525 |
| | WB-L | 900 | 50 | 375 |
| | WB-T | 900 | 150 | 125 |



TABLE 6-4: YEAR 2040 BUILD 2 QUEUING ANALYSIS RESULTS

| Intersection | Movement ¹ | Available Storage ² | AM Peak Hour | PM Peak Hour |
|---|-----------------------|--------------------------------|--|--|
| | | | 95 th Percentile Queue (ft) | 95 th Percentile Queue (ft) |
| 10: Innovation Way / Moffett Park Drive | SB-R | 525 | 100 | 100 |
| | EB-L | 850 | 175 | 925 |
| | WB-T | 975 | 200 | 650 |
| | WB-TR | 975 | 275 | 300 |
| 11: Innovation Way / Eleventh Avenue | NB-L | 125 | 75 | 250 |
| | NB-T | 575 | 175 | 475 |
| | SB-L | 175 | 75 | 125 |
| | SB-T | 1,000 | 100 | 75 |
| | SB-TR | 1,000 | 200 | 175 |
| | EB-L | 125 | 75 | 150 |
| | EB-LT | 300 | 50 | 3,500 |
| | EB-R | 300 | 50 | 1,325 |
| 12: Innovation Way / Juniper Driveway | WB-L | 325 | 50 | 75 |
| | WB-TR | 325 | 50 | 75 |
| | NB-L | 125 | 200 | 175 |
| | NB-T | 900 | 700 | 1,150 |
| | SB-T | 300 | 150 | 225 |
| | SB-TR | 300 | 300 | 250 |
| 13: Bordeaux Drive / Innovation Way | EB-L | 150 | 500 | >5,000 |
| | EB-R | 150 | 75 | >5,000 |
| | NB-L | 325 | 2,875 | >5,000 |
| | NB-TR | 2,025 | 1,050 | 1,000 |
| | SB-L | 125 | 25 | 25 |
| | SB-TR | 725 | 425 | 725 |
| | EB-LT | 375 | 450 | 125 |
| | EB-R | 125 | 150 | 125 |
| | WB-LT | 125 | 75 | 150 |
| | WB-R | 125 | 25 | 25 |

Notes: **Bold** denotes locations where storage length is exceeded.

1. NB-northbound, SB-southbound, EB-eastbound, WB-westbound, L-left-turn movement, T-through movement, R-right-turn movement, (MP)-turn onto/from Moffett Park Drive, (237)-turn onto/from SR 237 WB Ramps.
2. Available storage lengths are provided on a "per lane" basis. For example, an available storage of 425 means each lane in the associated movement has a storage length of 425 feet.

Source: Fehr & Peers, 2016.

MATHILDA AVENUE AND INNOVATION WAY TRAVEL TIMES

Table 6-5 presents the average travel times and delays along the Mathilda Avenue corridor under No Build and Build conditions. Both of the build alternatives would reduce the average travel time and delays on Mathilda Avenue when compared to No Build conditions. Build 1 Alternative would result in a northbound



delay reduction of just shy of 7 minutes and 6 minutes during the AM and PM peak hours, respectively. In the southbound direction, the Build 1 Alternative would reduce delays by over 8 minutes in the AM peak hour and 2 minutes during the PM peak hour.

Build 2 Alternative would result in a northbound delay reduction of over 5 minutes in the AM peak hour and roughly 30 seconds during the PM peak hour. In the southbound direction, Build 2 Alternative would reduce delays by about 10 minutes during the AM and PM peak hours.

TABLE 6-5: YEAR 2040 MATHILDA AVENUE TRAVEL TIMES

| Direction | Peak Hour | Free flow Travel Time (s) ² | No Build | | Build 1 Alternative | | Build 2 Alternative | |
|----------------------------|-----------|--|---------------------------|-----------|---------------------------|-----------|---------------------------|-----------|
| | | | Congested Travel Time (s) | Delay (s) | Congested Travel Time (s) | Delay (s) | Congested Travel Time (s) | Delay (s) |
| Mathilda Avenue Northbound | AM | 116.2 | 983.3 | 867.1 | 577.3 | 461.1 | 645.8 | 529.6 |
| | PM | 116.2 | 952.6 | 836.4 | 605.3 | 489.1 | 915.5 | 799.3 |
| Mathilda Avenue Southbound | AM | 116.2 | 954.3 | 838.1 | 437.7 | 321.5 | 362.9 | 246.7 |
| | PM | 116.2 | 1458.5 | 1342.3 | 1304.9 | 1188.7 | 834.4 | 718.2 |

Notes:

1. Travel time runs begin north of the San Aleso Avenue intersection and end south of the Lockheed Martin Way-Java Drive intersection (approximately 1.44 miles).
2. Free flow speed is calculated assuming a travel speed of 45 miles per hour.

Source: Fehr & Peers, 2016.

Table 6-6 presents the average travel times and delays along the Innovation Way corridor under No Build and Build conditions. The redistribution of traffic to this corridor under the build alternatives warrants a signal at the Innovation Way and Juniper Networks Driveway in order to increase output at that intersection as well as the Mathilda Avenue and Innovation Way intersection. Due to the implementation of a signal at Innovation Way and Juniper Networks Driveway, the average travel time and delay along Innovation Way decreases compared to No Build conditions.

The Build 1 Alternative would result in a northbound delay decrease on Innovation Way of over 4 minutes and 8 minutes during the AM and PM peak hours, respectively. In the southbound direction, Build 1 Alternative travel times would remain relatively unchanged in the AM peak hour and increase by approximately 30 seconds in the PM peak hour due to the slight increase in volume as a result of the closure of Moffett Park Drive on the east side of Mathilda Avenue under the Build 1 Alternative. Vehicles will need to use Innovation Way to travel east and west across Mathilda Avenue from Moffett Park Drive.

Build 2 Alternative would result in a northbound delay decrease of about 3 minutes and 1 minute the AM and PM peak hour, respectively. In the southbound direction, the Build 2 Alternative would decrease delay by around 15 seconds in the AM peak hour and by over 7 minutes during PM peak hour. The large decrease in delay in the southbound direction is due to the closure of eastbound Moffett Park Drive traffic under the Build 2 Alternative.



TABLE 6-6: YEAR 2040 INNOVATION WAY TRAVEL TIMES

| Direction | Peak Hour | Free flow Travel Time (s) ² | No Build | | Build 1 Alternative | | Build 2 Alternative | |
|---------------------------|-----------|--|---------------------------|-----------|---------------------------|-----------|---------------------------|-----------|
| | | | Congested Travel Time (s) | Delay (s) | Congested Travel Time (s) | Delay (s) | Congested Travel Time (s) | Delay (s) |
| Innovation Way Northbound | AM | 81.5 | 395.3 | 313.8 | 143.7 | 62.2 | 218.3 | 136.8 |
| | PM | 81.5 | 787.9 | 706.4 | 264.3 | 182.8 | 704.8 | 623.3 |
| Innovation Way Southbound | AM | 81.5 | 129.4 | 47.9 | 124.1 | 42.6 | 114.3 | 32.8 |
| | PM | 81.5 | 634.7 | 553.2 | 664.1 | 582.6 | 192.9 | 111.4 |

Notes:

1. Travel time runs begin at the Mathilda Avenue intersection and end at the Moffett Park Drive intersection (approximately 0.42 miles).
2. Free flow speed is calculated assuming a travel speed of 25 miles per hour.

Source: Fehr & Peers, 2016.

YEAR 2040 MAINLINE OPERATIONS

This section summarizes the mainline operations analysis for Year 2040 under No Build, Build 1 and Build 2 conditions using the calibrated/validated FREQ models developed under Existing Conditions. There are several projects identified in the Santa Clara Valley Transportation Plan (VTP) 2040 that could influence traffic operations on US 101 and SR 237 under Year 2040 Conditions. Below is a brief summary of the projects and how they were considered in the evaluation of the US 101 and SR 237 operations analysis under Year 2040 Conditions. (Projects assumed completed by Year 2018 are also listed and identified as such.)

- *SR 237 Express Lanes – Mathilda Avenue to SR 85:* SR 237 is expected to be widened to accommodate a HOT lane that continues from the current HOV terminus between Fair Oaks Avenue and Mathilda Avenue to the SR 85 interchange. (A conversion of the existing HOV lane to an HOT lane was assumed under Year 2018.)
- *US 101 Express Lanes – Whipple Avenue in San Mateo County to Cochrane Road in Morgan Hill (two lanes in each direction):* The addition of a second HOT lane in both directions is estimated to be completed by Year 2040. (A conversion of the existing HOV lane to one HOT lane was assumed under Year 2018.)
- *US 101 Southbound Auxiliary Lane – Ellis Street and SR 237:* An auxiliary lane is assumed to be constructed on US 101 southbound between Ellis Street on-ramp and SR 237 EB off-ramp.
- *SR 85 Express Lanes – US 101 to US 101:* The conversion of the existing HOV lanes along SR 85 to HOT lanes is anticipated to be completed by Year 2040.
- *Lawrence Expressway Ramp Improvements at SR 237:* The construction of an auxiliary lane on southbound Lawrence Expressway between the SR 237 loop ramps is anticipated to be completed by Year 2040.
- *Completed by Year 2018 – SR 237 Eastbound Auxiliary Lanes – Mathilda Avenue to Fair Oaks Avenue:* The SR 237 eastbound auxiliary lane between Mathilda Avenue and Fair Oaks Avenue is expected to be constructed by Year 2018.



- *Completed by Year 2018* – All freeway ramps metered on US 101 and SR 237 (includes widening of SR 237 EB on-ramp at Mathilda Avenue to two lanes): Ramp metering is assumed to be installed and operating at all US 101 and SR 237 on-ramps by Year 2018. As part of this project, the Mathilda Avenue to SR 237 eastbound on-ramp is assumed to extend the existing two-lane ramp and meter two mixed-flow lanes. The specific design of the SR 237 eastbound on-ramp will be determined during the design and construction phase of the ramp metering system.

As discussed above, congestion on the local street system would constrain on-ramp demand volumes at the Mathilda Avenue interchanges during the peak hours. **Table 6-7** and **Table 6-8** present the initial and constrained on-ramp volumes at the Mathilda Avenue/US 101 and Mathilda Avenue/SR 237 interchanges under the various alternatives. The initial demand volumes were replaced by the constrained volumes to determine US 101 and SR 237 traffic operations.

TABLE 6-7: YEAR 2040 AM ON-RAMP CONSTRAINED VOLUMES

| Alternative | Location from Mathilda | Initial FREQ Demand Volume | | Constrained Volume from SimTraffic (8AM-9AM) | Constrained FREQ Volume | |
|-------------|-------------------------|----------------------------|---------|--|-------------------------|---------|
| | | 7AM-8AM | 8AM-9AM | | 7AM-8AM | 8AM-9AM |
| No Build | SR 237 WB On | 290 | 390 | 268 | 200 | 268 |
| | SR 237 EB On | 730 | 1000 | 532 | 390 | 532 |
| | US 101 NB On | 420 | 570 | 254 | 190 | 254 |
| | US 101 SB On (loop) | 140 | 190 | 155 | 110 | 155 |
| | US 101 SB On (diagonal) | 510 | 700 | 328 | 240 | 328 |
| Build 1 | SR 237 WB On | 270 | 370 | 315 | 230 | 315 |
| | SR 237 EB On | 730 | 1000 | 795 | 580 | 795 |
| | US 101 NB On | 430 | 590 | 407 | 300 | 407 |
| | US 101 SB On (loop) | 140 | 190 | 169 | 120 | 169 |
| | US 101 SB On (diagonal) | 510 | 700 | 485 | 350 | 485 |
| Build 2 | SR 237 WB On | 270 | 370 | 295 | 220 | 295 |
| | SR 237 EB On | 730 | 1000 | 725 | 530 | 725 |
| | US 101 NB On | 430 | 590 | 364 | 270 | 364 |
| | US 101 SB On (loop) | 140 | 190 | 145 | 110 | 145 |
| | US 101 SB On (diagonal) | 510 | 700 | 421 | 310 | 421 |

Source: Fehr & Peers, 2016.



TABLE 6-8: YEAR 2040 PM ON-RAMP CONSTRAINED VOLUMES

| Alternative | Location from Mathilda | Initial FREQ Demand Volume | | | Constrained Volume from SimTraffic (5PM-6PM) | Constrained FREQ Volume | | |
|-------------|-------------------------|----------------------------|---------|---------|--|-------------------------|---------|---------|
| | | 4PM-5PM | 5PM-6PM | 6PM-7PM | | 4PM-5PM | 5PM-6PM | 6PM-7PM |
| No Build | SR 237 WB On | 850 | 900 | 720 | 499 | 470 | 499 | 400 |
| | SR 237 EB On | 1240 | 1320 | 1050 | 862 | 810 | 862 | 690 |
| | US 101 NB On | 320 | 340 | 270 | 202 | 190 | 202 | 160 |
| | US 101 SB On (loop) | 1380 | 1460 | 1160 | 1045 | 990 | 1045 | 830 |
| | US 101 SB On (diagonal) | 640 | 680 | 540 | 391 | 370 | 391 | 310 |
| Build 1 | SR 237 WB On | 810 | 860 | 690 | 495 | 470 | 495 | 400 |
| | SR 237 EB On | 1240 | 1320 | 1050 | 986 | 930 | 986 | 780 |
| | US 101 NB On | 360 | 380 | 300 | 332 | 310 | 332 | 260 |
| | US 101 SB On (loop) | 1380 | 1460 | 1160 | 920 | 870 | 920 | 730 |
| | US 101 SB On (diagonal) | 640 | 680 | 540 | 640 | 600 | 640 | 510 |
| Build 2 | SR 237 WB On | 810 | 860 | 690 | 587 | 550 | 587 | 470 |
| | SR 237 EB On | 1240 | 1320 | 1050 | 879 | 830 | 879 | 700 |
| | US 101 NB On | 360 | 380 | 300 | 266 | 250 | 266 | 210 |
| | US 101 SB On (loop) | 1380 | 1460 | 1160 | 948 | 900 | 948 | 750 |
| | US 101 SB On (diagonal) | 640 | 680 | 540 | 529 | 500 | 529 | 420 |

Source: Fehr & Peers, 2016.

PEAK HOUR LEVEL OF SERVICE

Table 6-9 and **Table 6-10** summarize the Year 2040 US 101 AM and PM peak hour density and LOS results, respectively, based on the FREQ model outputs. **Table 6-11** and **Table 6-12** summarize the Year 2040 SR 237 AM and PM peak hour density and LOS results, respectively, based on the FREQ model outputs. Locations in bold indicate LOS F operations. Results for the mixed-flow lanes are presented without parentheses while results for the high-occupancy toll (HOT) lanes are shown in parentheses. Detailed mainline analysis worksheets are presented in **Appendix P**. A more detailed discussion on peak hour level of service is presented after the analysis results tables.



TABLE 6-9: YEAR 2040 US 101 AM PEAK HOUR LEVEL OF SERVICE BASED ON FREQ MODEL RESULTS

| Segment | Type ¹ | # of Lanes | No Build | | Build 1 Alternative | | Build 2 Alternative | |
|--|-------------------|--------------------|-----------------------|-----------------|-----------------------|-----------------|-----------------------|-----------------|
| | | | Density ² | LOS | Density ² | LOS | Density ² | LOS |
| US 101 Northbound³ | | | | | | | | |
| Fair Oaks Off-Ramp | Diverge | 3 Mixed (2 HOT) | 80.3 (14.2) | F (B) | 78.7 (14.2) | F (B) | 78.6 (14.2) | F (B) |
| Fair Oaks Off-Ramp to Fair Oaks On-Ramp | Basic | 3 Mixed (2 HOT) | 72.5 (12.8) | F (B) | 70.9 (12.8) | F (B) | 70.8 (12.8) | F (B) |
| Fair Oaks On-Ramp | Merge | 3 Mixed (2 HOT) | 50.8 (13.7) | F (B) | 49.6 (13.7) | F (B) | 49.4 (13.7) | F (B) |
| Fair Oaks On-Ramp to Mathilda NB Off Ramp | Basic | 3 Mixed (2 HOT) | 53.7 (13.7) | F (B) | 52.4 (13.7) | F (B) | 52.3 (13.7) | F (B) |
| Mathilda NB Off-Ramp | Diverge | 3 Mixed (2 HOT) | 54.6 (13.7) | F (B) | 57.0 (13.7) | F (B) | 56.7 (13.7) | F (B) |
| Mathilda NB Off-Ramp to Mathilda NB On-Ramp | Basic | 3 Mixed (2 HOT) | 59.4 (12.8) | F (B) | 62.7 (12.0) | F (B) | 62.4 (12.0) | F (B) |
| Mathilda NB On-Ramp | Merge | 3 Mixed (2 HOT) | 59.9 (13.0) | F (B) | 62.9 (12.3) | F (B) | 62.8 (12.3) | F (B) |
| Mathilda NB On-Ramp to Mathilda SB Off-Ramp ⁵ | Basic | 3 Mixed (2 HOT) | 60.5 (13.0) | F (B) | 63.9 (12.3) | F (B) | 63.7 (12.3) | F (B) |
| Mathilda SB Off-Ramp ⁶ | Diverge | 3 Mixed (2 HOT) | 59.3 (13.0) | F (B) | N/A | N/A | N/A | N/A |
| Mathilda SB Off-Ramp to SR 237 WB Off-Ramp ⁶ | Basic | 3 Mixed (2 HOT) | 64.4 (12.2) | F (B) | N/A | N/A | N/A | N/A |
| SR 237 WB Off-Ramp | Diverge | 3 Mixed (2 HOT) | 65.0 (12.2) | F (B) | 66.0 (12.3) | F (B) | 66.0 (12.3) | F (B) |
| SR 237 WB Off-Ramp to SR 237 WB On-Ramp | Basic | 3 Mixed (2 HOT) | 80.3 (10.5) | F (A) | 81.7 (10.6) | F (A) | 81.5 (10.6) | F (A) |
| SR 237 WB On-Ramp | Merge | 3 Mixed (2 HOT) | 68.3 (12.5) | F (B) | 69.3 (12.6) | F (B) | 69.2 (12.5) | F (B) |
| SR 237 WB On-Ramp to Ellis | Basic | 3 Mixed (2 HOT) | 75.7 (12.5) | F (B) | 76.7 (12.6) | F (B) | 76.5 (12.5) | F (B) |



TABLE 6-9: YEAR 2040 US 101 AM PEAK HOUR LEVEL OF SERVICE BASED ON FREQ MODEL RESULTS

| Segment | Type ¹ | # of Lanes | No Build | | Build 1 Alternative | | Build 2 Alternative | |
|---|-------------------|---------------------------|----------------------|----------|----------------------|----------|----------------------|----------|
| | | | Density ² | LOS | Density ² | LOS | Density ² | LOS |
| US 101 Southbound⁴ | | | | | | | | |
| Ellis On-Ramp to SR 237 EB Off-Ramp | Weave | 3 Mixed, 1 AUX (2 HOT) | 21.3 (8.5) | C (A) | 21.3 (8.5) | C (A) | 21.3 (8.5) | C (A) |
| SR 237 EB Off-Ramp | Diverge | 3 Mixed, 1 AUX (2 HOT) | 21.3 (8.5) | C (A) | 21.3 (8.5) | C (A) | 21.3 (8.5) | C (A) |
| SR 237 EB Off-Ramp to SR 237 EB On-Ramp | Basic | 3 Mixed (2 HOT) | 18.6 (5.7) | C (A) | 19.8 (6.0) | C (A) | 19.8 (6.0) | C (A) |
| SR 237 EB On-Ramp | Merge | 3 Mixed, 1 AUX (2 HOT) | 17.4 (6.9) | B (A) | 18.3 (7.2) | C (A) | 18.3 (7.2) | C (A) |
| SR 237 EB On-Ramp to Mathilda Off-Ramp | Weave | 3 Mixed, 1 AUX (2 HOT) | 17.4 (6.9) | B (A) | 18.3 (7.2) | C (A) | 18.3 (7.2) | C (A) |
| Mathilda Off-Ramp | Diverge | 3 Mixed, 1 AUX (2 HOT) | 17.4 (6.9) | B (A) | 18.3 (7.2) | C (A) | 18.3 (7.2) | C (A) |
| Mathilda Off-Ramp to Mathilda SB On-Ramp | Basic | 3 Mixed (2 HOT) | 21.2 (6.5) | C (A) | 21.2 (6.5) | C (A) | 21.2 (6.5) | C (A) |
| Mathilda SB On-Ramp | Merge | 3 Mixed (2 HOT) | 21.7 (6.6) | C (A) | 21.7 (6.6) | C (A) | 21.7 (6.6) | C (A) |
| Mathilda NB On-Ramp | Merge | 3 Mixed (2 HOT) | 23.0 (6.9) | C (A) | 23.6 (7.0) | C (A) | 23.3 (7.0) | C (A) |
| Mathilda NB On-Ramp to Fair Oaks SB Off-Ramp | Basic | 3 Mixed (2 HOT) | 23.0 (6.9) | C (A) | 23.5 (7.0) | C (A) | 23.3 (7.0) | C (A) |
| Fair Oaks SB Off-Ramp | Diverge | 3 Mixed (2 HOT) | 23.0 (6.9) | C (A) | 23.6 (7.0) | C (A) | 23.3 (7.0) | C (A) |
| Fair Oaks SB Off-Ramp to Fair Oaks SB On-Ramp | Basic | 3 Mixed (2 HOT) | 21.4 (6.6) | C (A) | 21.8 (6.8) | C (A) | 21.6 (6.7) | C (A) |
| Fair Oaks SB On-Ramp | Merge | 3 Mixed, 1 AUX (2 HOT) | 16.8 (6.9) | B (A) | 17.2 (7.1) | B (A) | 17.0 (7.0) | B (A) |
| Fair Oaks NB Off-Ramp | Diverge | 3 Mixed, 1 AUX (2 HOT) | 16.8 (6.9) | B (A) | 17.2 (7.1) | B (A) | 17.0 (7.0) | B (A) |



TABLE 6-9: YEAR 2040 US 101 AM PEAK HOUR LEVEL OF SERVICE BASED ON FREQ MODEL RESULTS

| Segment | Type ¹ | # of Lanes | No Build | | Build 1 Alternative | | Build 2 Alternative | |
|---|-------------------|--------------------|----------------------|----------|----------------------|----------|----------------------|----------|
| | | | Density ² | LOS | Density ² | LOS | Density ² | LOS |
| Fair Oaks NB Off-Ramp to Fair Oaks NB On-Ramp | Basic | 3 Mixed (2 HOT) | 22.0 (6.8) | C (A) | 22.7 (7.0) | C (A) | 22.3 (6.9) | C (A) |
| Fair Oaks NB On-Ramp | Merge | 3 Mixed (2 HOT) | 25.5 (7.6) | C (A) | 26.2 (7.8) | D (A) | 25.9 (7.7) | C (A) |

Note: **Bold** font indicates LOS F conditions.

Locations marked with an asterisk () designate the end of bottleneck congestion. A segment may be designated LOS F even if the density is below the LOS F threshold if any portion of the segment is in queue.

1. Merge, diverge, and weave segments were not calculated differently from basic segments. All results are based on the density produced from FREQ. Weaving segments are further evaluated in the Mainline Weaving Analysis section of this report.
2. Density and LOS results shown as: mixed-flow lanes (HOT lane).
3. The AM peak hour for US 101 Northbound occurs between 7:00am and 8:00am.
4. The AM peak hour for US 101 Southbound occurs between 7:00am and 8:00am.
5. Due to the closure of the US 101 northbound loop off-ramp to southbound Mathilda Avenue, this freeway segment is assumed to extend from the Mathilda Avenue loop on-ramp to SR 237 westbound off-ramp.
6. These segments do not exist under both Build Alternatives due to the closure of the US 101 northbound loop off-ramp to southbound Mathilda Avenue.

Source: Fehr & Peers, 2016.



TABLE 6-10: YEAR 2040 US 101 PM PEAK HOUR LEVEL OF SERVICE BASED ON FREQ MODEL RESULTS

| Segment | Type ¹ | # of Lanes | No Build | | Build 1 Alternative | | Build 2 Alternative | |
|--|-------------------|--------------------|-----------------------|-----------------|-----------------------|-----------------|-----------------------|-----------------|
| | | | Density ² | LOS | Density ² | LOS | Density ² | LOS |
| US 101 Northbound³ | | | | | | | | |
| Fair Oaks Off-Ramp | Diverge | 3 Mixed (2 HOT) | 38.6* (6.7) | F (A) | 45.0 (6.7) | F (A) | 40.5 (6.7) | F (A) |
| Fair Oaks Off-Ramp to Fair Oaks On-Ramp | Basic | 3 Mixed (2 HOT) | 49.3 (5.7) | F (A) | 54.8 (5.7) | F (A) | 50.7 (5.7) | F (A) |
| Fair Oaks On-Ramp | Merge | 3 Mixed (2 HOT) | 58.1 (6.1) | F (A) | 62.4 (6.1) | F (A) | 59.0 (6.0) | F (A) |
| Fair Oaks On-Ramp to Mathilda NB Off Ramp | Basic | 3 Mixed (2 HOT) | 66.7 (6.1) | F (A) | 71.0 (6.1) | F (A) | 67.5 (6.0) | F (A) |
| Mathilda NB Off-Ramp | Diverge | 3 Mixed (2 HOT) | 74.1 (6.1) | F (A) | 85.3 (6.1) | F (A) | 81.0 (6.0) | F (A) |
| Mathilda NB Off-Ramp to Mathilda NB On-Ramp | Basic | 3 Mixed (2 HOT) | 87.9 (5.8) | F (A) | 119.8 (4.8) | F (A) | 114.5 (4.8) | F (A) |
| Mathilda NB On-Ramp | Merge | 3 Mixed (2 HOT) | 89.3 (5.9) | F (A) | 123.1 (5.1) | F (A) | 118.3 (5.0) | F (A) |
| Mathilda NB On-Ramp to Mathilda SB Off-Ramp ⁵ | Basic | 3 Mixed (2 HOT) | 90.7 (5.9) | F (A) | 126.0 (5.1) | F (A) | 121.0 (5.0) | F (A) |
| Mathilda SB Off-Ramp ⁶ | Diverge | 3 Mixed (2 HOT) | 88.0 (5.9) | F (A) | N/A | N/A | N/A | N/A |
| Mathilda SB Off-Ramp to SR 237 WB Off-Ramp ⁶ | Basic | 3 Mixed (2 HOT) | 116.4 (5.0) | F (A) | N/A | N/A | N/A | N/A |
| SR 237 WB Off-Ramp | Diverge | 3 Mixed (2 HOT) | 131.1 (5.0) | F (A) | 149.0 (5.1) | F (A) | 143.9 (5.0) | F (A) |
| SR 237 WB Off-Ramp to SR 237 WB On-Ramp | Basic | 3 Mixed (2 HOT) | 198.9 (4.0) | F (A) | 220.9 (4.1) | F (A) | 216.1 (4.0) | F (A) |
| SR 237 WB On-Ramp | Merge | 3 Mixed (2 HOT) | 154.9 (5.8) | F (A) | 156.8 (5.9) | F (A) | 156.4 (5.8) | F (A) |
| SR 237 WB On-Ramp to Ellis | Basic | 3 Mixed (2 HOT) | 169.8 (5.8) | F (A) | 170.1 (5.9) | F (A) | 169.7 (5.8) | F (A) |



TABLE 6-10: YEAR 2040 US 101 PM PEAK HOUR LEVEL OF SERVICE BASED ON FREQ MODEL RESULTS

| Segment | Type ¹ | # of Lanes | No Build | | Build 1 Alternative | | Build 2 Alternative | |
|---|-------------------|---------------------------|------------------------|-----------------|------------------------|-----------------|------------------------|-----------------|
| | | | Density ² | LOS | Density ² | LOS | Density ² | LOS |
| US 101 Southbound⁴ | | | | | | | | |
| Ellis On-Ramp to SR 237 EB Off-Ramp | Weave | 3 Mixed, 1 AUX (2 HOT) | 112.7 (13.9) | F (B) | 117.4 (13.9) | F (B) | 114.6 (13.9) | F (B) |
| SR 237 EB Off-Ramp | Diverge | 3 Mixed, 1 AUX (2 HOT) | 95.6 (13.9) | F (B) | 101.4 (13.9) | F (B) | 98.7 (13.9) | F (B) |
| SR 237 EB Off-Ramp to SR 237 EB On-Ramp | Basic | 3 Mixed (2 HOT) | 172.6 (10.8) | F (A) | 174.6 (11.0) | F (B) | 170.9 (11.0) | F (B) |
| SR 237 EB On-Ramp | Merge | 3 Mixed, 1 AUX (2 HOT) | 139.3 (11.8) | F (B) | 146.9 (12.0) | F (B) | 144.1 (12.0) | F (B) |
| SR 237 EB On-Ramp to Mathilda Off-Ramp | Weave | 3 Mixed, 1 AUX (2 HOT) | 144.8 (11.8) | F (B) | 152.2 (12.0) | F (B) | 149.4 (12.0) | F (B) |
| Mathilda Off-Ramp | Diverge | 3 Mixed, 1 AUX (2 HOT) | 138.7 (11.8) | F (B) | 145.0 (12.0) | F (B) | 142.3 (12.0) | F (B) |
| Mathilda Off-Ramp to Mathilda SB On-Ramp | Basic | 3 Mixed (2 HOT) | 170.2 (10.7) | F (A) | 177.3 (10.7) | F (A) | 173.6 (10.7) | F (A) |
| Mathilda SB On-Ramp | Merge | 3 Mixed (2 HOT) | 122.2 (12.1) | F (B) | 135.0 (11.9) | F (B) | 130.0 (12.0) | F (B) |
| Mathilda NB On-Ramp | Merge | 3 Mixed (2 HOT) | 116.4 (12.7) | F (B) | 114.9 (12.8) | F (B) | 115.3 (12.7) | F (B) |
| Mathilda NB On-Ramp to Fair Oaks SB Off-Ramp | Basic | 3 Mixed (2 HOT) | 120.4 (12.7) | F (B) | 121.4 (12.8) | F (B) | 120.7 (12.7) | F (B) |
| Fair Oaks SB Off-Ramp | Diverge | 3 Mixed (2 HOT) | 115.0 (12.7) | F (B) | 115.9 (12.8) | F (B) | 115.2 (12.7) | F (B) |
| Fair Oaks SB Off-Ramp to Fair Oaks SB On-Ramp | Basic | 3 Mixed (2 HOT) | 143.1 (11.9) | F (B) | 144.0 (12.1) | F (B) | 143.3 (12.0) | F (B) |
| Fair Oaks SB On-Ramp | Merge | 3 Mixed, 1 AUX (2 HOT) | 107.3 (12.4) | F (B) | 108.0 (12.6) | F (B) | 107.5 (12.5) | F (B) |
| Fair Oaks NB Off-Ramp | Diverge | 3 Mixed, 1 AUX (2 HOT) | 108.8 (12.4) | F (B) | 109.4 (12.6) | F (B) | 108.9 (12.5) | F (B) |



TABLE 6-10: YEAR 2040 US 101 PM PEAK HOUR LEVEL OF SERVICE BASED ON FREQ MODEL RESULTS

| Segment | Type ¹ | # of Lanes | No Build | | Build 1 Alternative | | Build 2 Alternative | |
|---|-------------------|--------------------|------------------------|-----------------|------------------------|-----------------|------------------------|-----------------|
| | | | Density ² | LOS | Density ² | LOS | Density ² | LOS |
| Fair Oaks NB Off-Ramp to Fair Oaks NB On-Ramp | Basic | 3 Mixed (2 HOT) | 139.8 (12.2) | F (B) | 140.7 (12.3) | F (B) | 140.0 (12.2) | F (B) |
| Fair Oaks NB On-Ramp | Merge | 3 Mixed (2 HOT) | 128.3 (12.6) | F (B) | 129.1 (12.7) | F (B) | 128.5 (12.6) | F (B) |

Note: **Bold** font indicates LOS F conditions.

Locations marked with an asterisk () designate the end of bottleneck congestion. A segment may be designated LOS F even if the density is below the LOS F threshold if any portion of the segment is in queue.

1. Merge, diverge, and weave segments were not calculated differently from basic segments. All results are based on the density produced from FREQ. Weaving segments are further evaluated in the Mainline Weaving Analysis section of this report.
2. Density and LOS results shown as: mixed-flow lanes (HOT lane).
3. The PM peak hour for US 101 Northbound occurs between 5:00pm and 6:00pm.
4. The PM peak hour for US 101 Southbound occurs between 5:00pm and 6:00pm.
5. Due to the closure of the US 101 northbound loop off-ramp to southbound Mathilda Avenue, this freeway segment is assumed to extend from the Mathilda Avenue loop on-ramp to SR 237 westbound off-ramp.
6. These segments do not exist under both Build Alternatives due to the closure of the US 101 northbound loop off-ramp to southbound Mathilda Avenue.

Source: Fehr & Peers, 2016.



TABLE 6-11: YEAR 2040 SR 237 AM PEAK HOUR LEVEL OF SERVICE BASED ON FREQ MODEL RESULTS

| Segment | Type ¹ | # of Lanes | No Build | | Build 1 Alternatives | | Build 2 Alternative | |
|---|-------------------|---------------------------|-----------------------|-----------------|-----------------------|-----------------|-----------------------|-----------------|
| | | | Density ² | LOS | Density ² | LOS | Density ² | LOS |
| SR 237 Westbound³ | | | | | | | | |
| Lawrence On-Ramp to Crossman On-Ramp | Basic | 2 Mixed (1 HOT) | 94.6 (22.7) | F (C) | 94.6 (22.7) | F (C) | 94.6 (22.7) | F (C) |
| Crossman On-Ramp | Merge | 2 Mixed (1 HOT) | 38.2 (23.6) | E (C) | 38.2 (23.6) | E (C) | 38.2 (23.6) | E (C) |
| Crossman On-Ramp to Mathilda Off-Ramp | Basic | 2 Mixed (1 HOT) | 37.3 (23.6) | E (C) | 37.3 (23.6) | E (C) | 37.3 (23.6) | E (C) |
| Mathilda Off-Ramp | Diverge | 2 Mixed (1 HOT) | 21.2 (23.6) | C (C) | 21.2 (23.6) | C (C) | 21.2 (23.6) | C (C) |
| Mathilda Off-Ramp to Mathilda On-Ramp | Basic | 2 Mixed (1 HOT) | 25.6 (19.1) | C (C) | 25.6 (19.1) | C (C) | 25.6 (19.1) | C (C) |
| Mathilda On-Ramp to US 101 NB Off-Ramp | Weave | 2 Mixed/1 AUX (1 HOT) | 17.8 (19.6) | B (C) | 17.9 (19.6) | B (C) | 17.9 (19.6) | B (C) |
| US 101 NB Off-Ramp to US 101 NB On-Ramp | Basic | 2 Mixed (1 HOT) | 17.8 (13.7) | B (B) | 18.0 (13.8) | B (B) | 17.9 (13.8) | B (B) |
| US 101 NB On-Ramp | Merge | 2 Mixed (1 HOT) | 22.1 (15.9) | C (B) | 22.3 (16.1) | C (B) | 22.3 (16.0) | C (B) |
| Maude Off-Ramp | Diverge | 2 Mixed (1 HOT) | 22.1 (15.9) | C (B) | 22.3 (16.1) | C (B) | 22.3 (16.0) | C (B) |
| SR 237 Eastbound⁴ | | | | | | | | |
| Maude On-Ramp to US 101 SB Off-Ramp | Weave | 2 Mixed, 1 AUX (1 HOT) | 20.9 (19.4) | C (C) | 20.6 (19.5) | C (C) | 20.9 (19.5) | C (C) |
| US 101 SB Off-Ramp to US 101 SB On-Ramp | Basic | 2 Mixed (1 HOT) | 21.6 (13.8) | C (B) | 21.0 (13.7) | C (B) | 21.5 (13.9) | C (B) |
| US 101 SB On-Ramp | Merge | 2 Mixed, 1 AUX (1 HOT) | 22.9 (20.6) | C (C) | 22.5 (20.5) | C (C) | 23.0 (20.0) | C (C) |
| US 101 SB On-Ramp to Mathilda Off-Ramp | Weave | 2 Mixed, 1 AUX (1 HOT) | 22.9 (20.6) | C (C) | 22.5 (20.5) | C (C) | 23.0 (20.0) | C (C) |
| Mathilda Off-Ramp | Diverge | 2 Mixed, 1 AUX (1 HOT) | 22.9 (20.6) | C (C) | 22.5 (20.5) | C (C) | 23.0 (20.0) | C (C) |



TABLE 6-11: YEAR 2040 SR 237 AM PEAK HOUR LEVEL OF SERVICE BASED ON FREQ MODEL RESULTS

| Segment | Type ¹ | # of Lanes | No Build | | Build 1 Alternatives | | Build 2 Alternative | |
|---------------------------------------|-------------------|--------------------|----------------------|----------|----------------------|----------|----------------------|----------|
| | | | Density ² | LOS | Density ² | LOS | Density ² | LOS |
| Mathilda Off-Ramp to Mathilda On-Ramp | Basic | 2 Mixed (1 HOT) | 26.9 (17.9) | D (B) | 28.9 (18.5) | D (C) | 30.0 (18.0) | D (B) |
| Mathilda On-Ramp | Merge | 2 Mixed (1 HOT) | 19.8 (19.7) | C (C) | 21.7 (21.2) | C (C) | 22.0 (20.5) | C (C) |
| Mathilda On-Ramp to Persian Off-Ramp | Basic | 2 Mixed (1 HOT) | 19.8 (19.7) | C (C) | 21.7 (21.2) | C (C) | 22.0 (20.5) | C (C) |
| Persian Off-Ramp to Lawrence | Diverge | 2 Mixed (1 HOT) | 27.8 (18.9) | D (C) | 32.0 (20.3) | D (C) | 32.7 (19.6) | D (C) |

Note: **Bold** font indicates LOS F conditions.

Locations marked with an asterisk () designate the end of bottleneck congestion. A segment may be designated LOS F even if the density is below the LOS F threshold if any portion of the segment is in queue.

* Results are preliminary and subject to change pending FREQ model evaluation

1. Merge, diverge, and weave segments were not calculated differently from basic segments. All results are based on the density produced from FREQ. Weaving segments are further evaluated in the Mainline Weaving Analysis section of this report.
2. Density and LOS results shown as: mixed-flow lanes (HOT lane).
3. The AM peak hour for SR 237 Westbound occurs between 7:00am and 8:00am.
4. The AM peak hour for SR 237 Eastbound occurs between 8:00am and 9:00am.

Source: Fehr & Peers, 2016.



TABLE 6-12: YEAR 2040 SR 237 PM PEAK HOUR LEVEL OF SERVICE BASED ON FREQ MODEL RESULTS

| Segment | Type ¹ | # of Lanes | No Build | | Build 1 Alternatives | | Build 2 Alternative | |
|---|-------------------|---------------------------|------------------------|-----------------|------------------------|-----------------|------------------------|-----------------|
| | | | Density ² | LOS | Density ² | LOS | Density ² | LOS |
| SR 237 Westbound³ | | | | | | | | |
| Lawrence On-Ramp to Crossman On-Ramp | Basic | 2 Mixed (1 HOT) | 110.8 (12.0) | F (B) | 110.8 (12.0) | F (B) | 110.8 (12.0) | F (B) |
| Crossman On-Ramp | Merge | 2 Mixed (1 HOT) | 38.3 (12.8) | E (B) | 38.3 (12.8) | E (B) | 38.3 (12.8) | E (B) |
| Crossman On-Ramp to Mathilda Off-Ramp | Basic | 2 Mixed (1 HOT) | 37.6 (12.8) | E (B) | 37.7 (12.8) | E (B) | 37.7 (12.8) | E (B) |
| Mathilda Off-Ramp | Diverge | 2 Mixed (1 HOT) | 21.2 (12.8) | C (B) | 21.3 (12.8) | C (B) | 21.3 (12.8) | C (B) |
| Mathilda Off-Ramp to Mathilda On-Ramp | Basic | 2 Mixed (1 HOT) | 24.4 (10.0) | C (A) | 24.4 (10.0) | C (A) | 24.4 (10.0) | C (A) |
| Mathilda On-Ramp to US 101 NB Off-Ramp | Weave | 2 Mixed, 1 AUX (1 HOT) | 18.8 (10.7) | C (A) | 18.8 (10.6) | C (A) | 19.2 (10.7) | C (A) |
| US 101 NB Off-Ramp to US 101 NB On-Ramp | Basic | 2 Mixed (1 HOT) | 17.7 (7.3) | B (A) | 17.5 (7.2) | B (A) | 18.0 (7.4) | C (A) |
| US 101 NB On-Ramp | Merge | 2 Mixed (1 HOT) | 24.4 (9.3) | C (A) | 24.2 (9.1) | C (A) | 24.7 (9.3) | C (A) |
| Maude Off-Ramp | Diverge | 2 Mixed (1 HOT) | 24.4 (9.3) | C (A) | 24.2 (9.1) | C (A) | 24.7 (9.3) | C (A) |
| SR 237 Eastbound⁴ | | | | | | | | |
| Maude On-Ramp to US 101 SB Off-Ramp | Weave | 2 Mixed, 1 AUX (1 HOT) | 127.7 (16) | F (B) | 115.3 (16.0) | F (B) | 99.6 (16.0) | F (B) |
| US 101 SB Off-Ramp to US 101 SB On-Ramp | Basic | 2 Mixed (1 HOT) | 183.3 (13.0) | F (B) | 164.3 (13.0) | F (B) | 142.1 (13.0) | F (B) |
| US 101 SB On-Ramp | Merge | 2 Mixed, 1 AUX (1 HOT) | 145.4 (17.1) | F (B) | 136.6 (16.8) | F (B) | 121.1 (16.8) | F (B) |
| US 101 SB On-Ramp to Mathilda Off-Ramp | Weave | 2 Mixed, 1 AUX (1 HOT) | 161.1 (17.1) | F (B) | 158.2 (16.8) | F (B) | 141.6 (16.8) | F (B) |
| Mathilda Off-Ramp | Diverge | 2 Mixed, 1 AUX (1 HOT) | 157.8 (17.1) | F (B) | 159.6 (16.8) | F (B) | 151.3 (16.8) | F (B) |



TABLE 6-12: YEAR 2040 SR 237 PM PEAK HOUR LEVEL OF SERVICE BASED ON FREQ MODEL RESULTS

| Segment | Type ¹ | # of Lanes | No Build | | Build 1 Alternatives | | Build 2 Alternative | |
|---------------------------------------|-------------------|--------------------|------------------------|-----------------|------------------------|-----------------|------------------------|-----------------|
| | | | Density ² | LOS | Density ² | LOS | Density ² | LOS |
| Mathilda Off-Ramp to Mathilda On-Ramp | Basic | 2 Mixed (1 HOT) | 171.8 (16.0) | F (B) | 169.3 (15.9) | F (B) | 164.1 (15.9) | F (B) |
| Mathilda On-Ramp | Merge | 2 Mixed (1 HOT) | 144.0 (18.5) | F (C) | 137.7 (18.7) | F (C) | 138.4 (18.4) | F (C) |
| Mathilda On-Ramp to Persian Off-Ramp | Basic | 2 Mixed (1 HOT) | 107.9 (18.5) | F (C) | 102.4 (18.7) | F (C) | 102.0 (18.4) | F (C) |
| Persian Off-Ramp to Lawrence | Diverge | 2 Mixed (1 HOT) | 148.6 (18.0) | F (B) | 142.8 (18.0) | F (C) | 142.1 (17.7) | F (B) |

Note: **Bold** font indicates LOS F conditions.

Locations marked with an asterisk () designate the end of bottleneck congestion. A segment may be designated LOS F even if the density is below the LOS F threshold if any portion of the segment is in queue.

1. Merge, diverge, and weave segments were not calculated differently from basic segments. All results are based on the density produced from FREQ. Weaving segments are further evaluated in the Mainline Weaving Analysis section of this report.
2. Density and LOS results shown as: mixed-flow lanes (HOT lane).
3. The PM peak hour for SR 237 Westbound occurs between 5:00pm and 6:00pm.
4. The PM peak hour for SR 237 Eastbound occurs between 5:00pm and 6:00pm.

Source: Fehr & Peers, 2016.



US 101 Northbound

AM Peak Hour

Under No Build conditions, the existing bottleneck north of the study area at the SR 85 and Shoreline Boulevard ramps would continue to worsen. The bottleneck results in upstream queuing that extends beyond the extents of the study segments. The study segments in queue would operate at LOS F. The northbound HOT lane is anticipated to operate at LOS A/B during the AM peak hour.

New bottlenecks are not anticipated to develop under the Build Alternatives. The general purpose lanes are anticipated to operate at the same level of service as No Build (LOS F) under both Build Alternatives. The northbound HOT lane is anticipated to operate at LOS A/B during the AM peak hour under the Build Alternatives.

PM Peak Hour

During the PM peak hour, a bottleneck would develop north of the study area at the SR 85 and Shoreline Boulevard ramps. This bottleneck exists for No Build and Build conditions. The bottleneck results in upstream queuing that extends throughout the study segments. The northbound HOT lane is anticipated to operate at LOS A during the PM peak hour.

Additional bottlenecks are not anticipated to develop under the Build Alternatives. The general purpose lanes are anticipated to operate at the same level of service as No Build (LOS F) under both Build Alternatives. The US 101 northbound results indicate an increase in travel time and mainline vehicle delay with both Build Alternatives. This increase is due to the increase in demand served at the ramp terminal intersection. Under the No Build Alternative, congestion along Mathilda Avenue prevents vehicles from accessing the US 101 northbound on-ramp. However, with both Build Alternatives, more of the demand volume is able to access the ramp, resulting in additional traffic entering US 101 northbound. The northbound HOT lane is anticipated to operate at LOS A during the PM peak hour under the Build Alternatives.

US 101 Southbound

AM Peak Hour

During the AM peak hour, there are no bottlenecks estimated to develop within the study area or spill back into the study area on US 101 southbound. The general purpose lanes operate at LOS B/C throughout the network under No Build conditions. The southbound HOT lane is anticipated to operate at LOS A during the AM peak hour.

New bottlenecks are not anticipated to develop under the Build Alternatives. Most of the general purpose lanes are anticipated to operate at the same level of service as No Build (LOS B/C) under both Build Alternatives. There are slight increases in level of service from LOS B to LOS C under both Build Alternatives between the SR 237 on-ramp and the Mathilda Avenue off-ramp, however, the change in density associated



with these LOS changes is less than one passenger car per hour per lane. The southbound HOT lane is anticipated to operate at LOS A during the AM peak hour under the Build Alternatives.

PM Peak Hour

Under No Build conditions, the existing bottleneck south of the study area at the De La Cruz Boulevard and SR 87 ramps would continue to worsen. The bottleneck results in upstream queuing that extends beyond the extents of the study segments. The study segments in queue would operate at LOS F. The southbound HOT lane is anticipated to operate at LOS A/B during the PM peak hour.

New bottlenecks are not anticipated to develop under the Build Alternatives. The general purpose lanes are anticipated to operate at the same level of service as No Build (LOS F) under both Build Alternatives. There are increases in density of southbound general purpose lanes south of the Mathilda Avenue interchange due to the shift in demand from SR 237 to US 101 and due to the increase in demand served at the ramp terminal intersection. The southbound HOT lane is anticipated to operate at LOS A/B during the PM peak hour under the Build Alternatives.

SR 237 Westbound

AM Peak Hour

Under No Build conditions, a bottleneck would develop at the Mathilda Avenue off-ramp operating at LOS E and would continue to worsen to LOS F at the Fair Oaks Avenue / Crossman Avenue on-ramp (this bottleneck occurs upstream of the current bottleneck at the US 101 northbound off-ramp) that would spill back beyond the study segments. The study segments in queue would operate at LOS E/F and are anticipated to operate at LOS B/C downstream of the Mathilda Avenue off-ramp. The westbound HOT lane is anticipated to operate at LOS B/C.

Additional bottlenecks are not anticipated to develop under the Build Alternatives. The general purpose lanes west of the bottleneck are anticipated to operate at the same level of service as No Build (LOS B/C) under both Build Alternatives. The westbound HOT lane is anticipated to operate at LOS B/C during the AM peak hour under the Build Alternatives.

PM Peak Hour

Under No Build conditions, a bottleneck would develop at the Mathilda Avenue off-ramp operating at LOS E and would continue to worsen to LOS F at the Fair Oaks Avenue / Crossman Avenue on-ramp (this bottleneck occurs upstream of the current bottleneck at the Mathilda Avenue off-ramp) and spills back beyond the study segments. The study segments in queue would operate at LOS E/F and are anticipated to operate at LOS B/C downstream of the Fair Oaks Avenue on-ramp. The westbound HOT lane is anticipated to operate at LOS A/B during the PM peak hour.

Additional bottlenecks are not anticipated to develop under the Build Alternatives. The general purpose lanes are anticipated to operate at the same level of service as No Build under both Build Alternatives. The



westbound HOT lane is anticipated to operate at LOS A/B during the PM peak hour under the Build Alternatives.

SR 237 Eastbound

AM Peak Hour

During the AM peak hour, there are no bottlenecks estimated to develop within the study area or spill back into the study area on SR 237 eastbound. The general purpose lanes operate at LOS C/D throughout the network under No Build conditions. The eastbound HOT lane is anticipated to operate at LOS B/C during the AM peak hour.

New bottlenecks are not anticipated to develop under the Build Alternatives. The general purpose lanes are anticipated to operate at approximately the same level of service as No Build (LOS C/D) under both Build Alternatives. The eastbound HOT lane is anticipated to operate at LOS B/C during the AM peak hour under the Build Alternatives. There is a slight increase in density east of the Mathilda Avenue on-ramp. Due to the increase in demand served along Mathilda Avenue, more vehicles are able to access the freeway on-ramp and an additional number of vehicles are estimated to enter the freeway under Build Conditions. This shift in traffic does not adversely affect the results of the freeway LOS results.

PM Peak Hour

Under No Build conditions, a bottleneck would develop east of the study area that most likely is due to the queue spillback from the I-880 ramps. The bottleneck results in upstream queuing that extends beyond the extents of the study network (LOS F). The study segments in queue would operate at LOS F. The eastbound HOT lane is anticipated to operate at LOS B/C during the PM peak hour.

New bottlenecks are not anticipated to develop under the Build Alternatives. The general purpose lanes are anticipated to operate at approximately the same level of service as No Build (LOS F) under both Build Alternatives. The general purpose lane density is anticipated to be slightly less for both Build Alternatives compared to the No Build Alternative due to the shift in traffic access northbound Mathilda Avenue from SR 237 to US 101. The eastbound HOT lane is anticipated to operate at LOS B/C during the PM peak hour under the Build Alternatives.

FREEWAY SYSTEM PERFORMANCE

Year 2040 peak hour system-wide MOEs for the US 101 and SR 237 study corridors are presented in **Table 6-13** and **Table 6-14** for the peak hour and peak period, respectively. These MOEs reflect the overall US 101 operations between the Fair Oaks Avenue and the Ellis Street interchanges and SR 237 operations between the Fair Oaks Avenue and Maude Avenue interchanges. MOEs including average travel time and average speed are the most informative as they relate directly to the traveler experience on US 101 and SR 237 through the corridor. Detailed analysis worksheets are presented in **Appendix P**.



Due to the nature of the project, local street demand served will increase with the project and will put more traffic on the ramps as a result. The increase in on-ramp volume produces some additional delay along the SR 237 eastbound network as see in **Table 6-13** and **Table 6-14**. With the implementation of a full-access interchange at US 101 and Mathilda Avenue, there is a shift in vehicular traffic from SR 237 to US 101. This results in slight increases and decreases in travel time, delay, and maximum individual delay along US 101 southbound and SR 237 eastbound.

As described above, the US 101 northbound results show an increase in travel time and mainline vehicle delay with both Build Alternatives. This increase is due to the increase in demand served at the ramp terminal intersection, which in turn results in additional Mathilda Avenue traffic entering northbound US 101 during peak hours.



TABLE 6-13: YEAR 2040 PEAK HOUR MEASURES OF EFFECTIVENESS

| Scenario | Measure of Effectiveness | Peak Hour | No Build Conditions | Build 1 Alternative | | Build 2 Alternative | |
|---|---|-----------|---------------------|---------------------|----------|---------------------|----------|
| | | | | Results | % Change | Results | % Change |
| US 101 Northbound | Vehicle Miles of Travel (vehicle-miles) | AM | 12,070 | 11,930 | -1.2% | 11,930 | -1.2% |
| | | PM | 10,400 | 10,110 | -2.9% | 10,120 | -2.8% |
| | Average Travel Time (min:sec) | AM | 6:32 | 6:49 | 4.2% | 6:48 | 3.9% |
| | | PM | 11:42 | 13:03 | 10.3% | 12:44 | 8.1% |
| Average Travel Speed (mph) | AM | 19.8 | 19.0 | -4.2% | 19.1 | -3.7% | |
| | PM | 11.1 | 9.9 | -12.1% | 10.2 | -8.8% | |
| Mainline Vehicle Delay (vehicle-hours) ¹ | AM | 290 | 300 | 3.3% | 300 | 3.3% | |
| | PM | 602 | 678 | 11.2% | 658 | 8.5% | |
| US 101 Southbound | Vehicle Miles of Travel (vehicle-miles) | AM | 11,190 | 11,450 | 2.3% | 11,380 | 1.7% |
| | | PM | 13,230 | 13,150 | -0.6% | 13,210 | -0.2% |
| | Average Travel Time (min:sec) | AM | 1:58 | 1:58 | 0.0% | 1:58 | 0.0% |
| | | PM | 11:16 | 11:49 | 4.7% | 11:19 | 0.4% |
| Average Travel Speed (mph) | AM | 64.1 | 64.1 | 0.0% | 64.1 | 0.0% | |
| | PM | 11.2 | 10.7 | -4.7% | 11.1 | -0.9% | |
| Mainline Vehicle Delay (vehicle-hours) ¹ | AM | 2 | 2 | 0.0% | 2 | 0.0% | |
| | PM | 715 | 747 | 4.3% | 717 | .3% | |
| SR 237 Westbound | Vehicle Miles of Travel (vehicle-miles) | AM | 12,660 | 12,690 | 0.2% | 12,680 | 0.2% |
| | | PM | 8,750 | 8,730 | -0.2% | 8,800 | 0.6% |
| | Average Travel Time (min:sec) | AM | 2:36 | 2:36 | 0.0% | 2:36 | 0.0% |
| | | PM | 3:09 | 3:09 | 0.0% | 3:09 | 0.0% |
| Average Travel Speed (mph) | AM | 51.6 | 51.6 | 0.0% | 51.6 | 0.0% | |
| | PM | 42.6 | 42.6 | 0.0% | 42.6 | 0.0% | |
| Mainline Vehicle Delay (vehicle-hours) ¹ | AM | 50 | 50 | 0.0% | 50 | 0.0% | |
| | PM | 61 | 61 | 0.0% | 61 | 0.0% | |
| SR 237 Eastbound | Vehicle Miles of Travel (vehicle-miles) | AM | 10,540 | 11,040 | 4.5% | 11,120 | 5.2% |
| | | PM | 8,520 | 8,690 | 2.0% | 8,780 | 3.0% |
| | Average Travel Time (min:sec) | AM | 2:11 | 2:14 | 2.2% | 2:14 | 2.2% |
| | | PM | 20:45 | 19:52 | -4.4% | 17:41 | -17.3% |
| Average Travel Speed (mph) | AM | 61.4 | 60.0 | -2.3% | 60.0 | -2.3% | |
| | PM | 6.5 | 6.7 | 3.0% | 7.6 | 14.5% | |
| Mainline Vehicle Delay (vehicle-hours) ¹ | AM | 8 | 11 | 27.7% | 12 | 30.8% | |
| | PM | 717 | 694 | -3.3% | 635 | -12.9% | |

Notes:

1. US 101 Northbound AM and PM peak hour is between 7:00AM and 8:00AM and 5:00PM to 6:00PM, respectively.
2. US 101 Southbound AM and PM peak hour is between 7:00AM and 8:00AM and 5:00PM to 6:00PM, respectively.
3. SR 237 Westbound AM and PM peak hour is between 7:00AM and 8:00AM and 5:00PM to 6:00PM, respectively.
4. SR 237 Eastbound AM and PM peak hour is between 8:00AM and 9:00AM and 5:00PM to 6:00PM, respectively.

Source: Fehr & Peers, 2016.



TABLE 6-14: YEAR 2040 PEAK PERIOD MEASURES OF EFFECTIVENESS

| Scenario | Measure of Effectiveness | Peak Hour | No Build Conditions | Build 1 Alternative | | Build 2 Alternative | |
|---|---|-----------|---------------------|---------------------|----------|---------------------|----------|
| | | | | Results | % Change | Results | % Change |
| US 101 Northbound | Vehicle Miles of Travel (vehicle-miles) | AM | 25,810 | 25,530 | -1.1% | 25,540 | -1.1% |
| | | PM | 32,500 | 31,660 | -2.7% | 31,700 | -2.5% |
| | Average Travel Time (min:sec) | AM | 6:36 | 7:04 | 6.6% | 7:02 | 6.2% |
| | | PM | 10:11 | 11:05 | 8.1% | 10:58 | 7.1% |
| | Average Travel Speed (mph) | AM | 19.6 | 18.3 | -7.1% | 18.4 | -6.5% |
| | | PM | 12.7 | 11.7 | -8.5% | 11.8 | -7.6% |
| Mainline Vehicle Delay (vehicle-hours) ¹ | AM | 660 | 730 | 9.6% | 720 | 8.3% | |
| | PM | 1,562 | 1,703 | 8.3% | 1,683 | 7.2% | |
| Maximum Individual Vehicle Delay (min:sec) | AM | 4:40 | 5:19 | 12.2% | 5:16 | 11.4% | |
| | PM | 14:32 | 15:43 | 7.5% | 15:43 | 7.5% | |
| US 101 Southbound | Vehicle Miles of Travel (vehicle-miles) | AM | 23,650 | 24,380 | 3.0% | 24,180 | 2.2% |
| | | PM | 35,910 | 35,760 | -0.4% | 35,910 | 0.0% |
| | Average Travel Time (min:sec) | AM | 1:59 | 2:01 | 1.7% | 2:00 | 0.8% |
| | | PM | 11:16 | 11:33 | 2.5% | 11:15 | -0.1% |
| | Average Travel Speed (mph) | AM | 63.6 | 62.5 | -1.8% | 63.1 | -0.8% |
| | | PM | 11.2 | 10.9 | -2.8% | 11.2 | 0.0% |
| Mainline Vehicle Delay (vehicle-hours) ¹ | AM | 8 | 12 | 33.3% | 10 | 20.0% | |
| | PM | 1,906 | 1,946 | 2.1% | 1903 | -0.2% | |
| Maximum Individual Vehicle Delay (min:sec) | AM | 0:05 | 0:06 | 16.7% | 0:06 | 16.7% | |
| | PM | 9:55 | 10:05 | 1.7% | 9:51 | -0.7% | |
| SR 237 Westbound | Vehicle Miles of Travel (vehicle-miles) | AM | 20,030 | 20,090 | 0.3% | 20,070 | 0.2% |
| | | PM | 27,300 | 27,230 | -0.3% | 27,410 | 0.4% |
| | Average Travel Time (min:sec) | AM | 2:33 | 2:33 | 0.0% | 2:33 | 0.0% |
| | | PM | 3:01 | 3:01 | 0.0% | 3:01 | 0.0% |
| | Average Travel Speed (mph) | AM | 52.6 | 52.6 | 0.0% | 52.6 | 0.0% |
| | | PM | 44.5 | 44.5 | 0.0% | 44.5 | 0.0% |
| Mainline Vehicle Delay (vehicle-hours) ¹ | AM | 110 | 110 | 0.0% | 110 | 0.0% | |
| | PM | 163 | 163 | 0.0% | 163 | 0.0% | |
| Maximum Individual Vehicle Delay (min:sec) | AM | 0:32 | 0:32 | 0.0% | 0:32 | 0.0% | |
| | PM | 1:05 | 1:05 | 0.0% | 1:05 | 0.0% | |
| SR 237 Eastbound | Vehicle Miles of Travel (vehicle-miles) | AM | 19,060 | 20,050 | 4.9% | 20,080 | 5.1% |
| | | PM | 22,020 | 22,820 | 3.5% | 23,240 | 5.2% |
| | Average Travel Time (min:sec) | AM | 2:10 | 2:12 | 1.5% | 2:12 | 1.5% |
| | | PM | 14:31 | 13:22 | -8.6% | 11:50 | -22.7% |
| | Average Travel Speed (mph) | AM | 61.8 | 60.9 | -1.5% | 60.9 | -1.5% |
| | | PM | 9.2 | 10.0 | 8.0% | 11.3 | 18.6% |
| Mainline Vehicle Delay (vehicle-hours) ¹ | AM | 14 | 17 | 20.0% | 18 | 22.3% | |
| | PM | 1,497 | 1,441 | -3.9% | 1,345 | -11.3% | |
| Maximum Individual Vehicle Delay (min:sec) | AM | 0:07 | 0:10 | 30.0% | 0:10 | 30.0% | |
| | PM | 18:41 | 17:49 | -4.9% | 15:38 | -19.5% | |

Source: Fehr & Peers, 2016.



MAINLINE WEAVING ANALYSIS

Per Caltrans' requirements, **Table 6-15** summarizes the Year 2040 Leisch Method AM and PM peak hour mainline weaving analysis at the US 101/Mathilda Avenue and SR 237/Mathilda Avenue interchanges. The Leisch Method analysis was applied for the constrained mainline and ramp volumes as determined by the FREQ models. The Leisch Method has a limitation of 3,600 passenger cars per hour for weaving volumes and a weaving length of 6,000 feet. There are no segments that are outside of the provided parameters.

The SR 237 eastbound weaving section improves from an LOS E to LOS D in the PM peak hour under both Build Alternatives while the US 101 southbound weaving section decreases from an LOS C to LOS E in the PM peak hour with the given shift in traffic due to the full access interchange at US 101/Mathilda Avenue. **Appendix Q** provides the Leisch analysis worksheets. These results differ from the FREQ results presented earlier due to the following reasons:

- Leisch Method uses default mainline capacities while the FREQ models use calibrated capacities to reflect observed conditions;
- Leisch Method evaluates mainline segments in isolation where bottlenecks and mainline queuing do not impact downstream or upstream traffic. FREQ models consider the effects of the bottlenecks and mainline queuing on the entire mainline system.



TABLE 6-15: YEAR 2040 PEAK HOUR WEAVING ANALYSIS BASED ON LEISCH METHOD

| Freeway | Location | Direction | Number of Lanes | No Build | Build 1 | Build 2 |
|-----------|---|-----------|-----------------------------------|----------|----------|----------|
| AM | | | | | | |
| US 101 | SR 237 EB on-ramp to Mathilda Avenue off-ramp | SB | 2 HOT 3 Mainline 1 Aux Lane | D | E | E |
| SR 237 | Mathilda Avenue on-ramp to US 101 NB off-ramp | WB | 1 HOT 2 Mainline 1 Aux Lane | D | D | D |
| | US 101 SB on-ramp to Mathilda Avenue off-ramp | EB | 1 HOT 2 Mainline 1 Aux Lane | F | F | F |
| PM | | | | | | |
| US 101 | SR 237 EB on-ramp to Mathilda Avenue off-ramp | SB | 2 HOT 3 Mainline 1 Aux Lane | C | E | E |
| SR 237 | Mathilda Avenue on-ramp to US 101 NB off-ramp | WB | 1 HOT 2 Mainline 1 Aux Lane | F | E | E |
| | US 101 SB on-ramp to Mathilda Avenue off-ramp | EB | 1 HOT 2 Mainline 1 Aux Lane | E | D | D |

Notes: **Bold** indicates weaving section operates at LOS F under un-congested conditions.

Source: Fehr & Peers, 2016.



7. TRAFFIC ANALYSIS SUMMARY

This section summarizes the results of the Opening Year 2018 and Design Year 2040 AM and PM peak hour traffic analysis results for the Mathilda Avenue Improvements between SR 237 and US 101 in Sunnyvale, California. The Build Alternatives are compared against the No Build Alternative in the following areas:

- **Intersection operations:** overall peak hour intersection delay, percent of demand served, and average travel times.
- **Freeway operations:** freeway mainline and ramp operations, and weaving section operations.
- **Bicycle and pedestrian conditions:** conditions for bicycle and pedestrians travelling in the corridor.

INTERSECTION OPERATIONS

Intersection operations are summarized in terms of the (1) peak hour delay, (2) percent of vehicle traffic demand served, and (3) average vehicle travel times.

PEAK HOUR DELAY

Under No Build conditions most study intersections along Mathilda Avenue are anticipated to operate at LOS F in both peak hours by Year 2018, a trend that is expected to continue to worsen to conditions resembling system gridlock in Year 2040. Compared to the No Build Alternative, there is an overall reduction in peak hour delay on local streets, as listed below, for both Build Alternatives.

- Build 1 Alternative Peak Hour Delay Reduction
 - Year 2018 AM Peak Hour – 63%
 - Year 2018 PM Peak Hour – 15%
 - Year 2040 AM Peak Hour – 35%
 - Year 2040 PM Peak Hour – 18%
- Build 2 Alternative Peak Hour Delay Reduction
 - Year 2018 AM Peak Hour – 42%
 - Year 2018 PM Peak Hour – 26%
 - Year 2040 AM Peak Hour – 14%
 - Year 2040 PM Peak Hour – 15%

While conditions are improved compared to No Build conditions, in the PM peak hour for the Build 1 Alternative the SR 237 ramp terminal intersections continue to act as a bottleneck for southbound traffic along Mathilda Avenue and eastbound traffic on Moffett Park Drive. By comparison, the key constraint point is moved upstream to the Mathilda Avenue/Innovation Way intersection in the PM peak hour under the Build 2 Alternative due to the large increase in traffic demand at this intersection, which lessens the benefit of the Build 2 Alternative compared to the Build 1 Alternative.

VEHICLE TRAFFIC DEMAND SERVED

Compared to the No Build Alternative, both Build Alternatives would increase the percent of peak hour traffic demand served through local intersections along the Mathilda Avenue corridor and at nearby study



intersections. The Build 1 Alternative provides a slightly larger increase in percent demand served on local streets when compared to the Build 2 Alternative.

Under Year 2018 conditions, the overall percent demand served increases by approximately 10 percent and 4 percent in the AM and PM peak hours, respectively, under the Build 1 Alternative and 6 percent in the AM and PM peak hours under the Build 2 Alternative. In Year 2040, the overall percent demand served increases by approximately 7 to 9 percent in the AM and PM peak hours under the Build 1 Alternative and by approximately 4 to 6 percent in the AM and PM peak hours, respectively, under the Build 2 Alternative.

TRAVEL TIMES

Both Build Alternatives would reduce the average travel time along Mathilda Avenue and increase the average travel speed on Mathilda Avenue in both the northbound and southbound directions when compared to No Build conditions, with the exception of Build 1 Alternative southbound Year 2018 PM peak hour travel times on Mathilda Avenue. Travel times under this scenario would slightly increase by approximately six percent, or 68 seconds, compared to No Build conditions due to slight increases in queue backups on southbound Mathilda Avenue north of SR 237; however, overall system-wide delay would still decrease compared to No Build conditions. Under all scenarios, the “combined” northbound and southbound travel time along Mathilda Avenue is expected to be reduced by at least 18 percent under the Build 1 Alternative and 27 percent under the Build 2 Alternative as indicated below.

- Build 1 Alternative “Combined” Mathilda Avenue Travel Time Reduction*
 - Year 2018 AM Peak Hour – 36%
 - Year 2018 PM Peak Hour – 18%
 - Year 2040 AM Peak Hour – 47%
 - Year 2040 PM Peak Hour – 21%
- Build 2 Alternative “Combined” Mathilda Avenue Travel Time Reduction*
 - Year 2018 AM Peak Hour – 29%
 - Year 2018 PM Peak Hour – 31%
 - Year 2040 AM Peak Hour – 48%
 - Year 2040 PM Peak Hour – 27%

*Indicates combined northbound and southbound travel time percent reduction for each peak hour showing overall Mathilda Avenue reductions in travel time.

FREEWAY OPERATIONS

Congestion at the US 101/Mathilda Avenue and SR 237/Mathilda Avenue interchanges under No Build conditions is anticipated to result in vehicle queue spillback onto the freeway mainlines during the AM and PM peak hours. In Year 2018, both Build Alternatives would improve ramp operations and result in little to no vehicle queue spillback onto the freeway mainlines. In Year 2040, some queue spillback is anticipated to return at some off-ramps, though queues will be substantially less than No Build conditions.

Freeway operations under No Build conditions result in mostly LOS F operations throughout the study area in the peak commute directions during both peak hours. Under Year 2018, there is a slight decrease in density in the PM peak hour on SR 237 eastbound between US 101 southbound on-ramp and the Mathilda Avenue off-ramp due to the shift in traffic induced with the project. This shift in traffic results in a slight increase in congestion on US 101 southbound between SR 237 eastbound on-ramp and the Mathilda



Avenue off-ramp. However, both Build Alternatives are not anticipated to change the freeway LOS and will have negligible effects on peak hour freeway congestion levels. Under Year 2040 No Build Conditions, the SR 237 westbound bottleneck moves upstream to the Fair Oaks Avenue on-ramp, and congestion on the mixed-flow lanes worsens compared to Year 2018. Both Build Alternatives are not anticipated to add additional bottlenecks. However, both Build Alternatives will slightly increase the length of the queuing along SR 237 eastbound in the PM peak hour due to increased on-ramp throughput.

Both Build Alternatives would eliminate the short, non-standard weaving segment on northbound US 101 between the on-ramp from northbound Mathilda Avenue and the off-ramp to southbound Mathilda Avenue. Similarly, both Build Alternatives will also eliminate the short weaving segment on southbound Mathilda Avenue between the northbound US 101 loop off-ramp and the southbound US 101 loop on-ramp. Removing weaving sections and lane drops will eliminate speed differentials along US 101 and southbound Mathilda Avenue may reduce the potential for rear-end and lane-change collisions in these areas.

In Year 2040, the SR 237 eastbound weaving section between US 101 and Mathilda Avenue off-ramp improves from an LOS E to LOS D in the PM peak hour under both Build Alternatives. In addition, the SR 237 westbound weaving section between the Mathilda Avenue on-ramp and US 101 is anticipated to improve from an LOS F to LOS E in the PM peak hour under both Build Alternatives, while the US 101 southbound weaving section between SR 237 and the Mathilda Avenue off-ramp decreases from an LOS C to LOS E in the PM peak hour with the given shift in traffic due to the full access interchange at US 101 and Mathilda Avenue.

BICYCLE AND PEDESTRIAN CONDITIONS

The Build Alternatives would also enhance pedestrian and bicycle facilities in the corridor, including along Mathilda Avenue and Moffett Park Drive. The following improvements to bicycle and pedestrian and conditions would be made:

- New pedestrian and bicycle facilities
 - New east-west Class I trails on Moffett Park Drive
 - Class II bicycle lanes on Mathilda Avenue
 - Continuous sidewalks on east side of Mathilda Avenue
- Controlled and more convenient pedestrian crossings
 - Eliminate uncontrolled ramp movements and construct tee-intersections for US 101 off-ramps to Mathilda Avenue
 - Crosswalks with optimum crossing distance and pedestrian refuges where applicable
 - Enhanced pavement delineation and signing treatments
- Improved bike circulation and connectivity
 - Improved bicycle connections between Mathilda Avenue and Moffett Park Drive
- Improvements to increase ADA access
 - New accessible curb ramps conforming to ADA guidelines
 - Pedestrian countdown signals at new or modified intersections



- Pushbutton-integrated Accessible Pedestrian Signals (APS)

CONCLUSIONS

There are several key conclusions based on the results of the freeway mainline and intersection level of service operations analysis. Conclusions for the traffic and transportation section of the PA/ED can be described as follows:

- 1) Based on the results in the TOAR, the existing Mathilda Avenue interchanges with US 101 and SR 237 currently do not provide sufficient capacity for Existing (2013) traffic volumes and will not provide sufficient capacity to serve the projected Year 2018 and Year 2040 traffic volumes.
- 2) Based on the results shown in the TOAR, Build 1 Alternative provides a larger increase in percent demand served on local streets when compared to the Build 2 Alternative.
- 3) Peak hour travel times along Mathilda Avenue during Year 2040 are anticipated to decrease with both Build Alternatives.
- 4) For both Build Alternatives, overall peak hour and peak period freeway operations are expected to be generally similar to No Build conditions. Construction of the full access interchange at US 101 and Mathilda Avenue would result in a slightly higher freeway mainline density along some sections of US 101 and a slightly lower density along SR 237. Differences in operations results for specific freeway sections are generally minor and are not expected to result in substantial changes to overall freeway performance.
- 5) Improved bicycle and pedestrian connectivity and new facilities to provide a broader range of pedestrian and bicycle access options.



APPENDIX A – RAW TRAFFIC COUNTS



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Groups Printed- Vehicles

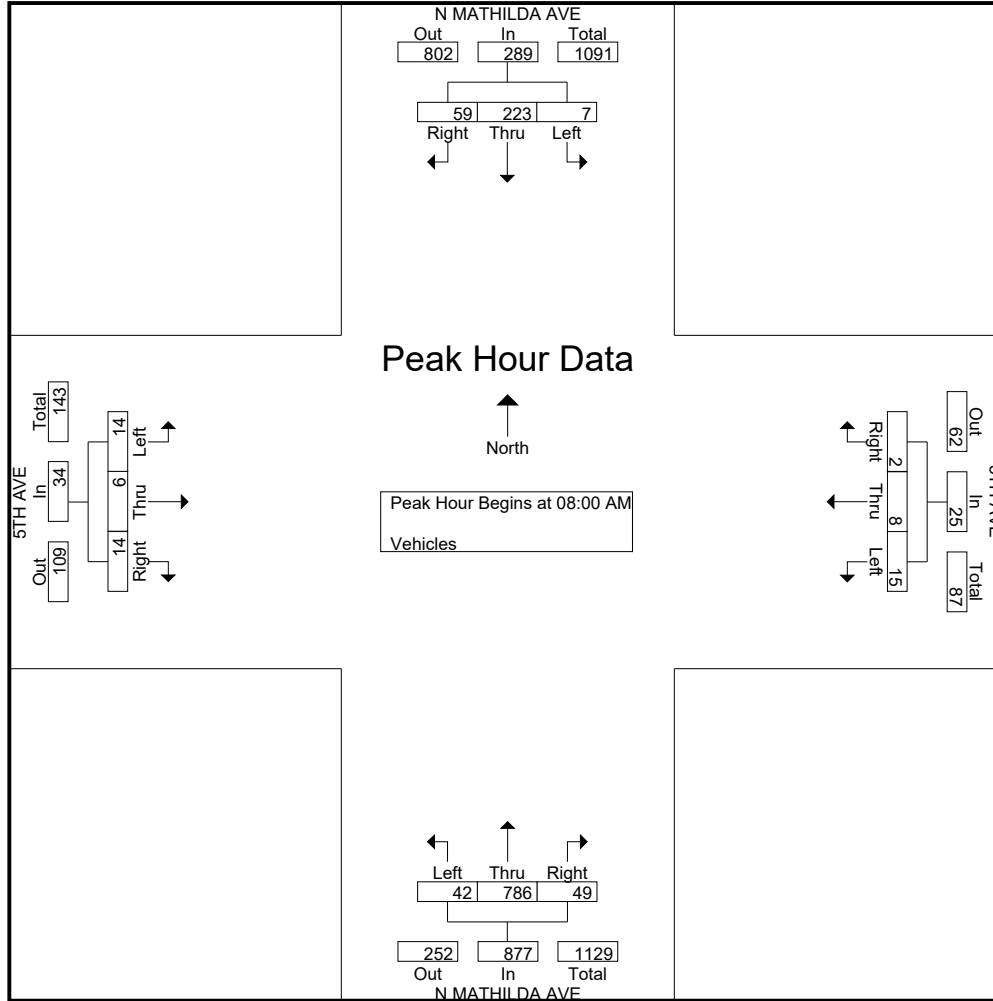
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| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 5 | 19 | 0 | 0 | 24 | 1 | 0 | 1 | 0 | 2 | 7 | 176 | 11 | 1 | 195 | 3 | 1 | 2 | 0 | 6 | 227 |
| 07:15 AM | 5 | 25 | 1 | 1 | 32 | 1 | 2 | 1 | 0 | 4 | 10 | 170 | 8 | 0 | 188 | 0 | 0 | 4 | 1 | 5 | 229 |
| 07:30 AM | 7 | 30 | 3 | 0 | 40 | 1 | 0 | 0 | 2 | 3 | 11 | 149 | 10 | 3 | 173 | 3 | 1 | 1 | 0 | 5 | 221 |
| 07:45 AM | 10 | 40 | 3 | 0 | 53 | 3 | 3 | 2 | 5 | 13 | 10 | 184 | 14 | 7 | 215 | 4 | 1 | 1 | 0 | 6 | 287 |
| Total | 27 | 114 | 7 | 1 | 149 | 6 | 5 | 4 | 7 | 22 | 38 | 679 | 43 | 11 | 771 | 10 | 3 | 8 | 1 | 22 | 964 |
| 08:00 AM | 12 | 54 | 0 | 0 | 66 | 0 | 2 | 5 | 0 | 7 | 6 | 196 | 14 | 1 | 217 | 5 | 1 | 3 | 0 | 9 | 299 |
| 08:15 AM | 15 | 51 | 3 | 1 | 70 | 1 | 1 | 3 | 2 | 7 | 9 | 200 | 12 | 5 | 226 | 1 | 2 | 3 | 2 | 8 | 311 |
| 08:30 AM | 15 | 57 | 2 | 3 | 77 | 0 | 2 | 2 | 2 | 6 | 12 | 186 | 10 | 10 | 218 | 3 | 0 | 5 | 3 | 11 | 312 |
| 08:45 AM | 17 | 61 | 2 | 0 | 80 | 1 | 3 | 5 | 2 | 11 | 22 | 204 | 6 | 7 | 239 | 5 | 3 | 3 | 0 | 11 | 341 |
| Total | 59 | 223 | 7 | 4 | 293 | 2 | 8 | 15 | 6 | 31 | 49 | 786 | 42 | 23 | 900 | 14 | 6 | 14 | 5 | 39 | 1263 |
| Grand Total | 86 | 337 | 14 | 5 | 442 | 8 | 13 | 19 | 13 | 53 | 87 | 1465 | 85 | 34 | 1671 | 24 | 9 | 22 | 6 | 61 | 2227 |
| Apprch % | 19.5 | 76.2 | 3.2 | 1.1 | | 15.1 | 24.5 | 35.8 | 24.5 | | 5.2 | 87.7 | 5.1 | 2 | | 39.3 | 14.8 | 36.1 | 9.8 | | |
| Total % | 3.9 | 15.1 | 0.6 | 0.2 | 19.8 | 0.4 | 0.6 | 0.9 | 0.6 | 2.4 | 3.9 | 65.8 | 3.8 | 1.5 | 75 | 1.1 | 0.4 | 1 | 0.3 | 2.7 | |

| Start Time | N MATHILDA AVE Southbound | | | | 5TH AVE Westbound | | | | N MATHILDA AVE Northbound | | | | 5TH AVE Eastbound | | | | Int. Total |
|--|---------------------------|------|------|------------|-------------------|------|------|------------|---------------------------|------|------|------------|-------------------|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 08:00 AM | | | | | | | | | | | | | | | | | |
| 08:00 AM | 12 | 54 | 0 | 66 | 0 | 2 | 5 | 7 | 6 | 196 | 14 | 216 | 5 | 1 | 3 | 9 | 298 |
| 08:15 AM | 15 | 51 | 3 | 69 | 1 | 1 | 3 | 5 | 9 | 200 | 12 | 221 | 1 | 2 | 3 | 6 | 301 |
| 08:30 AM | 15 | 57 | 2 | 74 | 0 | 2 | 2 | 4 | 12 | 186 | 10 | 208 | 3 | 0 | 5 | 8 | 294 |
| 08:45 AM | 17 | 61 | 2 | 80 | 1 | 3 | 5 | 9 | 22 | 204 | 6 | 232 | 5 | 3 | 3 | 11 | 332 |
| Total Volume | 59 | 223 | 7 | 289 | 2 | 8 | 15 | 25 | 49 | 786 | 42 | 877 | 14 | 6 | 14 | 34 | 1225 |
| % App. Total | 20.4 | 77.2 | 2.4 | | 8 | 32 | 60 | | 5.6 | 89.6 | 4.8 | | 41.2 | 17.6 | 41.2 | | |
| PHF | .868 | .914 | .583 | .903 | .500 | .667 | .750 | .694 | .557 | .963 | .750 | .945 | .700 | .500 | .700 | .773 | .922 |

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Groups Printed- Bikes

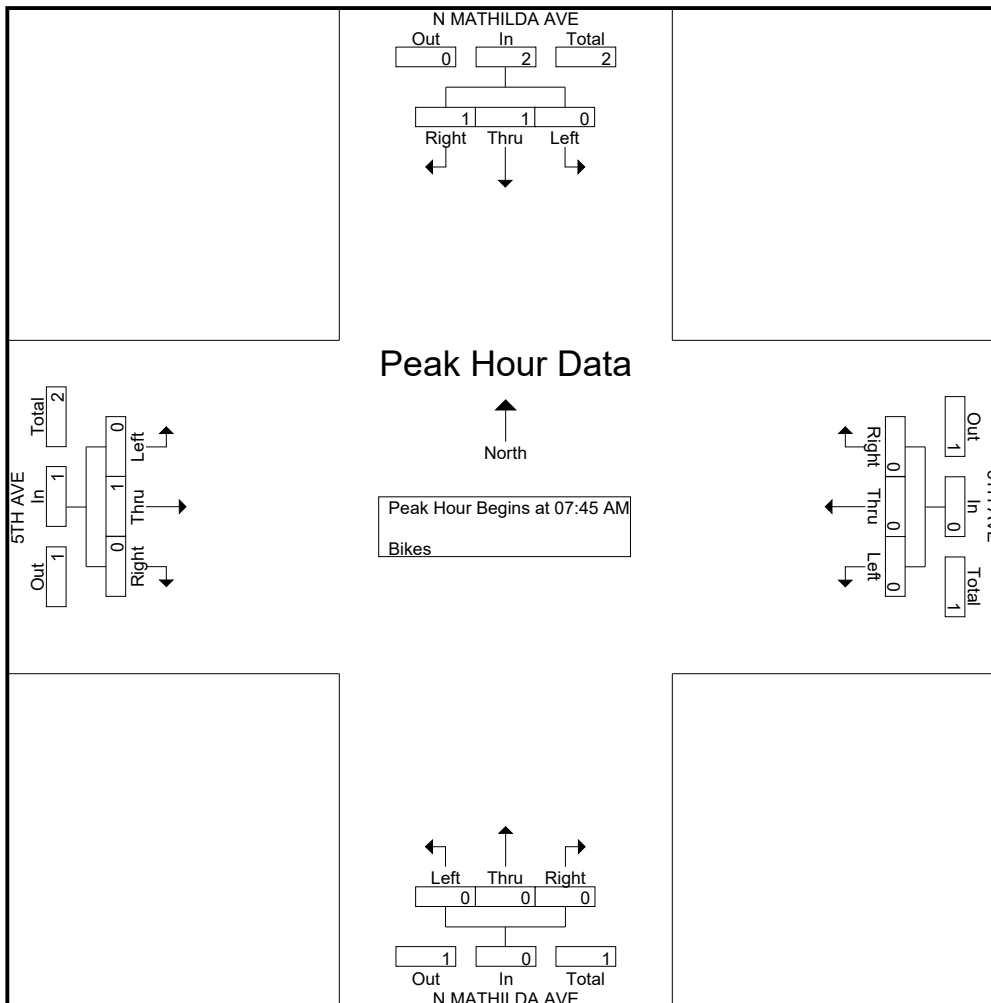
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|-------------|------------------------------|------|------|------|------------|----------------------|------|------|------|------------|------------------------------|------|------|------|------------|----------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:15 AM | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 08:30 AM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 2 |
| 08:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 1 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 3 |
| Grand Total | 1 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 4 |
| Apprch % | 50 | 50 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 100 | 0 | 0 | | 0 | 100 | 0 | 0 | | |
| Total % | 25 | 25 | 0 | 0 | 50 | 0 | 0 | 0 | 0 | 0 | 0 | 25 | 0 | 0 | 25 | 0 | 25 | 0 | 0 | 25 | |

| Start Time | N MATHILDA AVE Southbound | | | | 5TH AVE Westbound | | | | N MATHILDA AVE Northbound | | | | 5TH AVE Eastbound | | | | Int. Total |
|--|------------------------------|------|------|------------|----------------------|------|------|------------|------------------------------|------|------|------------|----------------------|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 07:45 AM | | | | | | | | | | | | | | | | | |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:15 AM | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 08:30 AM | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 2 |
| Total Volume | 1 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 3 |
| % App. Total | 50 | 50 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 100 | 0 | | |
| PHF | .250 | .250 | .000 | .500 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .250 | .000 | .250 | .375 |

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File Name : 1PM FINAL

Site Code : 00000001

Start Date : 11/13/2013

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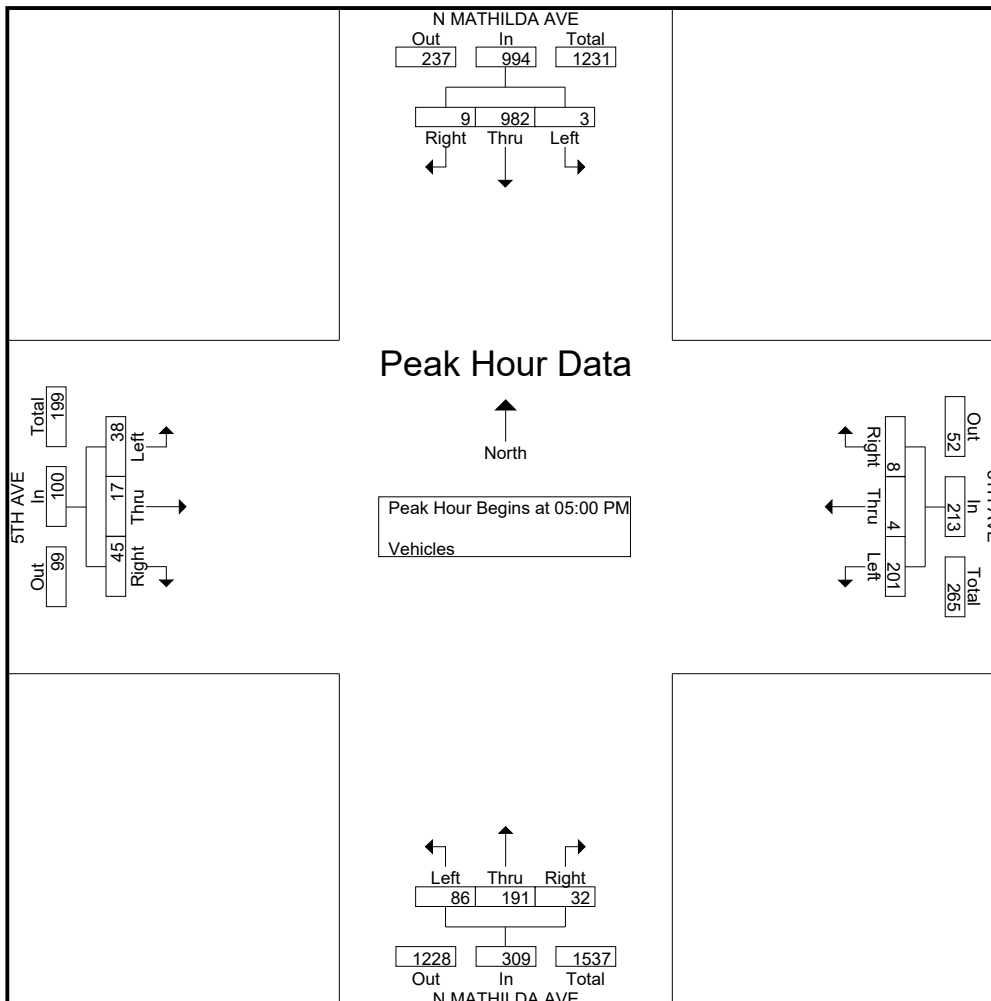
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| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:00 PM | 8 | 235 | 1 | 0 | 244 | 1 | 1 | 24 | 2 | 28 | 2 | 37 | 13 | 8 | 60 | 9 | 2 | 6 | 2 | 19 | 351 |
| 04:15 PM | 1 | 159 | 3 | 0 | 163 | 0 | 1 | 40 | 3 | 44 | 6 | 33 | 11 | 12 | 62 | 7 | 6 | 3 | 3 | 19 | 288 |
| 04:30 PM | 5 | 260 | 2 | 0 | 267 | 1 | 1 | 34 | 0 | 36 | 5 | 48 | 9 | 12 | 74 | 8 | 1 | 3 | 0 | 12 | 389 |
| 04:45 PM | 7 | 176 | 0 | 0 | 183 | 1 | 1 | 26 | 2 | 30 | 4 | 42 | 17 | 14 | 77 | 10 | 3 | 6 | 0 | 19 | 309 |
| Total | 21 | 830 | 6 | 0 | 857 | 3 | 4 | 124 | 7 | 138 | 17 | 160 | 50 | 46 | 273 | 34 | 12 | 18 | 5 | 69 | 1337 |
| 05:00 PM | 4 | 257 | 0 | 0 | 261 | 0 | 0 | 60 | 4 | 64 | 7 | 47 | 14 | 9 | 77 | 10 | 4 | 13 | 0 | 27 | 429 |
| 05:15 PM | 2 | 258 | 1 | 1 | 262 | 3 | 2 | 51 | 0 | 56 | 5 | 58 | 21 | 10 | 94 | 9 | 3 | 7 | 0 | 19 | 431 |
| 05:30 PM | 3 | 237 | 2 | 2 | 244 | 3 | 1 | 42 | 0 | 46 | 10 | 40 | 24 | 8 | 82 | 11 | 3 | 12 | 0 | 26 | 398 |
| 05:45 PM | 0 | 230 | 0 | 0 | 230 | 2 | 1 | 48 | 0 | 51 | 10 | 46 | 27 | 8 | 91 | 15 | 7 | 6 | 0 | 28 | 400 |
| Total | 9 | 982 | 3 | 3 | 997 | 8 | 4 | 201 | 4 | 217 | 32 | 191 | 86 | 35 | 344 | 45 | 17 | 38 | 0 | 100 | 1658 |
| 06:00 PM | 4 | 213 | 0 | 3 | 220 | 1 | 1 | 38 | 0 | 40 | 5 | 36 | 4 | 11 | 56 | 14 | 9 | 14 | 4 | 41 | 357 |
| 06:15 PM | 0 | 215 | 0 | 0 | 215 | 1 | 2 | 41 | 0 | 44 | 6 | 42 | 9 | 4 | 61 | 3 | 2 | 4 | 2 | 11 | 331 |
| 06:30 PM | 3 | 220 | 0 | 1 | 224 | 2 | 1 | 27 | 0 | 30 | 2 | 31 | 5 | 2 | 40 | 7 | 2 | 4 | 1 | 14 | 308 |
| 06:45 PM | 0 | 131 | 0 | 2 | 133 | 4 | 0 | 38 | 0 | 42 | 0 | 26 | 10 | 1 | 37 | 5 | 1 | 2 | 1 | 9 | 221 |
| Total | 7 | 779 | 0 | 6 | 792 | 8 | 4 | 144 | 0 | 156 | 13 | 135 | 28 | 18 | 194 | 29 | 14 | 24 | 8 | 75 | 1217 |
| Grand Total | 37 | 2591 | 9 | 9 | 2646 | 19 | 12 | 469 | 11 | 511 | 62 | 486 | 164 | 99 | 811 | 108 | 43 | 80 | 13 | 244 | 4212 |
| Apprch % | 1.4 | 97.9 | 0.3 | 0.3 | | 3.7 | 2.3 | 91.8 | 2.2 | | 7.6 | 59.9 | 20.2 | 12.2 | | 44.3 | 17.6 | 32.8 | 5.3 | | |
| Total % | 0.9 | 61.5 | 0.2 | 0.2 | 62.8 | 0.5 | 0.3 | 11.1 | 0.3 | 12.1 | 1.5 | 11.5 | 3.9 | 2.4 | 19.3 | 2.6 | 1 | 1.9 | 0.3 | 5.8 | |

| Start Time | N MATHILDA AVE Southbound | | | | 5TH AVE Westbound | | | | N MATHILDA AVE Northbound | | | | 5TH AVE Eastbound | | | | Int. Total |
|--|------------------------------|------|------|------------|----------------------|------|------|------------|------------------------------|------|------|------------|----------------------|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 04:00 PM to 06:45 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 05:00 PM | | | | | | | | | | | | | | | | | |
| 05:00 PM | 4 | 257 | 0 | 261 | 0 | 0 | 60 | 60 | 7 | 47 | 14 | 68 | 10 | 4 | 13 | 27 | 416 |
| 05:15 PM | 2 | 258 | 1 | 261 | 3 | 2 | 51 | 56 | 5 | 58 | 21 | 84 | 9 | 3 | 7 | 19 | 420 |
| 05:30 PM | 3 | 237 | 2 | 242 | 3 | 1 | 42 | 46 | 10 | 40 | 24 | 74 | 11 | 3 | 12 | 26 | 388 |
| 05:45 PM | 0 | 230 | 0 | 230 | 2 | 1 | 48 | 51 | 10 | 46 | 27 | 83 | 15 | 7 | 6 | 28 | 392 |
| Total Volume | 9 | 982 | 3 | 994 | 8 | 4 | 201 | 213 | 32 | 191 | 86 | 309 | 45 | 17 | 38 | 100 | 1616 |
| % App. Total | 0.9 | 98.8 | 0.3 | | 3.8 | 1.9 | 94.4 | | 10.4 | 61.8 | 27.8 | | 4.5 | 1.7 | 3.8 | | |
| PHF | .563 | .952 | .375 | .952 | .667 | .500 | .838 | .888 | .800 | .823 | .796 | .920 | .750 | .607 | .731 | .893 | .962 |

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Page No : 1

Groups Printed- Bikes

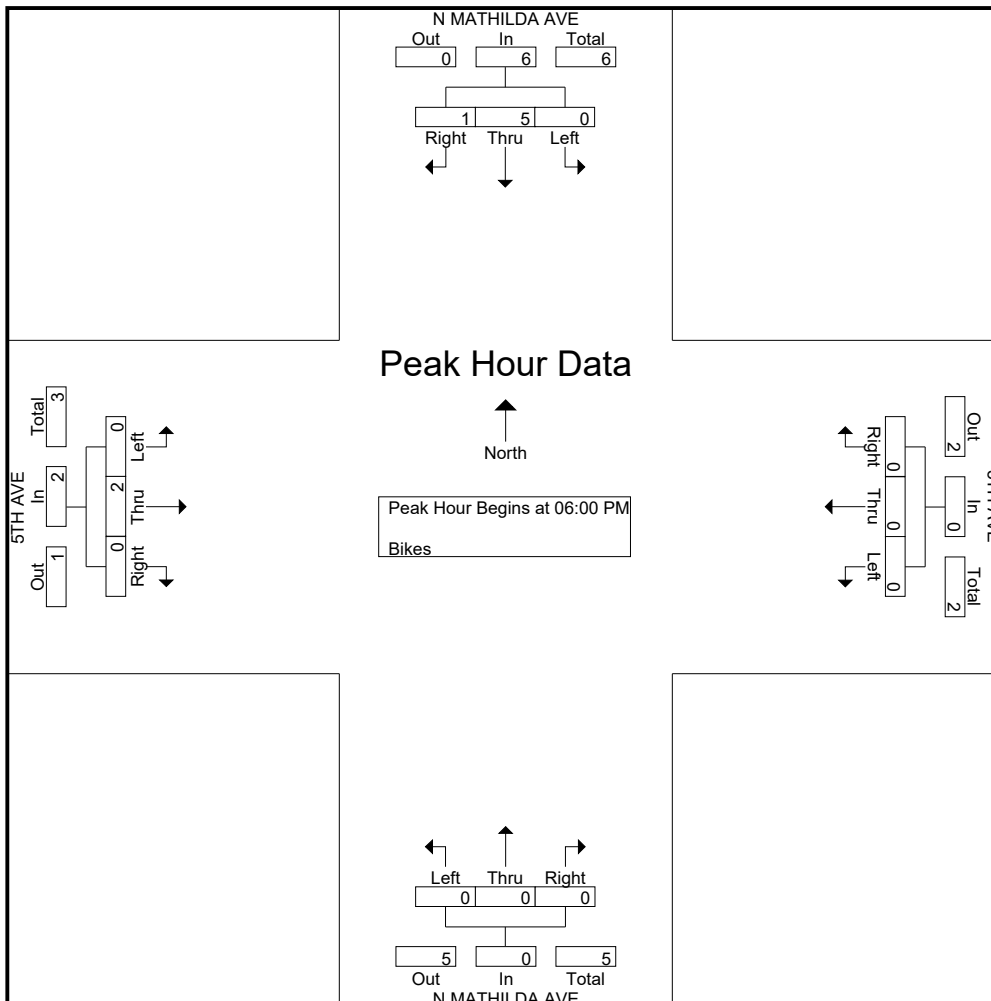
| Start Time | N MATHILDA AVE Southbound | | | | | 5TH AVE Westbound | | | | | N MATHILDA AVE Northbound | | | | | 5TH AVE Eastbound | | | | | Int. Total |
|--------------------|---------------------------|------|------|------|------------|-------------------|------|------|------|------------|---------------------------|------|------|------|------------|-------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 1 |
| 04:45 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 2 |
| 05:00 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 05:15 PM | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:45 PM | 1 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| Total | 1 | 4 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 06:00 PM | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 3 |
| 06:15 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 06:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 |
| 06:45 PM | 1 | 2 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| Total | 1 | 5 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 8 |
| Grand Total | 2 | 10 | 0 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 3 | 15 |
| Apprch % | 16.7 | 83.3 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 33.3 | 66.7 | 0 | 0 | | |
| Total % | 13.3 | 66.7 | 0 | 0 | 80 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6.7 | 13.3 | 0 | 0 | 20 | |

| Start Time | N MATHILDA AVE Southbound | | | | 5TH AVE Westbound | | | | N MATHILDA AVE Northbound | | | | 5TH AVE Eastbound | | | | Int. Total |
|--|---------------------------|------|------|------------|-------------------|------|------|------------|---------------------------|------|------|------------|-------------------|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 04:00 PM to 06:45 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 06:00 PM | | | | | | | | | | | | | | | | | |
| 06:00 PM | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 3 |
| 06:15 PM | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 06:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1 |
| 06:45 PM | 1 | 2 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| Total Volume | 1 | 5 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 8 |
| % App. Total | 16.7 | 83.3 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 100 | 0 | | |
| PHF | .250 | .625 | .000 | .500 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .500 | .000 | .500 | .667 |

Traffic Data Service

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 Site Code : 00000001
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Traffic Data Service

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 tdsbay@cs.com

File Name : 8AM FINAL
 Site Code : 00000008
 Start Date : 11/13/2013
 Page No : 1

Groups Printed- Vehicles

| Start Time | N MATHILDA AVE Southbound | | | | | Westbound | | | | | N MATHILDA AVE Northbound | | | | | INNOVATION WAY Eastbound | | | | | Int. Total |
|-------------|---------------------------|------|------|------|------------|-----------|------|------|------|------------|---------------------------|------|------|------|------------|--------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 8 | 18 | 0 | 1 | 27 | 0 | 0 | 0 | 2 | 2 | 0 | 196 | 47 | 0 | 243 | 1 | 0 | 1 | 0 | 2 | 274 |
| 07:15 AM | 6 | 25 | 0 | 0 | 31 | 0 | 0 | 0 | 1 | 1 | 0 | 200 | 41 | 0 | 241 | 3 | 0 | 0 | 1 | 4 | 277 |
| 07:30 AM | 4 | 32 | 0 | 0 | 36 | 0 | 0 | 0 | 1 | 1 | 0 | 173 | 83 | 0 | 256 | 2 | 0 | 2 | 0 | 4 | 297 |
| 07:45 AM | 11 | 36 | 1 | 4 | 52 | 0 | 0 | 0 | 5 | 5 | 0 | 202 | 78 | 0 | 280 | 5 | 0 | 2 | 1 | 8 | 345 |
| Total | 29 | 111 | 1 | 5 | 146 | 0 | 0 | 0 | 9 | 9 | 0 | 771 | 249 | 0 | 1020 | 11 | 0 | 5 | 2 | 18 | 1193 |
| 08:00 AM | 19 | 47 | 0 | 0 | 66 | 0 | 0 | 0 | 0 | 0 | 0 | 220 | 90 | 2 | 312 | 9 | 0 | 4 | 0 | 13 | 391 |
| 08:15 AM | 14 | 47 | 0 | 1 | 62 | 0 | 0 | 0 | 0 | 0 | 0 | 241 | 89 | 3 | 333 | 11 | 0 | 1 | 0 | 12 | 407 |
| 08:30 AM | 8 | 58 | 0 | 1 | 67 | 0 | 0 | 0 | 0 | 0 | 0 | 244 | 88 | 0 | 332 | 8 | 0 | 5 | 0 | 13 | 412 |
| 08:45 AM | 21 | 56 | 1 | 0 | 78 | 0 | 0 | 0 | 0 | 0 | 0 | 284 | 118 | 0 | 402 | 9 | 0 | 4 | 1 | 14 | 494 |
| Total | 62 | 208 | 1 | 2 | 273 | 0 | 0 | 0 | 0 | 0 | 0 | 989 | 385 | 5 | 1379 | 37 | 0 | 14 | 1 | 52 | 1704 |
| Grand Total | 91 | 319 | 2 | 7 | 419 | 0 | 0 | 0 | 9 | 9 | 0 | 1760 | 634 | 5 | 2399 | 48 | 0 | 19 | 3 | 70 | 2897 |
| Apprch % | 21.7 | 76.1 | 0.5 | 1.7 | | 0 | 0 | 0 | 100 | | 0 | 73.4 | 26.4 | 0.2 | | 68.6 | 0 | 27.1 | 4.3 | | |
| Total % | 3.1 | 11 | 0.1 | 0.2 | 14.5 | 0 | 0 | 0 | 0.3 | 0.3 | 0 | 60.8 | 21.9 | 0.2 | 82.8 | 1.7 | 0 | 0.7 | 0.1 | 2.4 | |

| Start Time | N MATHILDA AVE Southbound | | | | Westbound | | | | N MATHILDA AVE Northbound | | | | INNOVATION WAY Eastbound | | | | Int. Total |
|--------------|---------------------------|------|------|------------|-----------|------|------|------------|---------------------------|------|------|------------|--------------------------|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| 08:00 AM | 19 | 47 | 0 | 66 | 0 | 0 | 0 | 0 | 0 | 220 | 90 | 310 | 9 | 0 | 4 | 13 | 389 |
| 08:15 AM | 14 | 47 | 0 | 61 | 0 | 0 | 0 | 0 | 0 | 241 | 89 | 330 | 11 | 0 | 1 | 12 | 403 |
| 08:30 AM | 8 | 58 | 0 | 66 | 0 | 0 | 0 | 0 | 0 | 244 | 88 | 332 | 8 | 0 | 5 | 13 | 411 |
| 08:45 AM | 21 | 56 | 1 | 78 | 0 | 0 | 0 | 0 | 0 | 284 | 118 | 402 | 9 | 0 | 4 | 13 | 493 |
| Total Volume | 62 | 208 | 1 | 271 | 0 | 0 | 0 | 0 | 0 | 989 | 385 | 1374 | 37 | 0 | 14 | 51 | 1696 |
| % App. Total | 22.9 | 76.8 | 0.4 | | 0 | 0 | 0 | | 0 | 72 | 28 | | 72.5 | 0 | 27.5 | | |
| PHF | .738 | .897 | .250 | .869 | .000 | .000 | .000 | .000 | .000 | .871 | .816 | .854 | .841 | .000 | .700 | .981 | .860 |

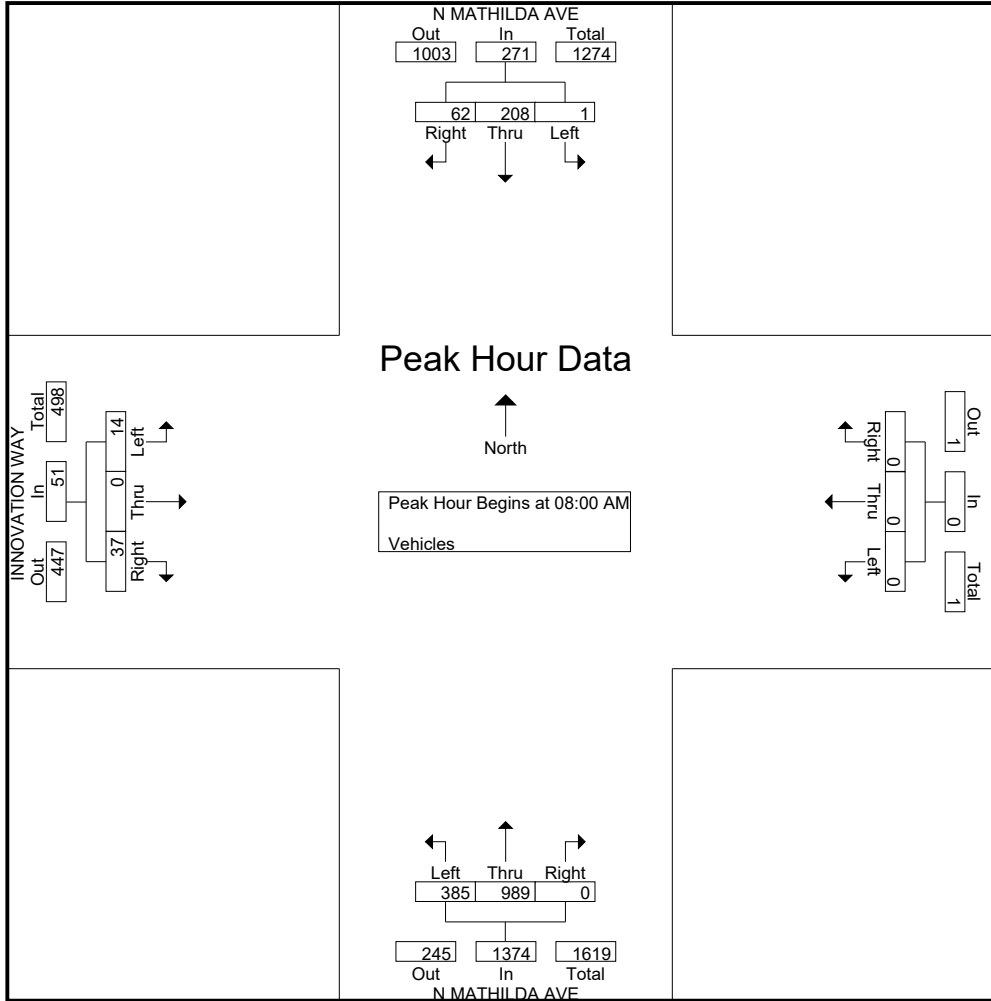
Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1

Peak Hour for Entire Intersection Begins at 08:00 AM

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 tdsbay@cs.com

File Name : 8AM FINAL
 Site Code : 00000008
 Start Date : 11/13/2013
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Groups Printed- Bikes

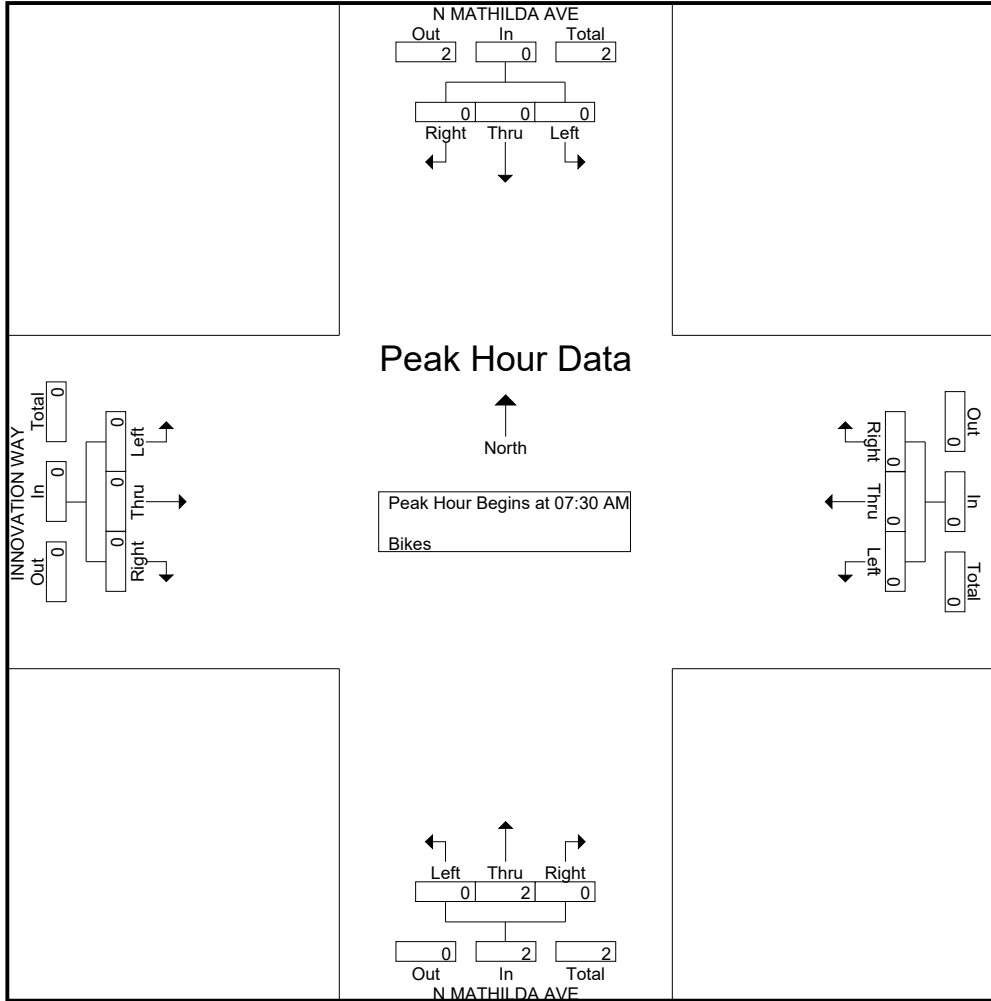
| Start Time | N MATHILDA AVE Southbound | | | | | Westbound | | | | | N MATHILDA AVE Northbound | | | | | INNOVATION WAY Eastbound | | | | | Int. Total |
|-------------|---------------------------|------|------|------|------------|-----------|------|------|------|------------|---------------------------|------|------|------|------------|--------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 |
| Apprch % | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 0 | 100 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total % | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 0 | 100 | 0 | 0 | 0 | 0 | 0 | 0 |

| Start Time | N MATHILDA AVE Southbound | | | | Westbound | | | | N MATHILDA AVE Northbound | | | | INNOVATION WAY Eastbound | | | | Int. Total |
|--|---------------------------|------|------|------------|-----------|------|------|------------|---------------------------|------|------|------------|--------------------------|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 07:30 AM | | | | | | | | | | | | | | | | | |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| % App. Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 100 | 0 | 0 | 0 | 0 | 0 |
| PHF | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .500 | .000 | .500 | .000 | .000 | .000 | .000 | .500 |

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 tdsbay@cs.com

File Name : 8PM FINAL
 Site Code : 00000008
 Start Date : 11/13/2013
 Page No : 1

Groups Printed- Vehicles

| Start Time | N MATHILDA AVE Southbound | | | | | Westbound | | | | | N MATHILDA AVE Northbound | | | | | INNOVATION WAY Eastbound | | | | | Int. Total |
|-------------|---------------------------|------|------|------|------------|-----------|------|------|------|------------|---------------------------|------|------|------|------------|--------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:00 PM | 0 | 258 | 0 | 1 | 259 | 0 | 0 | 0 | 0 | 0 | 0 | 48 | 10 | 1 | 59 | 62 | 0 | 7 | 0 | 69 | 387 |
| 04:15 PM | 4 | 232 | 0 | 5 | 241 | 0 | 0 | 0 | 3 | 3 | 0 | 40 | 8 | 0 | 48 | 63 | 0 | 7 | 0 | 70 | 362 |
| 04:30 PM | 2 | 279 | 0 | 4 | 285 | 0 | 0 | 0 | 0 | 0 | 0 | 37 | 7 | 0 | 44 | 71 | 0 | 10 | 1 | 82 | 411 |
| 04:45 PM | 4 | 237 | 0 | 1 | 242 | 0 | 0 | 0 | 2 | 2 | 0 | 49 | 14 | 0 | 63 | 95 | 0 | 6 | 0 | 101 | 408 |
| Total | 10 | 1006 | 0 | 11 | 1027 | 0 | 0 | 0 | 5 | 5 | 0 | 174 | 39 | 1 | 214 | 291 | 0 | 30 | 1 | 322 | 1568 |
| 05:00 PM | 10 | 343 | 0 | 1 | 354 | 0 | 0 | 0 | 0 | 0 | 0 | 40 | 12 | 0 | 52 | 122 | 0 | 16 | 0 | 138 | 544 |
| 05:15 PM | 11 | 326 | 0 | 0 | 337 | 0 | 0 | 0 | 2 | 2 | 0 | 58 | 11 | 0 | 69 | 117 | 0 | 15 | 1 | 133 | 541 |
| 05:30 PM | 7 | 314 | 0 | 1 | 322 | 0 | 0 | 0 | 1 | 1 | 0 | 44 | 18 | 0 | 62 | 106 | 0 | 15 | 0 | 121 | 506 |
| 05:45 PM | 8 | 291 | 0 | 0 | 299 | 0 | 0 | 0 | 1 | 1 | 0 | 49 | 20 | 0 | 69 | 114 | 0 | 18 | 0 | 132 | 501 |
| Total | 36 | 1274 | 0 | 2 | 1312 | 0 | 0 | 0 | 4 | 4 | 0 | 191 | 61 | 0 | 252 | 459 | 0 | 64 | 1 | 524 | 2092 |
| 06:00 PM | 2 | 287 | 1 | 0 | 290 | 0 | 0 | 0 | 1 | 1 | 0 | 34 | 15 | 0 | 49 | 84 | 0 | 8 | 1 | 93 | 433 |
| 06:15 PM | 1 | 264 | 0 | 0 | 265 | 0 | 0 | 0 | 0 | 0 | 0 | 45 | 10 | 0 | 55 | 76 | 0 | 11 | 0 | 87 | 407 |
| 06:30 PM | 3 | 232 | 0 | 2 | 237 | 0 | 0 | 0 | 2 | 2 | 0 | 30 | 8 | 0 | 38 | 54 | 0 | 9 | 0 | 63 | 340 |
| 06:45 PM | 3 | 189 | 0 | 0 | 192 | 0 | 0 | 0 | 1 | 1 | 0 | 29 | 12 | 0 | 41 | 58 | 0 | 4 | 0 | 62 | 296 |
| Total | 9 | 972 | 1 | 2 | 984 | 0 | 0 | 0 | 4 | 4 | 0 | 138 | 45 | 0 | 183 | 272 | 0 | 32 | 1 | 305 | 1476 |
| Grand Total | 55 | 3252 | 1 | 15 | 3323 | 0 | 0 | 0 | 13 | 13 | 0 | 503 | 145 | 1 | 649 | 1022 | 0 | 126 | 3 | 1151 | 5136 |
| Apprch % | 1.7 | 97.9 | 0 | 0.5 | | 0 | 0 | 0 | 100 | | 0 | 77.5 | 22.3 | 0.2 | | 88.8 | 0 | 10.9 | 0.3 | | |
| Total % | 1.1 | 63.3 | 0 | 0.3 | 64.7 | 0 | 0 | 0 | 0.3 | 0.3 | 0 | 9.8 | 2.8 | 0 | 12.6 | 19.9 | 0 | 2.5 | 0.1 | 22.4 | |

| Start Time | N MATHILDA AVE Southbound | | | | Westbound | | | | N MATHILDA AVE Northbound | | | | INNOVATION WAY Eastbound | | | | Int. Total |
|--------------|---------------------------|------------|------|------------|-----------|------|------|------------|---------------------------|-----------|-----------|------------|--------------------------|------|-----------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| 05:00 PM | 10 | 343 | 0 | 353 | 0 | 0 | 0 | 0 | 0 | 40 | 12 | 52 | 122 | 0 | 16 | 138 | 543 |
| 05:15 PM | 11 | 326 | 0 | 337 | 0 | 0 | 0 | 0 | 0 | 58 | 11 | 69 | 117 | 0 | 15 | 132 | 538 |
| 05:30 PM | 7 | 314 | 0 | 321 | 0 | 0 | 0 | 0 | 0 | 44 | 18 | 62 | 106 | 0 | 15 | 121 | 504 |
| 05:45 PM | 8 | 291 | 0 | 299 | 0 | 0 | 0 | 0 | 0 | 49 | 20 | 69 | 114 | 0 | 18 | 132 | 500 |
| Total Volume | 36 | 1274 | 0 | 1310 | 0 | 0 | 0 | 0 | 0 | 191 | 61 | 252 | 459 | 0 | 64 | 523 | 2085 |
| % App. Total | 2.7 | 97.3 | 0 | | 0 | 0 | 0 | | 0 | 75.8 | 24.2 | | 87.8 | 0 | 12.2 | | |
| PHF | .818 | .929 | .000 | .928 | .000 | .000 | .000 | .000 | .000 | .823 | .763 | .913 | .941 | .000 | .889 | .947 | .960 |

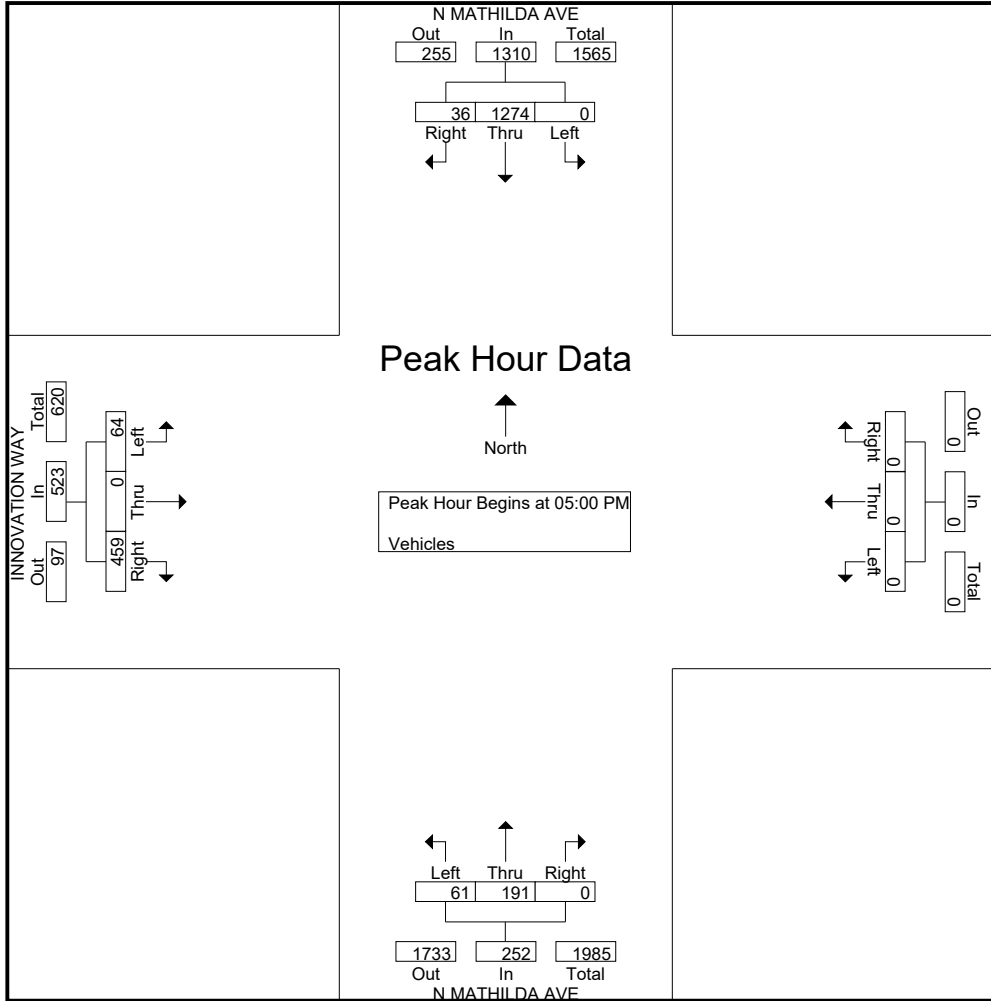
Peak Hour Analysis From 04:00 PM to 06:45 PM - Peak 1 of 1

Peak Hour for Entire Intersection Begins at 05:00 PM

Traffic Data Service

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 Site Code : 00000008
 Start Date : 11/13/2013
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Traffic Data Service

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File Name : 8PM FINAL
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Groups Printed- Bikes

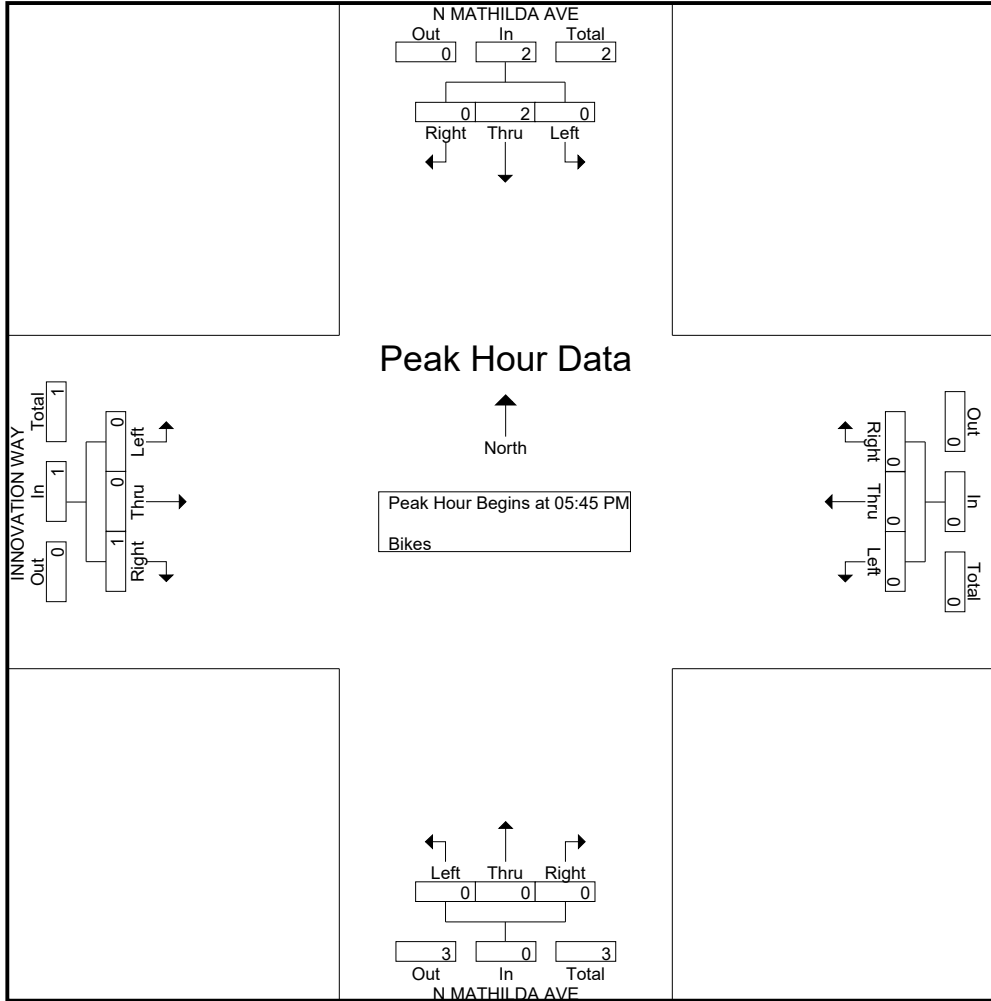
| Start Time | N MATHILDA AVE Southbound | | | | | Westbound | | | | | N MATHILDA AVE Northbound | | | | | INNOVATION WAY Eastbound | | | | | Int. Total |
|--------------------|---------------------------|------|------|------|------------|-----------|------|------|------|------------|---------------------------|------|------|------|------------|--------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:15 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:45 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| Total | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 06:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 06:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 1 |
| 06:30 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 06:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 2 |
| Grand Total | 0 | 3 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 5 |
| Apprch % | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 100 | 0 | 0 | | 100 | 0 | 0 | 0 | | |
| Total % | 0 | 60 | 0 | 0 | 60 | 0 | 0 | 0 | 0 | 0 | 0 | 20 | 0 | 0 | 20 | 20 | 0 | 0 | 0 | 20 | |

| Start Time | N MATHILDA AVE Southbound | | | | Westbound | | | | N MATHILDA AVE Northbound | | | | INNOVATION WAY Eastbound | | | | Int. Total |
|--|---------------------------|------|------|------------|-----------|------|------|------------|---------------------------|------|------|------------|--------------------------|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 04:00 PM to 06:45 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 05:45 PM | | | | | | | | | | | | | | | | | |
| 05:45 PM | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 06:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 06:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 |
| 06:30 PM | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| Total Volume | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 3 |
| % App. Total | 0 | 100 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 100 | 0 | 0 | | |
| PHF | .000 | .500 | .000 | .500 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .250 | .000 | .000 | .250 | .750 |

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 tdsbay@cs.com

File Name : 8PM FINAL
 Site Code : 00000008
 Start Date : 11/13/2013
 Page No : 2



Traffic Data Service

Campbell, CA
 (408) 377-2988
 tdsbay@cs.com

File Name : 5AM FINAL
 Site Code : 00000005
 Start Date : 2/12/2013
 Page No : 1

Groups Printed- Vehicles

| Start Time | MATHILDA AVE Southbound | | | | | MOFFETT PARK DR Westbound | | | | | MATHILDA AVE Northbound | | | | | MOFFETT PARK DR Eastbound | | | | | Int. Total |
|-------------|-------------------------|------|------|------|------------|---------------------------|------|------|------|------------|-------------------------|------|------|------|------------|---------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 3 | 13 | 0 | 0 | 16 | 1 | 7 | 13 | 1 | 22 | 96 | 225 | 84 | 0 | 405 | 11 | 1 | 2 | 0 | 14 | 457 |
| 07:15 AM | 4 | 28 | 0 | 0 | 32 | 3 | 15 | 10 | 1 | 29 | 113 | 246 | 67 | 0 | 426 | 3 | 6 | 3 | 0 | 12 | 499 |
| 07:30 AM | 18 | 26 | 0 | 0 | 44 | 3 | 41 | 16 | 0 | 60 | 142 | 272 | 101 | 0 | 515 | 10 | 2 | 0 | 0 | 12 | 631 |
| 07:45 AM | 23 | 35 | 2 | 0 | 60 | 4 | 40 | 18 | 1 | 63 | 165 | 315 | 123 | 6 | 609 | 14 | 7 | 3 | 0 | 24 | 756 |
| Total | 48 | 102 | 2 | 0 | 152 | 11 | 103 | 57 | 3 | 174 | 516 | 1058 | 375 | 6 | 1955 | 38 | 16 | 8 | 0 | 62 | 2343 |
| 08:00 AM | 18 | 49 | 4 | 1 | 72 | 5 | 38 | 14 | 1 | 58 | 188 | 307 | 125 | 0 | 620 | 13 | 10 | 4 | 0 | 27 | 777 |
| 08:15 AM | 20 | 46 | 3 | 0 | 69 | 4 | 39 | 15 | 1 | 59 | 182 | 334 | 131 | 0 | 647 | 4 | 11 | 4 | 0 | 19 | 794 |
| 08:30 AM | 26 | 44 | 1 | 0 | 71 | 5 | 36 | 17 | 1 | 59 | 171 | 325 | 109 | 0 | 605 | 15 | 14 | 6 | 0 | 35 | 770 |
| 08:45 AM | 18 | 57 | 0 | 0 | 75 | 7 | 47 | 26 | 1 | 81 | 182 | 396 | 146 | 0 | 724 | 6 | 12 | 7 | 0 | 25 | 905 |
| Total | 82 | 196 | 8 | 1 | 287 | 21 | 160 | 72 | 4 | 257 | 723 | 1362 | 511 | 0 | 2596 | 38 | 47 | 21 | 0 | 106 | 3246 |
| Grand Total | 130 | 298 | 10 | 1 | 439 | 32 | 263 | 129 | 7 | 431 | 1239 | 2420 | 886 | 6 | 4551 | 76 | 63 | 29 | 0 | 168 | 5589 |
| Apprch % | 29.6 | 67.9 | 2.3 | 0.2 | | 7.4 | 61 | 29.9 | 1.6 | | 27.2 | 53.2 | 19.5 | 0.1 | | 45.2 | 37.5 | 17.3 | 0 | | |
| Total % | 2.3 | 5.3 | 0.2 | 0 | 7.9 | 0.6 | 4.7 | 2.3 | 0.1 | 7.7 | 22.2 | 43.3 | 15.9 | 0.1 | 81.4 | 1.4 | 1.1 | 0.5 | 0 | 3 | |

| Start Time | MATHILDA AVE Southbound | | | | | MOFFETT PARK DR Westbound | | | | | MATHILDA AVE Northbound | | | | | MOFFETT PARK DR Eastbound | | | | | Int. Total |
|--|-------------------------|-----------|----------|----------|------------|---------------------------|-----------|-----------|----------|------------|-------------------------|------------|------------|------|------------|---------------------------|-----------|----------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 08:00 AM | | | | | | | | | | | | | | | | | | | | | |
| 08:00 AM | 18 | 49 | 4 | 1 | 72 | 5 | 38 | 14 | 1 | 58 | 188 | 307 | 125 | 0 | 620 | 13 | 10 | 4 | 0 | 27 | 777 |
| 08:15 AM | 20 | 46 | 3 | 0 | 69 | 4 | 39 | 15 | 1 | 59 | 182 | 334 | 131 | 0 | 647 | 4 | 11 | 4 | 0 | 19 | 794 |
| 08:30 AM | 26 | 44 | 1 | 0 | 71 | 5 | 36 | 17 | 1 | 59 | 171 | 325 | 109 | 0 | 605 | 15 | 14 | 6 | 0 | 35 | 770 |
| 08:45 AM | 18 | 57 | 0 | 0 | 75 | 7 | 47 | 26 | 1 | 81 | 182 | 396 | 146 | 0 | 724 | 6 | 12 | 7 | 0 | 25 | 905 |
| Total Volume | 82 | 196 | 8 | 1 | 287 | 21 | 160 | 72 | 4 | 257 | 723 | 1362 | 511 | 0 | 2596 | 38 | 47 | 21 | 0 | 106 | 3246 |
| % App. Total | | | | | | | | | | | | | | | | | | | | | |
| PHF | .788 | .860 | .500 | .250 | .957 | .750 | .851 | .692 | 1.00 | .793 | .961 | .860 | .875 | .000 | .896 | .633 | .839 | .750 | .000 | .757 | .897 |

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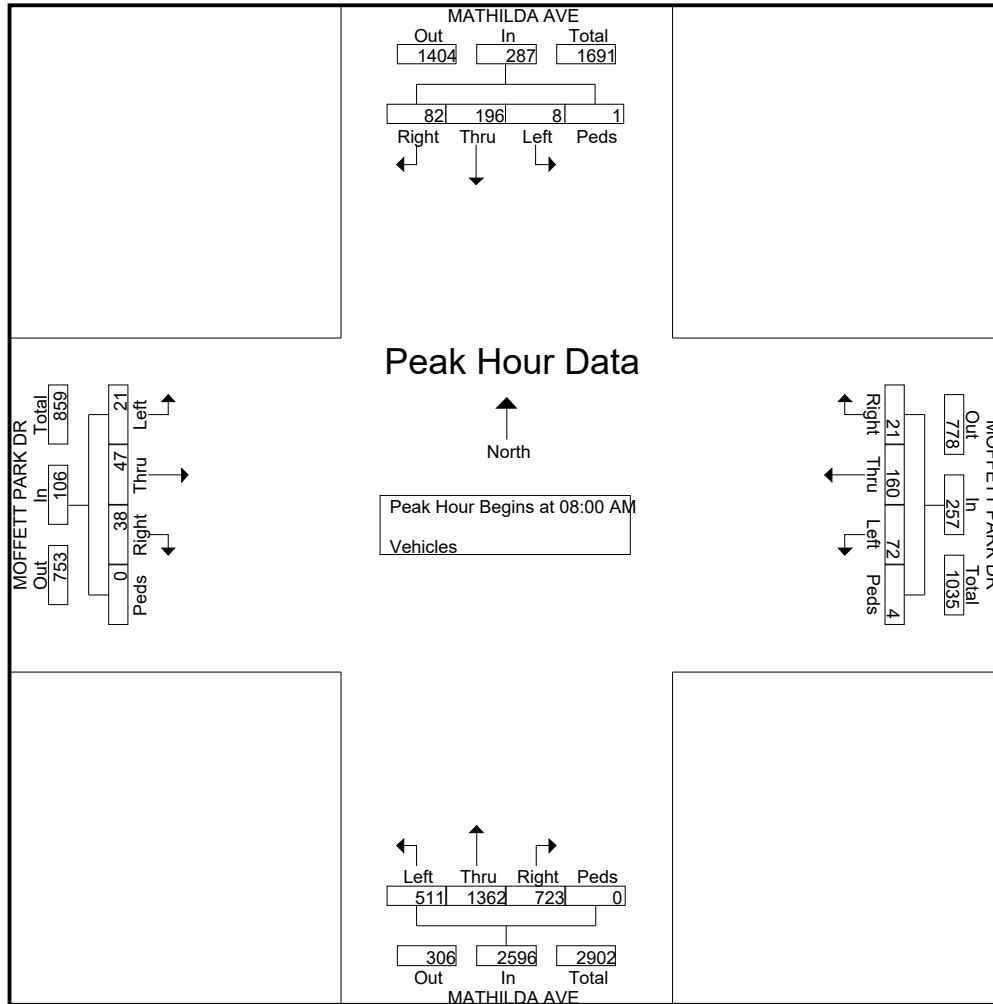
idsbay@cs.com

File Name : 5AM FINAL

Site Code : 00000005

Start Date : 2/12/2013

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 tdsbay@cs.com

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 Site Code : 00000005
 Start Date : 2/12/2013
 Page No : 1

Groups Printed- Bikes

| Start Time | MATHILDA AVE Southbound | | | | | MOFFETT PARK DR Westbound | | | | | MATHILDA AVE Northbound | | | | | MOFFETT PARK DR Eastbound | | | | | Int. Total | | | | | |
|--------------------|-------------------------|------|------|------|------------|---------------------------|------|------|------|------------|-------------------------|------|------|------|------------|---------------------------|------|------|------|------------|------------|------|---|---|------|----|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | | | | | | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 2 | 0 | 2 | 0 | 0 | 2 | 3 |
| 07:15 AM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 3 |
| 07:30 AM | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 0 | 0 | 5 | 0 | 1 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 2 | 8 |
| Total | 0 | 1 | 1 | 0 | 2 | 1 | 5 | 0 | 0 | 6 | 1 | 3 | 0 | 0 | 4 | 0 | 4 | 1 | 0 | 5 | 0 | 5 | 0 | 0 | 5 | 17 |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 0 | 3 | 0 | 0 | 3 | 3 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 1 | 0 | 4 | 0 | 0 | 4 | 0 | 4 | 0 | 0 | 4 | 7 |
| 08:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 5 | 0 | 5 | 0 | 0 | 5 | 7 |
| 08:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 3 | 0 | 0 | 3 | 0 | 3 | 0 | 0 | 3 | 5 |
| Total | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 0 | 0 | 5 | 0 | 2 | 0 | 0 | 2 | 0 | 15 | 0 | 0 | 15 | 0 | 15 | 0 | 0 | 15 | 22 |
| Grand Total | 0 | 1 | 1 | 0 | 2 | 2 | 9 | 0 | 0 | 11 | 1 | 5 | 0 | 0 | 6 | 0 | 19 | 1 | 0 | 20 | 0 | 20 | 0 | 0 | 20 | 39 |
| Apprch % | 0 | 50 | 50 | 0 | | 18.2 | 81.8 | 0 | 0 | | 16.7 | 83.3 | 0 | 0 | | 0 | 95 | 5 | 0 | | 0 | 95 | 5 | 0 | | |
| Total % | 0 | 2.6 | 2.6 | 0 | 5.1 | 5.1 | 23.1 | 0 | 0 | 28.2 | 2.6 | 12.8 | 0 | 0 | 15.4 | 0 | 48.7 | 2.6 | 0 | 51.3 | 0 | 51.3 | 0 | 0 | 51.3 | |

| Start Time | MATHILDA AVE Southbound | | | | | MOFFETT PARK DR Westbound | | | | | MATHILDA AVE Northbound | | | | | MOFFETT PARK DR Eastbound | | | | | Int. Total | | | | | |
|---------------------|-------------------------|------|------|------|------------|---------------------------|------|------|------|------------|-------------------------|------|------|------|------------|---------------------------|------|------|------|------------|------------|------|------|------|------|----|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | | | | | | |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 0 | 0 | 5 | 0 | 1 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 2 | 8 |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 0 | 3 | 0 | 0 | 3 | 3 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 1 | 0 | 4 | 0 | 0 | 4 | 0 | 4 | 0 | 0 | 4 | 7 |
| 08:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 5 | 0 | 5 | 0 | 0 | 5 | 7 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 2 | 7 | 0 | 0 | 9 | 0 | 2 | 0 | 0 | 2 | 0 | 14 | 0 | 0 | 14 | 0 | 14 | 0 | 0 | 14 | 25 |
| % App. Total | 0 | 0 | 0 | 0 | | 22.2 | 77.8 | 0 | 0 | | 0 | 100 | 0 | 0 | | 0 | 100 | 0 | 0 | | 0 | 100 | 0 | 0 | | |
| PHF | .000 | .000 | .000 | .000 | .000 | .500 | .438 | .000 | .000 | .450 | .000 | .500 | .000 | .000 | .500 | .000 | .700 | .000 | .000 | .700 | .000 | .781 | .000 | .000 | .781 | |

Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1

Peak Hour for Entire Intersection Begins at 07:45 AM

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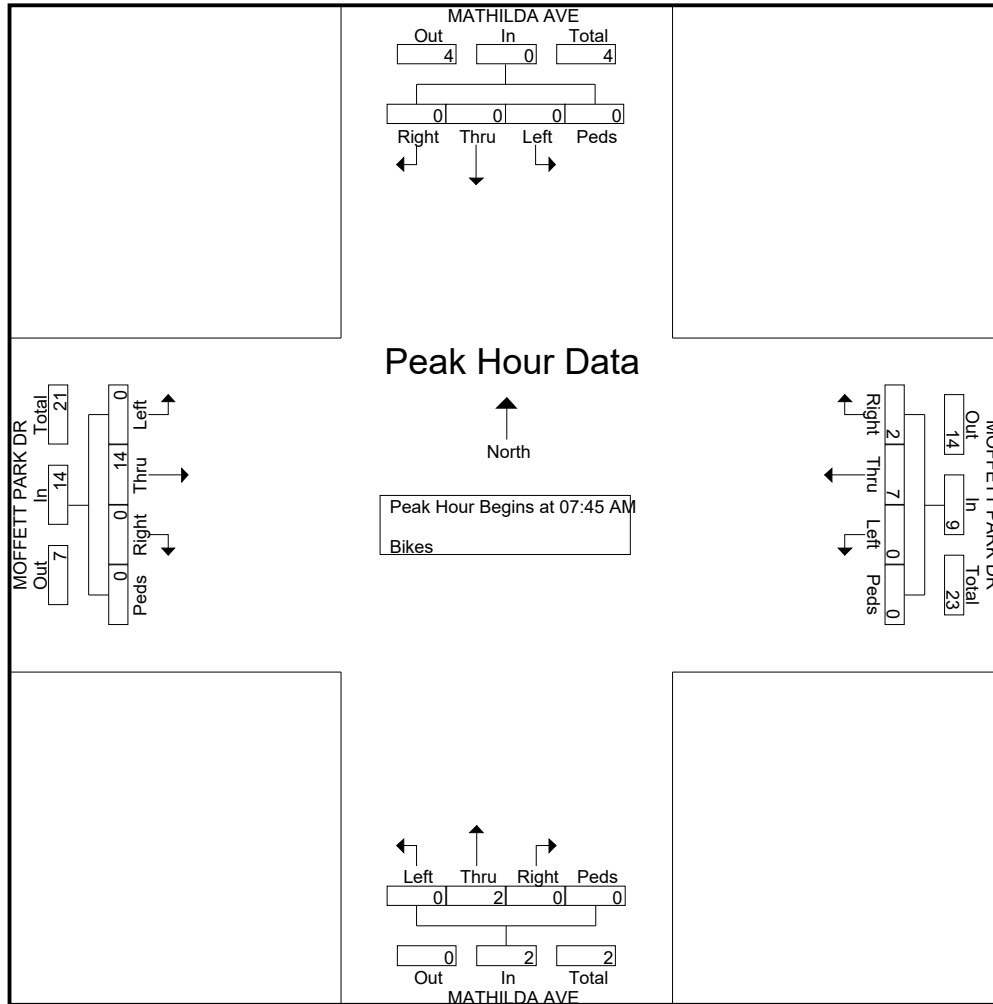
idsbay@cs.com

File Name : 5AM FINAL

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Site Code : 00000005

Start Date : 2/12/2013

Page No : 1

Groups Printed- Vehicles

| Start Time | MATHILDA AVE Southbound | | | | | MOFFETT PARK DR Westbound | | | | | MATHILDA AVE Northbound | | | | | MOFFETT PARK DR Eastbound | | | | | Int. Total |
|--------------------|-------------------------|-------------|-----------|----------|-------------|---------------------------|------------|------------|------------|-------------|-------------------------|------------|------------|----------|-------------|---------------------------|------------|------------|----------|-------------|-------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:30 PM | 14 | 334 | 4 | 0 | 352 | 3 | 36 | 73 | 1 | 113 | 50 | 41 | 18 | 0 | 109 | 73 | 4 | 3 | 0 | 80 | 654 |
| 04:45 PM | 12 | 357 | 2 | 0 | 371 | 3 | 38 | 86 | 1 | 128 | 27 | 46 | 13 | 0 | 86 | 56 | 12 | 7 | 0 | 75 | 660 |
| Total | 26 | 691 | 6 | 0 | 723 | 6 | 74 | 159 | 2 | 241 | 77 | 87 | 31 | 0 | 195 | 129 | 16 | 10 | 0 | 155 | 1314 |
| 05:00 PM | 12 | 408 | 3 | 0 | 423 | 2 | 50 | 79 | 3 | 134 | 23 | 54 | 25 | 0 | 102 | 57 | 16 | 5 | 0 | 78 | 737 |
| 05:15 PM | 17 | 403 | 17 | 1 | 438 | 6 | 70 | 61 | 3 | 140 | 31 | 66 | 20 | 0 | 117 | 55 | 12 | 6 | 0 | 73 | 768 |
| 05:30 PM | 21 | 439 | 9 | 0 | 469 | 6 | 65 | 52 | 7 | 130 | 44 | 77 | 19 | 0 | 140 | 55 | 16 | 7 | 0 | 78 | 817 |
| 05:45 PM | 21 | 387 | 5 | 1 | 414 | 6 | 52 | 93 | 4 | 155 | 31 | 60 | 20 | 0 | 111 | 68 | 12 | 5 | 0 | 85 | 765 |
| Total | 71 | 1637 | 34 | 2 | 1744 | 20 | 237 | 285 | 17 | 559 | 129 | 257 | 84 | 0 | 470 | 235 | 56 | 23 | 0 | 314 | 3087 |
| 06:00 PM | 20 | 362 | 8 | 0 | 390 | 3 | 72 | 90 | 0 | 165 | 20 | 36 | 12 | 0 | 68 | 53 | 7 | 7 | 0 | 67 | 690 |
| 06:15 PM | 20 | 341 | 9 | 0 | 370 | 3 | 49 | 100 | 1 | 153 | 28 | 52 | 7 | 0 | 87 | 49 | 8 | 2 | 0 | 59 | 669 |
| Grand Total | 137 | 3031 | 57 | 2 | 3227 | 32 | 432 | 634 | 20 | 1118 | 254 | 432 | 134 | 0 | 820 | 466 | 87 | 42 | 0 | 595 | 5760 |
| Apprch % | 4.2 | 93.9 | 1.8 | 0.1 | | 2.9 | 38.6 | 56.7 | 1.8 | | 31 | 52.7 | 16.3 | 0 | | 78.3 | 14.6 | 7.1 | 0 | | |
| Total % | 2.4 | 52.6 | 1 | 0 | 56 | 0.6 | 7.5 | 11 | 0.3 | 19.4 | 4.4 | 7.5 | 2.3 | 0 | 14.2 | 8.1 | 1.5 | 0.7 | 0 | 10.3 | |

| Start Time | MATHILDA AVE Southbound | | | | | MOFFETT PARK DR Westbound | | | | | MATHILDA AVE Northbound | | | | | MOFFETT PARK DR Eastbound | | | | | Int. Total |
|--|-------------------------|------------|-----------|----------|------------|---------------------------|-----------|-----------|----------|------------|-------------------------|-----------|-----------|------|------------|---------------------------|-----------|----------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| Peak Hour Analysis From 04:30 PM to 06:15 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 05:00 PM | | | | | | | | | | | | | | | | | | | | | |
| 05:00 PM | 12 | 408 | 3 | 0 | 423 | 2 | 50 | 79 | 3 | 134 | 23 | 54 | 25 | 0 | 102 | 57 | 16 | 5 | 0 | 78 | 737 |
| 05:15 PM | 17 | 403 | 17 | 1 | 438 | 6 | 70 | 61 | 3 | 140 | 31 | 66 | 20 | 0 | 117 | 55 | 12 | 6 | 0 | 73 | 768 |
| 05:30 PM | 21 | 439 | 9 | 0 | 469 | 6 | 65 | 52 | 7 | 130 | 44 | 77 | 19 | 0 | 140 | 55 | 16 | 7 | 0 | 78 | 817 |
| 05:45 PM | 21 | 387 | 5 | 1 | 414 | 6 | 52 | 93 | 4 | 155 | 31 | 60 | 20 | 0 | 111 | 68 | 12 | 5 | 0 | 85 | 765 |
| Total Volume | 71 | 1637 | 34 | 2 | 1744 | 20 | 237 | 285 | 17 | 559 | 129 | 257 | 84 | 0 | 470 | 235 | 56 | 23 | 0 | 314 | 3087 |
| % App. Total | | | | | | | | | | | | | | | | | | | | | |
| PHF | .845 | .932 | .500 | .500 | .930 | .833 | .846 | .766 | .607 | .902 | .733 | .834 | .840 | .000 | .839 | .864 | .875 | .821 | .000 | .924 | .945 |

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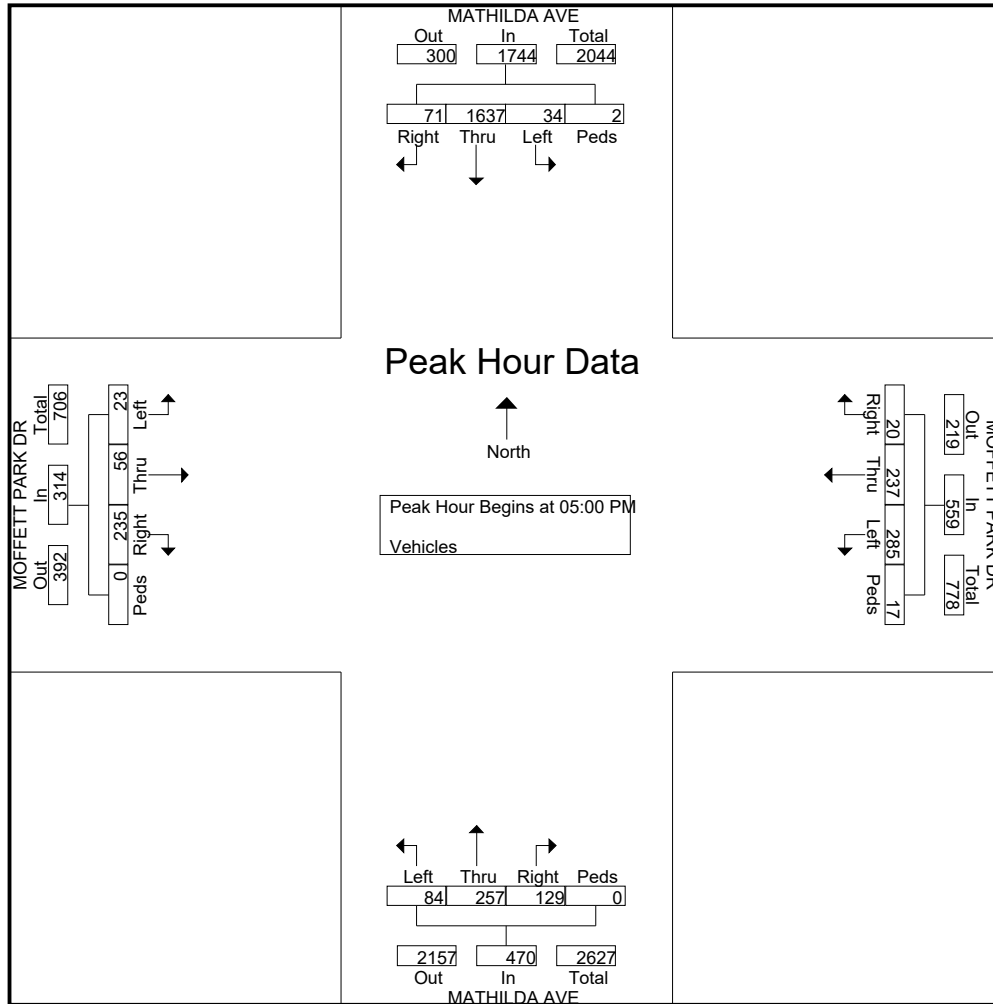
idsbay@cs.com

File Name : 5PM FINAL

Site Code : 00000005

Start Date : 2/12/2013

Page No : 2



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 tdsbay@cs.com

File Name : 5PM FINAL
 Site Code : 00000005
 Start Date : 2/12/2013
 Page No : 1

Groups Printed- Bikes

| Start Time | MATHILDA AVE Southbound | | | | | MOFFETT PARK DR Westbound | | | | | MATHILDA AVE Northbound | | | | | MOFFETT PARK DR Eastbound | | | | | Int. Total |
|-------------|-------------------------|------|------|------|------------|---------------------------|------|------|------|------------|-------------------------|------|------|------|------------|---------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 5 |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 8 |
| 05:30 PM | 0 | 1 | 0 | 0 | 1 | 0 | 6 | 0 | 0 | 6 | 0 | 1 | 0 | 0 | 1 | 0 | 3 | 0 | 0 | 3 | 11 |
| 05:45 PM | 0 | 1 | 0 | 0 | 1 | 1 | 3 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 1 | 0 | 6 | 11 |
| Total | 0 | 2 | 0 | 0 | 2 | 1 | 16 | 0 | 0 | 17 | 0 | 1 | 0 | 0 | 1 | 0 | 14 | 1 | 0 | 15 | 35 |
| 06:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 1 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 8 |
| 06:15 PM | 0 | 0 | 0 | 0 | 0 | 1 | 6 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| Grand Total | 0 | 2 | 0 | 0 | 2 | 2 | 28 | 1 | 0 | 31 | 0 | 2 | 0 | 0 | 2 | 0 | 16 | 1 | 0 | 17 | 52 |
| Apprch % | 0 | 100 | 0 | 0 | | 6.5 | 90.3 | 3.2 | 0 | | 0 | 100 | 0 | 0 | | 0 | 94.1 | 5.9 | 0 | | |
| Total % | 0 | 3.8 | 0 | 0 | 3.8 | 3.8 | 53.8 | 1.9 | 0 | 59.6 | 0 | 3.8 | 0 | 0 | 3.8 | 0 | 30.8 | 1.9 | 0 | 32.7 | |

| Start Time | MATHILDA AVE Southbound | | | | | MOFFETT PARK DR Westbound | | | | | MATHILDA AVE Northbound | | | | | MOFFETT PARK DR Eastbound | | | | | Int. Total |
|--------------|-------------------------|------|------|------|------------|---------------------------|------|------|------|------------|-------------------------|------|------|------|------------|---------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 8 |
| 05:30 PM | 0 | 1 | 0 | 0 | 1 | 0 | 6 | 0 | 0 | 6 | 0 | 1 | 0 | 0 | 1 | 0 | 3 | 0 | 0 | 3 | 11 |
| 05:45 PM | 0 | 1 | 0 | 0 | 1 | 1 | 3 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 1 | 0 | 6 | 11 |
| 06:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 1 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 8 |
| Total Volume | 0 | 2 | 0 | 0 | 2 | 1 | 19 | 1 | 0 | 21 | 0 | 1 | 0 | 0 | 1 | 0 | 13 | 1 | 0 | 14 | 38 |
| % App. Total | 0 | 100 | 0 | 0 | | 4.8 | 90.5 | 4.8 | 0 | | 0 | 100 | 0 | 0 | | 0 | 92.9 | 7.1 | 0 | | |
| PHF | .000 | .500 | .000 | .000 | .500 | .250 | .792 | .250 | .000 | .875 | .000 | .250 | .000 | .000 | .250 | .000 | .650 | .250 | .000 | .583 | .864 |

Peak Hour Analysis From 04:30 PM to 06:15 PM - Peak 1 of 1

Peak Hour for Entire Intersection Begins at 05:15 PM

Traffic Data Service

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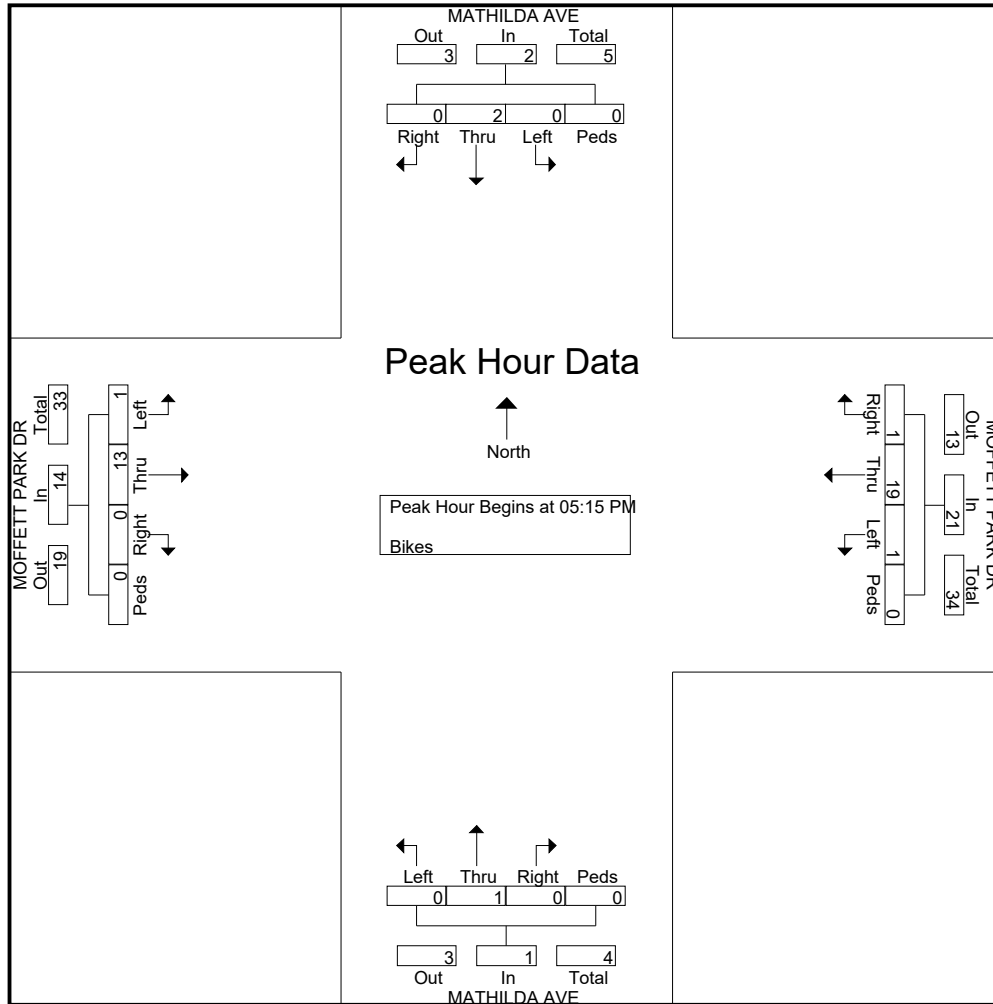
idsbay@cs.com

File Name : 5PM FINAL

Site Code : 00000005

Start Date : 2/12/2013

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 Site Code : 00000006
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Groups Printed- Vehicles

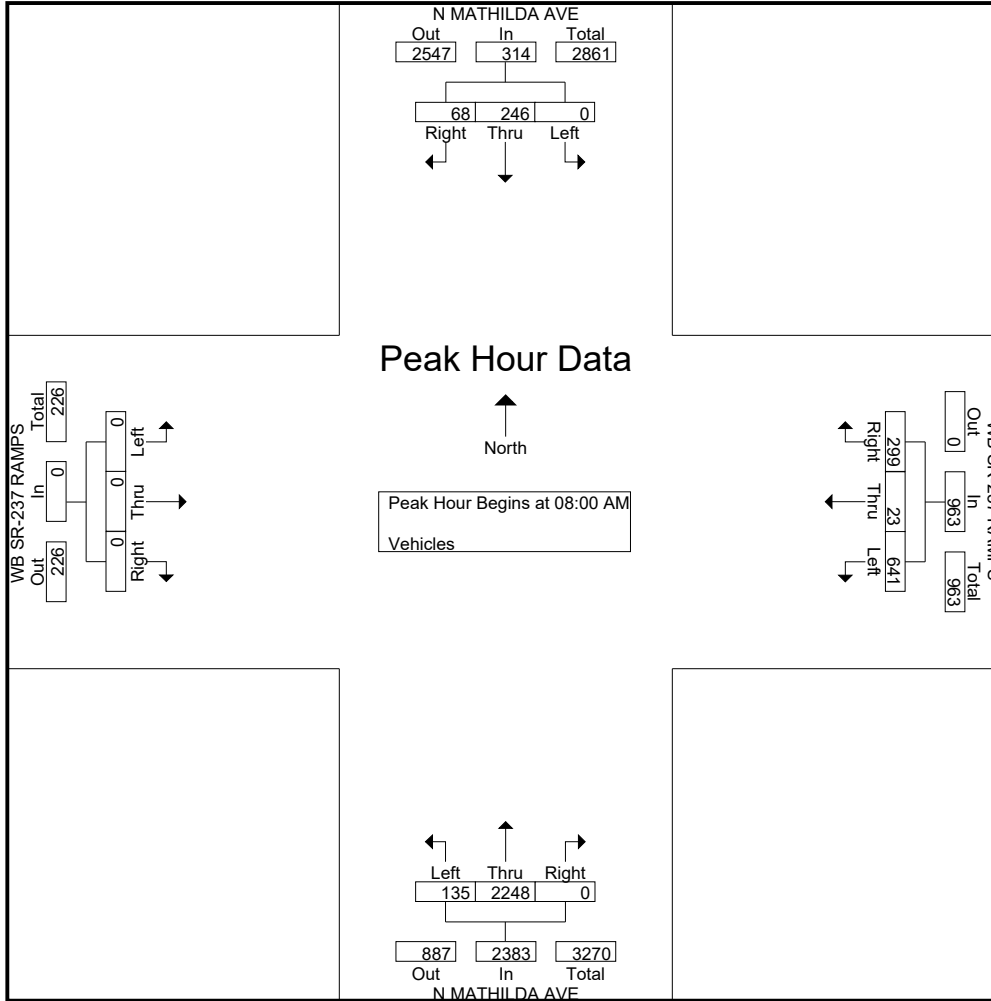
| Start Time | N MATHILDA AVE Southbound | | | | | WB SR-237 RAMPS Westbound | | | | | N MATHILDA AVE Northbound | | | | | WB SR-237 RAMPS Eastbound | | | | | Int. Total |
|-------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 10 | 22 | 0 | 0 | 32 | 46 | 0 | 118 | 0 | 164 | 0 | 358 | 32 | 0 | 390 | 0 | 0 | 0 | 0 | 0 | 586 |
| 07:15 AM | 9 | 27 | 0 | 0 | 36 | 58 | 0 | 124 | 0 | 182 | 0 | 413 | 23 | 0 | 436 | 0 | 0 | 0 | 0 | 0 | 654 |
| 07:30 AM | 13 | 34 | 0 | 0 | 47 | 83 | 0 | 126 | 0 | 209 | 0 | 411 | 37 | 0 | 448 | 0 | 0 | 0 | 0 | 0 | 704 |
| 07:45 AM | 19 | 50 | 0 | 1 | 70 | 62 | 0 | 170 | 0 | 232 | 0 | 534 | 38 | 0 | 572 | 0 | 0 | 0 | 0 | 0 | 874 |
| Total | 51 | 133 | 0 | 1 | 185 | 249 | 0 | 538 | 0 | 787 | 0 | 1716 | 130 | 0 | 1846 | 0 | 0 | 0 | 0 | 0 | 2818 |
| 08:00 AM | 9 | 59 | 0 | 0 | 68 | 73 | 12 | 137 | 3 | 225 | 0 | 520 | 37 | 0 | 557 | 0 | 0 | 0 | 0 | 0 | 850 |
| 08:15 AM | 25 | 61 | 0 | 0 | 86 | 62 | 7 | 148 | 5 | 222 | 0 | 567 | 45 | 0 | 612 | 0 | 0 | 0 | 0 | 0 | 920 |
| 08:30 AM | 16 | 59 | 0 | 0 | 75 | 83 | 3 | 145 | 1 | 232 | 0 | 534 | 29 | 0 | 563 | 0 | 0 | 0 | 0 | 0 | 870 |
| 08:45 AM | 18 | 67 | 0 | 0 | 85 | 81 | 1 | 211 | 3 | 296 | 0 | 627 | 24 | 0 | 651 | 0 | 0 | 0 | 0 | 0 | 1032 |
| Total | 68 | 246 | 0 | 0 | 314 | 299 | 23 | 641 | 12 | 975 | 0 | 2248 | 135 | 0 | 2383 | 0 | 0 | 0 | 0 | 0 | 3672 |
| Grand Total | 119 | 379 | 0 | 1 | 499 | 548 | 23 | 1179 | 12 | 1762 | 0 | 3964 | 265 | 0 | 4229 | 0 | 0 | 0 | 0 | 0 | 6490 |
| Apprch % | 23.8 | 76 | 0 | 0.2 | | 31.1 | 1.3 | 66.9 | 0.7 | | 0 | 93.7 | 6.3 | 0 | | 0 | 0 | 0 | 0 | 0 | |
| Total % | 1.8 | 5.8 | 0 | 0 | 7.7 | 8.4 | 0.4 | 18.2 | 0.2 | 27.1 | 0 | 61.1 | 4.1 | 0 | 65.2 | 0 | 0 | 0 | 0 | 0 | |

| Start Time | N MATHILDA AVE Southbound | | | | WB SR-237 RAMPS Westbound | | | | N MATHILDA AVE Northbound | | | | WB SR-237 RAMPS Eastbound | | | | Int. Total |
|--|------------------------------|-----------|------|------------|------------------------------|-----------|------------|------------|------------------------------|------------|-----------|------------|------------------------------|------|------|------------|-------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 08:00 AM | | | | | | | | | | | | | | | | | |
| 08:00 AM | 9 | 59 | 0 | 68 | 73 | 12 | 137 | 222 | 0 | 520 | 37 | 557 | 0 | 0 | 0 | 0 | 847 |
| 08:15 AM | 25 | 61 | 0 | 86 | 62 | 7 | 148 | 217 | 0 | 567 | 45 | 612 | 0 | 0 | 0 | 0 | 915 |
| 08:30 AM | 16 | 59 | 0 | 75 | 83 | 3 | 145 | 231 | 0 | 534 | 29 | 563 | 0 | 0 | 0 | 0 | 869 |
| 08:45 AM | 18 | 67 | 0 | 85 | 81 | 1 | 211 | 293 | 0 | 627 | 24 | 651 | 0 | 0 | 0 | 0 | 1029 |
| Total Volume | 68 | 246 | 0 | 314 | 299 | 23 | 641 | 963 | 0 | 2248 | 135 | 2383 | 0 | 0 | 0 | 0 | 3660 |
| % App. Total | 21.7 | 78.3 | 0 | | 31 | 2.4 | 66.6 | | 0 | 94.3 | 5.7 | | 0 | 0 | 0 | | |
| PHF | .680 | .918 | .000 | .913 | .901 | .479 | .759 | .822 | .000 | .896 | .750 | .915 | .000 | .000 | .000 | .000 | .889 |

Traffic Data Service

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 Site Code : 00000006
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Groups Printed- Bikes

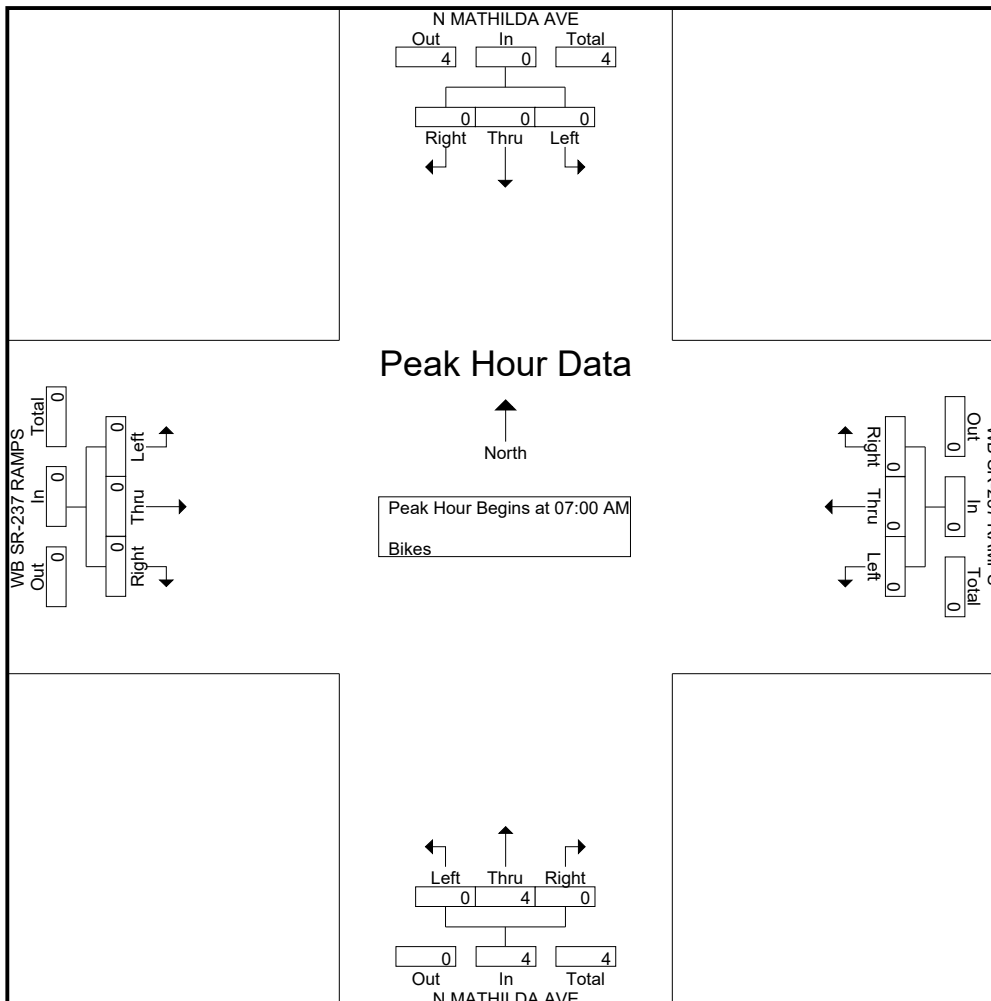
| Start Time | N MATHILDA AVE Southbound | | | | | WB SR-237 RAMPS Westbound | | | | | N MATHILDA AVE Northbound | | | | | WB SR-237 RAMPS Eastbound | | | | | Int. Total | | | | | |
|-------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------|---|---|---|---|---|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | | | | | | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| Apprch % | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 0 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Total % | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 0 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |

| Start Time | N MATHILDA AVE Southbound | | | | WB SR-237 RAMPS Westbound | | | | N MATHILDA AVE Northbound | | | | WB SR-237 RAMPS Eastbound | | | | Int. Total | | | | |
|--|------------------------------|------|------|------------|------------------------------|------|------|------------|------------------------------|------|------|------------|------------------------------|------|------|------------|------------|------|------|------|------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | | | | | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 07:00 AM | | | | | | | | | | | | | | | | | | | | | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| % App. Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| PHF | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .500 | .000 | .500 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .500 |

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Groups Printed- Vehicles

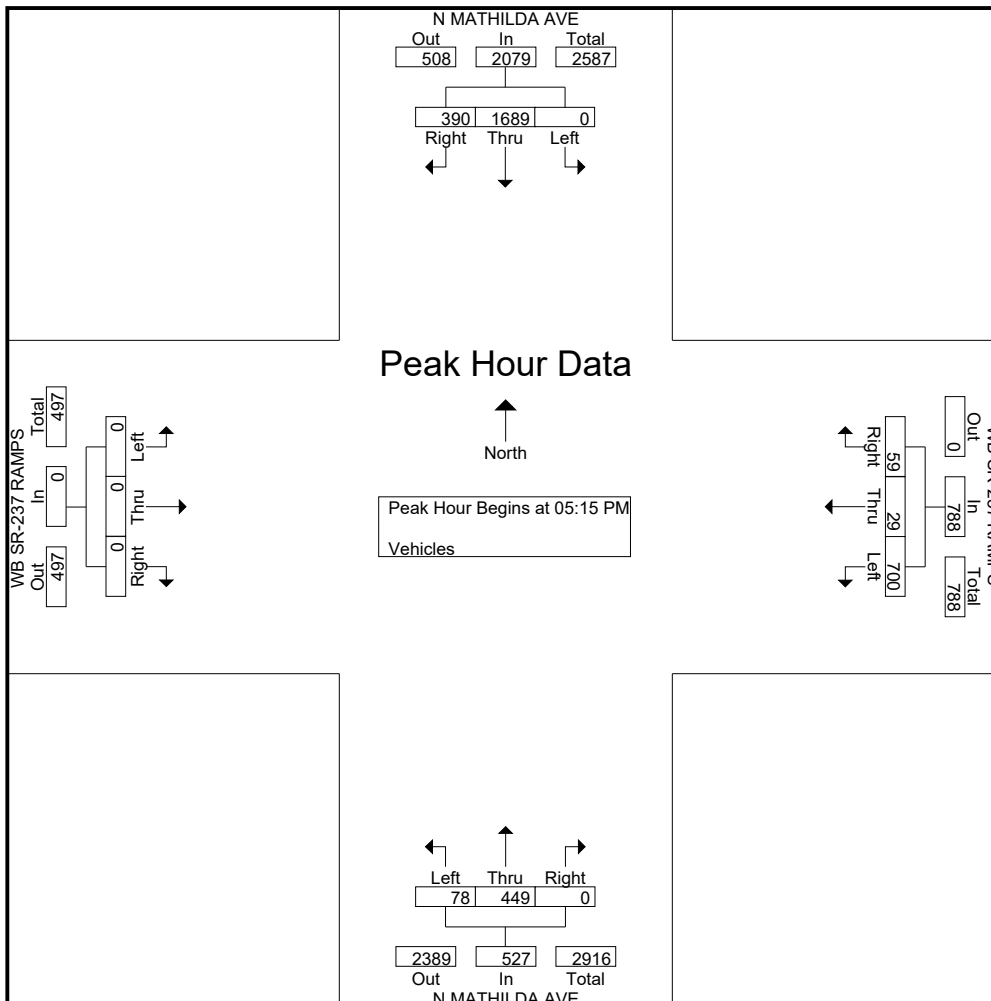
| Start Time | N MATHILDA AVE Southbound | | | | | WB SR-237 RAMPS Westbound | | | | | N MATHILDA AVE Northbound | | | | | WB SR-237 RAMPS Eastbound | | | | | Int. Total |
|-------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:00 PM | 80 | 328 | 0 | 0 | 408 | 10 | 2 | 109 | 2 | 123 | 0 | 113 | 23 | 0 | 136 | 0 | 0 | 0 | 0 | 0 | 667 |
| 04:15 PM | 70 | 283 | 0 | 0 | 353 | 15 | 8 | 125 | 1 | 149 | 0 | 88 | 14 | 0 | 102 | 0 | 0 | 0 | 0 | 0 | 604 |
| 04:30 PM | 76 | 340 | 0 | 0 | 416 | 6 | 4 | 121 | 2 | 133 | 0 | 83 | 26 | 0 | 109 | 0 | 0 | 0 | 0 | 0 | 658 |
| 04:45 PM | 78 | 440 | 0 | 0 | 518 | 12 | 2 | 149 | 1 | 164 | 0 | 102 | 20 | 0 | 122 | 0 | 0 | 0 | 0 | 0 | 804 |
| Total | 304 | 1391 | 0 | 0 | 1695 | 43 | 16 | 504 | 6 | 569 | 0 | 386 | 83 | 0 | 469 | 0 | 0 | 0 | 0 | 0 | 2733 |
| 05:00 PM | 120 | 403 | 0 | 0 | 523 | 11 | 4 | 169 | 3 | 187 | 0 | 99 | 24 | 0 | 123 | 0 | 0 | 0 | 0 | 0 | 833 |
| 05:15 PM | 119 | 499 | 0 | 0 | 618 | 8 | 4 | 178 | 2 | 192 | 0 | 111 | 27 | 0 | 138 | 0 | 0 | 0 | 0 | 0 | 948 |
| 05:30 PM | 88 | 410 | 0 | 0 | 498 | 12 | 1 | 175 | 3 | 191 | 0 | 107 | 17 | 0 | 124 | 0 | 0 | 0 | 0 | 0 | 813 |
| 05:45 PM | 76 | 373 | 0 | 0 | 449 | 20 | 8 | 187 | 1 | 216 | 0 | 120 | 14 | 0 | 134 | 0 | 0 | 0 | 0 | 0 | 799 |
| Total | 403 | 1685 | 0 | 0 | 2088 | 51 | 17 | 709 | 9 | 786 | 0 | 437 | 82 | 0 | 519 | 0 | 0 | 0 | 0 | 0 | 3393 |
| 06:00 PM | 107 | 407 | 0 | 0 | 514 | 19 | 16 | 160 | 4 | 199 | 0 | 111 | 20 | 0 | 131 | 0 | 0 | 0 | 0 | 0 | 844 |
| 06:15 PM | 100 | 402 | 0 | 0 | 502 | 16 | 6 | 179 | 0 | 201 | 0 | 91 | 15 | 0 | 106 | 0 | 0 | 0 | 0 | 0 | 809 |
| 06:30 PM | 98 | 333 | 0 | 0 | 431 | 8 | 10 | 181 | 5 | 204 | 0 | 73 | 22 | 0 | 95 | 0 | 0 | 0 | 0 | 0 | 730 |
| 06:45 PM | 99 | 300 | 0 | 0 | 399 | 11 | 4 | 179 | 0 | 194 | 0 | 59 | 19 | 0 | 78 | 0 | 0 | 0 | 0 | 0 | 671 |
| Total | 404 | 1442 | 0 | 0 | 1846 | 54 | 36 | 699 | 9 | 798 | 0 | 334 | 76 | 0 | 410 | 0 | 0 | 0 | 0 | 0 | 3054 |
| Grand Total | 1111 | 4518 | 0 | 0 | 5629 | 148 | 69 | 1912 | 24 | 2153 | 0 | 1157 | 241 | 0 | 1398 | 0 | 0 | 0 | 0 | 0 | 9180 |
| Apprch % | 19.7 | 80.3 | 0 | 0 | | 6.9 | 3.2 | 88.8 | 1.1 | | 0 | 82.8 | 17.2 | 0 | | 0 | 0 | 0 | 0 | | |
| Total % | 12.1 | 49.2 | 0 | 0 | 61.3 | 1.6 | 0.8 | 20.8 | 0.3 | 23.5 | 0 | 12.6 | 2.6 | 0 | 15.2 | 0 | 0 | 0 | 0 | | |

| Start Time | N MATHILDA AVE Southbound | | | | WB SR-237 RAMPS Westbound | | | | N MATHILDA AVE Northbound | | | | WB SR-237 RAMPS Eastbound | | | | Int. Total |
|--|------------------------------|------------|------|------------|------------------------------|-----------|------------|------------|------------------------------|------------|-----------|------------|------------------------------|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 04:00 PM to 06:45 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 05:15 PM | | | | | | | | | | | | | | | | | |
| 05:15 PM | 119 | 499 | 0 | 618 | 8 | 4 | 178 | 190 | 0 | 111 | 27 | 138 | 0 | 0 | 0 | 0 | 946 |
| 05:30 PM | 88 | 410 | 0 | 498 | 12 | 1 | 175 | 188 | 0 | 107 | 17 | 124 | 0 | 0 | 0 | 0 | 810 |
| 05:45 PM | 76 | 373 | 0 | 449 | 20 | 8 | 187 | 215 | 0 | 120 | 14 | 134 | 0 | 0 | 0 | 0 | 798 |
| 06:00 PM | 107 | 407 | 0 | 514 | 19 | 16 | 160 | 195 | 0 | 111 | 20 | 131 | 0 | 0 | 0 | 0 | 840 |
| Total Volume | 390 | 1689 | 0 | 2079 | 59 | 29 | 700 | 788 | 0 | 449 | 78 | 527 | 0 | 0 | 0 | 0 | 3394 |
| % App. Total | 18.8 | 81.2 | 0 | | 7.5 | 3.7 | 88.8 | | 0 | 85.2 | 14.8 | | 0 | 0 | 0 | | |
| PHF | .819 | .846 | .000 | .841 | .738 | .453 | .936 | .916 | .000 | .935 | .722 | .955 | .000 | .000 | .000 | .000 | .897 |

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Site Code : 00000006
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Groups Printed- Bikes

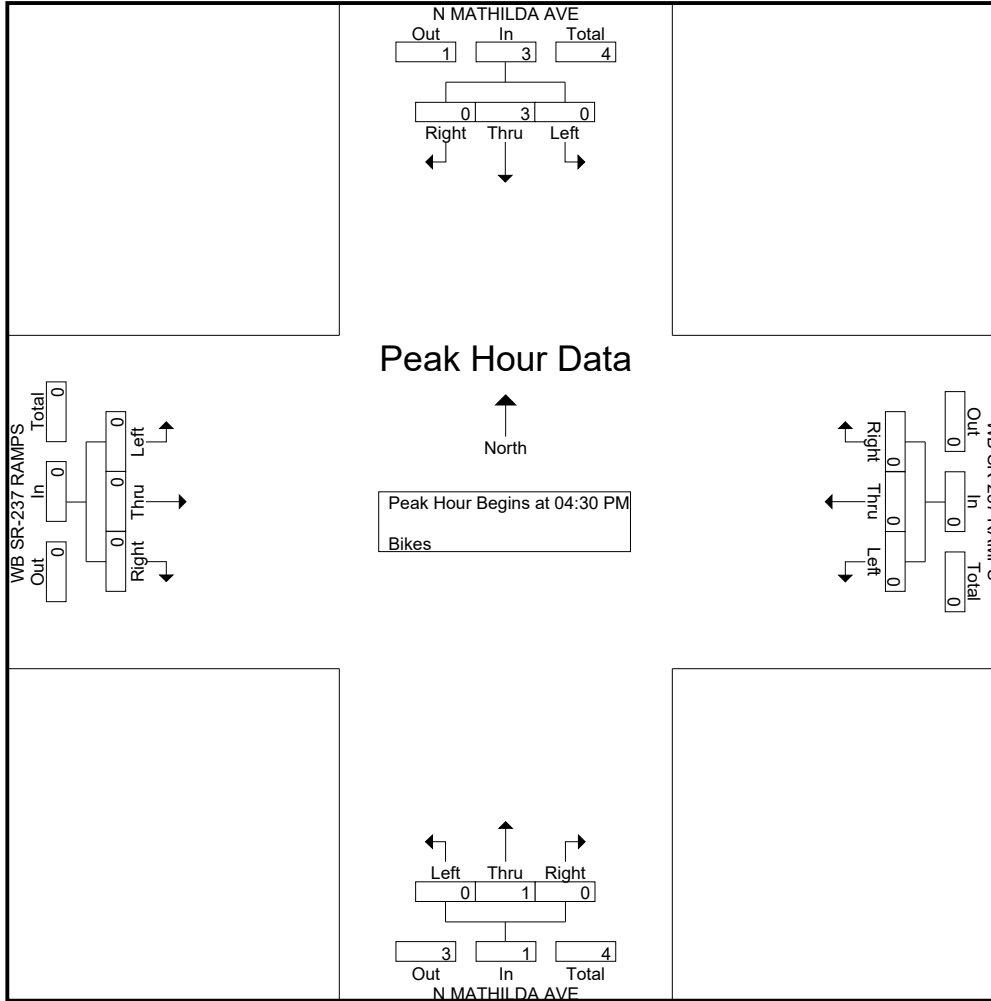
| Start Time | N MATHILDA AVE Southbound | | | | | WB SR-237 RAMPS Westbound | | | | | N MATHILDA AVE Northbound | | | | | WB SR-237 RAMPS Eastbound | | | | | Int. Total |
|--------------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:00 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 05:15 PM | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 3 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 06:00 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 06:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 06:30 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 06:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| Grand Total | 0 | 5 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 7 |
| Apprch % | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | |
| Total % | 0 | 71.4 | 0 | 0 | 71.4 | 0 | 0 | 0 | 0 | 0 | 0 | 28.6 | 0 | 0 | 28.6 | 0 | 0 | 0 | 0 | 0 | |

| Start Time | N MATHILDA AVE Southbound | | | | WB SR-237 RAMPS Westbound | | | | N MATHILDA AVE Northbound | | | | WB SR-237 RAMPS Eastbound | | | | Int. Total |
|--|------------------------------|------|------|------------|------------------------------|------|------|------------|------------------------------|------|------|------------|------------------------------|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 04:00 PM to 06:45 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 04:30 PM | | | | | | | | | | | | | | | | | |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:00 PM | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 05:15 PM | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| Total Volume | 0 | 3 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 4 |
| % App. Total | 0 | 100 | 0 | | 0 | 0 | 0 | | 0 | 100 | 0 | | 0 | 0 | 0 | | |
| PHF | .000 | .375 | .000 | .375 | .000 | .000 | .000 | .000 | .000 | .250 | .000 | .250 | .000 | .000 | .000 | .000 | .500 |

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 Site Code : 00000007
 Start Date : 11/13/2013
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Groups Printed- Vehicles

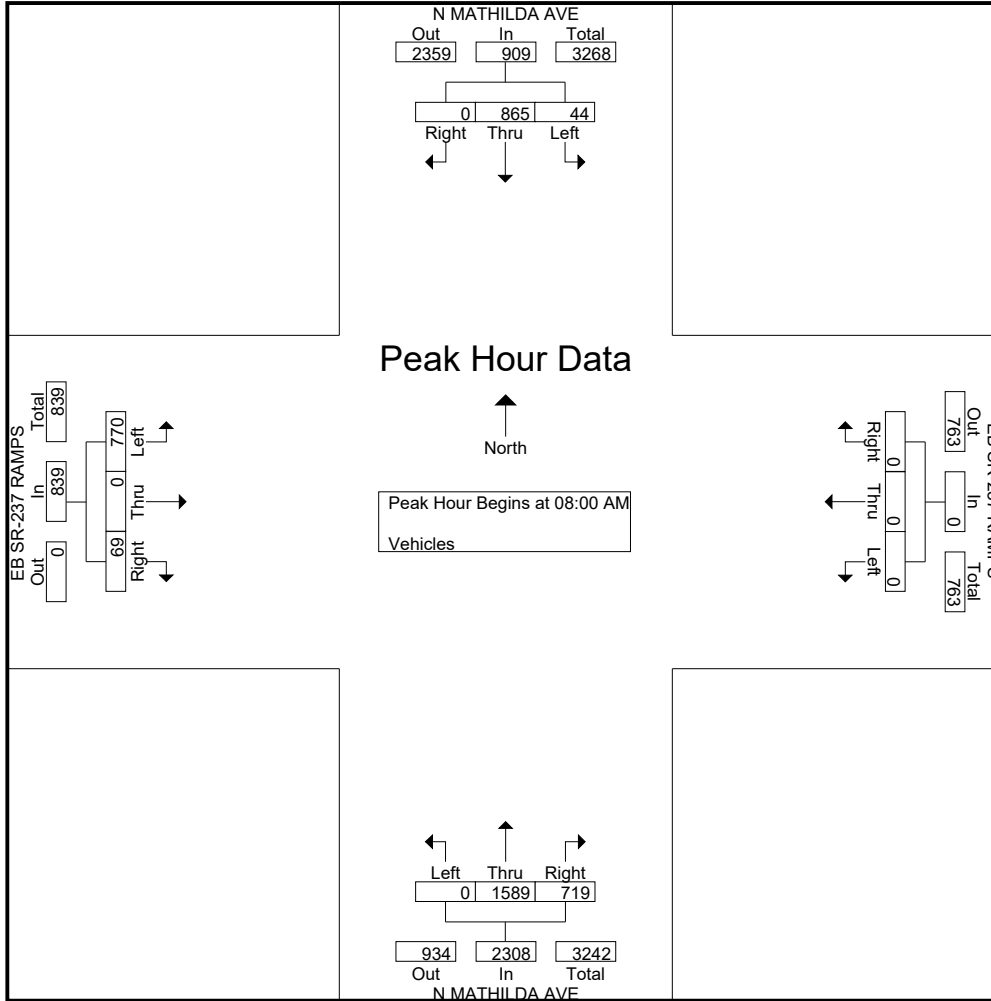
| Start Time | N MATHILDA AVE Southbound | | | | | EB SR-237 RAMPS Westbound | | | | | N MATHILDA AVE Northbound | | | | | EB SR-237 RAMPS Eastbound | | | | | Int. Total |
|--------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 0 | 136 | 4 | 0 | 140 | 0 | 0 | 0 | 2 | 2 | 101 | 252 | 0 | 0 | 353 | 14 | 1 | 139 | 0 | 154 | 649 |
| 07:15 AM | 0 | 138 | 9 | 0 | 147 | 0 | 0 | 0 | 2 | 2 | 97 | 286 | 0 | 0 | 383 | 10 | 0 | 135 | 0 | 145 | 677 |
| 07:30 AM | 0 | 163 | 9 | 0 | 172 | 0 | 0 | 0 | 2 | 2 | 124 | 309 | 0 | 0 | 433 | 11 | 0 | 132 | 0 | 143 | 750 |
| 07:45 AM | 0 | 197 | 15 | 0 | 212 | 0 | 0 | 0 | 2 | 2 | 142 | 387 | 0 | 0 | 529 | 18 | 0 | 163 | 0 | 181 | 924 |
| Total | 0 | 634 | 37 | 0 | 671 | 0 | 0 | 0 | 8 | 8 | 464 | 1234 | 0 | 0 | 1698 | 53 | 1 | 569 | 0 | 623 | 3000 |
| 08:00 AM | 0 | 182 | 16 | 0 | 198 | 0 | 0 | 0 | 0 | 0 | 174 | 372 | 0 | 0 | 546 | 26 | 0 | 183 | 0 | 209 | 953 |
| 08:15 AM | 0 | 218 | 3 | 0 | 221 | 0 | 0 | 0 | 0 | 0 | 171 | 436 | 0 | 0 | 607 | 15 | 0 | 180 | 0 | 195 | 1023 |
| 08:30 AM | 0 | 214 | 8 | 0 | 222 | 0 | 0 | 0 | 0 | 0 | 183 | 369 | 0 | 0 | 552 | 10 | 0 | 181 | 0 | 191 | 965 |
| 08:45 AM | 0 | 251 | 17 | 0 | 268 | 0 | 0 | 0 | 0 | 0 | 191 | 412 | 0 | 0 | 603 | 18 | 0 | 226 | 0 | 244 | 1115 |
| Total | 0 | 865 | 44 | 0 | 909 | 0 | 0 | 0 | 0 | 0 | 719 | 1589 | 0 | 0 | 2308 | 69 | 0 | 770 | 0 | 839 | 4056 |
| Grand Total | 0 | 1499 | 81 | 0 | 1580 | 0 | 0 | 0 | 8 | 8 | 1183 | 2823 | 0 | 0 | 4006 | 122 | 1 | 1339 | 0 | 1462 | 7056 |
| Apprch % | 0 | 94.9 | 5.1 | 0 | | 0 | 0 | 0 | 100 | | 29.5 | 70.5 | 0 | 0 | | 8.3 | 0.1 | 91.6 | 0 | | |
| Total % | 0 | 21.2 | 1.1 | 0 | 22.4 | 0 | 0 | 0 | 0.1 | 0.1 | 16.8 | 40 | 0 | 0 | 56.8 | 1.7 | 0 | 19 | 0 | 20.7 | |

| Start Time | N MATHILDA AVE Southbound | | | | EB SR-237 RAMPS Westbound | | | | N MATHILDA AVE Northbound | | | | EB SR-237 RAMPS Eastbound | | | | Int. Total |
|--|------------------------------|------------|-----------|------------|------------------------------|------|------|------------|------------------------------|------------|------|------------|------------------------------|------|------------|------------|-------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 08:00 AM | | | | | | | | | | | | | | | | | |
| 08:00 AM | 0 | 182 | 16 | 198 | 0 | 0 | 0 | 0 | 174 | 372 | 0 | 546 | 26 | 0 | 183 | 209 | 953 |
| 08:15 AM | 0 | 218 | 3 | 221 | 0 | 0 | 0 | 0 | 171 | 436 | 0 | 607 | 15 | 0 | 180 | 195 | 1023 |
| 08:30 AM | 0 | 214 | 8 | 222 | 0 | 0 | 0 | 0 | 183 | 369 | 0 | 552 | 10 | 0 | 181 | 191 | 965 |
| 08:45 AM | 0 | 251 | 17 | 268 | 0 | 0 | 0 | 0 | 191 | 412 | 0 | 603 | 18 | 0 | 226 | 244 | 1115 |
| Total Volume | 0 | 865 | 44 | 909 | 0 | 0 | 0 | 0 | 719 | 1589 | 0 | 2308 | 69 | 0 | 770 | 839 | 4056 |
| % App. Total | 0 | 95.2 | 4.8 | | 0 | 0 | 0 | | 31.2 | 68.8 | 0 | | 8.2 | 0 | 91.8 | | |
| PHF | .000 | .862 | .647 | .848 | .000 | .000 | .000 | .000 | .941 | .911 | .000 | .951 | .663 | .000 | .852 | .860 | .909 |

Traffic Data Service

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Groups Printed- Bikes

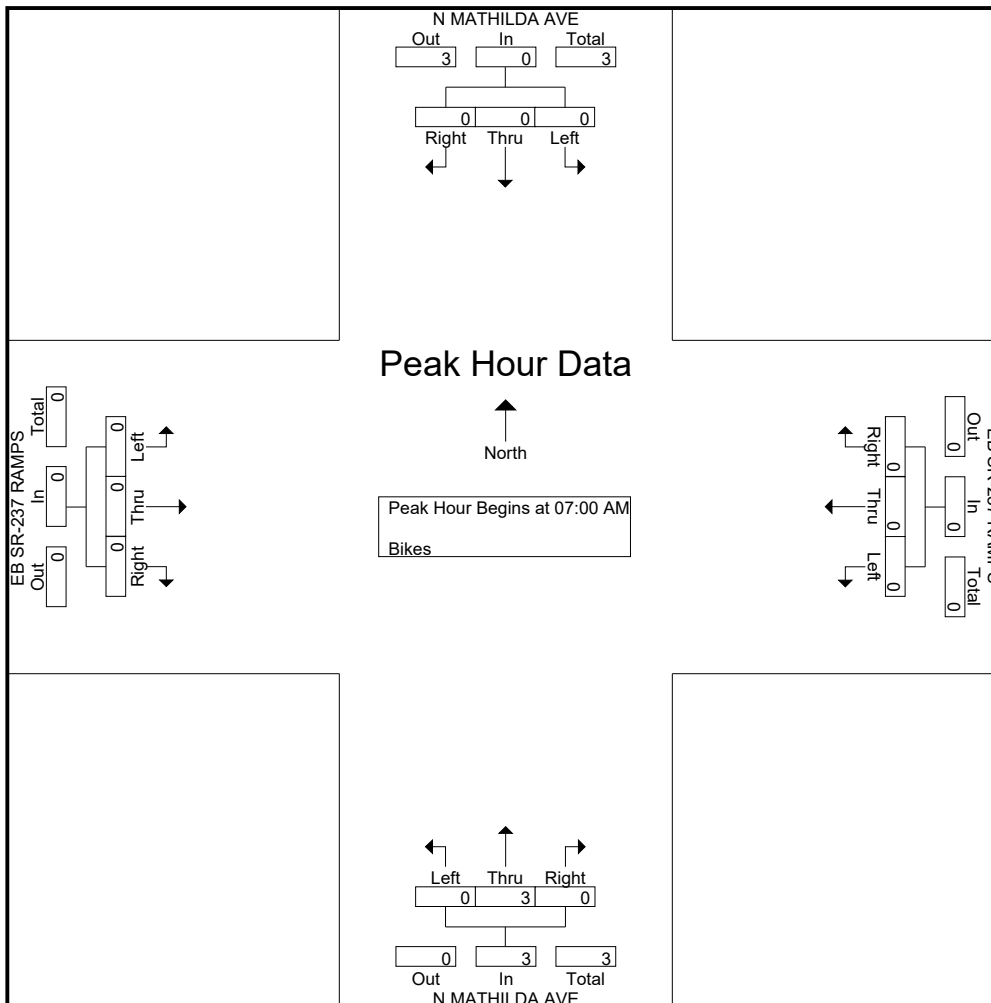
| Start Time | N MATHILDA AVE Southbound | | | | | EB SR-237 RAMPS Westbound | | | | | N MATHILDA AVE Northbound | | | | | EB SR-237 RAMPS Eastbound | | | | | Int. Total |
|--------------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 2 |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 3 |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 4 |
| Apprch % | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 0 | 100 | 0 | 0 | 0 | 0 | 0 | |
| Total % | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 0 | 100 | 0 | 0 | 0 | 0 | 0 | |

| Start Time | N MATHILDA AVE Southbound | | | | EB SR-237 RAMPS Westbound | | | | N MATHILDA AVE Northbound | | | | EB SR-237 RAMPS Eastbound | | | | Int. Total |
|--|------------------------------|------|------|------------|------------------------------|------|------|------------|------------------------------|------|------|------------|------------------------------|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 07:00 AM | | | | | | | | | | | | | | | | | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 0 | 0 | 0 | 0 | 3 |
| % App. Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 100 | 0 | 0 | 0 | 0 | |
| PHF | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .375 | .000 | .375 | .000 | .000 | .000 | .000 | .375 |

Traffic Data Service

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Groups Printed- Vehicles

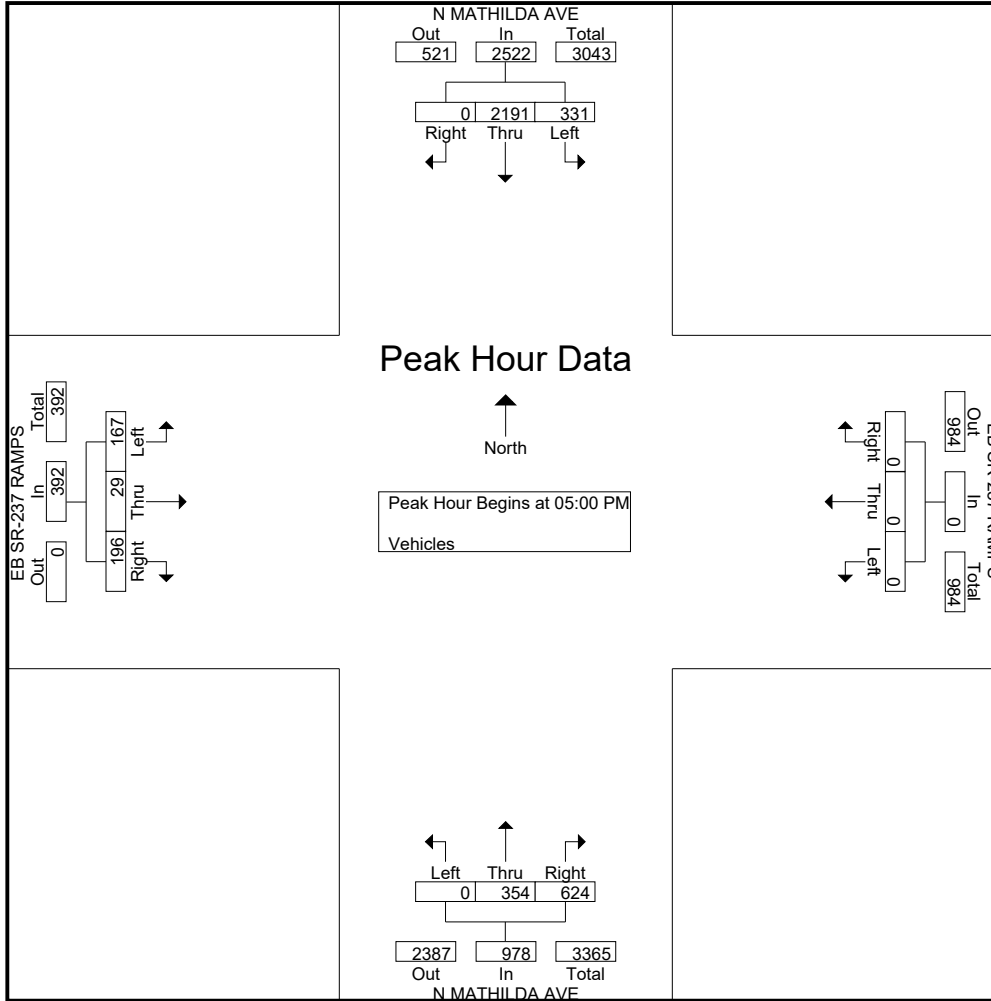
| Start Time | N MATHILDA AVE Southbound | | | | | EB SR-237 RAMPS Westbound | | | | | N MATHILDA AVE Northbound | | | | | EB SR-237 RAMPS Eastbound | | | | | Int. Total |
|-------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:00 PM | 0 | 342 | 102 | 0 | 444 | 0 | 0 | 0 | 0 | 0 | 154 | 94 | 0 | 0 | 248 | 22 | 0 | 32 | 0 | 54 | 746 |
| 04:15 PM | 0 | 332 | 87 | 0 | 419 | 0 | 0 | 0 | 0 | 0 | 91 | 78 | 0 | 0 | 169 | 41 | 5 | 33 | 0 | 79 | 667 |
| 04:30 PM | 0 | 427 | 85 | 0 | 512 | 0 | 0 | 0 | 0 | 0 | 155 | 80 | 0 | 0 | 235 | 32 | 5 | 37 | 0 | 74 | 821 |
| 04:45 PM | 0 | 472 | 89 | 0 | 561 | 0 | 0 | 0 | 0 | 0 | 140 | 90 | 0 | 0 | 230 | 39 | 1 | 29 | 0 | 69 | 860 |
| Total | 0 | 1573 | 363 | 0 | 1936 | 0 | 0 | 0 | 0 | 0 | 540 | 342 | 0 | 0 | 882 | 134 | 11 | 131 | 0 | 276 | 3094 |
| 05:00 PM | 0 | 532 | 74 | 0 | 606 | 0 | 0 | 0 | 3 | 3 | 170 | 79 | 0 | 0 | 249 | 45 | 6 | 35 | 0 | 86 | 944 |
| 05:15 PM | 0 | 591 | 88 | 0 | 679 | 0 | 0 | 0 | 2 | 2 | 149 | 91 | 0 | 0 | 240 | 48 | 7 | 49 | 0 | 104 | 1025 |
| 05:30 PM | 0 | 566 | 80 | 0 | 646 | 0 | 0 | 0 | 3 | 3 | 150 | 93 | 0 | 0 | 243 | 51 | 11 | 36 | 0 | 98 | 990 |
| 05:45 PM | 0 | 502 | 89 | 0 | 591 | 0 | 0 | 0 | 2 | 2 | 155 | 91 | 0 | 0 | 246 | 52 | 5 | 47 | 0 | 104 | 943 |
| Total | 0 | 2191 | 331 | 0 | 2522 | 0 | 0 | 0 | 10 | 10 | 624 | 354 | 0 | 0 | 978 | 196 | 29 | 167 | 0 | 392 | 3902 |
| 06:00 PM | 0 | 517 | 71 | 0 | 588 | 0 | 0 | 0 | 0 | 0 | 121 | 78 | 0 | 0 | 199 | 60 | 8 | 43 | 0 | 111 | 898 |
| 06:15 PM | 0 | 512 | 72 | 0 | 584 | 0 | 0 | 0 | 0 | 0 | 125 | 78 | 0 | 0 | 203 | 37 | 3 | 31 | 0 | 71 | 858 |
| 06:30 PM | 0 | 480 | 62 | 0 | 542 | 0 | 0 | 0 | 4 | 4 | 113 | 70 | 0 | 0 | 183 | 31 | 1 | 15 | 0 | 47 | 776 |
| 06:45 PM | 0 | 395 | 73 | 0 | 468 | 0 | 0 | 0 | 0 | 0 | 109 | 71 | 0 | 0 | 180 | 29 | 1 | 19 | 0 | 49 | 697 |
| Total | 0 | 1904 | 278 | 0 | 2182 | 0 | 0 | 0 | 4 | 4 | 468 | 297 | 0 | 0 | 765 | 157 | 13 | 108 | 0 | 278 | 3229 |
| Grand Total | 0 | 5668 | 972 | 0 | 6640 | 0 | 0 | 0 | 14 | 14 | 1632 | 993 | 0 | 0 | 2625 | 487 | 53 | 406 | 0 | 946 | 10225 |
| Apprch % | 0 | 85.4 | 14.6 | 0 | | 0 | 0 | 0 | 100 | | 62.2 | 37.8 | 0 | 0 | | 51.5 | 5.6 | 42.9 | 0 | | |
| Total % | 0 | 55.4 | 9.5 | 0 | 64.9 | 0 | 0 | 0 | 0.1 | 0.1 | 16 | 9.7 | 0 | 0 | 25.7 | 4.8 | 0.5 | 4 | 0 | 9.3 | |

| Start Time | N MATHILDA AVE Southbound | | | | EB SR-237 RAMPS Westbound | | | | N MATHILDA AVE Northbound | | | | EB SR-237 RAMPS Eastbound | | | | Int. Total |
|--|------------------------------|------------|-----------|------------|------------------------------|------|------|------------|------------------------------|-----------|------|------------|------------------------------|-----------|-----------|------------|-------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 04:00 PM to 06:45 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 05:00 PM | | | | | | | | | | | | | | | | | |
| 05:00 PM | 0 | 532 | 74 | 606 | 0 | 0 | 0 | 0 | 170 | 79 | 0 | 249 | 45 | 6 | 35 | 86 | 941 |
| 05:15 PM | 0 | 591 | 88 | 679 | 0 | 0 | 0 | 0 | 149 | 91 | 0 | 240 | 48 | 7 | 49 | 104 | 1023 |
| 05:30 PM | 0 | 566 | 80 | 646 | 0 | 0 | 0 | 0 | 150 | 93 | 0 | 243 | 51 | 11 | 36 | 98 | 987 |
| 05:45 PM | 0 | 502 | 89 | 591 | 0 | 0 | 0 | 0 | 155 | 91 | 0 | 246 | 52 | 5 | 47 | 104 | 941 |
| Total Volume | 0 | 2191 | 331 | 2522 | 0 | 0 | 0 | 0 | 624 | 354 | 0 | 978 | 196 | 29 | 167 | 392 | 3892 |
| % App. Total | 0 | 86.9 | 13.1 | | 0 | 0 | 0 | | 63.8 | 36.2 | 0 | | 50 | 7.4 | 42.6 | | |
| PHF | .000 | .927 | .930 | .929 | .000 | .000 | .000 | .000 | .918 | .952 | .000 | .982 | .942 | .659 | .852 | .942 | .951 |

Traffic Data Service

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Traffic Data Service

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 Site Code : 00000007
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Groups Printed- Bikes

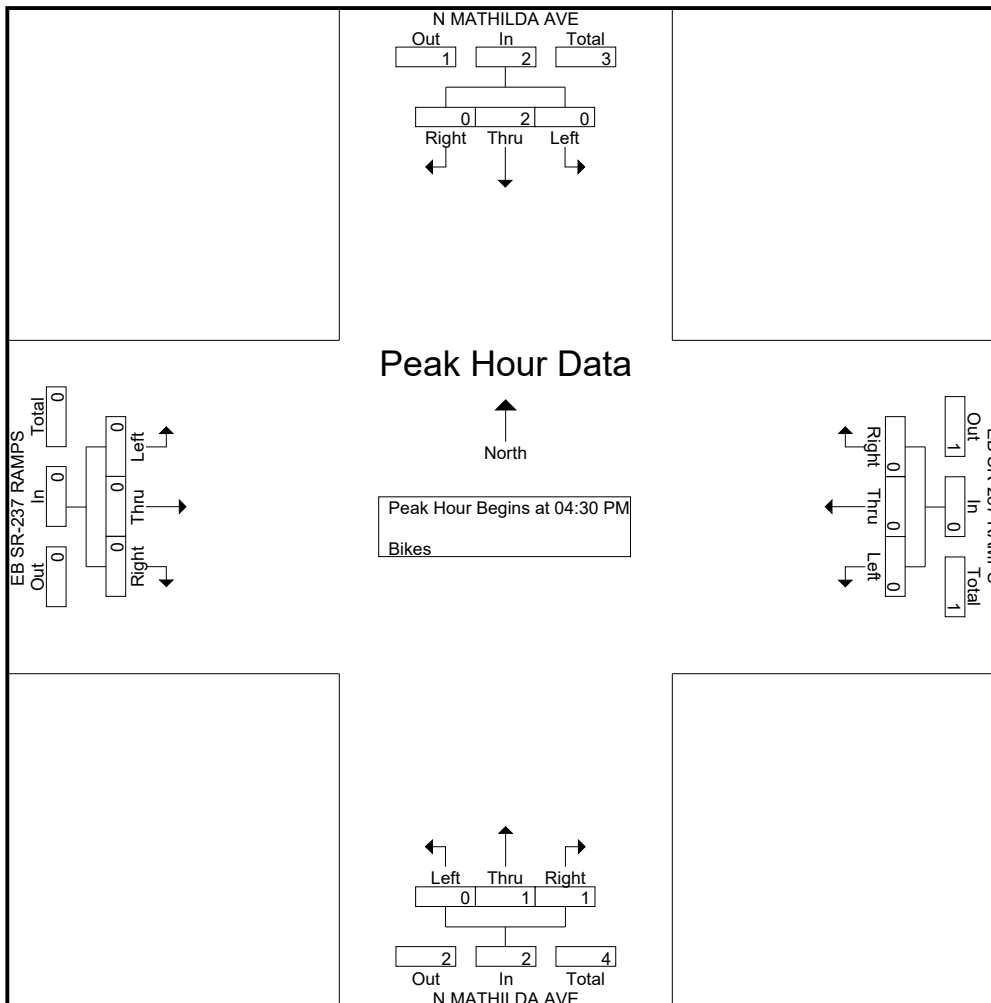
| Start Time | N MATHILDA AVE Southbound | | | | | EB SR-237 RAMPS Westbound | | | | | N MATHILDA AVE Northbound | | | | | EB SR-237 RAMPS Eastbound | | | | | Int. Total |
|--------------------|---------------------------|------|------|------|------------|---------------------------|------|------|------|------------|---------------------------|------|------|------|------------|---------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:00 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:15 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:30 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 3 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 06:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 06:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 06:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 06:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Grand Total | 0 | 3 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 |
| Apprch % | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | 33.3 | 66.7 | 0 | 0 | | 0 | 0 | 0 | 0 | | |
| Total % | 0 | 50 | 0 | 0 | 50 | 0 | 0 | 0 | 0 | 0 | 16.7 | 33.3 | 0 | 0 | 50 | 0 | 0 | 0 | 0 | 0 | |

| Start Time | N MATHILDA AVE Southbound | | | | EB SR-237 RAMPS Westbound | | | | N MATHILDA AVE Northbound | | | | EB SR-237 RAMPS Eastbound | | | | Int. Total |
|--|---------------------------|------|------|------------|---------------------------|------|------|------------|---------------------------|------|------|------------|---------------------------|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 04:00 PM to 06:45 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 04:30 PM | | | | | | | | | | | | | | | | | |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| 05:00 PM | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| 05:15 PM | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | |
| Total Volume | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | |
| % App. Total | 0 | 100 | 0 | | 0 | 0 | 0 | | 50 | 50 | 0 | | 0 | 0 | 0 | | |
| PHF | .000 | .500 | .000 | .500 | .000 | .000 | .000 | .000 | .250 | .250 | .000 | .500 | .000 | .000 | .000 | .000 | |

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Traffic Data Service

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File Name : 8AM FINAL
 Site Code : 00000008
 Start Date : 2/12/2013
 Page No : 1

Groups Printed- Vehicles

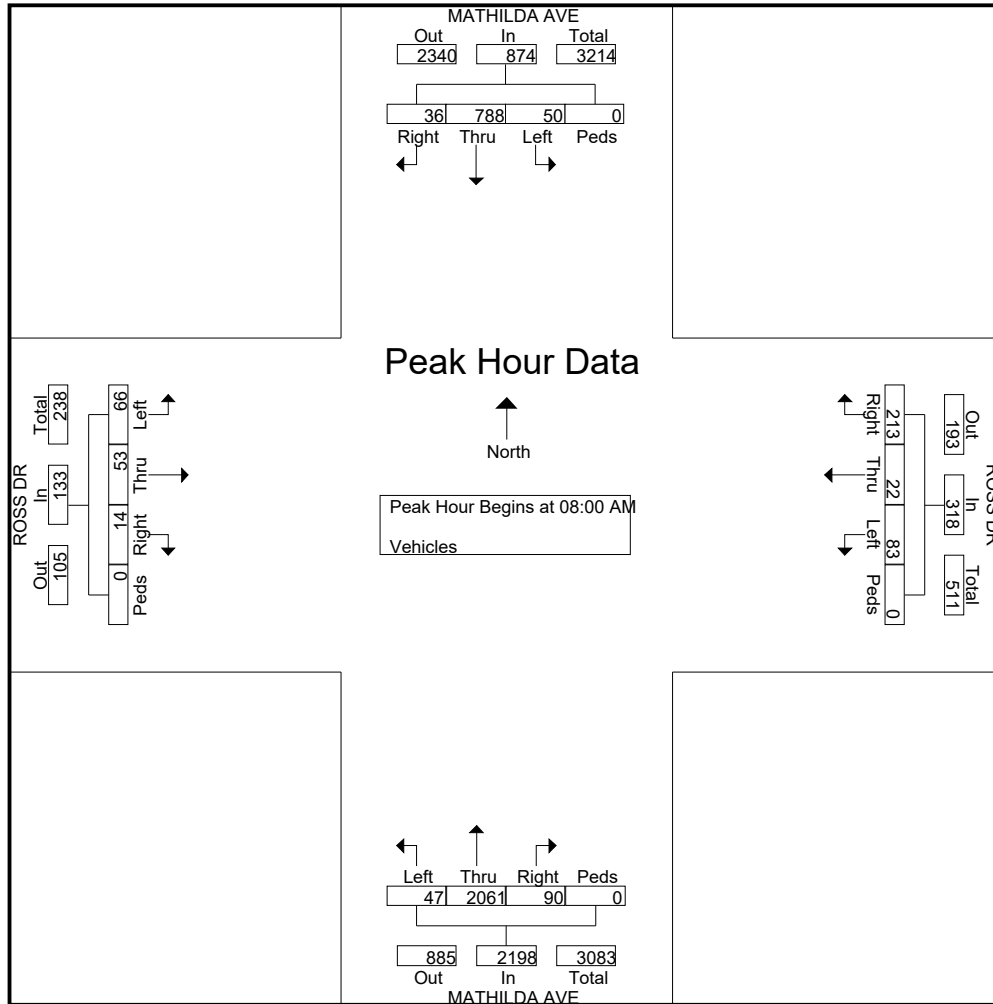
| Start Time | MATHILDA AVE Southbound | | | | | ROSS DR Westbound | | | | | MATHILDA AVE Northbound | | | | | ROSS DR Eastbound | | | | | Int. Total |
|-------------|-------------------------|------|------|------|------------|-------------------|------|------|------|------------|-------------------------|------|------|------|------------|-------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 12 | 121 | 11 | 0 | 144 | 28 | 1 | 21 | 0 | 50 | 19 | 289 | 7 | 0 | 315 | 3 | 11 | 9 | 0 | 23 | 532 |
| 07:15 AM | 6 | 132 | 15 | 0 | 153 | 38 | 3 | 18 | 0 | 59 | 21 | 325 | 5 | 0 | 351 | 4 | 10 | 15 | 0 | 29 | 592 |
| 07:30 AM | 14 | 173 | 18 | 0 | 205 | 26 | 8 | 14 | 0 | 48 | 16 | 414 | 6 | 0 | 436 | 7 | 15 | 8 | 0 | 30 | 719 |
| 07:45 AM | 9 | 181 | 16 | 0 | 206 | 46 | 10 | 24 | 0 | 80 | 28 | 455 | 9 | 0 | 492 | 8 | 12 | 14 | 0 | 34 | 812 |
| Total | 41 | 607 | 60 | 0 | 708 | 138 | 22 | 77 | 0 | 237 | 84 | 1483 | 27 | 0 | 1594 | 22 | 48 | 46 | 0 | 116 | 2655 |
| 08:00 AM | 10 | 189 | 25 | 0 | 224 | 24 | 7 | 12 | 0 | 43 | 23 | 524 | 8 | 0 | 555 | 1 | 5 | 10 | 0 | 16 | 838 |
| 08:15 AM | 11 | 195 | 11 | 0 | 217 | 22 | 2 | 14 | 0 | 38 | 27 | 483 | 11 | 0 | 521 | 3 | 11 | 11 | 0 | 25 | 801 |
| 08:30 AM | 8 | 203 | 9 | 0 | 220 | 86 | 3 | 26 | 0 | 115 | 25 | 503 | 12 | 0 | 540 | 3 | 17 | 18 | 0 | 38 | 913 |
| 08:45 AM | 7 | 201 | 5 | 0 | 213 | 81 | 10 | 31 | 0 | 122 | 15 | 551 | 16 | 0 | 582 | 7 | 20 | 27 | 0 | 54 | 971 |
| Total | 36 | 788 | 50 | 0 | 874 | 213 | 22 | 83 | 0 | 318 | 90 | 2061 | 47 | 0 | 2198 | 14 | 53 | 66 | 0 | 133 | 3523 |
| Grand Total | 77 | 1395 | 110 | 0 | 1582 | 351 | 44 | 160 | 0 | 555 | 174 | 3544 | 74 | 0 | 3792 | 36 | 101 | 112 | 0 | 249 | 6178 |
| Apprch % | 4.9 | 88.2 | 7 | 0 | | 63.2 | 7.9 | 28.8 | 0 | | 4.6 | 93.5 | 2 | 0 | | 14.5 | 40.6 | 45 | 0 | | |
| Total % | 1.2 | 22.6 | 1.8 | 0 | 25.6 | 5.7 | 0.7 | 2.6 | 0 | 9 | 2.8 | 57.4 | 1.2 | 0 | 61.4 | 0.6 | 1.6 | 1.8 | 0 | 4 | |

| Start Time | MATHILDA AVE Southbound | | | | | ROSS DR Westbound | | | | | MATHILDA AVE Northbound | | | | | ROSS DR Eastbound | | | | | Int. Total |
|--|-------------------------|------------|-----------|------|------------|-------------------|-----------|-----------|------|------------|-------------------------|------------|-----------|------|------------|-------------------|-----------|-----------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 08:00 AM | | | | | | | | | | | | | | | | | | | | | |
| 08:00 AM | 10 | 189 | 25 | 0 | 224 | 24 | 7 | 12 | 0 | 43 | 23 | 524 | 8 | 0 | 555 | 1 | 5 | 10 | 0 | 16 | 838 |
| 08:15 AM | 11 | 195 | 11 | 0 | 217 | 22 | 2 | 14 | 0 | 38 | 27 | 483 | 11 | 0 | 521 | 3 | 11 | 11 | 0 | 25 | 801 |
| 08:30 AM | 8 | 203 | 9 | 0 | 220 | 86 | 3 | 26 | 0 | 115 | 25 | 503 | 12 | 0 | 540 | 3 | 17 | 18 | 0 | 38 | 913 |
| 08:45 AM | 7 | 201 | 5 | 0 | 213 | 81 | 10 | 31 | 0 | 122 | 15 | 551 | 16 | 0 | 582 | 7 | 20 | 27 | 0 | 54 | 971 |
| Total Volume | 36 | 788 | 50 | 0 | 874 | 213 | 22 | 83 | 0 | 318 | 90 | 2061 | 47 | 0 | 2198 | 14 | 53 | 66 | 0 | 133 | 3523 |
| % App. Total | 4.1 | 90.2 | 5.7 | 0 | | 67 | 6.9 | 26.1 | 0 | | 4.1 | 93.8 | 2.1 | 0 | | 10.5 | 39.8 | 49.6 | 0 | | |
| PHF | .818 | .970 | .500 | .000 | .975 | .619 | .550 | .669 | .000 | .652 | .833 | .935 | .734 | .000 | .944 | .500 | .663 | .611 | .000 | .616 | .907 |

Traffic Data Service

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Traffic Data Service

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 tdsbay@cs.com

File Name : 8AM FINAL
 Site Code : 00000008
 Start Date : 2/12/2013
 Page No : 1

Groups Printed- Bikes

| Start Time | MATHILDA AVE Southbound | | | | | ROSS DR Westbound | | | | | MATHILDA AVE Northbound | | | | | ROSS DR Eastbound | | | | | Int. Total |
|--------------------|-------------------------|------|------|------|------------|-------------------|------|------|------|------------|-------------------------|------|------|------|------------|-------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 3 |
| Apprch % | 0 | 0 | 0 | 0 | | 100 | 0 | 0 | 0 | | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | |
| Total % | 0 | 0 | 0 | 0 | 0 | 33.3 | 0 | 0 | 0 | 33.3 | 0 | 66.7 | 0 | 0 | 66.7 | 0 | 0 | 0 | 0 | 0 | |

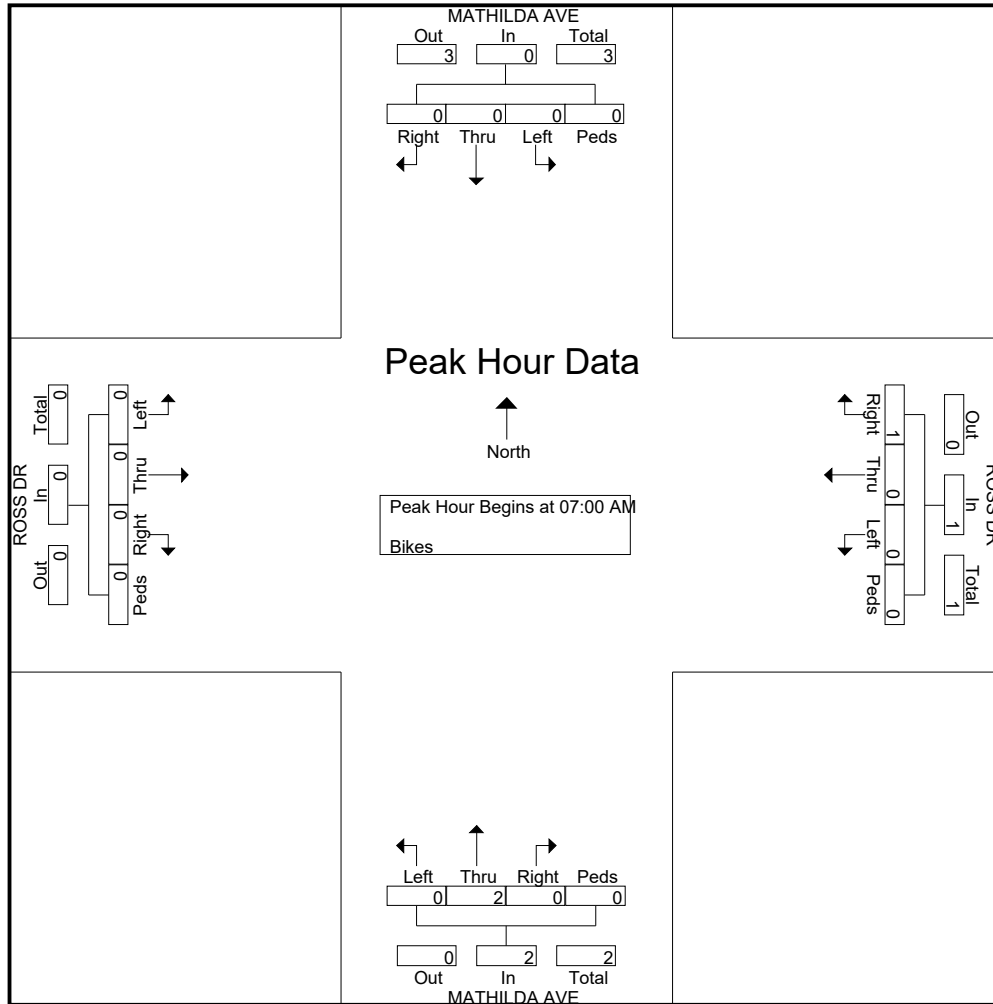
| Start Time | MATHILDA AVE Southbound | | | | | ROSS DR Westbound | | | | | MATHILDA AVE Northbound | | | | | ROSS DR Eastbound | | | | | Int. Total |
|---------------------|-------------------------|------|------|------|------------|-------------------|------|------|------|------------|-------------------------|------|------|------|------------|-------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 3 |
| % App. Total | 0 | 0 | 0 | 0 | | 100 | 0 | 0 | 0 | | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | |
| PHF | .000 | .000 | .000 | .000 | .000 | .250 | .000 | .000 | .000 | .250 | .000 | .500 | .000 | .000 | .500 | .000 | .000 | .000 | .000 | .000 | .750 |

Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1
 Peak Hour for Entire Intersection Begins at 07:00 AM

Traffic Data Service

Campbell, CA
(408) 377-2988
idsbay@cs.com

File Name : 8AM FINAL
Site Code : 00000008
Start Date : 2/12/2013
Page No : 2



Traffic Data Service

Campbell, CA
 (408) 377-2988
 tdsbay@cs.com

File Name : 8PM FINAL
 Site Code : 00000008
 Start Date : 2/12/2013
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Groups Printed- Vehicles

| Start Time | MATHILDA AVE Southbound | | | | | ROSS DR Westbound | | | | | MATHILDA AVE Northbound | | | | | ROSS DR Eastbound | | | | | Int. Total |
|-------------|-------------------------|------|------|------|------------|-------------------|------|------|------|------------|-------------------------|------|------|------|------------|-------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:30 PM | 11 | 399 | 26 | 0 | 436 | 20 | 2 | 36 | 0 | 58 | 25 | 199 | 26 | 0 | 250 | 3 | 18 | 11 | 0 | 32 | 776 |
| 04:45 PM | 15 | 475 | 28 | 0 | 518 | 29 | 4 | 28 | 0 | 61 | 63 | 169 | 28 | 0 | 260 | 8 | 19 | 9 | 0 | 36 | 875 |
| Total | 26 | 874 | 54 | 0 | 954 | 49 | 6 | 64 | 0 | 119 | 88 | 368 | 54 | 0 | 510 | 11 | 37 | 20 | 0 | 68 | 1651 |
| 05:00 PM | 16 | 527 | 26 | 0 | 569 | 22 | 13 | 46 | 0 | 81 | 58 | 196 | 25 | 0 | 279 | 7 | 44 | 11 | 0 | 62 | 991 |
| 05:15 PM | 21 | 545 | 32 | 0 | 598 | 25 | 10 | 50 | 0 | 85 | 57 | 215 | 14 | 0 | 286 | 6 | 35 | 3 | 0 | 44 | 1013 |
| 05:30 PM | 25 | 526 | 28 | 0 | 579 | 24 | 15 | 34 | 0 | 73 | 66 | 216 | 26 | 0 | 308 | 4 | 37 | 10 | 0 | 51 | 1011 |
| 05:45 PM | 23 | 509 | 41 | 0 | 573 | 23 | 10 | 39 | 0 | 72 | 71 | 191 | 22 | 0 | 284 | 11 | 27 | 14 | 0 | 52 | 981 |
| Total | 85 | 2107 | 127 | 0 | 2319 | 94 | 48 | 169 | 0 | 311 | 252 | 818 | 87 | 0 | 1157 | 28 | 143 | 38 | 0 | 209 | 3996 |
| 06:00 PM | 22 | 452 | 35 | 0 | 509 | 22 | 15 | 35 | 0 | 72 | 65 | 170 | 25 | 0 | 260 | 7 | 29 | 13 | 0 | 49 | 890 |
| 06:15 PM | 19 | 475 | 24 | 0 | 518 | 19 | 12 | 29 | 0 | 60 | 52 | 177 | 17 | 0 | 246 | 9 | 28 | 12 | 0 | 49 | 873 |
| Grand Total | 152 | 3908 | 240 | 0 | 4300 | 184 | 81 | 297 | 0 | 562 | 457 | 1533 | 183 | 0 | 2173 | 55 | 237 | 83 | 0 | 375 | 7410 |
| Apprch % | 3.5 | 90.9 | 5.6 | 0 | | 32.7 | 14.4 | 52.8 | 0 | | 21 | 70.5 | 8.4 | 0 | | 14.7 | 63.2 | 22.1 | 0 | | |
| Total % | 2.1 | 52.7 | 3.2 | 0 | 58 | 2.5 | 1.1 | 4 | 0 | 7.6 | 6.2 | 20.7 | 2.5 | 0 | 29.3 | 0.7 | 3.2 | 1.1 | 0 | 5.1 | |

| Start Time | MATHILDA AVE Southbound | | | | | ROSS DR Westbound | | | | | MATHILDA AVE Northbound | | | | | ROSS DR Eastbound | | | | | Int. Total |
|--|-------------------------|------------|-----------|------|------------|-------------------|-----------|-----------|------|------------|-------------------------|------------|-----------|------|------------|-------------------|-----------|-----------|------|------------|-------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| Peak Hour Analysis From 04:30 PM to 06:15 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 05:00 PM | | | | | | | | | | | | | | | | | | | | | |
| 05:00 PM | 16 | 527 | 26 | 0 | 569 | 22 | 13 | 46 | 0 | 81 | 58 | 196 | 25 | 0 | 279 | 7 | 44 | 11 | 0 | 62 | 991 |
| 05:15 PM | 21 | 545 | 32 | 0 | 598 | 25 | 10 | 50 | 0 | 85 | 57 | 215 | 14 | 0 | 286 | 6 | 35 | 3 | 0 | 44 | 1013 |
| 05:30 PM | 25 | 526 | 28 | 0 | 579 | 24 | 15 | 34 | 0 | 73 | 66 | 216 | 26 | 0 | 308 | 4 | 37 | 10 | 0 | 51 | 1011 |
| 05:45 PM | 23 | 509 | 41 | 0 | 573 | 23 | 10 | 39 | 0 | 72 | 71 | 191 | 22 | 0 | 284 | 11 | 27 | 14 | 0 | 52 | 981 |
| Total Volume | 85 | 2107 | 127 | 0 | 2319 | 94 | 48 | 169 | 0 | 311 | 252 | 818 | 87 | 0 | 1157 | 28 | 143 | 38 | 0 | 209 | 3996 |
| % App. Total | 3.7 | 90.9 | 5.5 | 0 | | 30.2 | 15.4 | 54.3 | 0 | | 21.8 | 70.7 | 7.5 | 0 | | 13.4 | 68.4 | 18.2 | 0 | | |
| PHF | .850 | .967 | .774 | .000 | .969 | .940 | .800 | .845 | .000 | .915 | .887 | .947 | .837 | .000 | .939 | .636 | .813 | .679 | .000 | .843 | .986 |

Traffic Data Service

Campbell, CA

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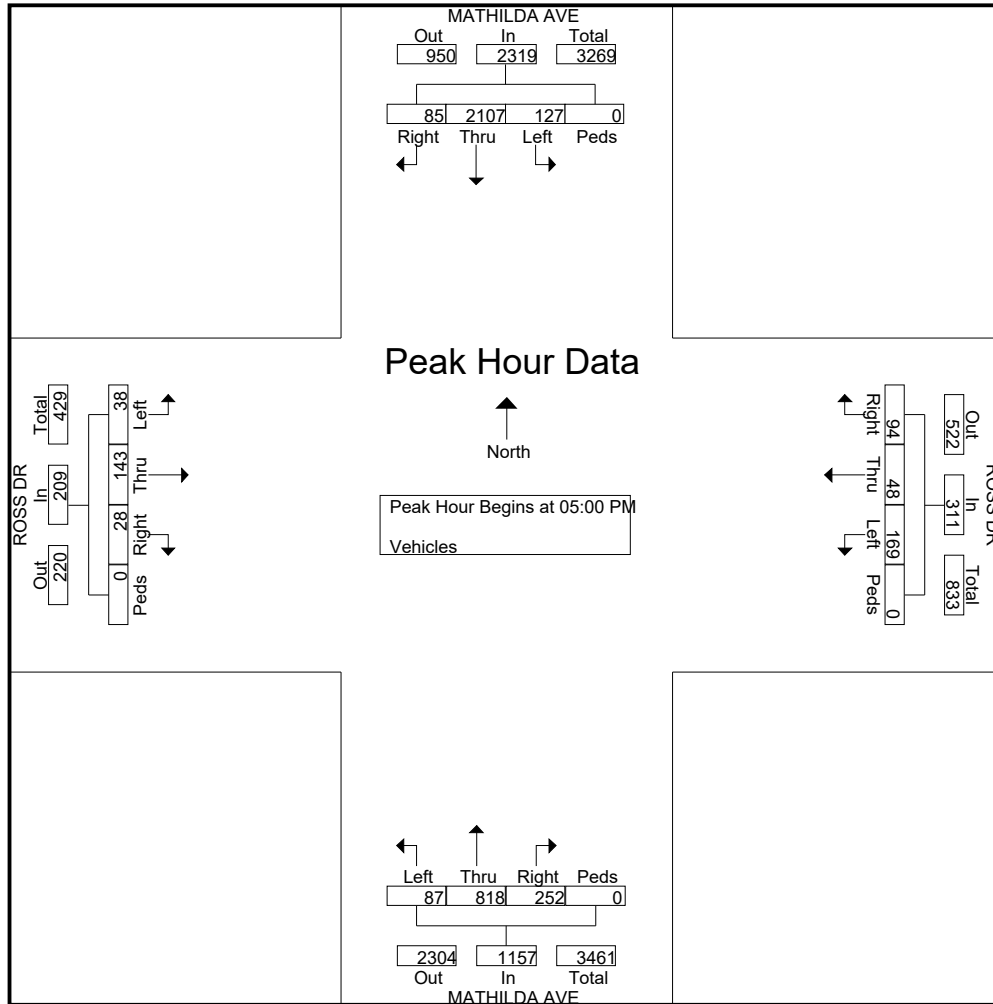
idsbay@cs.com

File Name : 8PM FINAL

Site Code : 00000008

Start Date : 2/12/2013

Page No : 2



Traffic Data Service

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 tdsbay@cs.com

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 Site Code : 00000008
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Groups Printed- Bikes

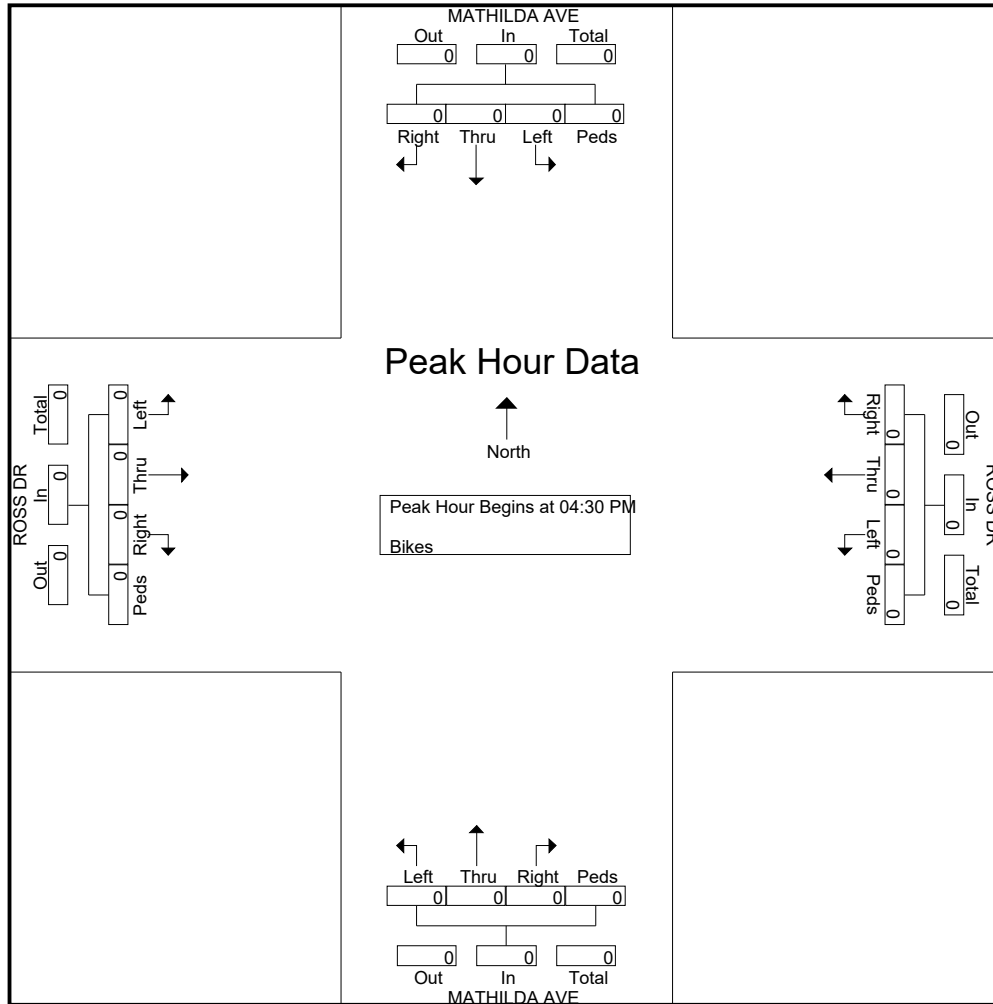
| Start Time | MATHILDA AVE Southbound | | | | | ROSS DR Westbound | | | | | MATHILDA AVE Northbound | | | | | ROSS DR Eastbound | | | | | Int. Total |
|-------------|-------------------------|------|------|------|------------|-------------------|------|------|------|------------|-------------------------|------|------|------|------------|-------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 06:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 06:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Apprch % | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | |
| Total % | | | | | | | | | | | | | | | | | | | | | |

| Start Time | MATHILDA AVE Southbound | | | | | ROSS DR Westbound | | | | | MATHILDA AVE Northbound | | | | | ROSS DR Eastbound | | | | | Int. Total |
|--|-------------------------|------|------|------|------------|-------------------|------|------|------|------------|-------------------------|------|------|------|------------|-------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| Peak Hour Analysis From 04:30 PM to 06:15 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 04:30 PM | | | | | | | | | | | | | | | | | | | | | |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| % App. Total | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | |
| PHF | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 |

Traffic Data Service

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File Name : 8PM FINAL
Site Code : 00000008
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Traffic Data Service

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(408) 377- 2988
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File Name : 2AM FINAL
Site Code : 00000002
Start Date : 11/13/2013
Page No : 1

Groups Printed- Vehicles

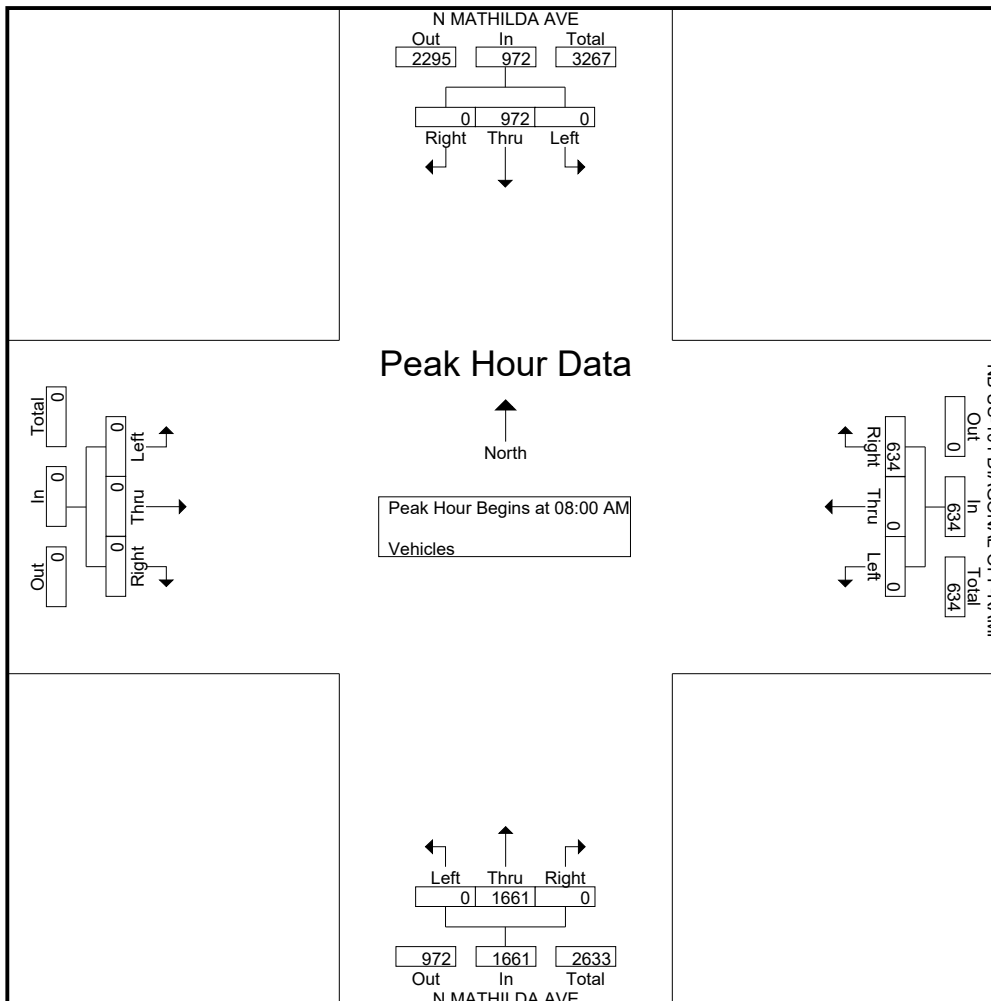
| Start Time | N MATHILDA AVE Southbound | | | | | NB US-101 DIAGONAL OFF- RAMP Westbound | | | | | N MATHILDA AVE Northbound | | | | | Eastbound | | | | | Int. Total |
|--------------|------------------------------|------|------|------|------------|--|------|------|------|------------|------------------------------|------|------|------|------------|-----------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 0 | 176 | 0 | 0 | 176 | 129 | 0 | 0 | 1 | 130 | 0 | 202 | 0 | 0 | 202 | 0 | 0 | 0 | 0 | 0 | 508 |
| 07:15 AM | 0 | 169 | 0 | 0 | 169 | 128 | 0 | 0 | 1 | 129 | 0 | 245 | 0 | 0 | 245 | 0 | 0 | 0 | 0 | 0 | 543 |
| 07:30 AM | 0 | 187 | 0 | 0 | 187 | 136 | 0 | 0 | 4 | 140 | 0 | 264 | 0 | 0 | 264 | 0 | 0 | 0 | 0 | 0 | 591 |
| 07:45 AM | 0 | 249 | 0 | 0 | 249 | 140 | 0 | 0 | 0 | 140 | 0 | 367 | 0 | 0 | 367 | 0 | 0 | 0 | 0 | 0 | 756 |
| Total | 0 | 781 | 0 | 0 | 781 | 533 | 0 | 0 | 6 | 539 | 0 | 1078 | 0 | 0 | 1078 | 0 | 0 | 0 | 0 | 0 | 2398 |
| 08:00 AM | 0 | 225 | 0 | 0 | 225 | 158 | 0 | 0 | 3 | 161 | 0 | 395 | 0 | 0 | 395 | 0 | 0 | 0 | 0 | 0 | 781 |
| 08:15 AM | 0 | 238 | 0 | 0 | 238 | 147 | 0 | 0 | 1 | 148 | 0 | 423 | 0 | 0 | 423 | 0 | 0 | 0 | 0 | 0 | 809 |
| 08:30 AM | 0 | 233 | 0 | 0 | 233 | 167 | 0 | 0 | 0 | 167 | 0 | 442 | 0 | 0 | 442 | 0 | 0 | 0 | 0 | 0 | 842 |
| 08:45 AM | 0 | 276 | 0 | 0 | 276 | 162 | 0 | 0 | 3 | 165 | 0 | 401 | 0 | 0 | 401 | 0 | 0 | 0 | 0 | 0 | 842 |
| Total | 0 | 972 | 0 | 0 | 972 | 634 | 0 | 0 | 7 | 641 | 0 | 1661 | 0 | 0 | 1661 | 0 | 0 | 0 | 0 | 0 | 3274 |
| Grand Total | 0 | 1753 | 0 | 0 | 1753 | 1167 | 0 | 0 | 13 | 1180 | 0 | 2739 | 0 | 0 | 2739 | 0 | 0 | 0 | 0 | 0 | 5672 |
| Apprch % | 0 | 100 | 0 | 0 | | 98.9 | 0 | 0 | 1.1 | | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | |
| Total % | 0 | 30.9 | 0 | 0 | 30.9 | 20.6 | 0 | 0 | 0.2 | 20.8 | 0 | 48.3 | 0 | 0 | 48.3 | 0 | 0 | 0 | 0 | 0 | |

| Start Time | N MATHILDA AVE Southbound | | | | NB US-101 DIAGONAL OFF- RAMP Westbound | | | | N MATHILDA AVE Northbound | | | | Eastbound | | | | Int. Total |
|--|------------------------------|------------|------|------------|--|------|------|------------|------------------------------|------------|------|------------|-----------|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 08:00 AM | | | | | | | | | | | | | | | | | |
| 08:00 AM | 0 | 225 | 0 | 225 | 158 | 0 | 0 | 158 | 0 | 395 | 0 | 395 | 0 | 0 | 0 | 0 | 778 |
| 08:15 AM | 0 | 238 | 0 | 238 | 147 | 0 | 0 | 147 | 0 | 423 | 0 | 423 | 0 | 0 | 0 | 0 | 808 |
| 08:30 AM | 0 | 233 | 0 | 233 | 167 | 0 | 0 | 167 | 0 | 442 | 0 | 442 | 0 | 0 | 0 | 0 | 842 |
| 08:45 AM | 0 | 276 | 0 | 276 | 162 | 0 | 0 | 162 | 0 | 401 | 0 | 401 | 0 | 0 | 0 | 0 | 839 |
| Total Volume | 0 | 972 | 0 | 972 | 634 | 0 | 0 | 634 | 0 | 1661 | 0 | 1661 | 0 | 0 | 0 | 0 | 3267 |
| % App. Total | 0 | 100 | 0 | | 100 | 0 | 0 | | 0 | 100 | 0 | | 0 | 0 | 0 | | |
| PHF | .000 | .880 | .000 | .880 | .949 | .000 | .000 | .949 | .000 | .939 | .000 | .939 | .000 | .000 | .000 | .000 | .970 |

Traffic Data Service

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 Site Code : 00000002
 Start Date : 11/13/2013
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Traffic Data Service

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(408) 377- 2988
tdsbay@cs.com

File Name : 2AM FINAL
Site Code : 00000002
Start Date : 11/13/2013
Page No : 1

Groups Printed- Bikes

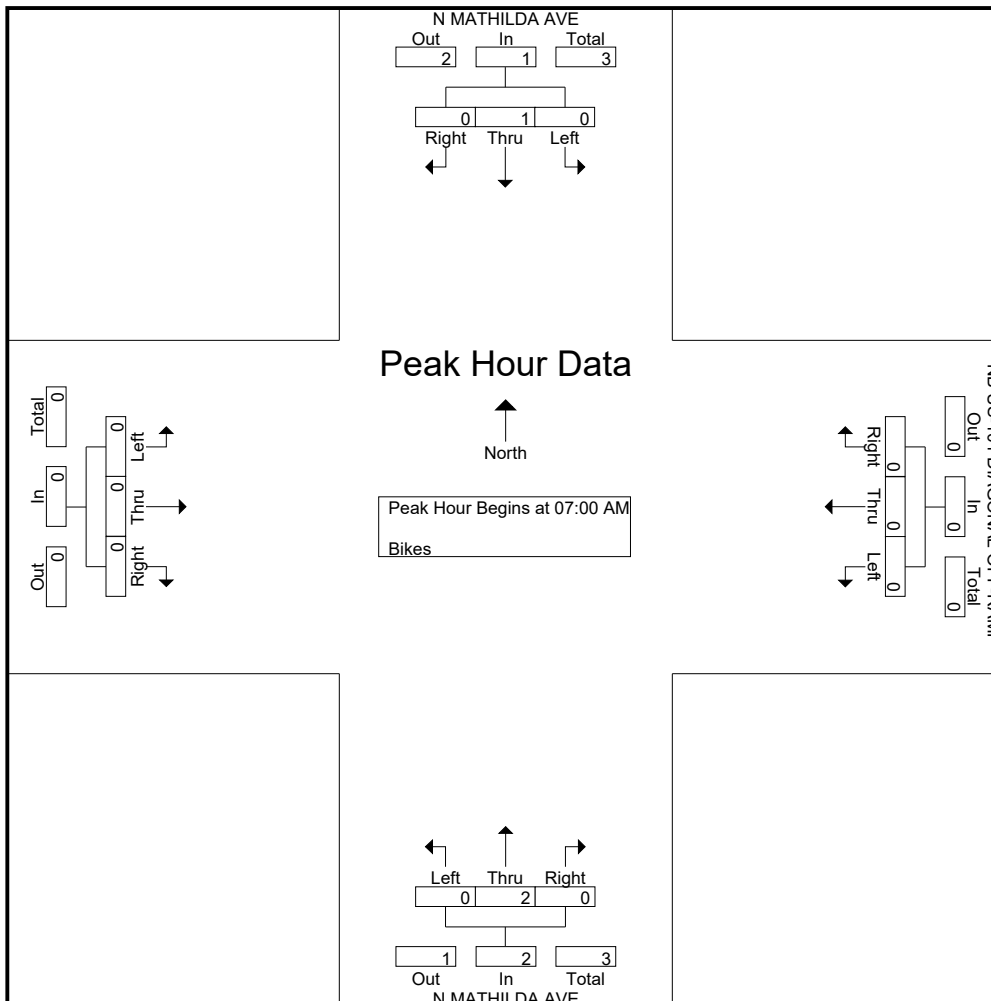
| Start Time | N MATHILDA AVE Southbound | | | | | NB US-101 DIAGONAL OFF- RAMP Westbound | | | | | N MATHILDA AVE Northbound | | | | | Eastbound | | | | | Int. Total |
|--------------------|------------------------------|------|------|------|------------|--|------|------|------|------------|------------------------------|------|------|------|------------|-----------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:15 AM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| Grand Total | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 |
| Apprch % | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | |
| Total % | 0 | 25 | 0 | 0 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 75 | 0 | 0 | 75 | 0 | 0 | 0 | 0 | 0 | 0 |

| Start Time | N MATHILDA AVE Southbound | | | | NB US-101 DIAGONAL OFF- RAMP Westbound | | | | N MATHILDA AVE Northbound | | | | Eastbound | | | | Int. Total |
|--|------------------------------|------|------|------------|--|------|------|------------|------------------------------|------|------|------------|-----------|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 07:00 AM | | | | | | | | | | | | | | | | | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 |
| 07:15 AM | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Volume | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 |
| % App. Total | 0 | 100 | 0 | | 0 | 0 | 0 | | 0 | 100 | 0 | | 0 | 0 | 0 | | |
| PHF | .000 | .250 | .000 | .250 | .000 | .000 | .000 | .000 | .000 | .250 | .000 | .250 | .000 | .000 | .000 | .000 | .375 |

Traffic Data Service

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File Name : 2AM FINAL
 Site Code : 00000002
 Start Date : 11/13/2013
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Traffic Data Service

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(408) 377- 2988
tdsbay@cs.com

File Name : 2PM FINAL
Site Code : 00000002
Start Date : 11/13/2013
Page No : 1

Groups Printed- Vehicles

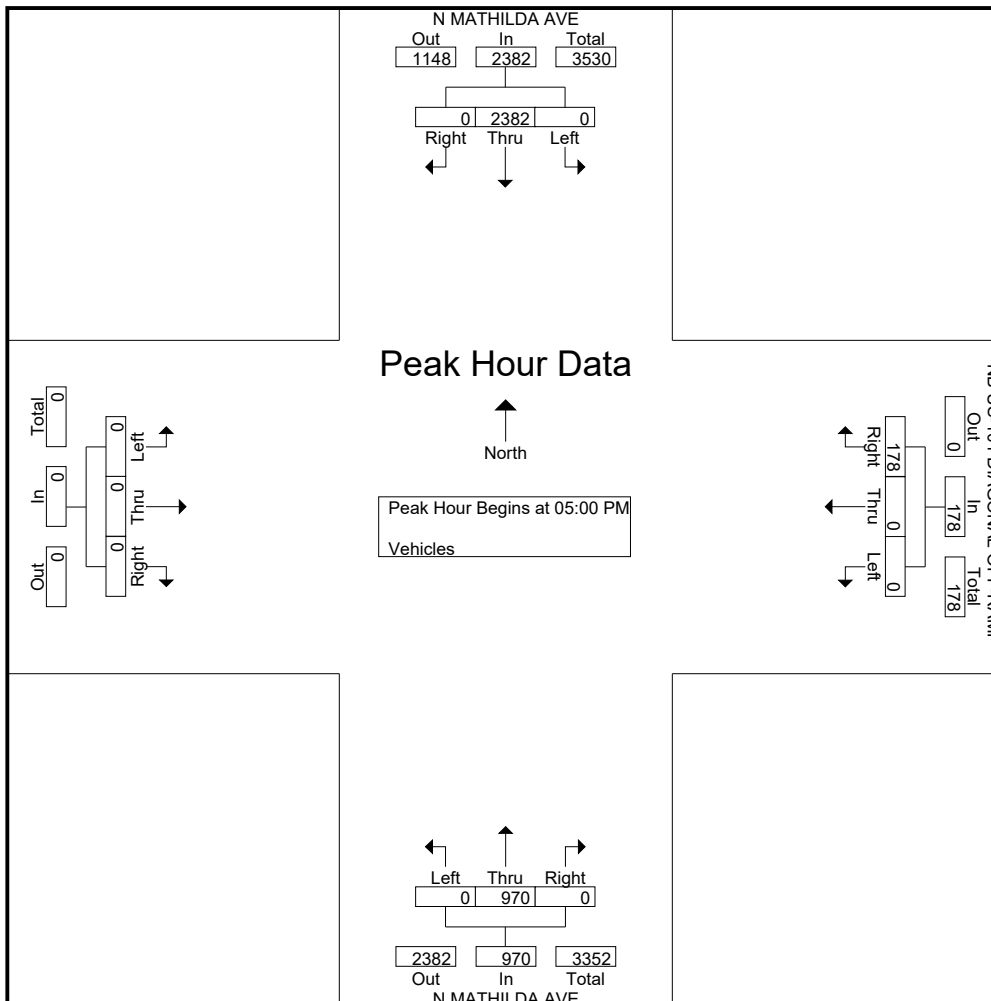
| Start Time | N MATHILDA AVE Southbound | | | | | NB US-101 DIAGONAL OFF- RAMP Westbound | | | | | N MATHILDA AVE Northbound | | | | | Eastbound | | | | | Int. Total |
|--------------------|------------------------------|------|------|------|------------|--|------|------|------|------------|------------------------------|------|------|------|------------|-----------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:00 PM | 0 | 407 | 0 | 0 | 407 | 32 | 0 | 0 | 0 | 32 | 0 | 215 | 0 | 0 | 215 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:15 PM | 0 | 397 | 0 | 0 | 397 | 34 | 0 | 0 | 2 | 36 | 0 | 163 | 0 | 0 | 163 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:30 PM | 0 | 516 | 0 | 0 | 516 | 44 | 0 | 0 | 0 | 44 | 0 | 207 | 0 | 0 | 207 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:45 PM | 0 | 542 | 0 | 0 | 542 | 42 | 0 | 0 | 2 | 44 | 0 | 222 | 0 | 0 | 222 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 1862 | 0 | 0 | 1862 | 152 | 0 | 0 | 4 | 156 | 0 | 807 | 0 | 0 | 807 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:00 PM | 0 | 592 | 0 | 0 | 592 | 29 | 0 | 0 | 1 | 30 | 0 | 261 | 0 | 0 | 261 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:15 PM | 0 | 637 | 0 | 0 | 637 | 39 | 0 | 0 | 2 | 41 | 0 | 218 | 0 | 0 | 218 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:30 PM | 0 | 590 | 0 | 0 | 590 | 61 | 0 | 0 | 1 | 62 | 0 | 245 | 0 | 0 | 245 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:45 PM | 0 | 563 | 0 | 0 | 563 | 49 | 0 | 0 | 2 | 51 | 0 | 246 | 0 | 0 | 246 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 2382 | 0 | 0 | 2382 | 178 | 0 | 0 | 6 | 184 | 0 | 970 | 0 | 0 | 970 | 0 | 0 | 0 | 0 | 0 | 0 |
| 06:00 PM | 0 | 617 | 0 | 0 | 617 | 34 | 0 | 0 | 1 | 35 | 0 | 208 | 0 | 0 | 208 | 0 | 0 | 0 | 0 | 0 | 0 |
| 06:15 PM | 0 | 602 | 0 | 0 | 602 | 38 | 0 | 0 | 0 | 38 | 0 | 190 | 0 | 0 | 190 | 0 | 0 | 0 | 0 | 0 | 0 |
| 06:30 PM | 0 | 514 | 0 | 0 | 514 | 38 | 0 | 0 | 0 | 38 | 0 | 195 | 0 | 0 | 195 | 0 | 0 | 0 | 0 | 0 | 0 |
| 06:45 PM | 0 | 466 | 0 | 0 | 466 | 40 | 0 | 0 | 0 | 40 | 0 | 182 | 0 | 0 | 182 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 2199 | 0 | 0 | 2199 | 150 | 0 | 0 | 1 | 151 | 0 | 775 | 0 | 0 | 775 | 0 | 0 | 0 | 0 | 0 | 0 |
| Grand Total | 0 | 6443 | 0 | 0 | 6443 | 480 | 0 | 0 | 11 | 491 | 0 | 2552 | 0 | 0 | 2552 | 0 | 0 | 0 | 0 | 0 | 0 |
| Apprch % | 0 | 100 | 0 | 0 | | 97.8 | 0 | 0 | 2.2 | | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | |
| Total % | 0 | 67.9 | 0 | 0 | 67.9 | 5.1 | 0 | 0 | 0.1 | 5.2 | 0 | 26.9 | 0 | 0 | 26.9 | 0 | 0 | 0 | 0 | 0 | |

| Start Time | N MATHILDA AVE Southbound | | | | NB US-101 DIAGONAL OFF- RAMP Westbound | | | | N MATHILDA AVE Northbound | | | | Eastbound | | | | Int. Total |
|--|------------------------------|------------|------|------------|--|------|------|------------|------------------------------|------------|------|------------|-----------|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 04:00 PM to 06:45 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 05:00 PM | | | | | | | | | | | | | | | | | |
| 05:00 PM | 0 | 592 | 0 | 592 | 29 | 0 | 0 | 29 | 0 | 261 | 0 | 261 | 0 | 0 | 0 | 0 | 0 |
| 05:15 PM | 0 | 637 | 0 | 637 | 39 | 0 | 0 | 39 | 0 | 218 | 0 | 218 | 0 | 0 | 0 | 0 | 0 |
| 05:30 PM | 0 | 590 | 0 | 590 | 61 | 0 | 0 | 61 | 0 | 245 | 0 | 245 | 0 | 0 | 0 | 0 | 896 |
| 05:45 PM | 0 | 563 | 0 | 563 | 49 | 0 | 0 | 49 | 0 | 246 | 0 | 246 | 0 | 0 | 0 | 0 | 858 |
| Total Volume | 0 | 2382 | 0 | 2382 | 178 | 0 | 0 | 178 | 0 | 970 | 0 | 970 | 0 | 0 | 0 | 0 | 3530 |
| % App. Total | 0 | 100 | 0 | | 100 | 0 | 0 | | 0 | 100 | 0 | | 0 | 0 | 0 | | |
| PHF | .000 | .935 | .000 | .935 | .730 | .000 | .000 | .730 | .000 | .929 | .000 | .929 | .000 | .000 | .000 | .000 | .985 |

Traffic Data Service

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File Name : 2PM FINAL
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Traffic Data Service

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 tdsbay@cs.com

File Name : 2PM FINAL
 Site Code : 00000002
 Start Date : 11/13/2013
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Groups Printed- Bikes

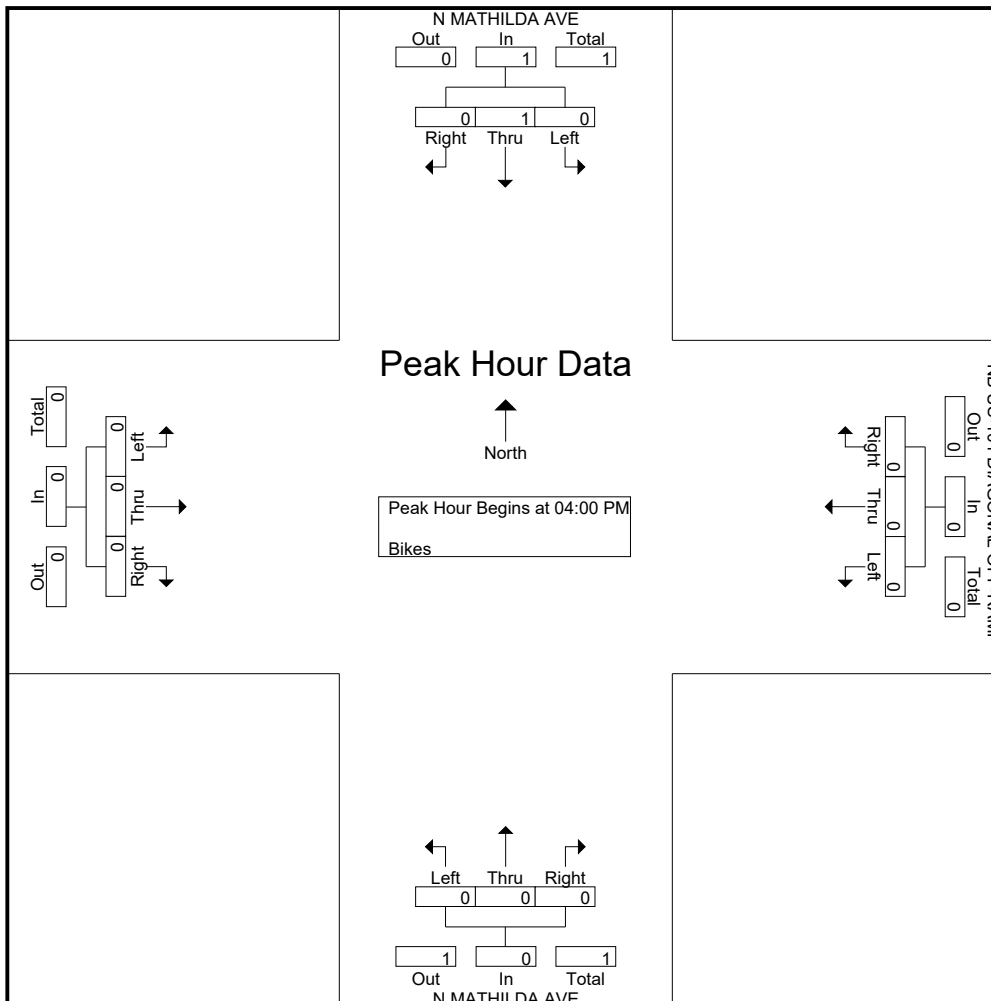
| Start Time | N MATHILDA AVE Southbound | | | | | NB US-101 DIAGONAL OFF- RAMP Westbound | | | | | N MATHILDA AVE Northbound | | | | | Eastbound | | | | | Int. Total |
|--------------------|------------------------------|------|------|------|------------|--|------|------|------|------------|------------------------------|------|------|------|------------|-----------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:00 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 05:00 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 06:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 06:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 06:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 06:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| Grand Total | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 3 |
| Apprch % | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | |
| Total % | 0 | 66.7 | 0 | 0 | 66.7 | 0 | 0 | 0 | 0 | 0 | 0 | 33.3 | 0 | 0 | 33.3 | 0 | 0 | 0 | 0 | 0 | |

| Start Time | N MATHILDA AVE Southbound | | | | NB US-101 DIAGONAL OFF- RAMP Westbound | | | | N MATHILDA AVE Northbound | | | | Eastbound | | | | Int. Total |
|--|------------------------------|------|------|------------|--|------|------|------------|------------------------------|------|------|------------|-----------|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 04:00 PM to 06:45 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 04:00 PM | | | | | | | | | | | | | | | | | |
| 04:00 PM | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Volume | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| % App. Total | 0 | 100 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | |
| PHF | .000 | .250 | .000 | .250 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .250 |

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Traffic Data Service

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File Name : 3AM FINAL
 Site Code : 00000003
 Start Date : 11/13/2013
 Page No : 1

Groups Printed- Vehicles

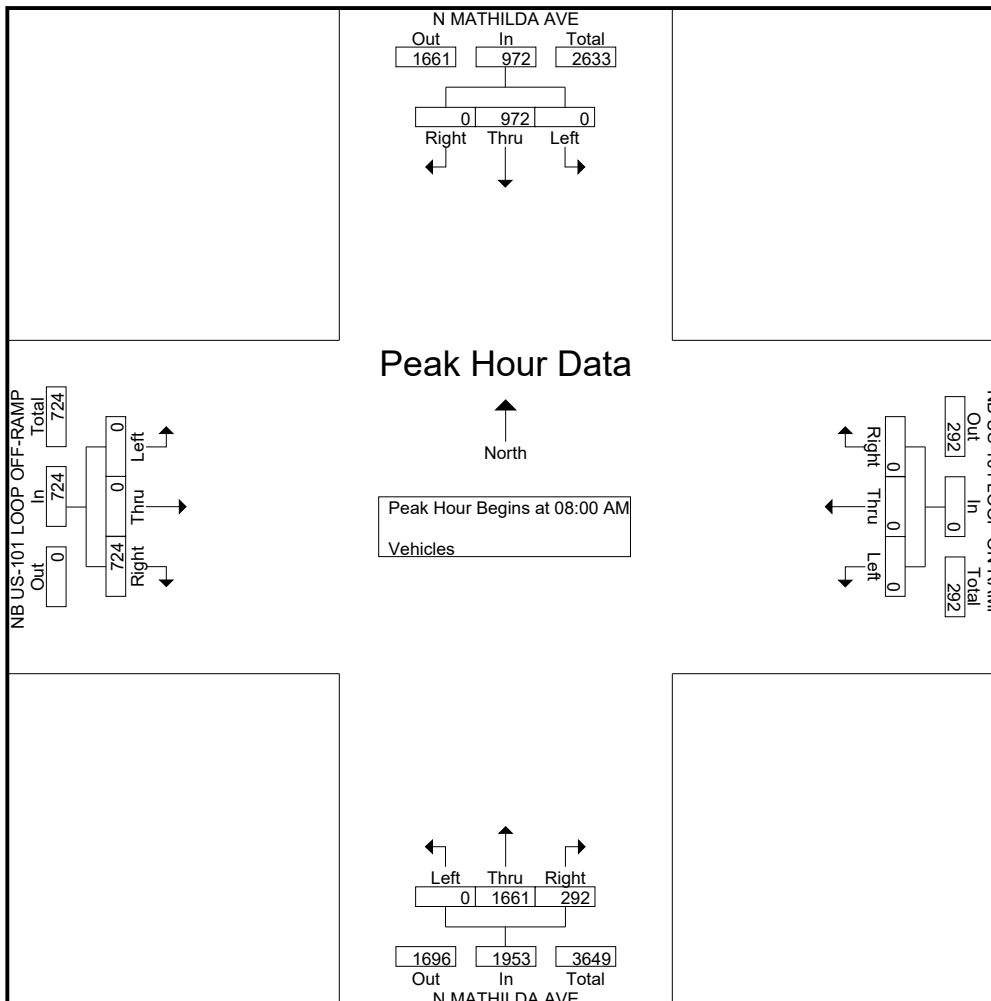
| Start Time | N MATHILDA AVE Southbound | | | | | NB US-101 LOOP ON-RAMP Westbound | | | | | N MATHILDA AVE Northbound | | | | | NB US-101 LOOP OFF-RAMP Eastbound | | | | | Int. Total |
|-------------|---------------------------|------|------|------|------------|----------------------------------|------|------|------|------------|---------------------------|------|------|------|------------|-----------------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 0 | 176 | 0 | 0 | 176 | 0 | 0 | 0 | 0 | 0 | 73 | 202 | 0 | 0 | 275 | 129 | 0 | 0 | 1 | 130 | 581 |
| 07:15 AM | 0 | 169 | 0 | 1 | 170 | 0 | 0 | 0 | 0 | 0 | 82 | 245 | 0 | 0 | 327 | 111 | 0 | 0 | 2 | 113 | 610 |
| 07:30 AM | 0 | 187 | 0 | 0 | 187 | 0 | 0 | 0 | 0 | 0 | 77 | 264 | 0 | 0 | 341 | 132 | 0 | 0 | 4 | 136 | 664 |
| 07:45 AM | 0 | 249 | 0 | 0 | 249 | 0 | 0 | 0 | 0 | 0 | 77 | 367 | 0 | 0 | 444 | 195 | 0 | 0 | 1 | 196 | 889 |
| Total | 0 | 781 | 0 | 1 | 782 | 0 | 0 | 0 | 0 | 0 | 309 | 1078 | 0 | 0 | 1387 | 567 | 0 | 0 | 8 | 575 | 2744 |
| 08:00 AM | 0 | 225 | 0 | 0 | 225 | 0 | 0 | 0 | 0 | 0 | 72 | 395 | 0 | 0 | 467 | 171 | 0 | 0 | 1 | 172 | 864 |
| 08:15 AM | 0 | 238 | 0 | 0 | 238 | 0 | 0 | 0 | 0 | 0 | 84 | 423 | 0 | 0 | 507 | 177 | 0 | 0 | 2 | 179 | 924 |
| 08:30 AM | 0 | 233 | 0 | 0 | 233 | 0 | 0 | 0 | 0 | 0 | 73 | 442 | 0 | 0 | 515 | 161 | 0 | 0 | 0 | 161 | 909 |
| 08:45 AM | 0 | 276 | 0 | 0 | 276 | 0 | 0 | 0 | 0 | 0 | 63 | 401 | 0 | 0 | 464 | 215 | 0 | 0 | 3 | 218 | 958 |
| Total | 0 | 972 | 0 | 0 | 972 | 0 | 0 | 0 | 0 | 0 | 292 | 1661 | 0 | 0 | 1953 | 724 | 0 | 0 | 6 | 730 | 3655 |
| Grand Total | 0 | 1753 | 0 | 1 | 1754 | 0 | 0 | 0 | 0 | 0 | 601 | 2739 | 0 | 0 | 3340 | 1291 | 0 | 0 | 14 | 1305 | 6399 |
| Apprch % | 0 | 99.9 | 0 | 0.1 | | 0 | 0 | 0 | 0 | | 18 | 82 | 0 | 0 | | 98.9 | 0 | 0 | 1.1 | | |
| Total % | 0 | 27.4 | 0 | 0 | 27.4 | 0 | 0 | 0 | 0 | 0 | 9.4 | 42.8 | 0 | 0 | 52.2 | 20.2 | 0 | 0 | 0.2 | 20.4 | |

| Start Time | N MATHILDA AVE Southbound | | | | NB US-101 LOOP ON-RAMP Westbound | | | | N MATHILDA AVE Northbound | | | | NB US-101 LOOP OFF-RAMP Eastbound | | | | Int. Total |
|--|---------------------------|------|------|------------|----------------------------------|------|------|------------|---------------------------|------|------|------------|-----------------------------------|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 08:00 AM | | | | | | | | | | | | | | | | | |
| 08:00 AM | 0 | 225 | 0 | 225 | 0 | 0 | 0 | 0 | 72 | 395 | 0 | 467 | 171 | 0 | 0 | 171 | 863 |
| 08:15 AM | 0 | 238 | 0 | 238 | 0 | 0 | 0 | 0 | 84 | 423 | 0 | 507 | 177 | 0 | 0 | 177 | 922 |
| 08:30 AM | 0 | 233 | 0 | 233 | 0 | 0 | 0 | 0 | 73 | 442 | 0 | 515 | 161 | 0 | 0 | 161 | 909 |
| 08:45 AM | 0 | 276 | 0 | 276 | 0 | 0 | 0 | 0 | 63 | 401 | 0 | 464 | 215 | 0 | 0 | 215 | 955 |
| Total Volume | 0 | 972 | 0 | 972 | 0 | 0 | 0 | 0 | 292 | 1661 | 0 | 1953 | 724 | 0 | 0 | 724 | 3649 |
| % App. Total | 0 | 100 | 0 | | 0 | 0 | 0 | | 15 | 85 | 0 | | 100 | 0 | 0 | | |
| PHF | .000 | .880 | .000 | .880 | .000 | .000 | .000 | .000 | .869 | .939 | .000 | .948 | .842 | .000 | .000 | .842 | .955 |

Traffic Data Service

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Traffic Data Service

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File Name : 3AM FINAL
 Site Code : 00000003
 Start Date : 11/13/2013
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Groups Printed- Bikes

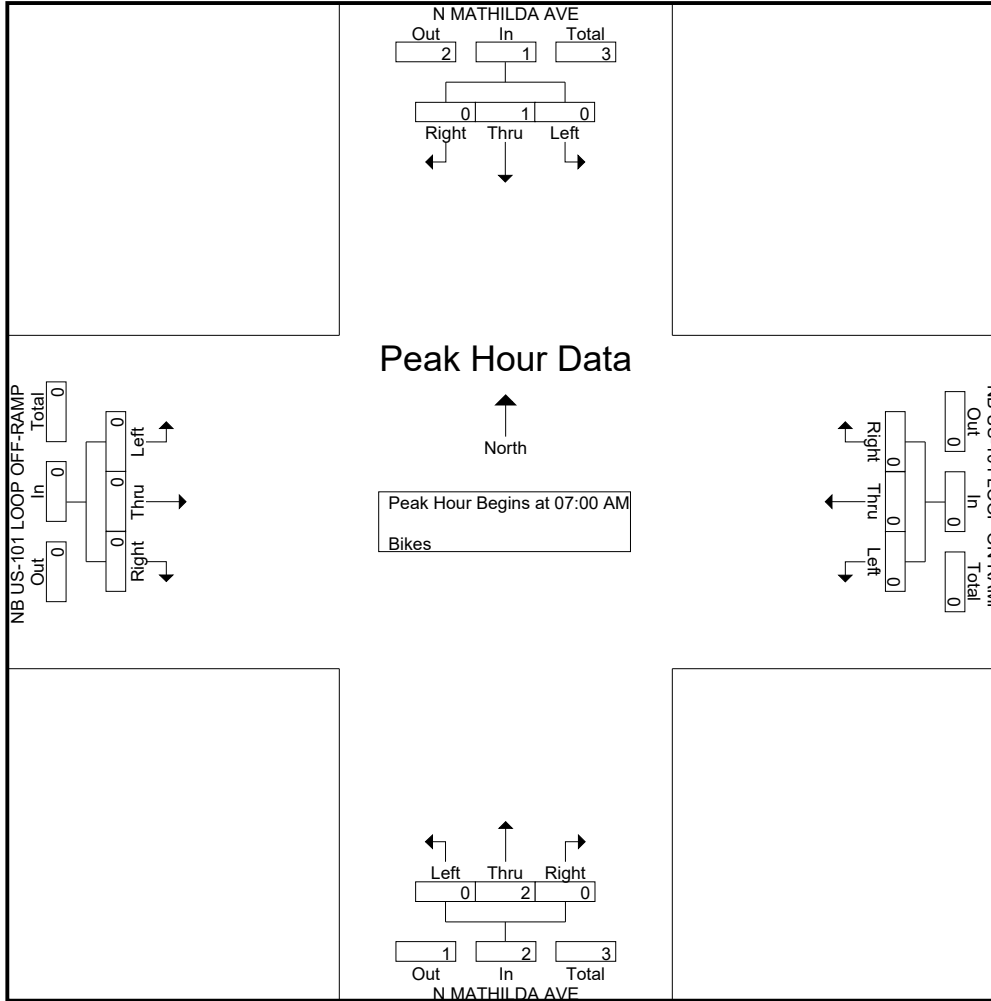
| Start Time | N MATHILDA AVE Southbound | | | | | NB US-101 LOOP ON-RAMP Westbound | | | | | N MATHILDA AVE Northbound | | | | | NB US-101 LOOP OFF-RAMP Eastbound | | | | | Int. Total |
|--------------|------------------------------|------|------|------|------------|-------------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|--------------------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 2 |
| 07:15 AM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 3 |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| Grand Total | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 4 |
| Apprch % | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | |
| Total % | 0 | 25 | 0 | 0 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 75 | 0 | 0 | 75 | 0 | 0 | 0 | 0 | 0 | |

| Start Time | N MATHILDA AVE Southbound | | | | NB US-101 LOOP ON-RAMP Westbound | | | | N MATHILDA AVE Northbound | | | | NB US-101 LOOP OFF-RAMP Eastbound | | | | Int. Total |
|--|------------------------------|------|------|------------|-------------------------------------|------|------|------------|------------------------------|------|------|------------|--------------------------------------|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 07:00 AM | | | | | | | | | | | | | | | | | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 07:15 AM | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Volume | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 3 |
| % App. Total | 0 | 100 | 0 | | 0 | 0 | 0 | | 0 | 100 | 0 | | 0 | 0 | 0 | | |
| PHF | .000 | .250 | .000 | .250 | .000 | .000 | .000 | .000 | .000 | .250 | .000 | .250 | .000 | .000 | .000 | .000 | .375 |

Traffic Data Service

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Traffic Data Service

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File Name : 3PM FINAL
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Groups Printed- Vehicles

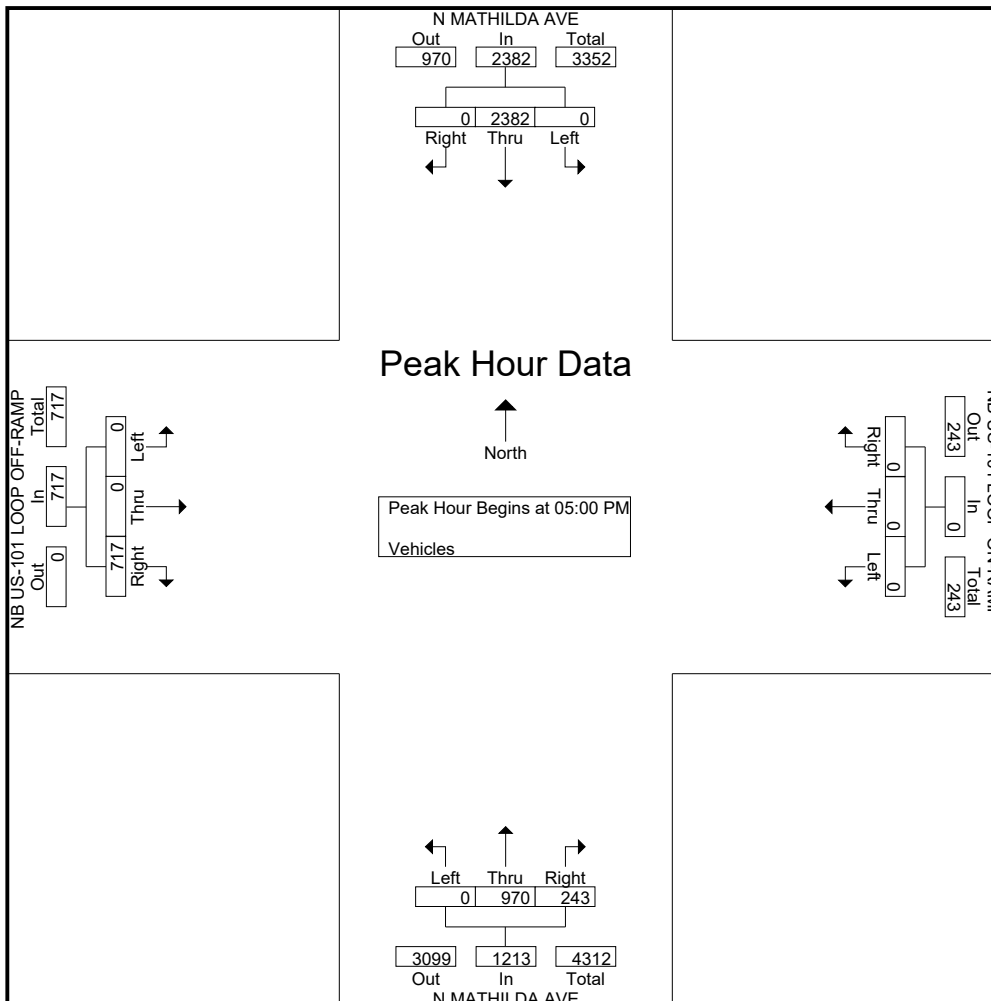
| Start Time | N MATHILDA AVE Southbound | | | | | NB US-101 LOOP ON-RAMP Westbound | | | | | N MATHILDA AVE Northbound | | | | | NB US-101 LOOP OFF-RAMP Eastbound | | | | | Int. Total |
|-------------|------------------------------|------|------|------|------------|-------------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|--------------------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:00 PM | 0 | 407 | 0 | 0 | 407 | 0 | 0 | 0 | 0 | 0 | 84 | 215 | 0 | 0 | 299 | 82 | 0 | 0 | 0 | 82 | 788 |
| 04:15 PM | 0 | 397 | 0 | 0 | 397 | 0 | 0 | 0 | 0 | 0 | 69 | 163 | 0 | 1 | 233 | 92 | 0 | 0 | 2 | 94 | 724 |
| 04:30 PM | 0 | 516 | 0 | 0 | 516 | 0 | 0 | 0 | 0 | 0 | 73 | 207 | 0 | 0 | 280 | 125 | 0 | 0 | 0 | 125 | 921 |
| 04:45 PM | 0 | 542 | 0 | 0 | 542 | 0 | 0 | 0 | 0 | 0 | 70 | 222 | 0 | 0 | 292 | 167 | 0 | 0 | 2 | 169 | 1003 |
| Total | 0 | 1862 | 0 | 0 | 1862 | 0 | 0 | 0 | 0 | 0 | 296 | 807 | 0 | 1 | 1104 | 466 | 0 | 0 | 4 | 470 | 3436 |
| 05:00 PM | 0 | 592 | 0 | 0 | 592 | 0 | 0 | 0 | 0 | 0 | 72 | 261 | 0 | 0 | 333 | 152 | 0 | 0 | 1 | 153 | 1078 |
| 05:15 PM | 0 | 637 | 0 | 0 | 637 | 0 | 0 | 0 | 0 | 0 | 63 | 218 | 0 | 0 | 281 | 204 | 0 | 0 | 2 | 206 | 1124 |
| 05:30 PM | 0 | 590 | 0 | 0 | 590 | 0 | 0 | 0 | 0 | 0 | 55 | 245 | 0 | 0 | 300 | 182 | 0 | 0 | 1 | 183 | 1073 |
| 05:45 PM | 0 | 563 | 0 | 0 | 563 | 0 | 0 | 0 | 0 | 0 | 53 | 246 | 0 | 0 | 299 | 179 | 0 | 0 | 2 | 181 | 1043 |
| Total | 0 | 2382 | 0 | 0 | 2382 | 0 | 0 | 0 | 0 | 0 | 243 | 970 | 0 | 0 | 1213 | 717 | 0 | 0 | 6 | 723 | 4318 |
| 06:00 PM | 0 | 617 | 0 | 0 | 617 | 0 | 0 | 0 | 0 | 0 | 55 | 208 | 0 | 0 | 263 | 181 | 0 | 0 | 2 | 183 | 1063 |
| 06:15 PM | 0 | 602 | 0 | 0 | 602 | 0 | 0 | 0 | 0 | 0 | 62 | 190 | 0 | 0 | 252 | 175 | 0 | 0 | 0 | 175 | 1029 |
| 06:30 PM | 0 | 514 | 0 | 0 | 514 | 0 | 0 | 0 | 0 | 0 | 67 | 195 | 0 | 0 | 262 | 148 | 0 | 0 | 0 | 148 | 924 |
| 06:45 PM | 0 | 466 | 0 | 0 | 466 | 0 | 0 | 0 | 0 | 0 | 66 | 182 | 0 | 0 | 248 | 150 | 0 | 0 | 0 | 150 | 864 |
| Total | 0 | 2199 | 0 | 0 | 2199 | 0 | 0 | 0 | 0 | 0 | 250 | 775 | 0 | 0 | 1025 | 654 | 0 | 0 | 2 | 656 | 3880 |
| Grand Total | 0 | 6443 | 0 | 0 | 6443 | 0 | 0 | 0 | 0 | 0 | 789 | 2552 | 0 | 1 | 3342 | 1837 | 0 | 0 | 12 | 1849 | 11634 |
| Apprch % | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | 23.6 | 76.4 | 0 | 0 | | 99.4 | 0 | 0 | 0.6 | | |
| Total % | 0 | 55.4 | 0 | 0 | 55.4 | 0 | 0 | 0 | 0 | 0 | 6.8 | 21.9 | 0 | 0 | 28.7 | 15.8 | 0 | 0 | 0.1 | 15.9 | |

| Start Time | N MATHILDA AVE Southbound | | | | NB US-101 LOOP ON-RAMP Westbound | | | | N MATHILDA AVE Northbound | | | | NB US-101 LOOP OFF-RAMP Eastbound | | | | Int. Total |
|--|------------------------------|------------|------|------------|-------------------------------------|------|------|------------|------------------------------|------------|------|------------|--------------------------------------|------|------|------------|-------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 04:00 PM to 06:45 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 05:00 PM | | | | | | | | | | | | | | | | | |
| 05:00 PM | 0 | 592 | 0 | 592 | 0 | 0 | 0 | 0 | 72 | 261 | 0 | 333 | 152 | 0 | 0 | 152 | 1077 |
| 05:15 PM | 0 | 637 | 0 | 637 | 0 | 0 | 0 | 0 | 63 | 218 | 0 | 281 | 204 | 0 | 0 | 204 | 1122 |
| 05:30 PM | 0 | 590 | 0 | 590 | 0 | 0 | 0 | 0 | 55 | 245 | 0 | 300 | 182 | 0 | 0 | 182 | 1072 |
| 05:45 PM | 0 | 563 | 0 | 563 | 0 | 0 | 0 | 0 | 53 | 246 | 0 | 299 | 179 | 0 | 0 | 179 | 1041 |
| Total Volume | 0 | 2382 | 0 | 2382 | 0 | 0 | 0 | 0 | 243 | 970 | 0 | 1213 | 717 | 0 | 0 | 717 | 4312 |
| % App. Total | 0 | 100 | 0 | | 0 | 0 | 0 | | 20 | 80 | 0 | | 100 | 0 | 0 | | |
| PHF | .000 | .935 | .000 | .935 | .000 | .000 | .000 | .000 | .844 | .929 | .000 | .911 | .879 | .000 | .000 | .879 | .961 |

Traffic Data Service

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File Name : 3PM FINAL
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Groups Printed- Bikes

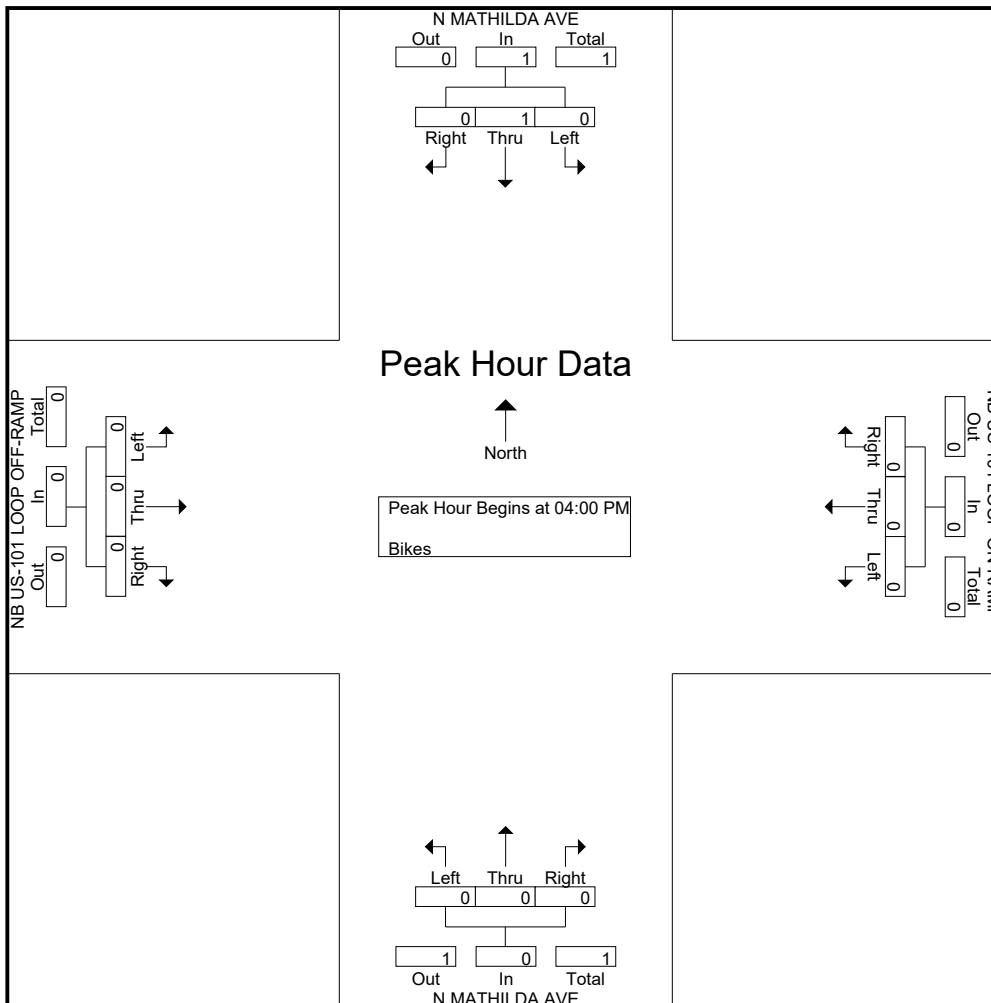
| Start Time | N MATHILDA AVE Southbound | | | | | NB US-101 LOOP ON-RAMP Westbound | | | | | N MATHILDA AVE Northbound | | | | | NB US-101 LOOP OFF-RAMP Eastbound | | | | | Int. Total | | | | | |
|--------------------|------------------------------|------|------|------|------------|-------------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|--------------------------------------|------|------|------|------------|------------|---|---|---|---|---|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | | | | | | |
| 04:00 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 05:00 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 06:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 06:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 06:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 06:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| Grand Total | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| Apprch % | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | |
| Total % | 0 | 66.7 | 0 | 0 | 66.7 | 0 | 0 | 0 | 0 | 0 | 0 | 33.3 | 0 | 0 | 33.3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |

| Start Time | N MATHILDA AVE Southbound | | | | NB US-101 LOOP ON-RAMP Westbound | | | | N MATHILDA AVE Northbound | | | | NB US-101 LOOP OFF-RAMP Eastbound | | | | Int. Total | | | | |
|--|------------------------------|------|------|------------|-------------------------------------|------|------|------------|------------------------------|------|------|------------|--------------------------------------|------|------|------------|------------|------|------|------|------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | | | | | |
| Peak Hour Analysis From 04:00 PM to 06:45 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 04:00 PM | | | | | | | | | | | | | | | | | | | | | |
| 04:00 PM | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Volume | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| % App. Total | 0 | 100 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | |
| PHF | .000 | .250 | .000 | .250 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .250 |

Traffic Data Service

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Traffic Data Service

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File Name : 4AM FINAL
Site Code : 00000004
Start Date : 11/13/2013
Page No : 1

Groups Printed- Vehicles

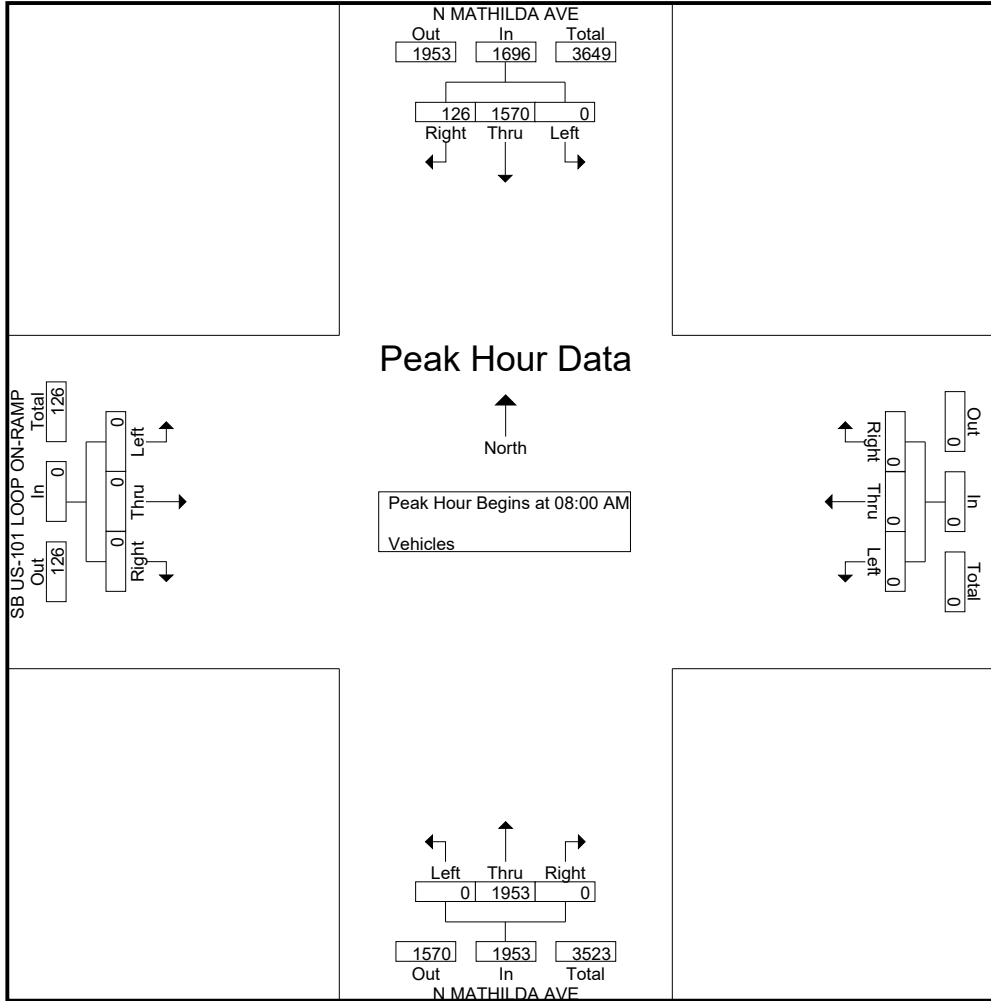
| Start Time | N MATHILDA AVE Southbound | | | | | Westbound | | | | | N MATHILDA AVE Northbound | | | | | SB US-101 LOOP ON-RAMP Eastbound | | | | | Int. Total |
|--------------|---------------------------|-------------|----------|----------|-------------|-----------|----------|----------|----------|------------|---------------------------|-------------|----------|----------|-------------|----------------------------------|----------|----------|----------|------------|-------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 20 | 285 | 0 | 0 | 305 | 0 | 0 | 0 | 0 | 0 | 0 | 275 | 0 | 0 | 275 | 0 | 0 | 0 | 0 | 0 | 580 |
| 07:15 AM | 16 | 264 | 0 | 0 | 280 | 0 | 0 | 0 | 0 | 0 | 0 | 327 | 0 | 0 | 327 | 0 | 0 | 0 | 0 | 0 | 607 |
| 07:30 AM | 21 | 298 | 0 | 0 | 319 | 0 | 0 | 0 | 0 | 0 | 0 | 341 | 0 | 0 | 341 | 0 | 0 | 0 | 0 | 0 | 660 |
| 07:45 AM | 27 | 417 | 0 | 0 | 444 | 0 | 0 | 0 | 0 | 0 | 0 | 444 | 0 | 0 | 444 | 0 | 0 | 0 | 0 | 0 | 888 |
| Total | 84 | 1264 | 0 | 0 | 1348 | 0 | 0 | 0 | 0 | 0 | 0 | 1387 | 0 | 0 | 1387 | 0 | 0 | 0 | 0 | 0 | 2735 |
| 08:00 AM | 22 | 374 | 0 | 0 | 396 | 0 | 0 | 0 | 0 | 0 | 0 | 467 | 0 | 0 | 467 | 0 | 0 | 0 | 0 | 0 | 863 |
| 08:15 AM | 29 | 386 | 0 | 0 | 415 | 0 | 0 | 0 | 0 | 0 | 0 | 507 | 0 | 0 | 507 | 0 | 0 | 0 | 0 | 0 | 922 |
| 08:30 AM | 34 | 360 | 0 | 0 | 394 | 0 | 0 | 0 | 0 | 0 | 0 | 515 | 0 | 0 | 515 | 0 | 0 | 0 | 0 | 0 | 909 |
| 08:45 AM | 41 | 450 | 0 | 0 | 491 | 0 | 0 | 0 | 0 | 0 | 0 | 464 | 0 | 0 | 464 | 0 | 0 | 0 | 0 | 0 | 955 |
| Total | 126 | 1570 | 0 | 0 | 1696 | 0 | 0 | 0 | 0 | 0 | 0 | 1953 | 0 | 0 | 1953 | 0 | 0 | 0 | 0 | 0 | 3649 |
| Grand Total | 210 | 2834 | 0 | 0 | 3044 | 0 | 0 | 0 | 0 | 0 | 0 | 3340 | 0 | 0 | 3340 | 0 | 0 | 0 | 0 | 0 | 6384 |
| Apprch % | 6.9 | 93.1 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | |
| Total % | 3.3 | 44.4 | 0 | 0 | 47.7 | 0 | 0 | 0 | 0 | 0 | 0 | 52.3 | 0 | 0 | 52.3 | 0 | 0 | 0 | 0 | 0 | |

| Start Time | N MATHILDA AVE Southbound | | | | Westbound | | | | N MATHILDA AVE Northbound | | | | SB US-101 LOOP ON-RAMP Eastbound | | | | Int. Total |
|--|---------------------------|------------|------|------------|-----------|------|------|------------|---------------------------|------------|------|------------|----------------------------------|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 08:00 AM | | | | | | | | | | | | | | | | | |
| 08:00 AM | 22 | 374 | 0 | 396 | 0 | 0 | 0 | 0 | 0 | 467 | 0 | 467 | 0 | 0 | 0 | 0 | 863 |
| 08:15 AM | 29 | 386 | 0 | 415 | 0 | 0 | 0 | 0 | 0 | 507 | 0 | 507 | 0 | 0 | 0 | 0 | 922 |
| 08:30 AM | 34 | 360 | 0 | 394 | 0 | 0 | 0 | 0 | 0 | 515 | 0 | 515 | 0 | 0 | 0 | 0 | 909 |
| 08:45 AM | 41 | 450 | 0 | 491 | 0 | 0 | 0 | 0 | 0 | 464 | 0 | 464 | 0 | 0 | 0 | 0 | 955 |
| Total Volume | 126 | 1570 | 0 | 1696 | 0 | 0 | 0 | 0 | 0 | 1953 | 0 | 1953 | 0 | 0 | 0 | 0 | 3649 |
| % App. Total | 7.4 | 92.6 | 0 | | 0 | 0 | 0 | | 0 | 100 | 0 | | 0 | 0 | 0 | | |
| PHF | .768 | .872 | .000 | .864 | .000 | .000 | .000 | .000 | .000 | .948 | .000 | .948 | .000 | .000 | .000 | .000 | .955 |

Traffic Data Service

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Traffic Data Service

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File Name : 4AM FINAL
 Site Code : 00000004
 Start Date : 11/13/2013
 Page No : 1

Groups Printed- Bikes

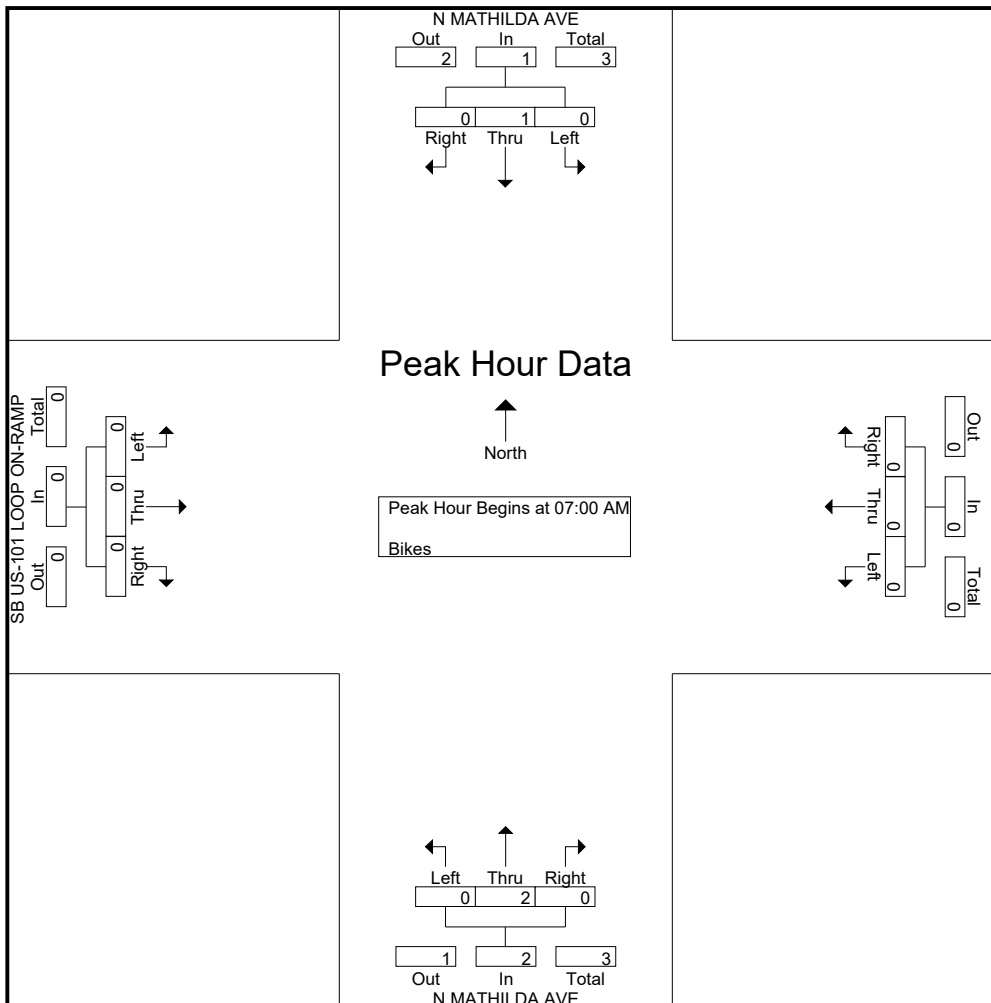
| Start Time | N MATHILDA AVE Southbound | | | | | Westbound | | | | | N MATHILDA AVE Northbound | | | | | SB US-101 LOOP ON-RAMP Eastbound | | | | | Int. Total |
|-------------|---------------------------|------|------|------|------------|-----------|------|------|------|------------|---------------------------|------|------|------|------------|----------------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 2 |
| 07:15 AM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 3 |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| Grand Total | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 4 |
| Apprch % | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | |
| Total % | 0 | 25 | 0 | 0 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 75 | 0 | 0 | 75 | 0 | 0 | 0 | 0 | 0 | |

| Start Time | N MATHILDA AVE Southbound | | | | Westbound | | | | N MATHILDA AVE Northbound | | | | SB US-101 LOOP ON-RAMP Eastbound | | | | Int. Total | |
|--|---------------------------|------|------|------------|-----------|------|------|------------|---------------------------|------|------|------------|----------------------------------|------|------|------------|------------|------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 07:00 AM | | | | | | | | | | | | | | | | | | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 2 |
| 07:15 AM | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Volume | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 3 |
| % App. Total | 0 | 100 | 0 | | 0 | 0 | 0 | | 0 | 100 | 0 | | 0 | 0 | 0 | | | |
| PHF | .000 | .250 | .000 | .250 | .000 | .000 | .000 | .000 | .000 | .000 | .250 | .000 | .250 | .000 | .000 | .000 | .000 | .375 |

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tdsbay@cs.com

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Site Code : 00000004
Start Date : 11/13/2013
Page No : 1

Groups Printed- Vehicles

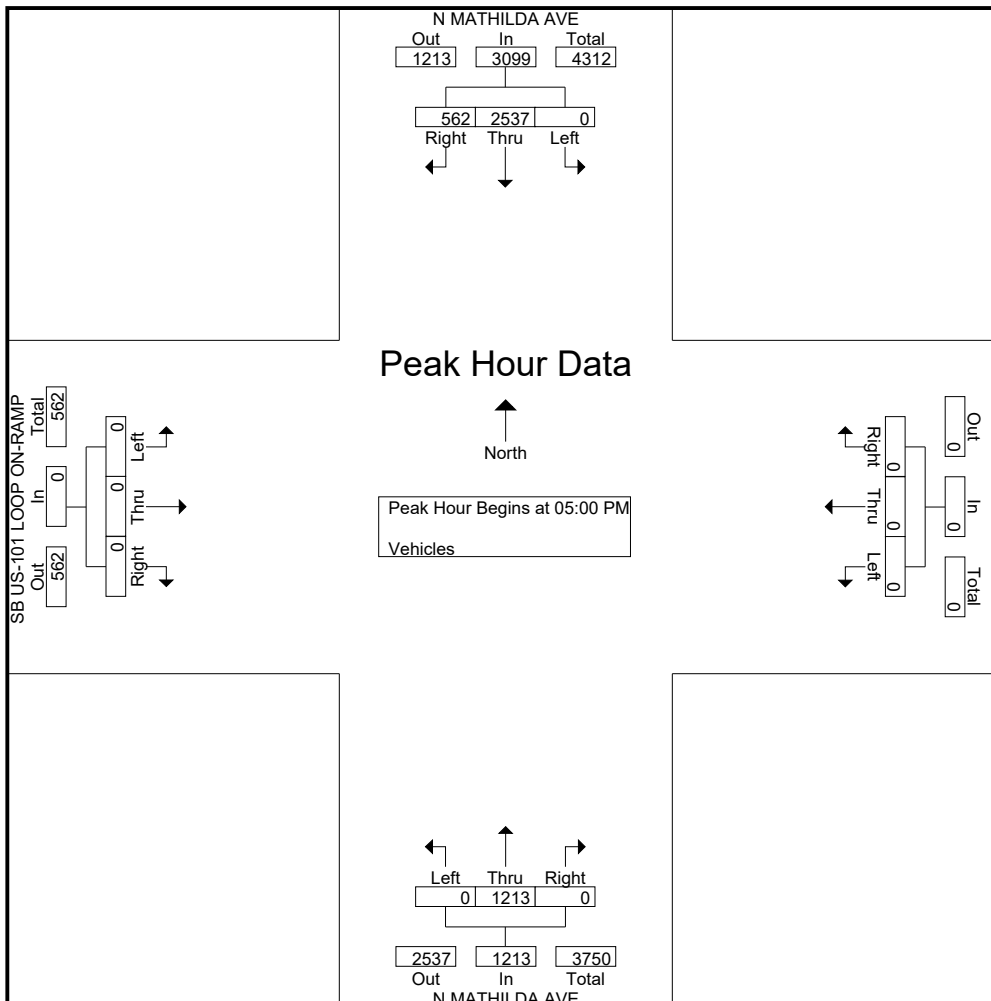
| Start Time | N MATHILDA AVE Southbound | | | | | Westbound | | | | | N MATHILDA AVE Northbound | | | | | SB US-101 LOOP ON-RAMP Eastbound | | | | | Int. Total |
|-------------|---------------------------|------|------|------|------------|-----------|------|------|------|------------|---------------------------|------|------|------|------------|----------------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:00 PM | 122 | 367 | 0 | 0 | 489 | 0 | 0 | 0 | 0 | 0 | 0 | 299 | 0 | 0 | 299 | 0 | 0 | 0 | 0 | 0 | 788 |
| 04:15 PM | 99 | 390 | 0 | 0 | 489 | 0 | 0 | 0 | 0 | 0 | 0 | 232 | 0 | 0 | 232 | 0 | 0 | 0 | 0 | 0 | 721 |
| 04:30 PM | 103 | 538 | 0 | 0 | 641 | 0 | 0 | 0 | 0 | 0 | 0 | 280 | 0 | 0 | 280 | 0 | 0 | 0 | 0 | 0 | 921 |
| 04:45 PM | 131 | 578 | 0 | 0 | 709 | 0 | 0 | 0 | 0 | 0 | 0 | 292 | 0 | 0 | 292 | 0 | 0 | 0 | 0 | 0 | 1001 |
| Total | 455 | 1873 | 0 | 0 | 2328 | 0 | 0 | 0 | 0 | 0 | 0 | 1103 | 0 | 0 | 1103 | 0 | 0 | 0 | 0 | 0 | 3431 |
| 05:00 PM | 167 | 577 | 0 | 0 | 744 | 0 | 0 | 0 | 0 | 0 | 0 | 333 | 0 | 0 | 333 | 0 | 0 | 0 | 0 | 0 | 1077 |
| 05:15 PM | 141 | 700 | 0 | 0 | 841 | 0 | 0 | 0 | 0 | 0 | 0 | 281 | 0 | 0 | 281 | 0 | 0 | 0 | 0 | 0 | 1122 |
| 05:30 PM | 128 | 644 | 0 | 0 | 772 | 0 | 0 | 0 | 0 | 0 | 0 | 300 | 0 | 0 | 300 | 0 | 0 | 0 | 0 | 0 | 1072 |
| 05:45 PM | 126 | 616 | 0 | 0 | 742 | 0 | 0 | 0 | 0 | 0 | 0 | 299 | 0 | 0 | 299 | 0 | 0 | 0 | 0 | 0 | 1041 |
| Total | 562 | 2537 | 0 | 0 | 3099 | 0 | 0 | 0 | 0 | 0 | 0 | 1213 | 0 | 0 | 1213 | 0 | 0 | 0 | 0 | 0 | 4312 |
| 06:00 PM | 155 | 643 | 0 | 0 | 798 | 0 | 0 | 0 | 0 | 0 | 0 | 263 | 0 | 0 | 263 | 0 | 0 | 0 | 0 | 0 | 1061 |
| 06:15 PM | 150 | 627 | 0 | 0 | 777 | 0 | 0 | 0 | 0 | 0 | 0 | 252 | 0 | 0 | 252 | 0 | 0 | 0 | 0 | 0 | 1029 |
| 06:30 PM | 127 | 535 | 0 | 0 | 662 | 0 | 0 | 0 | 0 | 0 | 0 | 262 | 0 | 0 | 262 | 0 | 0 | 0 | 0 | 0 | 924 |
| 06:45 PM | 99 | 517 | 0 | 0 | 616 | 0 | 0 | 0 | 0 | 0 | 0 | 248 | 0 | 0 | 248 | 0 | 0 | 0 | 0 | 0 | 864 |
| Total | 531 | 2322 | 0 | 0 | 2853 | 0 | 0 | 0 | 0 | 0 | 0 | 1025 | 0 | 0 | 1025 | 0 | 0 | 0 | 0 | 0 | 3878 |
| Grand Total | 1548 | 6732 | 0 | 0 | 8280 | 0 | 0 | 0 | 0 | 0 | 0 | 3341 | 0 | 0 | 3341 | 0 | 0 | 0 | 0 | 0 | 11621 |
| Apprch % | 18.7 | 81.3 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | |
| Total % | 13.3 | 57.9 | 0 | 0 | 71.3 | 0 | 0 | 0 | 0 | 0 | 0 | 28.7 | 0 | 0 | 28.7 | 0 | 0 | 0 | 0 | 0 | |

| Start Time | N MATHILDA AVE Southbound | | | | Westbound | | | | N MATHILDA AVE Northbound | | | | SB US-101 LOOP ON-RAMP Eastbound | | | | Int. Total |
|--|---------------------------|------|------|------------|-----------|------|------|------------|---------------------------|------|------|------------|----------------------------------|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 04:00 PM to 06:45 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 05:00 PM | | | | | | | | | | | | | | | | | |
| 05:00 PM | 167 | 577 | 0 | 744 | 0 | 0 | 0 | 0 | 0 | 333 | 0 | 333 | 0 | 0 | 0 | 0 | 1077 |
| 05:15 PM | 141 | 700 | 0 | 841 | 0 | 0 | 0 | 0 | 0 | 281 | 0 | 281 | 0 | 0 | 0 | 0 | 1122 |
| 05:30 PM | 128 | 644 | 0 | 772 | 0 | 0 | 0 | 0 | 0 | 300 | 0 | 300 | 0 | 0 | 0 | 0 | 1072 |
| 05:45 PM | 126 | 616 | 0 | 742 | 0 | 0 | 0 | 0 | 0 | 299 | 0 | 299 | 0 | 0 | 0 | 0 | 1041 |
| Total Volume | 562 | 2537 | 0 | 3099 | 0 | 0 | 0 | 0 | 0 | 1213 | 0 | 1213 | 0 | 0 | 0 | 0 | 4312 |
| % App. Total | 18.1 | 81.9 | 0 | | 0 | 0 | 0 | | 0 | 100 | 0 | | 0 | 0 | 0 | | |
| PHF | .841 | .906 | .000 | .921 | .000 | .000 | .000 | .000 | .000 | .911 | .000 | .911 | .000 | .000 | .000 | .000 | .961 |

Traffic Data Service

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File Name : 4PM FINAL
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Groups Printed- Bikes

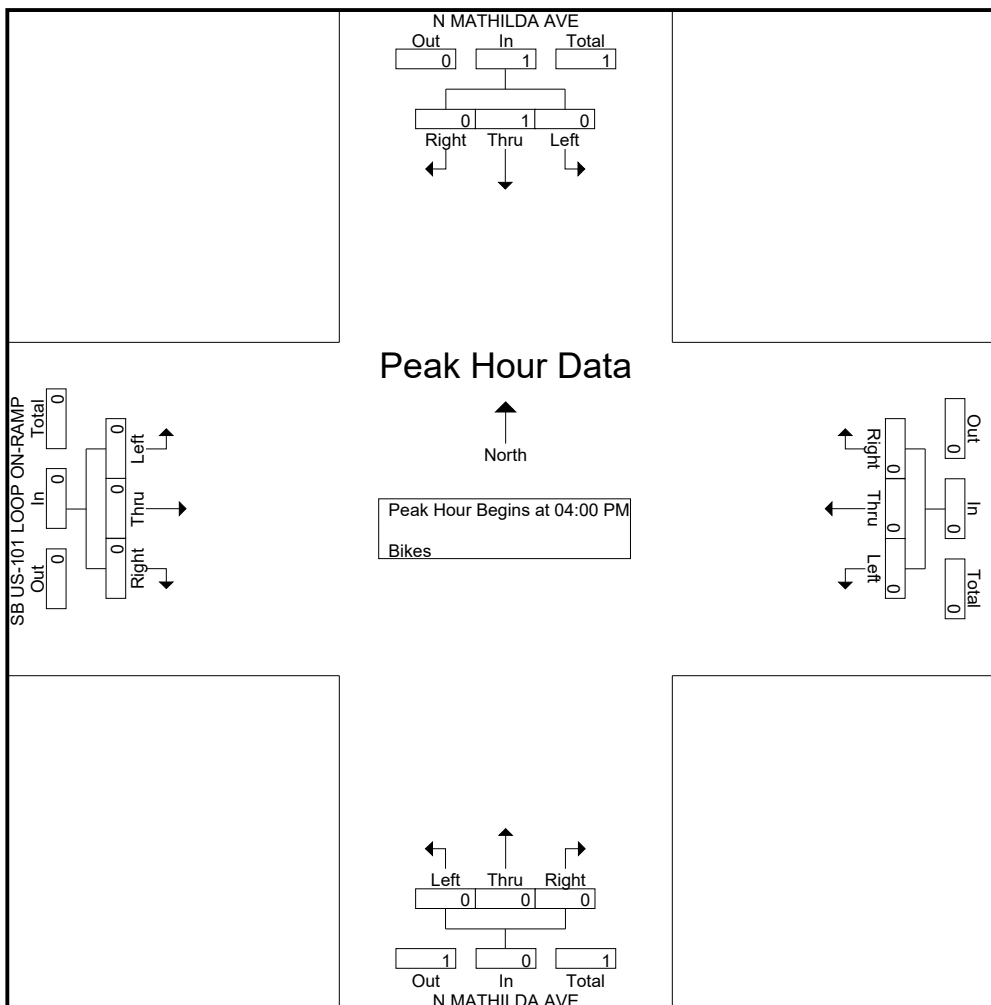
| Start Time | N MATHILDA AVE Southbound | | | | | Westbound | | | | | N MATHILDA AVE Northbound | | | | | SB US-101 LOOP ON-RAMP Eastbound | | | | | Int. Total |
|--------------------|---------------------------|----------|----------|----------|------------|-----------|----------|----------|----------|------------|---------------------------|----------|----------|----------|------------|----------------------------------|----------|----------|----------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:00 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 05:00 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 06:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 06:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 06:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 06:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| Grand Total | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 3 |
| Apprch % | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | |
| Total % | 0 | 66.7 | 0 | 0 | 66.7 | 0 | 0 | 0 | 0 | 0 | 0 | 33.3 | 0 | 0 | 33.3 | 0 | 0 | 0 | 0 | 0 | |

| Start Time | N MATHILDA AVE Southbound | | | | Westbound | | | | N MATHILDA AVE Northbound | | | | SB US-101 LOOP ON-RAMP Eastbound | | | | Int. Total |
|--|---------------------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|---------------------------|-------------|-------------|-------------|----------------------------------|-------------|-------------|-------------|-------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 04:00 PM to 06:45 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 04:00 PM | | | | | | | | | | | | | | | | | |
| 04:00 PM | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Volume | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| % App. Total | 0 | 100 | 0 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 100 |
| PHF | .000 | .250 | .000 | .250 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .250 |

Traffic Data Service

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File Name : 4PM FINAL
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Traffic Data Service

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File Name : 5AM FINAL
Site Code : 00000005
Start Date : 11/13/2013
Page No : 1

Groups Printed- Vehicles

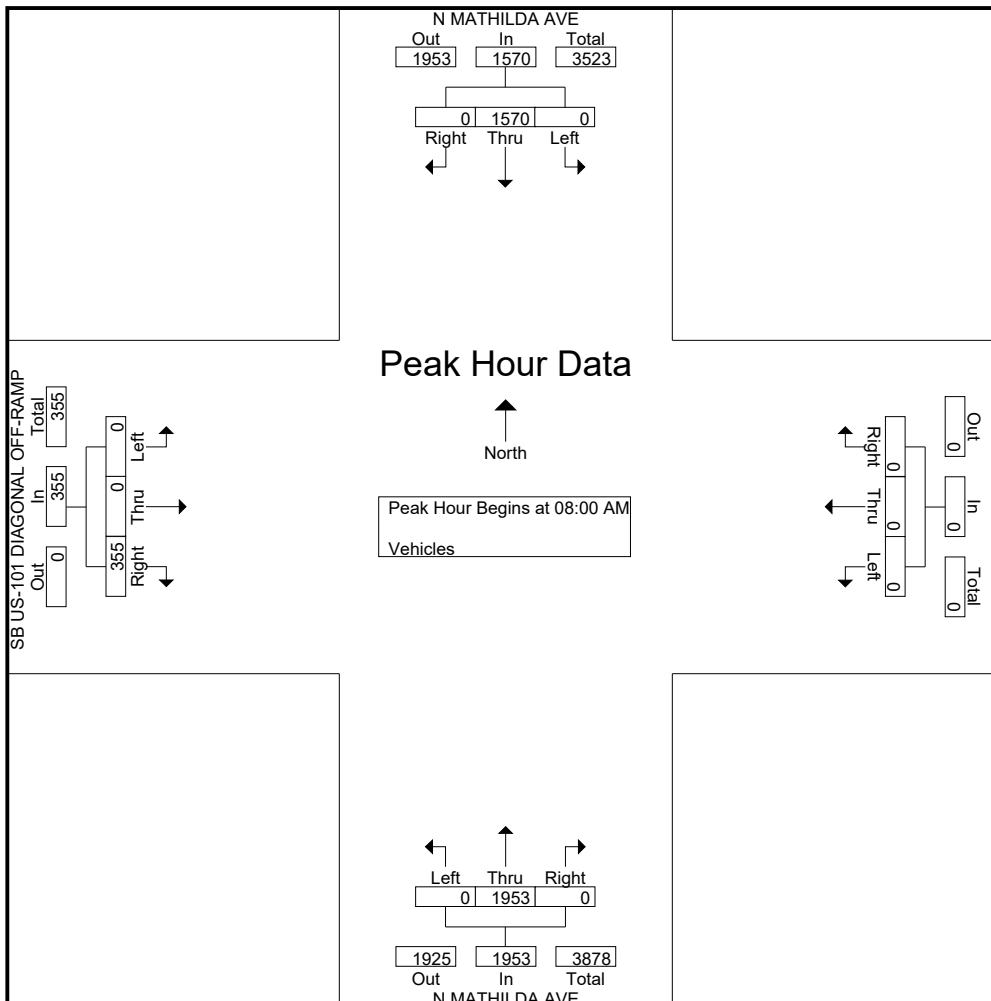
| Start Time | N MATHILDA AVE Southbound | | | | | Westbound | | | | | N MATHILDA AVE Northbound | | | | | SB US-101 DIAGONAL OFF- RAMP Eastbound | | | | | Int. Total |
|-------------|------------------------------|------|------|------|------------|-----------|------|------|------|------------|------------------------------|------|------|------|------------|--|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 0 | 285 | 0 | 0 | 285 | 0 | 0 | 0 | 0 | 0 | 0 | 275 | 0 | 0 | 275 | 62 | 0 | 0 | 0 | 62 | 622 |
| 07:15 AM | 0 | 264 | 0 | 0 | 264 | 0 | 0 | 0 | 0 | 0 | 0 | 327 | 0 | 0 | 327 | 81 | 0 | 0 | 0 | 81 | 672 |
| 07:30 AM | 0 | 298 | 0 | 0 | 298 | 0 | 0 | 0 | 0 | 0 | 0 | 341 | 0 | 0 | 341 | 73 | 0 | 0 | 0 | 73 | 712 |
| 07:45 AM | 0 | 417 | 0 | 0 | 417 | 0 | 0 | 0 | 0 | 0 | 0 | 444 | 0 | 0 | 444 | 70 | 0 | 0 | 0 | 70 | 931 |
| Total | 0 | 1264 | 0 | 0 | 1264 | 0 | 0 | 0 | 0 | 0 | 0 | 1387 | 0 | 0 | 1387 | 286 | 0 | 0 | 0 | 286 | 2937 |
| 08:00 AM | 0 | 374 | 0 | 0 | 374 | 0 | 0 | 0 | 0 | 0 | 0 | 467 | 0 | 0 | 467 | 87 | 0 | 0 | 0 | 87 | 928 |
| 08:15 AM | 0 | 386 | 0 | 0 | 386 | 0 | 0 | 0 | 0 | 0 | 0 | 507 | 0 | 0 | 507 | 80 | 0 | 0 | 0 | 80 | 973 |
| 08:30 AM | 0 | 360 | 0 | 0 | 360 | 0 | 0 | 0 | 0 | 0 | 0 | 515 | 0 | 0 | 515 | 76 | 0 | 0 | 0 | 76 | 951 |
| 08:45 AM | 0 | 450 | 0 | 0 | 450 | 0 | 0 | 0 | 0 | 0 | 0 | 464 | 0 | 0 | 464 | 112 | 0 | 0 | 0 | 112 | 1026 |
| Total | 0 | 1570 | 0 | 0 | 1570 | 0 | 0 | 0 | 0 | 0 | 0 | 1953 | 0 | 0 | 1953 | 355 | 0 | 0 | 0 | 355 | 3878 |
| Grand Total | 0 | 2834 | 0 | 0 | 2834 | 0 | 0 | 0 | 0 | 0 | 0 | 3340 | 0 | 0 | 3340 | 641 | 0 | 0 | 0 | 641 | 6815 |
| Apprch % | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 100 | 0 | 0 | | 100 | 0 | 0 | 0 | | |
| Total % | 0 | 41.6 | 0 | 0 | 41.6 | 0 | 0 | 0 | 0 | 0 | 0 | 49 | 0 | 0 | 49 | 9.4 | 0 | 0 | 0 | 9.4 | |

| Start Time | N MATHILDA AVE Southbound | | | | Westbound | | | | N MATHILDA AVE Northbound | | | | SB US-101 DIAGONAL OFF- RAMP Eastbound | | | | Int. Total |
|--|------------------------------|------------|------|------------|-----------|------|------|------------|------------------------------|------------|------|------------|--|------|------|------------|-------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 08:00 AM | | | | | | | | | | | | | | | | | |
| 08:00 AM | 0 | 374 | 0 | 374 | 0 | 0 | 0 | 0 | 0 | 467 | 0 | 467 | 87 | 0 | 0 | 87 | 928 |
| 08:15 AM | 0 | 386 | 0 | 386 | 0 | 0 | 0 | 0 | 0 | 507 | 0 | 507 | 80 | 0 | 0 | 80 | 973 |
| 08:30 AM | 0 | 360 | 0 | 360 | 0 | 0 | 0 | 0 | 0 | 515 | 0 | 515 | 76 | 0 | 0 | 76 | 951 |
| 08:45 AM | 0 | 450 | 0 | 450 | 0 | 0 | 0 | 0 | 0 | 464 | 0 | 464 | 112 | 0 | 0 | 112 | 1026 |
| Total Volume | 0 | 1570 | 0 | 1570 | 0 | 0 | 0 | 0 | 0 | 1953 | 0 | 1953 | 355 | 0 | 0 | 355 | 3878 |
| % App. Total | 0 | 100 | 0 | | 0 | 0 | 0 | | 0 | 100 | 0 | | 100 | 0 | 0 | | |
| PHF | .000 | .872 | .000 | .872 | .000 | .000 | .000 | .000 | .000 | .948 | .000 | .948 | .792 | .000 | .000 | .792 | .945 |

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Traffic Data Service

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 Site Code : 00000005
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Groups Printed- Bikes

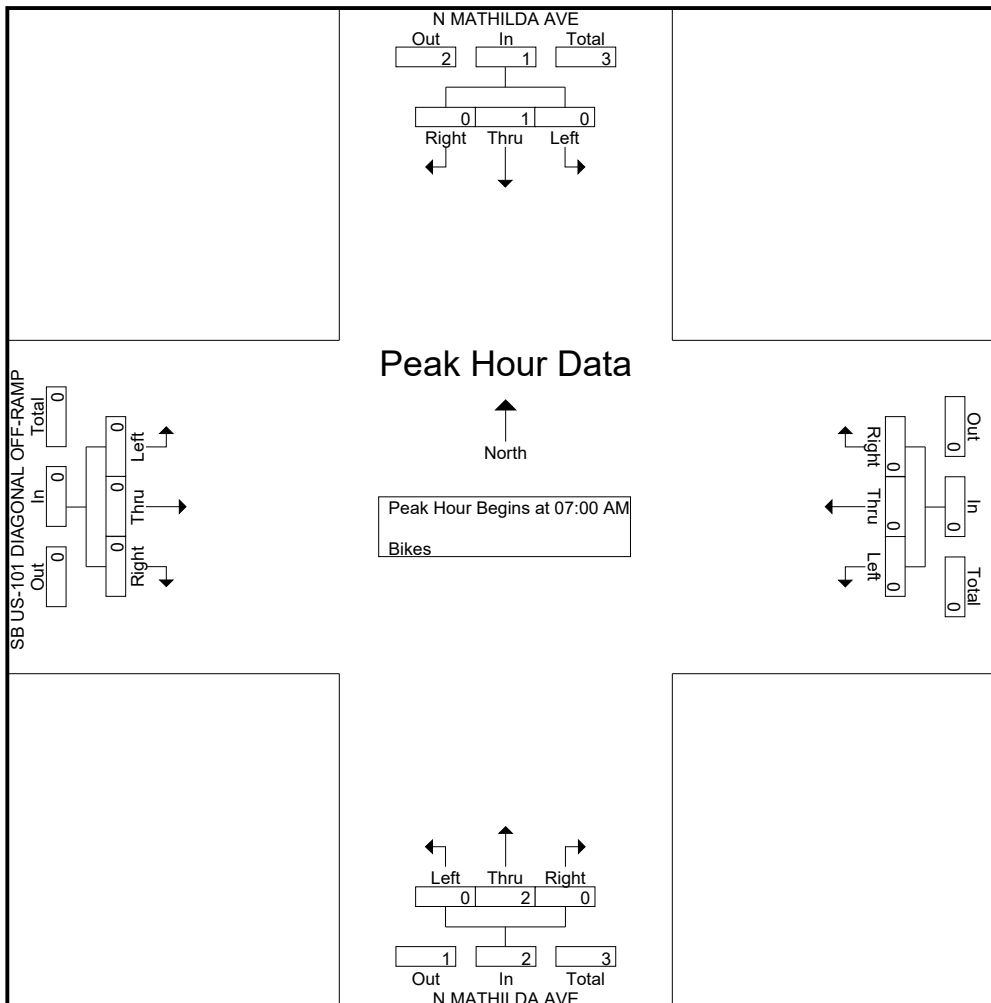
| Start Time | N MATHILDA AVE Southbound | | | | | Westbound | | | | | N MATHILDA AVE Northbound | | | | | SB US-101 DIAGONAL OFF- RAMP Eastbound | | | | | Int. Total |
|-------------|------------------------------|------|------|------|------------|-----------|------|------|------|------------|------------------------------|------|------|------|------------|--|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:15 AM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| Grand Total | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 |
| Apprch % | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | |
| Total % | 0 | 25 | 0 | 0 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 75 | 0 | 0 | 75 | 0 | 0 | 0 | 0 | 0 | |

| Start Time | N MATHILDA AVE Southbound | | | | Westbound | | | | N MATHILDA AVE Northbound | | | | SB US-101 DIAGONAL OFF- RAMP Eastbound | | | | Int. Total |
|--|------------------------------|------|------|------------|-----------|------|------|------------|------------------------------|------|------|------------|--|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 07:00 AM | | | | | | | | | | | | | | | | | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 |
| 07:15 AM | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Volume | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 |
| % App. Total | 0 | 100 | 0 | | 0 | 0 | 0 | | 0 | 100 | 0 | | 0 | 0 | 0 | | |
| PHF | .000 | .250 | .000 | .250 | .000 | .000 | .000 | .000 | .000 | .250 | .000 | .250 | .000 | .000 | .000 | .000 | .375 |

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File Name : 5PM FINAL
Site Code : 00000005
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Groups Printed- Vehicles

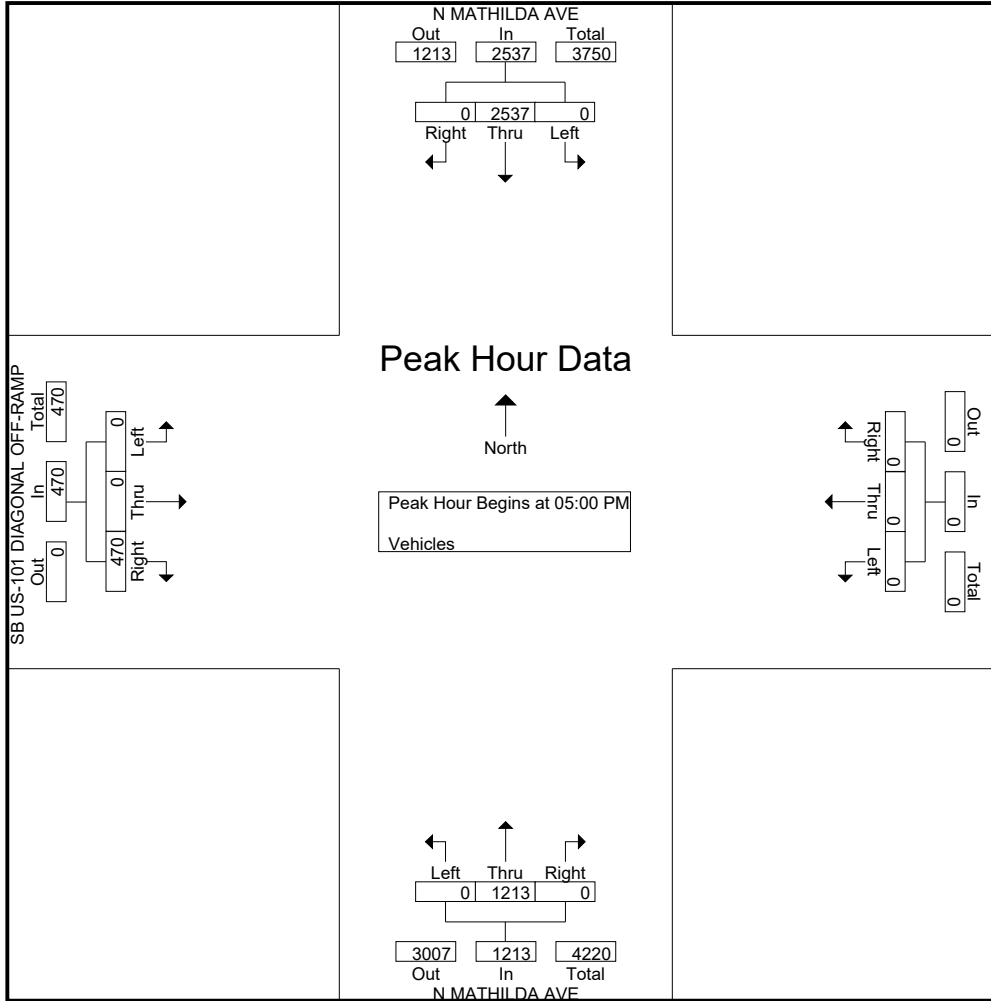
| Start Time | N MATHILDA AVE Southbound | | | | | Westbound | | | | | N MATHILDA AVE Northbound | | | | | SB US-101 DIAGONAL OFF- RAMP Eastbound | | | | | Int. Total |
|--------------------|------------------------------|------|------|------|------------|-----------|------|------|------|------------|------------------------------|------|------|------|------------|--|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:00 PM | 0 | 367 | 0 | 0 | 367 | 0 | 0 | 0 | 0 | 0 | 0 | 299 | 0 | 0 | 299 | 95 | 0 | 0 | 0 | 95 | 761 |
| 04:15 PM | 0 | 390 | 0 | 0 | 390 | 0 | 0 | 0 | 0 | 0 | 0 | 232 | 0 | 0 | 232 | 77 | 0 | 0 | 0 | 77 | 699 |
| 04:30 PM | 0 | 538 | 0 | 0 | 538 | 0 | 0 | 0 | 0 | 0 | 0 | 280 | 0 | 0 | 280 | 139 | 0 | 0 | 0 | 139 | 957 |
| 04:45 PM | 0 | 578 | 0 | 0 | 578 | 0 | 0 | 0 | 0 | 0 | 0 | 292 | 0 | 0 | 292 | 123 | 0 | 0 | 0 | 123 | 993 |
| Total | 0 | 1873 | 0 | 0 | 1873 | 0 | 0 | 0 | 0 | 0 | 0 | 1103 | 0 | 0 | 1103 | 434 | 0 | 0 | 0 | 434 | 3410 |
| 05:00 PM | 0 | 577 | 0 | 0 | 577 | 0 | 0 | 0 | 0 | 0 | 0 | 333 | 0 | 0 | 333 | 127 | 0 | 0 | 0 | 127 | 1037 |
| 05:15 PM | 0 | 700 | 0 | 0 | 700 | 0 | 0 | 0 | 0 | 0 | 0 | 281 | 0 | 0 | 281 | 96 | 0 | 0 | 0 | 96 | 1077 |
| 05:30 PM | 0 | 644 | 0 | 0 | 644 | 0 | 0 | 0 | 0 | 0 | 0 | 300 | 0 | 0 | 300 | 117 | 0 | 0 | 0 | 117 | 1061 |
| 05:45 PM | 0 | 616 | 0 | 0 | 616 | 0 | 0 | 0 | 0 | 0 | 0 | 299 | 0 | 0 | 299 | 130 | 0 | 0 | 0 | 130 | 1045 |
| Total | 0 | 2537 | 0 | 0 | 2537 | 0 | 0 | 0 | 0 | 0 | 0 | 1213 | 0 | 0 | 1213 | 470 | 0 | 0 | 0 | 470 | 4220 |
| 06:00 PM | 0 | 643 | 0 | 0 | 643 | 0 | 0 | 0 | 0 | 0 | 0 | 263 | 0 | 0 | 263 | 104 | 0 | 0 | 0 | 104 | 1010 |
| 06:15 PM | 0 | 627 | 0 | 0 | 627 | 0 | 0 | 0 | 0 | 0 | 0 | 252 | 0 | 0 | 252 | 97 | 0 | 0 | 0 | 97 | 976 |
| 06:30 PM | 0 | 535 | 0 | 0 | 535 | 0 | 0 | 0 | 0 | 0 | 0 | 262 | 0 | 0 | 262 | 111 | 0 | 0 | 0 | 111 | 908 |
| 06:45 PM | 0 | 517 | 0 | 0 | 517 | 0 | 0 | 0 | 0 | 0 | 0 | 248 | 0 | 0 | 248 | 112 | 0 | 0 | 0 | 112 | 877 |
| Total | 0 | 2322 | 0 | 0 | 2322 | 0 | 0 | 0 | 0 | 0 | 0 | 1025 | 0 | 0 | 1025 | 424 | 0 | 0 | 0 | 424 | 3771 |
| Grand Total | 0 | 6732 | 0 | 0 | 6732 | 0 | 0 | 0 | 0 | 0 | 0 | 3341 | 0 | 0 | 3341 | 1328 | 0 | 0 | 0 | 1328 | 11401 |
| Apprch % | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 100 | 0 | 0 | | 100 | 0 | 0 | 0 | | |
| Total % | 0 | 59 | 0 | 0 | 59 | 0 | 0 | 0 | 0 | 0 | 0 | 29.3 | 0 | 0 | 29.3 | 11.6 | 0 | 0 | 0 | 11.6 | |

| Start Time | N MATHILDA AVE Southbound | | | | Westbound | | | | N MATHILDA AVE Northbound | | | | SB US-101 DIAGONAL OFF- RAMP Eastbound | | | | Int. Total |
|--|------------------------------|------------|------|------------|-----------|------|------|------------|------------------------------|------------|------|------------|--|------|------|------------|-------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 04:00 PM to 06:45 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 05:00 PM | | | | | | | | | | | | | | | | | |
| 05:00 PM | 0 | 577 | 0 | 577 | 0 | 0 | 0 | 0 | 0 | 333 | 0 | 333 | 127 | 0 | 0 | 127 | 1037 |
| 05:15 PM | 0 | 700 | 0 | 700 | 0 | 0 | 0 | 0 | 0 | 281 | 0 | 281 | 96 | 0 | 0 | 96 | 1077 |
| 05:30 PM | 0 | 644 | 0 | 644 | 0 | 0 | 0 | 0 | 0 | 300 | 0 | 300 | 117 | 0 | 0 | 117 | 1061 |
| 05:45 PM | 0 | 616 | 0 | 616 | 0 | 0 | 0 | 0 | 0 | 299 | 0 | 299 | 130 | 0 | 0 | 130 | 1045 |
| Total Volume | 0 | 2537 | 0 | 2537 | 0 | 0 | 0 | 0 | 0 | 1213 | 0 | 1213 | 470 | 0 | 0 | 470 | 4220 |
| % App. Total | 0 | 100 | 0 | | 0 | 0 | 0 | | 0 | 100 | 0 | | 100 | 0 | 0 | | |
| PHF | .000 | .906 | .000 | .906 | .000 | .000 | .000 | .000 | .000 | .911 | .000 | .911 | .904 | .000 | .000 | .904 | .980 |

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Groups Printed- Bikes

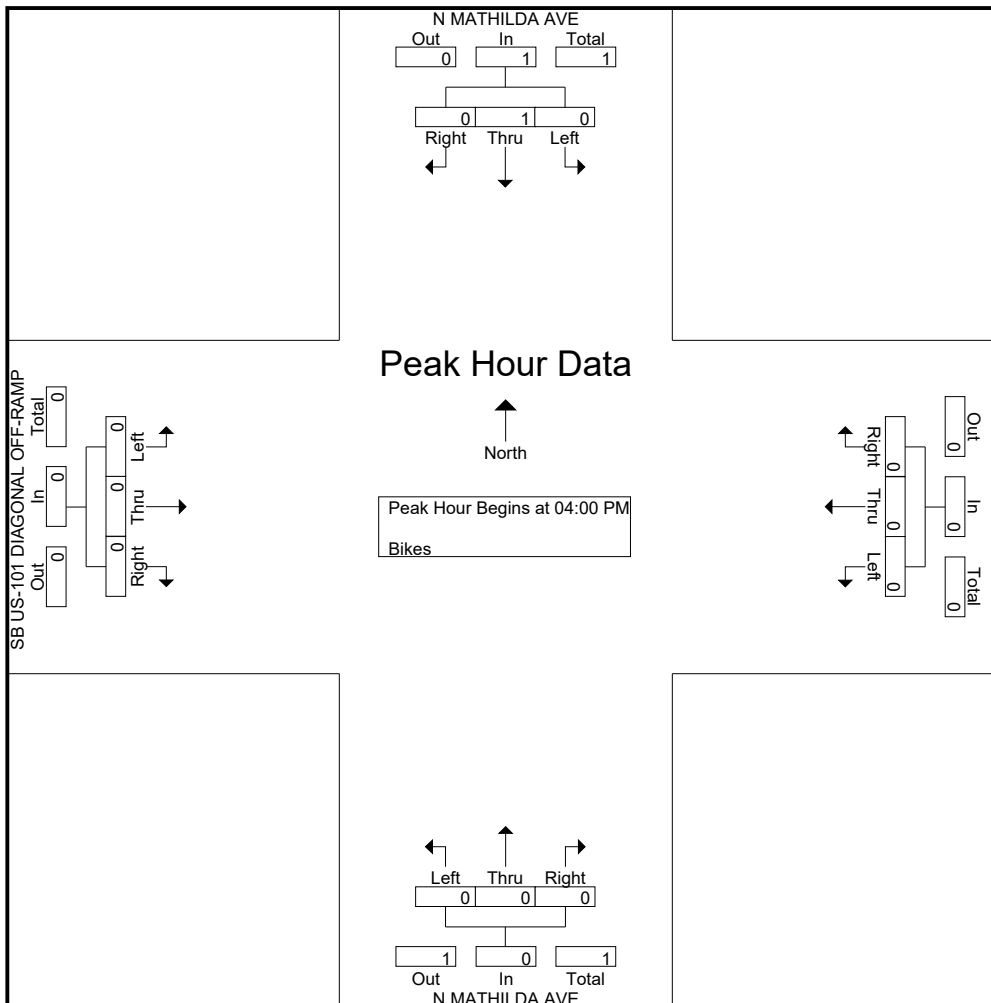
| Start Time | N MATHILDA AVE Southbound | | | | | Westbound | | | | | N MATHILDA AVE Northbound | | | | | SB US-101 DIAGONAL OFF- RAMP Eastbound | | | | | Int. Total |
|--------------------|------------------------------|------|------|------|------------|-----------|------|------|------|------------|------------------------------|------|------|------|------------|--|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:00 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 05:00 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 06:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 06:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 06:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 06:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| Grand Total | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 3 |
| Apprch % | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | |
| Total % | 0 | 66.7 | 0 | 0 | 66.7 | 0 | 0 | 0 | 0 | 0 | 0 | 33.3 | 0 | 0 | 33.3 | 0 | 0 | 0 | 0 | 0 | |

| Start Time | N MATHILDA AVE Southbound | | | | Westbound | | | | N MATHILDA AVE Northbound | | | | SB US-101 DIAGONAL OFF- RAMP Eastbound | | | | Int. Total |
|--|------------------------------|------|------|------------|-----------|------|------|------------|------------------------------|------|------|------------|--|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 04:00 PM to 06:45 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 04:00 PM | | | | | | | | | | | | | | | | | |
| 04:00 PM | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Volume | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| % App. Total | 0 | 100 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | |
| PHF | .000 | .250 | .000 | .250 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .250 |

Traffic Data Service

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Traffic Data Service

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File Name : 9AM FINAL
 Site Code : 00000009
 Start Date : 2/13/2013
 Page No : 1

Groups Printed- Vehicles

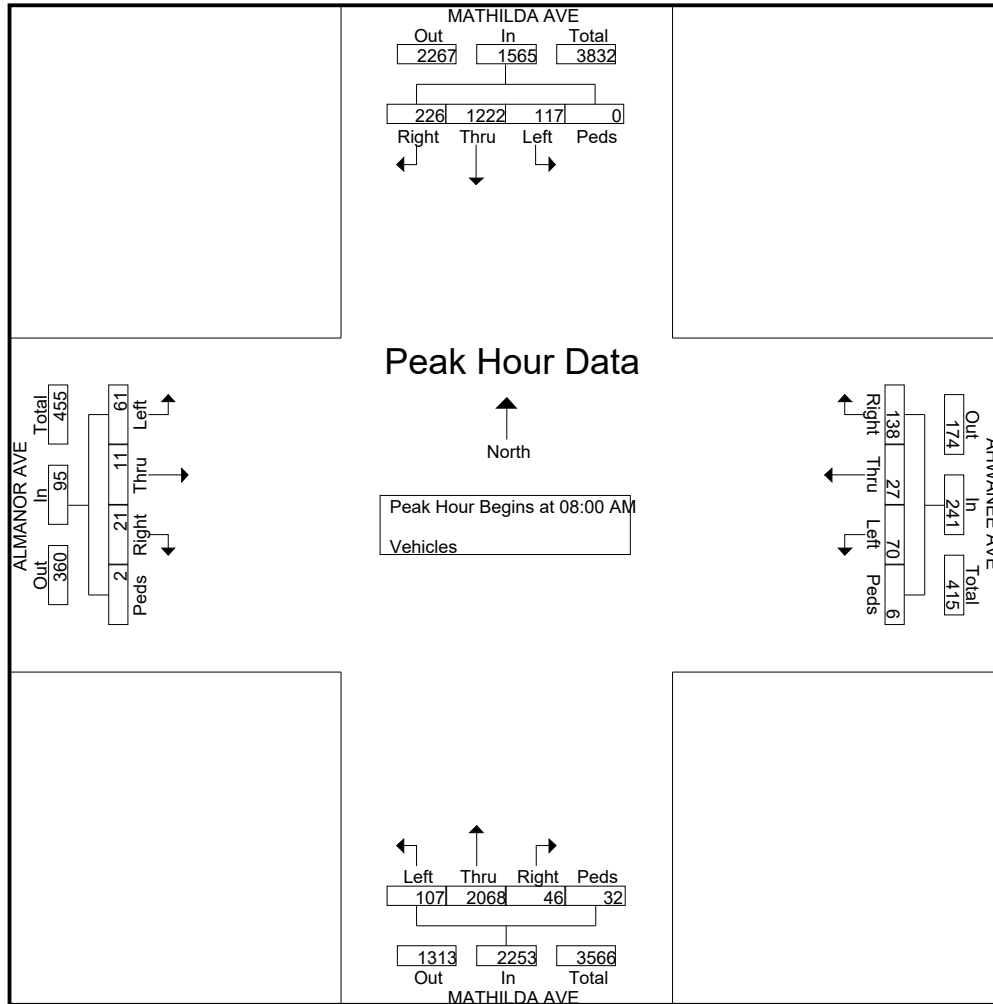
| Start Time | MATHILDA AVE Southbound | | | | | AHWANEE AVE Westbound | | | | | MATHILDA AVE Northbound | | | | | ALMANOR AVE Eastbound | | | | | Int. Total |
|-------------|----------------------------|------|------|------|------------|--------------------------|------|------|------|------------|----------------------------|------|------|------|------------|--------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 26 | 203 | 33 | 0 | 262 | 34 | 4 | 12 | 0 | 50 | 10 | 221 | 12 | 4 | 247 | 5 | 2 | 11 | 0 | 18 | 577 |
| 07:15 AM | 26 | 263 | 30 | 0 | 319 | 18 | 3 | 16 | 1 | 38 | 11 | 325 | 6 | 0 | 342 | 3 | 2 | 10 | 0 | 15 | 714 |
| 07:30 AM | 31 | 265 | 37 | 0 | 333 | 44 | 4 | 14 | 1 | 63 | 13 | 371 | 10 | 2 | 396 | 4 | 0 | 13 | 0 | 17 | 809 |
| 07:45 AM | 53 | 331 | 40 | 0 | 424 | 49 | 3 | 19 | 1 | 72 | 12 | 346 | 13 | 2 | 373 | 4 | 2 | 19 | 0 | 25 | 894 |
| Total | 136 | 1062 | 140 | 0 | 1338 | 145 | 14 | 61 | 3 | 223 | 46 | 1263 | 41 | 8 | 1358 | 16 | 6 | 53 | 0 | 75 | 2994 |
| 08:00 AM | 43 | 305 | 17 | 0 | 365 | 30 | 6 | 17 | 2 | 55 | 14 | 468 | 25 | 5 | 512 | 5 | 3 | 20 | 0 | 28 | 960 |
| 08:15 AM | 45 | 264 | 29 | 0 | 338 | 24 | 9 | 18 | 1 | 52 | 8 | 518 | 22 | 4 | 552 | 5 | 5 | 18 | 0 | 28 | 970 |
| 08:30 AM | 74 | 276 | 33 | 0 | 383 | 45 | 8 | 18 | 3 | 74 | 13 | 579 | 31 | 5 | 628 | 7 | 2 | 12 | 1 | 22 | 1107 |
| 08:45 AM | 64 | 377 | 38 | 0 | 479 | 39 | 4 | 17 | 0 | 60 | 11 | 503 | 29 | 18 | 561 | 4 | 1 | 11 | 1 | 17 | 1117 |
| Total | 226 | 1222 | 117 | 0 | 1565 | 138 | 27 | 70 | 6 | 241 | 46 | 2068 | 107 | 32 | 2253 | 21 | 11 | 61 | 2 | 95 | 4154 |
| Grand Total | 362 | 2284 | 257 | 0 | 2903 | 283 | 41 | 131 | 9 | 464 | 92 | 3331 | 148 | 40 | 3611 | 37 | 17 | 114 | 2 | 170 | 7148 |
| Apprch % | 12.5 | 78.7 | 8.9 | 0 | | 61 | 8.8 | 28.2 | 1.9 | | 2.5 | 92.2 | 4.1 | 1.1 | | 21.8 | 10 | 67.1 | 1.2 | | |
| Total % | 5.1 | 32 | 3.6 | 0 | 40.6 | 4 | 0.6 | 1.8 | 0.1 | 6.5 | 1.3 | 46.6 | 2.1 | 0.6 | 50.5 | 0.5 | 0.2 | 1.6 | 0 | 2.4 | |

| Start Time | MATHILDA AVE Southbound | | | | | AHWANEE AVE Westbound | | | | | MATHILDA AVE Northbound | | | | | ALMANOR AVE Eastbound | | | | | Int. Total |
|--|----------------------------|------------|-----------|------|------------|--------------------------|----------|-----------|----------|------------|----------------------------|------------|-----------|-----------|------------|--------------------------|----------|-----------|----------|------------|-------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 08:00 AM | | | | | | | | | | | | | | | | | | | | | |
| 08:00 AM | 43 | 305 | 17 | 0 | 365 | 30 | 6 | 17 | 2 | 55 | 14 | 468 | 25 | 5 | 512 | 5 | 3 | 20 | 0 | 28 | 960 |
| 08:15 AM | 45 | 264 | 29 | 0 | 338 | 24 | 9 | 18 | 1 | 52 | 8 | 518 | 22 | 4 | 552 | 5 | 5 | 18 | 0 | 28 | 970 |
| 08:30 AM | 74 | 276 | 33 | 0 | 383 | 45 | 8 | 18 | 3 | 74 | 13 | 579 | 31 | 5 | 628 | 7 | 2 | 12 | 1 | 22 | 1107 |
| 08:45 AM | 64 | 377 | 38 | 0 | 479 | 39 | 4 | 17 | 0 | 60 | 11 | 503 | 29 | 18 | 561 | 4 | 1 | 11 | 1 | 17 | 1117 |
| Total Volume | 226 | 1222 | 117 | 0 | 1565 | 138 | 27 | 70 | 6 | 241 | 46 | 2068 | 107 | 32 | 2253 | 21 | 11 | 61 | 2 | 95 | 4154 |
| % App. Total | 14.4 | 78.1 | 7.5 | 0 | | 57.3 | 11.2 | 29 | 2.5 | | 2 | 91.8 | 4.7 | 1.4 | | 22.1 | 11.6 | 64.2 | 2.1 | | |
| PHF | .764 | .810 | .770 | .000 | .817 | .767 | .750 | .972 | .500 | .814 | .821 | .893 | .863 | .444 | .897 | .750 | .550 | .763 | .500 | .848 | .930 |

Traffic Data Service

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Traffic Data Service

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 tdsbay@cs.com

File Name : 9AM FINAL
 Site Code : 00000009
 Start Date : 2/13/2013
 Page No : 1

Groups Printed- Bikes

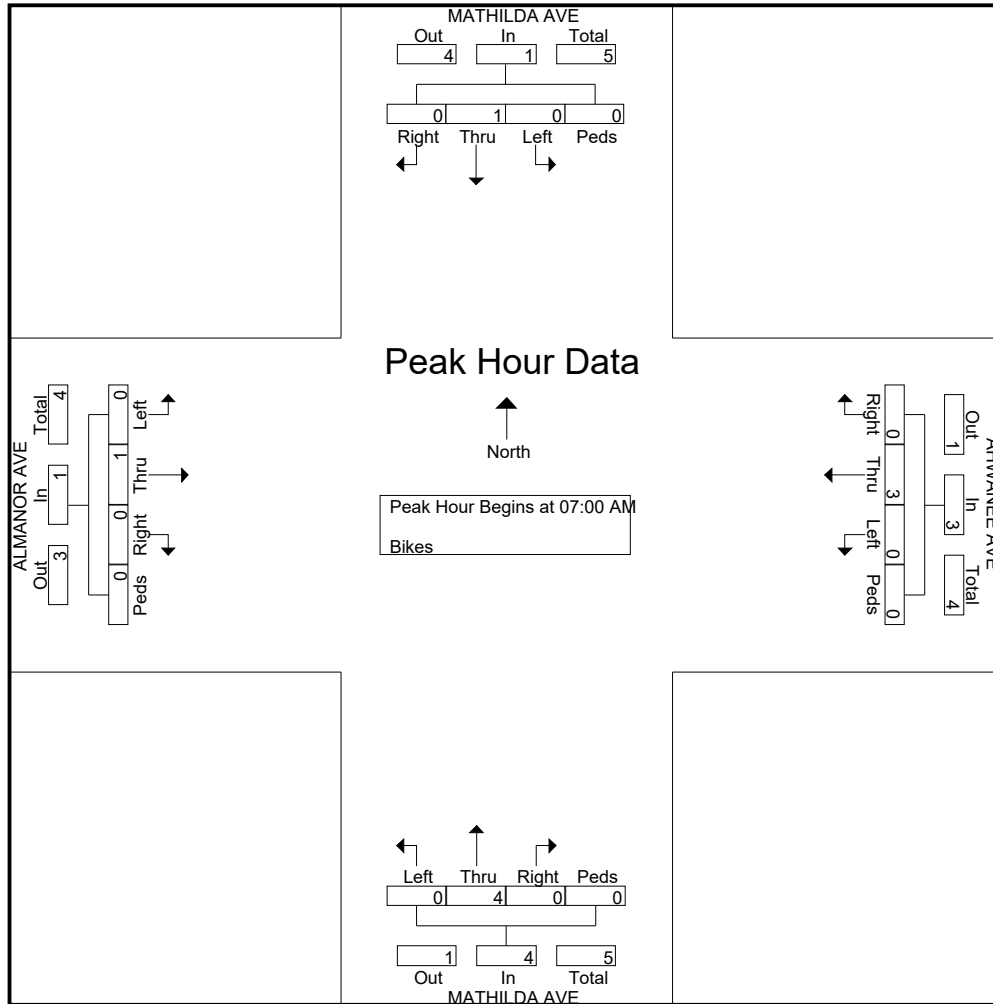
| Start Time | MATHILDA AVE Southbound | | | | | AHWANEE AVE Westbound | | | | | MATHILDA AVE Northbound | | | | | ALMANOR AVE Eastbound | | | | | Int. Total |
|--------------------|----------------------------|------|------|------|------------|--------------------------|------|------|------|------------|----------------------------|------|------|------|------------|--------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:30 AM | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 1 |
| Total | 0 | 1 | 0 | 0 | 1 | 0 | 3 | 0 | 0 | 3 | 0 | 4 | 0 | 0 | 4 | 0 | 1 | 0 | 0 | 1 | 9 |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 3 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 4 |
| Grand Total | 0 | 1 | 0 | 0 | 1 | 0 | 4 | 0 | 0 | 4 | 0 | 7 | 0 | 0 | 7 | 0 | 1 | 0 | 0 | 1 | 13 |
| Apprch % | 0 | 100 | 0 | 0 | | 0 | 100 | 0 | 0 | | 0 | 100 | 0 | 0 | | 0 | 100 | 0 | 0 | | |
| Total % | 0 | 7.7 | 0 | 0 | 7.7 | 0 | 30.8 | 0 | 0 | 30.8 | 0 | 53.8 | 0 | 0 | 53.8 | 0 | 7.7 | 0 | 0 | 7.7 | |

| Start Time | MATHILDA AVE Southbound | | | | | AHWANEE AVE Westbound | | | | | MATHILDA AVE Northbound | | | | | ALMANOR AVE Eastbound | | | | | Int. Total |
|--|----------------------------|------|------|------|------------|--------------------------|------|------|------|------------|----------------------------|------|------|------|------------|--------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 07:00 AM | | | | | | | | | | | | | | | | | | | | | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:30 AM | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 1 |
| Total Volume | 0 | 1 | 0 | 0 | 1 | 0 | 3 | 0 | 0 | 3 | 0 | 4 | 0 | 0 | 4 | 0 | 1 | 0 | 0 | 1 | 9 |
| % App. Total | 0 | 100 | 0 | 0 | | 0 | 100 | 0 | 0 | | 0 | 100 | 0 | 0 | | 0 | 100 | 0 | 0 | | |
| PHF | .000 | .250 | .000 | .000 | .250 | .000 | .375 | .000 | .000 | .375 | .000 | .500 | .000 | .000 | .500 | .000 | .250 | .000 | .000 | .250 | .563 |

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 Site Code : 00000009
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Groups Printed- Vehicles

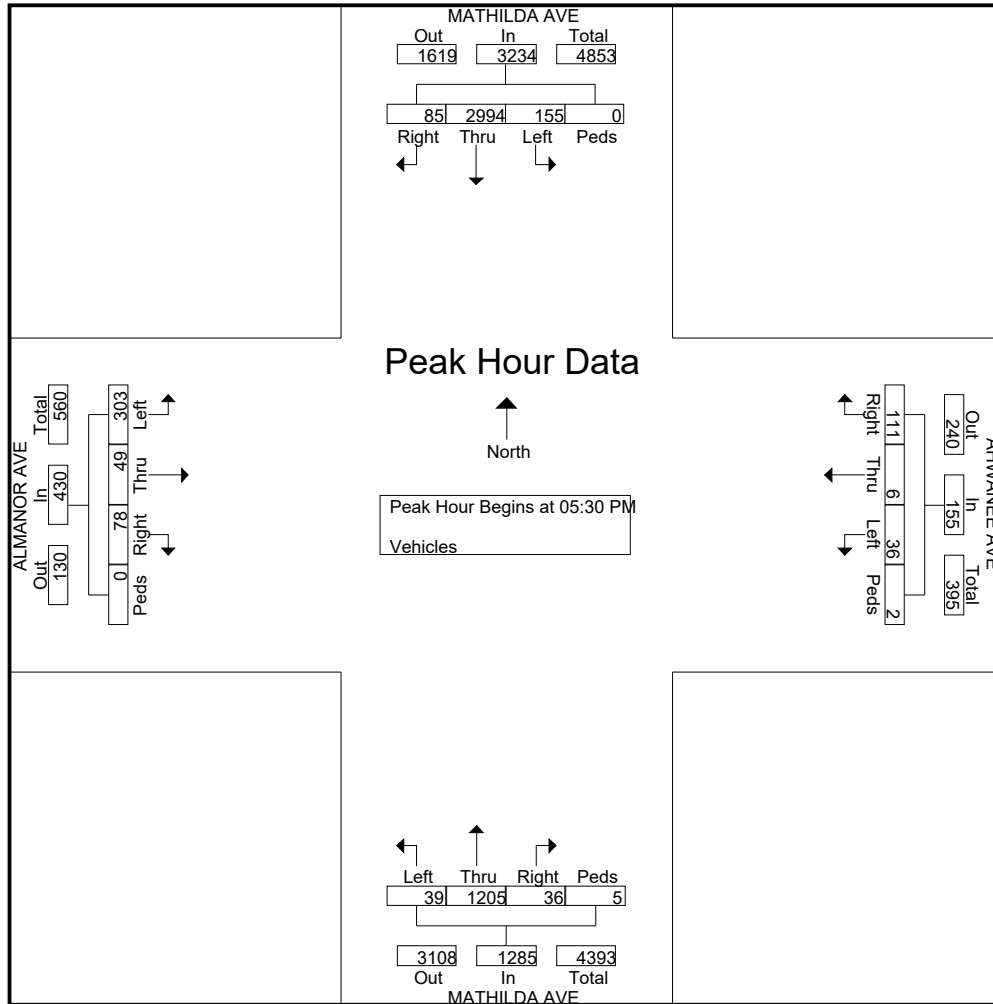
| Start Time | MATHILDA AVE Southbound | | | | | AHWANEE AVE Westbound | | | | | MATHILDA AVE Northbound | | | | | ALMANOR AVE Eastbound | | | | | Int. Total |
|-------------|----------------------------|------|------|------|------------|--------------------------|------|------|------|------------|----------------------------|------|------|------|------------|--------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:30 PM | 11 | 455 | 19 | 0 | 485 | 21 | 1 | 8 | 0 | 30 | 3 | 273 | 9 | 0 | 285 | 12 | 10 | 44 | 0 | 66 | 866 |
| 04:45 PM | 10 | 461 | 46 | 0 | 517 | 34 | 2 | 12 | 0 | 48 | 8 | 221 | 11 | 4 | 244 | 15 | 5 | 57 | 0 | 77 | 886 |
| Total | 21 | 916 | 65 | 0 | 1002 | 55 | 3 | 20 | 0 | 78 | 11 | 494 | 20 | 4 | 529 | 27 | 15 | 101 | 0 | 143 | 1752 |
| 05:00 PM | 14 | 541 | 25 | 0 | 580 | 48 | 1 | 11 | 0 | 60 | 11 | 278 | 11 | 2 | 302 | 15 | 7 | 64 | 0 | 86 | 1028 |
| 05:15 PM | 16 | 633 | 53 | 0 | 702 | 43 | 2 | 11 | 0 | 56 | 8 | 282 | 14 | 3 | 307 | 16 | 2 | 58 | 0 | 76 | 1141 |
| 05:30 PM | 15 | 786 | 37 | 0 | 838 | 32 | 0 | 4 | 1 | 37 | 7 | 264 | 17 | 1 | 289 | 12 | 7 | 53 | 0 | 72 | 1236 |
| 05:45 PM | 12 | 805 | 36 | 0 | 853 | 31 | 2 | 15 | 0 | 48 | 10 | 308 | 14 | 4 | 336 | 21 | 7 | 79 | 0 | 107 | 1344 |
| Total | 57 | 2765 | 151 | 0 | 2973 | 154 | 5 | 41 | 1 | 201 | 36 | 1132 | 56 | 10 | 1234 | 64 | 23 | 254 | 0 | 341 | 4749 |
| 06:00 PM | 31 | 745 | 35 | 0 | 811 | 26 | 2 | 9 | 0 | 37 | 13 | 336 | 1 | 0 | 350 | 14 | 16 | 77 | 0 | 107 | 1305 |
| 06:15 PM | 27 | 658 | 47 | 0 | 732 | 22 | 2 | 8 | 1 | 33 | 6 | 297 | 7 | 0 | 310 | 31 | 19 | 94 | 0 | 144 | 1219 |
| Grand Total | 136 | 5084 | 298 | 0 | 5518 | 257 | 12 | 78 | 2 | 349 | 66 | 2259 | 84 | 14 | 2423 | 136 | 73 | 526 | 0 | 735 | 9025 |
| Apprch % | 2.5 | 92.1 | 5.4 | 0 | | 73.6 | 3.4 | 22.3 | 0.6 | | 2.7 | 93.2 | 3.5 | 0.6 | | 18.5 | 9.9 | 71.6 | 0 | | |
| Total % | 1.5 | 56.3 | 3.3 | 0 | 61.1 | 2.8 | 0.1 | 0.9 | 0 | 3.9 | 0.7 | 25 | 0.9 | 0.2 | 26.8 | 1.5 | 0.8 | 5.8 | 0 | 8.1 | |

| Start Time | MATHILDA AVE Southbound | | | | | AHWANEE AVE Westbound | | | | | MATHILDA AVE Northbound | | | | | ALMANOR AVE Eastbound | | | | | Int. Total |
|--|----------------------------|------------|-----------|------|------------|--------------------------|----------|-----------|----------|------------|----------------------------|------------|-----------|----------|------------|--------------------------|-----------|-----------|------|------------|-------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| Peak Hour Analysis From 04:30 PM to 06:15 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 05:30 PM | | | | | | | | | | | | | | | | | | | | | |
| 05:30 PM | 15 | 786 | 37 | 0 | 838 | 32 | 0 | 4 | 1 | 37 | 7 | 264 | 17 | 1 | 289 | 12 | 7 | 53 | 0 | 72 | 1236 |
| 05:45 PM | 12 | 805 | 36 | 0 | 853 | 31 | 2 | 15 | 0 | 48 | 10 | 308 | 14 | 4 | 336 | 21 | 7 | 79 | 0 | 107 | 1344 |
| 06:00 PM | 31 | 745 | 35 | 0 | 811 | 26 | 2 | 9 | 0 | 37 | 13 | 336 | 1 | 0 | 350 | 14 | 16 | 77 | 0 | 107 | 1305 |
| 06:15 PM | 27 | 658 | 47 | 0 | 732 | 22 | 2 | 8 | 1 | 33 | 6 | 297 | 7 | 0 | 310 | 31 | 19 | 94 | 0 | 144 | 1219 |
| Total Volume | 85 | 2994 | 155 | 0 | 3234 | 111 | 6 | 36 | 2 | 155 | 36 | 1205 | 39 | 5 | 1285 | 78 | 49 | 303 | 0 | 430 | 5104 |
| % App. Total | 2.6 | 92.6 | 4.8 | 0 | | 71.6 | 3.9 | 23.2 | 1.3 | | 2.8 | 93.8 | 3 | 0.4 | | 18.1 | 11.4 | 70.5 | 0 | | |
| PHF | .685 | .930 | .824 | .000 | .948 | .867 | .750 | .600 | .500 | .807 | .692 | .897 | .574 | .313 | .918 | .629 | .645 | .806 | .000 | .747 | .949 |

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 tdsbay@cs.com

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 Site Code : 00000009
 Start Date : 2/13/2013
 Page No : 1

Groups Printed- Bikes

| Start Time | MATHILDA AVE Southbound | | | | | AHWANEЕ AVE Westbound | | | | | MATHILDA AVE Northbound | | | | | ALMANOR AVE Eastbound | | | | | Int. Total |
|-------------|-------------------------|------|------|------|------------|-----------------------|------|------|------|------------|-------------------------|------|------|------|------------|-----------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:45 PM | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:00 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:15 PM | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 3 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 |
| Total | 0 | 2 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 5 |
| 06:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 |
| 06:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Grand Total | 0 | 3 | 0 | 0 | 3 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 8 |
| Apprch % | 0 | 100 | 0 | 0 | | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 100 | 0 | 0 | | |
| Total % | 0 | 37.5 | 0 | 0 | 37.5 | 0 | 25 | 0 | 0 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 37.5 | 0 | 0 | 37.5 | |

| Start Time | MATHILDA AVE Southbound | | | | | AHWANEЕ AVE Westbound | | | | | MATHILDA AVE Northbound | | | | | ALMANOR AVE Eastbound | | | | | Int. Total |
|--|-------------------------|------|------|------|------------|-----------------------|------|------|------|------------|-------------------------|------|------|------|------------|-----------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| Peak Hour Analysis From 04:30 PM to 06:15 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 04:30 PM | | | | | | | | | | | | | | | | | | | | | |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:45 PM | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 05:00 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 05:15 PM | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 3 |
| Total Volume | 0 | 3 | 0 | 0 | 3 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 6 |
| % App. Total | 0 | 100 | 0 | 0 | | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 100 | 0 | 0 | | |
| PHF | .000 | .750 | .000 | .000 | .750 | .000 | .500 | .000 | .000 | .500 | .000 | .000 | .000 | .000 | .000 | .000 | .250 | .000 | .000 | .250 | .500 |

Traffic Data Service

Campbell, CA

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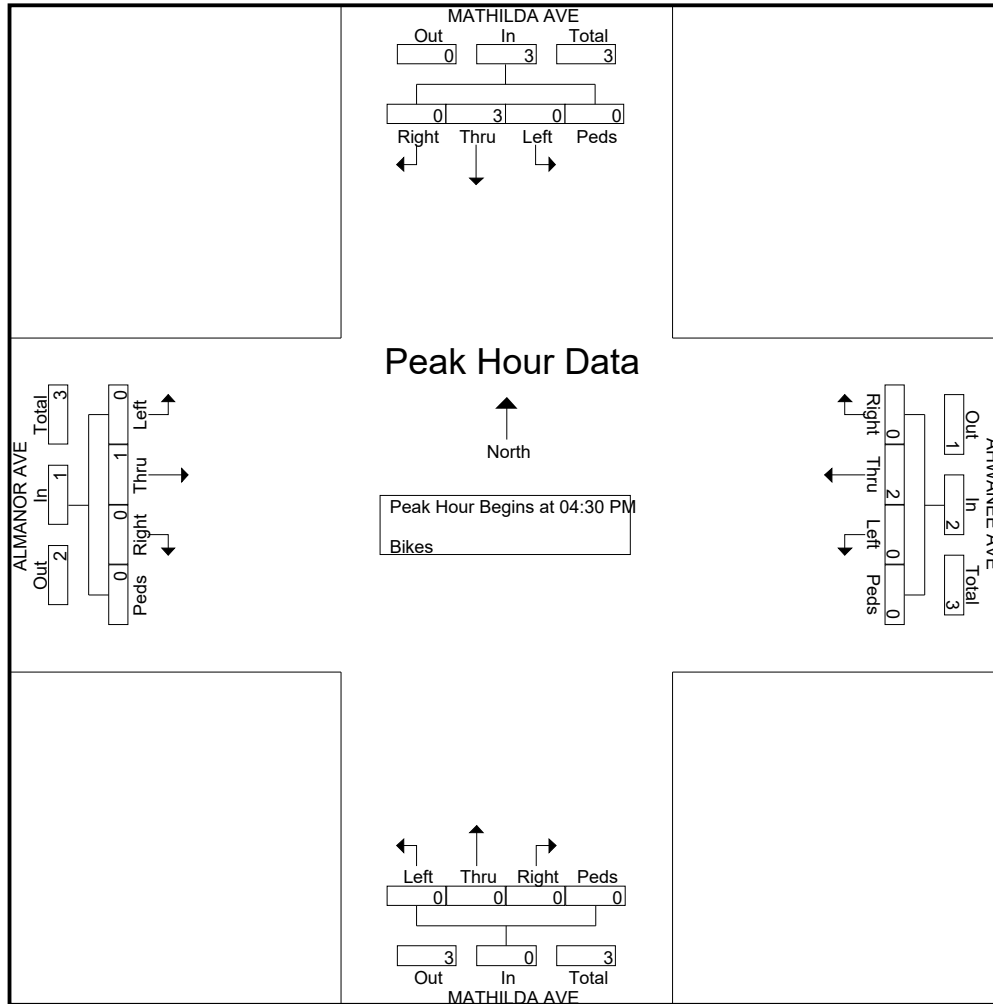
idsbay@cs.com

File Name : 9PM FINAL

Site Code : 00000009

Start Date : 2/13/2013

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Traffic Data Service

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Groups Printed- Vehicles

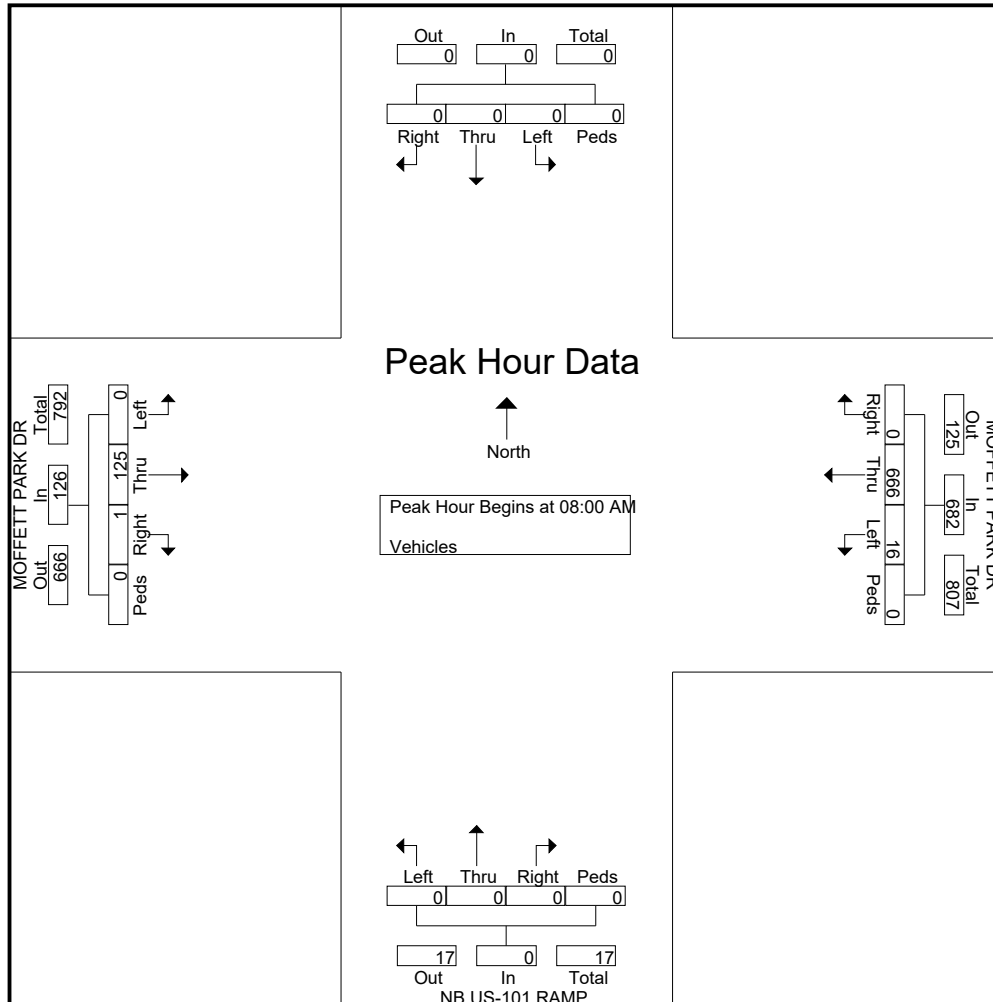
| Start Time | Southbound | | | | | MOFFETT PARK DR Westbound | | | | | NB US-101 RAMP Northbound | | | | | MOFFETT PARK DR Eastbound | | | | | Int. Total |
|-------------|------------|------|------|------|------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 83 | 0 | 0 | 83 | 0 | 0 | 0 | 0 | 0 | 1 | 18 | 0 | 0 | 19 | 102 |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 88 | 1 | 0 | 89 | 0 | 0 | 0 | 0 | 0 | 3 | 12 | 0 | 0 | 15 | 104 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 157 | 2 | 0 | 159 | 0 | 0 | 0 | 0 | 0 | 1 | 19 | 0 | 0 | 20 | 179 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 172 | 0 | 0 | 172 | 0 | 0 | 0 | 0 | 0 | 0 | 32 | 0 | 0 | 32 | 204 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 500 | 3 | 0 | 503 | 0 | 0 | 0 | 0 | 0 | 5 | 81 | 0 | 0 | 86 | 589 |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 158 | 4 | 0 | 162 | 0 | 0 | 0 | 0 | 0 | 1 | 29 | 0 | 0 | 30 | 192 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 167 | 4 | 0 | 171 | 0 | 0 | 0 | 0 | 0 | 0 | 18 | 0 | 0 | 18 | 189 |
| 08:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 147 | 5 | 0 | 152 | 0 | 0 | 0 | 0 | 0 | 0 | 44 | 0 | 0 | 44 | 196 |
| 08:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 194 | 3 | 0 | 197 | 0 | 0 | 0 | 0 | 0 | 0 | 34 | 0 | 0 | 34 | 231 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 666 | 16 | 0 | 682 | 0 | 0 | 0 | 0 | 0 | 1 | 125 | 0 | 0 | 126 | 808 |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 0 | 1166 | 19 | 0 | 1185 | 0 | 0 | 0 | 0 | 0 | 6 | 206 | 0 | 0 | 212 | 1397 |
| Apprch % | 0 | 0 | 0 | 0 | 0 | 0 | 98.4 | 1.6 | 0 | | 0 | 0 | 0 | 0 | | 2.8 | 97.2 | 0 | 0 | | |
| Total % | 0 | 0 | 0 | 0 | 0 | 0 | 83.5 | 1.4 | 0 | 84.8 | 0 | 0 | 0 | 0 | 0 | 0.4 | 14.7 | 0 | 0 | 15.2 | |

| Start Time | Southbound | | | | | MOFFETT PARK DR Westbound | | | | | NB US-101 RAMP Northbound | | | | | MOFFETT PARK DR Eastbound | | | | | Int. Total |
|--|------------|------|------|------|------------|------------------------------|------------|----------|------|------------|------------------------------|------|------|------|------------|------------------------------|-----------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 08:00 AM | | | | | | | | | | | | | | | | | | | | | |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 158 | 4 | 0 | 162 | 0 | 0 | 0 | 0 | 0 | 1 | 29 | 0 | 0 | 30 | 192 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 167 | 4 | 0 | 171 | 0 | 0 | 0 | 0 | 0 | 0 | 18 | 0 | 0 | 18 | 189 |
| 08:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 147 | 5 | 0 | 152 | 0 | 0 | 0 | 0 | 0 | 0 | 44 | 0 | 0 | 44 | 196 |
| 08:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 194 | 3 | 0 | 197 | 0 | 0 | 0 | 0 | 0 | 0 | 34 | 0 | 0 | 34 | 231 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 0 | 666 | 16 | 0 | 682 | 0 | 0 | 0 | 0 | 0 | 1 | 125 | 0 | 0 | 126 | 808 |
| % App. Total | 0 | 0 | 0 | 0 | 0 | 0 | 97.7 | 2.3 | 0 | | 0 | 0 | 0 | 0 | | 0.8 | 99.2 | 0 | 0 | | |
| PHF | .000 | .000 | .000 | .000 | .000 | .000 | .858 | .800 | .000 | .865 | .000 | .000 | .000 | .000 | .000 | .250 | .710 | .000 | .000 | .716 | .874 |

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 Site Code : 00000001
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Groups Printed- Bikes

| Start Time | Southbound | | | | | MOFFETT PARK DR Westbound | | | | | NB US-101 RAMP Northbound | | | | | MOFFETT PARK DR Eastbound | | | | | Int. Total |
|--------------------|------------|------|------|------|------------|---------------------------|------|------|------|------------|---------------------------|------|------|------|------------|---------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 2 |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 6 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 5 | 10 |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 5 | 5 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 3 |
| 08:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 8 | 10 |
| 08:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 3 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 17 | 0 | 0 | 17 | 21 |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 22 | 0 | 0 | 22 | 31 |
| Apprch % | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 0 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 0 | 100 | |
| Total % | 0 | 0 | 0 | 0 | 0 | 0 | 29 | 0 | 0 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 71 | 0 | 0 | 71 | |

| Start Time | Southbound | | | | | MOFFETT PARK DR Westbound | | | | | NB US-101 RAMP Northbound | | | | | MOFFETT PARK DR Eastbound | | | | | Int. Total |
|---------------------|------------|------|------|------|------------|---------------------------|----------|------|------|------------|---------------------------|------|------|------|------------|---------------------------|----------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 6 |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 5 | 5 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 3 |
| 08:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 8 | 10 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 17 | 0 | 0 | 17 | 24 |
| % App. Total | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 0 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 0 | 100 | |
| PHF | .000 | .000 | .000 | .000 | .000 | .000 | .438 | .000 | .000 | .438 | .000 | .000 | .000 | .000 | .000 | .000 | .531 | .000 | .000 | .531 | .600 |

Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1

Peak Hour for Entire Intersection Begins at 07:45 AM

Traffic Data Service

Campbell, CA

(408) 377-2988

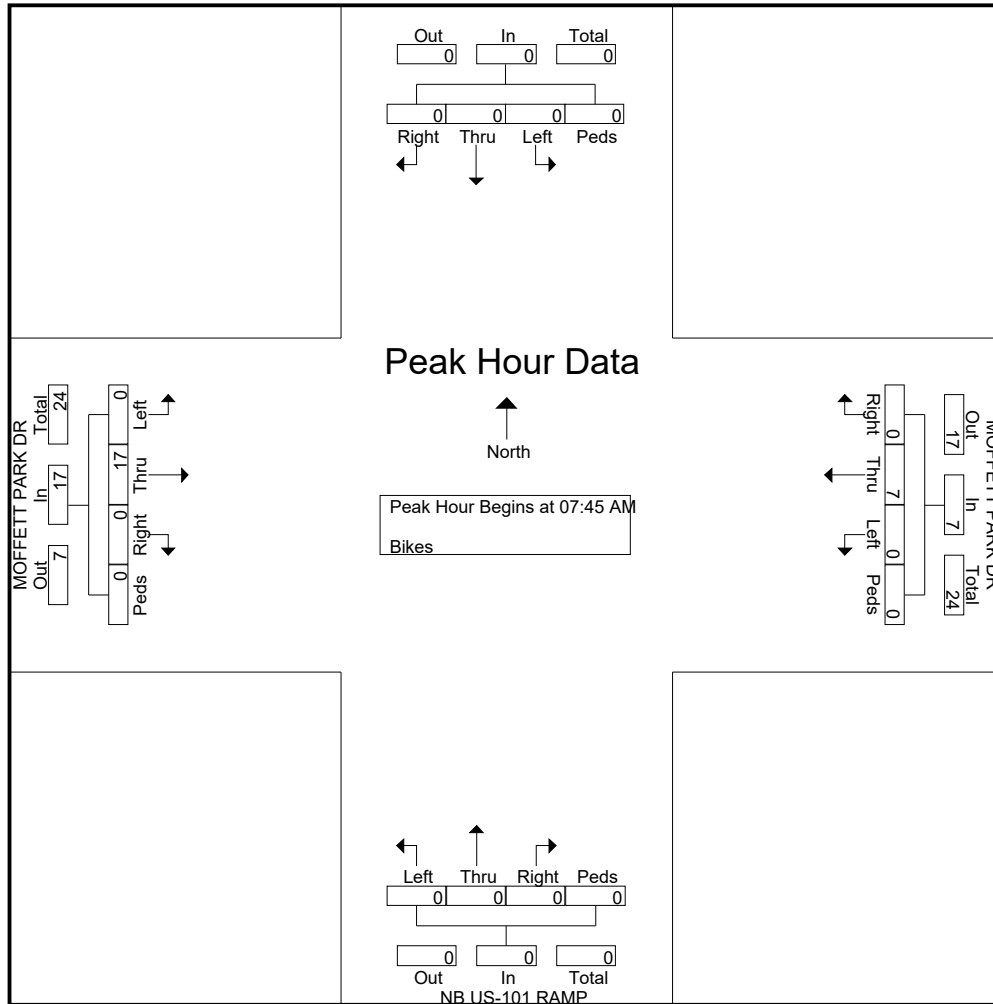
idsbay@cs.com

File Name : 1AM FINAL

Site Code : 00000001

Start Date : 2/12/2013

Page No : 2



Traffic Data Service

Campbell, CA
 (408) 377-2988
 tdsbay@cs.com

File Name : 1PM FINAL
 Site Code : 00000001
 Start Date : 2/12/2013
 Page No : 1

Groups Printed- Vehicles

| Start Time | Southbound | | | | | MOFFETT PARK DR Westbound | | | | | NB US-101 RAMP Northbound | | | | | MOFFETT PARK DR Eastbound | | | | | Int. Total |
|-------------|------------|------|------|------|------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 34 | 35 | 0 | 69 | 0 | 0 | 0 | 0 | 0 | 21 | 116 | 0 | 0 | 137 | 206 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 29 | 44 | 0 | 73 | 0 | 0 | 0 | 0 | 0 | 27 | 124 | 0 | 0 | 151 | 224 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 63 | 79 | 0 | 142 | 0 | 0 | 0 | 0 | 0 | 48 | 240 | 0 | 0 | 288 | 430 |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 53 | 42 | 0 | 95 | 0 | 0 | 0 | 0 | 0 | 24 | 146 | 0 | 0 | 170 | 265 |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 51 | 66 | 0 | 117 | 0 | 0 | 0 | 0 | 0 | 21 | 122 | 0 | 0 | 143 | 260 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 56 | 57 | 0 | 113 | 0 | 0 | 0 | 0 | 0 | 15 | 115 | 0 | 0 | 130 | 243 |
| 05:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 66 | 40 | 0 | 106 | 0 | 0 | 0 | 0 | 0 | 17 | 85 | 0 | 0 | 102 | 208 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 226 | 205 | 0 | 431 | 0 | 0 | 0 | 0 | 0 | 77 | 468 | 0 | 0 | 545 | 976 |
| 06:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 56 | 49 | 0 | 105 | 0 | 0 | 0 | 0 | 0 | 17 | 101 | 0 | 0 | 118 | 223 |
| 06:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 61 | 37 | 0 | 98 | 0 | 0 | 0 | 0 | 0 | 5 | 89 | 0 | 0 | 94 | 192 |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 0 | 406 | 370 | 0 | 776 | 0 | 0 | 0 | 0 | 0 | 147 | 898 | 0 | 0 | 1045 | 1821 |
| Apprch % | 0 | 0 | 0 | 0 | 0 | 0 | 52.3 | 47.7 | 0 | | 0 | 0 | 0 | 0 | 0 | 14.1 | 85.9 | 0 | 0 | | |
| Total % | 0 | 0 | 0 | 0 | 0 | 0 | 22.3 | 20.3 | 0 | 42.6 | 0 | 0 | 0 | 0 | 0 | 8.1 | 49.3 | 0 | 0 | 57.4 | |

| Start Time | Southbound | | | | | MOFFETT PARK DR Westbound | | | | | NB US-101 RAMP Northbound | | | | | MOFFETT PARK DR Eastbound | | | | | Int. Total |
|--------------|------------|------|------|------|------------|------------------------------|-----------|-----------|------|------------|------------------------------|------|------|------|------------|------------------------------|------------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 29 | 44 | 0 | 73 | 0 | 0 | 0 | 0 | 0 | 27 | 124 | 0 | 0 | 151 | 224 |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 53 | 42 | 0 | 95 | 0 | 0 | 0 | 0 | 0 | 24 | 146 | 0 | 0 | 170 | 265 |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 51 | 66 | 0 | 117 | 0 | 0 | 0 | 0 | 0 | 21 | 122 | 0 | 0 | 143 | 260 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 56 | 57 | 0 | 113 | 0 | 0 | 0 | 0 | 0 | 15 | 115 | 0 | 0 | 130 | 243 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 0 | 189 | 209 | 0 | 398 | 0 | 0 | 0 | 0 | 0 | 87 | 507 | 0 | 0 | 594 | 992 |
| % App. Total | 0 | 0 | 0 | 0 | 0 | 0 | 47.5 | 52.5 | 0 | | 0 | 0 | 0 | 0 | 0 | 14.6 | 85.4 | 0 | 0 | | |
| PHF | .000 | .000 | .000 | .000 | .000 | .000 | .844 | .792 | .000 | .850 | .000 | .000 | .000 | .000 | .000 | .806 | .868 | .000 | .000 | .874 | .936 |

Peak Hour Analysis From 04:30 PM to 06:15 PM - Peak 1 of 1

Peak Hour for Entire Intersection Begins at 04:45 PM

Traffic Data Service

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(408) 377-2988

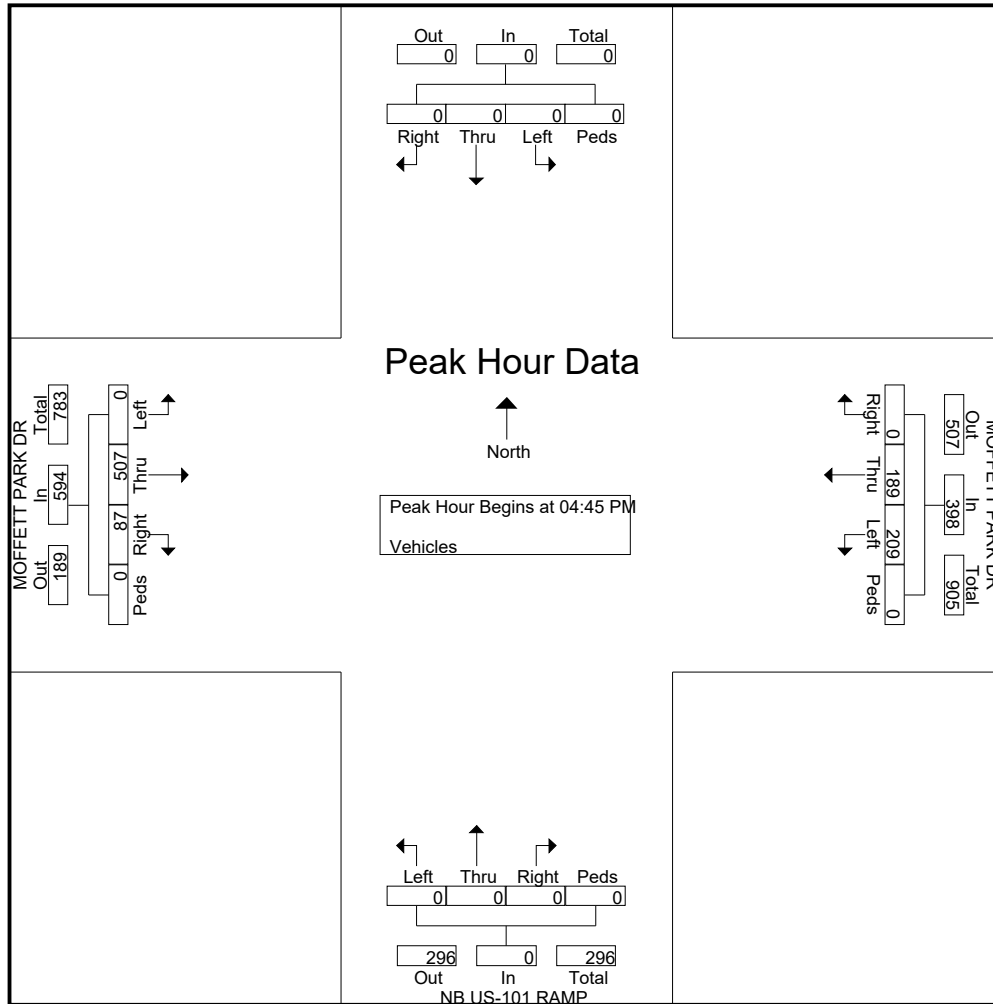
idsbay@cs.com

File Name : 1PM FINAL

Site Code : 00000001

Start Date : 2/12/2013

Page No : 2



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Campbell, CA

(408) 377-2988

tdsbay@cs.com

File Name : 1PM FINAL

Site Code : 00000001

Start Date : 2/12/2013

Page No : 1

Groups Printed- Bikes

| Start Time | Southbound | | | | | MOFFETT PARK DR Westbound | | | | | NB US-101 RAMP Northbound | | | | | MOFFETT PARK DR Eastbound | | | | | Int. Total |
|--------------------|------------|------|------|------|------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 2 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 3 |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 4 | 6 |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 6 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 9 |
| 05:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 5 | 8 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 0 | 0 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 0 | 0 | 13 | 29 |
| 06:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 06:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 0 | 30 | 0 | 0 | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 0 | 0 | 14 | 44 |
| Apprch % | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 0 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 0 | 100 | |
| Total % | 0 | 0 | 0 | 0 | 0 | 0 | 68.2 | 0 | 0 | 68.2 | 0 | 0 | 0 | 0 | 0 | 0 | 31.8 | 0 | 0 | 31.8 | |

| Start Time | Southbound | | | | | MOFFETT PARK DR Westbound | | | | | NB US-101 RAMP Northbound | | | | | MOFFETT PARK DR Eastbound | | | | | Int. Total |
|--|------------|------|------|------|------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| Peak Hour Analysis From 04:30 PM to 06:15 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 05:00 PM | | | | | | | | | | | | | | | | | | | | | |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 4 | 6 |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 6 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 9 |
| 05:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 5 | 8 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 0 | 0 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 0 | 0 | 13 | 29 |
| % App. Total | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 0 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 0 | 100 | |
| PHF | .000 | .000 | .000 | .000 | .000 | .000 | .571 | .000 | .000 | .571 | .000 | .000 | .000 | .000 | .000 | .000 | .650 | .000 | .000 | .650 | .806 |

Traffic Data Service

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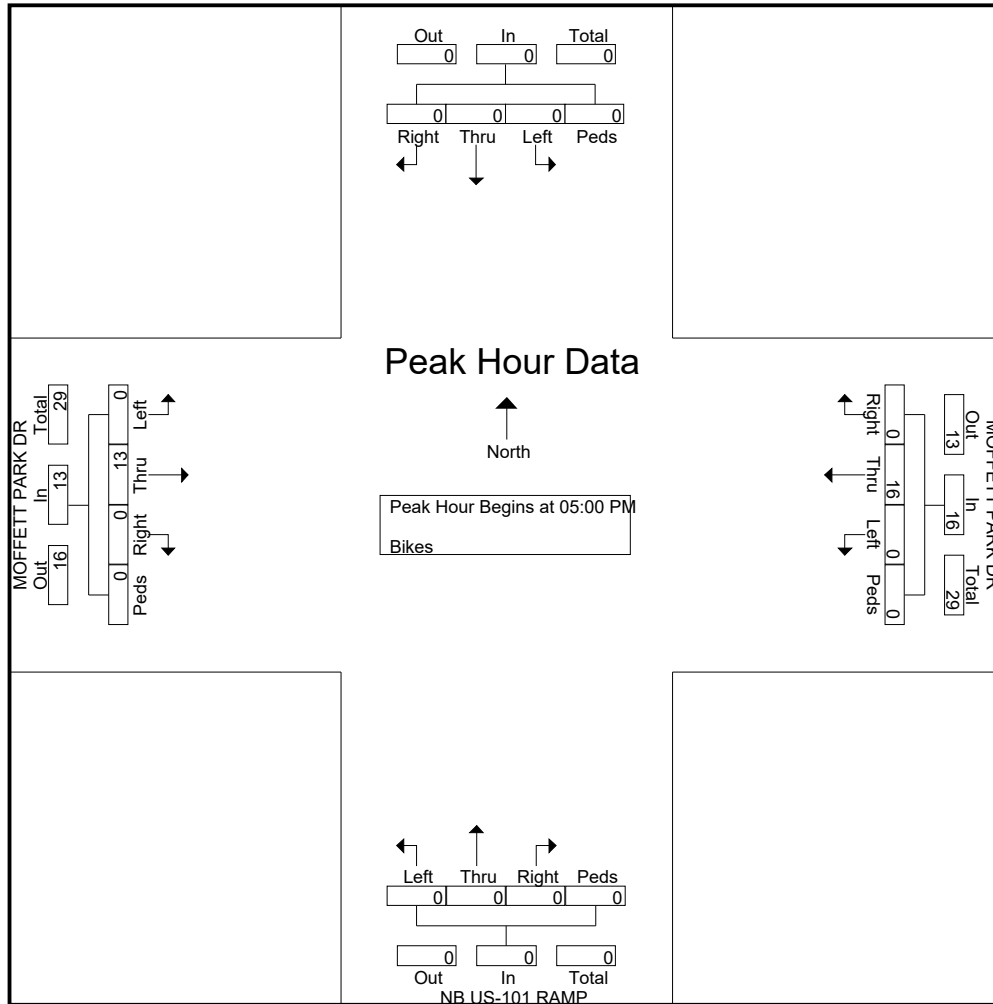
idsbay@cs.com

File Name : 1PM FINAL

Site Code : 00000001

Start Date : 2/12/2013

Page No : 2



Traffic Data Service

Campbell, CA
 (408) 377-2988
 tdsbay@cs.com

File Name : 1AM FINAL
 Site Code : 00000001
 Start Date : 11/18/2014
 Page No : 1

Groups Printed- Vehicles

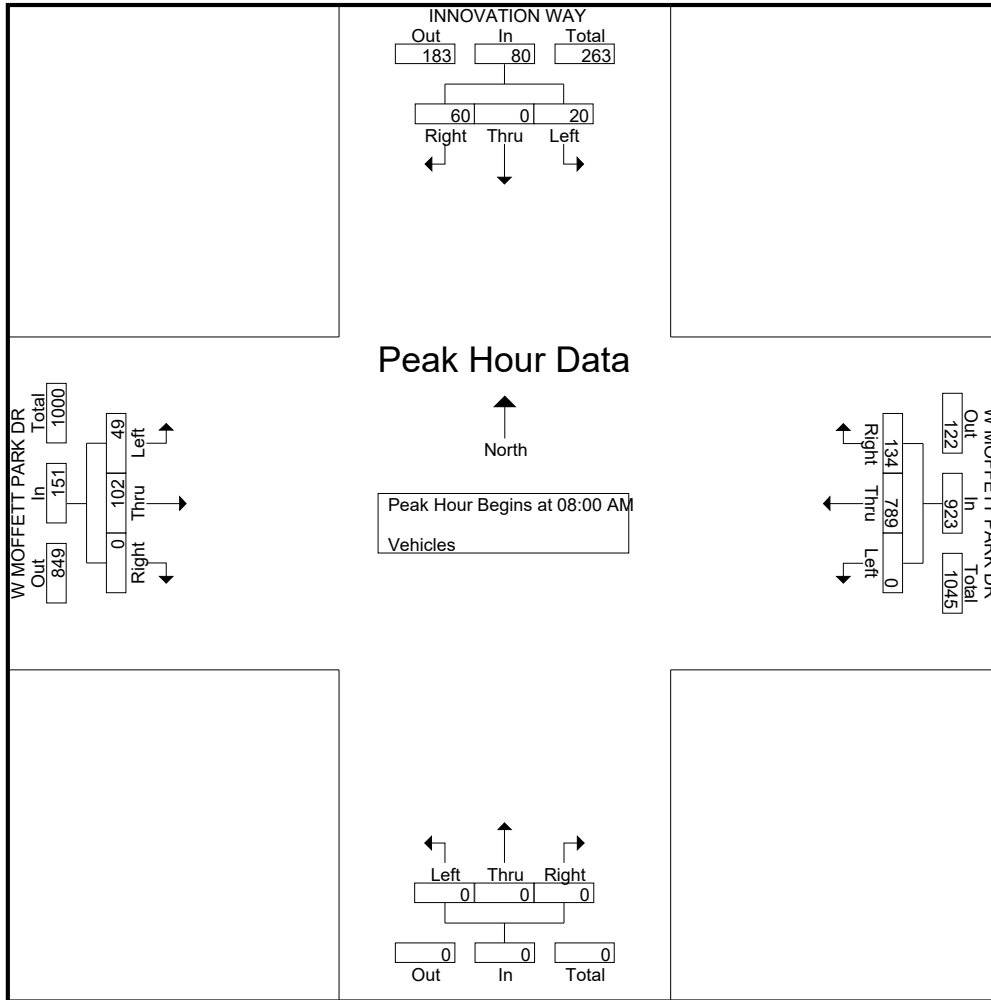
| Start Time | INNOVATION WAY Southbound | | | | | W MOFFETT PARK DR Westbound | | | | | Northbound | | | | | W MOFFETT PARK DR Eastbound | | | | | Int. Total |
|-------------|---------------------------|------|------|------|------------|-----------------------------|------|------|------|------------|------------|------|------|------|------------|-----------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 3 | 0 | 0 | 0 | 3 | 18 | 93 | 0 | 0 | 111 | 0 | 0 | 0 | 0 | 0 | 0 | 18 | 6 | 0 | 24 | 138 |
| 07:15 AM | 6 | 0 | 0 | 0 | 6 | 13 | 120 | 0 | 0 | 133 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 4 | 0 | 20 | 159 |
| 07:30 AM | 4 | 0 | 3 | 0 | 7 | 29 | 152 | 0 | 0 | 181 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 10 | 0 | 20 | 208 |
| 07:45 AM | 11 | 0 | 9 | 0 | 20 | 17 | 193 | 0 | 0 | 210 | 0 | 0 | 0 | 0 | 0 | 0 | 19 | 14 | 0 | 33 | 263 |
| Total | 24 | 0 | 12 | 0 | 36 | 77 | 558 | 0 | 0 | 635 | 0 | 0 | 0 | 0 | 0 | 0 | 63 | 34 | 0 | 97 | 768 |
| 08:00 AM | 14 | 0 | 1 | 0 | 15 | 32 | 200 | 0 | 0 | 232 | 0 | 0 | 0 | 0 | 0 | 0 | 15 | 7 | 0 | 22 | 269 |
| 08:15 AM | 14 | 0 | 2 | 0 | 16 | 28 | 184 | 0 | 0 | 212 | 0 | 0 | 0 | 0 | 0 | 0 | 25 | 13 | 0 | 38 | 266 |
| 08:30 AM | 9 | 0 | 4 | 0 | 13 | 36 | 205 | 0 | 0 | 241 | 0 | 0 | 0 | 0 | 0 | 0 | 23 | 14 | 0 | 37 | 291 |
| 08:45 AM | 23 | 0 | 13 | 0 | 36 | 38 | 200 | 0 | 0 | 238 | 0 | 0 | 0 | 0 | 0 | 0 | 39 | 15 | 0 | 54 | 328 |
| Total | 60 | 0 | 20 | 0 | 80 | 134 | 789 | 0 | 0 | 923 | 0 | 0 | 0 | 0 | 0 | 0 | 102 | 49 | 0 | 151 | 1154 |
| Grand Total | 84 | 0 | 32 | 0 | 116 | 211 | 1347 | 0 | 0 | 1558 | 0 | 0 | 0 | 0 | 0 | 0 | 165 | 83 | 0 | 248 | 1922 |
| Apprch % | 72.4 | 0 | 27.6 | 0 | | 13.5 | 86.5 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | 66.5 | 33.5 | 0 | | |
| Total % | 4.4 | 0 | 1.7 | 0 | 6 | 11 | 70.1 | 0 | 0 | 81.1 | 0 | 0 | 0 | 0 | 0 | 0 | 8.6 | 4.3 | 0 | 12.9 | |

| Start Time | INNOVATION WAY Southbound | | | | W MOFFETT PARK DR Westbound | | | | Northbound | | | | W MOFFETT PARK DR Eastbound | | | | Int. Total |
|--|---------------------------|------|-----------|------------|-----------------------------|------------|------|------------|------------|------|------|------------|-----------------------------|-----------|-----------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 08:00 AM | | | | | | | | | | | | | | | | | |
| 08:00 AM | 14 | 0 | 1 | 15 | 32 | 200 | 0 | 232 | 0 | 0 | 0 | 0 | 0 | 15 | 7 | 22 | 269 |
| 08:15 AM | 14 | 0 | 2 | 16 | 28 | 184 | 0 | 212 | 0 | 0 | 0 | 0 | 0 | 25 | 13 | 38 | 266 |
| 08:30 AM | 9 | 0 | 4 | 13 | 36 | 205 | 0 | 241 | 0 | 0 | 0 | 0 | 0 | 23 | 14 | 37 | 291 |
| 08:45 AM | 23 | 0 | 13 | 36 | 38 | 200 | 0 | 238 | 0 | 0 | 0 | 0 | 0 | 39 | 15 | 54 | 328 |
| Total Volume | 60 | 0 | 20 | 80 | 134 | 789 | 0 | 923 | 0 | 0 | 0 | 0 | 0 | 102 | 49 | 151 | 1154 |
| % App. Total | 75 | 0 | 25 | | 14.5 | 85.5 | 0 | | 0 | 0 | 0 | 0 | 0 | 67.5 | 32.5 | | |
| PHF | .652 | .000 | .385 | .556 | .882 | .962 | .000 | .957 | .000 | .000 | .000 | .000 | .000 | .654 | .817 | .699 | .880 |

Traffic Data Service

Campbell, CA
 (408) 377-2988
 tdsbay@cs.com

File Name : 1AM FINAL
 Site Code : 00000001
 Start Date : 11/18/2014
 Page No : 2



Traffic Data Service

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 tdsbay@cs.com

File Name : 1AM FINAL
 Site Code : 00000001
 Start Date : 11/18/2014
 Page No : 1

Groups Printed- Bikes

| Start Time | INNOVATION WAY Southbound | | | | | W MOFFETT PARK DR Westbound | | | | | Northbound | | | | | W MOFFETT PARK DR Eastbound | | | | | Int. Total |
|-------------|---------------------------|------|------|------|------------|-----------------------------|------|------|------|------------|------------|------|------|------|------------|-----------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 3 |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 6 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 9 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 7 |
| Total | 0 | 0 | 0 | 0 | 0 | 1 | 16 | 0 | 0 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 8 | 25 |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 7 | 9 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 8 |
| 08:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 2 |
| 08:45 AM | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 6 | 10 |
| Total | 0 | 0 | 0 | 0 | 0 | 1 | 11 | 0 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 17 | 0 | 0 | 17 | 29 |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 2 | 27 | 0 | 0 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 25 | 0 | 0 | 25 | 54 |
| Apprch % | 0 | 0 | 0 | 0 | 0 | 6.9 | 93.1 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 0 | | |
| Total % | 0 | 0 | 0 | 0 | 0 | 3.7 | 50 | 0 | 0 | 53.7 | 0 | 0 | 0 | 0 | 0 | 0 | 46.3 | 0 | 0 | 46.3 | |

| Start Time | INNOVATION WAY Southbound | | | | | W MOFFETT PARK DR Westbound | | | | | Northbound | | | | | W MOFFETT PARK DR Eastbound | | | | | Int. Total |
|--|---------------------------|------|------|------|------------|-----------------------------|------|------|------|------------|------------|------|------|------|------------|-----------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 07:30 AM | | | | | | | | | | | | | | | | | | | | | |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 9 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 7 |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 7 | 9 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 8 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 0 | 18 | 0 | 0 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 15 | 0 | 0 | 15 | 33 |
| % App. Total | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 100 | 0 | 0 | | |
| PHF | .000 | .000 | .000 | .000 | .000 | .000 | .750 | .000 | .750 | | .000 | .000 | .000 | .000 | | .000 | .536 | .000 | .536 | | .917 |

Traffic Data Service

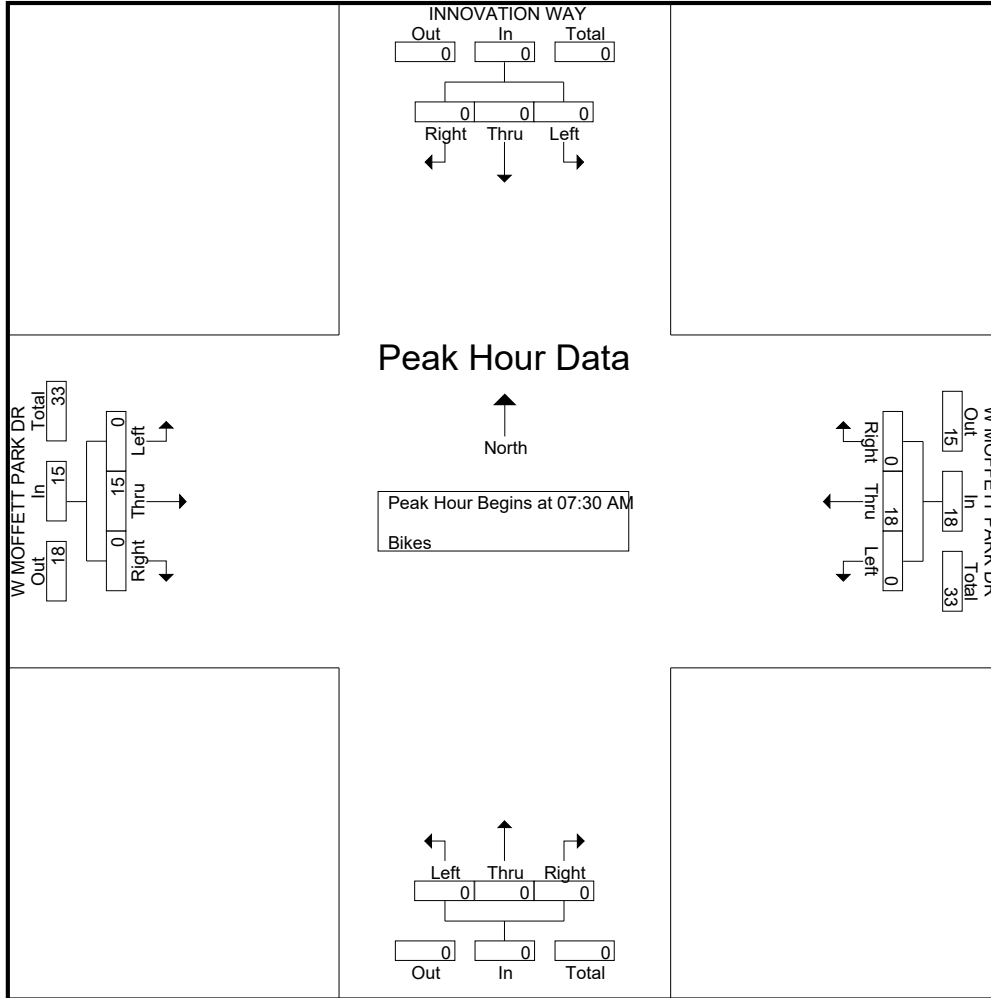
Campbell, CA
(408) 377-2988
idsbay@cs.com

File Name : 1AM FINAL

Site Code : 00000001

Start Date : 11/18/2014

Page No : 2



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 tdsbay@cs.com

File Name : 1PM FINAL
 Site Code : 00000001
 Start Date : 11/18/2014
 Page No : 1

Groups Printed- Vehicles

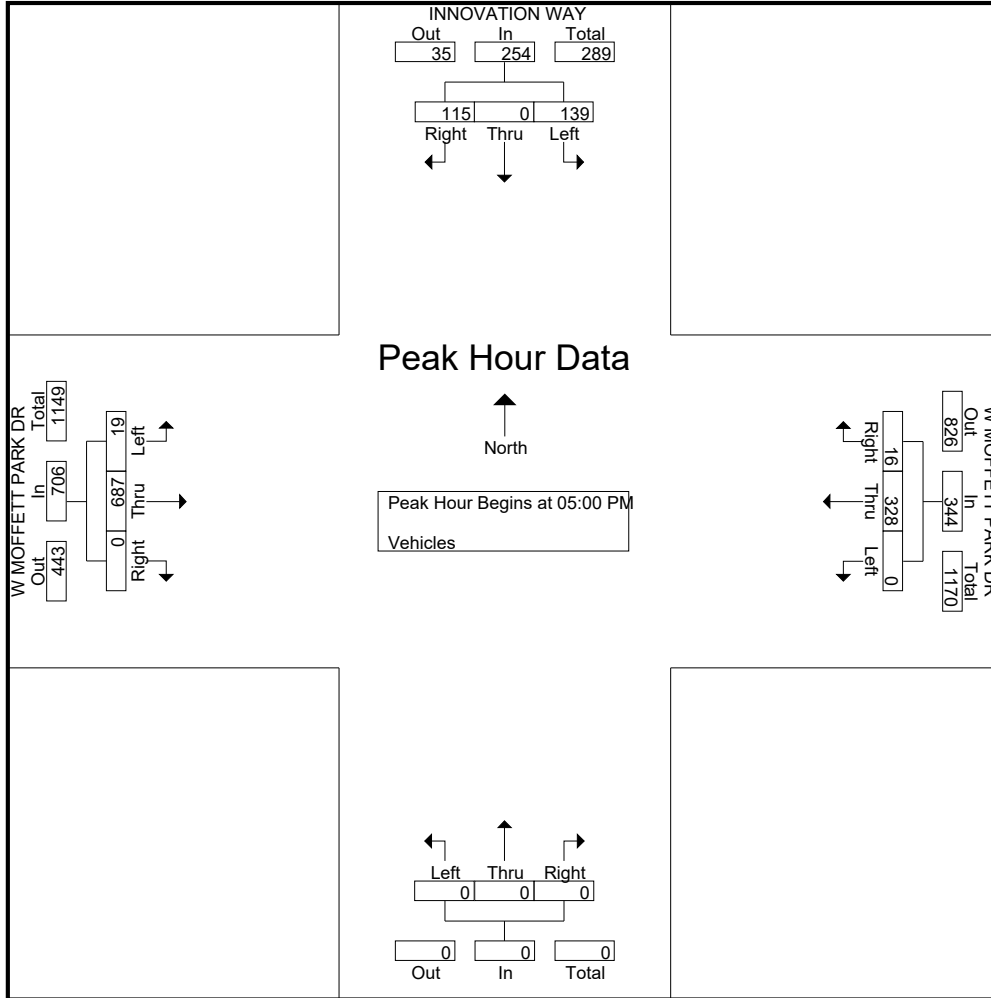
| Start Time | INNOVATION WAY Southbound | | | | | W MOFFETT PARK DR Westbound | | | | | Northbound | | | | | W MOFFETT PARK DR Eastbound | | | | | Int. Total |
|-------------|------------------------------|------|------|------|------------|--------------------------------|------|------|------|------------|------------|------|------|------|------------|--------------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:30 PM | 25 | 0 | 33 | 0 | 58 | 2 | 41 | 0 | 0 | 43 | 0 | 0 | 0 | 0 | 0 | 0 | 161 | 5 | 0 | 166 | 267 |
| 04:45 PM | 17 | 0 | 49 | 0 | 66 | 4 | 56 | 0 | 0 | 60 | 0 | 0 | 0 | 0 | 0 | 0 | 166 | 2 | 0 | 168 | 294 |
| Total | 42 | 0 | 82 | 0 | 124 | 6 | 97 | 0 | 0 | 103 | 0 | 0 | 0 | 0 | 0 | 0 | 327 | 7 | 0 | 334 | 561 |
| 05:00 PM | 31 | 0 | 47 | 0 | 78 | 3 | 68 | 0 | 0 | 71 | 0 | 0 | 0 | 0 | 0 | 0 | 192 | 1 | 0 | 193 | 342 |
| 05:15 PM | 27 | 0 | 35 | 0 | 62 | 4 | 81 | 0 | 0 | 85 | 0 | 0 | 0 | 0 | 0 | 0 | 224 | 8 | 0 | 232 | 379 |
| 05:30 PM | 32 | 0 | 22 | 0 | 54 | 6 | 81 | 0 | 0 | 87 | 0 | 0 | 0 | 0 | 0 | 0 | 123 | 5 | 0 | 128 | 269 |
| 05:45 PM | 25 | 0 | 35 | 0 | 60 | 3 | 98 | 0 | 0 | 101 | 0 | 0 | 0 | 0 | 0 | 0 | 148 | 5 | 0 | 153 | 314 |
| Total | 115 | 0 | 139 | 0 | 254 | 16 | 328 | 0 | 0 | 344 | 0 | 0 | 0 | 0 | 0 | 0 | 687 | 19 | 0 | 706 | 1304 |
| 06:00 PM | 31 | 0 | 34 | 0 | 65 | 3 | 82 | 0 | 0 | 85 | 0 | 0 | 0 | 0 | 0 | 0 | 120 | 3 | 0 | 123 | 273 |
| 06:15 PM | 18 | 0 | 20 | 0 | 38 | 3 | 70 | 0 | 0 | 73 | 0 | 0 | 0 | 0 | 0 | 0 | 136 | 2 | 0 | 138 | 249 |
| Grand Total | 206 | 0 | 275 | 0 | 481 | 28 | 577 | 0 | 0 | 605 | 0 | 0 | 0 | 0 | 0 | 0 | 1270 | 31 | 0 | 1301 | 2387 |
| Apprch % | 42.8 | 0 | 57.2 | 0 | | 4.6 | 95.4 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | 97.6 | 2.4 | 0 | | |
| Total % | 8.6 | 0 | 11.5 | 0 | 20.2 | 1.2 | 24.2 | 0 | 0 | 25.3 | 0 | 0 | 0 | 0 | 0 | 0 | 53.2 | 1.3 | 0 | 54.5 | |

| Start Time | INNOVATION WAY Southbound | | | | W MOFFETT PARK DR Westbound | | | | Northbound | | | | W MOFFETT PARK DR Eastbound | | | | Int. Total |
|--|------------------------------|------|-----------|------------|--------------------------------|-----------|------|------------|------------|------|------|------------|--------------------------------|------------|----------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 04:30 PM to 06:15 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 05:00 PM | | | | | | | | | | | | | | | | | |
| 05:00 PM | 31 | 0 | 47 | 78 | 3 | 68 | 0 | 71 | 0 | 0 | 0 | 0 | 0 | 192 | 1 | 193 | 342 |
| 05:15 PM | 27 | 0 | 35 | 62 | 4 | 81 | 0 | 85 | 0 | 0 | 0 | 0 | 0 | 224 | 8 | 232 | 379 |
| 05:30 PM | 32 | 0 | 22 | 54 | 6 | 81 | 0 | 87 | 0 | 0 | 0 | 0 | 0 | 123 | 5 | 128 | 269 |
| 05:45 PM | 25 | 0 | 35 | 60 | 3 | 98 | 0 | 101 | 0 | 0 | 0 | 0 | 0 | 148 | 5 | 153 | 314 |
| Total Volume | 115 | 0 | 139 | 254 | 16 | 328 | 0 | 344 | 0 | 0 | 0 | 0 | 0 | 687 | 19 | 706 | 1304 |
| % App. Total | 45.3 | 0 | 54.7 | | 4.7 | 95.3 | 0 | | 0 | 0 | 0 | | 0 | 97.3 | 2.7 | | |
| PHF | .898 | .000 | .739 | .814 | .667 | .837 | .000 | .851 | .000 | .000 | .000 | .000 | .000 | .767 | .594 | .761 | .860 |

Traffic Data Service

Campbell, CA
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idsbay@cs.com

File Name : 1PM FINAL
 Site Code : 00000001
 Start Date : 11/18/2014
 Page No : 2



Traffic Data Service

Campbell, CA
 (408) 377-2988
 tdsbay@cs.com

File Name : 1PM FINAL
 Site Code : 00000001
 Start Date : 11/18/2014
 Page No : 1

Groups Printed- Bikes

| Start Time | INNOVATION WAY Southbound | | | | | W MOFFETT PARK DR Westbound | | | | | Northbound | | | | | W MOFFETT PARK DR Eastbound | | | | | Int. Total |
|-------------|---------------------------|------|------|------|------------|-----------------------------|------|------|------|------------|------------|------|------|------|------------|-----------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 5 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 6 |
| 05:00 PM | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 2 |
| 05:15 PM | 0 | 0 | 2 | 0 | 2 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 4 | 10 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 05:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| Total | 0 | 0 | 3 | 0 | 3 | 0 | 9 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 5 | 17 |
| 06:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 06:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| Grand Total | 0 | 0 | 3 | 0 | 3 | 0 | 20 | 0 | 0 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 7 | 30 |
| Apprch % | 0 | 0 | 100 | 0 | | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 100 | 0 | 0 | | |
| Total % | 0 | 0 | 10 | 0 | 10 | 0 | 66.7 | 0 | 0 | 66.7 | 0 | 0 | 0 | 0 | 0 | 0 | 23.3 | 0 | 0 | 23.3 | |

| Start Time | INNOVATION WAY Southbound | | | | W MOFFETT PARK DR Westbound | | | | Northbound | | | | W MOFFETT PARK DR Eastbound | | | | Int. Total |
|--|---------------------------|------|------|------------|-----------------------------|------|------|------------|------------|------|------|------------|-----------------------------|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 04:30 PM to 06:15 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 05:15 PM | | | | | | | | | | | | | | | | | |
| 05:15 PM | 0 | 0 | 2 | 2 | 0 | 4 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 10 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 05:45 PM | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 06:00 PM | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| Total Volume | 0 | 0 | 2 | 2 | 0 | 13 | 0 | 13 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 19 |
| % App. Total | 0 | 0 | 100 | | 0 | 100 | 0 | | 0 | 0 | 0 | | 0 | 100 | 0 | | |
| PHF | .000 | .000 | .250 | .250 | .000 | .813 | .000 | .813 | .000 | .000 | .000 | .000 | .000 | .250 | .000 | .250 | .475 |

Traffic Data Service

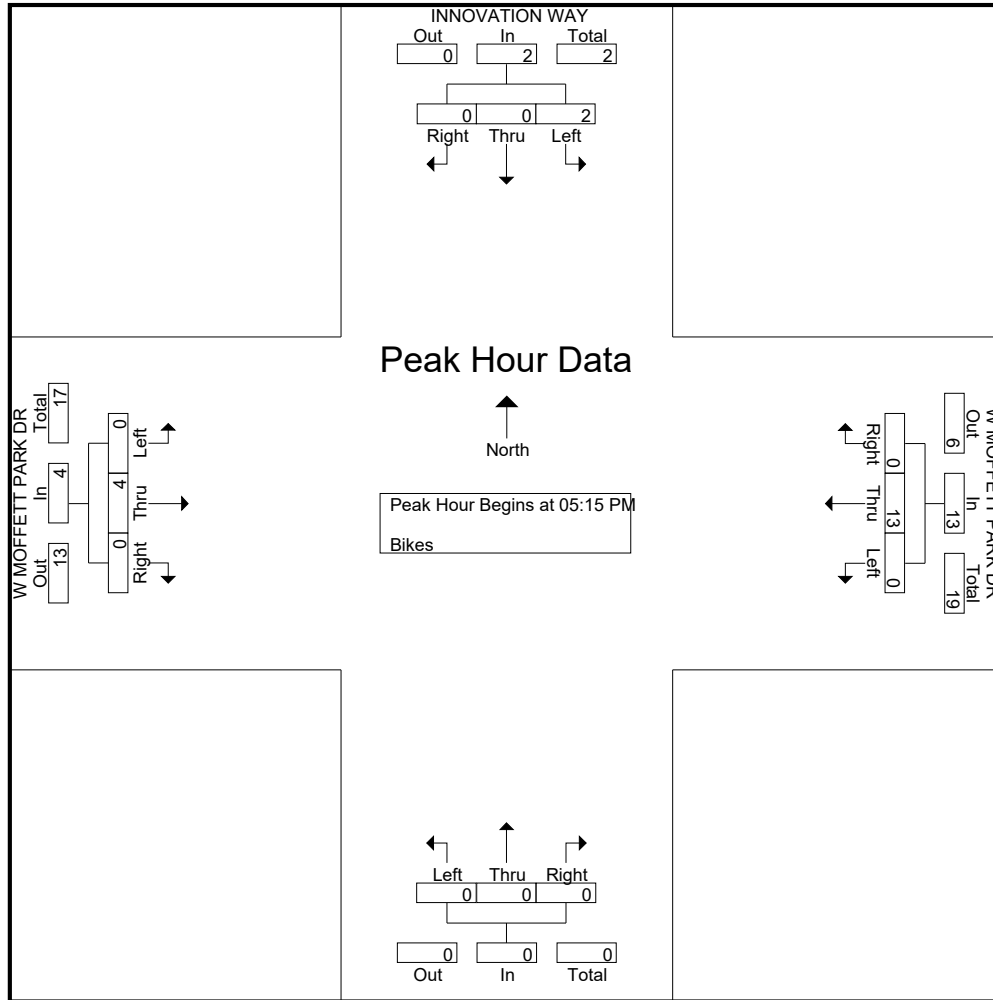
Campbell, CA
(408) 377-2988
idsbay@cs.com

File Name : 1PM FINAL

Site Code : 00000001

Start Date : 11/18/2014

Page No : 2



Traffic Data Service

Campbell, CA
 (408) 377-2988
 tdsbay@cs.com

File Name : 12AM FINAL
 Site Code : 00000012
 Start Date : 5/27/2015
 Page No : 1

Groups Printed- Vehicles

| Start Time | INNOVATION WAY Southbound | | | | | Westbound | | | | | INNOVATION WAY Northbound | | | | | 11TH AVE Eastbound | | | | | Int. Total |
|--------------|---------------------------|-----------|----------|----------|------------|-----------|----------|----------|----------|------------|---------------------------|----------|------------|----------|------------|--------------------|----------|----------|----------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 28 | 2 | 0 | 0 | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 14 | 0 | 15 | 4 | 0 | 1 | 0 | 5 | 50 |
| 07:15 AM | 23 | 8 | 0 | 0 | 31 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 20 | 0 | 21 | 8 | 0 | 1 | 0 | 9 | 61 |
| 07:30 AM | 27 | 9 | 0 | 1 | 37 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 21 | 0 | 21 | 15 | 0 | 2 | 0 | 17 | 75 |
| 07:45 AM | 47 | 11 | 0 | 1 | 59 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 29 | 0 | 29 | 10 | 0 | 2 | 0 | 12 | 100 |
| Total | 125 | 30 | 0 | 2 | 157 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 84 | 0 | 86 | 37 | 0 | 6 | 0 | 43 | 286 |
| 08:00 AM | 49 | 17 | 0 | 0 | 66 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 30 | 0 | 30 | 7 | 0 | 2 | 0 | 9 | 105 |
| 08:15 AM | 75 | 13 | 0 | 1 | 89 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 45 | 0 | 46 | 10 | 0 | 1 | 0 | 11 | 146 |
| 08:30 AM | 95 | 13 | 0 | 0 | 108 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 35 | 0 | 36 | 18 | 0 | 4 | 0 | 22 | 166 |
| 08:45 AM | 125 | 27 | 0 | 0 | 152 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 39 | 0 | 42 | 20 | 0 | 2 | 0 | 22 | 216 |
| Total | 344 | 70 | 0 | 1 | 415 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 149 | 0 | 154 | 55 | 0 | 9 | 0 | 64 | 633 |
| Grand Total | 469 | 100 | 0 | 3 | 572 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 233 | 0 | 240 | 92 | 0 | 15 | 0 | 107 | 919 |
| Apprch % | 82 | 17.5 | 0 | 0.5 | | 0 | 0 | 0 | 0 | 0 | 0 | 2.9 | 97.1 | 0 | | 86 | 0 | 14 | 0 | | |
| Total % | 51 | 10.9 | 0 | 0.3 | 62.2 | 0 | 0 | 0 | 0 | 0 | 0 | 0.8 | 25.4 | 0 | 26.1 | 10 | 0 | 1.6 | 0 | 11.6 | |

| Start Time | INNOVATION WAY Southbound | | | | Westbound | | | | INNOVATION WAY Northbound | | | | 11TH AVE Eastbound | | | | Int. Total | |
|--|---------------------------|------|------|------------|-----------|------|------|------------|---------------------------|------|------|------------|--------------------|------|------|------------|------------|------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 08:00 AM | | | | | | | | | | | | | | | | | | |
| 08:00 AM | 49 | 17 | 0 | 66 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 30 | 30 | 7 | 0 | 2 | 9 | 105 |
| 08:15 AM | 75 | 13 | 0 | 88 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 45 | 46 | 10 | 0 | 1 | 11 | 145 |
| 08:30 AM | 95 | 13 | 0 | 108 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 35 | 36 | 18 | 0 | 4 | 22 | 166 |
| 08:45 AM | 125 | 27 | 0 | 152 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 39 | 42 | 20 | 0 | 2 | 22 | 216 |
| Total Volume | 344 | 70 | 0 | 414 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 149 | 154 | 55 | 0 | 9 | 64 | 632 |
| % App. Total | 83.1 | 16.9 | 0 | | 0 | 0 | 0 | | 0 | 0 | 3.2 | 96.8 | | 85.9 | 0 | 14.1 | | |
| PHF | .688 | .648 | .000 | .681 | .000 | .000 | .000 | .000 | .000 | .000 | .417 | .828 | .837 | .688 | .000 | .563 | .727 | .731 |

Traffic Data Service

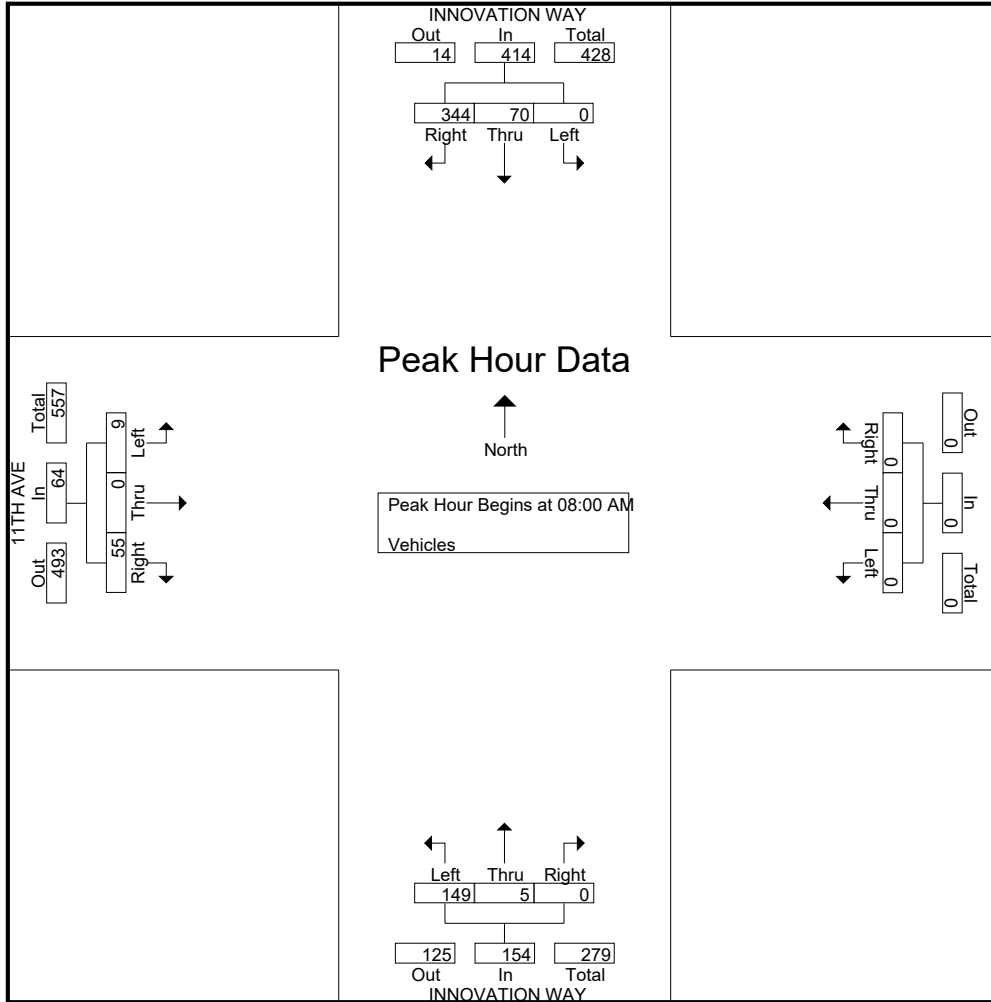
Campbell, CA
(408) 377-2988
idsbay@cs.com

File Name : 12AM FINAL

Site Code : 00000012

Start Date : 5/27/2015

Page No : 2



Traffic Data Service

Campbell, CA
 (408) 377-2988
 tdsbay@cs.com

File Name : 12AM FINAL
 Site Code : 00000012
 Start Date : 5/27/2015
 Page No : 1

Groups Printed- Bikes

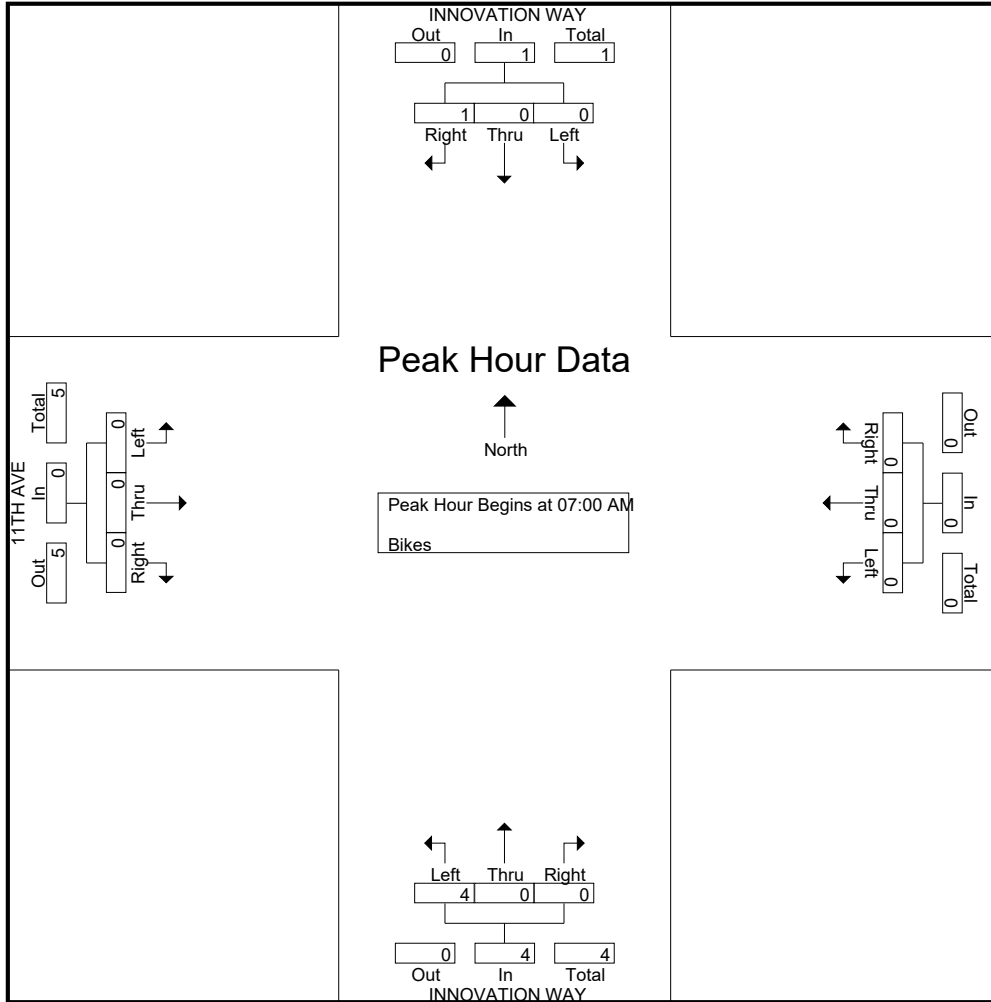
| Start Time | INNOVATION WAY Southbound | | | | | Westbound | | | | | INNOVATION WAY Northbound | | | | | 11TH AVE Eastbound | | | | | Int. Total |
|--------------|---------------------------|----------|----------|----------|------------|-----------|----------|----------|----------|------------|---------------------------|----------|----------|----------|------------|--------------------|----------|----------|----------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:15 AM | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 5 |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| Grand Total | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 6 |
| Apprch % | 100 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 20 | 80 | 0 | | 0 | 0 | 0 | 0 | | |
| Total % | 16.7 | 0 | 0 | 0 | 16.7 | 0 | 0 | 0 | 0 | 0 | 0 | 16.7 | 66.7 | 0 | 83.3 | 0 | 0 | 0 | 0 | 0 | |

| Start Time | INNOVATION WAY Southbound | | | | Westbound | | | | INNOVATION WAY Northbound | | | | 11TH AVE Eastbound | | | | Int. Total |
|--|---------------------------|------|------|------------|-----------|------|------|------------|---------------------------|------|------|------------|--------------------|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 07:00 AM | | | | | | | | | | | | | | | | | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 |
| 07:15 AM | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total Volume | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 4 | 0 | 0 | 0 | 0 | 5 |
| % App. Total | 100 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 100 | | 0 | 0 | 0 | | |
| PHF | .250 | .000 | .000 | .250 | .000 | .000 | .000 | .000 | .000 | .000 | .500 | .500 | .000 | .000 | .000 | .000 | .625 |

Traffic Data Service

Campbell, CA
 (408) 377-2988
 tdsbay@cs.com

File Name : 12AM FINAL
 Site Code : 00000012
 Start Date : 5/27/2015
 Page No : 2



Traffic Data Service

Campbell, CA
 (408) 377-2988
 tdsbay@cs.com

File Name : 12PM FINAL
 Site Code : 00000012
 Start Date : 5/27/2015
 Page No : 1

Groups Printed- Vehicles

| Start Time | INNOVATION WAY Southbound | | | | | Westbound | | | | | INNOVATION WAY Northbound | | | | | 11TH AVE Eastbound | | | | | Int. Total |
|--------------|---------------------------|-----------|----------|----------|------------|-----------|----------|----------|----------|------------|---------------------------|-----------|-----------|----------|------------|--------------------|----------|------------|----------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:00 PM | 4 | 4 | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 0 | 4 | 51 | 0 | 34 | 0 | 85 | 97 |
| 04:15 PM | 9 | 2 | 0 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 6 | 0 | 13 | 70 | 0 | 39 | 0 | 109 | 133 |
| 04:30 PM | 3 | 7 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 4 | 0 | 9 | 64 | 0 | 45 | 0 | 109 | 128 |
| 04:45 PM | 2 | 3 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 7 | 0 | 12 | 68 | 0 | 65 | 0 | 133 | 150 |
| Total | 18 | 16 | 0 | 0 | 34 | 0 | 0 | 0 | 0 | 0 | 0 | 19 | 19 | 0 | 38 | 253 | 0 | 183 | 0 | 436 | 508 |
| 05:00 PM | 3 | 4 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 15 | 3 | 0 | 18 | 75 | 0 | 93 | 0 | 168 | 193 |
| 05:15 PM | 3 | 11 | 0 | 0 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 27 | 8 | 0 | 35 | 68 | 0 | 106 | 0 | 174 | 223 |
| 05:30 PM | 4 | 2 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 2 | 0 | 12 | 58 | 0 | 85 | 0 | 143 | 161 |
| 05:45 PM | 4 | 15 | 0 | 0 | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 11 | 0 | 21 | 47 | 0 | 73 | 0 | 120 | 160 |
| Total | 14 | 32 | 0 | 0 | 46 | 0 | 0 | 0 | 0 | 0 | 0 | 62 | 24 | 0 | 86 | 248 | 0 | 357 | 0 | 605 | 737 |
| Grand Total | 32 | 48 | 0 | 0 | 80 | 0 | 0 | 0 | 0 | 0 | 0 | 81 | 43 | 0 | 124 | 501 | 0 | 540 | 0 | 1041 | 1245 |
| Apprch % | 40 | 60 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 65.3 | 34.7 | 0 | | 48.1 | 0 | 51.9 | 0 | | |
| Total % | 2.6 | 3.9 | 0 | 0 | 6.4 | 0 | 0 | 0 | 0 | 0 | 0 | 6.5 | 3.5 | 0 | 10 | 40.2 | 0 | 43.4 | 0 | 83.6 | |

| Start Time | INNOVATION WAY Southbound | | | | | Westbound | | | | | INNOVATION WAY Northbound | | | | | 11TH AVE Eastbound | | | | | Int. Total |
|--|---------------------------|-----------|------|------|------------|-----------|------|------|------|------------|---------------------------|-----------|-----------|------|------------|--------------------|------|------------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 05:00 PM | | | | | | | | | | | | | | | | | | | | | |
| 05:00 PM | 3 | 4 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 15 | 3 | 0 | 18 | 75 | 0 | 93 | 0 | 168 | 193 |
| 05:15 PM | 3 | 11 | 0 | 0 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 27 | 8 | 0 | 35 | 68 | 0 | 106 | 0 | 174 | 223 |
| 05:30 PM | 4 | 2 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 2 | 0 | 12 | 58 | 0 | 85 | 0 | 143 | 161 |
| 05:45 PM | 4 | 15 | 0 | 0 | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 11 | 0 | 21 | 47 | 0 | 73 | 0 | 120 | 160 |
| Total Volume | 14 | 32 | 0 | 0 | 46 | 0 | 0 | 0 | 0 | 0 | 0 | 62 | 24 | 0 | 86 | 248 | 0 | 357 | 0 | 605 | 737 |
| % App. Total | 30.4 | 69.6 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 72.1 | 27.9 | 0 | | 41 | 0 | 59 | 0 | | |
| PHF | .875 | .533 | .000 | .605 | | .000 | .000 | .000 | .000 | | .000 | .574 | .545 | .614 | | .827 | .000 | .842 | .869 | | .826 |

Traffic Data Service

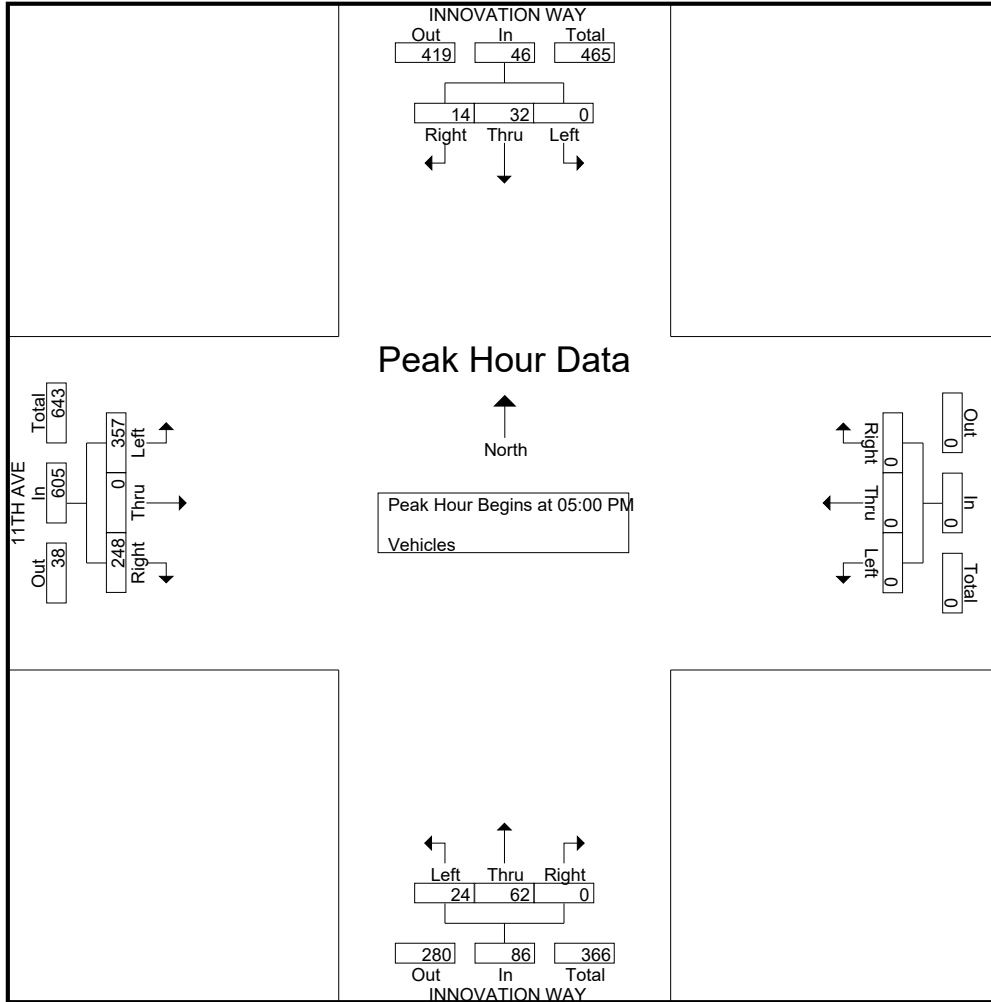
Campbell, CA
(408) 377-2988
idsbay@cs.com

File Name : 12PM FINAL

Site Code : 00000012

Start Date : 5/27/2015

Page No : 2



Traffic Data Service

Campbell, CA
 (408) 377-2988
 tdsbay@cs.com

File Name : 12PM FINAL
 Site Code : 00000012
 Start Date : 5/27/2015
 Page No : 1

Groups Printed- Bikes

| Start Time | INNOVATION WAY Southbound | | | | | Westbound | | | | | INNOVATION WAY Northbound | | | | | 11TH AVE Eastbound | | | | | Int. Total |
|--------------|---------------------------|----------|----------|----------|------------|-----------|----------|----------|----------|------------|---------------------------|----------|----------|----------|------------|--------------------|----------|----------|----------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 1 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 3 | 3 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 1 | 0 | 4 | 4 |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 1 |
| 05:45 PM | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 2 | 3 |
| Total | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 3 | 4 |
| Grand Total | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 2 | 0 | 7 | 8 |
| Apprch % | 100 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 71.4 | 0 | 28.6 | 0 | | |
| Total % | 12.5 | 0 | 0 | 0 | 12.5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 62.5 | 0 | 25 | 0 | 87.5 | |

| Start Time | INNOVATION WAY Southbound | | | | Westbound | | | | INNOVATION WAY Northbound | | | | 11TH AVE Eastbound | | | | Int. Total |
|--|---------------------------|------|------|------------|-----------|------|------|------------|---------------------------|------|------|------------|--------------------|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 04:00 PM | | | | | | | | | | | | | | | | | |
| 04:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 3 | 3 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 1 | 4 | 4 |
| % App. Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 75 | 0 | 25 | | |
| PHF | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .375 | .000 | .250 | .333 | .333 |

Traffic Data Service

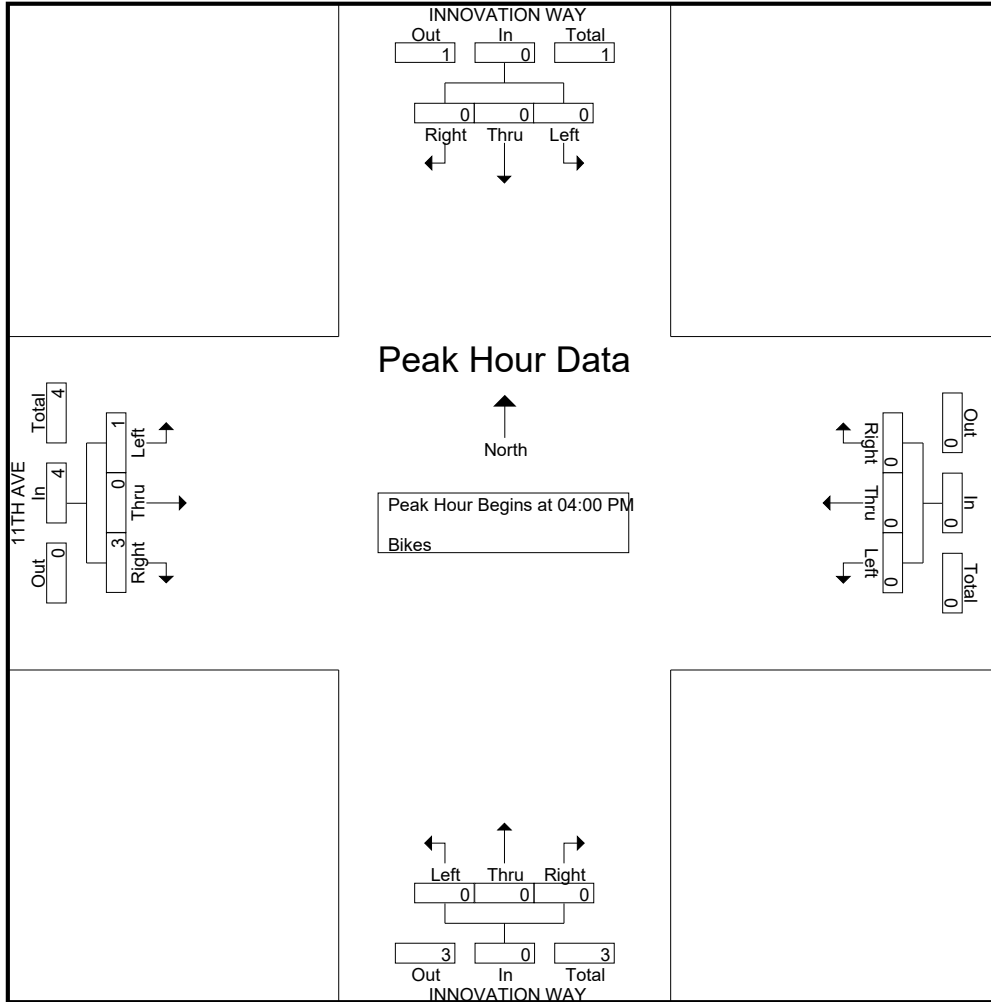
Campbell, CA
(408) 377-2988
idsbay@cs.com

File Name : 12PM FINAL

Site Code : 00000012

Start Date : 5/27/2015

Page No : 2



Traffic Data Service

Campbell, CA
 (408) 377-2988
 tdsbay@cs.com

File Name : 13AM FINAL
 Site Code : 00000013
 Start Date : 5/27/2015
 Page No : 1

Groups Printed- Vehicles

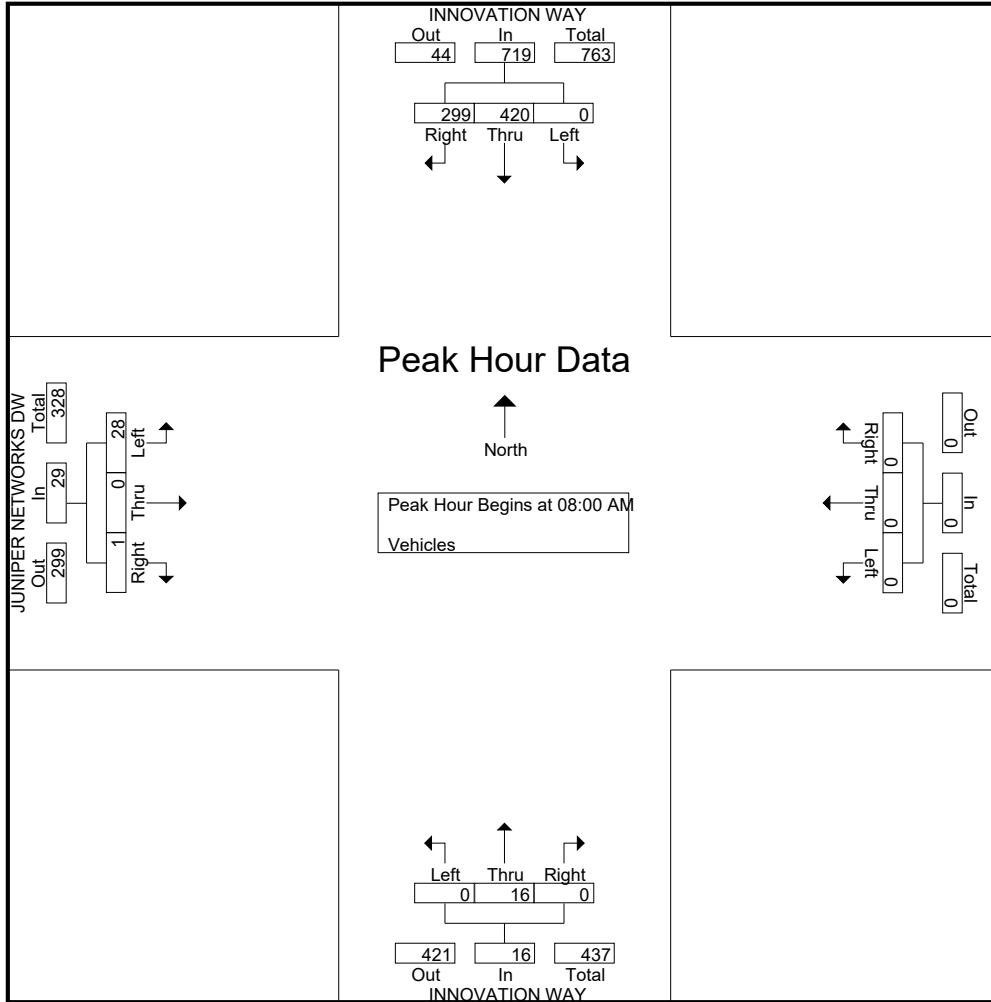
| Start Time | INNOVATION WAY Southbound | | | | | Westbound | | | | | INNOVATION WAY Northbound | | | | | JUNIPER NETWORKS DW Eastbound | | | | | Int. Total |
|--------------|---------------------------|------------|----------|----------|------------|-----------|----------|----------|----------|------------|---------------------------|-----------|----------|----------|------------|-------------------------------|----------|-----------|----------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 23 | 28 | 0 | 0 | 51 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 2 | 1 | 0 | 4 | 0 | 5 | 58 |
| 07:15 AM | 33 | 31 | 0 | 0 | 64 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 1 | 0 | 3 | 1 | 5 | 71 |
| 07:30 AM | 33 | 39 | 0 | 0 | 72 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 3 | 0 | 3 | 76 |
| 07:45 AM | 41 | 57 | 0 | 2 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 1 | 0 | 4 | 0 | 0 | 5 | 0 | 5 | 109 |
| Total | 130 | 155 | 0 | 2 | 287 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 2 | 0 | 9 | 2 | 0 | 15 | 1 | 18 | 314 |
| 08:00 AM | 66 | 67 | 0 | 0 | 133 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 3 | 0 | 0 | 11 | 0 | 11 | 147 |
| 08:15 AM | 77 | 93 | 0 | 0 | 170 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 5 | 0 | 5 | 177 |
| 08:30 AM | 69 | 107 | 0 | 0 | 176 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 1 | 7 | 0 | 0 | 8 | 0 | 8 | 191 |
| 08:45 AM | 87 | 153 | 0 | 0 | 240 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 6 | 1 | 0 | 4 | 0 | 5 | 251 |
| Total | 299 | 420 | 0 | 0 | 719 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 0 | 2 | 18 | 1 | 0 | 28 | 0 | 29 | 766 |
| Grand Total | 429 | 575 | 0 | 2 | 1006 | 0 | 0 | 0 | 0 | 0 | 0 | 23 | 2 | 2 | 27 | 3 | 0 | 43 | 1 | 47 | 1080 |
| Apprch % | 42.6 | 57.2 | 0 | 0.2 | | 0 | 0 | 0 | 0 | 0 | 0 | 85.2 | 7.4 | 7.4 | | 6.4 | 0 | 91.5 | 2.1 | | |
| Total % | 39.7 | 53.2 | 0 | 0.2 | 93.1 | 0 | 0 | 0 | 0 | 0 | 0 | 2.1 | 0.2 | 0.2 | 2.5 | 0.3 | 0 | 4 | 0.1 | 4.4 | |

| Start Time | INNOVATION WAY Southbound | | | | Westbound | | | | INNOVATION WAY Northbound | | | | JUNIPER NETWORKS DW Eastbound | | | | Int. Total | | |
|--|---------------------------|------------|----------|------------|-----------|----------|----------|------------|---------------------------|----------|----------|------------|-------------------------------|----------|----------|------------|------------|----------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | | | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 08:00 AM | | | | | | | | | | | | | | | | | | | |
| 08:00 AM | 66 | 67 | 0 | 133 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 2 | 0 | 0 | 11 | 11 | 146 |
| 08:15 AM | 77 | 93 | 0 | 170 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 2 | 0 | 0 | 5 | 5 | 177 |
| 08:30 AM | 69 | 107 | 0 | 176 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 6 | 0 | 6 | 0 | 0 | 8 | 8 | 190 |
| 08:45 AM | 87 | 153 | 0 | 240 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 6 | 0 | 6 | 1 | 0 | 4 | 5 | 251 |
| Total Volume | 299 | 420 | 0 | 719 | 0 | 0 | 0 | 0 | 0 | 16 | 0 | 16 | 0 | 16 | 1 | 0 | 28 | 29 | 764 |
| % App. Total | 41.6 | 58.4 | 0 | | 0 | 0 | 0 | | 0 | 100 | 0 | | | | 3.4 | 0 | 96.6 | | |
| PHF | .859 | .686 | .000 | .749 | .000 | .000 | .000 | .000 | .000 | .667 | .000 | .667 | .000 | .667 | .250 | .000 | .636 | .659 | .761 |

Traffic Data Service

Campbell, CA
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idsbay@cs.com

File Name : 13AM FINAL
 Site Code : 00000013
 Start Date : 5/27/2015
 Page No : 2



Traffic Data Service

Campbell, CA
 (408) 377-2988
 tdsbay@cs.com

File Name : 13AM FINAL
 Site Code : 00000013
 Start Date : 5/27/2015
 Page No : 1

Groups Printed- Bikes

| Start Time | INNOVATION WAY Southbound | | | | | Westbound | | | | | INNOVATION WAY Northbound | | | | | JUNIPER NETWORKS DW Eastbound | | | | | Int. Total |
|--------------|---------------------------|------|------|------|------------|-----------|------|------|------|------------|---------------------------|------|------|------|------------|-------------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 1 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 1 |
| 08:00 AM | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 3 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 3 |
| Grand Total | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 4 |
| Apprch % | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 100 | 0 | | 100 | 0 | 0 | 0 | | |
| Total % | 0 | 50 | 0 | 0 | 50 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 25 | 0 | 25 | 25 | 0 | 0 | 0 | 25 | |

| Start Time | INNOVATION WAY Southbound | | | | Westbound | | | | INNOVATION WAY Northbound | | | | JUNIPER NETWORKS DW Eastbound | | | | Int. Total |
|--|---------------------------|------|------|------------|-----------|------|------|------------|---------------------------|------|------|------------|-------------------------------|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 07:15 AM | | | | | | | | | | | | | | | | | |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:00 AM | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 3 |
| Total Volume | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 0 | 1 | 4 |
| % App. Total | 0 | 100 | 0 | | 0 | 0 | 0 | | 0 | 0 | 100 | | 100 | 0 | 0 | | |
| PHF | .000 | .250 | .000 | .250 | .000 | .000 | .000 | .000 | .000 | .000 | .250 | .250 | .250 | .000 | .000 | .250 | .333 |

Traffic Data Service

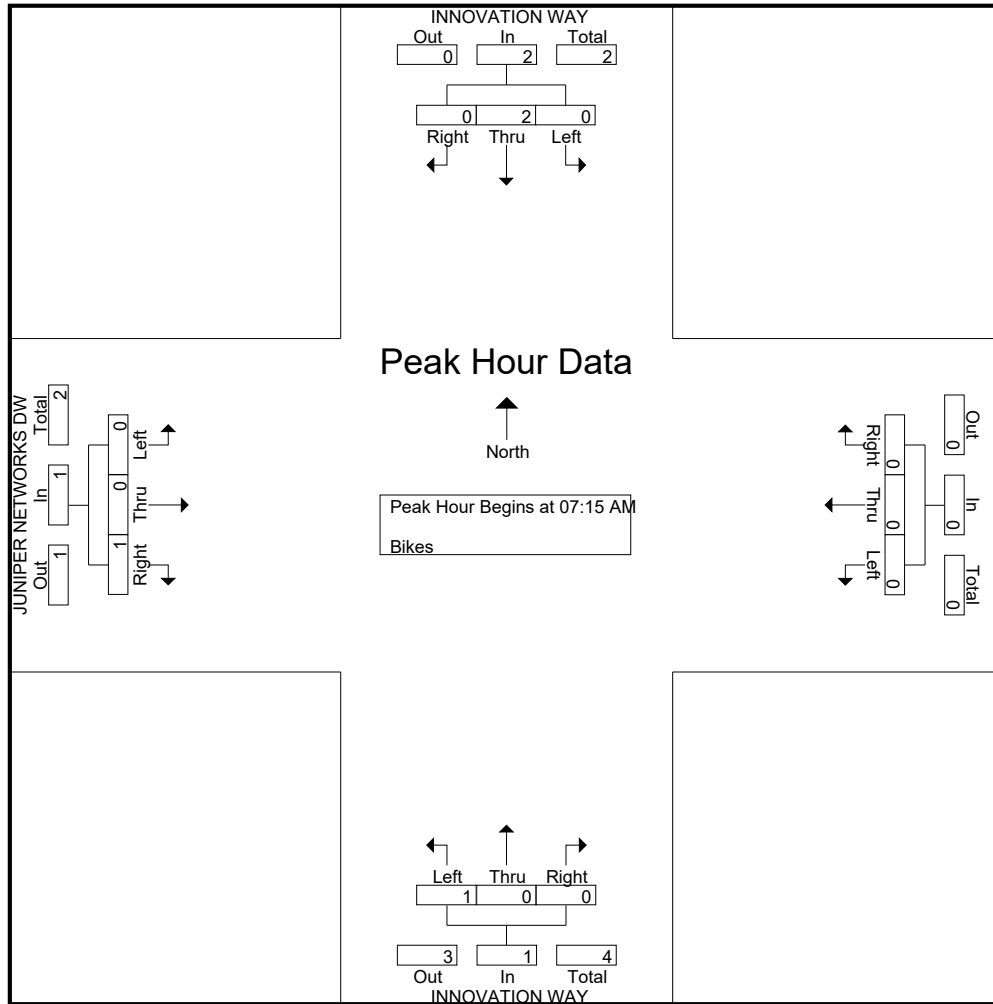
Campbell, CA
(408) 377-2988
idsbay@cs.com

File Name : 13AM FINAL

Site Code : 00000013

Start Date : 5/27/2015

Page No : 2



Traffic Data Service

Campbell, CA
 (408) 377-2988
 tdsbay@cs.com

File Name : 13PM FINAL
 Site Code : 00000013
 Start Date : 5/27/2015
 Page No : 1

Groups Printed- Vehicles

| Start Time | INNOVATION WAY Southbound | | | | | Westbound | | | | | INNOVATION WAY Northbound | | | | | JUNIPER NETWORKS DW Eastbound | | | | | Int. Total |
|--------------|---------------------------|-----------|----------|----------|------------|-----------|----------|----------|----------|------------|---------------------------|------------|----------|----------|------------|-------------------------------|----------|------------|----------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:00 PM | 12 | 7 | 0 | 0 | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 36 | 1 | 0 | 37 | 1 | 0 | 40 | 0 | 41 | 97 |
| 04:15 PM | 11 | 9 | 0 | 0 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 47 | 1 | 0 | 48 | 0 | 0 | 39 | 0 | 39 | 107 |
| 04:30 PM | 9 | 7 | 0 | 0 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 52 | 0 | 0 | 52 | 4 | 0 | 57 | 0 | 61 | 129 |
| 04:45 PM | 8 | 3 | 0 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 64 | 1 | 0 | 65 | 1 | 0 | 70 | 1 | 72 | 148 |
| Total | 40 | 26 | 0 | 0 | 66 | 0 | 0 | 0 | 0 | 0 | 0 | 199 | 3 | 0 | 202 | 6 | 0 | 206 | 1 | 213 | 481 |
| 05:00 PM | 13 | 6 | 0 | 0 | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 109 | 0 | 0 | 109 | 2 | 0 | 76 | 0 | 78 | 206 |
| 05:15 PM | 12 | 9 | 0 | 0 | 21 | 0 | 0 | 0 | 0 | 0 | 0 | 133 | 0 | 0 | 133 | 4 | 0 | 55 | 0 | 59 | 213 |
| 05:30 PM | 14 | 6 | 0 | 0 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 97 | 0 | 0 | 97 | 0 | 0 | 79 | 0 | 79 | 196 |
| 05:45 PM | 17 | 11 | 0 | 0 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 86 | 0 | 0 | 86 | 9 | 0 | 74 | 0 | 83 | 197 |
| Total | 56 | 32 | 0 | 0 | 88 | 0 | 0 | 0 | 0 | 0 | 0 | 425 | 0 | 0 | 425 | 15 | 0 | 284 | 0 | 299 | 812 |
| Grand Total | 96 | 58 | 0 | 0 | 154 | 0 | 0 | 0 | 0 | 0 | 0 | 624 | 3 | 0 | 627 | 21 | 0 | 490 | 1 | 512 | 1293 |
| Apprch % | 62.3 | 37.7 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | 99.5 | 0.5 | 0 | | 4.1 | 0 | 95.7 | 0.2 | | |
| Total % | 7.4 | 4.5 | 0 | 0 | 11.9 | 0 | 0 | 0 | 0 | 0 | 0 | 48.3 | 0.2 | 0 | 48.5 | 1.6 | 0 | 37.9 | 0.1 | 39.6 | |

| Start Time | INNOVATION WAY Southbound | | | | Westbound | | | | INNOVATION WAY Northbound | | | | JUNIPER NETWORKS DW Eastbound | | | | Int. Total | |
|--|---------------------------|------|------|------------|-----------|------|------|------------|---------------------------|------|------|------------|-------------------------------|------|------|------------|------------|------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | | |
| Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 05:00 PM | | | | | | | | | | | | | | | | | | |
| 05:00 PM | 13 | 6 | 0 | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 109 | 0 | 109 | 2 | 0 | 76 | 78 | 206 |
| 05:15 PM | 12 | 9 | 0 | 21 | 0 | 0 | 0 | 0 | 0 | 0 | 133 | 0 | 133 | 4 | 0 | 55 | 59 | 213 |
| 05:30 PM | 14 | 6 | 0 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 97 | 0 | 97 | 0 | 0 | 79 | 79 | 196 |
| 05:45 PM | 17 | 11 | 0 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 86 | 0 | 86 | 9 | 0 | 74 | 83 | 197 |
| Total Volume | 56 | 32 | 0 | 88 | 0 | 0 | 0 | 0 | 0 | 0 | 425 | 0 | 425 | 15 | 0 | 284 | 299 | 812 |
| % App. Total | 63.6 | 36.4 | 0 | | 0 | 0 | 0 | | 0 | 0 | 100 | 0 | | 5 | 0 | 95 | | |
| PHF | .824 | .727 | .000 | .786 | .000 | .000 | .000 | .000 | .000 | .000 | .799 | .000 | .799 | .417 | .000 | .899 | .901 | .953 |

Traffic Data Service

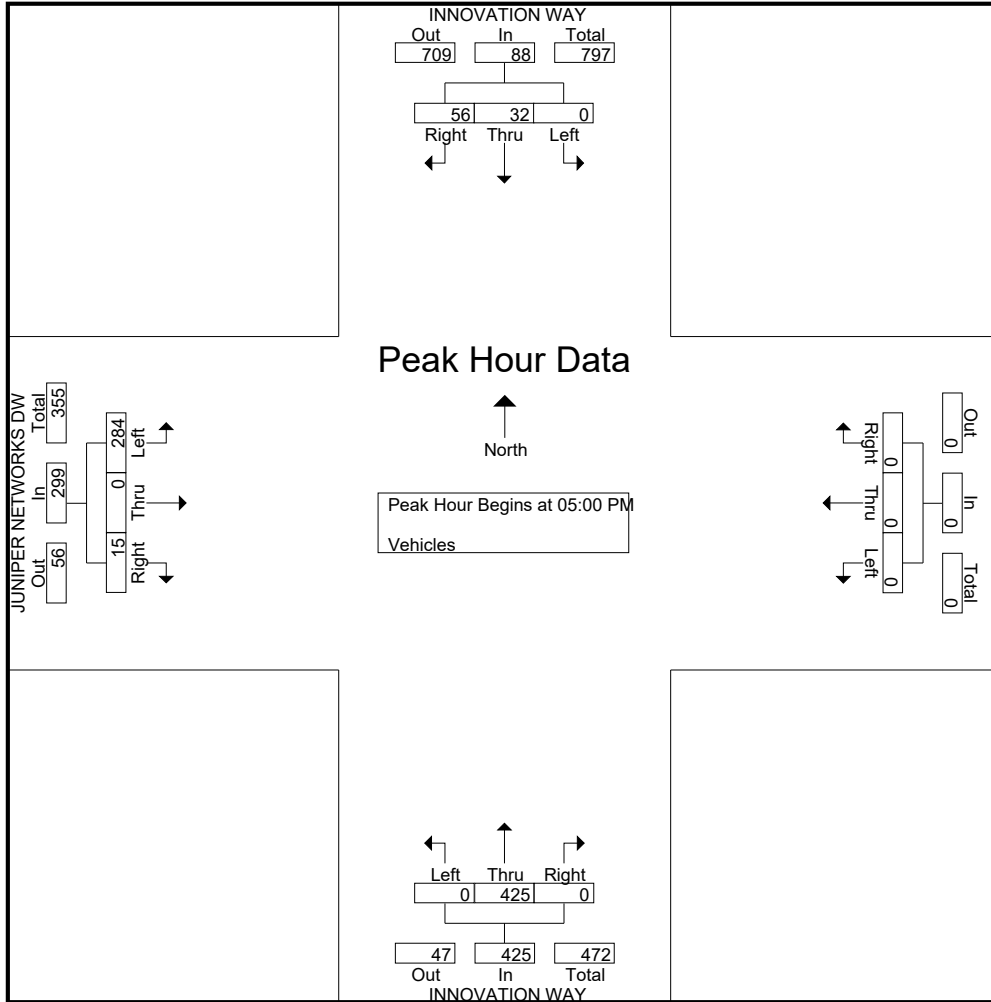
Campbell, CA
 (408) 377-2988
 tdsbay@cs.com

File Name : 13PM FINAL

Site Code : 00000013

Start Date : 5/27/2015

Page No : 2



Traffic Data Service

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 (408) 377-2988
 tdsbay@cs.com

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 Site Code : 00000013
 Start Date : 5/27/2015
 Page No : 1

Groups Printed- Bikes

| Start Time | INNOVATION WAY Southbound | | | | | Westbound | | | | | INNOVATION WAY Northbound | | | | | JUNIPER NETWORKS DW Eastbound | | | | | Int. Total |
|--------------|---------------------------|------|------|------|------------|-----------|------|------|------|------------|---------------------------|------|------|------|------------|-------------------------------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:45 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 |
| Total | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 |
| Grand Total | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 3 |
| Apprch % | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | |
| Total % | 0 | 33.3 | 0 | 0 | 33.3 | 0 | 0 | 0 | 0 | 0 | 0 | 66.7 | 0 | 0 | 66.7 | 0 | 0 | 0 | 0 | 0 | |

| Start Time | INNOVATION WAY Southbound | | | | Westbound | | | | INNOVATION WAY Northbound | | | | JUNIPER NETWORKS DW Eastbound | | | | Int. Total |
|--|---------------------------|------|------|------------|-----------|------|------|------------|---------------------------|------|------|------------|-------------------------------|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 05:00 PM | | | | | | | | | | | | | | | | | |
| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:45 PM | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 2 |
| Total Volume | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 2 |
| % App. Total | 0 | 100 | 0 | | 0 | 0 | 0 | | 0 | 100 | 0 | | 0 | 0 | 0 | | |
| PHF | .000 | .250 | .000 | .250 | .000 | .000 | .000 | .000 | .000 | .250 | .000 | .250 | .000 | .000 | .000 | .000 | .250 |

Traffic Data Service

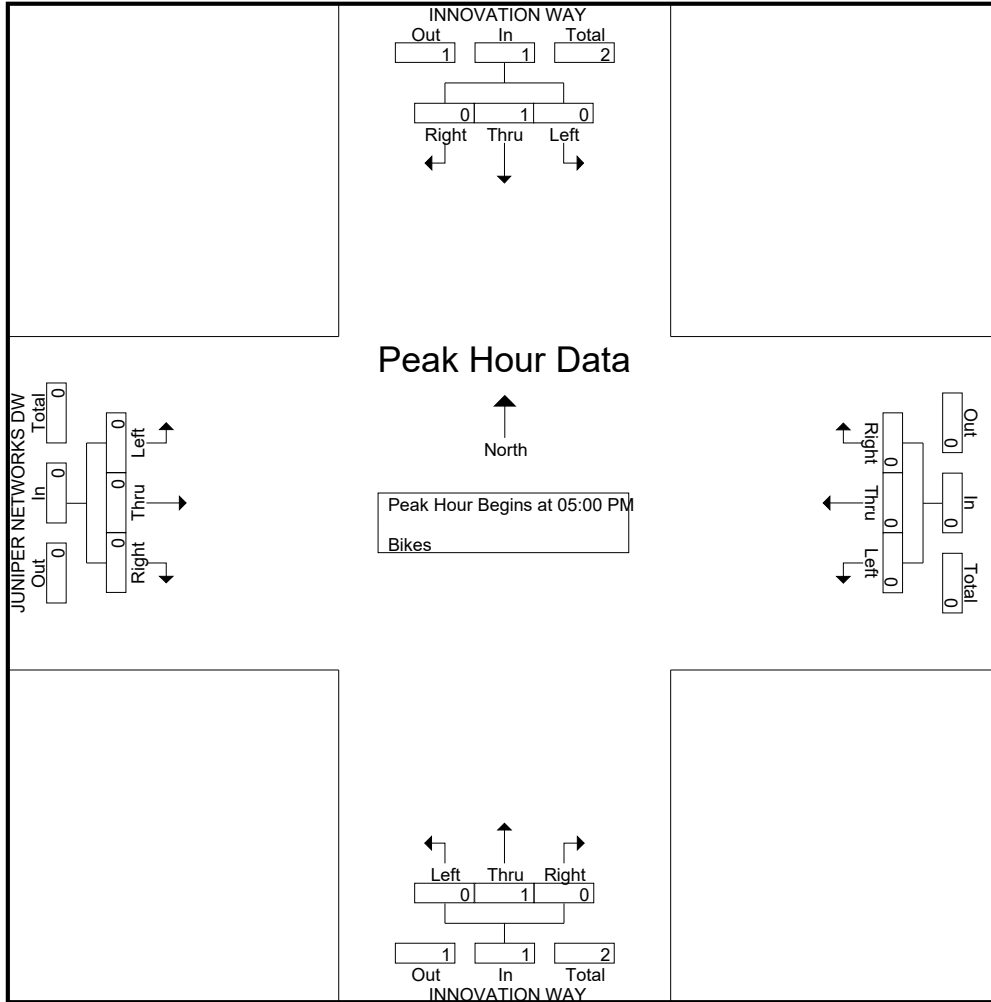
Campbell, CA
(408) 377-2988
tdsbay@cs.com

File Name : 13PM FINAL

Site Code : 00000013

Start Date : 5/27/2015

Page No : 2



Traffic Data Service

Campbell, CA
 (408) 377-2988
 tdsbay@cs.com

File Name : 14AM FINAL
 Site Code : 00000014
 Start Date : 5/27/2015
 Page No : 1

Groups Printed- Vehicles

| Start Time | BORDEAUX DR Southbound | | | | | INNOVATION WAY EXT Westbound | | | | | BORDEAUX DR Northbound | | | | | Eastbound | | | | | Int. Total |
|-------------|------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------------------|------|------|------|------------|-----------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 0 | 4 | 2 | 0 | 6 | 2 | 0 | 4 | 0 | 6 | 2 | 16 | 0 | 0 | 18 | 0 | 0 | 0 | 0 | 0 | 30 |
| 07:15 AM | 0 | 5 | 4 | 0 | 9 | 0 | 0 | 3 | 0 | 3 | 3 | 13 | 0 | 0 | 16 | 0 | 0 | 0 | 0 | 0 | 28 |
| 07:30 AM | 0 | 4 | 0 | 0 | 4 | 3 | 0 | 1 | 0 | 4 | 3 | 12 | 0 | 0 | 15 | 0 | 0 | 0 | 0 | 0 | 23 |
| 07:45 AM | 0 | 3 | 5 | 2 | 10 | 7 | 0 | 1 | 3 | 11 | 5 | 12 | 0 | 0 | 17 | 0 | 0 | 0 | 0 | 0 | 38 |
| Total | 0 | 16 | 11 | 2 | 29 | 12 | 0 | 9 | 3 | 24 | 13 | 53 | 0 | 0 | 66 | 0 | 0 | 0 | 0 | 0 | 119 |
| 08:00 AM | 0 | 7 | 0 | 0 | 7 | 3 | 0 | 3 | 0 | 6 | 12 | 14 | 0 | 0 | 26 | 0 | 0 | 0 | 0 | 0 | 39 |
| 08:15 AM | 0 | 10 | 6 | 0 | 16 | 1 | 0 | 1 | 3 | 5 | 7 | 27 | 0 | 2 | 36 | 0 | 0 | 0 | 0 | 0 | 57 |
| 08:30 AM | 0 | 7 | 3 | 0 | 10 | 2 | 0 | 1 | 0 | 3 | 6 | 21 | 0 | 0 | 27 | 0 | 0 | 0 | 0 | 0 | 40 |
| 08:45 AM | 0 | 7 | 1 | 0 | 8 | 2 | 0 | 1 | 1 | 4 | 5 | 29 | 0 | 2 | 36 | 0 | 0 | 0 | 0 | 0 | 48 |
| Total | 0 | 31 | 10 | 0 | 41 | 8 | 0 | 6 | 4 | 18 | 30 | 91 | 0 | 4 | 125 | 0 | 0 | 0 | 0 | 0 | 184 |
| Grand Total | 0 | 47 | 21 | 2 | 70 | 20 | 0 | 15 | 7 | 42 | 43 | 144 | 0 | 4 | 191 | 0 | 0 | 0 | 0 | 0 | 303 |
| Apprch % | 0 | 67.1 | 30 | 2.9 | | 47.6 | 0 | 35.7 | 16.7 | | 22.5 | 75.4 | 0 | 2.1 | | 0 | 0 | 0 | 0 | | |
| Total % | 0 | 15.5 | 6.9 | 0.7 | 23.1 | 6.6 | 0 | 5 | 2.3 | 13.9 | 14.2 | 47.5 | 0 | 1.3 | 63 | 0 | 0 | 0 | 0 | 0 | |

| Start Time | BORDEAUX DR Southbound | | | | INNOVATION WAY EXT Westbound | | | | BORDEAUX DR Northbound | | | | Eastbound | | | | Int. Total |
|--|------------------------|------|------|------------|------------------------------|------|------|------------|------------------------|------|------|------------|-----------|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 08:00 AM | | | | | | | | | | | | | | | | | |
| 08:00 AM | 0 | 7 | 0 | 7 | 3 | 0 | 3 | 6 | 12 | 14 | 0 | 26 | 0 | 0 | 0 | 0 | 39 |
| 08:15 AM | 0 | 10 | 6 | 16 | 1 | 0 | 1 | 2 | 7 | 27 | 0 | 34 | 0 | 0 | 0 | 0 | 52 |
| 08:30 AM | 0 | 7 | 3 | 10 | 2 | 0 | 1 | 3 | 6 | 21 | 0 | 27 | 0 | 0 | 0 | 0 | 40 |
| 08:45 AM | 0 | 7 | 1 | 8 | 2 | 0 | 1 | 3 | 5 | 29 | 0 | 34 | 0 | 0 | 0 | 0 | 45 |
| Total Volume | 0 | 31 | 10 | 41 | 8 | 0 | 6 | 14 | 30 | 91 | 0 | 121 | 0 | 0 | 0 | 0 | 176 |
| % App. Total | 0 | 75.6 | 24.4 | | 57.1 | 0 | 42.9 | | 24.8 | 75.2 | 0 | | 0 | 0 | 0 | | |
| PHF | .000 | .775 | .417 | .641 | .667 | .000 | .500 | .583 | .625 | .784 | .000 | .890 | .000 | .000 | .000 | .000 | .846 |

Traffic Data Service

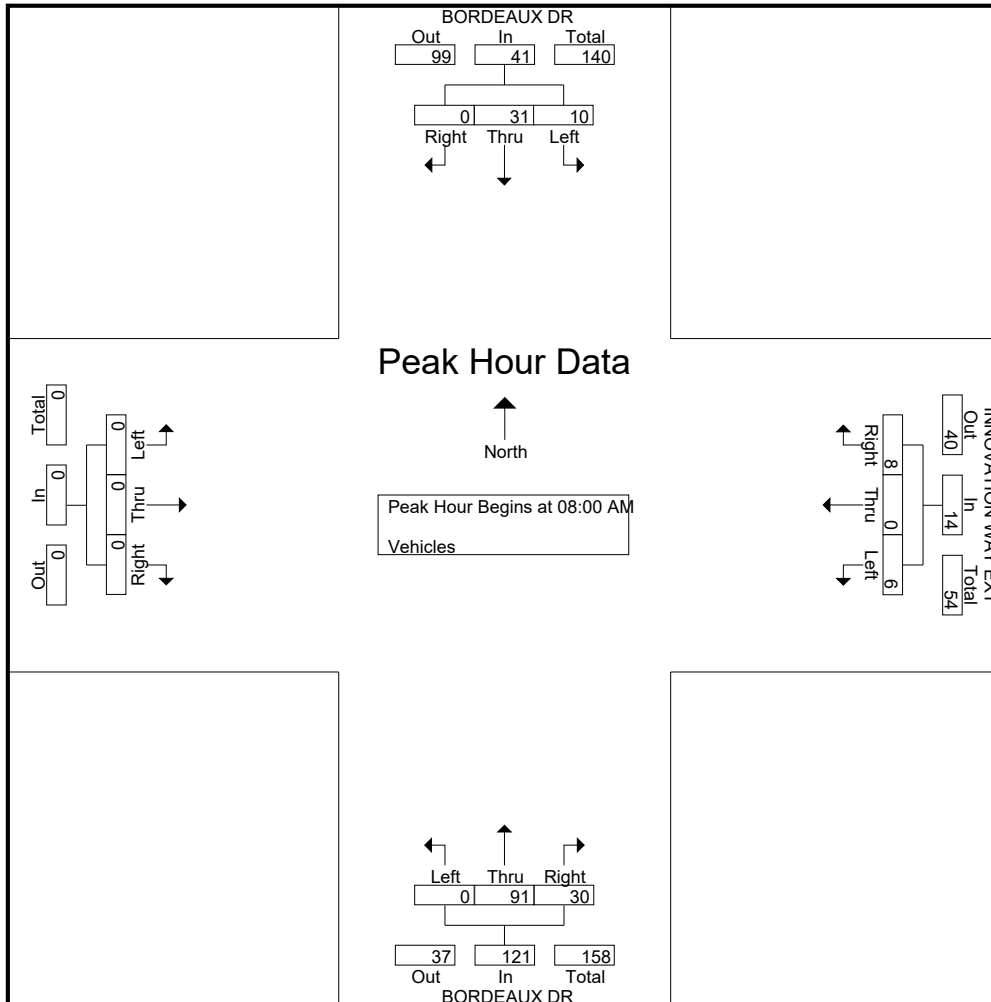
Campbell, CA
(408) 377-2988
idsbay@cs.com

File Name : 14AM FINAL

Site Code : 00000014

Start Date : 5/27/2015

Page No : 2



Traffic Data Service

Campbell, CA
 (408) 377-2988
 tdsbay@cs.com

File Name : 14AM FINAL
 Site Code : 00000014
 Start Date : 5/27/2015
 Page No : 1

Groups Printed- Bikes

| Start Time | BORDEAUX DR Southbound | | | | | INNOVATION WAY EXT Westbound | | | | | BORDEAUX DR Northbound | | | | | Eastbound | | | | | Int. Total |
|--------------|------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------------------|------|------|------|------------|-----------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 07:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 0 |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 0 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 11 |
| Apprch % | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 0 | 100 | 0 | 0 | 0 | 0 | 0 | 0 |
| Total % | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 0 | 100 | 0 | 0 | 0 | 0 | 0 | 0 |

| Start Time | BORDEAUX DR Southbound | | | | INNOVATION WAY EXT Westbound | | | | BORDEAUX DR Northbound | | | | Eastbound | | | | Int. Total |
|--|------------------------|------|------|------------|------------------------------|------|------|------------|------------------------|------|------|------------|-----------|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 07:45 AM | | | | | | | | | | | | | | | | | |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 08:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 0 | 0 | 0 | 0 | 3 |
| 08:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 5 | 0 | 0 | 0 | 0 | 5 |
| Total Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 0 | 10 | 0 | 0 | 0 | 0 | 10 |
| % App. Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 100 | 0 | 100 | 0 | 0 | 0 | 0 | 100 |
| PHF | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .500 | .000 | .500 | .000 | .000 | .000 | .000 | .500 |

Traffic Data Service

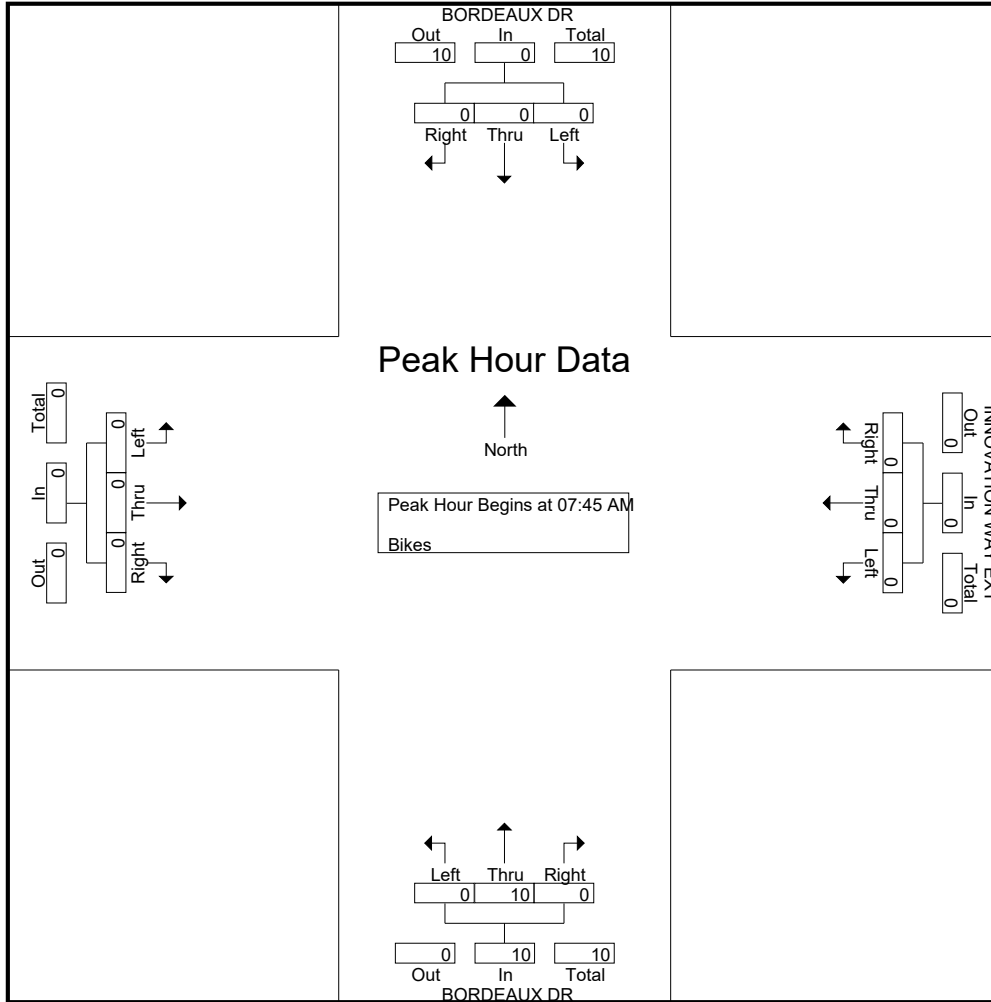
Campbell, CA
(408) 377-2988
idsbay@cs.com

File Name : 14AM FINAL

Site Code : 00000014

Start Date : 5/27/2015

Page No : 2



Traffic Data Service

Campbell, CA
 (408) 377-2988
 tdsbay@cs.com

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 Site Code : 00000014
 Start Date : 5/27/2015
 Page No : 1

Groups Printed- Vehicles

| Start Time | BORDEAUX DR Southbound | | | | | INNOVATION WAY EXT Westbound | | | | | BORDEAUX DR Northbound | | | | | Eastbound | | | | | Int. Total |
|-------------|------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------------------|------|------|------|------------|-----------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:00 PM | 0 | 22 | 0 | 0 | 22 | 1 | 0 | 6 | 0 | 7 | 0 | 7 | 0 | 1 | 8 | 0 | 0 | 0 | 0 | 0 | 37 |
| 04:15 PM | 0 | 25 | 2 | 0 | 27 | 2 | 0 | 6 | 0 | 8 | 2 | 6 | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 43 |
| 04:30 PM | 0 | 34 | 0 | 0 | 34 | 2 | 0 | 5 | 0 | 7 | 0 | 6 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 47 |
| 04:45 PM | 0 | 37 | 1 | 0 | 38 | 3 | 0 | 4 | 0 | 7 | 2 | 6 | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 53 |
| Total | 0 | 118 | 3 | 0 | 121 | 8 | 0 | 21 | 0 | 29 | 4 | 25 | 0 | 1 | 30 | 0 | 0 | 0 | 0 | 0 | 180 |
| 05:00 PM | 0 | 27 | 3 | 0 | 30 | 1 | 0 | 7 | 0 | 8 | 0 | 2 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 41 |
| 05:15 PM | 0 | 28 | 0 | 0 | 28 | 1 | 0 | 4 | 0 | 5 | 1 | 2 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 36 |
| 05:30 PM | 0 | 26 | 0 | 0 | 26 | 0 | 0 | 6 | 1 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 33 |
| 05:45 PM | 0 | 22 | 0 | 0 | 22 | 0 | 0 | 1 | 0 | 1 | 1 | 2 | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 0 | 27 |
| Total | 0 | 103 | 3 | 0 | 106 | 2 | 0 | 18 | 1 | 21 | 2 | 6 | 0 | 2 | 10 | 0 | 0 | 0 | 0 | 0 | 137 |
| Grand Total | 0 | 221 | 6 | 0 | 227 | 10 | 0 | 39 | 1 | 50 | 6 | 31 | 0 | 3 | 40 | 0 | 0 | 0 | 0 | 0 | 317 |
| Apprch % | 0 | 97.4 | 2.6 | 0 | | 20 | 0 | 78 | 2 | | 15 | 77.5 | 0 | 7.5 | | 0 | 0 | 0 | 0 | | |
| Total % | 0 | 69.7 | 1.9 | 0 | 71.6 | 3.2 | 0 | 12.3 | 0.3 | 15.8 | 1.9 | 9.8 | 0 | 0.9 | 12.6 | 0 | 0 | 0 | 0 | 0 | |

| Start Time | BORDEAUX DR Southbound | | | | INNOVATION WAY EXT Westbound | | | | BORDEAUX DR Northbound | | | | Eastbound | | | | Int. Total |
|--|------------------------|------|------|------------|------------------------------|------|------|------------|------------------------|------|------|------------|-----------|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 04:15 PM | | | | | | | | | | | | | | | | | |
| 04:15 PM | 0 | 25 | 2 | 27 | 2 | 0 | 6 | 8 | 2 | 6 | 0 | 8 | 0 | 0 | 0 | 0 | 43 |
| 04:30 PM | 0 | 34 | 0 | 34 | 2 | 0 | 5 | 7 | 0 | 6 | 0 | 6 | 0 | 0 | 0 | 0 | 47 |
| 04:45 PM | 0 | 37 | 1 | 38 | 3 | 0 | 4 | 7 | 2 | 6 | 0 | 8 | 0 | 0 | 0 | 0 | 53 |
| 05:00 PM | 0 | 27 | 3 | 30 | 1 | 0 | 7 | 8 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 40 |
| Total Volume | 0 | 123 | 6 | 129 | 8 | 0 | 22 | 30 | 4 | 20 | 0 | 24 | 0 | 0 | 0 | 0 | 183 |
| % App. Total | 0 | 95.3 | 4.7 | | 26.7 | 0 | 73.3 | | 16.7 | 83.3 | 0 | | 0 | 0 | 0 | | |
| PHF | .000 | .831 | .500 | .849 | .667 | .000 | .786 | .938 | .500 | .833 | .000 | .750 | .000 | .000 | .000 | .000 | .863 |

Traffic Data Service

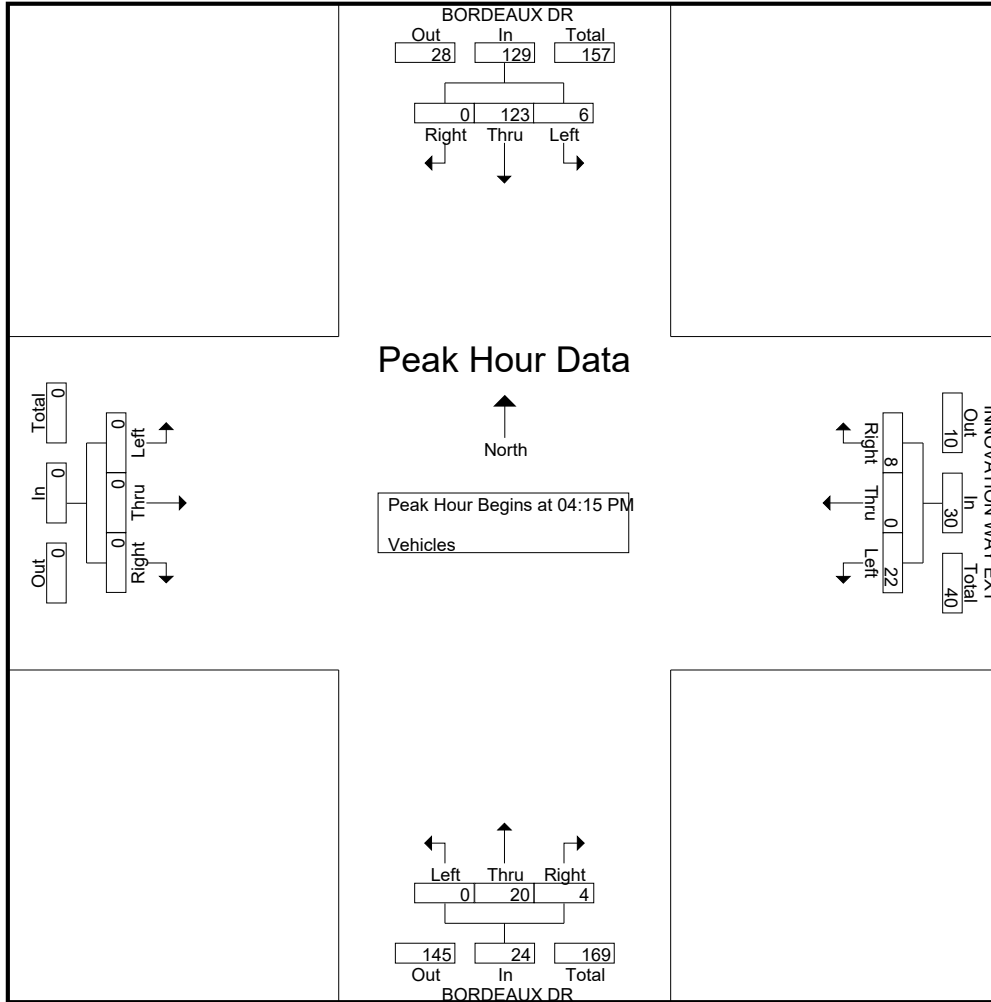
Campbell, CA
(408) 377-2988
idsbay@cs.com

File Name : 14PM FINAL

Site Code : 00000014

Start Date : 5/27/2015

Page No : 2



Traffic Data Service

Campbell, CA
 (408) 377-2988
 tdsbay@cs.com

File Name : 14PM FINAL
 Site Code : 00000014
 Start Date : 5/27/2015
 Page No : 1

Groups Printed- Bikes

| Start Time | BORDEAUX DR Southbound | | | | | INNOVATION WAY EXT Westbound | | | | | BORDEAUX DR Northbound | | | | | Eastbound | | | | | Int. Total |
|--------------|------------------------|------|------|------|------------|------------------------------|------|------|------|------------|------------------------|------|------|------|------------|-----------|------|------|------|------------|------------|
| | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Total | |
| 04:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:30 PM | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 04:45 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| Total | 0 | 5 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 05:00 PM | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 05:15 PM | 0 | 3 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 05:30 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 05:45 PM | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| Total | 0 | 8 | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| Grand Total | 0 | 13 | 0 | 0 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 |
| Apprch % | 0 | 100 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | |
| Total % | 0 | 100 | 0 | 0 | 100 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |

| Start Time | BORDEAUX DR Southbound | | | | INNOVATION WAY EXT Westbound | | | | BORDEAUX DR Northbound | | | | Eastbound | | | | Int. Total |
|--|------------------------|------|------|------------|------------------------------|------|------|------------|------------------------|------|------|------------|-----------|------|------|------------|------------|
| | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | Right | Thru | Left | App. Total | |
| Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1 | | | | | | | | | | | | | | | | | |
| Peak Hour for Entire Intersection Begins at 04:30 PM | | | | | | | | | | | | | | | | | |
| 04:30 PM | 0 | 4 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 04:45 PM | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 05:00 PM | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 05:15 PM | 0 | 3 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| Total Volume | 0 | 10 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 |
| % App. Total | 0 | 100 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | |
| PHF | .000 | .625 | .000 | .625 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .000 | .625 |

Traffic Data Service

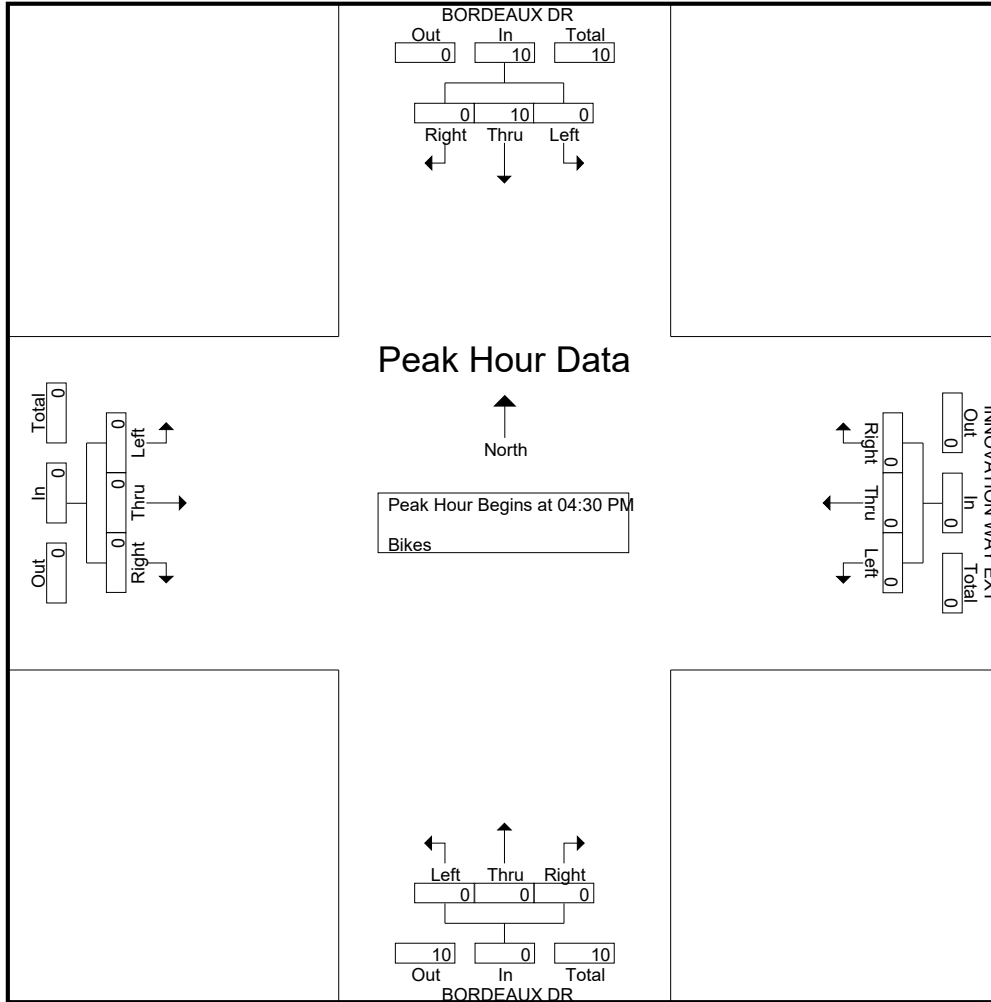
Campbell, CA
(408) 377-2988
idsbay@cs.com

File Name : 14PM FINAL

Site Code : 00000014

Start Date : 5/27/2015

Page No : 2



**November 13, 2013 - Count Data at Pedestrian Overcrossing between Mathilda Avenue
and Fair Oaks Avenue**

| Time | EB SR-237 | | WB SR-237 | Pedestrian Overcrossing | | | |
|---------|-----------|---------|-----------|-------------------------|---------|----------|----------|
| | HOV | REGULAR | REGULAR | NB PEDS | SB PEDS | NB BIKES | SB BIKES |
| 7:00 AM | 27 | 558 | 1044 | 0 | 0 | 2 | 0 |
| 7:15 AM | 44 | 712 | 1077 | 0 | 0 | 2 | 1 |
| 7:30 AM | 59 | 826 | 1043 | 1 | 0 | 6 | 0 |
| 7:45 AM | 71 | 903 | 1112 | 0 | 0 | 4 | 1 |
| 8:00 AM | 86 | 991 | 1011 | 0 | 1 | 2 | 0 |
| 8:15 AM | 92 | 992 | 1052 | 2 | 0 | 3 | 1 |
| 8:30 AM | 94 | 992 | 1187 | 1 | 0 | 5 | 1 |
| 8:45 AM | 111 | 997 | 1145 | 0 | 2 | 4 | 5 |
| | | | | | | | |
| 4:00 PM | 191 | 810 | 796 | 0 | 0 | 0 | 5 |
| 4:15 PM | 215 | 674 | 900 | 0 | 0 | 3 | 0 |
| 4:30 PM | 246 | 715 | 866 | 0 | 0 | 1 | 6 |
| 4:45 PM | 239 | 718 | 945 | 0 | 1 | 2 | 10 |
| 5:00 PM | 234 | 685 | 1020 | 0 | 0 | 0 | 8 |
| 5:15 PM | 294 | 687 | 946 | 0 | 0 | 0 | 5 |
| 5:30 PM | 295 | 611 | 956 | 0 | 0 | 2 | 7 |
| 5:45 PM | 308 | 621 | 702 | 0 | 0 | 0 | 4 |
| 6:00 PM | 240 | 575 | 771 | 0 | 0 | 1 | 1 |
| 6:15 PM | 280 | 649 | 956 | 0 | 0 | 0 | 3 |
| 6:30 PM | 197 | 677 | 879 | 0 | 0 | 0 | 11 |
| 6:45 PM | 162 | 633 | 799 | 0 | 0 | 2 | 3 |

Source: Fehr & Peers, November 2013.

APPENDIX B – US 101 TRAVEL TIME RUN TABLES



US 101 Travel Time Runs

(GPS travel time surveys conducted on November 2013)

US 101 Northbound AM - Mixed Flow Lanes

| Segment ID | Segment Location | Distance (miles) | Travel Time Run 1 | | Travel Time Run 2 | | Travel Time Run 3 | |
|------------|--|------------------|--------------------|-------|--------------------|-------|--------------------|-------|
| | | | Segment Start Time | Speed | Segment Start Time | Speed | Segment Start Time | Speed |
| 1 | Lawrence Expressway to End of Merge Lane | 0.217 | 7:46:28 | 11.85 | 8:26:12 | 26.79 | 8:57:47 | 46.20 |
| 2 | End of Merge Lane to Fair Oaks Off-Ramp | 0.439 | 7:47:28 | 19.54 | 8:26:39 | 27.46 | 8:58:02 | 37.48 |
| 3 | Fair Oaks Off-Ramp to Fair Oaks Bridge | 0.153 | 7:48:46 | 19.22 | 8:27:35 | 28.06 | 8:58:43 | 39.58 |
| 4 | Fair Oaks Bridge to Fair Oaks On-Ramp | 0.122 | 7:49:13 | 5.99 | 8:27:54 | 27.67 | 8:58:56 | 39.20 |
| 5 | Fair Oaks On-Ramp to Mathilda Off-Ramp | 0.550 | 7:50:17 | 27.14 | 8:28:09 | 31.50 | 8:59:07 | 35.28 |
| 6 | Mathilda Off-Ramp to Mathilda On-Ramp | 0.167 | 7:51:27 | 26.92 | 8:29:10 | 22.73 | 9:00:01 | 44.47 |
| 7 | Mathilda On-Ramp to Mathilda Off-Ramp | 0.028 | 7:51:49 | 23.15 | 8:29:36 | 27.96 | 9:00:15 | 42.87 |
| 8 | Mathilda Off-Ramp to SR 237 WB Off-Ramp | 0.432 | 7:51:53 | 19.94 | 8:29:40 | 18.08 | 9:00:17 | 30.20 |
| 9 | SR 237 WB Off-Ramp to Part-way to Ellis Street | 0.457 | 7:53:08 | 11.47 | 8:31:01 | 16.79 | 9:01:07 | 20.65 |

Source: Fehr & Peers, November 2013.

US 101 Northbound PM - Mixed Flow Lanes

| Segment ID | Segment Location | Distance (miles) | Travel Time Run 1 | | Travel Time Run 2 | | Travel Time Run 3 | |
|------------|--|------------------|--------------------|-------|--------------------|-------|--------------------|-------|
| | | | Segment Start Time | Speed | Segment Start Time | Speed | Segment Start Time | Speed |
| 1 | Lawrence Expressway to End of Merge Lane | 0.217 | :: | 0.00 | 17:49:39 | 41.87 | 18:58:46 | 44.48 |
| 2 | End of Merge Lane to Fair Oaks Off-Ramp | 0.439 | :: | 0.00 | 17:49:58 | 46.73 | 18:59:02 | 57.51 |
| 3 | Fair Oaks Off-Ramp to Fair Oaks Bridge | 0.153 | :: | 0.00 | 17:50:31 | 48.75 | 18:59:29 | 62.34 |
| 4 | Fair Oaks Bridge to Fair Oaks On-Ramp | 0.122 | :: | 0.00 | 17:50:42 | 48.93 | 18:59:38 | 60.54 |
| 5 | Fair Oaks On-Ramp to Mathilda Off-Ramp | 0.550 | 17:05:09 | 47.74 | 17:50:50 | 58.57 | 18:59:45 | 59.87 |
| 6 | Mathilda Off-Ramp to Mathilda On-Ramp | 0.167 | 17:05:28 | 46.34 | 17:51:24 | 59.28 | 19:00:17 | 60.77 |
| 7 | Mathilda On-Ramp to Mathilda Off-Ramp | 0.028 | 17:05:40 | 43.50 | 17:51:34 | 57.17 | 19:00:27 | 62.14 |
| 8 | Mathilda Off-Ramp to SR 237 WB Off-Ramp | 0.432 | 17:05:43 | 50.52 | 17:51:35 | 45.65 | 19:00:28 | 59.46 |
| 9 | SR 237 WB Off-Ramp to Part-way to Ellis Street | 0.457 | 17:06:13 | 47.24 | 17:52:09 | 22.19 | 19:00:54 | 48.05 |

Source: Fehr & Peers, November 2013.

US 101 Southbound AM - Mixed Flow Lanes

| Segment ID | Segment Location | Distance (miles) | Travel Time Run 1 | | Travel Time Run 2 | | Travel Time Run 3 | |
|------------|---|------------------|--------------------|-------|--------------------|-------|--------------------|-------|
| | | | Segment Start Time | Speed | Segment Start Time | Speed | Segment Start Time | Speed |
| 1 | SR 237 WB Off-Ramp to SR 237 WB On-Ramp | 0.137 | 8:00:06 | 53.09 | 8:35:19 | 57.94 | 9:06:37 | 61.87 |
| 2 | SR 237 WB On-Ramp to Mathilda Off-Ramp | 0.198 | 8:00:15 | 52.82 | 8:35:27 | 59.76 | 9:06:44 | 62.91 |
| 3 | Mathilda Off-Ramp to Mathilda On-Ramp | 0.123 | 8:00:28 | 54.84 | 8:35:39 | 60.89 | 9:06:56 | 62.76 |
| 4 | Mathilda On-Ramp to Mathilda On-Ramp | 0.175 | 8:00:36 | 58.18 | 8:35:46 | 58.52 | 9:07:02 | 61.35 |
| 5 | Mathilda On-Ramp to Fair Oaks Off-Ramp | 0.530 | 8:00:47 | 57.39 | 8:35:57 | 59.34 | 9:07:13 | 62.61 |
| 6 | Fair Oaks Off-Ramp to Fair Oaks On-Ramp | 0.135 | 8:01:20 | 55.92 | 8:36:29 | 60.43 | 9:07:43 | 61.60 |
| 7 | Fair Oaks On-Ramp to Fair Oaks Off-Ramp | 0.026 | 8:01:28 | 54.68 | 8:36:37 | 57.17 | 9:07:50 | 62.14 |
| 8 | Fair Oaks Off-Ramp to Fair Oaks On-Ramp | 0.137 | 8:01:30 | 54.61 | 8:36:38 | 55.79 | 9:07:52 | 56.48 |
| 9 | Fair Oaks On-Ramp to Half-way to Lawrence Expressway | 0.332 | 8:01:39 | 51.90 | 8:36:47 | 52.96 | 9:08:01 | 46.01 |
| 10 | Half-way to Lawrence Expressway to Lawrence Expressway Off-Ramp | 0.315 | 8:02:02 | 49.06 | 8:37:09 | 54.21 | 9:08:26 | 52.20 |

Source: Fehr & Peers, November 2013.

US 101 Southbound PM - Mixed Flow Lanes

| Segment ID | Segment Location | Distance (miles) | Travel Time Run 1 | | Travel Time Run 2 | | Travel Time Run 3 | |
|------------|---|------------------|--------------------|-------|--------------------|-------|--------------------|-------|
| | | | Segment Start Time | Speed | Segment Start Time | Speed | Segment Start Time | Speed |
| 1 | SR 237 WB Off-Ramp to SR 237 WB On-Ramp | 0.137 | 17:12:08 | 9.19 | 18:00:22 | 14.89 | 18:44:50 | 35.23 |
| 2 | SR 237 WB On-Ramp to Mathilda Off-Ramp | 0.198 | 17:12:54 | 11.16 | 18:00:47 | 7.01 | 18:45:03 | 32.31 |
| 3 | Mathilda Off-Ramp to Mathilda On-Ramp | 0.123 | 17:13:52 | 14.27 | 18:02:24 | 7.01 | 18:45:25 | 8.12 |
| 4 | Mathilda On-Ramp to Mathilda On-Ramp | 0.175 | 17:14:21 | 16.50 | 18:03:20 | 7.81 | 18:46:13 | 13.90 |
| 5 | Mathilda On-Ramp to Fair Oaks Off-Ramp | 0.530 | 17:14:57 | 14.86 | 18:04:38 | 14.39 | 18:46:54 | 19.95 |
| 6 | Fair Oaks Off-Ramp to Fair Oaks On-Ramp | 0.135 | 17:16:58 | 12.66 | 18:06:42 | 11.89 | 18:48:26 | 9.93 |
| 7 | Fair Oaks On-Ramp to Fair Oaks Off-Ramp | 0.026 | 17:17:35 | 21.75 | 18:07:20 | 7.83 | 18:49:11 | 5.01 |
| 8 | Fair Oaks Off-Ramp to Fair Oaks On-Ramp | 0.137 | 17:17:39 | 18.26 | 18:07:30 | 12.54 | 18:49:26 | 10.00 |
| 9 | Fair Oaks On-Ramp to Half-way to Lawrence Expre | 0.332 | 17:18:05 | 16.42 | 18:08:07 | 14.22 | 18:50:11 | 19.25 |
| 10 | Half-way to Lawrence Expressway to Lawrence Exp | 0.315 | 17:19:13 | 31.86 | 18:09:25 | 33.97 | 18:51:09 | 30.77 |

Source: Fehr & Peers, November 2013.

US 101 Travel Time Runs
(INRIX data in November 2013)

Speed on US-101 between De La Cruz Blvd and Ellis St

Averaged by 15 minutes for November 19, 2013, for November 20, 2013, and for November 21, 2013

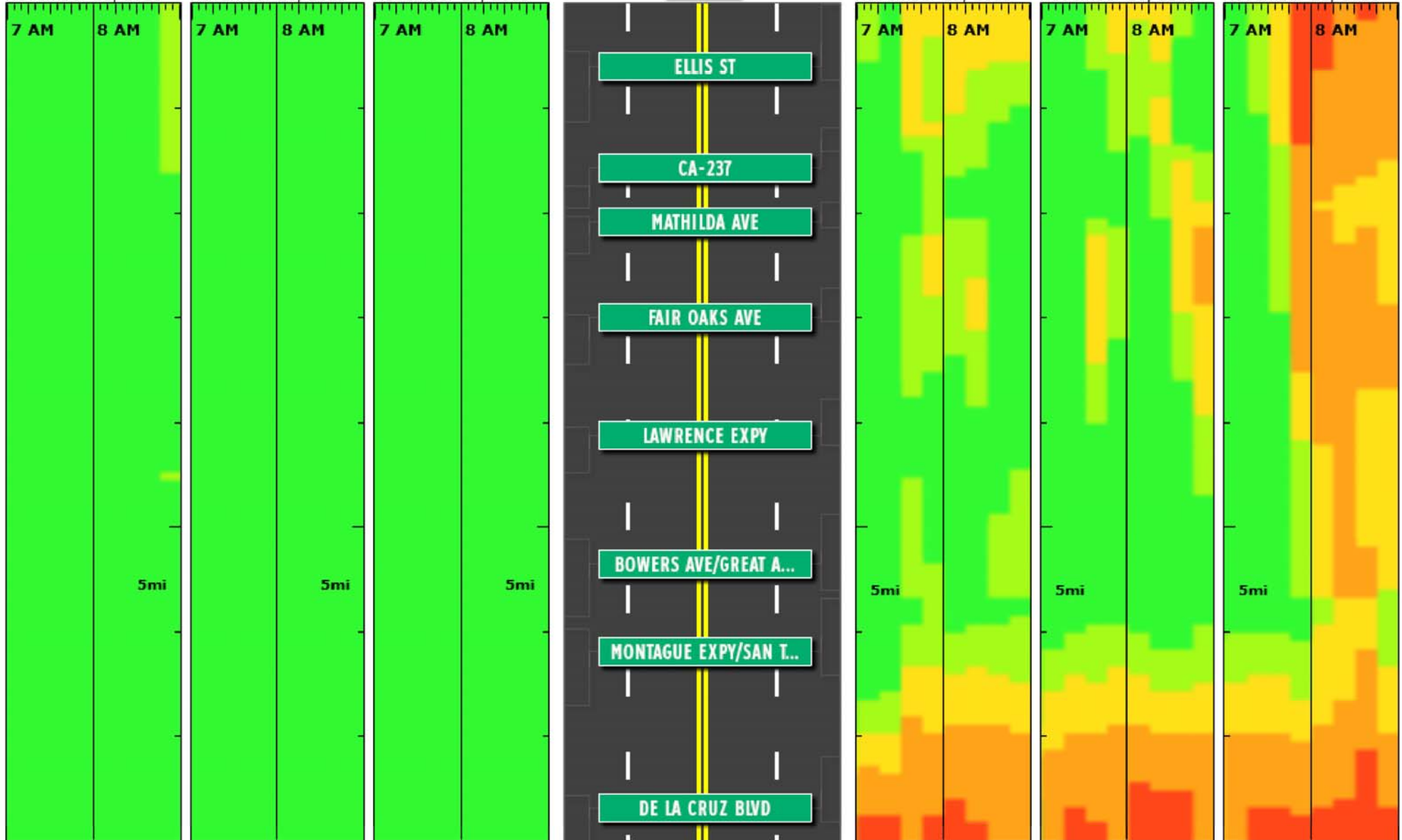


Southbound

Northbound

November 21, 2013 November 20, 2013 November 19, 2013

November 19, 2013 November 20, 2013 November 21, 2013



The raw measured speed.



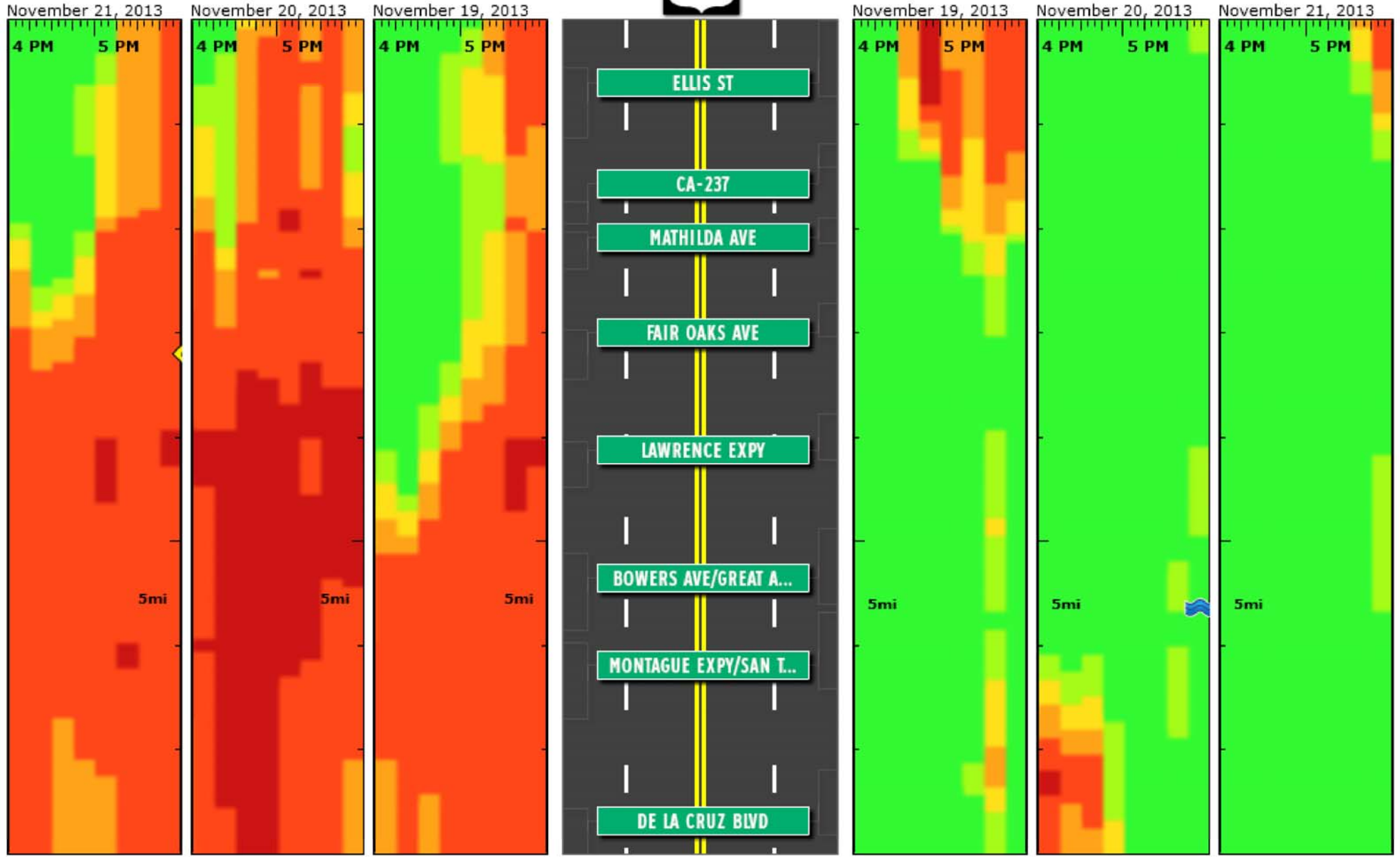
Speed on US-101 between De La Cruz Blvd and Ellis St

Averaged by 15 minutes for November 19, 2013, for November 20, 2013, and for November 21, 2013

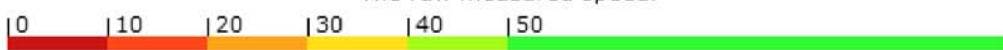


↓ Southbound ↓

↑ Northbound ↑



The raw measured speed.



APPENDIX C – SR 237 TRAVEL TIME RUN INFORMATION



SR 237 Travel Time Runs

(Phase II of the SR 237 Existing Conditions Report -
Chapter 4.3)

4.3 SR-237 Mainline Bottleneck Output Flows

Mainline counts were gathered locations just downstream of existing bottleneck locations. A summary of these counts are shown in **Table 4-6**.

Table 4-6 SR-237 Bottleneck Output Flow Summary

| Description | Flow Volume (vph) | | | | | | | | | |
|---|-------------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|-------------|
| | AM | | | | | PM | | | | |
| | 6 to 7 | 7 to 8 | 8 to 9 | 9 to 10 | 10 to 11 | 3 to 4 | 4 to 5 | 5 to 6 | 6 to 7 | 7 to 8 |
| Westbound SR-237 | | | | | | | | | | |
| Between N. 1 st Street Off-ramp and On-ramp (GP Lanes) | 3847 | 3967 | 4188 | 3919 | 3519 | 2806 | 3206 | 3449 | 2956 | 2200 |
| Between N. 1 st Street Off-ramp and On-ramp (HOV Lane – Just downstream of the EL Double White Line End) | 961 | 1529 | 1540 | 1614 | 1528 | 286 | 326 | 619 | 506 | 511 |
| Total Mainline (Between N. 1st St Off-ramp and On-ramp) | 4808 | 5496 | 5728 | 5533 | 5047 | 3092 | 3532 | 4068 | 3462 | 2711 |
| Between Lawrence Expy On-ramp and Fair Oaks On-ramp (GP Lanes) | 2663 | 3090 | 3167 | 2513 | 2281 | 2452 | 2813 | 3066 | 2564 | 1929 |
| Between Lawrence Expy On-ramp and Fair Oaks On-ramp (HOV Lane) | 707 | 1150 | 988 | 1292 | 1194 | 390 | 442 | 744 | 698 | 818 |
| Total Mainline (Between Lawrence Expy On-ramp and Fair Oaks On-ramp) | 3370 | 4240 | 4155 | 3805 | 3475 | 2842 | 3255 | 3810 | 3262 | 2747 |
| Eastbound SR-237 | | | | | | | | | | |
| Between Mathilda Ave On-ramp and Lawrence Expy Off-ramp (GP Lanes) | 1391 | 2823 | 3666 | 2813 | 2168 | 2977 | 2966 | 2810 | 2406 | 2068 |
| Between Mathilda Ave On-ramp and Lawrence Expy Off-ramp (HOV Lane) | 62 | 172 | 380 | 1189 | 662 | 573 | 687 | 991 | 778 | 712 |
| Total Mainline (Between Mathilda Ave On-ramp and Lawrence Expy Off-ramp) | 1453 | 2995 | 4046 | 4002 | 2830 | 3550 | 3652 | 3800 | 3184 | 2780 |
| Between Zanker Rd Off-ramp and On-ramp (GP Lanes) | 1493 | 2744 | 3404 | 2587 | 2042 | 3294 | 3627 | 3549 | 3437 | 3162 |
| Between Zanker Rd Off-ramp and On-ramp (HOV Lane – Just upstream of the EL Double White Line Start) | 75 | 203 | 313 | 874 | 581 | 1135 | 1400 | 1547 | 1353 | 1576 |
| Total Mainline (Between Zanker Rd Off-ramp and On-ramp) | 1568 | 2947 | 3717 | 3461 | 2623 | 4429 | 5027 | 5096 | 4790 | 4738 |

Source: VTA and DKS Associates, 2013

4.4 Truck Percentage

Truck percentage data for SR-237 within the study area were derived from the 2011 Caltrans Annual Average Daily Truck Traffic Database. The data represent the number of trucks as a percentage of the vehicle composition for certain locations. This report listed average daily truck percentage at one location in the study area, as shown in **Table 4-7**.

Table 4-7 Truck Percentage

| Locations | Truck Percentage | Year Verified/Estimated |
|-------------------------------|------------------|-------------------------|
| SR-237 at Jct. Rte. 101 | 4% | 2001V |
| Jct. Rte. 880, Nimitz Freeway | 6% | 1998V |

Source: Caltrans Annual Average Daily Truck Traffic 2011

4.5 Corridor Segment Travel Times

Corridor travel times were extracted from tachograph runs conducted in March to May 2013.

Table 4-8 and **Table 4-9** summarize the average general purpose lane travel times in each direction during the respective peak periods. The travel time results for the HOV lane are presented in **Table 4-10** and **Table 4-11**. The speed versus distance plots for each travel time run are provided in **Appendix B**. **Figure 4-5** and **Figure 4-6** show the average travel time by hour, direction and facility type along SR-237.



Table 4-8 Southbound I-880/Westbound SR-237 General Purpose Lane Average Travel Times

| Segment | Distance (miles) | AM (Minutes) | | | | | PM (Minutes) | | | | |
|---|------------------|--------------|------|------|------|-------|--------------|-----|------|------|-----|
| | | 6-7 | 7-8 | 8-9 | 9-10 | 10-11 | 3-4 | 4-5 | 5-6 | 6-7 | 7-8 |
| Southbound I-880 to Westbound SR-237 | | | | | | | | | | | |
| Mission Blvd (SR-262) to Dixon Landing Rd | 2.17 | 2.1 | 2.2 | 2.7 | 2.8 | 2.1 | 2.0 | 2.1 | 2.1 | 2.1 | 2.0 |
| Dixon Landing Rd to McCarthy Blvd | 2.29 | 3.9 | 5.4 | 6.6 | 8.3 | 3.1 | 2.2 | 2.3 | 2.3 | 2.3 | 2.3 |
| McCarthy Blvd to Zanker Rd | 0.94 | 2.1 | 3.5 | 4.0 | 3.1 | 2.4 | 0.9 | 0.9 | 1.6 | 1.0 | 0.9 |
| Zanker Rd to N 1st St** | 1.08 | 1.3 | 1.5 | 1.6 | 1.5 | 1.5 | 1.0 | 1.1 | 1.3 | 1.5 | 1.1 |
| N. 1st St to Great America Pkwy | 1.01 | 1.2 | 1.2 | 1.2 | 1.1 | 1.1 | 0.9 | 1.0 | 1.1 | 1.0 | 0.9 |
| Great America Pkwy to Lawrence Expy | 1.24 | 1.2 | 1.2 | 1.4 | 1.2 | 1.2 | 0.7 | 0.8 | 1.3 | 0.6 | 0.6 |
| Lawrence Expy to Fair Oaks Ave | 0.64 | 0.6 | 0.7 | 0.7 | 0.6 | 0.6 | 0.8 | 0.8 | 1.2 | 1.0 | 0.9 |
| Fair Oaks Ave to Mathilda Ave | 0.96 | 0.9 | 1.2 | 0.8 | 0.9 | 0.9 | 0.8 | 0.8 | 1.8 | 0.9 | 0.8 |
| Mathilda Ave to US-101 | 0.55 | 0.6 | 0.7 | 0.5 | 0.6 | 0.6 | 0.5 | 0.5 | 0.6 | 0.6 | 0.5 |
| Total Travel Time (Mission to Zanker) | 5.4 | 8.2 | 11.1 | 13.3 | 14.1 | 7.6 | 5.1 | 5.3 | 5.9 | 5.4 | 5.3 |
| Total Travel Time (Zanker to Mathilda) | 4.9 | 5.2 | 5.8 | 5.7 | 5.4 | 5.3 | 4.3 | 4.5 | 6.6 | 4.9 | 4.3 |
| Total Travel Time (Mission to Mathilda) | 10.3 | 13.4 | 17.0 | 19.0 | 19.6 | 12.9 | 9.4 | 9.8 | 12.5 | 10.3 | 9.6 |
| Westbound Calaveras Blvd | | | | | | | | | | | |
| I-680 to S Milpitas Blvd | 0.69 | 1.6 | 1.5 | N/A | 3.0 | 3.6 | | | | | |
| S Milpitas Blvd to N Abel St | 0.49 | 0.8 | 2.0 | N/A | 3.8 | 3.3 | | | | | |
| N Abel St to I-880 | 0.60 | 1.8 | 5.2 | N/A | 4.9 | 3.8 | | | | | |
| I-880 to N McCarthy Blvd (via McCarthy Off/On) | 0.40 | 1.2 | 1.1 | 3.2 | 2.1 | 1.4 | | | | | |
| N. McCarthy Blvd to Zanker Rd (via McCarthy Off/On) | 0.94 | 1.7 | 2.8 | 2.6 | 3.2 | 1.9 | | | | | |
| I-880 to N McCarthy Blvd (via SR-237) | 0.40 | 1.2 | 2.1 | 4.2 | 3.7 | 2.8 | | | | | |
| McCarthy Blvd to Zanker Rd (via SR-237) | 0.94 | 2.3 | 3.1 | 4.0 | 3.0 | 2.7 | | | | | |
| Total Travel Time (I-680 to Zanker via HOV bypass/McCarthy Off/On) | 3.12 | 7.1 | 12.6 | N/A | 17.0 | 14.1 | | | | | |
| Total Travel Time (I-680 to Zanker via SR-237) | 3.12 | 7.6 | 14.2 | N/A | 18.5 | 16.0 | | | | | |

Source: DKS Associates, 2013



Table 4-9 Eastbound SR-237/Northbound I-880 General Purpose Lane Average Travel Times

| Segment | Distance (miles) | AM (Minutes) | | | | | PM (Minutes) | | | | |
|--|------------------|--------------|-------------|-------------|-------------|-------------|--------------|-------------|-------------|-------------|-------------|
| | | 6-7 | 7-8 | 8-9 | 9-10 | 10-11 | 3-4 | 4-5 | 5-6 | 6-7 | 7-8 |
| Eastbound SR-237 to Northbound I-880 | | | | | | | | | | | |
| US-101 to Mathilda Ave | 0.54 | 0.5 | 0.5 | 0.7 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 |
| Mathilda Ave to Fair Oaks Ave | 0.95 | 0.8 | 0.9 | 1.1 | 0.9 | 0.9 | 0.9 | 0.9 | 1.1 | 1.0 | 0.9 |
| Fair Oaks Ave to Lawrence Expy | 0.63 | 0.6 | 0.6 | 0.6 | 0.6 | 0.6 | 0.5 | 0.6 | 0.7 | 0.7 | 0.5 |
| Lawrence Expy to Great American Pkwy | 1.25 | 1.2 | 1.2 | 1.4 | 1.2 | 1.2 | 1.7 | 2.3 | 4.3 | 5.7 | 1.2 |
| Great American Pkwy to N. 1st St. | 1.06 | 1.0 | 1.1 | 1.1 | 1.1 | 1.1 | 1.9 | 2.4 | 3.0 | 4.1 | 1.3 |
| N. 1st St. to Zanker Rd | 1.07 | 1.1 | 1.1 | 1.2 | 1.1 | 1.0 | 1.6 | 1.7 | 2.4 | 2.7 | 1.4 |
| Zanker Rd to N. McCarthy Blvd | 0.97 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.4 | 1.2 | 1.3 | 1.2 | 1.0 |
| N. McCarthy Blvd to Dixon Landing Rd | 2.36 | 2.3 | 2.2 | 2.3 | 2.2 | 2.2 | 8.9 | 9.8 | 10.0 | 5.8 | 2.6 |
| Dixon Landing Rd to Mission Blvd (SR-262) | 2.19 | 2.1 | 2.0 | 2.1 | 2.1 | 2.0 | 2.6 | 6.5 | 6.6 | 7.3 | 2.2 |
| Total Travel Time (Mathilda to Zanker) | 4.96 | 4.7 | 4.9 | 5.4 | 4.8 | 4.8 | 6.6 | 7.9 | 11.5 | 14.2 | 5.3 |
| Total Travel Time (Zanker to Mission) | 5.51 | 5.3 | 5.2 | 5.4 | 5.2 | 5.2 | 12.9 | 17.4 | 17.9 | 14.4 | 5.8 |
| Total Travel Time (Mathilda to Mission) | 10.47 | 10.0 | 10.1 | 10.7 | 10.0 | 10.1 | 19.5 | 25.3 | 29.5 | 28.6 | 11.1 |
| Eastbound Calaveras Blvd | | | | | | | | | | | |
| N. McCarthy Blvd to I-880 | 0.40 | 0.6 | 0.6 | 0.6 | 0.7 | 0.8 | | | | | |
| I-880 to N Abel St | 0.61 | 1.3 | 1.8 | 0.9 | 1.2 | 1.6 | | | | | |
| N Abel St to S Milpitas Blvd | 0.48 | 0.7 | 0.6 | 0.6 | 0.3 | 1.1 | | | | | |
| S Milpitas Blvd to I-680 | 0.62 | 0.5 | N/A | N/A | N/A | 0.6 | | | | | |
| Total Travel Time (McCarthy to I-680) | 2.11 | 3.1 | N/A | N/A | N/A | 4.2 | | | | | |

Source: DKS Associates, 2013

Table 4-10 Southbound I-880/Westbound SR-237 HOV/EL Average Travel Times

| Segment | Distance (miles) | AM (Minutes) | | | | | PM (Minutes) | | | | |
|--|------------------|--------------|------------|------------|-------------|------------|--------------|------------|------------|------------|------------|
| | | 6-7 | 7-8 | 8-9 | 9-10 | 10-11 | 3-4 | 4-5 | 5-6 | 6-7 | 7-8 |
| Southbound I-880 to Westbound SR-237 | | | | | | | | | | | |
| Mission Blvd (SR-262) to Dixon Landing Rd | 2.17 | 1.9 | 2.0 | 2.3 | 2.6 | 1.9 | 1.9 | 1.8 | 1.9 | 1.8 | 1.8 |
| Dixon Landing Rd to McCarthy Blvd | 2.33 | 2.2 | 2.3 | 2.5 | 2.8 | 3.0 | 2.1 | 2.1 | 2.1 | 2.1 | 2.0 |
| McCarthy Blvd to Zanker Rd | 0.94 | 1.0 | 1.1 | 1.2 | 1.2 | 1.2 | 0.8 | 0.9 | 0.9 | 0.9 | 0.8 |
| Zanker Rd to N 1st St | 1.10 | 1.0 | 1.2 | 1.2 | 1.2 | 1.1 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| N. 1st St. to Great America Pkwy | 1.02 | 0.9 | 1.0 | 1.0 | 0.9 | 0.9 | 0.9 | 0.9 | 0.9 | 1.0 | 0.9 |
| Great America Pkwy to Lawrence Expy | 1.28 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 |
| Lawrence Expy to N. Fair Oaks Ave | 0.64 | 0.6 | 0.6 | 0.6 | 0.5 | 0.5 | 0.6 | 0.5 | 0.6 | 0.6 | 0.6 |
| HOV/EL Total Travel Time (Mission to Zanker) | 5.44 | 5.0 | 5.4 | 6.0 | 6.6 | 6.1 | 4.8 | 4.7 | 4.8 | 4.8 | 4.7 |
| HOV/EL Total Travel Time (Zanker to Fair Oaks) | 4.04 | 3.6 | 3.8 | 3.8 | 3.7 | 3.6 | 3.5 | 3.5 | 3.6 | 3.7 | 3.5 |
| HOV/EL Total Travel Time (Mission to Fair Oaks) | 9.48 | 8.6 | 9.2 | 9.8 | 10.2 | 9.8 | 8.3 | 8.2 | 8.4 | 8.5 | 8.2 |

Source: DKS Associates, 2013

Table 4-11 Eastbound SR-237/Northbound I-880 HOV/EL Average Travel Times

| Segment | Distance (miles) | AM (Minutes) | | | | | PM (Minutes) | | | | |
|--|------------------|--------------|------------|------------|------------|------------|--------------|-------------|-------------|-------------|------------|
| | | 6-7 | 7-8 | 8-9 | 9-10 | 10-11 | 3-4 | 4-5 | 5-6 | 6-7 | 7-8 |
| Eastbound SR-237 to Northbound I-880 | | | | | | | | | | | |
| N. Fair Oaks Ave to Lawrence Expy | 0.63 | 0.4 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.6 | 0.7 | 0.7 | 0.5 |
| Lawrence Expy to Great America Pkwy | 1.24 | 0.8 | 1.1 | 1.1 | 1.1 | 1.0 | 1.2 | 1.3 | 1.4 | 1.5 | 1.1 |
| Great America Pkwy to N. 1st St. | 1.08 | 0.7 | 0.9 | 0.9 | 0.9 | 0.9 | 1.1 | 1.1 | 1.2 | 1.4 | 1.1 |
| N. 1st St to Zanker Rd | 1.08 | 0.7 | 0.9 | 0.9 | 0.9 | 0.9 | 1.1 | 1.3 | 1.2 | 1.3 | 1.2 |
| Zanker Rd to N. McCarthy Blvd | 0.94 | 0.6 | 0.8 | 0.8 | 0.8 | 0.8 | 1.0 | 1.0 | 1.0 | 1.0 | 0.9 |
| N. McCarthy Blvd to Dixon Landing Rd | 2.33 | 1.6 | 2.1 | 2.1 | 2.1 | 2.5 | 2.3 | 3.0 | 5.8 | 3.6 | 2.2 |
| Dixon Landing Rd to Mission Blvd (SR-262) | 2.19 | 1.4 | 1.9 | 1.9 | 1.8 | 2.0 | 2.0 | 3.3 | 4.3 | 4.0 | 2.0 |
| HOV/EL Total Travel Time (Fair Oaks to Zanker) | 4.0 | 2.5 | 3.4 | 3.4 | 3.4 | 3.4 | 4.0 | 4.3 | 4.5 | 5.0 | 3.9 |
| HOV/EL Total Travel Time (Zanker to Mission) | 5.5 | 3.6 | 4.8 | 4.9 | 4.7 | 5.3 | 5.2 | 7.3 | 11.0 | 8.5 | 5.0 |
| HOV/EL Total Travel Time (Fair Oaks to Mission) | 10.4 | 7.0 | 9.1 | 9.4 | 9.0 | 9.6 | 10.1 | 12.5 | 16.6 | 14.5 | 9.9 |

Source: DKS Associates, 2013

Figure 4-5 AM Peak Period Average Travel Time

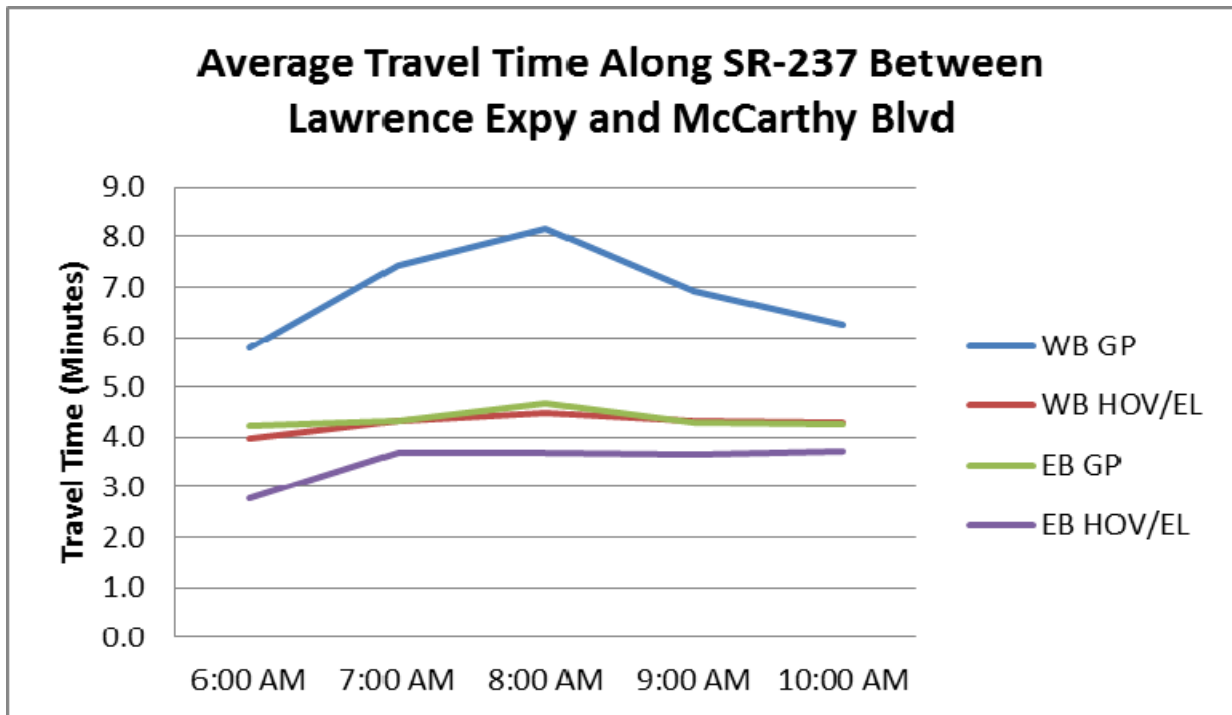
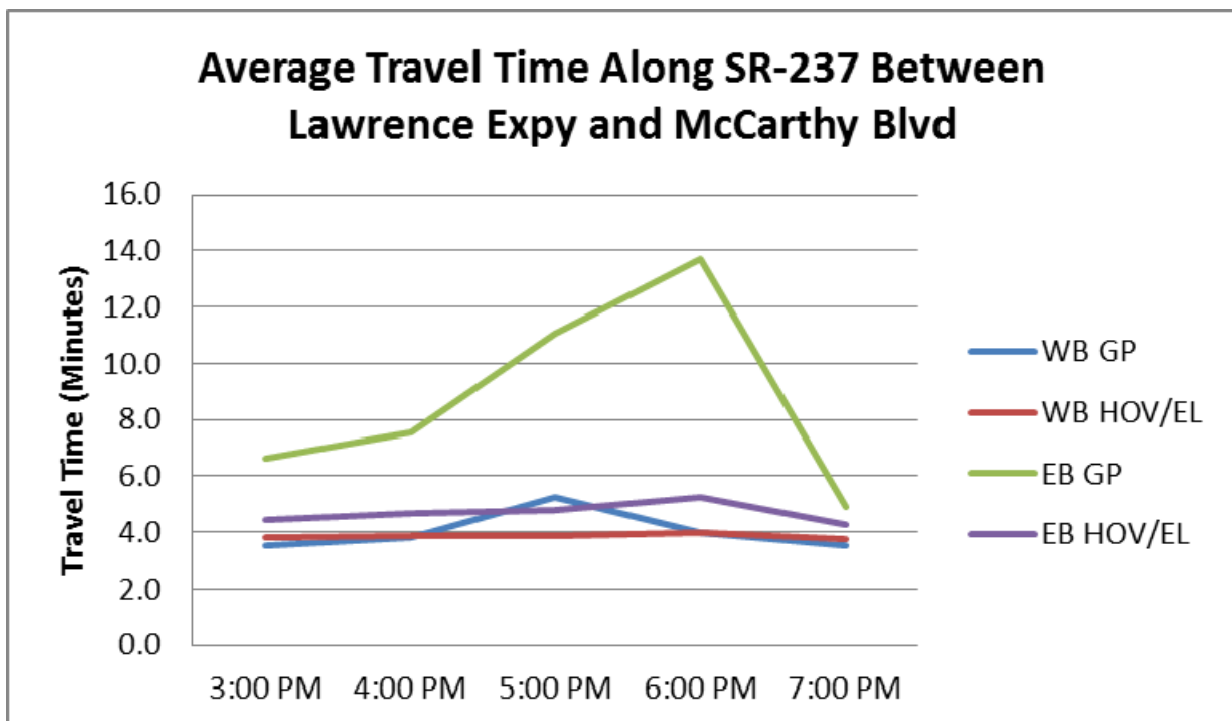


Figure 4-6 PM Peak Period Average Travel Time



4.6 Existing Congestion Patterns and Bottlenecks

Bottleneck locations within the study area were compiled from a variety of sources including, Spring 2013 Tach Runs, INRIX historical speeds (See **Appendix C**), and DKS field observations. The primary source used for this effort was the Spring 2013 Tach Run data as it also provides travel time data that may be used in the model calibration process. In general, the bottleneck locations are consistent; but the queue lengths and durations can vary between the sources.

4.6.1 Existing AM Peak Congestion Pattern

A review of available INRIX historical speed sampling revealed that the current bottleneck for the westbound direction within the study corridor is in the area between the Zanker Rd on-ramp to the N. 1st Street off-ramp. Field observations and travel time runs conducted in Spring 2013 confirm that this segment is the bottleneck location. This bottleneck forms at approximately 6:30 AM and does not dissipate until nearly 10:45 AM. During the peak hour, the back of the resulting queue reaches well beyond the interchange with I-880 along Calaveras Road to the east and general purpose lanes on I-880 to the north.

Field observations showed some minor congestion in the southbound to westbound HOV lane during the AM peak period. This typically occurred near Calaveras Blvd when the express/HOV lane was adjacent to congested traffic in the mixed flow lanes. This slowing occurred even though the express/HOV lanes are separated by pavement markings. This same area was also a common point of entry for vehicles violating the lane striping and illegally crossing the solid white lines to enter the express/HOV lane. Observations observed that Express/HOV lane users are generally cautious of vehicles entering into the lane and this may explain the slowing through this area.

In the eastbound direction, field observations confirmed that there are no bottlenecks through the study corridor during the AM Peak Period.

Existing AM peak-period bottlenecks and queues are displayed in **Figure 4-7**.

4.6.2 Existing PM Peak Congestion Pattern

In the westbound direction the current bottleneck is in the area between Zanker Rd and McCarthy Blvd. This bottleneck forms at approximately 5:30 PM and dissipates by 6:30 PM. At its peak the queue from this bottleneck spills back to McCarthy Blvd.

In the eastbound direction, the initial bottleneck is located between the Great America On-ramp and the N. 1st Street Off-ramp. This bottleneck begins to form by 4:00 PM and does not dissipate until 7:00 PM. During the peak hour, the back of the resulting queue of this bottleneck reaches as far back as the Fair Oaks Ave Interchange.

For much of the PM peak period, the resulting queue from the initial bottleneck merges with the queue from the next bottleneck which is located between the N. 1st Street on-ramp and the Zanker Rd off-ramp. This bottleneck is fully developed by 4:30 PM and does not dissipate until 7:00 PM. The resulting queue from this bottleneck extends beyond the Great America Interchange and merges with the previous bottleneck.

The next bottleneck is located at the ramp meters at the EB SR-237 to NB-I-880 Connector. This bottleneck is governed by the metering rates at the stop line. This queue develops at approximately 3:00 PM does not extend beyond the McCarthy Blvd interchange.

The westbound express/HOV lanes are generally uncongested during the PM Peak Period.

The speeds in the eastbound HOV lane are faster than the speeds in the mixed flow lanes from Mathilda Ave to Zanker Rd. At Zanker Rd the express/HOV lane separates from the mixed flow lanes and the speeds increase. There is some slowing for the area just before the start of the express lane at Zanker Rd. This could be a result of increased weaving prior to the express lane barrier start.

In the northbound direction along I-880, the bottleneck is located between the Mission Blvd on-ramp and the Fremont Blvd off-ramp. This bottleneck forms by 5:00 PM and does not dissipate until 7 PM. During the peak hour, the back of the resulting queue reaches beyond the SR-237 interchange. This queue sometimes reaches the eastbound to northbound express lane connector. When this occurs, the express lane tolling operations switches to "HOV Only" operation until the queue clears and average speeds in the express lane increases to 45 MPH.

Existing PM peak-period bottlenecks and queues are displayed in **Figure 4-8**.

4.7 Volume Balancing and Demand

A volume balancing and demand estimating exercise was conducted to adjust the volumes entering and exiting the study network. A brief summary of the volume balancing and demand estimating procedure is listed below. The existing AM peak and PM peak demands to be used in the VISSIM operational model are shown in **Appendix D**.

- Conduct a quality check of count data gathered in March and April 2013 to filter out "bad" counts. Caltrans Census was used as a point of comparison to filter the counts as well as to supplement at locations where the March/April count was deemed unreliable.
- Identify locations that was counted in-queue (and therefore does not represent demand) or that was counted under good flowing conditions and represent the true demand. If any location was in-queue, then the extent of the queue was identified to estimate the stored demand. The demand was estimated based on the observed count, its exact location and the extent of the queuing near the count location.
- Demand volumes were then balanced over the five-hour peak period at on and off-ramps.

Legend

- Study Corridor
- Local Roads
- Queue Segment
- Bottleneck Segment
- Queue Segment from US 101

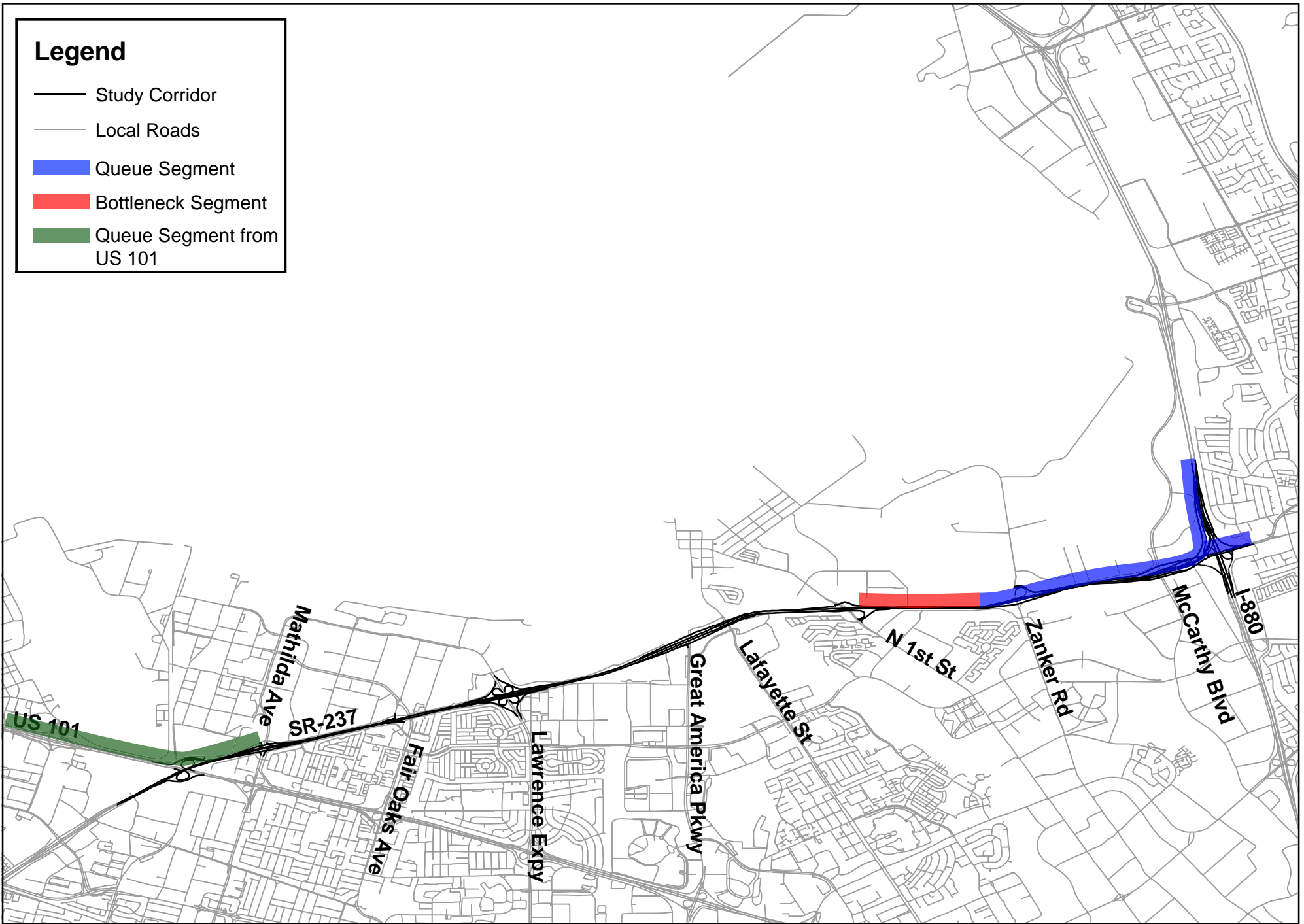


Figure 4-7

SR-237 Congestion Map AM Peak Period

Legend

- Study Corridor
- Local Roads
- Queue Segment
- Bottleneck Segment
- Queue Segment from US 101

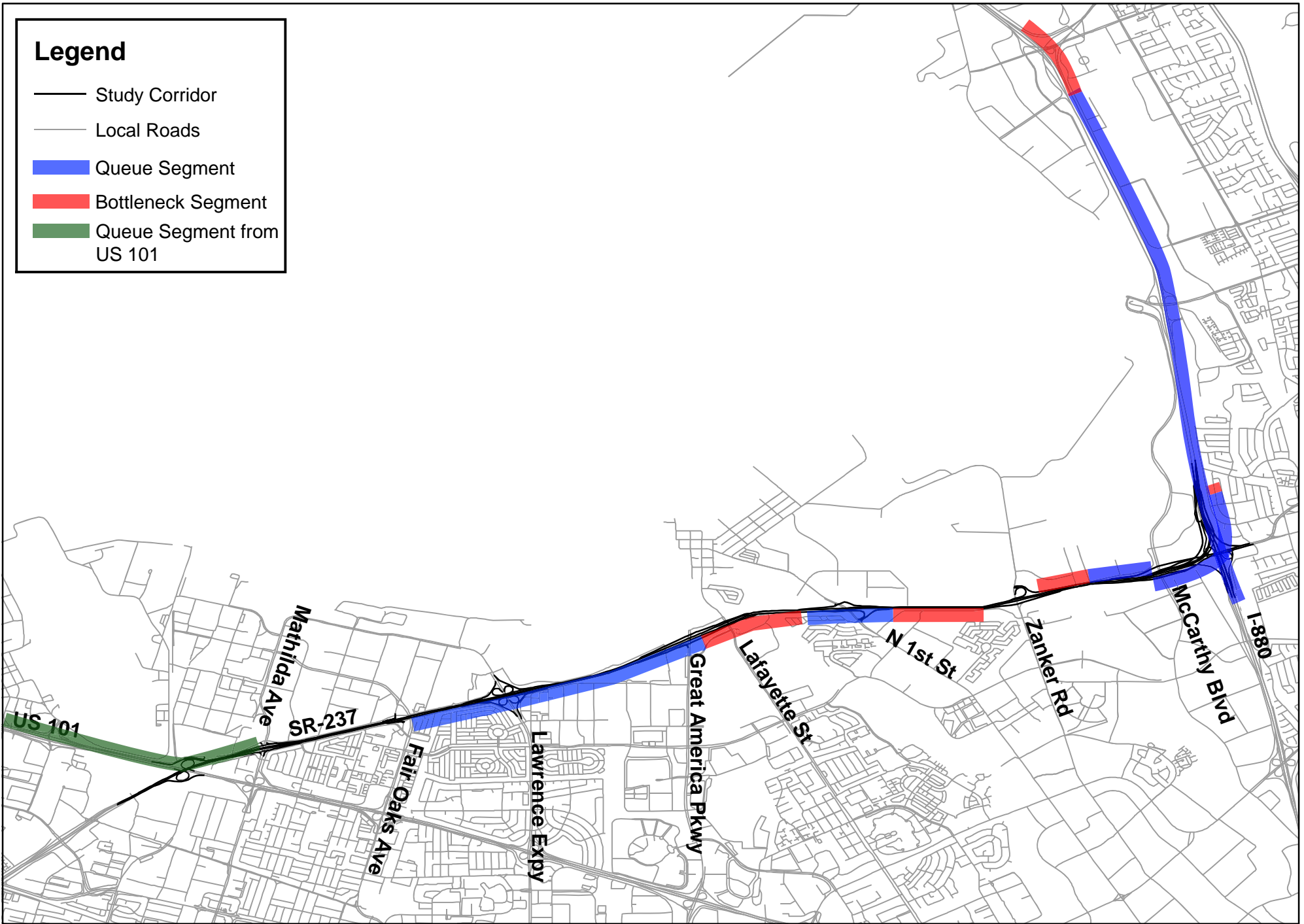
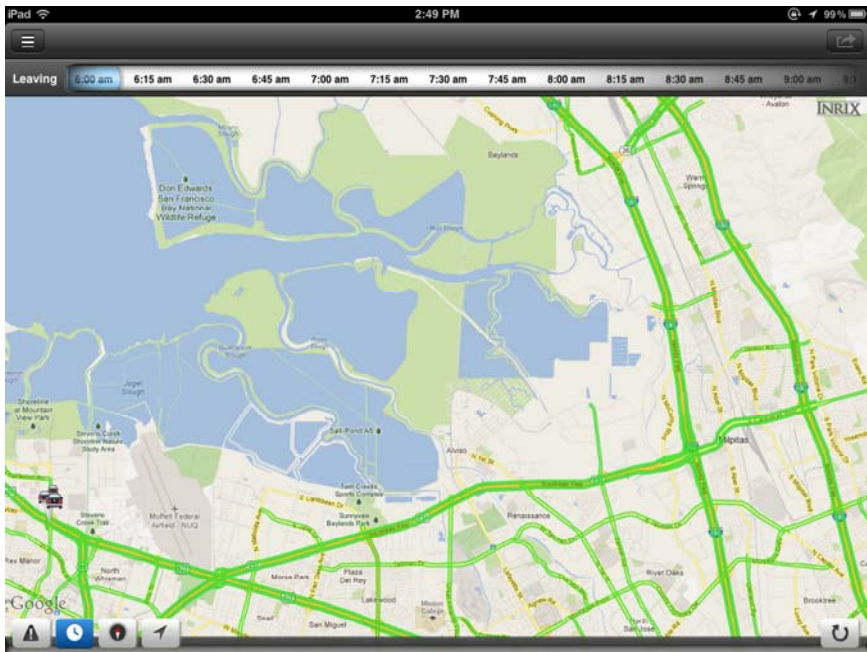


Figure 4-8

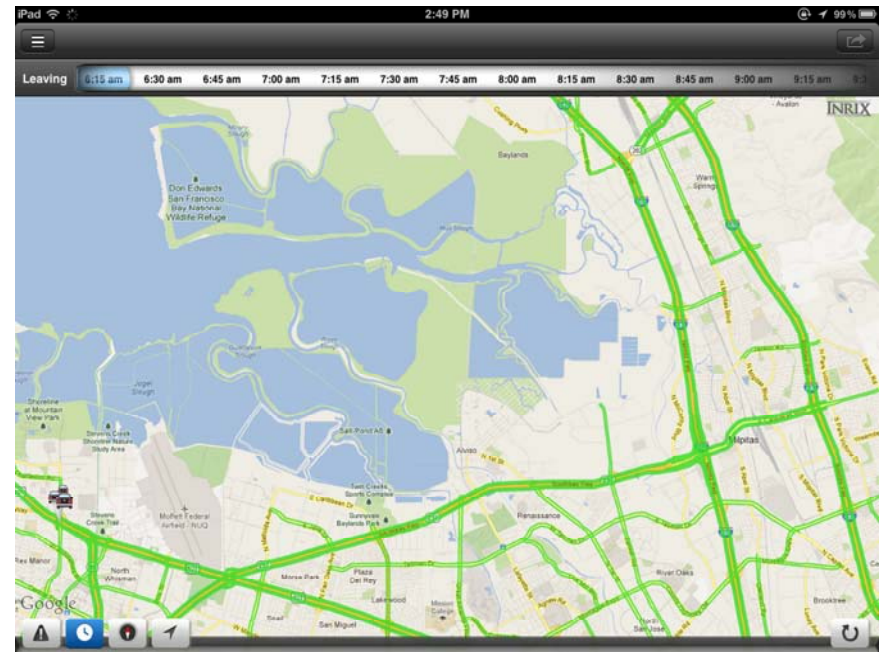
SR-237 Congestion Map PM Peak Period

SR 237 Travel Time Runs

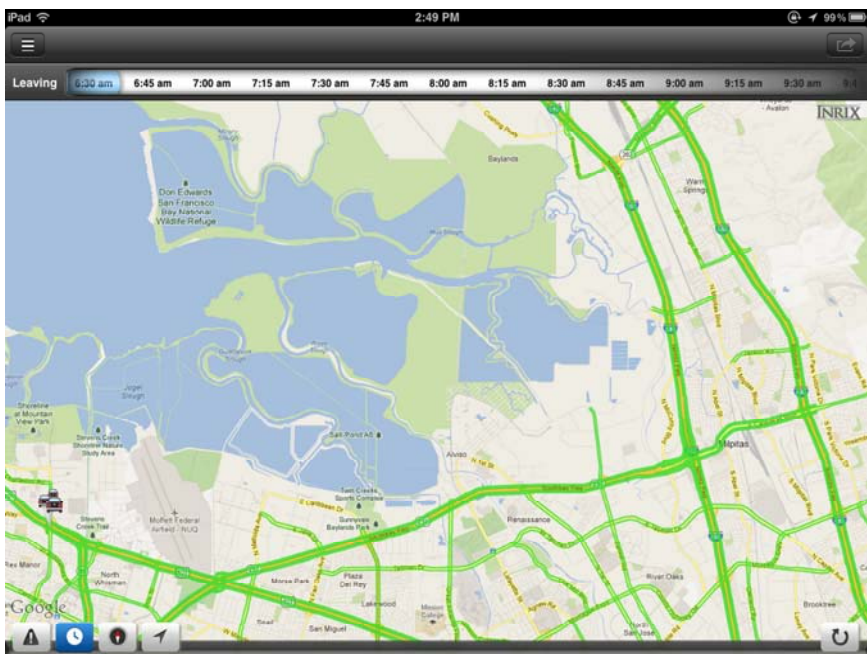
(Phase II of the SR 237 Existing Conditions Report -
Appendix C – INRIX Congestion Maps)



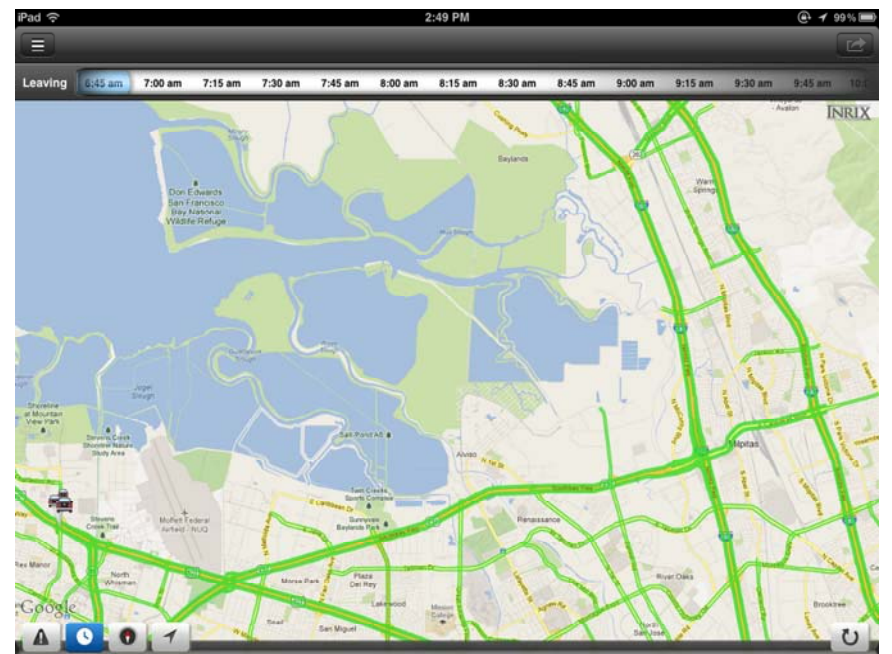
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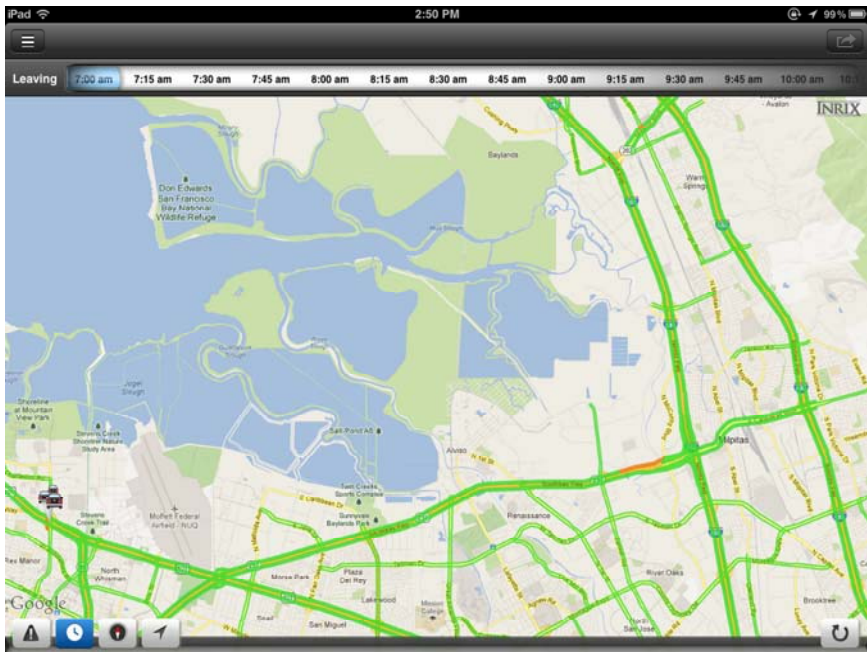
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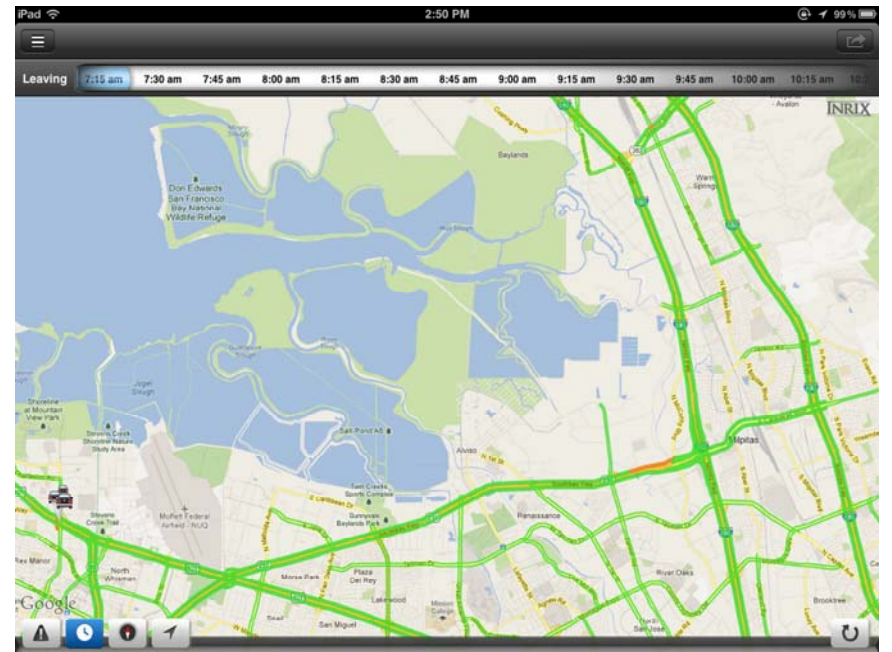
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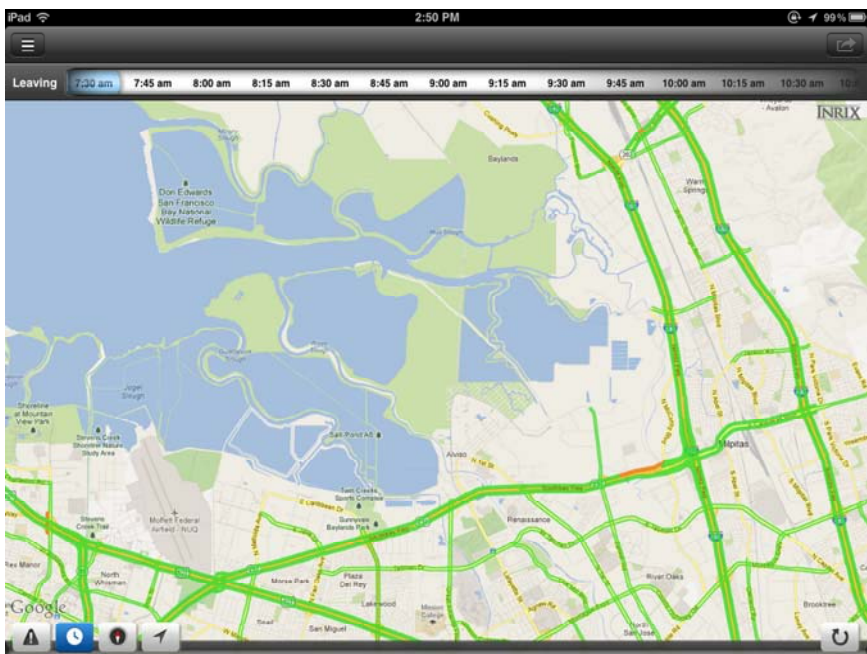
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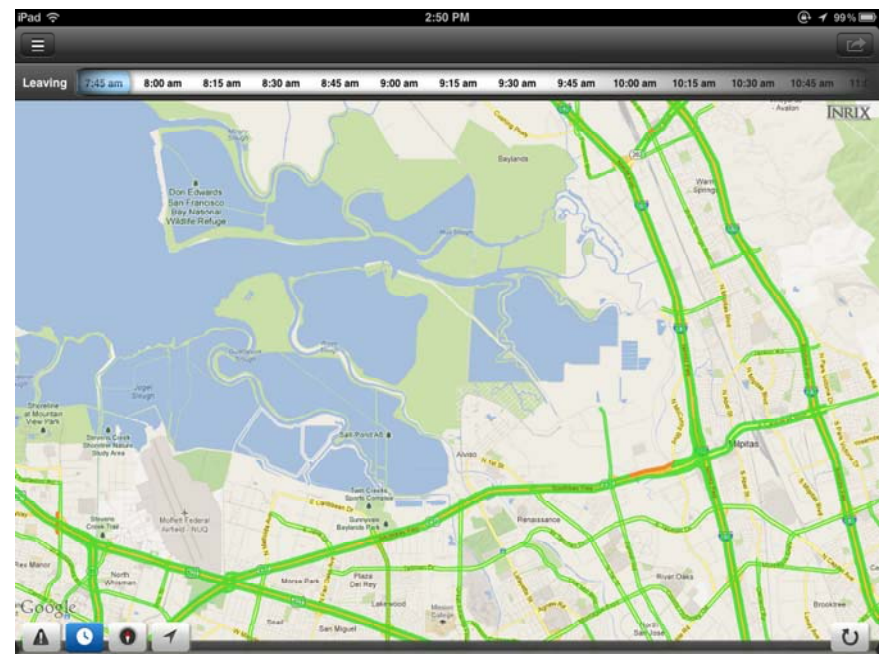
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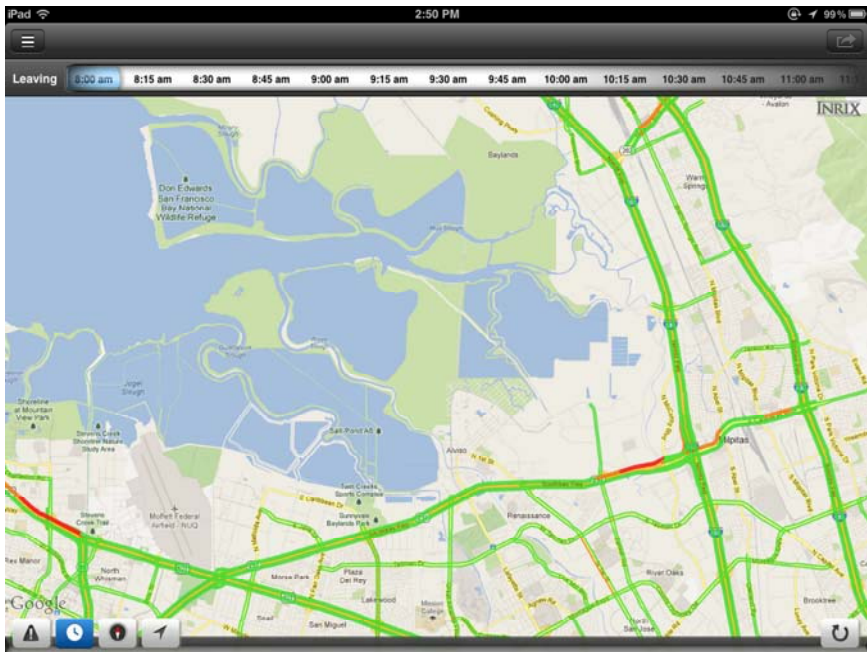
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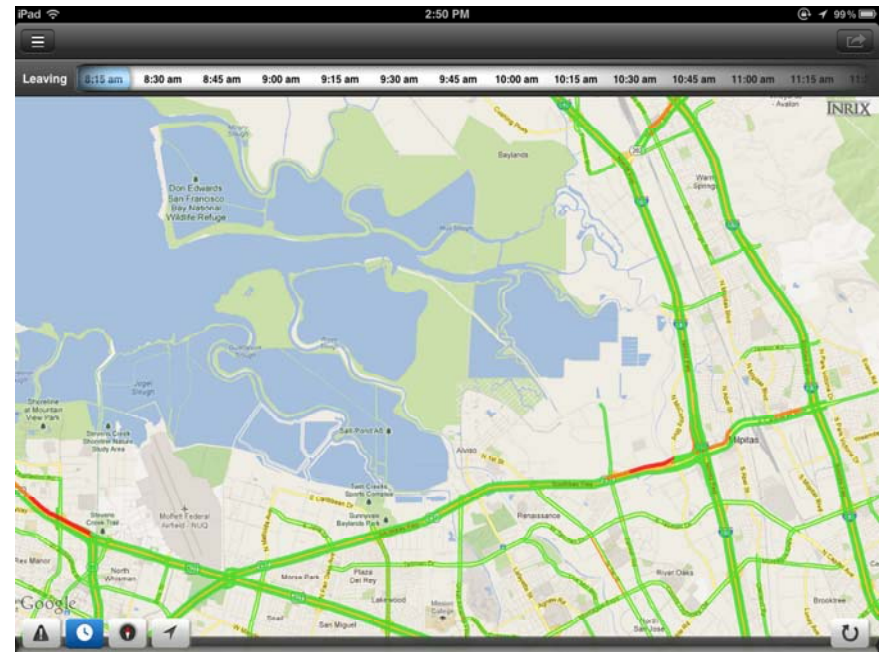
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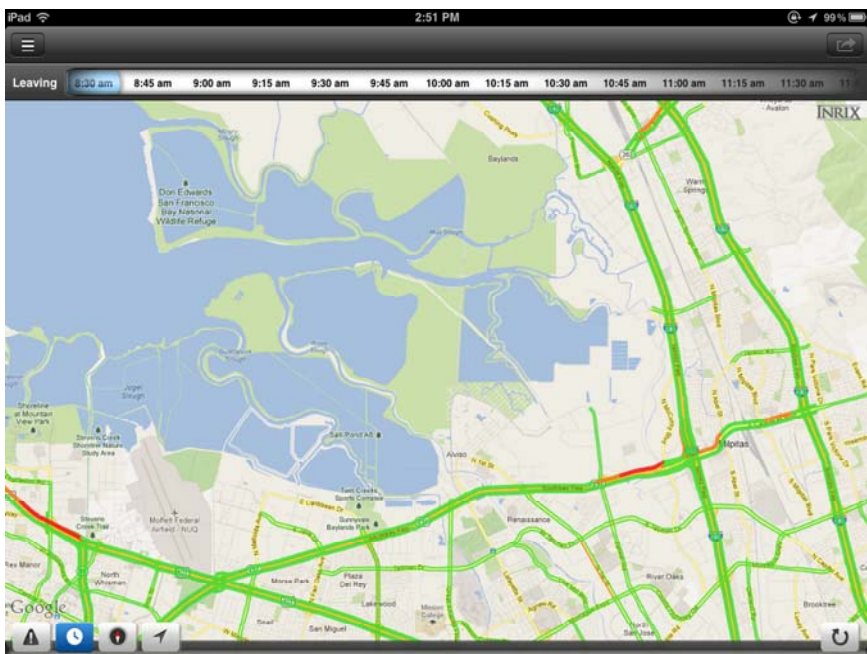
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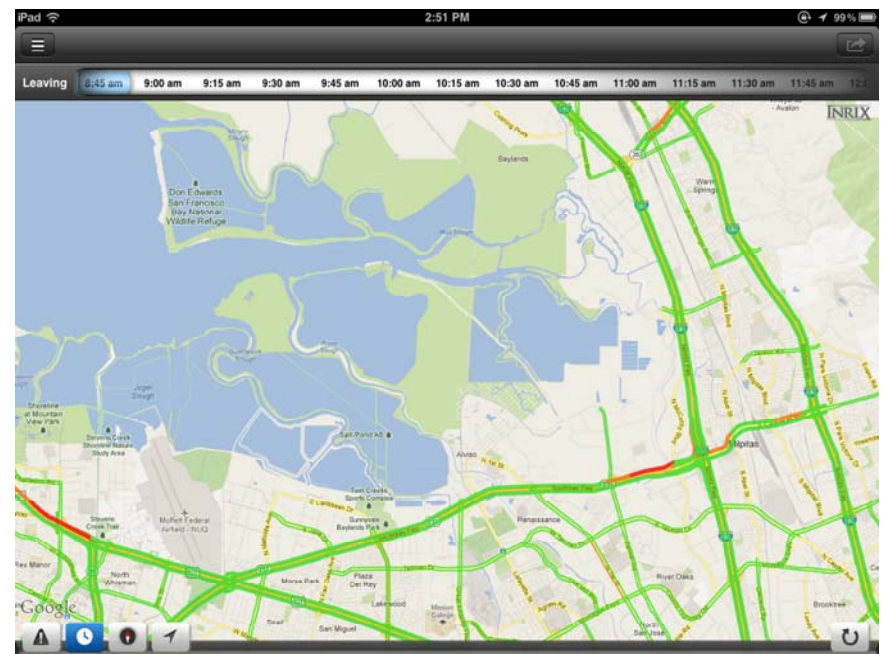
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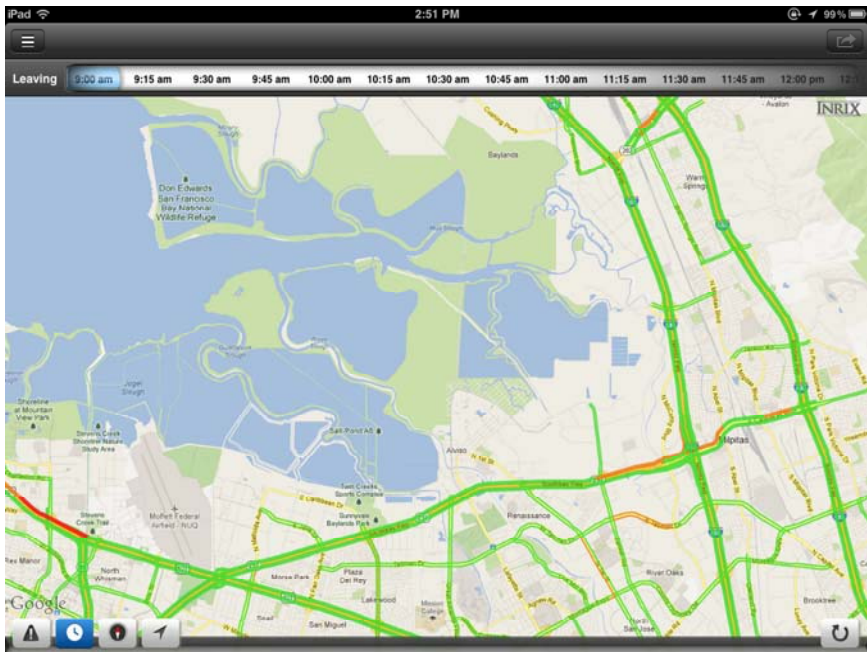
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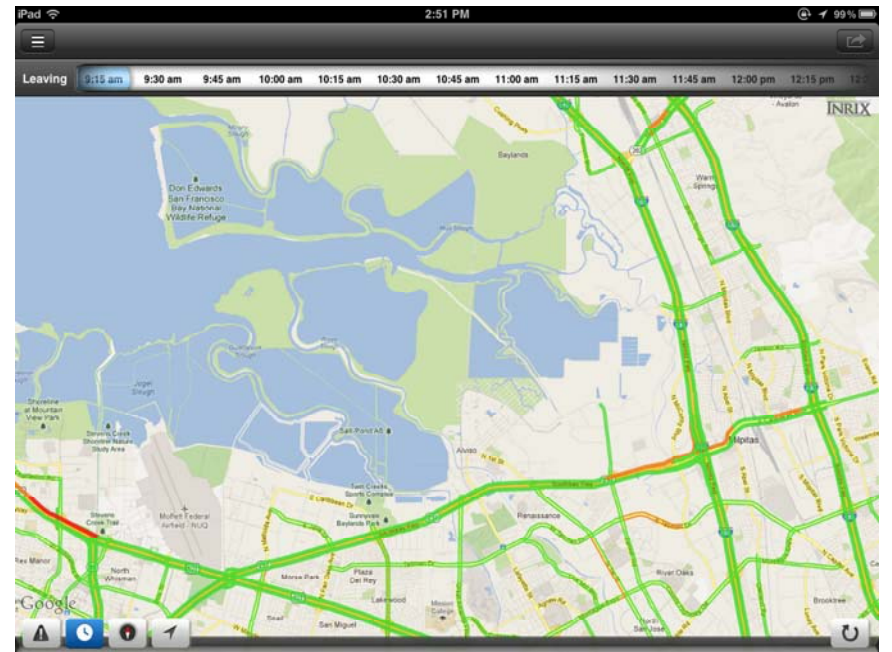
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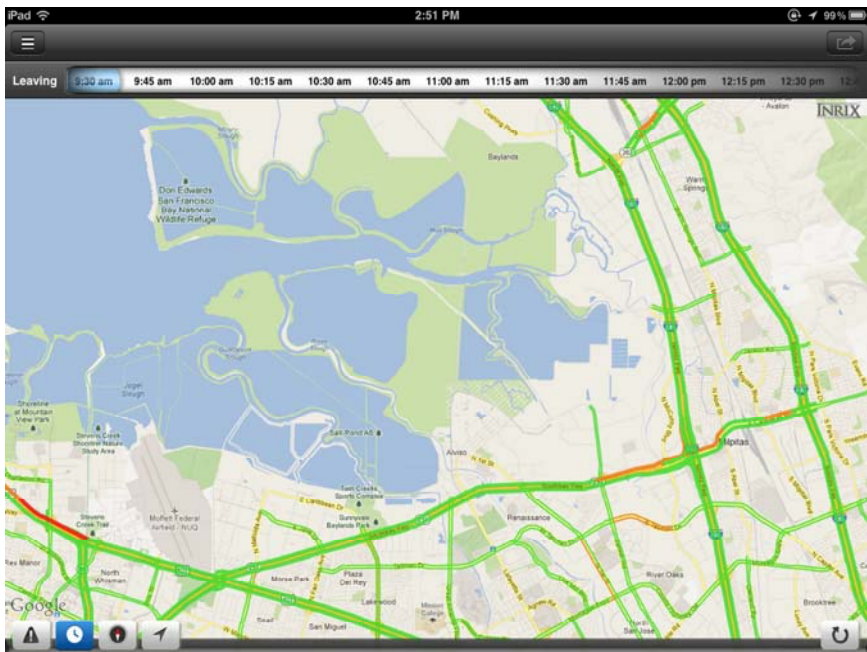
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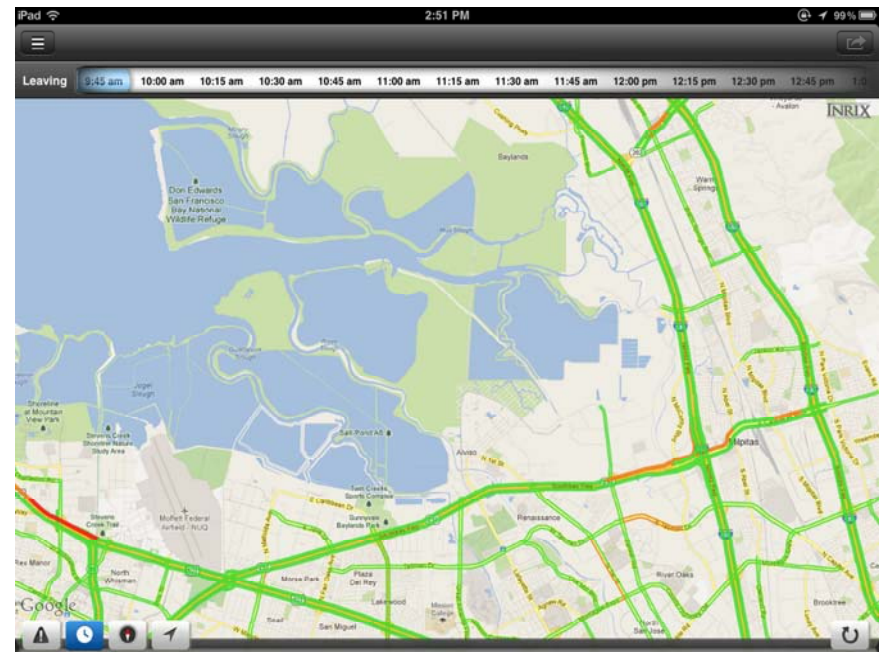
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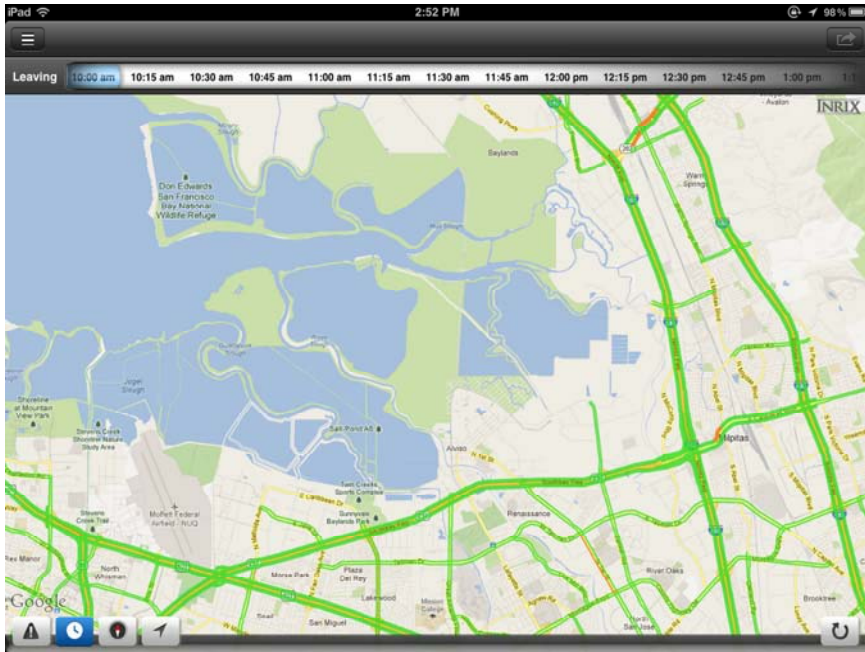
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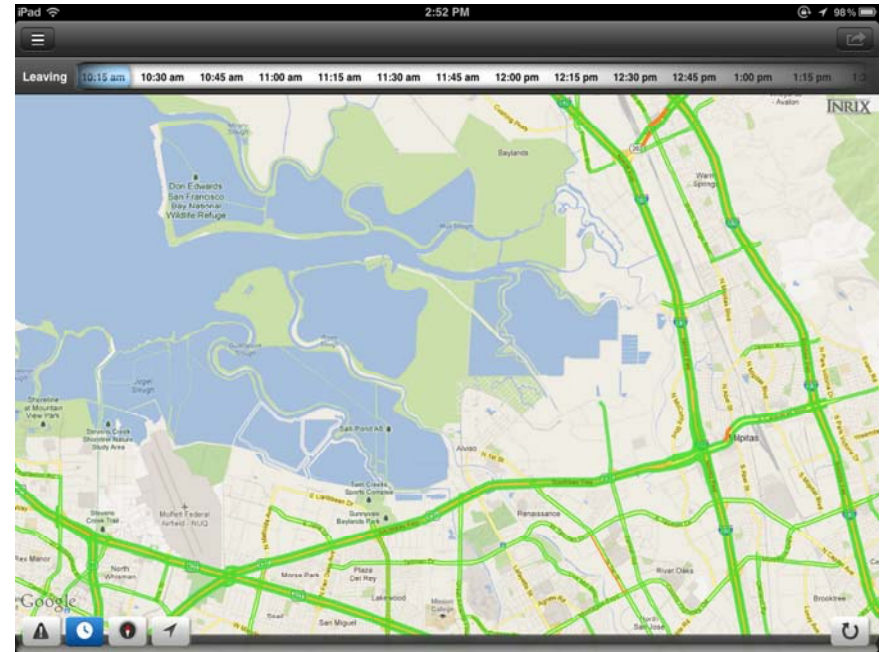
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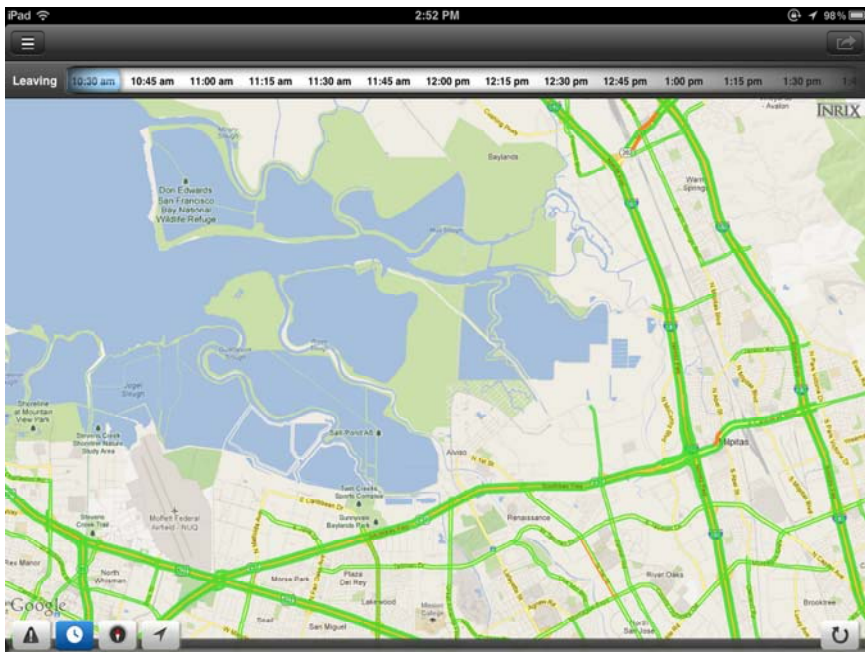
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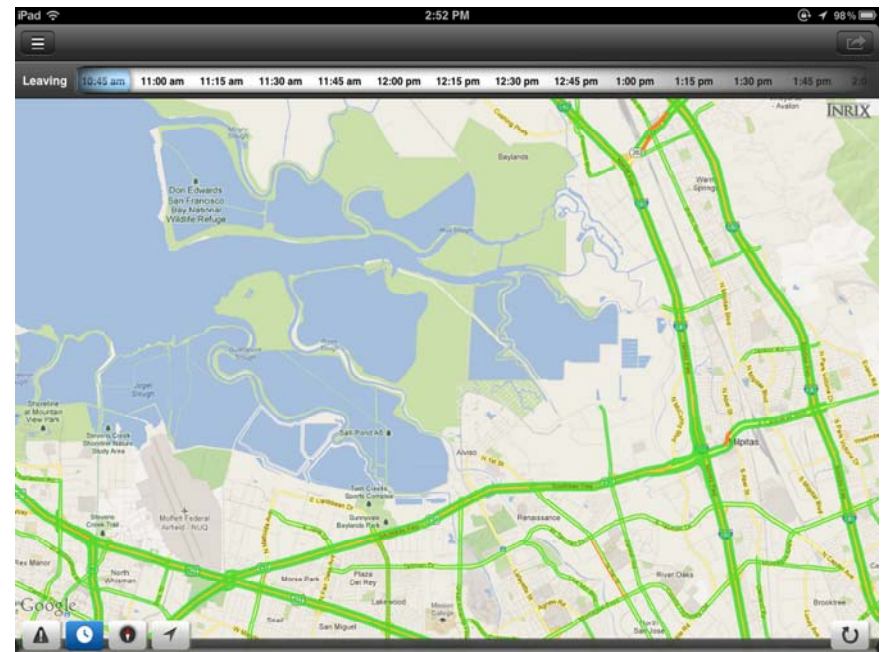
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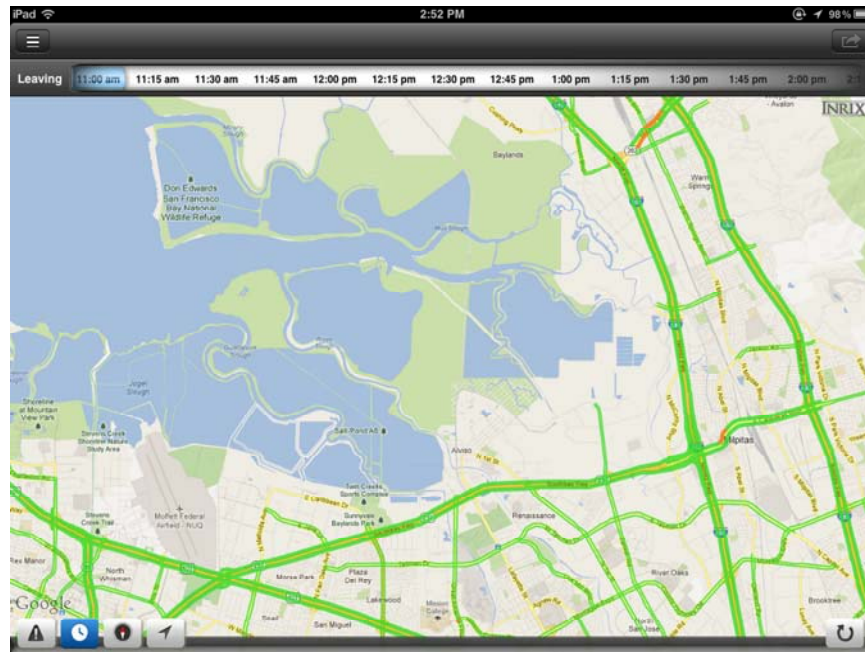
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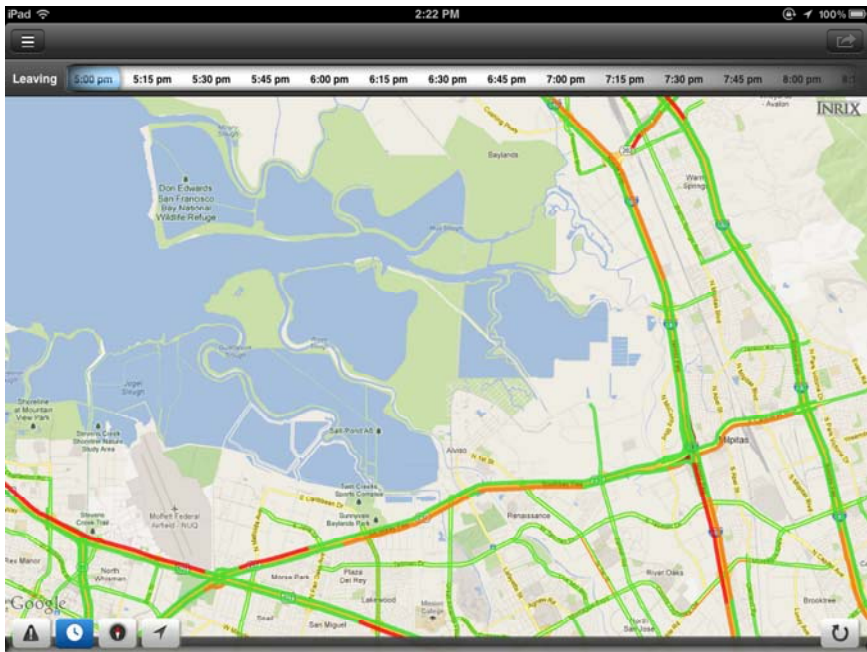
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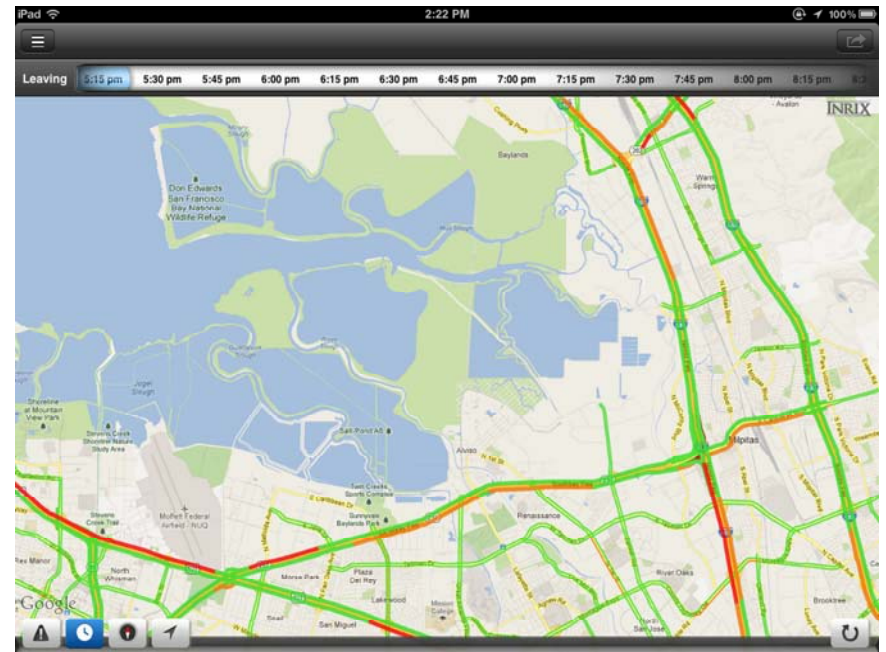
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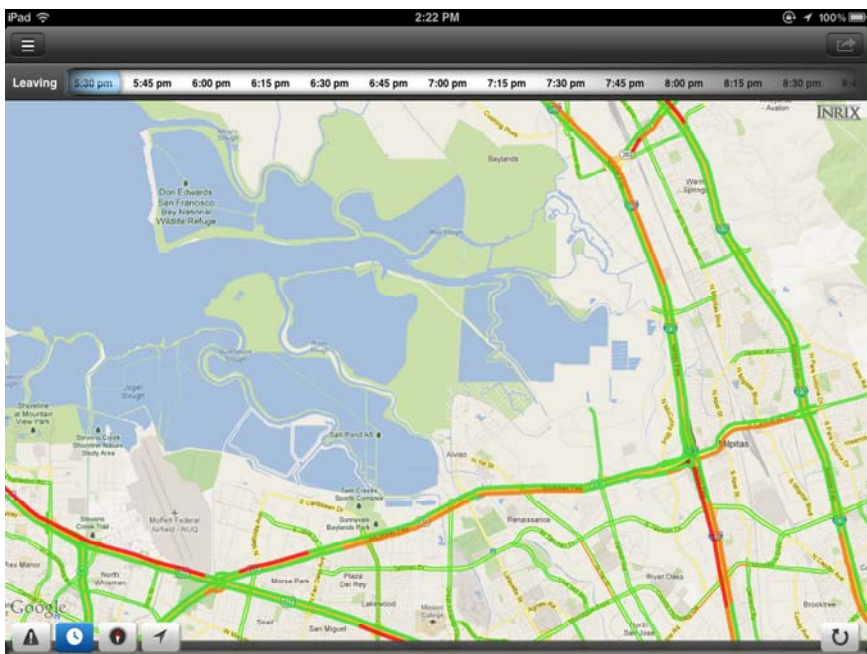
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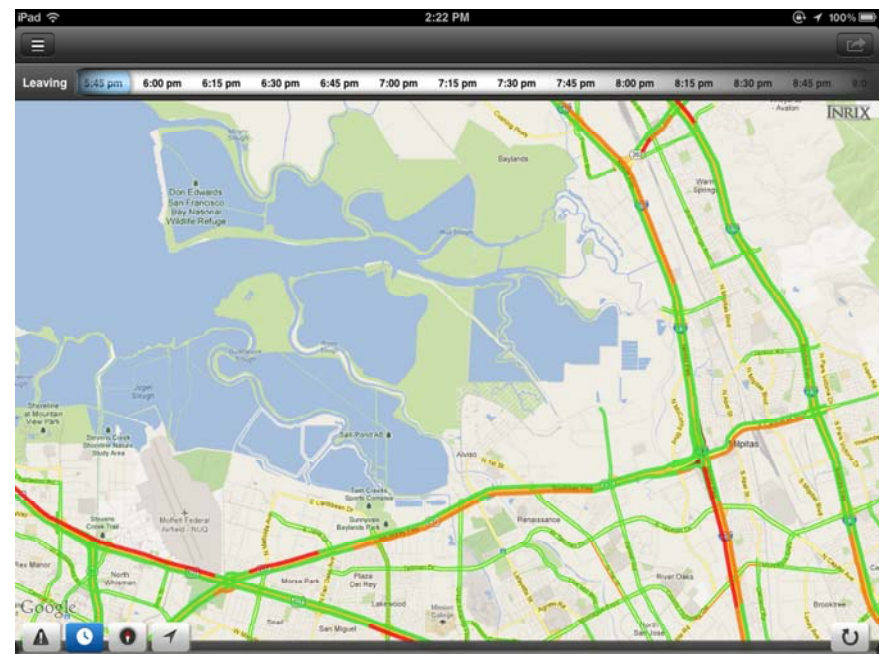
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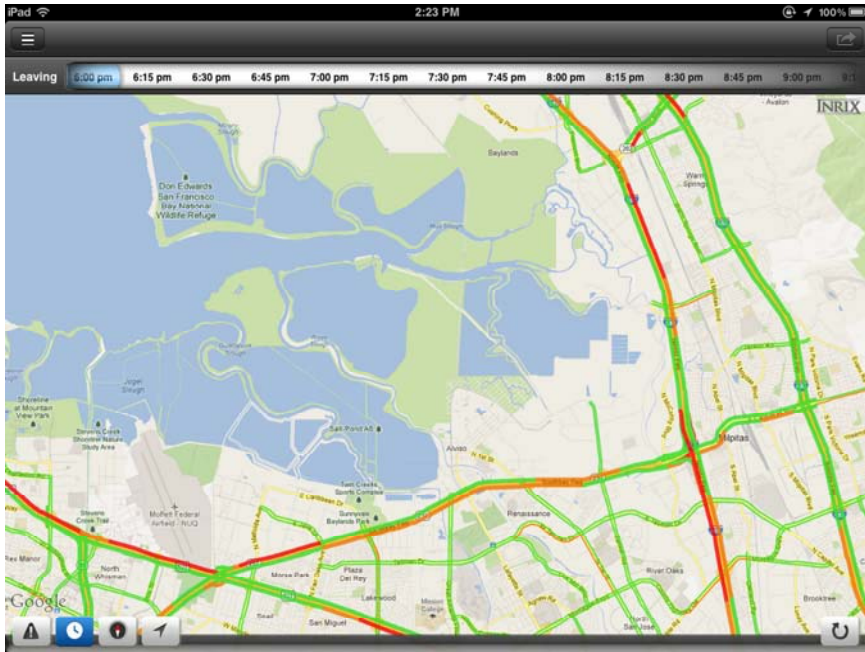
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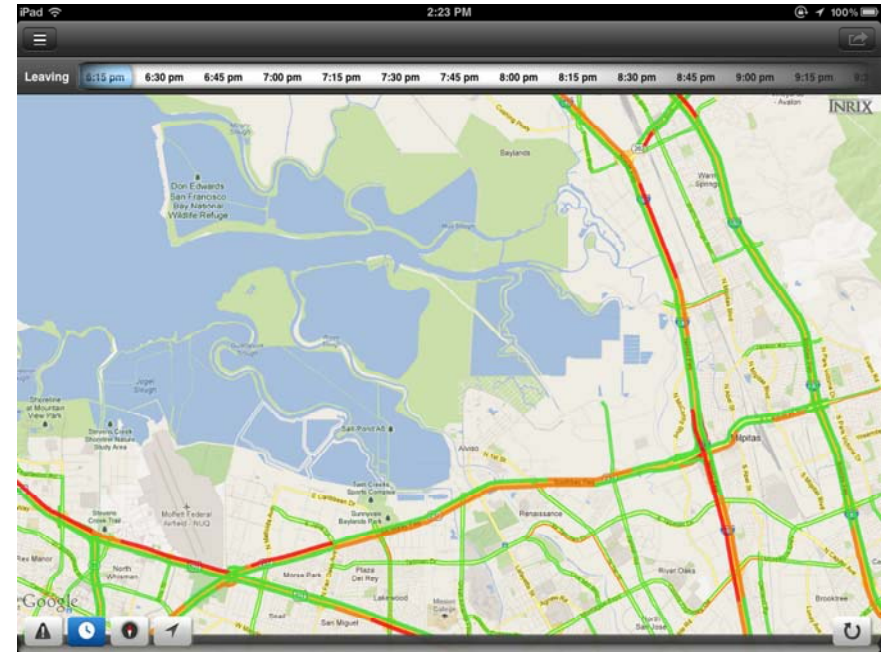
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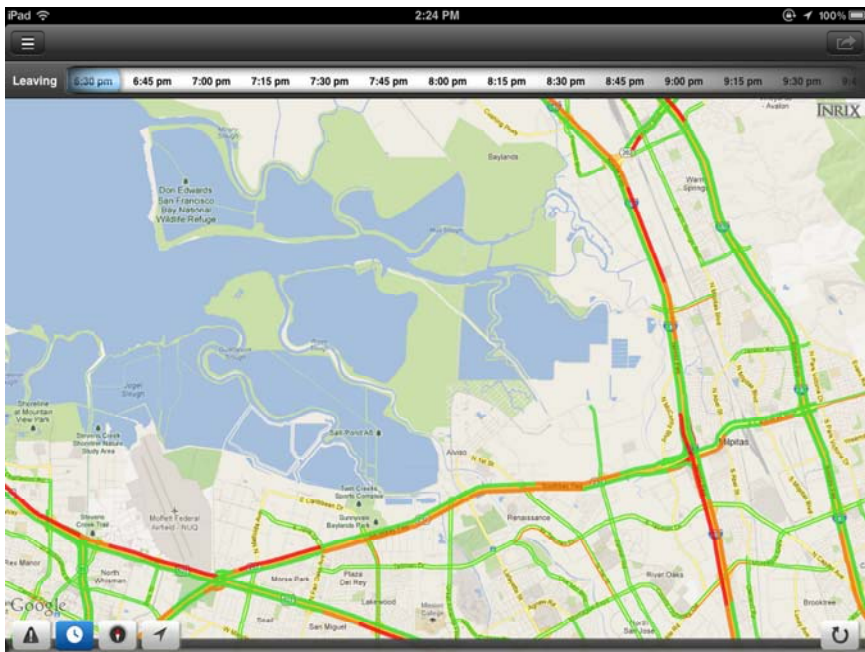
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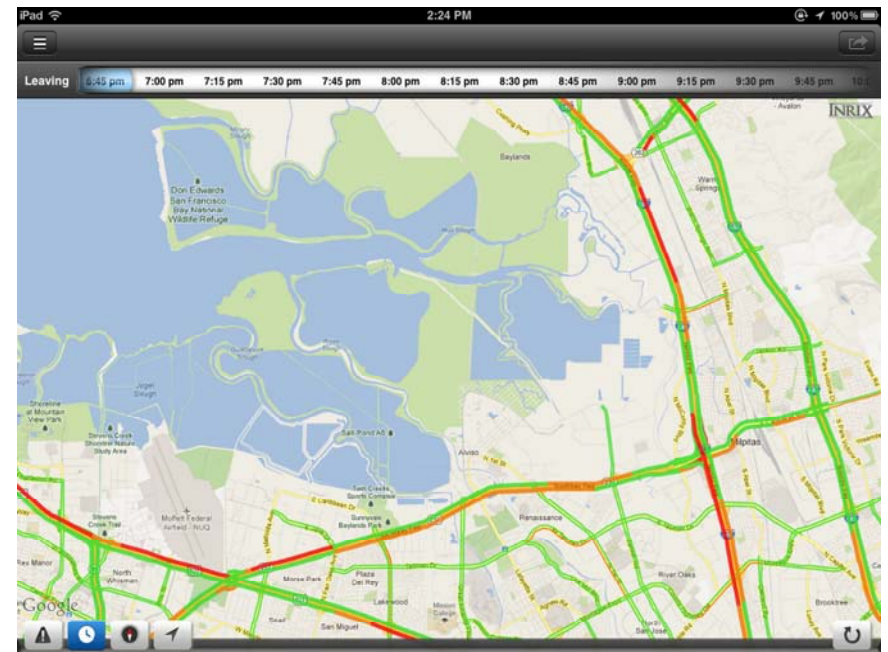
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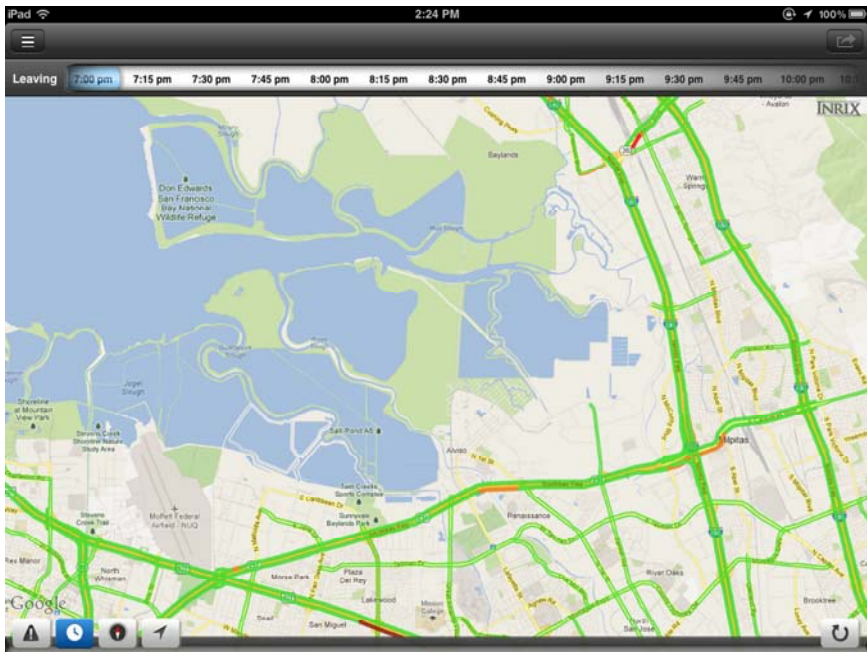
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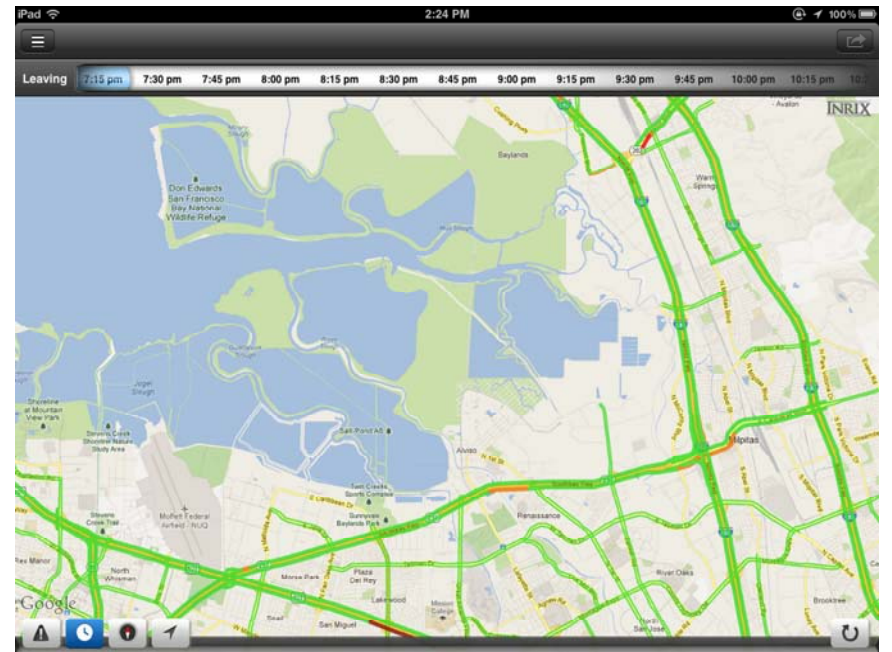
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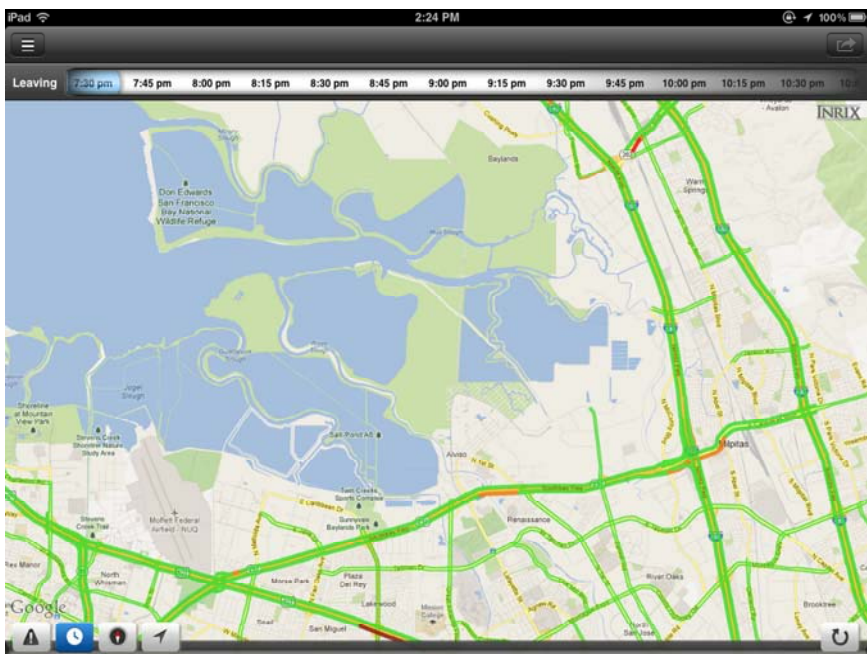
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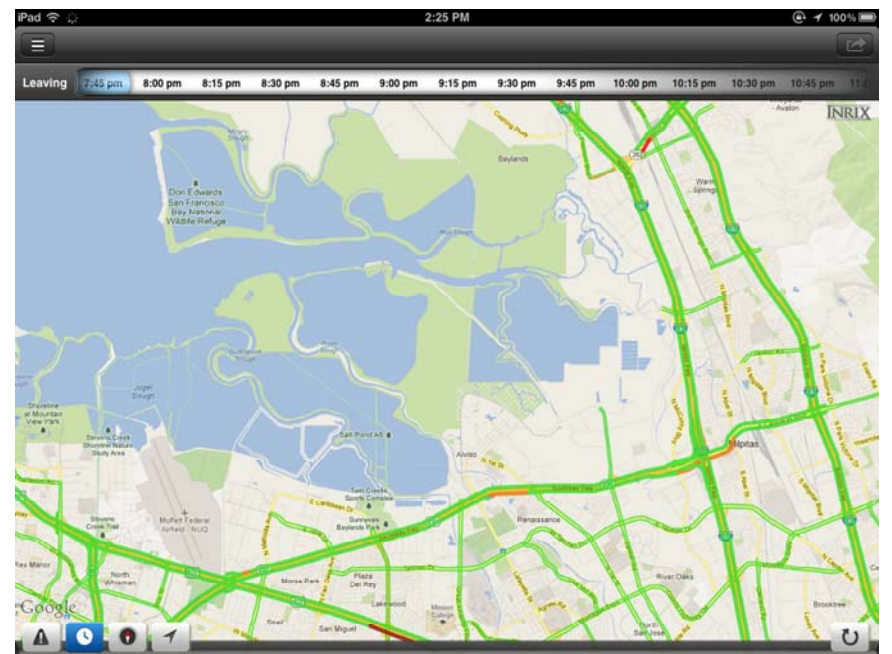
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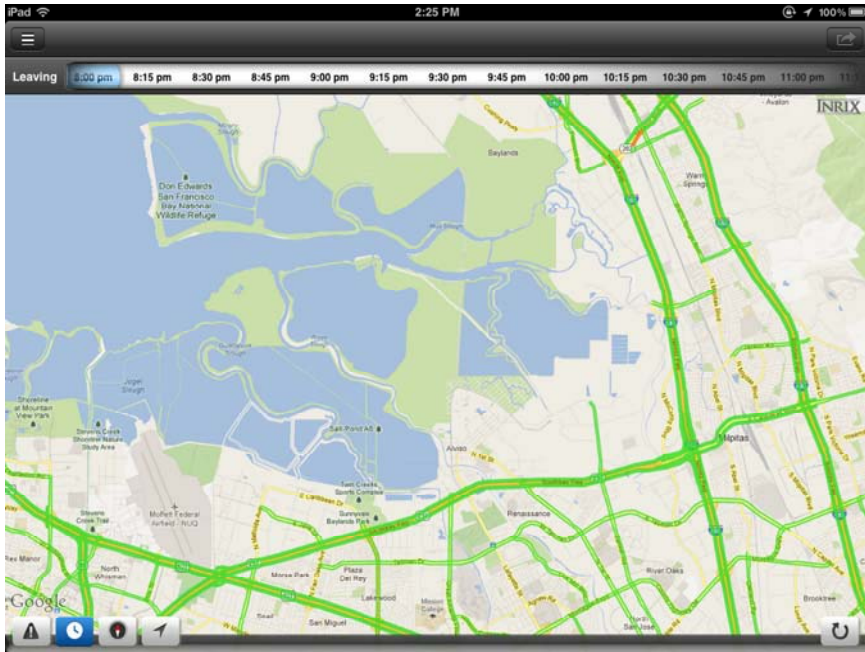
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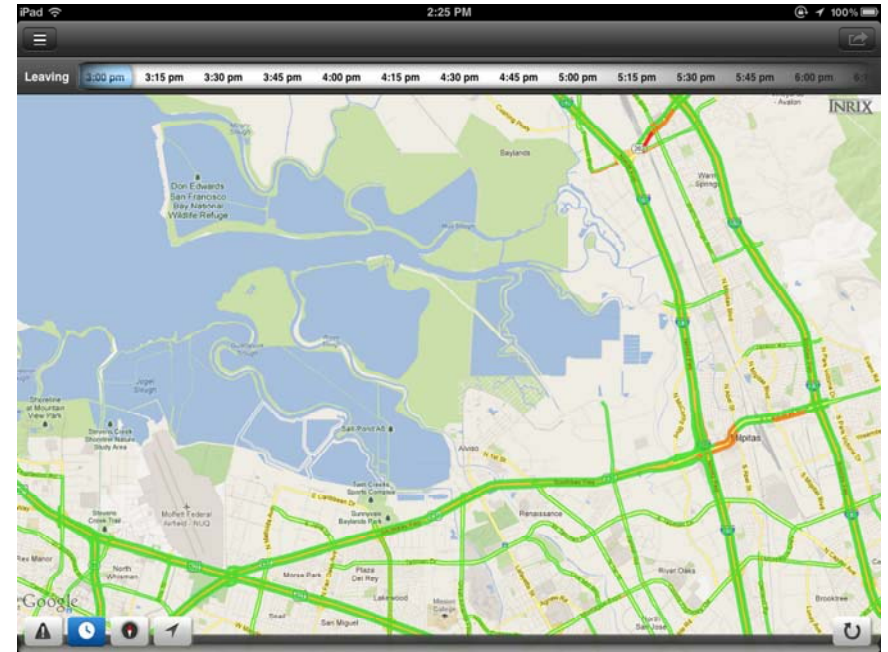
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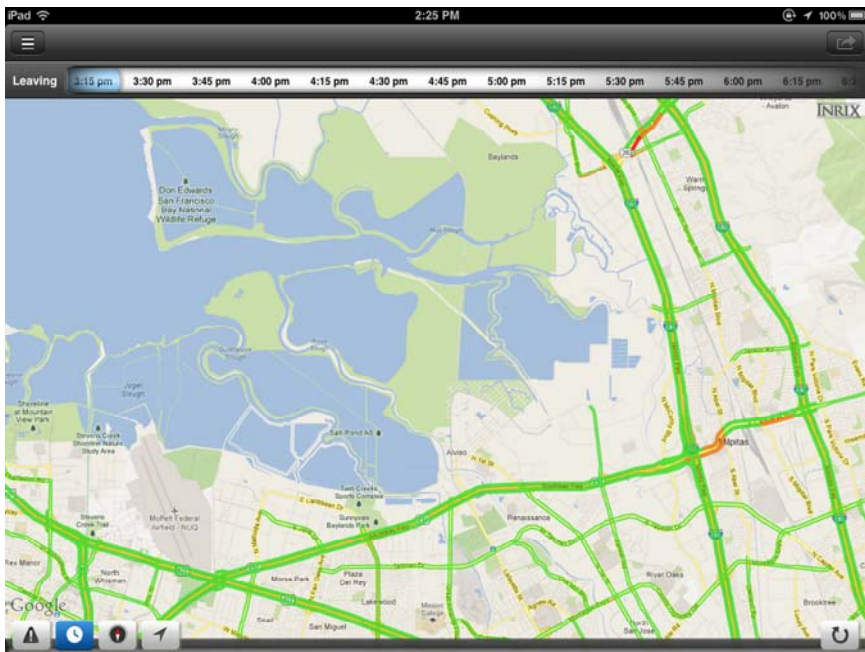
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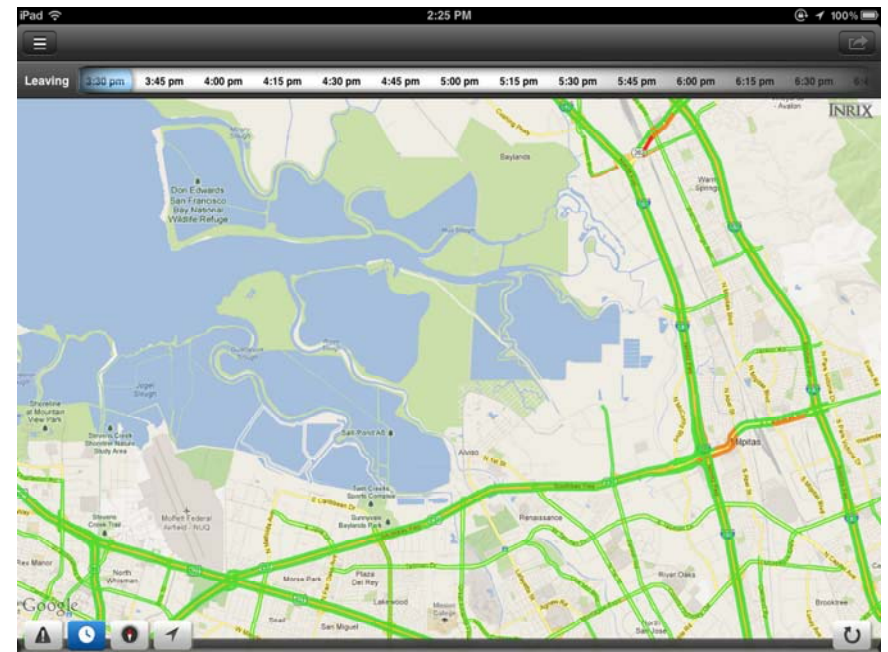
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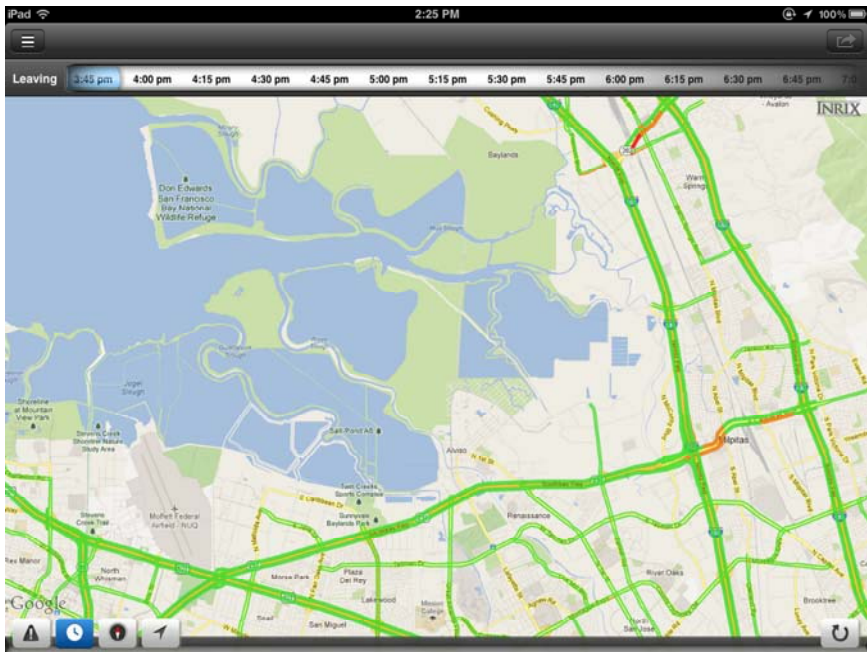
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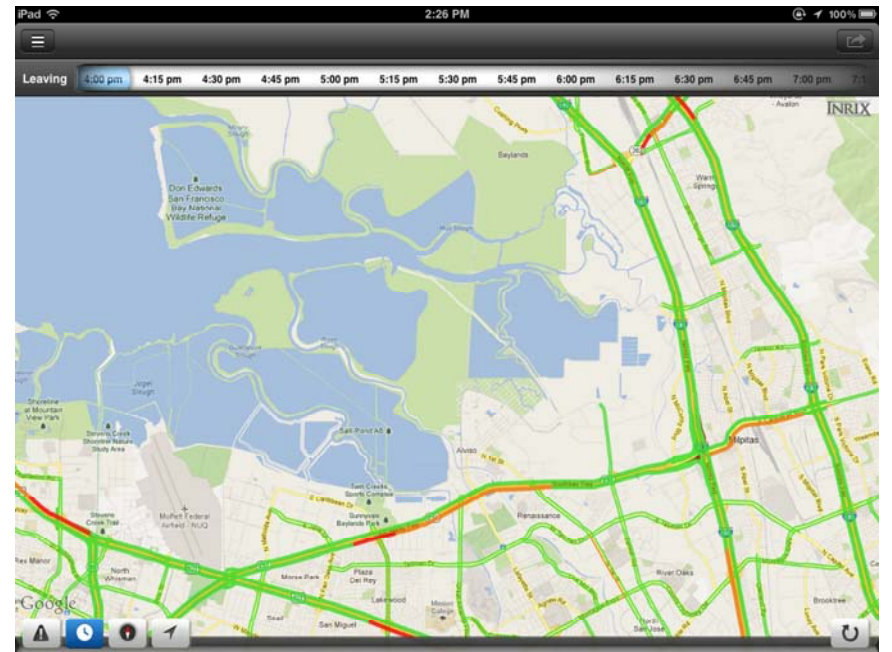
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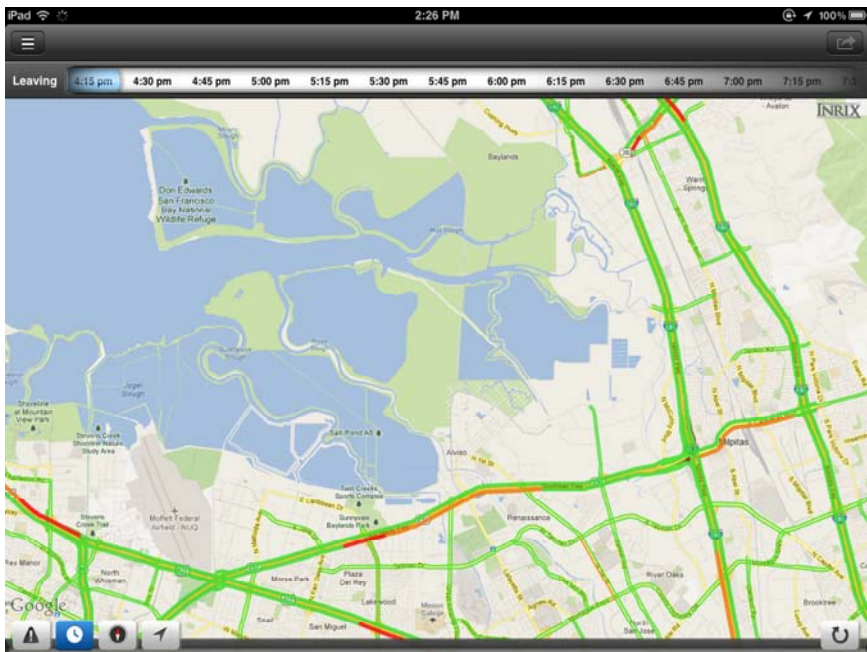
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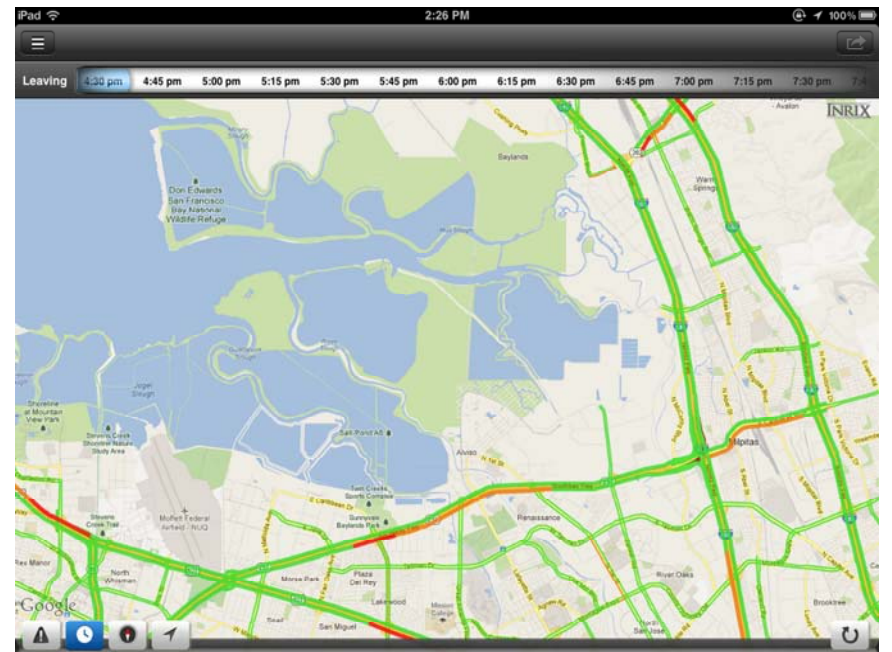
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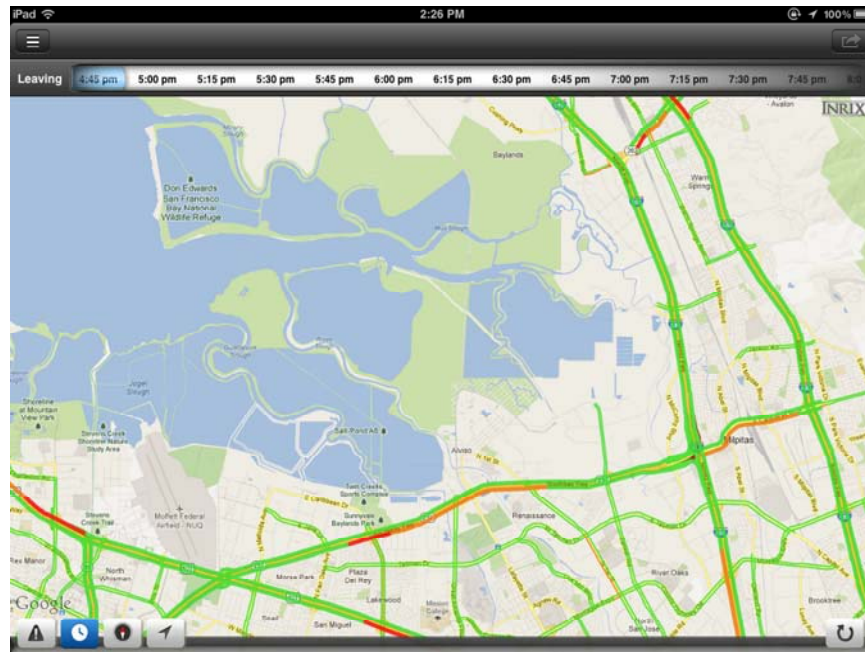
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System_4.15P



System_4.30P



System_4.45P

SR 237 Travel Time Runs

(INRIX data in November 2013)

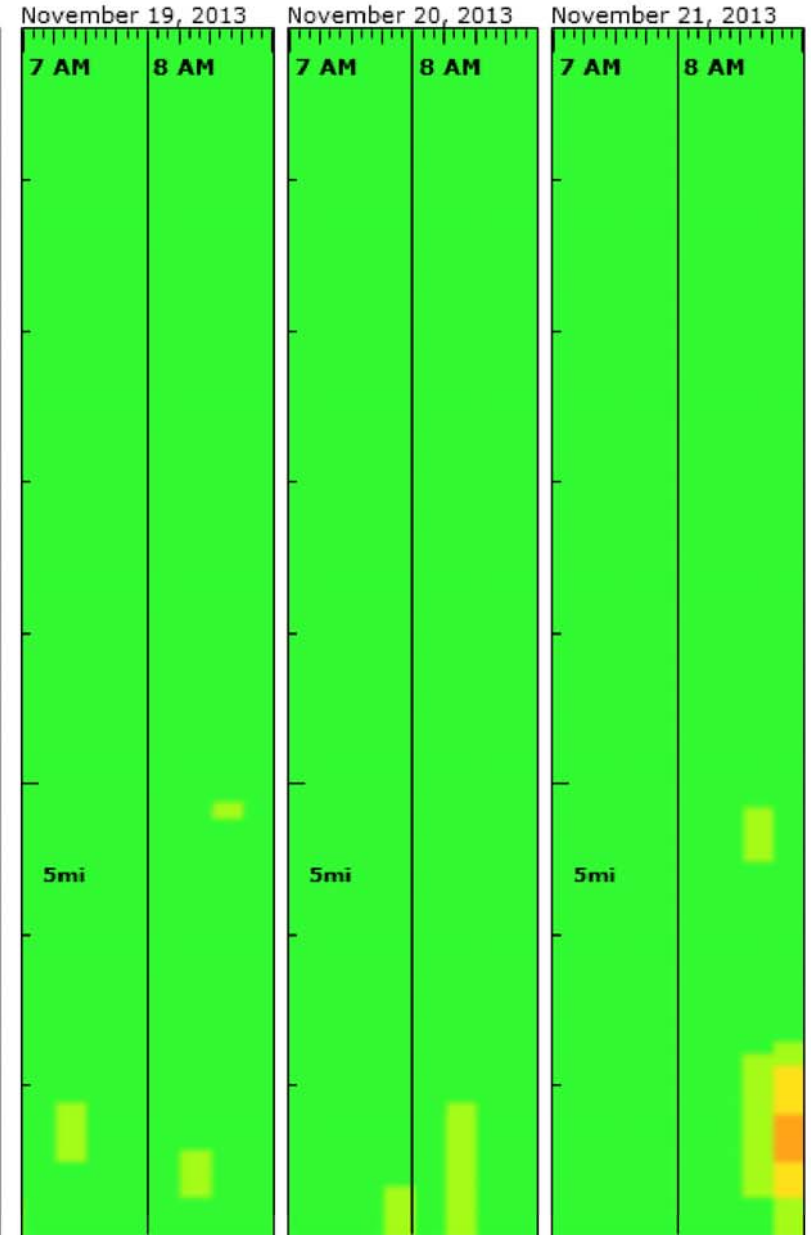
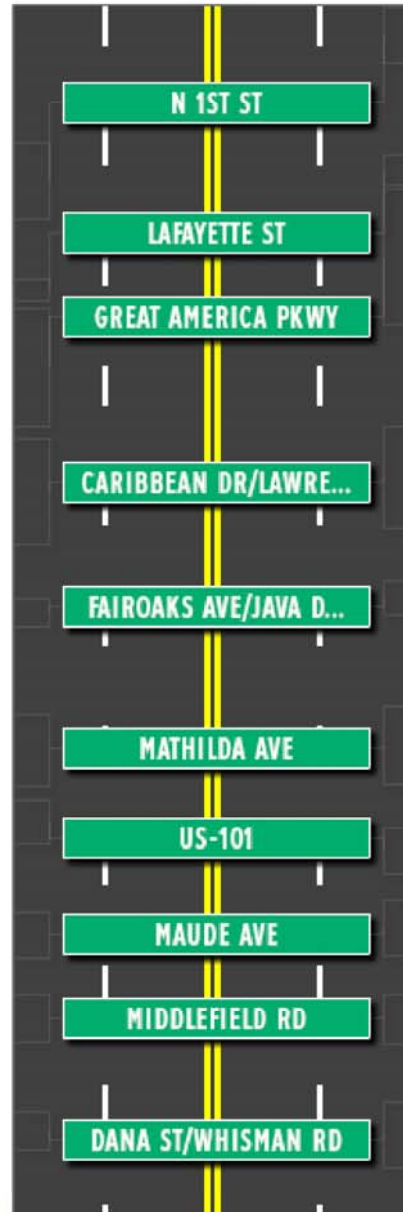
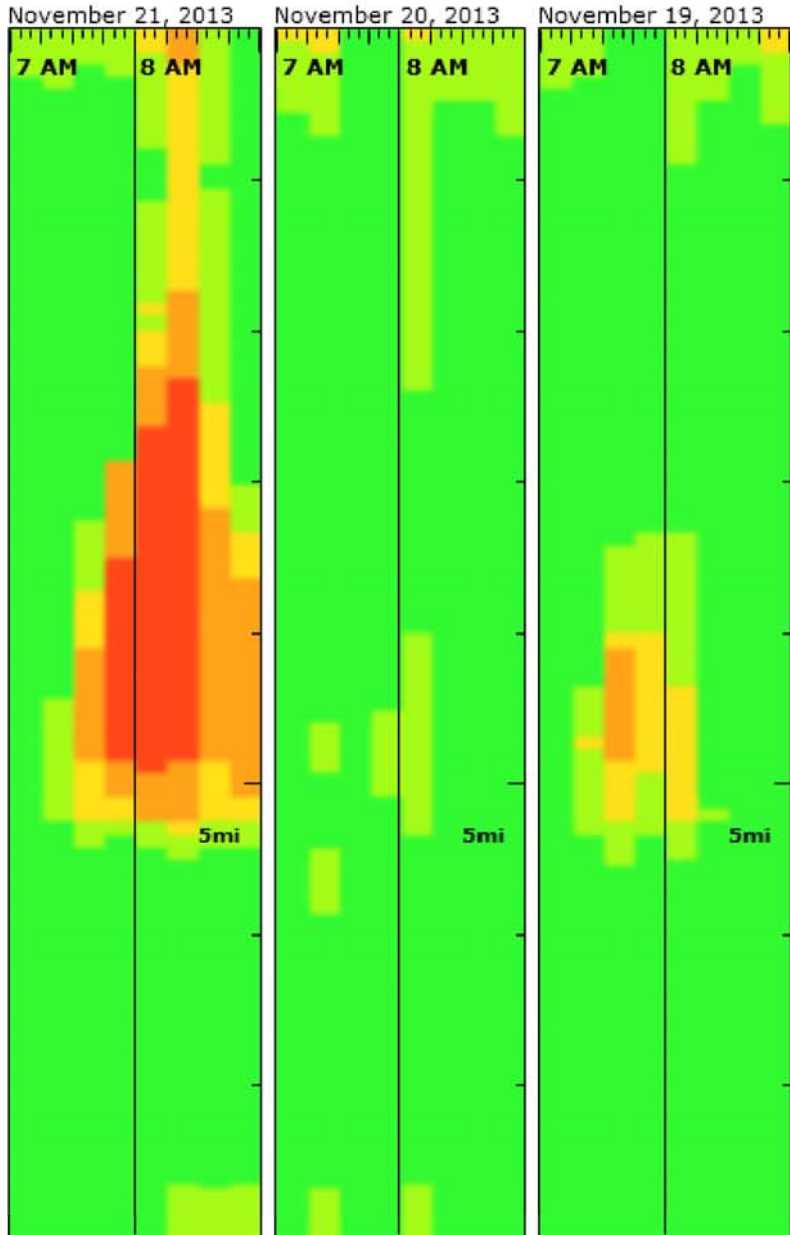
Speed on CA-237 between N 1st St and CA-85

Averaged by 15 minutes for November 19, 2013, for November 20, 2013, and for November 21, 2013

Westbound



Eastbound



The raw measured speed.



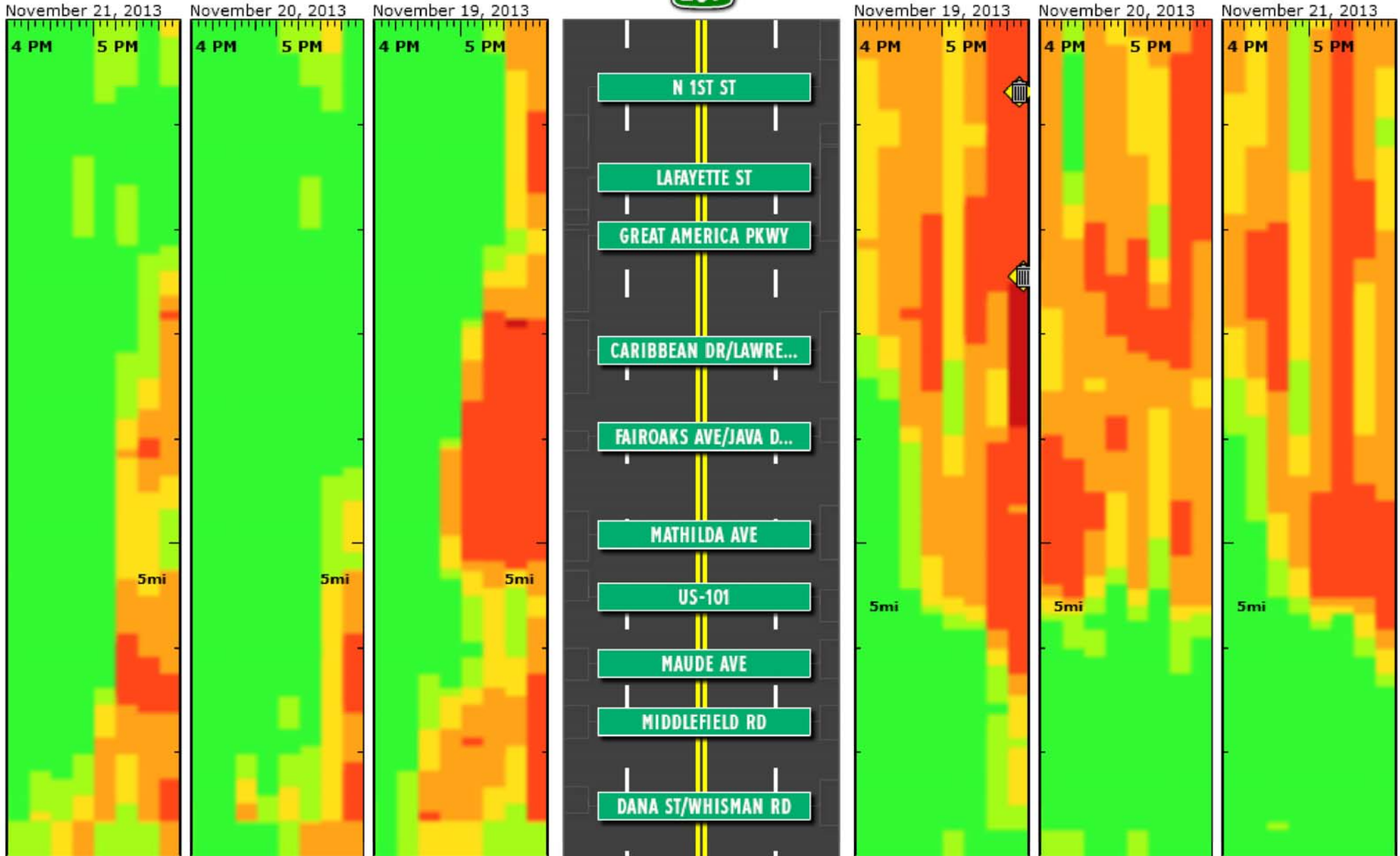
Speed on CA-237 between N 1st St and CA-85

Averaged by 15 minutes for November 19, 2013, for November 20, 2013, and for November 21, 2013



Westbound

Eastbound



The raw measured speed.



APPENDIX D – MATHILDA AVENUE TRAVEL TIME RUN INFORMATION





Mathilda Avenue

Northbound AM

Run 1



Mathilda Avenue

Northbound AM

Run 2



Mathilda Avenue

Southbound AM

Run 1



Mathilda Avenue

Southbound AM

Run 2



Mathilda Avenue

Northbound PM

Run 1



Mathilda Avenue

Northbound PM

Run 2



Mathilda Avenue

Northbound PM

Run 3



Mathilda Avenue

Northbound PM

Run 4



Mathilda Avenue

Southbound PM

Run 1



Mathilda Avenue

Southbound PM

Run 2



Mathilda Avenue

Southbound PM

Run 3



Mathilda Avenue

Southbound PM

Run 4

APPENDIX E – EXISTING INTERSECTION CALCULATION SHEETS



SimTraffic Post-Processor
 Average Results from 10 Runs
 Volume and Delay by Movement

Mathilda Avenue Improvements
 Existing Conditions
 AM Peak Hour

Intersection 1 Mathilda Avenue/5th Avenue Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 52 | 48 | 93.1% | 40.0 | 8.4 | D |
| | Through | 890 | 859 | 96.5% | 13.7 | 0.6 | B |
| | Right Turn | 61 | 62 | 101.0% | 12.1 | 2.6 | B |
| | Subtotal | 1,003 | 969 | 96.6% | 14.9 | 0.5 | B |
| SB | Left Turn | 7 | 6 | 88.6% | 48.5 | 16.6 | D |
| | Through | 330 | 335 | 101.4% | 13.4 | 1.2 | B |
| | Right Turn | 59 | 60 | 101.4% | 2.5 | 0.7 | A |
| | Subtotal | 396 | 401 | 101.1% | 12.3 | 1.2 | B |
| EB | Left Turn | 14 | 12 | 88.6% | 45.2 | 8.5 | D |
| | Through | 6 | 7 | 115.0% | 22.8 | 7.2 | C |
| | Right Turn | 17 | 17 | 98.2% | 8.6 | 3.5 | A |
| | Subtotal | 37 | 36 | 97.3% | 23.8 | 3.6 | C |
| WB | Left Turn | 19 | 19 | 98.9% | 42.1 | 7.0 | D |
| | Through | 8 | 10 | 118.8% | 23.7 | 11.4 | C |
| | Right Turn | 2 | 3 | 135.0% | 8.4 | 5.8 | A |
| | Subtotal | 29 | 31 | 106.9% | 33.3 | 6.8 | C |
| Total | | 1,465 | 1,436 | 98.0% | 14.8 | 0.5 | B |

Intersection 2 Mathilda Avenue/Innovation Way-Driveway Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 619 | 595 | 96.1% | 38.7 | 6.9 | D |
| | Through | 989 | 947 | 95.7% | 10.5 | 2.4 | B |
| | Right Turn | | | | | | |
| | Subtotal | 1,608 | 1,542 | 95.9% | 21.4 | 3.7 | C |
| SB | Left Turn | 1 | 0 | 10.0% | 1.1 | 3.4 | A |
| | Through | 265 | 261 | 98.6% | 17.8 | 1.4 | B |
| | Right Turn | 100 | 108 | 107.6% | 7.2 | 1.4 | A |
| | Subtotal | 366 | 369 | 100.8% | 14.7 | 1.0 | B |
| EB | Left Turn | 14 | 14 | 100.7% | 39.9 | 10.0 | D |
| | Through | | | | | | |
| | Right Turn | 37 | 39 | 104.3% | 40.5 | 5.2 | D |
| | Subtotal | 51 | 53 | 103.3% | 40.4 | 6.3 | D |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 2,025 | 1,963 | 96.9% | 20.6 | 3.1 | C |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Existing Conditions
AM Peak Hour

Intersection 3

Mathilda Avenue/Moffett Park Drive/SR 237 WB Ramps

Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-------------------------|--------------------------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn (Moffett Park) | 637 | 609 | 95.6% | 27.4 | 0.8 | C |
| | Left Turn (SR 237 WB On-Ramp) | 135 | 129 | 95.6% | 29.0 | 4.2 | C |
| | Through | 2,615 | 2,477 | 94.7% | 23.5 | 0.8 | C |
| | Right Turn (Moffett Park) | 759 | 716 | 94.3% | 19.8 | 1.0 | B |
| | Subtotal | 4,146 | 3,931 | 94.8% | 23.6 | 0.9 | C |
| SB | Left Turn (Moffett Park) | 8 | 8 | 102.5% | 74.6 | 16.0 | E |
| | Through | 197 | 194 | 98.4% | 101.7 | 6.6 | F |
| | Right Turn (Moffett Park) | 97 | 95 | 97.9% | 38.6 | 5.0 | D |
| | Right Turn (SR 237 WB On-Ramp) | 68 | 61 | 89.1% | 79.8 | 7.9 | E |
| | Subtotal | 370 | 358 | 96.8% | 80.6 | 6.7 | F |
| EB (Moffett Park) | Left Turn | 31 | 31 | 100.3% | 63.4 | 10.0 | E |
| | Through | 54 | 52 | 95.7% | 56.5 | 6.3 | E |
| | Right Turn | 45 | 48 | 106.7% | 63.6 | 7.8 | E |
| | Subtotal | 130 | 131 | 100.8% | 60.7 | 5.6 | E |
| WB (Moffett Park) | Left Turn | 72 | 72 | 100.3% | 107.0 | 8.8 | F |
| | Through | 189 | 192 | 101.3% | 59.7 | 2.4 | E |
| | Right Turn | 24 | 22 | 92.9% | 49.6 | 4.8 | D |
| | Subtotal | 285 | 286 | 100.4% | 70.8 | 2.7 | E |
| WB (SR 237 WB Off-Ramp) | Left Turn | 663 | 667 | 100.6% | 78.9 | 21.4 | E |
| | Through | 23 | 24 | 106.1% | 73.5 | 12.2 | E |
| | Right Turn | 334 | 338 | 101.1% | 94.5 | 18.2 | F |
| | Subtotal | 1,020 | 1,030 | 100.9% | 83.9 | 19.7 | F |
| Total | | 5,951 | 5,735 | 96.4% | 131.0 | 10.4 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Existing Conditions
AM Peak Hour

Intersection 4 Mathilda Avenue/SR 237 EB Off-Ramp-SR 237 EB On-Ramp Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | 1,980 | 1,847 | 93.3% | 41.3 | 3.6 | D |
| | Right Turn | 721 | 677 | 93.8% | 3.8 | 0.4 | A |
| | Subtotal | 2,701 | 2,523 | 93.4% | 31.2 | 2.5 | C |
| SB | Left Turn | 44 | 41 | 92.5% | 56.2 | 7.0 | E |
| | Through | 865 | 879 | 101.7% | 15.7 | 2.6 | B |
| | Right Turn | | | | | | |
| | Subtotal | 909 | 920 | 101.2% | 17.5 | 2.4 | B |
| EB | Left Turn | 770 | 761 | 98.8% | 41.6 | 3.3 | D |
| | Through | | | | | | |
| | Right Turn | 70 | 70 | 99.7% | 28.6 | 4.2 | C |
| | Subtotal | 840 | 831 | 98.9% | 40.5 | 3.1 | D |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 4,450 | 4,274 | 96.0% | 30.1 | 1.0 | C |

Intersection 5 Mathilda Avenue/Ross Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 50 | 52 | 104.6% | 49.1 | 5.9 | D |
| | Through | 2,388 | 2,221 | 93.0% | 142.0 | 36.0 | F |
| | Right Turn | 96 | 93 | 96.4% | 85.0 | 12.0 | F |
| | Subtotal | 2,534 | 2,366 | 93.4% | 137.7 | 34.0 | F |
| SB | Left Turn | 50 | 48 | 96.2% | 50.2 | 6.0 | D |
| | Through | 849 | 866 | 102.0% | 19.8 | 3.8 | B |
| | Right Turn | 36 | 40 | 110.6% | 14.2 | 5.4 | B |
| | Subtotal | 935 | 954 | 102.1% | 21.1 | 3.5 | C |
| EB | Left Turn | 74 | 75 | 100.8% | 41.2 | 5.0 | D |
| | Through | 53 | 55 | 103.0% | 29.4 | 2.9 | C |
| | Right Turn | 18 | 18 | 100.0% | 9.6 | 1.8 | A |
| | Subtotal | 145 | 147 | 101.5% | 32.9 | 3.6 | C |
| WB | Left Turn | 105 | 104 | 98.8% | 43.6 | 6.5 | D |
| | Through | 22 | 22 | 101.4% | 40.6 | 7.8 | D |
| | Right Turn | 239 | 239 | 99.8% | 29.9 | 4.6 | C |
| | Subtotal | 366 | 365 | 99.6% | 34.5 | 5.0 | C |
| Total | | 3,980 | 3,832 | 96.3% | 94.6 | 19.6 | F |

Intersection 8

Mathilda Avenue/Almanor Avenue-Ahwanee Avenue

Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 107 | 110 | 102.4% | 77.7 | 11.9 | E |
| | Through | 2,458 | 2,461 | 100.1% | 55.6 | 12.5 | E |
| | Right Turn | 46 | 44 | 95.2% | 51.1 | 13.1 | D |
| | Subtotal | 2,611 | 2,614 | 100.1% | 56.5 | 12.3 | E |
| SB | Left Turn | 144 | 146 | 101.7% | 120.2 | 27.5 | F |
| | Through | 1,505 | 1,513 | 100.5% | 46.5 | 6.5 | D |
| | Right Turn | 278 | 281 | 101.0% | 32.7 | 5.4 | C |
| | Subtotal | 1,927 | 1,940 | 100.7% | 50.1 | 7.1 | D |
| EB | Left Turn | 75 | 71 | 94.1% | 51.9 | 4.3 | D |
| | Through | 11 | 11 | 103.6% | 39.9 | 9.2 | D |
| | Right Turn | 21 | 20 | 95.7% | 8.2 | 3.1 | A |
| | Subtotal | 107 | 102 | 95.4% | 41.8 | 3.0 | D |
| WB | Left Turn | 70 | 69 | 98.7% | 60.7 | 11.2 | E |
| | Through | 27 | 28 | 103.0% | 35.9 | 5.5 | D |
| | Right Turn | 171 | 174 | 101.5% | 21.1 | 2.8 | C |
| | Subtotal | 268 | 271 | 100.9% | 32.8 | 2.9 | C |
| Total | | 4,913 | 4,927 | 100.3% | 52.3 | 7.9 | D |

Intersection 9

US 101 On-Ramp/Moffett Park Drive

Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| EB | Left Turn | | | | | | |
| | Through | 151 | 150 | 99.5% | 3.4 | 0.3 | A |
| | Right Turn | 1 | 1 | 80.0% | 2.8 | 1.4 | A |
| | Subtotal | 152 | 151 | 99.3% | 3.4 | 0.3 | A |
| WB | Left Turn | 16 | 17 | 105.6% | 8.3 | 0.6 | A |
| | Through | 873 | 841 | 96.3% | 4.7 | 0.3 | A |
| | Right Turn | | | | | | |
| | Subtotal | 889 | 858 | 96.5% | 4.8 | 0.4 | A |
| Total | | 1,041 | 1,009 | 96.9% | 4.6 | 0.3 | A |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Existing Conditions
AM Peak Hour

Intersection 10 Innovation Way/Moffett Park Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | 32 | 29 | 91.6% | 13.9 | 3.2 | B |
| | Through | | | | | | |
| | Right Turn | 100 | 98 | 98.2% | 10.5 | 1.7 | B |
| | Subtotal | 132 | 128 | 96.6% | 11.3 | 1.8 | B |
| EB | Left Turn | 49 | 46 | 93.1% | 33.1 | 6.2 | C |
| | Through | 102 | 105 | 102.9% | 4.1 | 0.9 | A |
| | Right Turn | | | | | | |
| | Subtotal | 151 | 151 | 99.7% | 12.8 | 1.5 | B |
| WB | Left Turn | | | | | | |
| | Through | 789 | 762 | 96.5% | 13.2 | 1.4 | B |
| | Right Turn | 134 | 131 | 97.5% | 8.4 | 0.9 | A |
| | Subtotal | 923 | 892 | 96.7% | 12.5 | 1.2 | B |
| Total | | 1,206 | 1,170 | 97.0% | 12.4 | 1.0 | B |

Intersection 11 Innovation Way/11th Avenue All-way Stop

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 169 | 160 | 94.4% | 5.9 | 0.2 | A |
| | Through | 14 | 16 | 114.3% | 5.8 | 0.8 | A |
| | Right Turn | | | | | | |
| | Subtotal | 183 | 176 | 96.0% | 5.8 | 0.2 | A |
| SB | Left Turn | | | | | | |
| | Through | 77 | 73 | 94.7% | 9.6 | 1.2 | A |
| | Right Turn | 344 | 335 | 97.3% | 8.9 | 1.2 | A |
| | Subtotal | 421 | 408 | 96.8% | 9.0 | 1.2 | A |
| EB | Left Turn | 9 | 8 | 92.2% | 4.3 | 0.4 | A |
| | Through | | | | | | |
| | Right Turn | 55 | 57 | 102.7% | 4.3 | 0.3 | A |
| | Subtotal | 64 | 65 | 101.3% | 4.3 | 0.3 | A |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 668 | 648 | 97.0% | 7.7 | 0.8 | A |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Existing Conditions
AM Peak Hour

Intersection 12

Innovation Way/Juniper Driveway

All-way Stop

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | 23 | 23 | 100.4% | 4.7 | 0.2 | A |
| | Right Turn | | | | | | |
| | Subtotal | 23 | 23 | 100.4% | 4.7 | 0.2 | A |
| SB | Left Turn | | | | | | |
| | Through | 420 | 409 | 97.4% | 14.7 | 1.3 | B |
| | Right Turn | 299 | 295 | 98.7% | 9.2 | 1.1 | A |
| | Subtotal | 719 | 704 | 97.9% | 12.4 | 1.2 | B |
| EB | Left Turn | 28 | 29 | 103.6% | 5.3 | 0.5 | A |
| | Through | | | | | | |
| | Right Turn | 1 | 1 | 130.0% | 3.5 | 2.5 | A |
| | Subtotal | 29 | 30 | 104.5% | 5.3 | 0.4 | A |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 771 | 758 | 98.2% | 11.9 | 1.1 | B |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Existing Conditions
PM Peak Hour

Intersection 1 Mathilda Avenue/5th Avenue Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 97 | 90 | 92.5% | 68.1 | 8.0 | E |
| | Through | 329 | 308 | 93.6% | 18.1 | 3.0 | B |
| | Right Turn | 37 | 38 | 102.7% | 11.4 | 4.3 | B |
| | Subtotal | 463 | 436 | 94.1% | 27.9 | 3.0 | C |
| SB | Left Turn | 3 | 2 | 70.0% | 113.2 | 132.2 | F |
| | Through | 1,102 | 1,012 | 91.8% | 149.4 | 53.3 | F |
| | Right Turn | 9 | 9 | 96.7% | 113.3 | 50.4 | F |
| | Subtotal | 1,114 | 1,023 | 91.8% | 149.1 | 53.1 | F |
| EB | Left Turn | 38 | 37 | 96.3% | 40.4 | 4.4 | D |
| | Through | 17 | 16 | 91.8% | 56.6 | 13.4 | E |
| | Right Turn | 51 | 60 | 117.5% | 13.4 | 4.1 | B |
| | Subtotal | 106 | 112 | 105.8% | 28.0 | 4.3 | C |
| WB | Left Turn | 229 | 211 | 92.0% | 157.9 | 87.0 | F |
| | Through | 4 | 4 | 92.5% | 186.1 | 123.5 | F |
| | Right Turn | 8 | 8 | 96.3% | 123.3 | 65.8 | F |
| | Subtotal | 241 | 222 | 92.1% | 156.9 | 85.4 | F |
| Total | | 1,924 | 1,793 | 93.2% | 112.4 | 38.5 | F |

Intersection 2 Mathilda Avenue/Innovation Way-Driveway Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 61 | 58 | 94.3% | 57.6 | 7.9 | E |
| | Through | 376 | 353 | 93.8% | 17.1 | 1.2 | B |
| | Right Turn | | | | | | |
| | Subtotal | 437 | 410 | 93.9% | 22.8 | 1.5 | C |
| SB | Left Turn | | | | | | |
| | Through | 1,346 | 1,137 | 84.5% | 280.1 | 31.5 | F |
| | Right Turn | 36 | 33 | 91.1% | 243.0 | 51.1 | F |
| | Subtotal | 1,382 | 1,170 | 84.7% | 279.0 | 31.7 | F |
| EB | Left Turn | 87 | 82 | 94.5% | 63.0 | 5.8 | E |
| | Through | | | | | | |
| | Right Turn | 622 | 560 | 90.0% | 62.7 | 7.6 | E |
| | Subtotal | 709 | 642 | 90.6% | 62.7 | 7.3 | E |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 2,528 | 2,223 | 87.9% | 168.9 | 15.9 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Existing Conditions
PM Peak Hour

Intersection 3

Mathilda Avenue/Moffett Park Drive/SR 237 WB Ramps

Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-------------------------|--------------------------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn (Moffett Park) | 84 | 80 | 95.6% | 47.2 | 3.5 | D |
| | Left Turn (SR 237 WB On-Ramp) | 82 | 79 | 95.7% | 128.1 | 27.0 | F |
| | Through | 438 | 434 | 99.2% | 40.5 | 4.4 | D |
| | Right Turn (Moffett Park) | 145 | 145 | 99.7% | 24.1 | 4.4 | C |
| | Subtotal | 749 | 738 | 98.5% | 47.3 | 5.4 | D |
| SB | Left Turn (Moffett Park) | 39 | 32 | 83.1% | 184.7 | 16.7 | F |
| | Through | 1,858 | 1,590 | 85.6% | 224.7 | 7.8 | F |
| | Right Turn (Moffett Park) | 71 | 60 | 84.1% | 256.3 | 13.4 | F |
| | Right Turn (SR 237 WB On-Ramp) | 403 | 343 | 85.2% | 218.3 | 7.5 | F |
| | Subtotal | 2,371 | 2,026 | 85.4% | 223.9 | 7.6 | F |
| EB (Moffett Park) | Left Turn | 44 | 41 | 92.0% | 244.0 | 38.5 | F |
| | Through | 165 | 146 | 88.2% | 225.3 | 40.0 | F |
| | Right Turn | 403 | 346 | 85.9% | 258.0 | 39.8 | F |
| | Subtotal | 612 | 532 | 87.0% | 248.0 | 39.7 | F |
| WB (Moffett Park) | Left Turn | 285 | 284 | 99.5% | 78.3 | 5.1 | E |
| | Through | 237 | 237 | 100.2% | 42.9 | 1.5 | D |
| | Right Turn | 20 | 21 | 103.5% | 36.8 | 6.9 | D |
| | Subtotal | 542 | 542 | 100.0% | 61.2 | 3.3 | E |
| WB (SR 237 WB Off-Ramp) | Left Turn | 709 | 613 | 86.4% | 620.8 | 174.5 | F |
| | Through | 17 | 16 | 95.9% | 622.6 | 170.9 | F |
| | Right Turn | 164 | 136 | 83.0% | 534.0 | 164.7 | F |
| | Subtotal | 890 | 765 | 86.0% | 605.4 | 173.3 | F |
| Total | | 5,164 | 4,602 | 89.1% | 286.7 | 28.0 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Existing Conditions
PM Peak Hour

Intersection 4 Mathilda Avenue/SR 237 EB Off-Ramp-SR 237 EB On-Ramp Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | 354 | 338 | 95.6% | 32.9 | 4.1 | C |
| | Right Turn | 625 | 625 | 100.0% | 4.6 | 0.2 | A |
| | Subtotal | 979 | 963 | 98.4% | 14.5 | 1.5 | B |
| SB | Left Turn | 331 | 296 | 89.4% | 41.2 | 4.1 | D |
| | Through | 2,521 | 2,168 | 86.0% | 16.9 | 1.5 | B |
| | Right Turn | | | | | | |
| | Subtotal | 2,852 | 2,464 | 86.4% | 19.8 | 1.7 | B |
| EB | Left Turn | 166 | 172 | 103.7% | 46.4 | 2.7 | D |
| | Through | 29 | 29 | 100.0% | 56.2 | 14.5 | E |
| | Right Turn | 195 | 191 | 97.7% | 26.3 | 6.8 | C |
| | Subtotal | 390 | 392 | 100.4% | 37.5 | 5.0 | D |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 4,221 | 3,819 | 90.5% | 20.3 | 1.4 | C |

Intersection 5 Mathilda Avenue/Ross Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 87 | 86 | 98.6% | 52.1 | 4.4 | D |
| | Through | 843 | 842 | 99.9% | 59.6 | 9.4 | E |
| | Right Turn | 252 | 245 | 97.2% | 68.6 | 11.7 | E |
| | Subtotal | 1,182 | 1,173 | 99.2% | 60.9 | 9.2 | E |
| SB | Left Turn | 130 | 115 | 88.3% | 41.1 | 4.9 | D |
| | Through | 2,499 | 2,158 | 86.3% | 22.7 | 1.5 | C |
| | Right Turn | 87 | 77 | 88.7% | 19.3 | 2.4 | B |
| | Subtotal | 2,716 | 2,350 | 86.5% | 23.5 | 1.5 | C |
| EB | Left Turn | 39 | 36 | 92.3% | 42.0 | 6.0 | D |
| | Through | 143 | 135 | 94.7% | 38.6 | 3.2 | D |
| | Right Turn | 35 | 37 | 106.9% | 27.2 | 4.7 | C |
| | Subtotal | 217 | 209 | 96.2% | 37.2 | 1.9 | D |
| WB | Left Turn | 210 | 214 | 101.9% | 168.4 | 96.6 | F |
| | Through | 48 | 44 | 91.9% | 156.4 | 96.4 | F |
| | Right Turn | 97 | 97 | 100.2% | 136.7 | 100.2 | F |
| | Subtotal | 355 | 355 | 100.1% | 158.3 | 97.4 | F |
| Total | | 4,470 | 4,087 | 91.4% | 46.7 | 10.7 | D |

Intersection 8 **Mathilda Avenue/Almanor Avenue-Ahwanee Avenue** **Signal**

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|--------------|-----------------|---------------------|---------------------|--------------|-----------------------|------------|----------|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 56 | 55 | 98.0% | 67.3 | 3.2 | E |
| | Through | 1,275 | 1,260 | 98.8% | 21.8 | 1.8 | C |
| | Right Turn | 36 | 38 | 105.8% | 13.9 | 3.1 | B |
| | Subtotal | 1,367 | 1,353 | 98.9% | 23.4 | 1.8 | C |
| SB | Left Turn | 156 | 145 | 93.1% | 85.5 | 6.6 | F |
| | Through | 2,680 | 2,482 | 92.6% | 62.8 | 5.6 | E |
| | Right Turn | 58 | 55 | 95.3% | 18.0 | 4.0 | B |
| | Subtotal | 2,894 | 2,682 | 92.7% | 63.1 | 5.5 | E |
| EB | Left Turn | 285 | 284 | 99.5% | 59.3 | 7.7 | E |
| | Through | 23 | 21 | 93.0% | 52.8 | 12.2 | D |
| | Right Turn | 64 | 62 | 96.9% | 23.9 | 6.8 | C |
| | Subtotal | 372 | 367 | 98.7% | 53.0 | 7.2 | D |
| WB | Left Turn | 41 | 41 | 99.8% | 58.3 | 4.8 | E |
| | Through | 5 | 5 | 104.0% | 71.6 | 21.3 | E |
| | Right Turn | 172 | 163 | 94.7% | 12.8 | 1.0 | B |
| | Subtotal | 218 | 209 | 95.9% | 23.0 | 1.6 | C |
| Total | | 4,851 | 4,611 | 95.1% | 48.8 | 3.4 | D |

Intersection 9 **US 101 On-Ramp/Moffett Park Drive** **Signal**

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|--------------|-----------------|---------------------|---------------------|--------------|-----------------------|-------------|----------|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| EB | Left Turn | | | | | | |
| | Through | 731 | 668 | 91.4% | 100.9 | 60.4 | F |
| | Right Turn | 77 | 73 | 94.7% | 78.5 | 50.4 | E |
| | Subtotal | 808 | 741 | 91.7% | 98.7 | 59.6 | F |
| WB | Left Turn | 205 | 183 | 89.2% | 32.8 | 15.3 | C |
| | Through | 282 | 276 | 98.0% | 1.9 | 0.3 | A |
| | Right Turn | | | | | | |
| | Subtotal | 487 | 459 | 94.3% | 14.2 | 6.3 | B |
| Total | | 1,295 | 1,200 | 92.7% | 65.6 | 36.8 | E |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Existing Conditions
PM Peak Hour

Intersection 10 Innovation Way/Moffett Park Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | 153 | 150 | 98.2% | 15.7 | 3.4 | B |
| | Through | | | | | | |
| | Right Turn | 137 | 127 | 92.8% | 5.7 | 1.0 | A |
| | Subtotal | 290 | 278 | 95.7% | 11.1 | 1.9 | B |
| EB | Left Turn | 44 | 36 | 81.6% | 106.5 | 53.3 | F |
| | Through | 687 | 585 | 85.2% | 159.0 | 91.9 | F |
| | Right Turn | | | | | | |
| | Subtotal | 731 | 621 | 85.0% | 156.0 | 89.8 | F |
| WB | Left Turn | | | | | | |
| | Through | 350 | 336 | 96.0% | 17.2 | 1.6 | B |
| | Right Turn | 42 | 43 | 102.9% | 4.1 | 0.4 | A |
| | Subtotal | 392 | 379 | 96.7% | 15.7 | 1.5 | B |
| Total | | 1,413 | 1,278 | 90.4% | 81.5 | 41.8 | F |

Intersection 11 Innovation Way/11th Avenue All-way Stop

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 24 | 23 | 95.4% | 6.0 | 0.9 | A |
| | Through | 62 | 57 | 91.3% | 6.2 | 0.3 | A |
| | Right Turn | | | | | | |
| | Subtotal | 86 | 80 | 92.4% | 6.1 | 0.4 | A |
| SB | Left Turn | | | | | | |
| | Through | 42 | 35 | 82.4% | 6.8 | 2.0 | A |
| | Right Turn | 14 | 12 | 86.4% | 3.4 | 0.5 | A |
| | Subtotal | 56 | 47 | 83.4% | 5.9 | 1.5 | A |
| EB | Left Turn | 363 | 365 | 100.4% | 7.3 | 0.4 | A |
| | Through | | | | | | |
| | Right Turn | 248 | 244 | 98.2% | 6.5 | 3.2 | A |
| | Subtotal | 611 | 608 | 99.5% | 7.0 | 1.5 | A |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 753 | 734 | 97.5% | 6.8 | 1.3 | A |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Existing Conditions
PM Peak Hour

Intersection 12

Innovation Way/Juniper Driveway

All-way Stop

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | 425 | 403 | 94.9% | 89.3 | 46.8 | F |
| | Right Turn | | | | | | |
| | Subtotal | 425 | 403 | 94.9% | 89.3 | 46.8 | F |
| SB | Left Turn | | | | | | |
| | Through | 41 | 35 | 85.1% | 39.6 | 14.5 | E |
| | Right Turn | 56 | 55 | 97.7% | 25.6 | 6.8 | D |
| | Subtotal | 97 | 90 | 92.4% | 31.2 | 8.7 | D |
| EB | Left Turn | | | | | | |
| | Through | 284 | 251 | 88.4% | 213.2 | 133.0 | F |
| | Right Turn | 15 | 12 | 80.0% | 25.3 | 31.9 | D |
| | Subtotal | 299 | 263 | 88.0% | 204.3 | 127.2 | F |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 821 | 756 | 92.1% | 120.6 | 64.8 | F |

Intersection 1

Mathilda Avenue/5th Avenue

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 625 | 25 | 6 | 50 | 17 | 50 | 17 | 0% | 0% |
| | Through | 625 | 25 | 3 | 25 | 5 | 50 | 7 | 0% | 0% |
| | Right Turn | 625 | 25 | 2 | 25 | 8 | 25 | 19 | 0% | 0% |
| NB | Left Turn | 425 | 50 | 3 | 75 | 9 | 100 | 18 | 0% | 0% |
| | Through | 1,150 | 100 | 8 | 225 | 21 | 275 | 48 | 0% | 0% |
| | Through/Right | 1,150 | 125 | 7 | 275 | 17 | 300 | 38 | 0% | 0% |
| SB | Left Turn | 225 | 25 | 3 | 50 | 6 | 50 | 12 | 0% | 0% |
| | Through | 1,375 | 75 | 7 | 150 | 18 | 175 | 39 | 0% | 0% |
| | Right Turn | 225 | 25 | 2 | 25 | 14 | 50 | 30 | 0% | 0% |
| WB | Left Turn | 925 | 25 | 9 | 50 | 23 | 75 | 34 | 2% | 0% |
| | Through/Right | 75 | 25 | 4 | 50 | 9 | 75 | 21 | 1% | 0% |

Intersection 2

Mathilda Avenue/Innovation Way-Driveway

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 125 | 25 | 3 | 50 | 4 | 50 | 5 | 0% | 0% |
| | Right Turn | 200 | 25 | 5 | 50 | 8 | 50 | 14 | 0% | 1% |
| NB | Left Turn | 400 | 225 | 30 | 375 | 69 | 400 | 113 | 1% | 0% |
| | Through | 1,075 | 75 | 23 | 200 | 102 | 375 | 243 | 0% | 0% |
| | Through/Right | 1,075 | 100 | 18 | 200 | 36 | 250 | 54 | 0% | 0% |
| SB | Left Turn | 75 | 25 | 0 | 25 | 0 | 25 | 6 | 0% | 0% |
| | Through | 1,150 | 75 | 6 | 125 | 15 | 150 | 35 | 2% | 0% |
| | Right Turn | 225 | 25 | 8 | 100 | 21 | 125 | 39 | 0% | 0% |
| WB | Shared | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |

SimTraffic Post-Processor
Average Results from 10 Runs
Queue Length

Mathilda Avenue Improvements
Existing Conditions
AM Peak Hour

Intersection 3

Mathilda Avenue/Moffett Park Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-------------------------|-----------------------------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB (Moffett Park) | Left Turn | 350 | 25 | 5 | 50 | 18 | 75 | 33 | 0% | 0% |
| | Through/Right | 1,100 | 75 | 7 | 125 | 12 | 150 | 24 | 0% | 0% |
| | Right Turn | 1,100 | 25 | 6 | 50 | 15 | 75 | 16 | 0% | 0% |
| NB | Left Turn (Moffett Park) | 125 | 75 | 6 | 125 | 8 | 150 | 11 | 0% | 23% |
| | Through | 325 | 275 | 18 | 400 | 20 | 400 | 46 | 0% | 37% |
| | Through/Right (Moffett Park) | 325 | 275 | 16 | 375 | 19 | 375 | 42 | 0% | 43% |
| | Left Turn (SR 237 WB On-Ramp) | 200 | 100 | 5 | 150 | 15 | 175 | 26 | 0% | 1% |
| SB | Left Turn (Moffett Park) | 175 | 25 | 2 | 50 | 6 | 75 | 16 | 0% | 0% |
| | Through | 1,200 | 75 | 14 | 150 | 32 | 200 | 56 | 0% | 28% |
| | Through/Right (Moffett Park) | 1,075 | 125 | 8 | 200 | 16 | 250 | 36 | 0% | 0% |
| WB (Moffett Park) | Through/Right (SR 237 WB On-Ramp) | 1,200 | 75 | 14 | 175 | 32 | 225 | 52 | 0% | 20% |
| | Left Turn | 300 | 75 | 5 | 125 | 9 | 150 | 31 | 0% | 0% |
| WB (Moffett Park) | Through/Right | 650 | 150 | 12 | 250 | 18 | 275 | 18 | 0% | 0% |
| | Left Turn | 1,125 | 350 | 109 | 650 | 311 | 800 | 286 | 8% | 1% |
| WB (SR 237 WB Off-Ramp) | Left/Through | 325 | 275 | 29 | 425 | 60 | 425 | 16 | 8% | 0% |
| | Right Turn | 325 | 250 | 21 | 400 | 31 | 375 | 1 | 8% | 0% |

Intersection 4

Mathilda Avenue/SR 237 EB Off-Ramp-SR 237 EB On-Ramp

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,075 | 225 | 19 | 325 | 38 | 375 | 70 | 0% | 0% |
| | Shared | 450 | 175 | 12 | 275 | 23 | 325 | 48 | 0% | 0% |
| NB | Through | 275 | 250 | 10 | 325 | 20 | 325 | 27 | 0% | 25% |
| | Right Turn | 275 | 100 | 28 | 300 | 44 | 325 | 22 | 0% | 4% |
| SB | Left Turn | 200 | 50 | 9 | 100 | 18 | 100 | 24 | 0% | 0% |
| | Through | 200 | 125 | 19 | 275 | 31 | 250 | 23 | 0% | 6% |
| | | | | | | | | | | |

Intersection 5

Mathilda Avenue/Ross Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 650 | 75 | 6 | 150 | 19 | 200 | 59 | 43% | 0% |
| | Through | 75 | 50 | 5 | 100 | 6 | 100 | 0 | 26% | 0% |
| | Right Turn | 50 | 25 | 5 | 75 | 7 | 75 | 4 | 3% | 0% |
| NB | Left Turn | 150 | 50 | 5 | 100 | 19 | 150 | 50 | 0% | 0% |
| | Through | 2,200 | 775 | 90 | 950 | 137 | 1,025 | 116 | 0% | 1% |
| | Through/Right | 450 | 500 | 23 | 625 | 37 | 550 | 6 | 0% | 59% |
| SB | Left Turn | 125 | 50 | 9 | 125 | 21 | 200 | 44 | 1% | 0% |
| | Through | 250 | 125 | 22 | 275 | 30 | 275 | 17 | 11% | 3% |
| | Through/Right | 250 | 150 | 22 | 275 | 27 | 275 | 17 | 0% | 5% |
| WB | Left Turn | 75 | 150 | 24 | 300 | 49 | 375 | 40 | 14% | 0% |
| | Through | 75 | 75 | 7 | 125 | 6 | 100 | 0 | 6% | 0% |
| | Right Turn | 75 | 75 | 2 | 100 | 4 | 100 | 0 | 29% | 0% |

Intersection 8

Mathilda Avenue/Almanor Avenue-Ahwanee Avenue

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 350 | 50 | 5 | 100 | 13 | 125 | 28 | 0% | 0% |
| | Through/Right | 125 | 25 | 5 | 75 | 9 | 75 | 13 | 0% | 0% |
| NB | Left Turn | 375 | 150 | 31 | 325 | 61 | 375 | 0 | 0% | 0% |
| | Through | 675 | 450 | 52 | 675 | 91 | 675 | 49 | 51% | 2% |
| | Right Turn | 75 | 25 | 8 | 75 | 23 | 100 | 3 | 0% | 0% |
| SB | Left Turn | 125 | 150 | 10 | 225 | 9 | 175 | 0 | 44% | 0% |
| | Through | 2,200 | 450 | 44 | 575 | 96 | 625 | 97 | 15% | 0% |
| | Through/Right | 350 | 275 | 19 | 425 | 34 | 450 | 54 | 0% | 4% |
| WB | Left Turn | 250 | 75 | 10 | 125 | 21 | 150 | 28 | 0% | 0% |
| | Through | 625 | 75 | 15 | 150 | 34 | 200 | 52 | 4% | 0% |
| | Right Turn | 75 | 75 | 5 | 125 | 10 | 125 | 3 | 17% | 0% |

Intersection 9

US 101 On-Ramp/Moffett Park Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Through | 875 | 25 | 2 | 50 | 8 | 75 | 17 | 0% | 0% |
| | Right Turn | 150 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| WB | Left Turn | 900 | 25 | 3 | 50 | 3 | 50 | 11 | 0% | 0% |
| | Through | 900 | 25 | 25 | 125 | 178 | 250 | 401 | 0% | 0% |
| | | | | | | | | | | |
| | | | | | | | | | | |

Intersection 10

Innovation Way/Moffett Park Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 225 | 50 | 4 | 75 | 6 | 100 | 14 | 0% | 0% |
| | Through | 900 | 25 | 3 | 75 | 8 | 100 | 15 | 0% | 0% |
| SB | Left Turn | 525 | 25 | 3 | 50 | 5 | 50 | 12 | 0% | 0% |
| | Shared | 525 | 50 | 5 | 100 | 10 | 125 | 18 | 0% | 0% |
| WB | Through | 1,100 | 175 | 21 | 325 | 49 | 400 | 64 | 2% | 0% |
| | Right Turn | 225 | 25 | 19 | 125 | 52 | 225 | 44 | 0% | 0% |
| | | | | | | | | | | |

Intersection 11

Innovation Way/11th Avenue

All-way Stop

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 125 | 25 | 3 | 50 | 5 | 50 | 0 | 0% | 0% |
| | Right Turn | 1,150 | 25 | 2 | 50 | 4 | 75 | 11 | 0% | 0% |
| NB | Left Turn | 125 | 50 | 3 | 75 | 4 | 75 | 9 | 0% | 0% |
| | Left/Through | 500 | 50 | 2 | 75 | 6 | 100 | 15 | 0% | 0% |
| | Through | 500 | 25 | 3 | 50 | 7 | 50 | 8 | 0% | 0% |
| SB | Through | 900 | 25 | 3 | 50 | 6 | 50 | 12 | 0% | 0% |
| | Through/Right | 900 | 100 | 9 | 175 | 27 | 200 | 50 | 0% | 0% |
| | | | | | | | | | | |

Intersection 12

Innovation Way/Juniper Driveway

All-way Stop

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 300 | 25 | 3 | 50 | 4 | 75 | 13 | 0% | 0% |
| | Right Turn | 300 | 25 | 1 | 25 | 7 | 50 | 16 | 0% | 0% |
| NB | Left Turn | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | Through | 900 | 25 | 5 | 50 | 10 | 50 | 13 | 0% | 0% |
| SB | Through/Right | 300 | 175 | 12 | 250 | 17 | 250 | 14 | 0% | 24% |
| | Right Turn | 300 | 100 | 12 | 175 | 21 | 200 | 31 | 0% | 7% |
| | | | | | | | | | | |

Intersection 13

Bordeaux Drive/Innovation Way

All-way Stop

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Through | 800 | 25 | 0 | 25 | 3 | 25 | 9 | 0% | 0% |
| NB | Through | 1,350 | 50 | 3 | 75 | 7 | 75 | 12 | 0% | 0% |
| SB | Through | 675 | 50 | 4 | 75 | 6 | 75 | 13 | 0% | 0% |
| WB | Through | 625 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |

Intersection 1

Mathilda Avenue/5th Avenue

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 625 | 25 | 7 | 75 | 10 | 75 | 16 | 0% | 0% |
| | Through | 625 | 25 | 3 | 25 | 4 | 50 | 5 | 0% | 0% |
| | Right Turn | 625 | 25 | 6 | 50 | 14 | 75 | 17 | 0% | 0% |
| NB | Left Turn | 425 | 75 | 6 | 125 | 9 | 150 | 22 | 0% | 0% |
| | Through | 1,150 | 50 | 6 | 125 | 15 | 150 | 25 | 0% | 0% |
| | Through/Right | 1,150 | 75 | 9 | 150 | 13 | 175 | 20 | 0% | 0% |
| SB | Left Turn | 225 | 25 | 8 | 50 | 53 | 125 | 135 | 0% | 0% |
| | Through | 1,375 | 500 | 140 | 1,050 | 325 | 1,150 | 303 | 47% | 1% |
| | Right Turn | 225 | 25 | 9 | 150 | 33 | 300 | 0 | 0% | 0% |
| WB | Left Turn | 925 | 225 | 99 | 500 | 254 | 600 | 211 | 71% | 2% |
| | Through/Right | 75 | 25 | 5 | 75 | 12 | 100 | 0 | 3% | 0% |

Intersection 2

Mathilda Avenue/Innovation Way-Driveway

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 125 | 50 | 12 | 125 | 19 | 150 | 22 | 0% | 8% |
| | Right Turn | 200 | 225 | 14 | 275 | 16 | 275 | 22 | 0% | 47% |
| NB | Left Turn | 400 | 25 | 6 | 75 | 15 | 100 | 20 | 0% | 0% |
| | Through | 1,075 | 50 | 8 | 125 | 14 | 150 | 31 | 0% | 0% |
| | Through/Right | 1,075 | 75 | 8 | 150 | 17 | 175 | 27 | 0% | 0% |
| SB | Through | 1,150 | 1,000 | 94 | 1,450 | 78 | 1,225 | 15 | 81% | 27% |
| | Right Turn | 225 | 125 | 22 | 350 | 33 | 275 | 0 | 0% | 0% |
| WB | Shared | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |

SimTraffic Post-Processor
Average Results from 10 Runs
Queue Length

Mathilda Avenue Improvements
Existing Conditions
PM Peak Hour

Intersection 3

Mathilda Avenue/Moffett Park Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-------------------------|-----------------------------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB (Moffett Park) | Left Turn | 350 | 500 | 396 | 900 | 492 | 850 | 412 | 1% | 0% |
| | Through/Right | 1,100 | 1,000 | 155 | 1,400 | 139 | 1,200 | 51 | 0% | 24% |
| | Right Turn | 1,100 | 525 | 480 | 625 | 541 | 600 | 512 | 0% | 23% |
| NB | Left Turn (Moffett Park) | 125 | 25 | 2 | 50 | 10 | 75 | 20 | 0% | 4% |
| | Through | 325 | 100 | 11 | 200 | 42 | 250 | 108 | 0% | 29% |
| | Through/Right (Moffett Park) | 325 | 100 | 14 | 200 | 37 | 250 | 103 | 0% | 22% |
| | Left Turn (SR 237 WB On-Ramp) | 200 | 125 | 20 | 225 | 30 | 250 | 21 | 0% | 13% |
| SB | Left Turn (Moffett Park) | 175 | 50 | 8 | 75 | 17 | 125 | 46 | 0% | 0% |
| | Through | 1,200 | 1,175 | 27 | 1,275 | 44 | 1,275 | 41 | 69% | 61% |
| | Through/Right (Moffett Park) | 1,075 | 1,125 | 7 | 1,175 | 26 | 1,175 | 12 | 0% | 48% |
| WB (Moffett Park) | Through/Right (SR 237 WB On-Ramp) | 1,200 | 1,225 | 20 | 1,300 | 43 | 1,275 | 38 | 69% | 79% |
| | Left Turn | 300 | 200 | 22 | 325 | 66 | 350 | 115 | 3% | 0% |
| WB (Moffett Park) | Through/Right | 650 | 150 | 14 | 250 | 33 | 275 | 60 | 0% | 0% |
| | Left Turn | 1,125 | 1,075 | 7 | 1,100 | 32 | 1,100 | 14 | 72% | 60% |
| WB (SR 237 WB Off-Ramp) | Left/Through | 325 | 425 | 4 | 450 | 8 | 450 | 0 | 71% | 0% |
| | Right Turn | 325 | 250 | 30 | 500 | 22 | 375 | 0 | 0% | 0% |

Intersection 4

Mathilda Avenue/SR 237 EB Off-Ramp-SR 237 EB On-Ramp

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,075 | 50 | 5 | 125 | 14 | 150 | 30 | 0% | 0% |
| | Shared | 450 | 150 | 25 | 275 | 49 | 325 | 59 | 0% | 0% |
| NB | Through | 275 | 50 | 21 | 125 | 46 | 175 | 68 | 0% | 1% |
| | Right Turn | 275 | 25 | 5 | 100 | 32 | 175 | 79 | 0% | 0% |
| SB | Left Turn | 200 | 125 | 16 | 225 | 20 | 250 | 26 | 0% | 10% |
| | Through | 200 | 200 | 20 | 300 | 21 | 275 | 18 | 0% | 17% |
| | | | | | | | | | | |

Intersection 5

Mathilda Avenue/Ross Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 650 | 125 | 19 | 250 | 24 | 275 | 31 | 25% | 0% |
| | Through | 75 | 75 | 3 | 125 | 4 | 100 | 0 | 51% | 0% |
| | Right Turn | 50 | 50 | 5 | 75 | 6 | 75 | 2 | 11% | 0% |
| NB | Left Turn | 150 | 75 | 4 | 150 | 9 | 175 | 38 | 2% | 0% |
| | Through | 2,200 | 325 | 28 | 450 | 86 | 450 | 111 | 1% | 4% |
| | Through/Right | 450 | 325 | 19 | 450 | 43 | 450 | 48 | 0% | 3% |
| SB | Left Turn | 125 | 100 | 20 | 200 | 37 | 225 | 4 | 5% | 0% |
| | Through | 250 | 250 | 24 | 350 | 18 | 325 | 25 | 16% | 8% |
| | Through/Right | 250 | 275 | 16 | 350 | 11 | 325 | 20 | 0% | 32% |
| WB | Left Turn | 75 | 575 | 304 | 925 | 429 | 975 | 475 | 71% | 0% |
| | Through | 75 | 100 | 6 | 125 | 6 | 100 | 0 | 3% | 0% |
| | Right Turn | 75 | 50 | 4 | 100 | 4 | 75 | 0 | 5% | 0% |

Intersection 8

Mathilda Avenue/Almanor Avenue-Ahwanee Avenue

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 350 | 175 | 14 | 250 | 25 | 325 | 51 | 28% | 0% |
| | Through/Right | 125 | 75 | 15 | 175 | 32 | 225 | 0 | 2% | 0% |
| NB | Left Turn | 375 | 75 | 7 | 125 | 14 | 150 | 19 | 0% | 0% |
| | Through | 675 | 200 | 20 | 325 | 30 | 350 | 59 | 27% | 0% |
| | Right Turn | 75 | 25 | 6 | 75 | 15 | 100 | 0 | 0% | 0% |
| SB | Left Turn | 125 | 150 | 7 | 200 | 7 | 175 | 0 | 29% | 0% |
| | Through | 2,200 | 925 | 33 | 1,225 | 48 | 1,375 | 49 | 24% | 0% |
| | Through/Right | 350 | 250 | 24 | 400 | 26 | 425 | 48 | 0% | 2% |
| WB | Left Turn | 250 | 50 | 4 | 100 | 9 | 125 | 16 | 0% | 0% |
| | Through | 625 | 25 | 5 | 75 | 11 | 125 | 16 | 0% | 0% |
| | Right Turn | 75 | 50 | 4 | 100 | 7 | 125 | 5 | 9% | 0% |

Intersection 9

US 101 On-Ramp/Moffett Park Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Through | 875 | 400 | 144 | 750 | 298 | 775 | 243 | 37% | 4% |
| | Right Turn | 150 | 100 | 47 | 250 | 141 | 325 | 123 | 0% | 0% |
| WB | Left Turn | 900 | 125 | 32 | 250 | 85 | 325 | 147 | 0% | 0% |
| | | | | | | | | | | |
| | | | | | | | | | | |

Intersection 10

Innovation Way/Moffett Park Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 225 | 100 | 39 | 275 | 118 | 300 | 108 | 0% | 0% |
| | Through | 900 | 475 | 225 | 975 | 349 | 850 | 237 | 35% | 14% |
| SB | Left Turn | 525 | 75 | 46 | 200 | 82 | 300 | 89 | 0% | 0% |
| | Shared | 525 | 150 | 63 | 325 | 99 | 375 | 98 | 0% | 2% |
| WB | Through | 1,100 | 100 | 8 | 150 | 19 | 200 | 28 | 0% | 0% |
| | Right Turn | 225 | 25 | 3 | 25 | 26 | 50 | 70 | 0% | 0% |
| | | | | | | | | | | |

Intersection 11

Innovation Way/11th Avenue

All-way Stop

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 125 | 75 | 3 | 125 | 5 | 125 | 5 | 1% | 0% |
| | Right Turn | 1,150 | 50 | 8 | 100 | 31 | 125 | 74 | 0% | 0% |
| NB | Left Turn | 125 | 25 | 1 | 25 | 6 | 50 | 14 | 0% | 0% |
| | Left/Through | 500 | 50 | 5 | 75 | 5 | 75 | 13 | 0% | 0% |
| | Through | 500 | 25 | 2 | 75 | 4 | 75 | 15 | 0% | 0% |
| SB | Through | 900 | 25 | 3 | 25 | 8 | 50 | 0 | 0% | 0% |
| | Through/Right | 900 | 25 | 3 | 75 | 5 | 75 | 9 | 0% | 0% |
| | | | | | | | | | | |

Intersection 12

Innovation Way/Juniper Driveway

All-way Stop

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 300 | 500 | 243 | 1,000 | 448 | 1,000 | 286 | 0% | 5% |
| | Right Turn | 300 | 75 | 110 | 250 | 390 | 400 | 519 | 0% | 0% |
| NB | Left Turn | 125 | 25 | 4 | 50 | 31 | 100 | 84 | 0% | 0% |
| | Through | 900 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| SB | Through/Right | 300 | 50 | 9 | 100 | 19 | 125 | 40 | 0% | 5% |
| | Right Turn | 300 | 50 | 4 | 100 | 14 | 125 | 37 | 0% | 3% |
| | | | | | | | | | | |

Intersection 13

Bordeaux Drive/Innovation Way

All-way Stop

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NB | Through | 1,350 | 25 | 3 | 50 | 3 | 75 | 12 | 0% | 0% |
| | | | | | | | | | | |
| SB | Through | 675 | 50 | 2 | 75 | 4 | 75 | 8 | 0% | 0% |
| | | | | | | | | | | |
| 0 | | | | | | | | | | |
| WB | Through | 625 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | | | | | | | | | | |

Arterial Level of Service: NB Mathilda Ave

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|----------------------|------|---------------|-----------------|------------|----------------|
| Ahwanee Ave | 8 | 48.7 | 59.7 | 0.1 | 8 |
| US 101 SB Diag. On-R | 702 | 9.2 | 15.8 | 0.1 | 18 |
| US 101 SB Loop On-Ra | 701 | 5.6 | 13.5 | 0.1 | 28 |
| US 101 NB Loop On-Ra | 602 | 13.2 | 19.0 | 0.1 | 13 |
| US 101 NB Diag.Off-R | 601 | 43.1 | 50.1 | 0.1 | 7 |
| Ross Dr | 5 | 67.8 | 75.3 | 0.1 | 4 |
| SR 237 EB On-Ramp | 4 | 41.6 | 47.0 | 0.1 | 5 |
| SR 237 WB Off-Ramp | 33 | 16.3 | 20.0 | 0.0 | 8 |
| Moffett Park Dr | 3 | 5.7 | 8.5 | 0.0 | 18 |
| Innovation Way | 2 | 10.6 | 28.2 | 0.2 | 27 |
| 5th Ave | 1 | 13.7 | 32.5 | 0.2 | 26 |
| | 107 | 4.2 | 26.2 | 0.3 | 37 |
| Total | | 279.7 | 395.7 | 1.5 | 13 |

Arterial Level of Service: SB Mathilda Ave

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|----------------------|------|---------------|-----------------|------------|----------------|
| 5th Ave | 1 | 12.7 | 35.4 | 0.3 | 28 |
| Innovation Way | 2 | 17.8 | 36.6 | 0.2 | 23 |
| Moffett Park Dr | 3 | 53.6 | 70.9 | 0.2 | 11 |
| SR 237 WB On-Ramp | 33 | 55.7 | 58.7 | 0.0 | 3 |
| SR 237 Off/On Ramp | 4 | 17.3 | 21.4 | 0.0 | 8 |
| Ross Dr | 5 | 19.9 | 24.8 | 0.1 | 9 |
| US 101 NB Diag.Off-R | 601 | 6.0 | 14.3 | 0.1 | 23 |
| US 101 NB Loop Off-R | 602 | 2.7 | 8.4 | 0.1 | 39 |
| US 101 SB Loop On-Ra | 701 | 1.2 | 7.2 | 0.1 | 33 |
| US 101 SB Off-Ramp | 702 | 1.9 | 8.6 | 0.1 | 44 |
| Almanor Ave | 8 | 30.5 | 38.6 | 0.1 | 8 |
| San Aleso Ave | 201 | 4.0 | 15.4 | 0.1 | 33 |
| Total | | 223.4 | 340.4 | 1.5 | 15 |

Arterial Level of Service: NB Mathilda Ave

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|----------------------|------|---------------|-----------------|------------|----------------|
| Ahwanee Ave | 8 | 19.9 | 31.0 | 0.1 | 16 |
| US 101 SB Diag. On-R | 702 | 3.3 | 10.0 | 0.1 | 29 |
| US 101 SB Loop On-Ra | 701 | 0.7 | 8.6 | 0.1 | 44 |
| US 101 NB Loop On-Ra | 602 | 0.3 | 6.1 | 0.1 | 39 |
| US 101 NB Diag.Off-R | 601 | 1.3 | 8.3 | 0.1 | 39 |
| Ross Dr | 5 | 53.3 | 60.9 | 0.1 | 5 |
| SR 237 EB On-Ramp | 4 | 30.6 | 36.0 | 0.1 | 6 |
| SR 237 WB Off-Ramp | 33 | 5.5 | 9.3 | 0.0 | 19 |
| Moffett Park Dr | 3 | 39.9 | 42.7 | 0.0 | 3 |
| Innovation Way | 2 | 17.9 | 35.1 | 0.2 | 22 |
| 5th Ave | 1 | 18.6 | 37.2 | 0.2 | 23 |
| | 107 | 3.3 | 25.2 | 0.3 | 39 |
| Total | | 194.5 | 310.5 | 1.5 | 17 |

Arterial Level of Service: SB Mathilda Ave

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|----------------------|------|---------------|-----------------|------------|----------------|
| 5th Ave | 1 | 146.5 | 168.0 | 0.3 | 6 |
| Innovation Way | 2 | 268.7 | 286.0 | 0.2 | 3 |
| Moffett Park Dr | 3 | 204.1 | 220.2 | 0.2 | 3 |
| SR 237 WB On-Ramp | 33 | 5.7 | 8.7 | 0.0 | 17 |
| SR 237 Off/On Ramp | 4 | 9.6 | 13.8 | 0.0 | 13 |
| Ross Dr | 5 | 19.4 | 24.5 | 0.1 | 10 |
| US 101 NB Diag.Off-R | 601 | 24.1 | 32.3 | 0.1 | 10 |
| US 101 NB Loop Off-R | 602 | 9.8 | 15.4 | 0.1 | 21 |
| US 101 SB Loop On-Ra | 701 | 3.6 | 9.7 | 0.1 | 25 |
| US 101 SB Off-Ramp | 702 | 2.0 | 8.6 | 0.1 | 44 |
| Almanor Ave | 8 | 23.4 | 31.6 | 0.1 | 9 |
| San Aleso Ave | 201 | 5.1 | 16.5 | 0.1 | 31 |
| Total | | 722.1 | 835.2 | 1.5 | 6 |

Lanes, Volumes, Timings

1: Mathilda Ave & 5th Ave

12/11/2015



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------|-------|------|--------|-------|-------|------|-------|-------|------|-------|------|--------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 14 | 6 | 17 | 19 | 8 | 2 | 52 | 890 | 61 | 7 | 330 | 59 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 0 | | 0 | 310 | | 50 | 400 | | 0 | 220 | | 220 |
| Storage Lanes | 2 | | 1 | 1 | | 1 | 2 | | 0 | 1 | | 1 |
| Taper Length (ft) | 90 | | | 30 | | | 170 | | | 60 | | |
| Lane Util. Factor | 0.97 | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 | 0.97 | 0.91 | 0.91 | 1.00 | 0.91 | 1.00 |
| Ped Bike Factor | | | 0.93 | | 1.00 | | | 1.00 | | | | 0.98 |
| Frt | | | 0.850 | | 0.973 | | | 0.990 | | | | 0.850 |
| Flt Protected | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 3433 | 1863 | 1583 | 3433 | 1805 | 0 | 3433 | 5020 | 0 | 1770 | 5085 | 1583 |
| Flt Permitted | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (perm) | 3433 | 1863 | 1478 | 3433 | 1805 | 0 | 3433 | 5020 | 0 | 1770 | 5085 | 1548 |
| Right Turn on Red | | | No | | | Yes | | | Yes | | | No |
| Satd. Flow (RTOR) | | | | | 2 | | | 5 | | | | |
| Link Speed (mph) | | 25 | | | 25 | | | 45 | | | 45 | |
| Link Distance (ft) | | 107 | | | 1003 | | | 1249 | | | 1438 | |
| Travel Time (s) | | 2.9 | | | 27.4 | | | 18.9 | | | 21.8 | |
| Confl. Peds. (#/hr) | | | 23 | | | 4 | | | 6 | | | 5 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 15 | 7 | 18 | 21 | 9 | 2 | 57 | 967 | 66 | 8 | 359 | 64 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 15 | 7 | 18 | 21 | 11 | 0 | 57 | 1033 | 0 | 8 | 359 | 64 |
| Turn Type | Prot | NA | custom | Prot | NA | | Prot | NA | | Prot | NA | custom |
| Protected Phases | 7 13 | 4 13 | | 3 | 8 | | 5 | 2 9 | | 1 | 6 9 | |
| Permitted Phases | | | 4 | | | | | | | | | 6 |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | | 5 | 2 | | 1 | 6 | 6 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 13.0 | 12.0 | 8.0 | | 11.0 | | | 10.0 | | 12.0 |
| Minimum Split (s) | | | 38.1 | 16.5 | 38.1 | | 15.5 | | | 14.5 | | 41.3 |
| Total Split (s) | | | 38.1 | 34.5 | 38.1 | | 34.5 | | | 34.5 | | 70.3 |
| Total Split (%) | | | 14.8% | 13.4% | 14.8% | | 13.4% | | | 13.4% | | 27.3% |
| Yellow Time (s) | | | 5.1 | 3.5 | 5.1 | | 3.5 | | | 3.5 | | 4.3 |
| All-Red Time (s) | | | 1.0 | 1.0 | 1.0 | | 1.0 | | | 1.0 | | 1.0 |
| Lost Time Adjust (s) | | | 0.0 | 0.0 | 0.0 | | 0.0 | | | 0.0 | | 0.0 |
| Total Lost Time (s) | | | 6.1 | 4.5 | 6.1 | | 4.5 | | | 4.5 | | 5.3 |
| Lead/Lag | | | Lag | Lead | Lag | | Lead | | | Lead | | Lag |
| Lead-Lag Optimize? | | | Yes | Yes | Yes | | Yes | | | Yes | | Yes |
| Recall Mode | | | None | None | None | | None | | | None | | Min |

Intersection Summary

Area Type: Other

Cycle Length: 257.6

Actuated Cycle Length: 77.5

Natural Cycle: 180

Control Type: Actuated-Uncoordinated

Splits and Phases: 1: Mathilda Ave & 5th Ave

| | | | | |
|--------|--------|--------|--------|-------------|
| | | | | |
| 34.5 s | 70.5 s | 34.5 s | 38.1 s | 14 s 50 s |
| | | | | |
| 34.5 s | 70.3 s | 50.5 s | 38.1 s | |

Lanes, Volumes, Timings
 1: Mathilda Ave & 5th Ave

12/11/2015

| Lane Group | ø2 | ø7 | ø9 | ø13 |
|-----------------------------|------|------|------|------|
| Lane Configurations | | | | |
| Volume (vph) | | | | |
| Ideal Flow (vphpl) | | | | |
| Storage Length (ft) | | | | |
| Storage Lanes | | | | |
| Taper Length (ft) | | | | |
| Lane Util. Factor | | | | |
| Ped Bike Factor | | | | |
| Frt | | | | |
| Flt Protected | | | | |
| Satd. Flow (prot) | | | | |
| Flt Permitted | | | | |
| Satd. Flow (perm) | | | | |
| Right Turn on Red | | | | |
| Satd. Flow (RTOR) | | | | |
| Link Speed (mph) | | | | |
| Link Distance (ft) | | | | |
| Travel Time (s) | | | | |
| Confl. Peds. (#/hr) | | | | |
| Peak Hour Factor | | | | |
| Adj. Flow (vph) | | | | |
| Shared Lane Traffic (%) | | | | |
| Lane Group Flow (vph) | | | | |
| Turn Type | | | | |
| Protected Phases | 2 | 7 | 9 | 13 |
| Permitted Phases | | | | |
| Detector Phase | | | | |
| Switch Phase | | | | |
| Minimum Initial (s) | 12.0 | 12.0 | 46.0 | 10.0 |
| Minimum Split (s) | 35.5 | 17.5 | 50.0 | 14.0 |
| Total Split (s) | 70.5 | 50.5 | 50.0 | 14.0 |
| Total Split (%) | 27% | 20% | 19% | 5% |
| Yellow Time (s) | 4.5 | 4.5 | 3.0 | 3.0 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | | | | |
| Total Lost Time (s) | | | | |
| Lead/Lag | Lag | Lead | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes |
| Recall Mode | Min | None | None | None |
| Intersection Summary | | | | |

Lanes, Volumes, Timings
2: Mathilda Ave & Innovation Way

12/11/2015



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------|-------|------|-------|-------|-------|------|-------|------|------|-------|------|--------|
| Lane Configurations | ↖ | | ↗↘ | | ↔ | | ↖↗ | ↕↔ | | ↖ | ↕↕↕ | ↗ |
| Volume (vph) | 14 | 0 | 37 | 0 | 0 | 0 | 619 | 989 | 0 | 1 | 265 | 100 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 170 | | 0 | 0 | | 0 | 390 | | 0 | 70 | | 210 |
| Storage Lanes | 0 | | 2 | 0 | | 0 | 2 | | 0 | 1 | | 1 |
| Taper Length (ft) | 30 | | | 25 | | | 90 | | | 60 | | |
| Lane Util. Factor | 1.00 | 1.00 | 0.88 | 1.00 | 1.00 | 1.00 | 0.97 | 0.91 | 0.91 | 1.00 | 0.91 | 1.00 |
| Ped Bike Factor | | | | | | | | | | | | 0.99 |
| Frt | | | 0.850 | | | | | | | | | 0.850 |
| Flt Protected | 0.950 | | | | | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1770 | 0 | 2787 | 0 | 1863 | 0 | 3433 | 5085 | 0 | 1770 | 5085 | 1583 |
| Flt Permitted | 0.950 | | | | | | 0.950 | | | 0.950 | | |
| Satd. Flow (perm) | 1770 | 0 | 2787 | 0 | 1863 | 0 | 3433 | 5085 | 0 | 1770 | 5085 | 1561 |
| Right Turn on Red | | | No | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | | | | | | | | | | | 112 |
| Link Speed (mph) | | 25 | | | 25 | | | 45 | | | 45 | |
| Link Distance (ft) | | 121 | | | 908 | | | 1130 | | | 1249 | |
| Travel Time (s) | | 3.3 | | | 24.8 | | | 17.1 | | | 18.9 | |
| Confl. Peds. (#/hr) | | | 5 | | | 2 | | | | | | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 15 | 0 | 40 | 0 | 0 | 0 | 673 | 1075 | 0 | 1 | 288 | 109 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 15 | 0 | 40 | 0 | 0 | 0 | 673 | 1075 | 0 | 1 | 288 | 109 |
| Turn Type | Prot | | Prot | | | | Prot | NA | | Prot | NA | custom |
| Protected Phases | 4 13 | | 4 | | 8 | | 5 | 2 9 | | 1 | 6 9 | |
| Permitted Phases | | | | 8 | | | | | | | | 6 |
| Detector Phase | 4 | | 4 | 8 | 8 | | 5 | 2 | | 1 | 6 | 6 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 14.0 | 10.0 | 10.0 | | 13.0 | | | 10.0 | | 12.0 |
| Minimum Split (s) | | | 39.0 | 39.0 | 39.0 | | 18.0 | | | 14.0 | | 41.3 |
| Total Split (s) | | | 45.0 | 39.0 | 39.0 | | 45.0 | | | 34.0 | | 40.3 |
| Total Split (%) | | | 19.3% | 16.7% | 16.7% | | 19.3% | | | 14.6% | | 17.3% |
| Yellow Time (s) | | | 4.0 | 4.0 | 4.0 | | 4.0 | | | 3.0 | | 4.3 |
| All-Red Time (s) | | | 1.0 | 1.0 | 1.0 | | 1.0 | | | 1.0 | | 1.0 |
| Lost Time Adjust (s) | | | 0.0 | | 0.0 | | 0.0 | | | 0.0 | | 0.0 |
| Total Lost Time (s) | | | 5.0 | | 5.0 | | 5.0 | | | 4.0 | | 5.3 |
| Lead/Lag | | | | | | | Lead | | | Lead | | Lag |
| Lead-Lag Optimize? | | | | | | | Yes | | | Yes | | Yes |
| Recall Mode | | | None | None | None | | None | | | None | | Min |

Intersection Summary

Area Type: Other

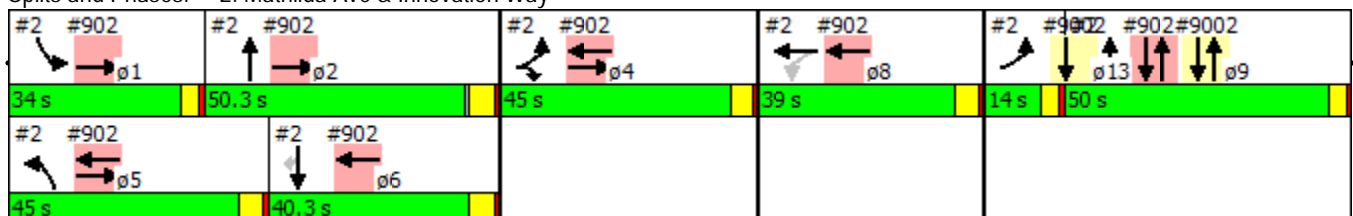
Cycle Length: 233.3

Actuated Cycle Length: 100.4

Natural Cycle: 205

Control Type: Semi Act-Uncoord

Splits and Phases: 2: Mathilda Ave & Innovation Way



| Lane Group | ø2 | ø9 | ø13 |
|-----------------------------|------|------|------|
| Lane Configurations | | | |
| Volume (vph) | | | |
| Ideal Flow (vphpl) | | | |
| Storage Length (ft) | | | |
| Storage Lanes | | | |
| Taper Length (ft) | | | |
| Lane Util. Factor | | | |
| Ped Bike Factor | | | |
| Frt | | | |
| Flt Protected | | | |
| Satd. Flow (prot) | | | |
| Flt Permitted | | | |
| Satd. Flow (perm) | | | |
| Right Turn on Red | | | |
| Satd. Flow (RTOR) | | | |
| Link Speed (mph) | | | |
| Link Distance (ft) | | | |
| Travel Time (s) | | | |
| Confl. Peds. (#/hr) | | | |
| Peak Hour Factor | | | |
| Adj. Flow (vph) | | | |
| Shared Lane Traffic (%) | | | |
| Lane Group Flow (vph) | | | |
| Turn Type | | | |
| Protected Phases | 2 | 9 | 13 |
| Permitted Phases | | | |
| Detector Phase | | | |
| Switch Phase | | | |
| Minimum Initial (s) | 12.0 | 46.0 | 10.0 |
| Minimum Split (s) | 17.3 | 50.0 | 14.0 |
| Total Split (s) | 50.3 | 50.0 | 14.0 |
| Total Split (%) | 22% | 21% | 6% |
| Yellow Time (s) | 4.3 | 3.0 | 3.0 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | | | |
| Total Lost Time (s) | | | |
| Lead/Lag | Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes | Yes |
| Recall Mode | Min | None | None |
| Intersection Summary | | | |

Lanes, Volumes, Timings
3: Mathilda Ave & Moffett Park Dr

12/11/2015



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------|-------|-------|-------|-------|-------|------|-------|-------|------|-------|-------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 31 | 54 | 45 | 72 | 189 | 24 | 637 | 1553 | 759 | 8 | 197 | 97 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 263 | | 0 | 280 | | 0 | 90 | | 0 | 150 | | 0 |
| Storage Lanes | 0 | | 1 | 2 | | 0 | 0 | | 0 | 2 | | 0 |
| Taper Length (ft) | 55 | | | 240 | | | 0 | | | 90 | | |
| Lane Util. Factor | 1.00 | 0.95 | 0.95 | 0.97 | 1.00 | 1.00 | 0.97 | 0.91 | 0.91 | 1.00 | 0.86 | 0.86 |
| Ped Bike Factor | | | | | 1.00 | | | 0.99 | | | | |
| Frt | | 0.988 | 0.850 | | 0.983 | | | 0.951 | | | 0.951 | |
| Flt Protected | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1770 | 1748 | 1504 | 3433 | 1828 | 0 | 3433 | 4791 | 0 | 1770 | 6094 | 0 |
| Flt Permitted | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (perm) | 1770 | 1748 | 1504 | 3433 | 1828 | 0 | 3433 | 4791 | 0 | 1770 | 6094 | 0 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | 3 | 65 | | 5 | | | 133 | | | 85 | |
| Link Speed (mph) | | 40 | | | 40 | | | 45 | | | 45 | |
| Link Distance (ft) | | 265 | | | 725 | | | 221 | | | 1130 | |
| Travel Time (s) | | 4.5 | | | 12.4 | | | 3.3 | | | 17.1 | |
| Confl. Peds. (#/hr) | | | | | | 1 | | | 4 | | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 34 | 59 | 49 | 78 | 205 | 26 | 692 | 1688 | 825 | 9 | 214 | 105 |
| Shared Lane Traffic (%) | | | 10% | | | | | | | | | |
| Lane Group Flow (vph) | 34 | 64 | 44 | 78 | 231 | 0 | 692 | 2513 | 0 | 9 | 319 | 0 |
| Turn Type | Prot | NA | pm+ov | Prot | NA | | Prot | NA | | Prot | NA | |
| Protected Phases | 7 | 4 | 5 | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | | | 4 | | | | | | | | | |
| Detector Phase | 7 | 4 | 5 | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 8.0 | 8.0 | 4.0 | 8.0 | 8.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Minimum Split (s) | 12.0 | 12.9 | 8.0 | 12.0 | 38.9 | | 8.0 | 33.3 | | 8.0 | 9.3 | |
| Total Split (s) | 12.0 | 23.0 | 49.0 | 28.0 | 39.0 | | 49.0 | 59.0 | | 10.0 | 20.0 | |
| Total Split (%) | 10.0% | 19.2% | 40.8% | 23.3% | 32.5% | | 40.8% | 49.2% | | 8.3% | 16.7% | |
| Yellow Time (s) | 3.0 | 3.9 | 3.0 | 3.0 | 3.9 | | 3.0 | 4.3 | | 3.0 | 4.3 | |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | | 1.0 | 1.0 | | 1.0 | 1.0 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | 4.0 | 4.9 | 4.0 | 4.0 | 4.9 | | 4.0 | 5.3 | | 4.0 | 5.3 | |
| Lead/Lag | Lead | Lead | Lag | Lag | Lag | | Lag | Lead | | Lag | Lead | |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | | Yes | Yes | | Yes | Yes | |
| Recall Mode | None | None | C-Max | None | None | | C-Max | C-Max | | None | None | |

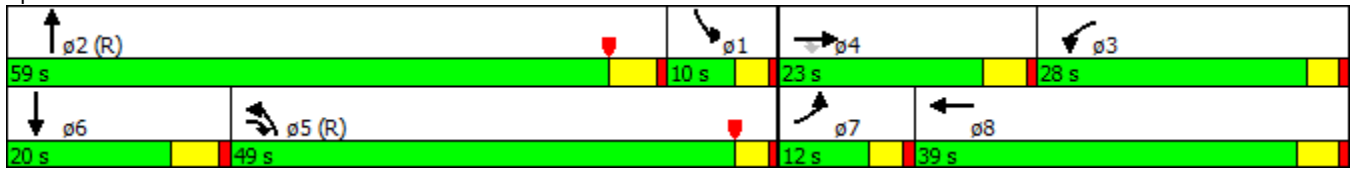
Intersection Summary

Area Type: Other
 Cycle Length: 120
 Actuated Cycle Length: 120
 Offset: 90 (75%), Referenced to phase 2:NBT and 5:NBL, Start of Yellow
 Natural Cycle: 125
 Control Type: Actuated-Coordinated

Lanes, Volumes, Timings
 3: Mathilda Ave & Moffett Park Dr

12/11/2015

Splits and Phases: 3: Mathilda Ave & Moffett Park Dr



Lanes, Volumes, Timings

4: Mathilda Ave & SR 237 Off/On Ramp/SR 237 EB On-Ramp

12/11/2015



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------|-------|-------|------|------|------|------|------|-------|-------|-------|-------|------|
| Lane Configurations | ↔↔ | ↔ | | | | | | ↑↑↑↑ | ↔ | ↔ | ↑↑↑↑ | |
| Volume (vph) | 770 | 0 | 70 | 0 | 0 | 0 | 0 | 1980 | 721 | 44 | 865 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 440 | | 430 | 0 | | 0 | 0 | | 0 | 0 | | 0 |
| Storage Lanes | 0 | | 1 | 0 | | 0 | 0 | | 1 | 1 | | 0 |
| Taper Length (ft) | 25 | | | 25 | | | 25 | | | 25 | | |
| Lane Util. Factor | 0.91 | 0.91 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.81 | 1.00 | 1.00 | 0.91 | 1.00 |
| Ped Bike Factor | | | | | | | | | 0.99 | | | |
| Frt | | 0.962 | | | | | | | 0.850 | | | |
| Flt Protected | 0.950 | 0.964 | | | | | | | | 0.950 | | |
| Satd. Flow (prot) | 3221 | 1572 | 0 | 0 | 0 | 0 | 0 | 7544 | 1583 | 1770 | 5085 | 0 |
| Flt Permitted | 0.950 | 0.964 | | | | | | | | 0.950 | | |
| Satd. Flow (perm) | 3221 | 1572 | 0 | 0 | 0 | 0 | 0 | 7544 | 1560 | 1770 | 5085 | 0 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | 87 | | | | | | | 784 | | | |
| Link Speed (mph) | | 45 | | | 45 | | | 45 | | | 45 | |
| Link Distance (ft) | | 1145 | | | 778 | | | 341 | | | 246 | |
| Travel Time (s) | | 17.3 | | | 11.8 | | | 5.2 | | | 3.7 | |
| Confl. Bikes (#/hr) | | | | | | | | | 5 | | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 837 | 0 | 76 | 0 | 0 | 0 | 0 | 2152 | 784 | 48 | 940 | 0 |
| Shared Lane Traffic (%) | 27% | | | | | | | | | | | |
| Lane Group Flow (vph) | 611 | 302 | 0 | 0 | 0 | 0 | 0 | 2152 | 784 | 48 | 940 | 0 |
| Turn Type | Split | NA | | | | | | NA | Perm | Prot | NA | |
| Protected Phases | 4 | 4 | | | | | | 2 | | 1 | 6 | |
| Permitted Phases | | | | | | | | | 2 | | | |
| Detector Phase | 4 | 4 | | | | | | 2 | 2 | 1 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | | | | | | 4.0 | 4.0 | 4.0 | 4.0 | |
| Minimum Split (s) | 10.9 | 10.9 | | | | | | 20.3 | 20.3 | 10.3 | 10.3 | |
| Total Split (s) | 45.0 | 45.0 | | | | | | 60.0 | 60.0 | 15.0 | 75.0 | |
| Total Split (%) | 37.5% | 37.5% | | | | | | 50.0% | 50.0% | 12.5% | 62.5% | |
| Yellow Time (s) | 3.9 | 3.9 | | | | | | 4.3 | 4.3 | 4.3 | 4.3 | |
| All-Red Time (s) | 2.0 | 2.0 | | | | | | 2.0 | 2.0 | 2.0 | 2.0 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | | | | | | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | 5.9 | 5.9 | | | | | | 6.3 | 6.3 | 6.3 | 6.3 | |
| Lead/Lag | | | | | | | | Lead | Lead | Lag | | |
| Lead-Lag Optimize? | | | | | | | | Yes | Yes | Yes | | |
| Recall Mode | None | None | | | | | | C-Max | C-Max | None | None | |

Intersection Summary

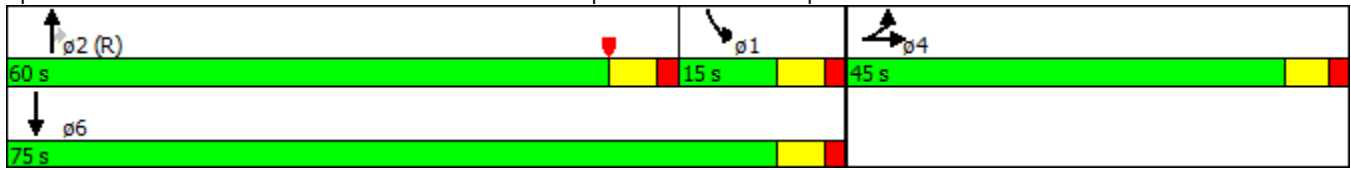
Area Type: Other
 Cycle Length: 120
 Actuated Cycle Length: 120
 Offset: 114 (95%), Referenced to phase 2:NBT, Start of Yellow
 Natural Cycle: 60
 Control Type: Actuated-Coordinated

Lanes, Volumes, Timings

4: Mathilda Ave & SR 237 Off/On Ramp/SR 237 EB On-Ramp

12/11/2015

Splits and Phases: 4: Mathilda Ave & SR 237 Off/On Ramp/SR 237 EB On-Ramp



Lanes, Volumes, Timings
5: Mathilda Ave & Ross Dr

12/11/2015



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------|-------|-------|-------|-------|-------|-------|-------|-------|------|-------|-------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 74 | 53 | 18 | 105 | 22 | 239 | 50 | 2388 | 96 | 50 | 849 | 36 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 80 | | 30 | 30 | | 60 | 130 | | 0 | 100 | | 0 |
| Storage Lanes | 0 | | 2 | 0 | | 2 | 1 | | 0 | 1 | | 0 |
| Taper Length (ft) | 30 | | | 25 | | | 90 | | | 120 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.81 | 0.81 | 1.00 | 0.91 | 0.91 |
| Ped Bike Factor | | | 0.98 | 1.00 | | | | 1.00 | | | | |
| Frt | | | 0.850 | | | 0.850 | | 0.994 | | | 0.994 | |
| Flt Protected | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1770 | 1863 | 1583 | 1770 | 1863 | 1583 | 1770 | 7490 | 0 | 1770 | 5055 | 0 |
| Flt Permitted | 0.742 | | | 0.719 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (perm) | 1382 | 1863 | 1557 | 1333 | 1863 | 1583 | 1770 | 7490 | 0 | 1770 | 5055 | 0 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | | 105 | | | 245 | | 10 | | | 7 | |
| Link Speed (mph) | | 25 | | | 25 | | | 45 | | | 45 | |
| Link Distance (ft) | | 696 | | | 2916 | | | 487 | | | 341 | |
| Travel Time (s) | | 19.0 | | | 79.5 | | | 7.4 | | | 5.2 | |
| Confl. Peds. (#/hr) | | | 5 | 5 | | | | | 5 | | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 80 | 58 | 20 | 114 | 24 | 260 | 54 | 2596 | 104 | 54 | 923 | 39 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 80 | 58 | 20 | 114 | 24 | 260 | 54 | 2700 | 0 | 54 | 962 | 0 |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | Prot | NA | | Prot | NA | |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | | | | | | |
| Detector Phase | 4 | 4 | 4 | 8 | 8 | 8 | 5 | 2 | | 1 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 4.0 | 5.0 | | 4.0 | 5.0 | |
| Minimum Split (s) | 40.0 | 40.0 | 40.0 | 10.0 | 10.0 | 10.0 | 8.0 | 32.3 | | 8.0 | 10.3 | |
| Total Split (s) | 40.0 | 40.0 | 40.0 | 40.0 | 40.0 | 40.0 | 20.0 | 60.0 | | 20.0 | 60.0 | |
| Total Split (%) | 33.3% | 33.3% | 33.3% | 33.3% | 33.3% | 33.3% | 16.7% | 50.0% | | 16.7% | 50.0% | |
| Yellow Time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 4.3 | | 3.0 | 4.3 | |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | | 1.0 | 1.0 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 5.3 | | 4.0 | 5.3 | |
| Lead/Lag | | | | | | | Lead | Lead | | Lag | Lag | |
| Lead-Lag Optimize? | | | | | | | Yes | Yes | | Yes | Yes | |
| Recall Mode | None | None | None | None | None | None | None | C-Max | | None | None | |

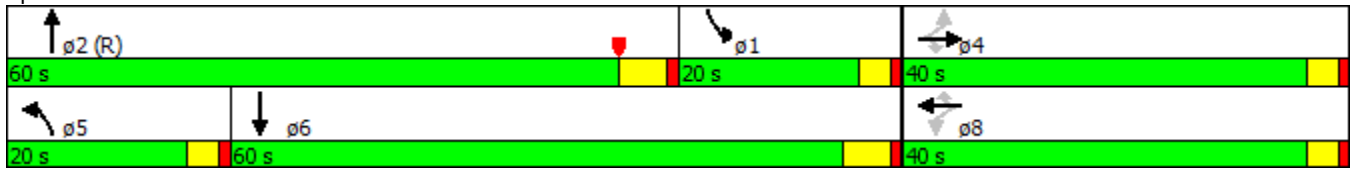
Intersection Summary

Area Type: Other
 Cycle Length: 120
 Actuated Cycle Length: 120
 Offset: 0 (0%), Referenced to phase 2:NBT, Start of Yellow, Master Intersection
 Natural Cycle: 85
 Control Type: Actuated-Coordinated

Lanes, Volumes, Timings
5: Mathilda Ave & Ross Dr

12/11/2015

Splits and Phases: 5: Mathilda Ave & Ross Dr



Lanes, Volumes, Timings
 8: Mathilda Ave & Almanor Ave/Ahwanee Ave

12/11/2015



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------|-------|-------|------|-------|-------|-------|-------|-------|-------|-------|-------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 75 | 11 | 21 | 70 | 27 | 171 | 107 | 2458 | 46 | 144 | 1505 | 278 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 320 | | 120 | 230 | | 50 | 350 | | 70 | 110 | | 0 |
| Storage Lanes | 1 | | 1 | 1 | | 1 | 1 | | 1 | 1 | | 0 |
| Taper Length (ft) | 90 | | | 120 | | | 25 | | | 60 | | |
| Lane Util. Factor | 0.97 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.86 | 1.00 | 1.00 | 0.86 | 0.86 |
| Ped Bike Factor | | 0.97 | | | | | | | | | 1.00 | |
| Frt | | 0.901 | | | | 0.850 | | | 0.850 | | 0.977 | |
| Flt Protected | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 3433 | 1635 | 0 | 1770 | 1863 | 1583 | 1770 | 6408 | 1583 | 1770 | 6235 | 0 |
| Flt Permitted | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (perm) | 3433 | 1635 | 0 | 1770 | 1863 | 1583 | 1770 | 6408 | 1583 | 1770 | 6235 | 0 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | 23 | | | | 186 | | | 90 | | 41 | |
| Link Speed (mph) | | 30 | | | 30 | | | 45 | | | 45 | |
| Link Distance (ft) | | 422 | | | 706 | | | 740 | | | 427 | |
| Travel Time (s) | | 9.6 | | | 16.0 | | | 11.2 | | | 6.5 | |
| Confl. Peds. (#/hr) | | | 32 | | | | | | | | | 2 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 82 | 12 | 23 | 76 | 29 | 186 | 116 | 2672 | 50 | 157 | 1636 | 302 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 82 | 35 | 0 | 76 | 29 | 186 | 116 | 2672 | 50 | 157 | 1938 | 0 |
| Turn Type | Prot | NA | | Prot | NA | Perm | Prot | NA | Perm | Prot | NA | |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | | | | | | 8 | | | 2 | | | |
| Detector Phase | 7 | 4 | | 3 | 8 | 8 | 5 | 2 | 2 | 1 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 8.0 | 8.0 | | 8.0 | 8.0 | 8.0 | 8.0 | 12.0 | 12.0 | 8.0 | 12.0 | |
| Minimum Split (s) | 12.1 | 46.7 | | 12.1 | 12.7 | 12.7 | 12.1 | 17.3 | 17.3 | 12.1 | 26.3 | |
| Total Split (s) | 13.0 | 47.0 | | 13.0 | 47.0 | 47.0 | 16.0 | 44.0 | 44.0 | 16.0 | 44.0 | |
| Total Split (%) | 10.8% | 39.2% | | 10.8% | 39.2% | 39.2% | 13.3% | 36.7% | 36.7% | 13.3% | 36.7% | |
| Yellow Time (s) | 3.1 | 3.7 | | 3.1 | 3.7 | 3.7 | 3.1 | 4.3 | 4.3 | 3.1 | 4.3 | |
| All-Red Time (s) | 1.0 | 1.0 | | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | 4.1 | 4.7 | | 4.1 | 4.7 | 4.7 | 4.1 | 5.3 | 5.3 | 4.1 | 5.3 | |
| Lead/Lag | Lead | Lag | | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | |
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | |
| Recall Mode | None | None | | None | None | None | None | C-Max | C-Max | None | C-Max | |









Intersection Summary

Area Type: Other
 Cycle Length: 120
 Actuated Cycle Length: 120
 Offset: 73 (61%), Referenced to phase 2:NBT and 6:SBT, Start of Yellow
 Natural Cycle: 140
 Control Type: Actuated-Coordinated

Lanes, Volumes, Timings
 8: Mathilda Ave & Almanor Ave/Ahwanee Ave

12/11/2015

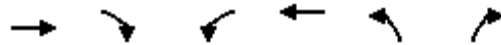
Splits and Phases: 8: Mathilda Ave & Almanor Ave/Ahwanee Ave

| | | | |
|--|--|--|---|
|  $\phi 1$ 16 s |  $\phi 2 (R)$ 44 s |  $\phi 3$ 13 s |  $\phi 4$ 47 s |
|  $\phi 5$ 16 s |  $\phi 6 (R)$ 44 s |  $\phi 7$ 13 s |  $\phi 8$ 47 s |

Lanes, Volumes, Timings

9: US 101 On-Ramp & Moffett Park Dr

12/11/2015

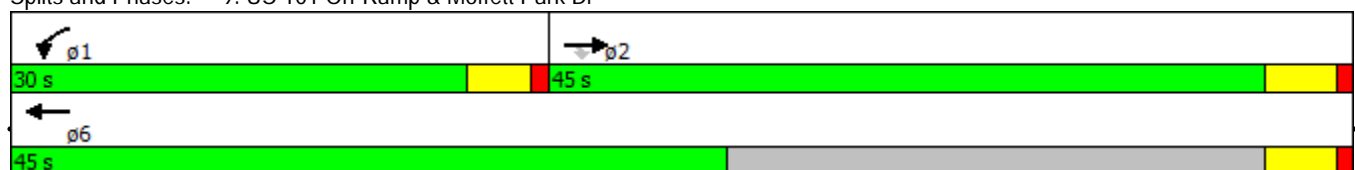


| Lane Group | EBT | EBR | WBL | WBT | NBL | NBR |
|-------------------------|-------|-------|-------|-------|------|------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ | | |
| Volume (vph) | 151 | 1 | 16 | 873 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | | 130 | 0 | | 0 | 0 |
| Storage Lanes | | 1 | 1 | | 0 | 0 |
| Taper Length (ft) | | | 25 | | 25 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | | 0.850 | | | | |
| Flt Protected | | | 0.950 | | | |
| Satd. Flow (prot) | 1863 | 1583 | 1770 | 1863 | 0 | 0 |
| Flt Permitted | | | 0.950 | | | |
| Satd. Flow (perm) | 1863 | 1583 | 1770 | 1863 | 0 | 0 |
| Right Turn on Red | | Yes | | | | Yes |
| Satd. Flow (RTOR) | | 1 | | | | |
| Link Speed (mph) | 30 | | | 30 | 30 | |
| Link Distance (ft) | 939 | | | 921 | 120 | |
| Travel Time (s) | 21.3 | | | 20.9 | 2.7 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 164 | 1 | 17 | 949 | 0 | 0 |
| Shared Lane Traffic (%) | | | | | | |
| Lane Group Flow (vph) | 164 | 1 | 17 | 949 | 0 | 0 |
| Turn Type | NA | Perm | Prot | NA | | |
| Protected Phases | 2 | | 1 | 6 | | |
| Permitted Phases | | 2 | | | | |
| Detector Phase | 2 | 2 | 1 | 6 | | |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 15.0 | 15.0 | 6.0 | 15.0 | | |
| Minimum Split (s) | 20.0 | 20.0 | 10.5 | 20.0 | | |
| Total Split (s) | 45.0 | 45.0 | 30.0 | 45.0 | | |
| Total Split (%) | 60.0% | 60.0% | 40.0% | 60.0% | | |
| Yellow Time (s) | 4.0 | 4.0 | 3.5 | 4.0 | | |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | | |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | | |
| Total Lost Time (s) | 5.0 | 5.0 | 4.5 | 5.0 | | |
| Lead/Lag | Lag | Lag | Lead | | | |
| Lead-Lag Optimize? | | | | | | |
| Recall Mode | Min | Min | None | Min | | |

Intersection Summary

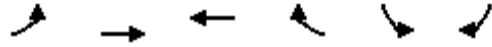
Area Type: Other
 Cycle Length: 75
 Actuated Cycle Length: 42.8
 Natural Cycle: 40
 Control Type: Semi Act-Uncoord

Splits and Phases: 9: US 101 On-Ramp & Moffett Park Dr



Lanes, Volumes, Timings
 10: Moffett Park Dr & Innovation Way

12/11/2015

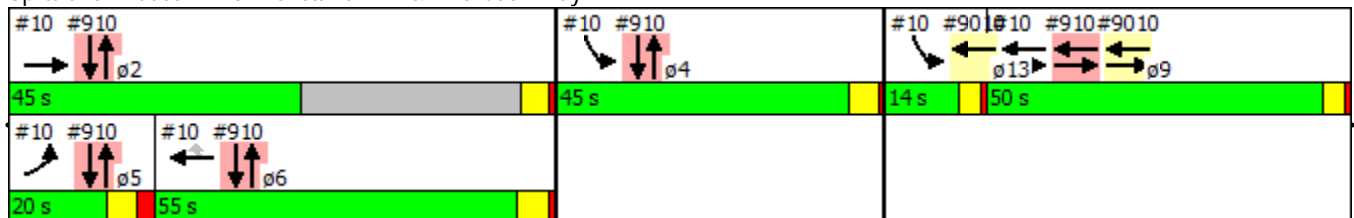


| Lane Group | EBL | EBT | WBT | WBR | SBL | SBR | ø2 | ø4 | ø9 | ø13 |
|-------------------------|-------|------|------|--------|-------|------|------|------|------|------|
| Lane Configurations | ↖ | ↑↑ | ↑↑ | ↗ | ↘↘ | | | | | |
| Volume (vph) | 49 | 102 | 789 | 134 | 32 | 100 | | | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | | | | |
| Storage Length (ft) | 200 | | | 200 | 0 | 0 | | | | |
| Storage Lanes | 1 | | | 1 | 2 | 0 | | | | |
| Taper Length (ft) | 140 | | | | 25 | | | | | |
| Lane Util. Factor | 1.00 | 0.95 | 0.95 | 1.00 | 0.97 | 0.95 | | | | |
| Frt | | | | 0.850 | 0.886 | | | | | |
| Flt Protected | 0.950 | | | | 0.988 | | | | | |
| Satd. Flow (prot) | 1770 | 3539 | 3539 | 1583 | 3163 | 0 | | | | |
| Flt Permitted | 0.950 | | | | 0.988 | | | | | |
| Satd. Flow (perm) | 1770 | 3539 | 3539 | 1583 | 3163 | 0 | | | | |
| Right Turn on Red | | | | Yes | | No | | | | |
| Satd. Flow (RTOR) | | | | 78 | | | | | | |
| Link Speed (mph) | | 40 | 40 | | 30 | | | | | |
| Link Distance (ft) | | 921 | 1032 | | 121 | | | | | |
| Travel Time (s) | | 15.7 | 17.6 | | 2.8 | | | | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | | | | |
| Adj. Flow (vph) | 53 | 111 | 858 | 146 | 35 | 109 | | | | |
| Shared Lane Traffic (%) | | | | | | | | | | |
| Lane Group Flow (vph) | 53 | 111 | 858 | 146 | 144 | 0 | | | | |
| Turn Type | Prot | NA | NA | custom | Prot | | | | | |
| Protected Phases | 5 | 2 9 | 6 9 | | 4 13 | | 2 | 4 | 9 | 13 |
| Permitted Phases | | | | 6 | | | | | | |
| Detector Phase | 5 | 2 | 6 | 6 | 4 | | | | | |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 8.0 | | | 10.0 | | | 10.0 | 10.0 | 46.0 | 10.0 |
| Minimum Split (s) | 14.5 | | | 15.5 | | | 14.9 | 15.0 | 50.0 | 14.0 |
| Total Split (s) | 20.0 | | | 55.0 | | | 45.0 | 45.0 | 50.0 | 14.0 |
| Total Split (%) | 10.9% | | | 29.9% | | | 24% | 24% | 27% | 8% |
| Yellow Time (s) | 4.0 | | | 4.5 | | | 3.9 | 4.0 | 3.0 | 3.0 |
| All-Red Time (s) | 2.5 | | | 1.0 | | | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | | | 0.0 | | | | | | |
| Total Lost Time (s) | 6.5 | | | 5.5 | | | | | | |
| Lead/Lag | Lead | | | Lag | | | | | Lag | Lead |
| Lead-Lag Optimize? | Yes | | | Yes | | | | | Yes | Yes |
| Recall Mode | None | | | Min | | | Min | None | None | None |

Intersection Summary

Area Type: Other
 Cycle Length: 184
 Actuated Cycle Length: 70.9
 Natural Cycle: 110
 Control Type: Actuated-Uncoordinated

Splits and Phases: 10: Moffett Park Dr & Innovation Way



Lanes, Volumes, Timings
11: Innovation Way & 11th Ave

12/11/2015



| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
|-------------------------|-------|-------|-------|-------|-------|------|
| Lane Configurations | | | | | | |
| Volume (vph) | 9 | 55 | 169 | 14 | 77 | 344 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 100 | 0 | 100 | | | 0 |
| Storage Lanes | 1 | 2 | 1 | | | 0 |
| Taper Length (ft) | 30 | | 60 | | | |
| Lane Util. Factor | 1.00 | 0.88 | 0.91 | 0.91 | 0.95 | 0.95 |
| Ped Bike Factor | | | | | | |
| Frt | | 0.850 | | | 0.878 | |
| Flt Protected | 0.950 | | 0.950 | 0.959 | | |
| Satd. Flow (prot) | 1770 | 2787 | 1610 | 3251 | 3107 | 0 |
| Flt Permitted | 0.950 | | 0.950 | 0.959 | | |
| Satd. Flow (perm) | 1770 | 2787 | 1610 | 3251 | 3107 | 0 |
| Link Speed (mph) | 25 | | | 25 | 25 | |
| Link Distance (ft) | 1177 | | | 601 | 841 | |
| Travel Time (s) | 32.1 | | | 16.4 | 22.9 | |
| Confl. Peds. (#/hr) | 5 | 5 | 5 | | | 5 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 10 | 60 | 184 | 15 | 84 | 374 |
| Shared Lane Traffic (%) | | | 50% | | | |
| Lane Group Flow (vph) | 10 | 60 | 92 | 107 | 458 | 0 |
| Sign Control | Stop | | | Stop | Stop | |

Intersection Summary

Area Type: Other

Control Type: Unsignalized

Lanes, Volumes, Timings
 12: Innovation Way & Juniper Driveway

12/11/2015



















| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
|-------------------------|-------|-------|------|------|-------|-------|
| Lane Configurations | | | | | | |
| Volume (vph) | 28 | 1 | 0 | 23 | 420 | 299 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 0 | 0 | 100 | | | 0 |
| Storage Lanes | 1 | 1 | 1 | | | 1 |
| Taper Length (ft) | 25 | | 60 | | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 |
| Ped Bike Factor | | | | | | |
| Frt | | 0.850 | | | 0.990 | 0.850 |
| Flt Protected | 0.950 | | | | | |
| Satd. Flow (prot) | 1770 | 1583 | 1863 | 3539 | 1752 | 1504 |
| Flt Permitted | 0.950 | | | | | |
| Satd. Flow (perm) | 1770 | 1583 | 1863 | 3539 | 1752 | 1504 |
| Link Speed (mph) | 30 | | | 25 | 25 | |
| Link Distance (ft) | 335 | | | 299 | 197 | |
| Travel Time (s) | 7.6 | | | 8.2 | 5.4 | |
| Confl. Peds. (#/hr) | | 5 | 5 | | | 5 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 30 | 1 | 0 | 25 | 457 | 325 |
| Shared Lane Traffic (%) | | | | | | 10% |
| Lane Group Flow (vph) | 30 | 1 | 0 | 25 | 490 | 292 |
| Sign Control | Stop | | | Stop | Stop | |

Intersection Summary

Area Type: Other
 Control Type: Unsignalized

Lanes, Volumes, Timings
 13: Bordeaux Dr & Innovation Way/Driveway

12/11/2015

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | |  | | |  | | |  | | |  | |
| Volume (vph) | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 99 | 0 | 0 | 41 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | | | | | | | | | | | | |
| Flt | | | | | | | | | | | | |
| Flt Protected | | | | | | | | | | | | |
| Satd. Flow (prot) | 0 | 1863 | 0 | 0 | 1863 | 0 | 0 | 1863 | 0 | 0 | 1863 | 0 |
| Flt Permitted | | | | | | | | | | | | |
| Satd. Flow (perm) | 0 | 1863 | 0 | 0 | 1863 | 0 | 0 | 1863 | 0 | 0 | 1863 | 0 |
| Link Speed (mph) | 30 | | | | 25 | | | | 30 | | 30 | |
| Link Distance (ft) | 908 | | | | 601 | | | | 1425 | | 725 | |
| Travel Time (s) | 20.6 | | | | 16.4 | | | | 32.4 | | 16.5 | |
| Confl. Peds. (#/hr) | 2 | | | | | | | | | 1 | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 108 | 0 | 0 | 45 | 0 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 108 | 0 | 0 | 45 | 0 |
| Sign Control | Stop | | | | Stop | | | | Stop | | Stop | |
| Intersection Summary | | | | | | | | | | | | |
| Area Type: | Other | | | | | | | | | | | |
| Control Type: | Unsignalized | | | | | | | | | | | |

Lanes, Volumes, Timings

33: Mathilda Ave & SR 237 WB On-Ramp/SR 237 WB Off-Ramp

12/11/2015



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------|------|------|------|-------|-------|-------|-------|-------|------|------|-------|------|
| Lane Configurations | | | | ↙ | ↖ | ↗ | ↘ | ↑↑↑ | | | ↑↑↑ | ↘ |
| Volume (vph) | 0 | 0 | 0 | 663 | 23 | 334 | 135 | 2615 | 0 | 0 | 246 | 68 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 0 | | 0 | 310 | | 310 | 0 | | 0 | 0 | | 0 |
| Storage Lanes | 0 | | 0 | 0 | | 2 | 1 | | 0 | 0 | | 0 |
| Taper Length (ft) | 25 | | | 25 | | | 25 | | | 25 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 1.00 | 0.86 | 1.00 | 1.00 | 0.86 | 0.86 |
| Ped Bike Factor | | | | | | | | | | | | |
| Frt | | | | | | 0.850 | | | | | 0.967 | |
| Flt Protected | | | | 0.950 | 0.955 | | 0.950 | | | | | |
| Satd. Flow (prot) | 0 | 0 | 0 | 1681 | 1690 | 1583 | 1770 | 6408 | 0 | 0 | 6196 | 0 |
| Flt Permitted | | | | 0.950 | 0.955 | | 0.950 | | | | | |
| Satd. Flow (perm) | 0 | 0 | 0 | 1681 | 1690 | 1583 | 1770 | 6408 | 0 | 0 | 6196 | 0 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | | | | | 69 | | | | | | 74 |
| Link Speed (mph) | | 30 | | | 45 | | | 45 | | | | 45 |
| Link Distance (ft) | | 107 | | | 1242 | | | 246 | | | | 221 |
| Travel Time (s) | | 2.4 | | | 18.8 | | | 3.7 | | | | 3.3 |
| Confl. Peds. (#/hr) | | | | | | | | | 12 | | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 0 | 0 | 0 | 721 | 25 | 363 | 147 | 2842 | 0 | 0 | 267 | 74 |
| Shared Lane Traffic (%) | | | | 48% | | | | | | | | |
| Lane Group Flow (vph) | 0 | 0 | 0 | 375 | 371 | 363 | 147 | 2842 | 0 | 0 | 341 | 0 |
| Turn Type | | | | Split | NA | Perm | Prot | NA | | | NA | |
| Protected Phases | | | | 8 | 8 | | 5 | 2 | | | 6 | |
| Permitted Phases | | | | | | 8 | | | | | | |
| Detector Phase | | | | 8 | 8 | 8 | 5 | 2 | | | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | 4.0 | |
| Minimum Split (s) | | | | 8.9 | 8.9 | 8.9 | 9.3 | 18.3 | | | 9.3 | |
| Total Split (s) | | | | 30.0 | 30.0 | 30.0 | 25.0 | 90.0 | | | 65.0 | |
| Total Split (%) | | | | 25.0% | 25.0% | 25.0% | 20.8% | 75.0% | | | 54.2% | |
| Yellow Time (s) | | | | 3.9 | 3.9 | 3.9 | 4.3 | 4.3 | | | 4.3 | |
| All-Red Time (s) | | | | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | | | 1.0 | |
| Lost Time Adjust (s) | | | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | 0.0 | |
| Total Lost Time (s) | | | | 4.9 | 4.9 | 4.9 | 5.3 | 5.3 | | | 5.3 | |
| Lead/Lag | | | | | | | Lag | | | | Lead | |
| Lead-Lag Optimize? | | | | | | | Yes | | | | Yes | |
| Recall Mode | | | | Max | Max | Max | None | C-Max | | | None | |

Intersection Summary

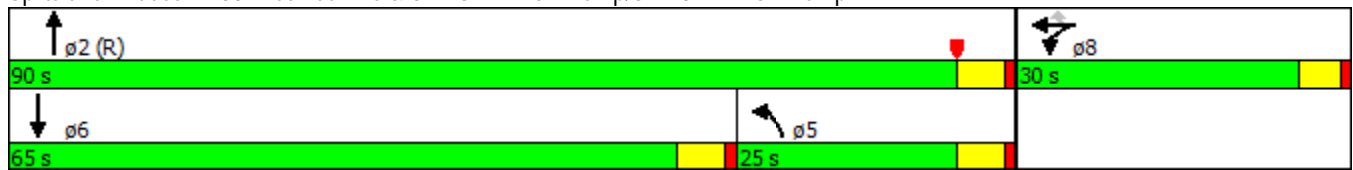
Area Type: Other
 Cycle Length: 120
 Actuated Cycle Length: 120
 Offset: 83 (69%), Referenced to phase 2:NBT, Start of Yellow
 Natural Cycle: 50
 Control Type: Actuated-Coordinated

Lanes, Volumes, Timings

33: Mathilda Ave & SR 237 WB On-Ramp/SR 237 WB Off-Ramp

12/11/2015

Splits and Phases: 33: Mathilda Ave & SR 237 WB On-Ramp/SR 237 WB Off-Ramp



Lanes, Volumes, Timings

1: Mathilda Ave & 5th Ave

12/11/2015



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------|-------|------|--------|-------|-------|------|-------|-------|------|-------|------|--------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 38 | 17 | 51 | 229 | 4 | 8 | 97 | 329 | 37 | 3 | 1102 | 9 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 0 | | 0 | 310 | | 50 | 400 | | 0 | 220 | | 220 |
| Storage Lanes | 2 | | 1 | 1 | | 1 | 2 | | 0 | 1 | | 1 |
| Taper Length (ft) | 90 | | | 30 | | | 170 | | | 60 | | |
| Lane Util. Factor | 0.97 | 1.00 | 1.00 | 0.97 | 1.00 | 1.00 | 0.97 | 0.91 | 0.91 | 1.00 | 0.91 | 1.00 |
| Ped Bike Factor | | | 0.91 | | 0.99 | | | 1.00 | | | | 0.99 |
| Frt | | | 0.850 | | 0.900 | | | 0.985 | | | | 0.850 |
| Flt Protected | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 3433 | 1863 | 1583 | 3433 | 1655 | 0 | 3433 | 4990 | 0 | 1770 | 5085 | 1583 |
| Flt Permitted | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (perm) | 3433 | 1863 | 1433 | 3433 | 1655 | 0 | 3433 | 4990 | 0 | 1770 | 5085 | 1561 |
| Right Turn on Red | | | No | | | Yes | | | Yes | | | No |
| Satd. Flow (RTOR) | | | | | 8 | | | 9 | | | | |
| Link Speed (mph) | | 25 | | | 25 | | | 45 | | | 45 | |
| Link Distance (ft) | | 107 | | | 1003 | | | 1249 | | | 1438 | |
| Travel Time (s) | | 2.9 | | | 27.4 | | | 18.9 | | | 21.8 | |
| Confl. Peds. (#/hr) | | | 35 | | | 3 | | | 4 | | | 1 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 39 | 18 | 53 | 236 | 4 | 8 | 100 | 339 | 38 | 3 | 1136 | 9 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 39 | 18 | 53 | 236 | 12 | 0 | 100 | 377 | 0 | 3 | 1136 | 9 |
| Turn Type | Prot | NA | custom | Prot | NA | | Prot | NA | | Prot | NA | custom |
| Protected Phases | 7 13 | 4 13 | | 3 | 8 | | 5 | 2 9 | | 1 | 6 9 | |
| Permitted Phases | | | 4 | | | | | | | | | 6 |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | | 5 | 2 | | 1 | 6 | 6 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 13.0 | 12.0 | 8.0 | | 11.0 | | | 10.0 | | 12.0 |
| Minimum Split (s) | | | 38.1 | 16.5 | 38.1 | | 15.5 | | | 14.5 | | 41.3 |
| Total Split (s) | | | 38.1 | 34.5 | 38.1 | | 34.5 | | | 34.5 | | 70.3 |
| Total Split (%) | | | 14.8% | 13.4% | 14.8% | | 13.4% | | | 13.4% | | 27.3% |
| Yellow Time (s) | | | 5.1 | 3.5 | 5.1 | | 3.5 | | | 3.5 | | 4.3 |
| All-Red Time (s) | | | 1.0 | 1.0 | 1.0 | | 1.0 | | | 1.0 | | 1.0 |
| Lost Time Adjust (s) | | | 0.0 | 0.0 | 0.0 | | 0.0 | | | 0.0 | | 0.0 |
| Total Lost Time (s) | | | 6.1 | 4.5 | 6.1 | | 4.5 | | | 4.5 | | 5.3 |
| Lead/Lag | | | Lag | Lead | Lag | | Lead | | | Lead | | Lag |
| Lead-Lag Optimize? | | | Yes | Yes | Yes | | Yes | | | Yes | | Yes |
| Recall Mode | | | None | None | None | | None | | | None | | Min |

Intersection Summary

Area Type: Other
 Cycle Length: 257.6
 Actuated Cycle Length: 108.1
 Natural Cycle: 180
 Control Type: Actuated-Uncoordinated

Splits and Phases: 1: Mathilda Ave & 5th Ave

| | | | | |
|--------|--------|--------|--------|-------------|
| | | | | |
| 34.5 s | 70.5 s | 34.5 s | 38.1 s | 14 s 50 s |
| | | | | |
| 34.5 s | 70.3 s | 50.5 s | 38.1 s | |

Lanes, Volumes, Timings
1: Mathilda Ave & 5th Ave

12/11/2015

| Lane Group | ø2 | ø7 | ø9 | ø13 |
|-----------------------------|------|------|------|------|
| Lane Configurations | | | | |
| Volume (vph) | | | | |
| Ideal Flow (vphpl) | | | | |
| Storage Length (ft) | | | | |
| Storage Lanes | | | | |
| Taper Length (ft) | | | | |
| Lane Util. Factor | | | | |
| Ped Bike Factor | | | | |
| Frt | | | | |
| Flt Protected | | | | |
| Satd. Flow (prot) | | | | |
| Flt Permitted | | | | |
| Satd. Flow (perm) | | | | |
| Right Turn on Red | | | | |
| Satd. Flow (RTOR) | | | | |
| Link Speed (mph) | | | | |
| Link Distance (ft) | | | | |
| Travel Time (s) | | | | |
| Confl. Peds. (#/hr) | | | | |
| Peak Hour Factor | | | | |
| Adj. Flow (vph) | | | | |
| Shared Lane Traffic (%) | | | | |
| Lane Group Flow (vph) | | | | |
| Turn Type | | | | |
| Protected Phases | 2 | 7 | 9 | 13 |
| Permitted Phases | | | | |
| Detector Phase | | | | |
| Switch Phase | | | | |
| Minimum Initial (s) | 12.0 | 12.0 | 46.0 | 10.0 |
| Minimum Split (s) | 35.5 | 17.5 | 50.0 | 14.0 |
| Total Split (s) | 70.5 | 50.5 | 50.0 | 14.0 |
| Total Split (%) | 27% | 20% | 19% | 5% |
| Yellow Time (s) | 4.5 | 4.5 | 3.0 | 3.0 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | | | | |
| Total Lost Time (s) | | | | |
| Lead/Lag | Lag | Lead | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes |
| Recall Mode | Min | None | None | None |
| Intersection Summary | | | | |

Lanes, Volumes, Timings
2: Mathilda Ave & Innovation Way

12/11/2015



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------|-------|------|-------|-------|-------|------|-------|------|------|-------|------|--------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 87 | 0 | 622 | 0 | 0 | 0 | 61 | 376 | 0 | 0 | 1346 | 36 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 170 | | 0 | 0 | | 0 | 390 | | 0 | 70 | | 210 |
| Storage Lanes | 0 | | 2 | 0 | | 0 | 2 | | 0 | 1 | | 1 |
| Taper Length (ft) | 30 | | | 25 | | | 90 | | | 60 | | |
| Lane Util. Factor | 1.00 | 1.00 | 0.88 | 1.00 | 1.00 | 1.00 | 0.97 | 0.91 | 0.91 | 1.00 | 0.91 | 1.00 |
| Ped Bike Factor | | | | | | | | | | | | 0.99 |
| Frt | | | 0.850 | | | | | | | | | 0.850 |
| Flt Protected | 0.950 | | | | | | 0.950 | | | | | |
| Satd. Flow (prot) | 1770 | 0 | 2787 | 0 | 1863 | 0 | 3433 | 5085 | 0 | 1863 | 5085 | 1583 |
| Flt Permitted | 0.950 | | | | | | 0.950 | | | | | |
| Satd. Flow (perm) | 1770 | 0 | 2787 | 0 | 1863 | 0 | 3433 | 5085 | 0 | 1863 | 5085 | 1561 |
| Right Turn on Red | | | No | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | | | | | | | | | | | 89 |
| Link Speed (mph) | | 25 | | | 25 | | | 45 | | | 45 | |
| Link Distance (ft) | | 121 | | | 908 | | | 1130 | | | 1249 | |
| Travel Time (s) | | 3.3 | | | 24.8 | | | 17.1 | | | 18.9 | |
| Confl. Peds. (#/hr) | | | | | | 2 | | | 4 | | | 1 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 90 | 0 | 641 | 0 | 0 | 0 | 63 | 388 | 0 | 0 | 1388 | 37 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 90 | 0 | 641 | 0 | 0 | 0 | 63 | 388 | 0 | 0 | 1388 | 37 |
| Turn Type | Prot | | Prot | | | | Prot | NA | | Prot | NA | custom |
| Protected Phases | 4 13 | | 4 | | 8 | | 5 | 2 9 | | 1 | 6 9 | |
| Permitted Phases | | | | 8 | | | | | | | | 6 |
| Detector Phase | 4 | | 4 | 8 | 8 | | 5 | 2 | | 1 | 6 | 6 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 14.0 | 10.0 | 10.0 | | 13.0 | | | 10.0 | | 12.0 |
| Minimum Split (s) | | | 39.0 | 39.0 | 39.0 | | 18.0 | | | 14.0 | | 41.3 |
| Total Split (s) | | | 45.0 | 39.0 | 39.0 | | 35.0 | | | 34.0 | | 50.3 |
| Total Split (%) | | | 19.3% | 16.7% | 16.7% | | 15.0% | | | 14.6% | | 21.6% |
| Yellow Time (s) | | | 4.0 | 4.0 | 4.0 | | 4.0 | | | 3.0 | | 4.3 |
| All-Red Time (s) | | | 1.0 | 1.0 | 1.0 | | 1.0 | | | 1.0 | | 1.0 |
| Lost Time Adjust (s) | | | 0.0 | | 0.0 | | 0.0 | | | 0.0 | | 0.0 |
| Total Lost Time (s) | | | 5.0 | | 5.0 | | 5.0 | | | 4.0 | | 5.3 |
| Lead/Lag | | | | | | | Lead | | | Lead | | Lag |
| Lead-Lag Optimize? | | | | | | | Yes | | | Yes | | Yes |
| Recall Mode | | | Max | None | None | | None | | | None | | Min |

Intersection Summary

Area Type: Other

Cycle Length: 233.3

Actuated Cycle Length: 132.2

Natural Cycle: 205

Control Type: Semi Act-Uncoord

Splits and Phases: 2: Mathilda Ave & Innovation Way

| | | | | | |
|--|--|--|--|--|--|
| | | | | | |
| | | | | | |

Lanes, Volumes, Timings
 2: Mathilda Ave & Innovation Way

12/11/2015

| Lane Group | ø2 | ø9 | ø13 |
|-----------------------------|------|------|------|
| Lane Configurations | | | |
| Volume (vph) | | | |
| Ideal Flow (vphpl) | | | |
| Storage Length (ft) | | | |
| Storage Lanes | | | |
| Taper Length (ft) | | | |
| Lane Util. Factor | | | |
| Ped Bike Factor | | | |
| Frt | | | |
| Flt Protected | | | |
| Satd. Flow (prot) | | | |
| Flt Permitted | | | |
| Satd. Flow (perm) | | | |
| Right Turn on Red | | | |
| Satd. Flow (RTOR) | | | |
| Link Speed (mph) | | | |
| Link Distance (ft) | | | |
| Travel Time (s) | | | |
| Confl. Peds. (#/hr) | | | |
| Peak Hour Factor | | | |
| Adj. Flow (vph) | | | |
| Shared Lane Traffic (%) | | | |
| Lane Group Flow (vph) | | | |
| Turn Type | | | |
| Protected Phases | 2 | 9 | 13 |
| Permitted Phases | | | |
| Detector Phase | | | |
| Switch Phase | | | |
| Minimum Initial (s) | 12.0 | 46.0 | 10.0 |
| Minimum Split (s) | 17.3 | 50.0 | 14.0 |
| Total Split (s) | 50.3 | 50.0 | 14.0 |
| Total Split (%) | 22% | 21% | 6% |
| Yellow Time (s) | 4.3 | 3.0 | 3.0 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | | | |
| Total Lost Time (s) | | | |
| Lead/Lag | Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes | Yes |
| Recall Mode | Min | None | None |
| Intersection Summary | | | |

Lanes, Volumes, Timings
3: Mathilda Ave & Moffett Park Dr

12/11/2015



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------|-------|-------|-------|-------|-------|------|-------|-------|------|-------|-------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 44 | 165 | 403 | 285 | 237 | 20 | 84 | 373 | 145 | 39 | 1858 | 71 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 263 | | 0 | 280 | | 0 | 90 | | 0 | 150 | | 0 |
| Storage Lanes | 0 | | 1 | 2 | | 0 | 0 | | 0 | 2 | | 0 |
| Taper Length (ft) | 55 | | | 240 | | | 0 | | | 90 | | |
| Lane Util. Factor | 1.00 | 0.95 | 0.95 | 0.97 | 1.00 | 1.00 | 0.97 | 0.91 | 0.91 | 1.00 | 0.86 | 0.86 |
| Ped Bike Factor | | | | | 1.00 | | | 0.98 | | | | |
| Frt | | 0.933 | 0.850 | | 0.988 | | | 0.958 | | | 0.994 | |
| Flt Protected | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1770 | 1651 | 1504 | 3433 | 1838 | 0 | 3433 | 4788 | 0 | 1770 | 6369 | 0 |
| Flt Permitted | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (perm) | 1770 | 1651 | 1504 | 3433 | 1838 | 0 | 3433 | 4788 | 0 | 1770 | 6369 | 0 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | 27 | 122 | | 3 | | | 68 | | | 6 | |
| Link Speed (mph) | | 40 | | | 40 | | | 45 | | | 45 | |
| Link Distance (ft) | | 265 | | | 725 | | | 214 | | | 1130 | |
| Travel Time (s) | | 4.5 | | | 12.4 | | | 3.2 | | | 17.1 | |
| Confl. Peds. (#/hr) | | | | | | 2 | | | 17 | | | |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 45 | 170 | 415 | 294 | 244 | 21 | 87 | 385 | 149 | 40 | 1915 | 73 |
| Shared Lane Traffic (%) | | | 33% | | | | | | | | | |
| Lane Group Flow (vph) | 45 | 307 | 278 | 294 | 265 | 0 | 87 | 534 | 0 | 40 | 1988 | 0 |
| Turn Type | Prot | NA | pm+ov | Prot | NA | | Prot | NA | | Prot | NA | |
| Protected Phases | 7 | 4 | 5 | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | | | 4 | | | | | | | | | |
| Detector Phase | 7 | 4 | 5 | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 8.0 | 8.0 | 4.0 | 8.0 | 8.0 | | 4.0 | 4.0 | | 4.0 | 4.0 | |
| Minimum Split (s) | 12.0 | 12.9 | 8.0 | 12.0 | 38.9 | | 8.0 | 33.3 | | 8.0 | 9.3 | |
| Total Split (s) | 29.0 | 38.0 | 13.0 | 35.0 | 44.0 | | 13.0 | 43.0 | | 24.0 | 54.0 | |
| Total Split (%) | 20.7% | 27.1% | 9.3% | 25.0% | 31.4% | | 9.3% | 30.7% | | 17.1% | 38.6% | |
| Yellow Time (s) | 3.0 | 3.9 | 3.0 | 3.0 | 3.9 | | 3.0 | 4.3 | | 3.0 | 4.3 | |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | | 1.0 | 1.0 | | 1.0 | 1.0 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | 4.0 | 4.9 | 4.0 | 4.0 | 4.9 | | 4.0 | 5.3 | | 4.0 | 5.3 | |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | | Lag | Lead | | Lag | Lead | |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | | Yes | Yes | | Yes | Yes | |
| Recall Mode | None | Max | Max | Max | None | | Max | Max | | None | C-Max | |

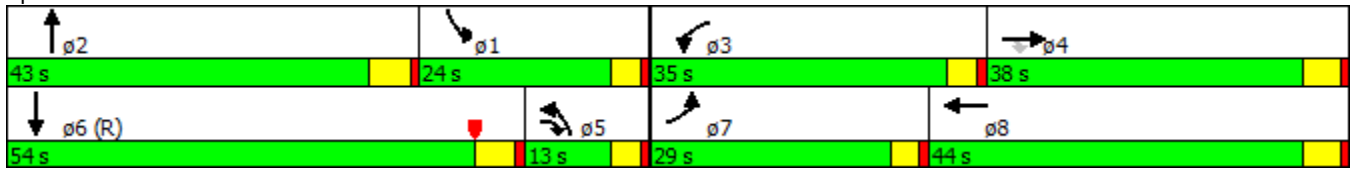
Intersection Summary

Area Type: Other
 Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 0 (0%), Referenced to phase 6:SBT, Start of Yellow, Master Intersection
 Natural Cycle: 95
 Control Type: Actuated-Coordinated

Lanes, Volumes, Timings
 3: Mathilda Ave & Moffett Park Dr

12/11/2015

Splits and Phases: 3: Mathilda Ave & Moffett Park Dr



Lanes, Volumes, Timings

4: Mathilda Ave & SR 237 Off/On Ramp/SR 237 EB On-Ramp

12/11/2015



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------|-------|-------|------|------|------|------|------|-------|-------|-------|-------|------|
| Lane Configurations | ↖↗ | ↕ | | | | | | ↑↑↑↑ | ↖ | ↗ | ↑↑↑↑ | |
| Volume (vph) | 166 | 29 | 195 | 0 | 0 | 0 | 0 | 354 | 625 | 331 | 2521 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 440 | | 430 | 0 | | 0 | 0 | | 0 | 0 | | 0 |
| Storage Lanes | 0 | | 1 | 0 | | 0 | 0 | | 1 | 1 | | 0 |
| Taper Length (ft) | 25 | | | 25 | | | 25 | | | 25 | | |
| Lane Util. Factor | 0.91 | 0.91 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.81 | 1.00 | 1.00 | 0.91 | 1.00 |
| Ped Bike Factor | | | | | | | | | 0.99 | | | |
| Frt | | 0.878 | | | | | | | 0.850 | | | |
| Flt Protected | 0.950 | 0.997 | | | | | | | | 0.950 | | |
| Satd. Flow (prot) | 3221 | 1484 | 0 | 0 | 0 | 0 | 0 | 7544 | 1583 | 1770 | 5085 | 0 |
| Flt Permitted | 0.950 | 0.997 | | | | | | | | 0.950 | | |
| Satd. Flow (perm) | 3221 | 1484 | 0 | 0 | 0 | 0 | 0 | 7544 | 1560 | 1770 | 5085 | 0 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | 6 | | | | | | | 520 | | | |
| Link Speed (mph) | | 45 | | | 45 | | | 45 | | | 45 | |
| Link Distance (ft) | | 1146 | | | 778 | | | 341 | | | 254 | |
| Travel Time (s) | | 17.4 | | | 11.8 | | | 5.2 | | | 3.8 | |
| Confl. Bikes (#/hr) | | | | | | | | | 5 | | | |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 171 | 30 | 201 | 0 | 0 | 0 | 0 | 365 | 644 | 341 | 2599 | 0 |
| Shared Lane Traffic (%) | 10% | | | | | | | | | | | |
| Lane Group Flow (vph) | 154 | 248 | 0 | 0 | 0 | 0 | 0 | 365 | 644 | 341 | 2599 | 0 |
| Turn Type | Split | NA | | | | | | NA | Perm | Prot | NA | |
| Protected Phases | 4 | 4 | | | | | | 2 | | 1 | 6 | |
| Permitted Phases | | | | | | | | | 2 | | | |
| Detector Phase | 4 | 4 | | | | | | 2 | 2 | 1 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | | | | | | 4.0 | 4.0 | 4.0 | 4.0 | |
| Minimum Split (s) | 10.9 | 10.9 | | | | | | 20.3 | 20.3 | 10.3 | 10.3 | |
| Total Split (s) | 36.0 | 36.0 | | | | | | 61.0 | 61.0 | 43.0 | 104.0 | |
| Total Split (%) | 25.7% | 25.7% | | | | | | 43.6% | 43.6% | 30.7% | 74.3% | |
| Yellow Time (s) | 3.9 | 3.9 | | | | | | 4.3 | 4.3 | 4.3 | 4.3 | |
| All-Red Time (s) | 2.0 | 2.0 | | | | | | 2.0 | 2.0 | 2.0 | 2.0 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | | | | | | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | 5.9 | 5.9 | | | | | | 6.3 | 6.3 | 6.3 | 6.3 | |
| Lead/Lag | | | | | | | | Lag | Lag | Lead | | |
| Lead-Lag Optimize? | | | | | | | | Yes | Yes | Yes | | |
| Recall Mode | Max | Max | | | | | | None | None | Max | C-Max | |

Intersection Summary

Area Type: Other
 Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 50 (36%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 75
 Control Type: Actuated-Coordinated

Lanes, Volumes, Timings

4: Mathilda Ave & SR 237 Off/On Ramp/SR 237 EB On-Ramp

12/11/2015

Splits and Phases: 4: Mathilda Ave & SR 237 Off/On Ramp/SR 237 EB On-Ramp



Lanes, Volumes, Timings
5: Mathilda Ave & Ross Dr

12/11/2015



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------|-------|-------|-------|-------|-------|-------|-------|-------|------|-------|-------|------|
| Lane Configurations | ↖ | ↑ | ↗ | ↖ | ↑ | ↗ | ↖ | ↑↑↑↑ | | ↖ | ↑↑↑ | |
| Volume (vph) | 39 | 143 | 35 | 210 | 48 | 97 | 87 | 843 | 252 | 130 | 2499 | 87 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 80 | | 30 | 30 | | 60 | 130 | | 0 | 100 | | 0 |
| Storage Lanes | 0 | | 2 | 0 | | 2 | 1 | | 0 | 1 | | 0 |
| Taper Length (ft) | 30 | | | 25 | | | 90 | | | 120 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.81 | 0.81 | 1.00 | 0.91 | 0.91 |
| Ped Bike Factor | | | 0.98 | 1.00 | | | | 0.99 | | | | |
| Frt | | | 0.850 | | | 0.850 | | 0.965 | | | 0.995 | |
| Flt Protected | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1770 | 1863 | 1583 | 1770 | 1863 | 1583 | 1770 | 7225 | 0 | 1770 | 5060 | 0 |
| Flt Permitted | 0.725 | | | 0.586 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (perm) | 1350 | 1863 | 1555 | 1087 | 1863 | 1583 | 1770 | 7225 | 0 | 1770 | 5060 | 0 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | | 90 | | | 100 | | 74 | | | 5 | |
| Link Speed (mph) | | 25 | | | 25 | | | 45 | | | 45 | |
| Link Distance (ft) | | 696 | | | 2916 | | | 487 | | | 341 | |
| Travel Time (s) | | 19.0 | | | 79.5 | | | 7.4 | | | 5.2 | |
| Confl. Peds. (#/hr) | | | 5 | 5 | | | | | 5 | | | |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 40 | 147 | 36 | 216 | 49 | 100 | 90 | 869 | 260 | 134 | 2576 | 90 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 40 | 147 | 36 | 216 | 49 | 100 | 90 | 1129 | 0 | 134 | 2666 | 0 |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | Prot | NA | | Prot | NA | |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | | | | | | |
| Detector Phase | 4 | 4 | 4 | 8 | 8 | 8 | 5 | 2 | | 1 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 4.0 | 5.0 | | 4.0 | 5.0 | |
| Minimum Split (s) | 40.0 | 40.0 | 40.0 | 10.0 | 10.0 | 10.0 | 8.0 | 32.3 | | 8.0 | 10.3 | |
| Total Split (s) | 45.0 | 45.0 | 45.0 | 45.0 | 45.0 | 45.0 | 23.0 | 72.0 | | 23.0 | 72.0 | |
| Total Split (%) | 32.1% | 32.1% | 32.1% | 32.1% | 32.1% | 32.1% | 16.4% | 51.4% | | 16.4% | 51.4% | |
| Yellow Time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 4.3 | | 3.0 | 4.3 | |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | | 1.0 | 1.0 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | |
| Total Lost Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 5.3 | | 4.0 | 5.3 | |
| Lead/Lag | | | | | | | Lead | Lead | | Lag | Lag | |
| Lead-Lag Optimize? | | | | | | | Yes | Yes | | Yes | Yes | |
| Recall Mode | Max | Max | Max | Max | Max | Max | Max | None | | None | C-Max | |

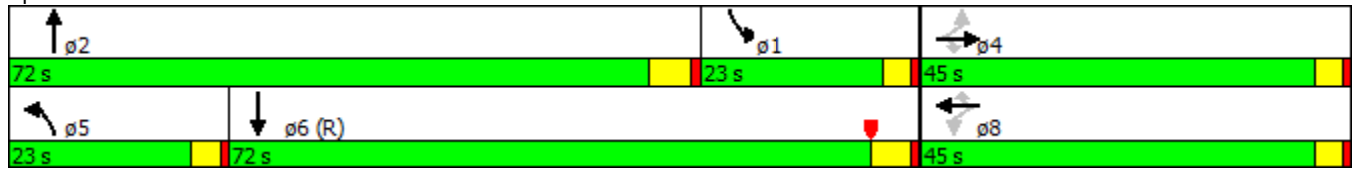
Intersection Summary

Area Type: Other
 Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 35 (25%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 115
 Control Type: Actuated-Coordinated

Lanes, Volumes, Timings
5: Mathilda Ave & Ross Dr

12/11/2015

Splits and Phases: 5: Mathilda Ave & Ross Dr



Lanes, Volumes, Timings
 8: Mathilda Ave & Almanor Ave/Ahwanee Ave

12/11/2015



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------|-------|-------|------|-------|-------|-------|-------|-------|-------|-------|-------|------|
| Lane Configurations | ↔↔ | ↔ | | ↔ | ↔ | ↔ | ↔ | ↑↑↑ | ↔ | ↔ | ↑↑↑↔ | |
| Volume (vph) | 285 | 23 | 64 | 41 | 5 | 172 | 56 | 1275 | 36 | 156 | 2680 | 58 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 320 | | 120 | 230 | | 50 | 350 | | 70 | 110 | | 0 |
| Storage Lanes | 1 | | 1 | 1 | | 1 | 1 | | 1 | 1 | | 0 |
| Taper Length (ft) | 90 | | | 120 | | | 25 | | | 60 | | |
| Lane Util. Factor | 0.97 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.86 | 1.00 | 1.00 | 0.86 | 0.86 |
| Ped Bike Factor | | 0.98 | | | | | | | 0.98 | | 1.00 | |
| Frt | | 0.890 | | | | 0.850 | | | 0.850 | | 0.997 | |
| Flt Protected | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 3433 | 1631 | 0 | 1770 | 1863 | 1583 | 1770 | 6408 | 1583 | 1770 | 6384 | 0 |
| Flt Permitted | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (perm) | 3433 | 1631 | 0 | 1770 | 1863 | 1583 | 1770 | 6408 | 1549 | 1770 | 6384 | 0 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | 66 | | | | 177 | | | 109 | | 3 | |
| Link Speed (mph) | | 30 | | | 30 | | | 45 | | | 45 | |
| Link Distance (ft) | | 422 | | | 706 | | | 740 | | | 427 | |
| Travel Time (s) | | 9.6 | | | 16.0 | | | 11.2 | | | 6.5 | |
| Confl. Peds. (#/hr) | | | 10 | | | | | | 1 | | | 5 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 294 | 24 | 66 | 42 | 5 | 177 | 58 | 1314 | 37 | 161 | 2763 | 60 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 294 | 90 | 0 | 42 | 5 | 177 | 58 | 1314 | 37 | 161 | 2823 | 0 |
| Turn Type | Prot | NA | | Prot | NA | Perm | Prot | NA | Perm | Prot | NA | |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | | | | | | 8 | | | 2 | | | |
| Detector Phase | 7 | 4 | | 3 | 8 | 8 | 5 | 2 | 2 | 1 | 6 | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 8.0 | 8.0 | | 8.0 | 8.0 | 8.0 | 8.0 | 12.0 | 12.0 | 8.0 | 12.0 | |
| Minimum Split (s) | 12.1 | 46.7 | | 12.1 | 12.7 | 12.7 | 12.1 | 17.3 | 17.3 | 12.1 | 26.3 | |
| Total Split (s) | 19.0 | 55.0 | | 19.0 | 55.0 | 55.0 | 18.0 | 43.0 | 43.0 | 23.0 | 48.0 | |
| Total Split (%) | 13.6% | 39.3% | | 13.6% | 39.3% | 39.3% | 12.9% | 30.7% | 30.7% | 16.4% | 34.3% | |
| Yellow Time (s) | 3.1 | 3.7 | | 3.1 | 3.7 | 3.7 | 3.1 | 4.3 | 4.3 | 3.1 | 4.3 | |
| All-Red Time (s) | 1.0 | 1.0 | | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | |
| Lost Time Adjust (s) | 0.0 | 0.0 | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | 4.1 | 4.7 | | 4.1 | 4.7 | 4.7 | 4.1 | 5.3 | 5.3 | 4.1 | 5.3 | |
| Lead/Lag | Lead | Lag | | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | |
| Lead-Lag Optimize? | Yes | Yes | | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | |
| Recall Mode | None | None | | None | None | None | None | C-Max | C-Max | None | C-Max | |

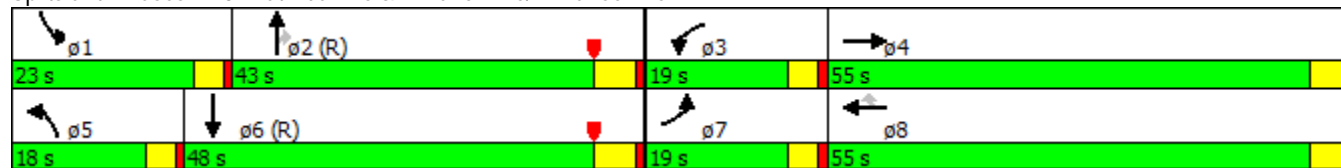
Intersection Summary

Area Type: Other
 Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 36 (26%), Referenced to phase 2:NBT and 6:SBT, Start of Yellow
 Natural Cycle: 130
 Control Type: Actuated-Coordinated

Lanes, Volumes, Timings
 8: Mathilda Ave & Almanor Ave/Ahwanee Ave

12/11/2015

Splits and Phases: 8: Mathilda Ave & Almanor Ave/Ahwanee Ave



Lanes, Volumes, Timings
 9: 101 On Ramp & Moffett Park Dr

12/11/2015

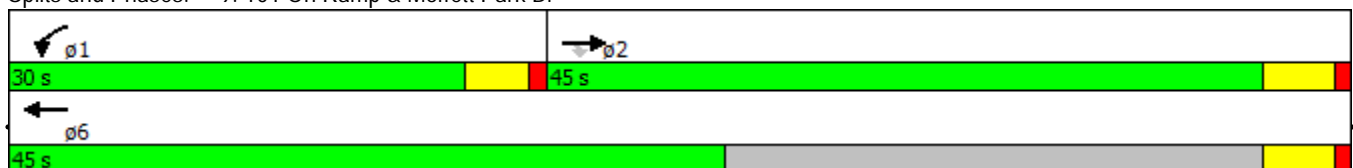


| Lane Group | EBT | EBR | WBL | WBT | NBL | NBR |
|-------------------------|-------|-------|-------|-------|------|------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ | | |
| Volume (vph) | 731 | 77 | 205 | 282 | 0 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | | 130 | 0 | | 0 | 0 |
| Storage Lanes | | 1 | 1 | | 0 | 0 |
| Taper Length (ft) | | | 25 | | 25 | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | | 0.850 | | | | |
| Flt Protected | | | 0.950 | | | |
| Satd. Flow (prot) | 1863 | 1583 | 1770 | 1863 | 0 | 0 |
| Flt Permitted | | | 0.950 | | | |
| Satd. Flow (perm) | 1863 | 1583 | 1770 | 1863 | 0 | 0 |
| Right Turn on Red | | Yes | | | | Yes |
| Satd. Flow (RTOR) | | 67 | | | | |
| Link Speed (mph) | 30 | | | 30 | 30 | |
| Link Distance (ft) | 939 | | | 921 | 120 | |
| Travel Time (s) | 21.3 | | | 20.9 | 2.7 | |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 754 | 79 | 211 | 291 | 0 | 0 |
| Shared Lane Traffic (%) | | | | | | |
| Lane Group Flow (vph) | 754 | 79 | 211 | 291 | 0 | 0 |
| Turn Type | NA | Perm | Prot | NA | | |
| Protected Phases | 2 | | 1 | 6 | | |
| Permitted Phases | | 2 | | | | |
| Detector Phase | 2 | 2 | 1 | 6 | | |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 15.0 | 15.0 | 6.0 | 15.0 | | |
| Minimum Split (s) | 20.0 | 20.0 | 10.5 | 20.0 | | |
| Total Split (s) | 45.0 | 45.0 | 30.0 | 45.0 | | |
| Total Split (%) | 60.0% | 60.0% | 40.0% | 60.0% | | |
| Yellow Time (s) | 4.0 | 4.0 | 3.5 | 4.0 | | |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | | |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | | |
| Total Lost Time (s) | 5.0 | 5.0 | 4.5 | 5.0 | | |
| Lead/Lag | Lag | Lag | Lead | | | |
| Lead-Lag Optimize? | | | | | | |
| Recall Mode | Min | Min | Max | Min | | |

Intersection Summary

Area Type: Other
 Cycle Length: 75
 Actuated Cycle Length: 67.3
 Natural Cycle: 50
 Control Type: Semi Act-Uncoord

Splits and Phases: 9: 101 On Ramp & Moffett Park Dr



Lanes, Volumes, Timings

10: Moffett Park Dr & Innovation Way

12/11/2015

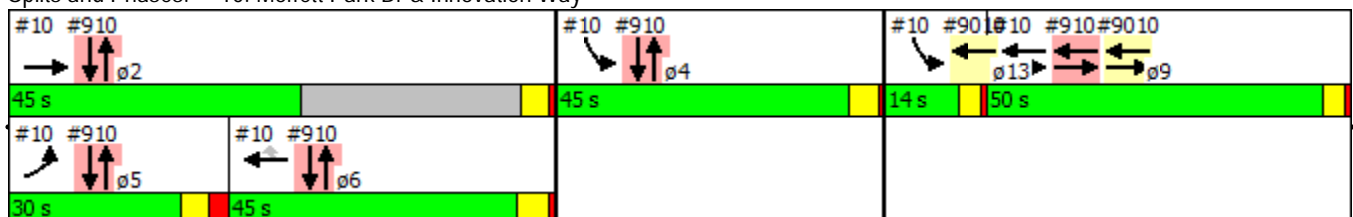


| Lane Group | EBL | EBT | WBT | WBR | SBL | SBR | ø2 | ø4 | ø9 | ø13 |
|-------------------------|-------|------|------|--------|-------|------|------|------|------|------|
| Lane Configurations | ↖ | ↑↑ | ↑↑ | ↗ | ↖↗ | | | | | |
| Volume (vph) | 44 | 687 | 350 | 42 | 153 | 137 | | | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | | | | |
| Storage Length (ft) | 200 | | | 200 | 0 | 0 | | | | |
| Storage Lanes | 1 | | | 1 | 2 | 0 | | | | |
| Taper Length (ft) | 140 | | | | 25 | | | | | |
| Lane Util. Factor | 1.00 | 0.95 | 0.95 | 1.00 | 0.97 | 0.95 | | | | |
| Frt | | | | 0.850 | 0.929 | | | | | |
| Flt Protected | 0.950 | | | | 0.974 | | | | | |
| Satd. Flow (prot) | 1770 | 3539 | 3539 | 1583 | 3270 | 0 | | | | |
| Flt Permitted | 0.950 | | | | 0.974 | | | | | |
| Satd. Flow (perm) | 1770 | 3539 | 3539 | 1583 | 3270 | 0 | | | | |
| Right Turn on Red | | | | Yes | | No | | | | |
| Satd. Flow (RTOR) | | | | 43 | | | | | | |
| Link Speed (mph) | | 40 | 40 | | 30 | | | | | |
| Link Distance (ft) | | 921 | 1032 | | 121 | | | | | |
| Travel Time (s) | | 15.7 | 17.6 | | 2.8 | | | | | |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | | | | |
| Adj. Flow (vph) | 45 | 708 | 361 | 43 | 158 | 141 | | | | |
| Shared Lane Traffic (%) | | | | | | | | | | |
| Lane Group Flow (vph) | 45 | 708 | 361 | 43 | 299 | 0 | | | | |
| Turn Type | Prot | NA | NA | custom | Prot | | | | | |
| Protected Phases | 5 | 2 9 | 6 9 | | 4 13 | | 2 | 4 | 9 | 13 |
| Permitted Phases | | | | 6 | | | | | | |
| Detector Phase | 5 | 2 | 6 | 6 | 4 | | | | | |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 8.0 | | | 10.0 | | | 10.0 | 10.0 | 46.0 | 10.0 |
| Minimum Split (s) | 14.5 | | | 15.5 | | | 14.9 | 15.0 | 50.0 | 14.0 |
| Total Split (s) | 30.0 | | | 45.0 | | | 45.0 | 45.0 | 50.0 | 14.0 |
| Total Split (%) | 16.3% | | | 24.5% | | | 24% | 24% | 27% | 8% |
| Yellow Time (s) | 4.0 | | | 4.5 | | | 3.9 | 4.0 | 3.0 | 3.0 |
| All-Red Time (s) | 2.5 | | | 1.0 | | | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | | | 0.0 | | | | | | |
| Total Lost Time (s) | 6.5 | | | 5.5 | | | | | | |
| Lead/Lag | Lead | | | Lag | | | | | Lag | Lead |
| Lead-Lag Optimize? | Yes | | | Yes | | | | | Yes | Yes |
| Recall Mode | None | | | Min | | | Min | None | None | None |

Intersection Summary

Area Type: Other
 Cycle Length: 184
 Actuated Cycle Length: 57.3
 Natural Cycle: 110
 Control Type: Actuated-Uncoordinated

Splits and Phases: 10: Moffett Park Dr & Innovation Way



Lanes, Volumes, Timings
11: Innovation Way & 11th Ave

12/11/2015



| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
|-------------------------|-------|-------|-------|-------|-------|------|
| Lane Configurations | | | | | | |
| Volume (vph) | 363 | 248 | 24 | 62 | 42 | 14 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 100 | 0 | 100 | | | 0 |
| Storage Lanes | 1 | 2 | 1 | | | 0 |
| Taper Length (ft) | 30 | | 60 | | | |
| Lane Util. Factor | 1.00 | 0.88 | 0.91 | 0.91 | 0.95 | 0.95 |
| Ped Bike Factor | | | | | | |
| Frt | | 0.850 | | | 0.963 | |
| Flt Protected | 0.950 | | 0.950 | 0.998 | | |
| Satd. Flow (prot) | 1770 | 2787 | 1610 | 3383 | 3408 | 0 |
| Flt Permitted | 0.950 | | 0.950 | 0.998 | | |
| Satd. Flow (perm) | 1770 | 2787 | 1610 | 3383 | 3408 | 0 |
| Link Speed (mph) | 25 | | | 25 | 25 | |
| Link Distance (ft) | 1177 | | | 601 | 841 | |
| Travel Time (s) | 32.1 | | | 16.4 | 22.9 | |
| Confl. Peds. (#/hr) | 5 | 5 | 5 | | | 5 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 374 | 256 | 25 | 64 | 43 | 14 |
| Shared Lane Traffic (%) | | | 10% | | | |
| Lane Group Flow (vph) | 374 | 256 | 22 | 67 | 57 | 0 |
| Sign Control | Stop | | | Stop | Stop | |

Intersection Summary

Area Type: Other

Control Type: Unsignalized

Lanes, Volumes, Timings
 12: Innovation Way & Juniper Driveway

12/11/2015



















| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
|-------------------------|-------|-------|------|------|-------|-------|
| Lane Configurations | | | | | | |
| Volume (vph) | 284 | 15 | 0 | 425 | 41 | 56 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 0 | 0 | 100 | | | 0 |
| Storage Lanes | 1 | 1 | 1 | | | 1 |
| Taper Length (ft) | 25 | | 60 | | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 |
| Ped Bike Factor | | | | | | |
| Frt | | 0.850 | | | 0.969 | 0.850 |
| Flt Protected | 0.950 | | | | | |
| Satd. Flow (prot) | 1770 | 1583 | 1863 | 3539 | 1715 | 1504 |
| Flt Permitted | 0.950 | | | | | |
| Satd. Flow (perm) | 1770 | 1583 | 1863 | 3539 | 1715 | 1504 |
| Link Speed (mph) | 30 | | | 25 | 25 | |
| Link Distance (ft) | 1347 | | | 299 | 197 | |
| Travel Time (s) | 30.6 | | | 8.2 | 5.4 | |
| Confl. Peds. (#/hr) | | 5 | 5 | | | 5 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 293 | 15 | 0 | 438 | 42 | 58 |
| Shared Lane Traffic (%) | | | | | | 19% |
| Lane Group Flow (vph) | 293 | 15 | 0 | 438 | 53 | 47 |
| Sign Control | Stop | | | Stop | Stop | |

Intersection Summary

Area Type: Other
 Control Type: Unsignalized

Lanes, Volumes, Timings
 13: Bordeaux Dr & Innovation Way/Driveway

12/11/2015

| |  |  |  |  |  |  |  |  |  |  |  |  |
|-----------------------------|---|---|---|---|---|---|--|---|---|---|---|---|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | |  | | |  | | |  | | |  | |
| Volume (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 28 | 0 | 0 | 129 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | | | | | | | | | | | | |
| Flt | | | | | | | | | | | | |
| Flt Protected | | | | | | | | | | | | |
| Satd. Flow (prot) | 0 | 1863 | 0 | 0 | 1863 | 0 | 0 | 1863 | 0 | 0 | 1863 | 0 |
| Flt Permitted | | | | | | | | | | | | |
| Satd. Flow (perm) | 0 | 1863 | 0 | 0 | 1863 | 0 | 0 | 1863 | 0 | 0 | 1863 | 0 |
| Link Speed (mph) | 30 | | | | 25 | | | | 30 | | 30 | |
| Link Distance (ft) | 908 | | | | 601 | | | | 1425 | | 725 | |
| Travel Time (s) | 20.6 | | | | 16.4 | | | | 32.4 | | 16.5 | |
| Confl. Peds. (#/hr) | 2 | | | | | | | | | 1 | | |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 29 | 0 | 0 | 133 | 0 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 29 | 0 | 0 | 133 | 0 |
| Sign Control | Stop | | | | Stop | | | | Stop | | Stop | |
| Intersection Summary | | | | | | | | | | | | |
| Area Type: | Other | | | | | | | | | | | |
| Control Type: | Unsignalized | | | | | | | | | | | |

Lanes, Volumes, Timings

33: Mathilda Ave & SR 237 WB On-Ramp/SR 237 WB Off-Ramp

12/11/2015



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
|-------------------------|------|------|------|-------|-------|-------|-------|-------|------|------|-------|-------|
| Lane Configurations | | | | ↙ | ↖ | ↗ | ↘ | ↑↑↑ | | | ↑↑↑ | ↗ |
| Volume (vph) | 0 | 0 | 0 | 709 | 17 | 164 | 82 | 438 | 0 | 0 | 2143 | 403 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 0 | | 0 | 310 | | 310 | 0 | | 0 | 0 | | 0 |
| Storage Lanes | 0 | | 0 | 0 | | 2 | 1 | | 0 | 0 | | 0 |
| Taper Length (ft) | 25 | | | 25 | | | 25 | | | 25 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 1.00 | 0.86 | 1.00 | 1.00 | 0.86 | 0.86 |
| Ped Bike Factor | | | | | | | | | | | | |
| Frt | | | | | | 0.850 | | | | | 0.976 | |
| Flt Protected | | | | 0.950 | 0.955 | | 0.950 | | | | | |
| Satd. Flow (prot) | 0 | 0 | 0 | 1681 | 1690 | 1583 | 1770 | 6408 | 0 | 0 | 6254 | 0 |
| Flt Permitted | | | | 0.950 | 0.955 | | 0.950 | | | | | |
| Satd. Flow (perm) | 0 | 0 | 0 | 1681 | 1690 | 1583 | 1770 | 6408 | 0 | 0 | 6254 | 0 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | | | | | 169 | | | | | | 56 |
| Link Speed (mph) | | 30 | | | 45 | | | 45 | | | | 45 |
| Link Distance (ft) | | 132 | | | 1141 | | | 254 | | | | 214 |
| Travel Time (s) | | 3.0 | | | 17.3 | | | 3.8 | | | | 3.2 |
| Confl. Peds. (#/hr) | | | | | | | | | 9 | | | |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 0 | 0 | 0 | 731 | 18 | 169 | 85 | 452 | 0 | 0 | 2209 | 415 |
| Shared Lane Traffic (%) | | | | 49% | | | | | | | | |
| Lane Group Flow (vph) | 0 | 0 | 0 | 373 | 376 | 169 | 85 | 452 | 0 | 0 | 2624 | 0 |
| Turn Type | | | | Split | NA | Perm | Prot | NA | | | NA | |
| Protected Phases | | | | 8 | 8 | | 5 | 2 | | | | 6 |
| Permitted Phases | | | | | | 8 | | | | | | |
| Detector Phase | | | | 8 | 8 | 8 | 5 | 2 | | | | 6 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | | | 4.0 |
| Minimum Split (s) | | | | 8.9 | 8.9 | 8.9 | 9.3 | 18.3 | | | | 9.3 |
| Total Split (s) | | | | 32.0 | 32.0 | 32.0 | 23.0 | 108.0 | | | | 85.0 |
| Total Split (%) | | | | 22.9% | 22.9% | 22.9% | 16.4% | 77.1% | | | | 60.7% |
| Yellow Time (s) | | | | 3.9 | 3.9 | 3.9 | 4.3 | 4.3 | | | | 4.3 |
| All-Red Time (s) | | | | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | | | | 1.0 |
| Lost Time Adjust (s) | | | | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | | | 0.0 |
| Total Lost Time (s) | | | | 4.9 | 4.9 | 4.9 | 5.3 | 5.3 | | | | 5.3 |
| Lead/Lag | | | | | | | Lead | | | | | Lag |
| Lead-Lag Optimize? | | | | | | | Yes | | | | | Yes |
| Recall Mode | | | | Max | Max | Max | Max | Max | | | | C-Max |

Intersection Summary

Area Type: Other
 Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 33 (24%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 80
 Control Type: Actuated-Coordinated

Lanes, Volumes, Timings

33: Mathilda Ave & SR 237 WB On-Ramp/SR 237 WB Off-Ramp

12/11/2015

Splits and Phases: 33: Mathilda Ave & SR 237 WB On-Ramp/SR 237 WB Off-Ramp

| | | | |
|--|--|--|--|
|  $\phi 2$ | |  $\phi 8$ | |
| 108 s | | 32 s | |
|  $\phi 5$ |  $\phi 6 (R)$ | | |
| 23 s | 85 s | | |

APPENDIX F – EXISTING FREQ MAINLINE CALCULATION SHEETS



US 101 Northbound

```

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 PPP PPP LLL
FFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP LLL
FFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 11111111 222222222 PPP LLLLLLLLLL
    
```

FREQ12PL

1. A TYPE 0 PRIORITY LANE BETWEEN SUBSECTIONS 2 AND 29 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
 LOWER LIMB (AT V/C=1) = 35
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

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*****
*****
**
**
**
*****
*****
**
** SUB NO. SSEC SSEC DESIGN ORG TRK SSEC PCT PCT DES SPECIAL FF. SPD. CAP. ART GRADE SUBSECTI ON LOCATI ON
** SEC LNS CAP LENGTH SPEED DES FAC GRAD TRK TRUCKS RAMP ALT. RTE ALT. RTE TYPE ALT. RTE
**
*****
**
** 1
**
** 2 1 1650. 99999. 60 0 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Queue Capture
**
** 3 1 1650. 2830. 60 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 SR-87 to DLC loop-on
**
** 4 1 1650. 930. 60 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 DLC loop on to dia-on
**
** 5 1 1650. 1490. 60 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 DLC dia-on to Tomas off
**
** 6 1 1650. 3020. 60 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Tomas off to on
**
** 7 1 1650. 1030. 60 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Tomas on to bowers off
**
** 8 1 1650. 1440. 60 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Bowers off to loop-on
**
** 9 1 1650. 1430. 60 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Bowers loop-on to dia
**
** 10 1 1650. 3480. 60 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Bowers dia-on to law-off
**
** 11 1 1650. 1020. 60 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Law off to loop-on
**
    
```

| ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** |
|----|----|----|-------|-------|----|----|------|-----|----|-----|-----|-----|----|------|-----|-----------------------|----|
| ** | 12 | 1 | 1650. | 980. | 60 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Lawr Loop to di ag | |
| ** | 13 | 1 | 1650. | 1800. | 60 | | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Lawrence On-ramp | |
| ** | 14 | 1 | 1650. | 1500. | 60 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks Off-Ramp | |
| ** | 15 | 1 | 1650. | 1300. | 60 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Fair Oaks | |
| ** | 16 | 1 | 1650. | 1000. | 60 | O | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Fair Oaks On-Ramp | |
| ** | 17 | 1 | 1650. | 1100. | 60 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Mathilda | |
| ** | 18 | 1 | 1650. | 1000. | 60 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda NB Off-Ramp | |
| ** | 19 | 1 | 1650. | 900. | 60 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | |
| ** | 20 | 1 | 1650. | 100. | 60 | O | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda NB On-Ramp | |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 10/19/2015 14: 5 PAGE 3
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE

 **
 ** FREeway AND ARTERIAL DESIGN FEATURES **
 **

| ** | SUB NO. | SSEC | SSEC | DESIGN | ORG | TRK | SSEC | PCT | PCT | DES | SPECIAL | FF. SPD. | CAP. | ART | GRADE | SUBSECTI ON | LOCATI ON |
|----|---------|------|-------|--------|-----|-----|------|-----|--------|------|---------|----------|----------|------|----------|----------------------|-----------|
| ** | SEC | LNS | CAP | LENGTH | DES | FAC | GRAD | TRK | TRUCKS | RAMP | | ALT. RTE | ALT. RTE | TYPE | ALT. RTE | | |
| ** | 21 | 1 | 1650. | 100. | 60 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | |
| ** | 22 | 1 | 1650. | 100. | 60 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda SB Off-ramp | |
| ** | 23 | 1 | 1650. | 700. | 60 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / SR-237 | |
| ** | 24 | 1 | 1650. | 1500. | 60 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 WB Off-Ramp | |
| ** | 25 | 1 | 1650. | 800. | 60 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 / SR-237 | |
| ** | 26 | 1 | 1650. | 1000. | 60 | O | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 WB On-Ramp | |
| ** | 27 | 1 | 1650. | 800. | 60 | | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 / Ellis | |
| ** | 28 | 1 | 1650. | 1000. | 60 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Ellis Off-ramp | |
| ** | 29 | 1 | 1650. | 8000. | 60 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | |
| ** | 30 | | | | | | | | | | | | | | | | |
| ** | 31 | | | | | | | | | | | | | | | | |
| ** | 32 | | | | | | | | | | | | | | | | |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 10/19/2015 14: 5 PAGE 4
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF NON-PRIORITY LANES

 **
 ** FREeway AND ARTERIAL DESIGN FEATURES **
 **

| ** | SUB NO. | SSEC | SSEC | DESIGN | ORG | TRK | SSEC | PCT | PCT | DES | SPECIAL | FF. SPD. | CAP. | ART | GRADE | SUBSECTI ON | LOCATI ON |
|----|---------|------|--------|--------|-----|-----|------|-----|--------|------|---------|----------|----------|------|----------|---------------|-----------|
| ** | SEC | LNS | CAP | LENGTH | DES | FAC | GRAD | TRK | TRUCKS | RAMP | | ALT. RTE | ALT. RTE | TYPE | ALT. RTE | | |
| ** | 1 | 4 | 10000. | 500. | 65 | OD | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Seedi ng | |
| ** | 2 | 3 | 7000. | 99999. | 60 | O | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | |

| | | | | | | | | | | | | | | | | |
|----|----|---|-------|-------|----|---|------|-----|---|---|-----|-----|----|------|-----|--------------------------|
| ** | 3 | 3 | 7000. | 2830. | 60 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-87 to DLC loop-on |
| ** | 4 | 3 | 7000. | 930. | 60 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | DLC loop on to dia-on |
| ** | 5 | 3 | 7000. | 1490. | 60 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | DLC dia-on to Tomas off |
| ** | 6 | 3 | 7000. | 3020. | 60 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas off to on |
| ** | 7 | 3 | 7000. | 1030. | 60 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas on to bowers off |
| ** | 8 | 3 | 7000. | 1440. | 60 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers off to loop-on |
| ** | 9 | 3 | 7000. | 1430. | 60 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers loop-on to dia |
| ** | 10 | 3 | 7000. | 3480. | 60 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers dia-on to law-off |
| ** | 11 | 3 | 7000. | 1020. | 60 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Law off to loop-on |
| ** | 12 | 3 | 7000. | 980. | 60 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawr Loop to di ag |
| ** | 13 | 3 | 7000. | 1800. | 60 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Lawrence On-ramp |
| ** | 14 | 3 | 7000. | 1500. | 60 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks Off-Ramp |
| ** | 15 | 3 | 6000. | 1300. | 60 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Fair Oaks |
| ** | 16 | 3 | 6000. | 1000. | 60 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Fair Oaks On-Ramp |
| ** | 17 | 3 | 6000. | 1100. | 60 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Mathilda |
| ** | 18 | 3 | 6000. | 1000. | 60 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda NB Off-Ramp |
| ** | 19 | 3 | 6000. | 900. | 60 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda |
| ** | 20 | 3 | 6000. | 100. | 60 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda NB On-Ramp |

FREEWAY AND ARTERIAL DESIGN FEATURES

| ** SUB NO. | ** SSEC | ** SSEC | ** DESIGN | ** ORG | ** TRK | ** SSEC | ** PCT | ** PCT | ** DES | ** SPECIAL | ** FF.SPD. | ** CAP. | ** ART | ** GRADE | ** SUBSECTI | ** ON | ** LOCATION |
|------------|---------|---------|-----------|----------|--------|---------|---------|--------|-----------|------------|------------|------------|---------|------------|-------------|----------------------|-------------|
| ** SEC | ** LNS | ** CAP | ** LENGTH | ** SPEED | ** DES | ** FAC | ** GRAD | ** TRK | ** TRUCKS | ** RAMP | ** ALT.RTE | ** ALT.RTE | ** TYPE | ** ALT.RTE | ** ON | ** ON | ** ON |
| ** | 21 | 3 | 6000. | 100. | 60 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | |
| ** | 22 | 3 | 6000. | 100. | 60 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda SB Off-ramp | |
| ** | 23 | 3 | 6000. | 700. | 60 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / SR-237 | |
| ** | 24 | 3 | 6000. | 1500. | 60 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 WB Off-Ramp | |
| ** | 25 | 3 | 6000. | 800. | 60 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 / SR-237 | |
| ** | 26 | 3 | 6000. | 1000. | 60 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 WB On-Ramp | |
| ** | 27 | 3 | 6000. | 800. | 60 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 / Ellis | |
| ** | 28 | 3 | 6000. | 1000. | 60 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Ellis Off-ramp | |
| ** | 29 | 3 | 6000. | 8000. | 60 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | |
| ** | 30 | 4 | 8000. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | |
| ** | 31 | 4 | 6000. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Dummy Bottleneck | |
| ** | 32 | 4 | 8000. | 2640. | 65 | D | 1.00 | 0.0 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End of Network | |

```

FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP LLL
FFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 2222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 11111111 222222222 PPP LLLLLLLLLL
    
```

FREQ12PL

1. A TYPE 0 PRIORITY LANE BETWEEN SUBSECTIONS 2 AND 29 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
 LOWER LIMB (AT V/C=1) = 35
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

```

*****
**
**          FREeway TRAVEL TIME (MINUTES)
**
*****
    
```

```

*****
* ORIGINS          DESTINATIONS ACROSS
* DOWN
*      1      2      3      4      5      6      7      8
*
+
*
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 2 * 0.00 22.91 23.74 23.97 24.38 25.07 26.58 0.00
+
* 3 * 0.00 0.00 0.00 0.00 0.00 0.00 3.43 0.00
+
* 4 * 0.00 0.00 0.00 0.00 0.00 0.00 2.67 0.00
+
* 5 * 0.00 0.00 0.00 0.00 0.00 0.00 2.05 0.00
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
*
*
*****
    
```

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB SEC | NO. LNS | SSEC LENGTH | O-D DATA ORG | DEMANDS DES | SSEC | ADJUSTED VOLUMES ORG | DES | SSEC | SSEC CAP. | WEAVE EFF | CONGEST LENGTH | STORAGE RATE | V/C RATIO | SPEED MPH | DENSITY VPMP | LOS LEVEL | FUEL MPG | EMI SS GS/VM |
|---------|---------|-------------|--------------|-------------|-------|----------------------|-------|-------|-----------|-----------|----------------|--------------|-----------------|----------------|--------------|-----------|----------|--------------|
| 1 | | | | | | | | | | | | | | | | | | |
| 2 | 1 | 99999. | 1387. | 0. | 1387. | 1387. | 0. | 1387. | 1650. | 0. | 0. | 0. | .84 | 60. | 23.1 | C | 22.7 | 12.1 |
| 3 | 1 | 2830. | 0. | 0. | 1387. | 0. | 0. | 1387. | 1650. | 0. | 0. | 0. | .84 | 60. | 23.1 | C | 22.7 | 12.1 |
| 4 | 1 | 930. | 0. | 0. | 1387. | 0. | 0. | 1387. | 1650. | 0. | 0. | 0. | .84 | 60. | 23.1 | C | 22.7 | 12.1 |
| 5 | 1 | 1490. | 0. | 0. | 1387. | 0. | 0. | 1387. | 1650. | 0. | 0. | 0. | .84 | 60. | 23.1 | C | 22.7 | 12.1 |
| 6 | 1 | 3020. | 0. | 0. | 1387. | 0. | 0. | 1387. | 1650. | 0. | 0. | 0. | .84 | 60. | 23.1 | C | 22.7 | 12.1 |
| 7 | 1 | 1030. | 0. | 0. | 1387. | 0. | 0. | 1387. | 1650. | 0. | 0. | 0. | .84 | 60. | 23.1 | C | 22.7 | 12.1 |
| 8 | 1 | 1440. | 0. | 0. | 1387. | 0. | 0. | 1387. | 1650. | 0. | 0. | 0. | .84 | 60. | 23.1 | C | 22.7 | 12.1 |
| 9 | 1 | 1430. | 0. | 0. | 1387. | 0. | 0. | 1387. | 1650. | 0. | 0. | 0. | .84 | 60. | 23.1 | C | 22.7 | 12.1 |
| 10 | 1 | 3480. | 0. | 0. | 1387. | 0. | 0. | 1387. | 1650. | 0. | 0. | 0. | .84 | 60. | 23.1 | C | 22.7 | 12.1 |
| 11 | 1 | 1020. | 0. | 0. | 1387. | 0. | 0. | 1387. | 1650. | 0. | 0. | 0. | .84 | 60. | 23.1 | C | 22.7 | 12.1 |
| 12 | 1 | 980. | 0. | 0. | 1387. | 0. | 0. | 1387. | 1650. | 0. | 0. | 0. | .84 | 60. | 23.1 | C | 22.7 | 12.1 |
| 13 | 1 | 1800. | 0. | 0. | 1387. | 0. | 0. | 1387. | 1650. | 0. | 0. | 0. | .84 | 60. | 23.1 | C | 22.7 | 12.1 |
| 14 | 1 | 1500. | 0. | 160. | 1387. | 0. | 160. | 1387. | 1650. | 0. | 0. | 0. | .84 | 60. | 23.1 | C | 22.7 | 12.1 |
| 15 | 1 | 1300. | 0. | 0. | 1227. | 0. | 0. | 1227. | 1650. | 0. | 0. | 0. | .74 | 60. | 20.4 | C | 22.7 | 12.1 |
| 16 | 1 | 1000. | 80. | 0. | 1307. | 80. | 0. | 1307. | 1650. | 0. | 0. | 0. | .79 | 60. | 21.8 | C | 22.7 | 12.1 |
| 17 | 1 | 1100. | 0. | 0. | 1307. | 0. | 0. | 1307. | 1650. | 0. | 0. | 0. | .79 | 60. | 21.8 | C | 22.7 | 12.1 |
| 18 | 1 | 1000. | 0. | 97. | 1307. | 0. | 97. | 1307. | 1650. | 0. | 0. | 0. | .79 | 60. | 21.8 | C | 22.7 | 12.1 |
| 19 | 1 | 900. | 0. | 0. | 1211. | 0. | 0. | 1211. | 1650. | 0. | 0. | 0. | .73 | 60. | 20.2 | C | 22.7 | 12.1 |
| 20 | 1 | 100. | 42. | 0. | 1252. | 42. | 0. | 1252. | 1650. | 0. | 0. | 0. | .76 | 60. | 20.9 | C | 22.7 | 12.1 |
| 21 | 1 | 100. | 0. | 0. | 1252. | 0. | 0. | 1252. | 1650. | 0. | 0. | 0. | .76 | 60. | 20.9 | C | 22.7 | 12.1 |
| 22 | 1 | 100. | 0. | 94. | 1252. | 0. | 94. | 1252. | 1650. | 0. | 0. | 0. | .76 | 60. | 20.9 | C | 22.7 | 12.1 |
| 23 | 1 | 700. | 0. | 0. | 1158. | 0. | 0. | 1158. | 1650. | 0. | 0. | 0. | .70 | 60. | 19.3 | C | 22.7 | 12.1 |
| 24 | 1 | 1500. | 0. | 137. | 1158. | 0. | 137. | 1158. | 1650. | 0. | 0. | 0. | .70 | 60. | 19.3 | C | 22.7 | 12.1 |
| 25 | 1 | 800. | 0. | 0. | 1021. | 0. | 0. | 1021. | 1650. | 0. | 0. | 0. | .62 | 60. | 17.0 | B | 22.7 | 12.1 |
| 26 | 1 | 1000. | 204. | 0. | 1225. | 204. | 0. | 1225. | 1650. | 0. | 0. | 0. | .74 | 60. | 20.4 | C | 22.7 | 12.1 |
| 27 | 1 | 800. | 0. | 0. | 1225. | 0. | 0. | 1225. | 1650. | 0. | 0. | 0. | .74 | 60. | 20.4 | C | 22.7 | 12.1 |
| 28 | 1 | 1000. | 0. | 58. | 1225. | 0. | 58. | 1225. | 1650. | 0. | 0. | 0. | .74 | 60. | 20.4 | C | 22.7 | 12.1 |
| 29 | 1 | 8000. | 0. | 1167. | 1167. | 0. | 1167. | 1167. | 1650. | 0. | 0. | 0. | .71 | 60. | 19.5 | C | 22.7 | 12.1 |
| 30 | | | | | | | | | | | | | | | | | | |
| 31 | | | | | | | | | | | | | | | | | | |
| 32 | | | | | | | | | | | | | | | | | | |
| TOTAL | 140349. | = | 26.6 MILES | | | | | | | | | | MAX(V/C) = 0.84 | LOWEST LOS = C | AVG = 60. | 22.7 | 22.7 | 12.1 |

| | CURRENT TIME SLICE | | | CUMULATIVE VALUES | | | | |
|-----------------------------|--------------------|------------|--------|-------------------|--------|------------|--------|----------|
| FREWAY TRAVEL TIME = | 603. | VEH-HRS | 1206. | PASS-HRS | 603. | VEH-HRS | 1206. | PASS-HRS |
| FREWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 603. | VEH-HRS | 1206. | PASS-HRS | 603. | VEH-HRS | 1206. | PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 36179. | VEH-MI. | 72358. | PASS-MI. | 36179. | VEH-MI. | 72358. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 60. | MPH. | | | 60. | MPH. | | |
| AVERAGE DENSITY = | 23. | VPMP | | | 23. | VPMP | | |
| TOTAL FUEL = | 1592. | GALLONS | | | 1592. | GALLONS | | |
| TOTAL EMISSIONS = | 438. | KI LOGRAMS | | | 438. | KI LOGRAMS | | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 33.68 | 3 | 0.95 | 4 | 0.31 | 5 | 0.50 |
| 6 | 1.02 | 7 | 0.35 | 8 | 0.49 | 9 | 0.48 | 10 | 1.17 |
| 11 | 0.34 | 12 | 0.33 | 13 | 0.61 | 14 | 0.51 | 15 | 0.39 |
| 16 | 0.32 | 17 | 0.35 | 18 | 0.32 | 19 | 0.26 | 20 | 0.03 |
| 21 | 0.03 | 22 | 0.03 | 23 | 0.20 | 24 | 0.42 | 25 | 0.20 |
| 26 | 0.30 | 27 | 0.24 | 28 | 0.30 | 29 | 2.27 | 30 | 0.00 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 46.4 VEH-HRS ***** AVERAGE DELAY = 2.04 MIN/VEH *****

**
** FREeway TRAVEL TIME (MI NUTES) **
**

| ***** | | | | | | | | | | |
|-----------|---------------------|-------|-------|-------|-------|-------|-------|------|------|---|
| * ORIGINS | DESTINATIONS ACROSS | | | | | | | | * | |
| * DOWN | | | | | | | | | | * |
| * 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | * |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | * |
| * 2 * | 0.00 | 22.91 | 23.74 | 23.97 | 24.38 | 25.07 | 26.58 | 0.00 | | * |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.43 | 0.00 | | * |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.67 | 0.00 | | * |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.05 | 0.00 | | * |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | * |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | * |
| * * | | | | | | | | | | * |
| ***** | | | | | | | | | | |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB | NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS | | | |
|---------|---------|--------|----------|---------|------------------|-------|-------|-----------------|----------------|-----------|-------|---------|-------|------|--------|---|------|------|
| * SEC | LNS | LENGTH | ORG | DES | ORG | DES | EFF | LENGTH | RATE | RATIO | MPH | VPMP | LEVEL | MPG | GS/VM | | | |
| * 1 | | | | | | | | | | | | | | | | | | |
| * 2 | 1 | 99999. | 1205. | 0. | 1205. | 1205. | 0. | 1205. | 1650. | 0. | 0. | 0. | .73 | 60. | 20.1 | C | 22.7 | 12.1 |
| * 3 | 1 | 2830. | 0. | 0. | 1205. | 0. | 0. | 1205. | 1650. | 0. | 0. | 0. | .73 | 60. | 20.1 | C | 22.7 | 12.1 |
| * 4 | 1 | 930. | 0. | 0. | 1205. | 0. | 0. | 1205. | 1650. | 0. | 0. | 0. | .73 | 60. | 20.1 | C | 22.7 | 12.1 |
| * 5 | 1 | 1490. | 0. | 0. | 1205. | 0. | 0. | 1205. | 1650. | 0. | 0. | 0. | .73 | 60. | 20.1 | C | 22.7 | 12.1 |
| * 6 | 1 | 3020. | 0. | 0. | 1205. | 0. | 0. | 1205. | 1650. | 0. | 0. | 0. | .73 | 60. | 20.1 | C | 22.7 | 12.1 |
| * 7 | 1 | 1030. | 0. | 0. | 1205. | 0. | 0. | 1205. | 1650. | 0. | 0. | 0. | .73 | 60. | 20.1 | C | 22.7 | 12.1 |
| * 8 | 1 | 1440. | 0. | 0. | 1205. | 0. | 0. | 1205. | 1650. | 0. | 0. | 0. | .73 | 60. | 20.1 | C | 22.7 | 12.1 |
| * 9 | 1 | 1430. | 0. | 0. | 1205. | 0. | 0. | 1205. | 1650. | 0. | 0. | 0. | .73 | 60. | 20.1 | C | 22.7 | 12.1 |
| * 10 | 1 | 3480. | 0. | 0. | 1205. | 0. | 0. | 1205. | 1650. | 0. | 0. | 0. | .73 | 60. | 20.1 | C | 22.7 | 12.1 |
| * 11 | 1 | 1020. | 0. | 0. | 1205. | 0. | 0. | 1205. | 1650. | 0. | 0. | 0. | .73 | 60. | 20.1 | C | 22.7 | 12.1 |
| * 12 | 1 | 980. | 0. | 0. | 1205. | 0. | 0. | 1205. | 1650. | 0. | 0. | 0. | .73 | 60. | 20.1 | C | 22.7 | 12.1 |
| * 13 | 1 | 1800. | 0. | 0. | 1205. | 0. | 0. | 1205. | 1650. | 0. | 0. | 0. | .73 | 60. | 20.1 | C | 22.7 | 12.1 |
| * 14 | 1 | 1500. | 0. | 146. | 1205. | 0. | 146. | 1205. | 1650. | 0. | 0. | 0. | .73 | 60. | 20.1 | C | 22.7 | 12.1 |
| * 15 | 1 | 1300. | 0. | 0. | 1059. | 0. | 0. | 1059. | 1650. | 0. | 0. | 0. | .64 | 60. | 17.6 | B | 22.7 | 12.1 |
| * 16 | 1 | 1000. | 69. | 0. | 1128. | 69. | 0. | 1128. | 1650. | 0. | 0. | 0. | .68 | 60. | 18.8 | C | 22.7 | 12.1 |
| * 17 | 1 | 1100. | 0. | 0. | 1128. | 0. | 0. | 1128. | 1650. | 0. | 0. | 0. | .68 | 60. | 18.8 | C | 22.7 | 12.1 |
| * 18 | 1 | 1000. | 0. | 106. | 1128. | 0. | 106. | 1128. | 1650. | 0. | 0. | 0. | .68 | 60. | 18.8 | C | 22.7 | 12.1 |
| * 19 | 1 | 900. | 0. | 0. | 1023. | 0. | 0. | 1023. | 1650. | 0. | 0. | 0. | .62 | 60. | 17.0 | B | 22.7 | 12.1 |
| * 20 | 1 | 100. | 35. | 0. | 1057. | 35. | 0. | 1057. | 1650. | 0. | 0. | 0. | .64 | 60. | 17.6 | B | 22.7 | 12.1 |
| * 21 | 1 | 100. | 0. | 0. | 1057. | 0. | 0. | 1057. | 1650. | 0. | 0. | 0. | .64 | 60. | 17.6 | B | 22.7 | 12.1 |
| * 22 | 1 | 100. | 0. | 106. | 1057. | 0. | 106. | 1057. | 1650. | 0. | 0. | 0. | .64 | 60. | 17.6 | B | 22.7 | 12.1 |
| * 23 | 1 | 700. | 0. | 0. | 952. | 0. | 0. | 952. | 1650. | 0. | 0. | 0. | .58 | 60. | 15.9 | B | 22.7 | 12.1 |
| * 24 | 1 | 1500. | 0. | 153. | 952. | 0. | 153. | 952. | 1650. | 0. | 0. | 0. | .58 | 60. | 15.9 | B | 22.7 | 12.1 |
| * 25 | 1 | 800. | 0. | 0. | 799. | 0. | 0. | 799. | 1650. | 0. | 0. | 0. | .48 | 60. | 13.3 | B | 22.7 | 12.1 |
| * 26 | 1 | 1000. | 159. | 0. | 958. | 159. | 0. | 958. | 1650. | 0. | 0. | 0. | .58 | 60. | 16.0 | B | 22.7 | 12.1 |
| * 27 | 1 | 800. | 0. | 0. | 958. | 0. | 0. | 958. | 1650. | 0. | 0. | 0. | .58 | 60. | 16.0 | B | 22.7 | 12.1 |
| * 28 | 1 | 1000. | 0. | 68. | 958. | 0. | 68. | 958. | 1650. | 0. | 0. | 0. | .58 | 60. | 16.0 | B | 22.7 | 12.1 |
| * 29 | 1 | 8000. | 0. | 890. | 890. | 0. | 890. | 890. | 1650. | 0. | 0. | 0. | .54 | 60. | 14.8 | B | 22.7 | 12.1 |
| * 30 | | | | | | | | | | | | | | | | | | |
| * 31 | | | | | | | | | | | | | | | | | | |
| * 32 | | | | | | | | | | | | | | | | | | |
| * TOTAL | 140349. | = | 26.6 | MI LBS | | | | MAX(V/C) = 0.73 | LOWEST LOS = C | AVG = 60. | 19.5 | 22.7 | 12.1 | | | | | |

| | CURRENT TIME SLICE | | | CUMULATIVE VALUES | | |
|-----------------------------|--------------------|-----------------|----------------|-------------------|--|--|
| FREEWAY TRAVEL TIME = | 519. VEH-HRS | 1038. PASS-HRS | 1122. VEH-HRS | 2244. PASS-HRS | | |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | | |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | | |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | | |
| TOTAL SYSTEM TRAVEL TIME = | 519. VEH-HRS | 1038. PASS-HRS | 1122. VEH-HRS | 2244. PASS-HRS | | |
| TOTAL FRWAY TRAV DISTANCE = | 31138. VEH-MI. | 62275. PASS-MI. | 67316. VEH-MI. | 134633. PASS-MI. | | |
| AVERAGE SYSTEM SPEED = | 60. MPH. | | 60. MPH. | | | |
| AVERAGE DENSITY = | 20. VPMP/L | | 21. VPMP/L | | | |
| TOTAL FUEL = | 1370. GALLONS | | 2962. GALLONS | | | |
| TOTAL EMISSIONS = | 377. KILOGRAMS | | 816. KILOGRAMS | | | |

***** MAI NLI NE DELAY (VEH-HRS) ***** DESI RED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 29.26 | 3 | 0.83 | 4 | 0.27 | 5 | 0.44 |
| 6 | 0.88 | 7 | 0.30 | 8 | 0.42 | 9 | 0.42 | 10 | 1.02 |
| 11 | 0.30 | 12 | 0.29 | 13 | 0.53 | 14 | 0.44 | 15 | 0.33 |
| 16 | 0.27 | 17 | 0.30 | 18 | 0.27 | 19 | 0.22 | 20 | 0.03 |
| 21 | 0.03 | 22 | 0.03 | 23 | 0.16 | 24 | 0.35 | 25 | 0.16 |
| 26 | 0.23 | 27 | 0.19 | 28 | 0.23 | 29 | 1.73 | 30 | 0.00 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 39.9 VEH-HRS ***** AVERAGE DELAY = 2.04 MI N/VEH *****

QUEUE COLL. SECTION 16 T2= 0.616

 **
 ** FREEWAY TRAVEL TIME (MI NUTES) **
 **

| * ORI GINS | DESTI NATIONS ACROSS | | | | | | | | * |
|------------|----------------------|-------|-------|-------|-------|-------|------|-------|---|
| * DOWN | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | * |
| * 1 * | 0.09 | 29.14 | 31.20 | 31.81 | 33.15 | 35.60 | 0.00 | 43.82 | * |
| * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | * |
| * 3 * | 0.00 | 0.00 | 1.29 | 1.90 | 3.24 | 5.69 | 0.00 | 13.91 | * |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.14 | 1.48 | 3.93 | 0.00 | 12.15 | * |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.74 | 0.00 | 9.96 | * |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.80 | * |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.69 | * |

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB SEC | NO. LNS | SSEC LENGTH | O-D DATA ORG | DEMANDS DES SSEC | ADJUSTED VOLUMES ORG DES SSEC | SSEC CAP. | WEAVE EFF | CONGEST LENGTH | STORAGE RATE | V/C RATIO | SPEED MPH | DENSITY VPML | LOS LEVEL | FUEL MPG | EMI SS GS/VM | | | | |
|---------|---------|-------------|--------------|------------------|-------------------------------|-----------|-----------|----------------|--------------|-----------|-----------|--------------|-----------|----------|--------------|-------|------|------|------|
| * 1 | 4 | 500. | 8160. | 1387. | 8160. | 1387. | 8160. | 10000. | 0. | 0. | 0. | .82 | 63. | 32.6 | D | 20.2 | 13.2 | | |
| * 2 | 3 | 99999. | 0. | 0. | 6773. | 0. | 0. | 6773. | 7000. | 0. | 0. | .97 | 53. | 42.3 | E | 23.5 | 11.2 | | |
| * 3 | 3 | 2830. | 0. | 0. | 6773. | 0. | 0. | 4720. | 7000. | 0. | * | 2109. | 2053. | .67 | 51. | 31.0 | F | 23.3 | 11.4 |
| * 4 | 3 | 930. | 0. | 0. | 6773. | 0. | 0. | 4720. | 7000. | 0. | ** | 930. | 2053. | .67 | 45. | 34.7 | F | 22.8 | 11.7 |
| * 5 | 3 | 1490. | 0. | 0. | 6773. | 0. | 0. | 4720. | 7000. | 0. | ** | 1490. | 2053. | .67 | 42. | 37.2 | F | 22.4 | 12.0 |
| * 6 | 3 | 3020. | 0. | 0. | 6773. | 0. | 0. | 4720. | 7000. | 0. | ** | 3020. | 2053. | .67 | 37. | 42.1 | F | 21.8 | 12.4 |
| * 7 | 3 | 1030. | 0. | 0. | 6773. | 0. | 0. | 4720. | 7000. | 0. | ** | 1030. | 2053. | .67 | 34. | 46.6 | F | 21.2 | 12.9 |
| * 8 | 3 | 1440. | 0. | 0. | 6773. | 0. | 0. | 4720. | 7000. | 0. | ** | 1440. | 2053. | .67 | 32. | 49.5 | F | 20.9 | 13.2 |
| * 9 | 3 | 1430. | 0. | 0. | 6773. | 0. | 0. | 4720. | 7000. | 0. | ** | 1430. | 2053. | .67 | 30. | 52.8 | F | 20.5 | 13.5 |
| * 10 | 3 | 3480. | 0. | 0. | 6773. | 0. | 0. | 4720. | 7000. | 0. | ** | 3480. | 2053. | .67 | 27. | 58.8 | F | 19.8 | 14.1 |
| * 11 | 3 | 1020. | 0. | 0. | 6773. | 0. | 0. | 4720. | 7000. | 0. | ** | 1020. | 2053. | .67 | 24. | 64.5 | F | 19.2 | 14.6 |
| * 12 | 3 | 980. | 0. | 0. | 6773. | 0. | 0. | 4720. | 7000. | 0. | ** | 980. | 2053. | .67 | 23. | 67.1 | F | 19.0 | 14.9 |
| * 13 | 3 | 1800. | 0. | 0. | 6773. | 0. | 0. | 4720. | 7000. | 0. | ** | 1800. | 2053. | .67 | 22. | 70.8 | F | 18.6 | 15.2 |
| * 14 | 3 | 1500. | 0. | 784. | 6773. | 0. | 784. | 4720. | 7000. | 0. | ** | 1500. | 2053. | .67 | 21. | 75.4 | F | 18.2 | 15.7 |
| * 15 | 3 | 1300. | 0. | 0. | 5989. | 0. | 0. | 3936. | 6000. | 0. | ** | 1300. | 2053. | .66 | 19. | 68.1 | F | 17.9 | 16.0 |
| * 16 | 3 | 1000. | 610. | 0. | 6599. | 610. | 0. | 4546. | 6000. | 0. | ** | 1000. | 1454. | .76 | 28. | 53.8 | F | 20.7 | 13.7 |
| * 17 | 3 | 1100. | 0. | 0. | 6599. | 0. | 0. | 4546. | 6000. | 0. | ** | 1100. | 1454. | .76 | 27. | 55.6 | F | 20.5 | 13.9 |
| * 18 | 3 | 1000. | 0. | 525. | 6599. | 0. | 478. | 4546. | 6000. | 0. | ** | 1000. | 1454. | .76 | 26. | 57.3 | F | 20.3 | 14.1 |
| * 19 | 3 | 900. | 0. | 0. | 6073. | 0. | 0. | 4067. | 6000. | 0. | ** | 900. | 1454. | .68 | 22. | 61.4 | F | 18.2 | 15.6 |
| * 20 | 3 | 100. | 288. | 0. | 6362. | 288. | 0. | 4356. | 6000. | 0. | ** | 100. | 1454. | .73 | 24. | 61.3 | F | 19.1 | 15.0 |
| * 21 | 3 | 100. | 0. | 0. | 6362. | 0. | 0. | 4356. | 6000. | 0. | ** | 100. | 1454. | .73 | 24. | 61.5 | F | 19.1 | 15.0 |
| * 22 | 3 | 100. | 0. | 539. | 6362. | 0. | 493. | 4356. | 6000. | 0. | ** | 100. | 1454. | .73 | 24. | 61.7 | F | 19.0 | 15.0 |
| * 23 | 3 | 700. | 0. | 0. | 5823. | 0. | 0. | 3862. | 6000. | 0. | ** | 700. | 1454. | .64 | 19. | 66.1 | F | 17.3 | 16.4 |
| * 24 | 3 | 1500. | 0. | 787. | 5823. | 0. | 720. | 3862. | 6000. | 0. | ** | 1500. | 1454. | .64 | 18. | 70.1 | F | 17.0 | 16.8 |
| * 25 | 3 | 800. | 0. | 0. | 5036. | 0. | 0. | 3143. | 6000. | 0. | ** | 800. | 1454. | .52 | 13. | 82.2 | F | 13.6 | 19.3 |
| * 26 | 3 | 1000. | 1076. | 0. | 6112. | 1076. | 0. | 4219. | 6000. | 0. | ** | 1000. | 1454. | .70 | 19. | 74.3 | F | 17.4 | 16.6 |
| * 27 | 3 | 800. | 0. | 0. | 6112. | 0. | 0. | 4219. | 6000. | 0. | ** | 800. | 1454. | .70 | 18. | 76.9 | F | 17.2 | 16.9 |
| * 28 | 3 | 1000. | 0. | 414. | 6112. | 0. | 386. | 4219. | 6000. | 0. | ** | 1000. | 1454. | .70 | 18. | 79.5 | F | 17.0 | 17.2 |
| * 29 | 3 | 8000. | 0. | 0. | 5698. | 0. | 0. | 3833. | 6000. | 0. | ** | 8000. | 1454. | .64 | 12. | 104.3 | F | 14.5 | 20.5 |
| * 30 | 4 | 100. | 1167. | 0. | 6865. | 1167. | 0. | 5000. | 8000. | 0. | ** | 100. | 1454. | .63 | 10. | 126.8 | F | 12.9 | 23.0 |
| * 31 | 4 | 1000. | 1000. | 0. | 7865. | 1000. | 0. | 6000. | 6000. | 0. | * | 0. | 0. | 1.00 | 52. | 28.7 | E | 23.8 | 11.1 |
| * 32 | 4 | 2640. | 0. | 7865. | 7865. | 0. | 6000. | 6000. | 8000. | 0. | * | 0. | 0. | .75 | 64. | 23.4 | C | 20.4 | 13.5 |

TOTAL 144589. = 27.4 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 41. 48.6 22.1 12.2

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|-----------------------------|--------------------|------------------|-------------------|------------------|
| FREEWAY TRAVEL TIME = | 4301. VEH-HRS | 4318. PASS-HRS | 4301. VEH-HRS | 4318. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 4301. VEH-HRS | 4318. PASS-HRS | 4301. VEH-HRS | 4318. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 174619. VEH-MI. | 175513. PASS-MI. | 174619. VEH-MI. | 175513. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 41. MPH. | | 41. MPH. | |
| AVERAGE DENSITY = | 49. VPML | | 49. VPML | |
| TOTAL FUEL = | 7894. GALLONS | | 7894. GALLONS | |
| TOTAL EMISSIONS = | 2125. KILOGRAMS | | 2125. KILOGRAMS | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|--------|------------|-------|------------|--------|------------|-------|
| 1 | 0.44 | 2 | 430.03 | 3 | 15.70 | 4 | 7.80 | 5 | 15.36 |
| 6 | 41.93 | 7 | 17.61 | 8 | 27.44 | 9 | 30.51 | 10 | 87.81 |
| 11 | 29.38 | 12 | 29.78 | 13 | 58.67 | 14 | 52.82 | 15 | 43.75 |
| 16 | 20.66 | 17 | 23.88 | 18 | 22.75 | 19 | 24.65 | 20 | 2.59 |
| 21 | 2.60 | 22 | 2.61 | 23 | 21.81 | 24 | 50.15 | 25 | 35.62 |
| 26 | 33.75 | 27 | 28.07 | 28 | 36.42 | 29 | 406.84 | 30 | 8.16 |
| 31 | 4.28 | 32 | 0.59 | | | | | | |

***** TOTAL DELAY = 1614.5 VEH-HRS ***** AVERAGE DELAY = 20.82 MIN/VEH *****

**
 ** FREEWAY TRAVEL TIME (MI NUTES) **
 **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|--|-----------------------|-------|-------|-------|-------|-------|------|-------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | | 0.09 | 30.78 | 32.58 | 33.17 | 34.55 | 37.12 | 0.00 | 44.51 |
| * 2 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 3 * | | 0.00 | 0.00 | 1.11 | 1.71 | 3.09 | 5.66 | 0.00 | 13.04 |
| * 4 * | | 0.00 | 0.00 | 0.00 | 0.13 | 1.51 | 4.08 | 0.00 | 11.46 |
| * 5 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.77 | 0.00 | 9.15 |
| * 6 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.79 |
| * 7 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.69 |

* TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB SEC | * NO. LNS | * SSEC LENGTH | * O-D DATA ORG | * DEMANDS DES | * SSEC | * ADJUSTED ORG | * VOLUMES DES | * SSEC SSEC | * CAP. | * WEAVE EFF | * CONGEST LENGTH | * STORAGE RATE | * V/C RATIO | * SPEED MPH | * DENSITY VPMP | * LOS LEVEL | * FUEL MPG | * EMISSIONS GS/VM |
|-----------|-----------|---------------|----------------|---------------|--------|----------------|---------------|-------------|--------|-------------|------------------|----------------|-------------|-------------|----------------|-------------|------------|-------------------|
| * 1 | 4 | 500. | 7089. | 1205. | 7089. | 7089. | 1205. | 7089. | 10000. | 0. | 0. | 0. | .71 | 65. | 27.4 | D | 19.3 | 13.9 |
| * 2 | 3 | 99999. | 0. | 0. | 5884. | 0. | 0. | 5884. | 7000. | 0. | 0. | 0. | .84 | 59. | 33.4 | D | 22.0 | 12.1 |
| * 3 | 3 | 2830. | 0. | 0. | 5884. | 0. | 0. | 5949. | 7000. | 0. | 375. | -65. | .85 | 32. | 62.7 | F | 20.3 | 13.9 |
| * 4 | 3 | 930. | 0. | 0. | 5884. | 0. | 0. | 5949. | 7000. | 0. | 930. | -65. | .85 | 20. | 99.4 | F | 18.5 | 16.1 |
| * 5 | 3 | 1490. | 0. | 0. | 5884. | 0. | 0. | 5949. | 7000. | 0. | 1490. | -65. | .85 | 20. | 99.4 | F | 18.5 | 16.1 |
| * 6 | 3 | 3020. | 0. | 0. | 5884. | 0. | 0. | 5949. | 7000. | 0. | 3020. | -65. | .85 | 20. | 99.4 | F | 18.5 | 16.1 |
| * 7 | 3 | 1030. | 0. | 0. | 5884. | 0. | 0. | 5949. | 7000. | 0. | 1030. | -65. | .85 | 20. | 99.4 | F | 18.5 | 16.1 |
| * 8 | 3 | 1440. | 0. | 0. | 5884. | 0. | 0. | 5949. | 7000. | 0. | 1440. | -65. | .85 | 20. | 99.4 | F | 18.5 | 16.1 |
| * 9 | 3 | 1430. | 0. | 0. | 5884. | 0. | 0. | 5949. | 7000. | 0. | 1430. | -65. | .85 | 20. | 99.4 | F | 18.5 | 16.1 |
| * 10 | 3 | 3480. | 0. | 0. | 5884. | 0. | 0. | 5949. | 7000. | 0. | 3480. | -65. | .85 | 20. | 99.4 | F | 18.5 | 16.1 |
| * 11 | 3 | 1020. | 0. | 0. | 5884. | 0. | 0. | 5949. | 7000. | 0. | 1020. | -65. | .85 | 20. | 99.4 | F | 18.5 | 16.1 |
| * 12 | 3 | 980. | 0. | 0. | 5884. | 0. | 0. | 5949. | 7000. | 0. | 980. | -65. | .85 | 20. | 99.4 | F | 18.5 | 16.1 |
| * 13 | 3 | 1800. | 0. | 0. | 5884. | 0. | 0. | 5949. | 7000. | 0. | 1800. | -65. | .85 | 20. | 99.4 | F | 18.5 | 16.1 |
| * 14 | 3 | 1500. | 0. | 714. | 5884. | 0. | 714. | 5949. | 7000. | 0. | 1500. | -65. | .85 | 20. | 99.4 | F | 18.5 | 16.1 |
| * 15 | 3 | 1300. | 0. | 0. | 5170. | 0. | 0. | 5235. | 6000. | 0. | 1300. | -65. | .87 | 22. | 81.0 | F | 19.0 | 15.5 |
| * 16 | 3 | 1000. | 621. | 0. | 5791. | 621. | 0. | 5856. | 6000. | 0. | 1000. | -65. | .98 | 32. | 61.6 | F | 21.9 | 12.4 |
| * 17 | 3 | 1100. | 0. | 0. | 5791. | 0. | 0. | 5856. | 6000. | 0. | 1100. | -65. | .98 | 32. | 61.6 | F | 21.9 | 12.4 |
| * 18 | 3 | 1000. | 0. | 584. | 5791. | 0. | 584. | 5856. | 6000. | 0. | 1000. | -65. | .98 | 32. | 61.6 | F | 21.9 | 12.4 |
| * 19 | 3 | 900. | 0. | 0. | 5206. | 0. | 0. | 5271. | 6000. | 0. | 900. | -65. | .88 | 22. | 79.8 | F | 19.1 | 15.3 |
| * 20 | 3 | 100. | 275. | 0. | 5482. | 275. | 0. | 5547. | 6000. | 0. | 100. | -65. | .92 | 26. | 71.3 | F | 20.4 | 13.9 |
| * 21 | 3 | 100. | 0. | 0. | 5482. | 0. | 0. | 5547. | 6000. | 0. | 100. | -65. | .92 | 26. | 71.3 | F | 20.4 | 13.9 |
| * 22 | 3 | 100. | 0. | 619. | 5482. | 0. | 619. | 5547. | 6000. | 0. | 100. | -65. | .92 | 26. | 71.3 | F | 20.4 | 13.9 |
| * 23 | 3 | 700. | 0. | 0. | 4862. | 0. | 0. | 4927. | 6000. | 0. | 700. | -65. | .82 | 18. | 90.5 | F | 17.6 | 17.1 |
| * 24 | 3 | 1500. | 0. | 897. | 4862. | 0. | 897. | 4927. | 6000. | 0. | 1500. | -65. | .82 | 18. | 90.5 | F | 17.6 | 17.1 |
| * 25 | 3 | 800. | 0. | 0. | 3965. | 0. | 0. | 4030. | 6000. | 0. | 800. | -65. | .67 | 11. | 118.4 | F | 13.9 | 21.7 |
| * 26 | 3 | 1000. | 881. | 0. | 4846. | 881. | 0. | 4911. | 6000. | 0. | 1000. | -65. | .82 | 18. | 91.0 | F | 17.5 | 17.2 |
| * 27 | 3 | 800. | 0. | 0. | 4846. | 0. | 0. | 4911. | 6000. | 0. | 800. | -65. | .82 | 18. | 91.0 | F | 17.5 | 17.2 |
| * 28 | 3 | 1000. | 0. | 501. | 4846. | 0. | 501. | 4911. | 6000. | 0. | 1000. | -65. | .82 | 18. | 91.0 | F | 17.5 | 17.2 |
| * 29 | 3 | 8000. | 0. | 0. | 4345. | 0. | 0. | 4410. | 6000. | 0. | 8000. | -65. | .74 | 14. | 106.6 | F | 15.4 | 19.8 |
| * 30 | 4 | 100. | 890. | 0. | 5235. | 890. | 0. | 5300. | 8000. | 0. | 100. | -65. | .66 | 11. | 120.2 | F | 13.7 | 22.0 |
| * 31 | 4 | 1000. | 700. | 0. | 5935. | 700. | 0. | 6000. | 6000. | 0. | 0. | 0. | 1.00 | 52. | 28.7 | E | 23.8 | 11.1 |
| * 32 | 4 | 2640. | 0. | 5935. | 5935. | 0. | 6000. | 6000. | 8000. | 0. | 0. | 0. | .75 | 64. | 23.4 | C | 20.4 | 13.5 |

| | | | | | | | | | | | | | | | | |
|---------|---------|---|------|--------|----------|---|------|------------|---|---|-----|---|-----|------|------|------|
| * TOTAL | 144589. | = | 27.4 | MI LBS | MAX(V/C) | = | 1.00 | LOWEST LOS | = | F | AVG | = | 38. | 50.0 | 20.8 | 13.2 |
|---------|---------|---|------|--------|----------|---|------|------------|---|---|-----|---|-----|------|------|------|

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|-----------------------------|--------------------|------------------|-------------------|------------------|
| FREEWAY TRAVEL TIME = | 4127. VEH-HRS | 4145. PASS-HRS | 8428. VEH-HRS | 8464. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 4127. VEH-HRS | 4145. PASS-HRS | 8428. VEH-HRS | 8464. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 157819. VEH-MI. | 158724. PASS-MI. | 332438. VEH-MI. | 334236. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 38. MPH. | | 39. MPH. | |
| AVERAGE DENSITY = | 50. VPMP/L | | 49. VPMP/L | |
| TOTAL FUEL = | 7592. GALLONS | | 15486. GALLONS | |
| TOTAL EMISSIONS = | 2089. KI LOGRAMS | | 4215. KI LOGRAMS | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|--------|------------|--------|------------|-------|------------|--------|------------|--------|
| 1 | 0.05 | 2 | 183.70 | 3 | 51.52 | 4 | 36.39 | 5 | 58.31 |
| 6 | 118.18 | 7 | 40.31 | 8 | 56.35 | 9 | 55.96 | 10 | 136.18 |
| 11 | 39.92 | 12 | 38.35 | 13 | 70.44 | 14 | 58.70 | 15 | 39.96 |
| 16 | 17.96 | 17 | 19.75 | 18 | 17.96 | 19 | 27.00 | 20 | 2.43 |
| 21 | 2.43 | 22 | 2.43 | 23 | 25.96 | 24 | 55.62 | 25 | 44.44 |
| 26 | 37.42 | 27 | 29.93 | 28 | 37.42 | 29 | 381.87 | 30 | 7.56 |
| 31 | 4.28 | 32 | 0.59 | | | | | | |

***** TOTAL DELAY = 1699.4 VEH-HRS ***** AVERAGE DELAY = 19.22 MIN/VEH *****

```

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A.D.MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQQ QQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP LLL
FFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 2222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 11111111 2222222222 PPP LLLLLLLLLL
    
```

FREQ12PL

1. A TYPE 0 PRIORITY LANE BETWEEN SUBSECTIONS 2 AND 29 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
 LOWER LIMB (AT V/C=1) = 25
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

```

*****
*****
**                                     **
**                               FREeway AND ARTERIAL DESIGN FEATURES                               **
**                                     **
*****
*****
** SUB NO.  SSEC  SSEC  DESIGN  ORG  TRK  SSEC  PCT  PCT  DES  SPECIAL  FF. SPD.  CAP.  ART  GRADE  SUBSECTION LOCATION  **
** SEC LNS  CAP   LENGTH SPEED  DES  FAC  GRAD  TRK  TRUCKS  RAMP  ALT. RTE  ALT. RTE  TYPE  ALT. RTE  **
**                                     **
** 1                                               **
** 2  1  1650.  99999.  60    0  0.96  0.0  0  100  NO    0.0    0.  GOOD  0.0  Queue Capture  **
** 3  1  1650.  2830.   60    0  0.96  0.0  0  100  NO    0.0    0.  GOOD  0.0  SR-87 to DLC loop-on  **
** 4  1  1650.   930.   60    0  0.96  0.0  0  100  NO    0.0    0.  GOOD  0.0  DLC loop on to dia-on  **
** 5  1  1650.  1490.   60    0  0.96  0.0  0  100  NO    0.0    0.  GOOD  0.0  DLC dia-on to Tomas off  **
** 6  1  1650.  3020.   60    0  0.96  0.0  0  100  NO    0.0    0.  GOOD  0.0  Tomas off to on  **
** 7  1  1650.  1030.   60    0  0.96  0.0  0  100  NO    0.0    0.  GOOD  0.0  Tomas on to bowers off  **
** 8  1  1650.  1440.   60    0  0.96  0.0  0  100  NO    0.0    0.  GOOD  0.0  Bowers off to loop-on  **
** 9  1  1650.  1430.   60    0  0.96  0.0  0  100  NO    0.0    0.  GOOD  0.0  Bowers loop-on to dia  **
** 10 1  1650.  3480.   60    0  0.96  0.0  0  100  NO    0.0    0.  GOOD  0.0  Bowers dia-on to law-off  **
** 11 1  1650.  1020.   60    0  0.96  0.0  0  100  NO    0.0    0.  GOOD  0.0  Law off to loop-on  **
    
```

```

**
**  12  1  1650.   980.  60        0.96  0.0  0  100    NO    0.0    0.0  GOOD  0.0  Lawr Loop to diag
**
**  13  1  1650.  1800.  60        0.96  0.0  0  100    YES   0.0    0.0  GOOD  0.0  Lawrence On-ramp
**
**  14  1  1650.  1500.  60         D 0.96  0.0  0  100    NO    0.0    0.0  GOOD  0.0  Fair Oaks Off-Ramp
**
**  15  1  1650.  1300.  60        0.96  0.0  0  100    NO    0.0    0.0  GOOD  0.0  Fair Oaks / Fair Oaks
**
**  16  1  1650.  1000.  60         0 0.96  0.0  0  100    YES   0.0    0.0  GOOD  0.0  Fair Oaks On-Ramp
**
**  17  1  1650.  1100.  60        0.96  0.0  0  100    NO    0.0    0.0  GOOD  0.0  Fair Oaks / Mathilda
**
**  18  1  1650.  1000.  60         D 0.96  0.0  0  100    NO    0.0    0.0  GOOD  0.0  Mathilda NB Off-Ramp
**
**  19  1  1650.   900.  60        0.96  0.0  0  100    NO    0.0    0.0  GOOD  0.0  Mathilda / Mathilda
**
**  20  1  1650.   100.  60         0 0.96  0.0  0  100    YES   0.0    0.0  GOOD  0.0  Mathilda NB On-Ramp
**
*****
*****

```

```

*****
*****
**
**                                FREeway AND ARTERIAL DESIGN FEATURES
**
*****
*****
** SUB NO.   SSEC   SSEC   DESIGN   ORG   TRK   SSEC   PCT   PCT   DES   SPECIAL   FF. SPD.   CAP.   ART   GRADE   SUBSECTION LOCATION
**  SEC LNS   CAP   LENGTH  SPEED   DES   FAC   GRAD  TRK   TRUCKS RAMP     ALT. RTE  ALT. RTE TYPE ALT. RTE
**
**  21  1  1650.   100.  60        0.96  0.0  0  100    NO    0.0    0.0  GOOD  0.0  Mathilda / Mathilda
**
**  22  1  1650.   100.  60         D 0.96  0.0  0  100    NO    0.0    0.0  GOOD  0.0  Mathilda SB Off-ramp
**
**  23  1  1650.   700.  60        0.96  0.0  0  100    NO    0.0    0.0  GOOD  0.0  Mathilda / SR-237
**
**  24  1  1650.  1500.  60         D 0.96  0.0  0  100    NO    0.0    0.0  GOOD  0.0  SR-237 WB Off-Ramp
**
**  25  1  1650.   800.  60        0.96  0.0  0  100    NO    0.0    0.0  GOOD  0.0  SR-237 / SR-237
**
**  26  1  1650.  1000.  60         0 0.96  0.0  0  100    YES   0.0    0.0  GOOD  0.0  SR-237 WB On-Ramp
**
**  27  1  1650.   800.  60        0.96  0.0  0  100    YES   0.0    0.0  GOOD  0.0  SR-237 / Ellis
**
**  28  1  1650.  1000.  60         D 0.96  0.0  0  100    NO    0.0    0.0  GOOD  0.0  Ellis Off-ramp
**
**  29  1  1650.  8000.  60         D 0.96  0.0  0  100    NO    0.0    0.0  GOOD  0.0  HOV Dummy
**
**  30
**
**  31
**
**  32
**
*****
*****

```

```

*****
*****
**
**                                FREeway AND ARTERIAL DESIGN FEATURES
**
*****
*****
** SUB NO.   SSEC   SSEC   DESIGN   ORG   TRK   SSEC   PCT   PCT   DES   SPECIAL   FF. SPD.   CAP.   ART   GRADE   SUBSECTION LOCATION
**  SEC LNS   CAP   LENGTH  SPEED   DES   FAC   GRAD  TRK   TRUCKS RAMP     ALT. RTE  ALT. RTE TYPE ALT. RTE
**
**  1  4  10000.   500.  65        OD 0.96  0.0  4   0    NO    0.0    0.0  GOOD  0.0  Seeding
**
**  2  3  7000.   99999.  60         0 0.96  0.0  4   0    NO    0.0    0.0  GOOD  0.0  Queue Capture
**

```



```

FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEEEE Q*A.D.MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQQ QQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP LLL
FFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 11111111 2222222222 PPP LLLLLLLLLL
    
```

FREQ12PL

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 2 AND 29 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
 LOWER LIMB (AT V/C=1) = 25
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

```

*****
**
**          FREEWAY TRAVEL TIME (MINUTES)
**
*****
    
```

```

*****
* ORIGINS          DESTINATIONS ACROSS
* DOWN
*      1      2      3      4      5      6      7      8
+
* *****
* *
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 2 * 0.00 22.91 23.74 23.97 24.38 25.07 26.58 0.00
+
* 3 * 0.00 0.00 0.00 0.00 0.00 0.00 3.43 0.00
+
* 4 * 0.00 0.00 0.00 0.00 0.00 0.00 2.67 0.00
+
* 5 * 0.00 0.00 0.00 0.00 0.00 0.00 2.05 0.00
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
*
* *
*****
    
```

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMI | * SS | | | | |
|-----------|---------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|--------|---------|-----------|--------|---------|-----------------|----------------|-----------|------|------|------|
| * SEC | * LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | | | |
| * 1 | | | | | | | | | | | | | | | | | | | | |
| * 2 | 1 | 99999 | 894. | 0. | 894. | 894. | 0. | 894. | 1650. | 0. | 0. | .54 | 60. | 14.9 | B | 22.7 | 12.1 | | | |
| * 3 | 1 | 2830. | 0. | 0. | 894. | 0. | 0. | 894. | 1650. | 0. | 0. | .54 | 60. | 14.9 | B | 22.7 | 12.1 | | | |
| * 4 | 1 | 930. | 0. | 0. | 894. | 0. | 0. | 894. | 1650. | 0. | 0. | .54 | 60. | 14.9 | B | 22.7 | 12.1 | | | |
| * 5 | 1 | 1490. | 0. | 0. | 894. | 0. | 0. | 894. | 1650. | 0. | 0. | .54 | 60. | 14.9 | B | 22.7 | 12.1 | | | |
| * 6 | 1 | 3020. | 0. | 0. | 894. | 0. | 0. | 894. | 1650. | 0. | 0. | .54 | 60. | 14.9 | B | 22.7 | 12.1 | | | |
| * 7 | 1 | 1030. | 0. | 0. | 894. | 0. | 0. | 894. | 1650. | 0. | 0. | .54 | 60. | 14.9 | B | 22.7 | 12.1 | | | |
| * 8 | 1 | 1440. | 0. | 0. | 894. | 0. | 0. | 894. | 1650. | 0. | 0. | .54 | 60. | 14.9 | B | 22.7 | 12.1 | | | |
| * 9 | 1 | 1430. | 0. | 0. | 894. | 0. | 0. | 894. | 1650. | 0. | 0. | .54 | 60. | 14.9 | B | 22.7 | 12.1 | | | |
| * 10 | 1 | 3480. | 0. | 0. | 894. | 0. | 0. | 894. | 1650. | 0. | 0. | .54 | 60. | 14.9 | B | 22.7 | 12.1 | | | |
| * 11 | 1 | 1020. | 0. | 0. | 894. | 0. | 0. | 894. | 1650. | 0. | 0. | .54 | 60. | 14.9 | B | 22.7 | 12.1 | | | |
| * 12 | 1 | 980. | 0. | 0. | 894. | 0. | 0. | 894. | 1650. | 0. | 0. | .54 | 60. | 14.9 | B | 22.7 | 12.1 | | | |
| * 13 | 1 | 1800. | 0. | 0. | 894. | 0. | 0. | 894. | 1650. | 0. | 0. | .54 | 60. | 14.9 | B | 22.7 | 12.1 | | | |
| * 14 | 1 | 1500. | 0. | 104. | 894. | 0. | 104. | 894. | 1650. | 0. | 0. | .54 | 60. | 14.9 | B | 22.7 | 12.1 | | | |
| * 15 | 1 | 1300. | 0. | 0. | 791. | 0. | 0. | 791. | 1650. | 0. | 0. | .48 | 60. | 13.2 | B | 22.7 | 12.1 | | | |
| * 16 | 1 | 1000. | 40. | 0. | 830. | 40. | 0. | 830. | 1650. | 0. | 0. | .50 | 60. | 13.8 | B | 22.7 | 12.1 | | | |
| * 17 | 1 | 1100. | 0. | 0. | 830. | 0. | 0. | 830. | 1650. | 0. | 0. | .50 | 60. | 13.8 | B | 22.7 | 12.1 | | | |
| * 18 | 1 | 1000. | 0. | 27. | 830. | 0. | 27. | 830. | 1650. | 0. | 0. | .50 | 60. | 13.8 | B | 22.7 | 12.1 | | | |
| * 19 | 1 | 900. | 0. | 0. | 803. | 0. | 0. | 803. | 1650. | 0. | 0. | .49 | 60. | 13.4 | B | 22.7 | 12.1 | | | |
| * 20 | 1 | 100. | 37. | 0. | 840. | 37. | 0. | 840. | 1650. | 0. | 0. | .51 | 60. | 14.0 | B | 22.7 | 12.1 | | | |
| * 21 | 1 | 100. | 0. | 0. | 840. | 0. | 0. | 840. | 1650. | 0. | 0. | .51 | 60. | 14.0 | B | 22.7 | 12.1 | | | |
| * 22 | 1 | 100. | 0. | 72. | 840. | 0. | 72. | 840. | 1650. | 0. | 0. | .51 | 60. | 14.0 | B | 22.7 | 12.1 | | | |
| * 23 | 1 | 700. | 0. | 0. | 768. | 0. | 0. | 768. | 1650. | 0. | 0. | .47 | 60. | 12.8 | B | 22.7 | 12.1 | | | |
| * 24 | 1 | 1500. | 0. | 99. | 768. | 0. | 99. | 768. | 1650. | 0. | 0. | .47 | 60. | 12.8 | B | 22.7 | 12.1 | | | |
| * 25 | 1 | 800. | 0. | 0. | 669. | 0. | 0. | 669. | 1650. | 0. | 0. | .41 | 60. | 11.2 | B | 22.7 | 12.1 | | | |
| * 26 | 1 | 1000. | 243. | 0. | 913. | 243. | 0. | 913. | 1650. | 0. | 0. | .55 | 60. | 15.2 | B | 22.7 | 12.1 | | | |
| * 27 | 1 | 800. | 0. | 0. | 913. | 0. | 0. | 913. | 1650. | 0. | 0. | .55 | 60. | 15.2 | B | 22.7 | 12.1 | | | |
| * 28 | 1 | 1000. | 0. | 35. | 913. | 0. | 35. | 913. | 1650. | 0. | 0. | .55 | 60. | 15.2 | B | 22.7 | 12.1 | | | |
| * 29 | 1 | 8000. | 0. | 878. | 878. | 0. | 878. | 878. | 1650. | 0. | 0. | .53 | 60. | 14.6 | B | 22.7 | 12.1 | | | |
| * 30 | | | | | | | | | | | | | | | | | | | | |
| * 31 | | | | | | | | | | | | | | | | | | | | |
| * 32 | | | | | | | | | | | | | | | | | | | | |
| ***** | | | | | | | | | | | | | | | | | | | | |
| * TOTAL | 140349. | = | 26.6 | MILES | | | | | | | | | | | MAX(V/C) = 0.55 | LOWEST LOS = B | AVG = 60. | 14.8 | 22.7 | 12.1 |
| ***** | | | | | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|-----------------------------|--------------------|-----------------|-------------------|-----------------|
| FREWAY TRAVEL TIME = | 393. VEH-HRS | 786. PASS-HRS | 393. VEH-HRS | 786. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 393. VEH-HRS | 786. PASS-HRS | 393. VEH-HRS | 786. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 23590. VEH-MI. | 47180. PASS-MI. | 23590. VEH-MI. | 47180. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 60. MPH. | | 60. MPH. | |
| AVERAGE DENSITY = | 15. VPMP | | 15. VPMP | |
| TOTAL FUEL = | 1038. GALLONS | | 1038. GALLONS | |
| TOTAL EMISSIONS = | 286. KILOGRAMS | | 286. KILOGRAMS | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 21.72 | 3 | 0.61 | 4 | 0.20 | 5 | 0.32 |
| 6 | 0.66 | 7 | 0.22 | 8 | 0.31 | 9 | 0.31 | 10 | 0.76 |
| 11 | 0.22 | 12 | 0.21 | 13 | 0.39 | 14 | 0.33 | 15 | 0.25 |
| 16 | 0.20 | 17 | 0.22 | 18 | 0.20 | 19 | 0.18 | 20 | 0.02 |
| 21 | 0.02 | 22 | 0.02 | 23 | 0.13 | 24 | 0.28 | 25 | 0.13 |
| 26 | 0.22 | 27 | 0.18 | 28 | 0.22 | 29 | 1.71 | 30 | 0.00 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 30.2 VEH-HRS ***** AVERAGE DELAY = 2.04 MIN/VEH *****

**
** FREEWAY TRAVEL TIME (MINUTES) **
**

| ***** | | | | | | | | | |
|-----------|-----------------------|-------|-------|-------|-------|-------|-------|------|------|
| * ORIGINS | * DESTINATIONS ACROSS | | | | | | | | * |
| * DOWN | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | * |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 22.91 | 23.74 | 23.97 | 24.38 | 25.07 | 26.58 | 0.00 | |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.43 | 0.00 | |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.67 | 0.00 | |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.05 | 0.00 | |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| * * | | | | | | | | | |
| ***** | | | | | | | | | |

*
* TIME SLICE FREEWAY PERFORMANCE TABLE *
*

| * SUB NO. | * SEC LNS | * SSEC LENGTH | * O-D DATA ORG DES | * DEMANDS SSEC | * ADJUSTED VOLUMES ORG DES | * SSEC CAP. | * WEAVE EFF | * CONGEST LENGTH | * STORAGE RATE | * V/C RATIO | * SPEED MPH | * DENSITY VP/MPH | * LOS LEVEL | * FUEL MPG | * EMISSIONS GS/VM |
|-----------|-----------|---------------|--------------------|----------------|----------------------------|-------------|-------------|------------------|----------------|-------------|-------------|------------------|-------------|------------|-------------------|
| * 1 | | | | | | | | | | | | | | | |
| * 2 | 1 | 99999. | 952. | 0. | 952. | 952. | 0. | 952. | 1650. | 0. | 0. | .58 | 60. | 15.9 | B 22.7 12.1 |
| * 3 | 1 | 2830. | 0. | 0. | 952. | 0. | 0. | 952. | 1650. | 0. | 0. | .58 | 60. | 15.9 | B 22.7 12.1 |
| * 4 | 1 | 930. | 0. | 0. | 952. | 0. | 0. | 952. | 1650. | 0. | 0. | .58 | 60. | 15.9 | B 22.7 12.1 |
| * 5 | 1 | 1490. | 0. | 0. | 952. | 0. | 0. | 952. | 1650. | 0. | 0. | .58 | 60. | 15.9 | B 22.7 12.1 |
| * 6 | 1 | 3020. | 0. | 0. | 952. | 0. | 0. | 952. | 1650. | 0. | 0. | .58 | 60. | 15.9 | B 22.7 12.1 |
| * 7 | 1 | 1030. | 0. | 0. | 952. | 0. | 0. | 952. | 1650. | 0. | 0. | .58 | 60. | 15.9 | B 22.7 12.1 |
| * 8 | 1 | 1440. | 0. | 0. | 952. | 0. | 0. | 952. | 1650. | 0. | 0. | .58 | 60. | 15.9 | B 22.7 12.1 |
| * 9 | 1 | 1430. | 0. | 0. | 952. | 0. | 0. | 952. | 1650. | 0. | 0. | .58 | 60. | 15.9 | B 22.7 12.1 |
| * 10 | 1 | 3480. | 0. | 0. | 952. | 0. | 0. | 952. | 1650. | 0. | 0. | .58 | 60. | 15.9 | B 22.7 12.1 |
| * 11 | 1 | 1020. | 0. | 0. | 952. | 0. | 0. | 952. | 1650. | 0. | 0. | .58 | 60. | 15.9 | B 22.7 12.1 |
| * 12 | 1 | 980. | 0. | 0. | 952. | 0. | 0. | 952. | 1650. | 0. | 0. | .58 | 60. | 15.9 | B 22.7 12.1 |
| * 13 | 1 | 1800. | 0. | 0. | 952. | 0. | 0. | 952. | 1650. | 0. | 0. | .58 | 60. | 15.9 | B 22.7 12.1 |
| * 14 | 1 | 1500. | 0. | 158. | 952. | 0. | 158. | 952. | 1650. | 0. | 0. | .58 | 60. | 15.9 | B 22.7 12.1 |
| * 15 | 1 | 1300. | 0. | 0. | 794. | 0. | 0. | 794. | 1650. | 0. | 0. | .48 | 60. | 13.2 | B 22.7 12.1 |
| * 16 | 1 | 1000. | 39. | 0. | 833. | 39. | 0. | 833. | 1650. | 0. | 0. | .50 | 60. | 13.9 | B 22.7 12.1 |
| * 17 | 1 | 1100. | 0. | 0. | 833. | 0. | 0. | 833. | 1650. | 0. | 0. | .50 | 60. | 13.9 | B 22.7 12.1 |
| * 18 | 1 | 1000. | 0. | 30. | 833. | 0. | 30. | 833. | 1650. | 0. | 0. | .50 | 60. | 13.9 | B 22.7 12.1 |
| * 19 | 1 | 900. | 0. | 0. | 803. | 0. | 0. | 803. | 1650. | 0. | 0. | .49 | 60. | 13.4 | B 22.7 12.1 |
| * 20 | 1 | 100. | 27. | 0. | 830. | 27. | 0. | 830. | 1650. | 0. | 0. | .50 | 60. | 13.8 | B 22.7 12.1 |
| * 21 | 1 | 100. | 0. | 0. | 830. | 0. | 0. | 830. | 1650. | 0. | 0. | .50 | 60. | 13.8 | B 22.7 12.1 |
| * 22 | 1 | 100. | 0. | 111. | 830. | 0. | 111. | 830. | 1650. | 0. | 0. | .50 | 60. | 13.8 | B 22.7 12.1 |
| * 23 | 1 | 700. | 0. | 0. | 719. | 0. | 0. | 719. | 1650. | 0. | 0. | .44 | 60. | 12.0 | B 22.7 12.1 |
| * 24 | 1 | 1500. | 0. | 138. | 719. | 0. | 138. | 719. | 1650. | 0. | 0. | .44 | 60. | 12.0 | B 22.7 12.1 |
| * 25 | 1 | 800. | 0. | 0. | 581. | 0. | 0. | 581. | 1650. | 0. | 0. | .35 | 60. | 9.7 | A 22.7 12.1 |
| * 26 | 1 | 1000. | 215. | 0. | 796. | 215. | 0. | 796. | 1650. | 0. | 0. | .48 | 60. | 13.3 | B 22.7 12.1 |
| * 27 | 1 | 800. | 0. | 0. | 796. | 0. | 0. | 796. | 1650. | 0. | 0. | .48 | 60. | 13.3 | B 22.7 12.1 |
| * 28 | 1 | 1000. | 0. | 36. | 796. | 0. | 36. | 796. | 1650. | 0. | 0. | .48 | 60. | 13.3 | B 22.7 12.1 |
| * 29 | 1 | 8000. | 0. | 760. | 760. | 0. | 760. | 760. | 1650. | 0. | 0. | .46 | 60. | 12.7 | B 22.7 12.1 |
| * 30 | | | | | | | | | | | | | | | |
| * 31 | | | | | | | | | | | | | | | |
| * 32 | | | | | | | | | | | | | | | |
| * TOTAL | 140349. | = | 26.6 | MI | LES | | | MAX(V/C) = 0.58 | LOWEST LOS = B | AVG = 60. | 15.4 | 22.7 | 12.1 | | |

CURRENT TIME SLICE CUMULATIVE VALUES
FREeway TRAVEL TIME = 411. VEH-HRS 821. PASS-HRS 804. VEH-HRS 1608. PASS-HRS
FREeway MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 411. VEH-HRS 821. PASS-HRS 804. VEH-HRS 1608. PASS-HRS
TOTAL FRWAY TRAV DISTANCE = 24637. VEH-MI. 49274. PASS-MI. 48227. VEH-MI. 96455. PASS-MI.
AVERAGE SYSTEM SPEED = 60. MPH.
AVERAGE DENSITY = 15. VPMP/L
TOTAL FUEL = 1084. GALLONS
TOTAL EMISSIONS = 299. KI LOGRAMS 585. KI LOGRAMS

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

Table with 10 columns: SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY. Rows 1-31 showing delay values for various subsections.

***** TOTAL DELAY = 31.6 VEH-HRS ***** AVERAGE DELAY = 2.04 MIN/VEH *****

**
** FREeway TRAVEL TIME (MINUTES) **
**

Table with columns: ORIGINS, DESTINATIONS ACROSS, DOWN, 1, 2, 3, 4, 5, 6, 7, 8. Rows 1-8 showing travel times between subsections.

*
* TIME SLICE FREEWAY PERFORMANCE TABLE *

* SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMI SS *
* SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMP/L LEVEL MPG GS/VM *

```

*****
*
* 1
* 2 1 99999. 836. 0. 836. 836. 0. 836. 1650. 0. 0. 0. .51 60. 13.9 B 22.7 12.1 *
* 3 1 2830. 0. 0. 836. 0. 0. 836. 1650. 0. 0. 0. .51 60. 13.9 B 22.7 12.1 *
* 4 1 930. 0. 0. 836. 0. 0. 836. 1650. 0. 0. 0. .51 60. 13.9 B 22.7 12.1 *
* 5 1 1490. 0. 0. 836. 0. 0. 836. 1650. 0. 0. 0. .51 60. 13.9 B 22.7 12.1 *
* 6 1 3020. 0. 0. 836. 0. 0. 836. 1650. 0. 0. 0. .51 60. 13.9 B 22.7 12.1 *
* 7 1 1030. 0. 0. 836. 0. 0. 836. 1650. 0. 0. 0. .51 60. 13.9 B 22.7 12.1 *
* 8 1 1440. 0. 0. 836. 0. 0. 836. 1650. 0. 0. 0. .51 60. 13.9 B 22.7 12.1 *
* 9 1 1430. 0. 0. 836. 0. 0. 836. 1650. 0. 0. 0. .51 60. 13.9 B 22.7 12.1 *
* 10 1 3480. 0. 0. 836. 0. 0. 836. 1650. 0. 0. 0. .51 60. 13.9 B 22.7 12.1 *
* 11 1 1020. 0. 0. 836. 0. 0. 836. 1650. 0. 0. 0. .51 60. 13.9 B 22.7 12.1 *
* 12 1 980. 0. 0. 836. 0. 0. 836. 1650. 0. 0. 0. .51 60. 13.9 B 22.7 12.1 *
* 13 1 1800. 0. 0. 836. 0. 0. 836. 1650. 0. 0. 0. .51 60. 13.9 B 22.7 12.1 *
* 14 1 1500. 0. 124. 836. 0. 124. 836. 1650. 0. 0. 0. .51 60. 13.9 B 22.7 12.1 *
* 15 1 1300. 0. 0. 712. 0. 0. 712. 1650. 0. 0. 0. .43 60. 11.9 B 22.7 12.1 *
* 16 1 1000. 37. 0. 749. 37. 0. 749. 1650. 0. 0. 0. .45 60. 12.5 B 22.7 12.1 *
* 17 1 1100. 0. 0. 749. 0. 0. 749. 1650. 0. 0. 0. .45 60. 12.5 B 22.7 12.1 *
* 18 1 1000. 0. 24. 749. 0. 24. 749. 1650. 0. 0. 0. .45 60. 12.5 B 22.7 12.1 *
* 19 1 900. 0. 0. 725. 0. 0. 725. 1650. 0. 0. 0. .44 60. 12.1 B 22.7 12.1 *
* 20 1 100. 28. 0. 753. 28. 0. 753. 1650. 0. 0. 0. .46 60. 12.6 B 22.7 12.1 *
* 21 1 100. 0. 0. 753. 0. 0. 753. 1650. 0. 0. 0. .46 60. 12.6 B 22.7 12.1 *
* 22 1 100. 0. 97. 753. 0. 97. 753. 1650. 0. 0. 0. .46 60. 12.6 B 22.7 12.1 *
* 23 1 700. 0. 0. 656. 0. 0. 656. 1650. 0. 0. 0. .40 60. 10.9 A 22.7 12.1 *
* 24 1 1500. 0. 117. 656. 0. 117. 656. 1650. 0. 0. 0. .40 60. 10.9 A 22.7 12.1 *
* 25 1 800. 0. 0. 538. 0. 0. 538. 1650. 0. 0. 0. .33 60. 9.0 A 22.7 12.1 *
* 26 1 1000. 225. 0. 763. 225. 0. 763. 1650. 0. 0. 0. .46 60. 12.7 B 22.7 12.1 *
* 27 1 800. 0. 0. 763. 0. 0. 763. 1650. 0. 0. 0. .46 60. 12.7 B 22.7 12.1 *
* 28 1 1000. 0. 23. 763. 0. 23. 763. 1650. 0. 0. 0. .46 60. 12.7 B 22.7 12.1 *
* 29 1 8000. 0. 740. 740. 0. 740. 740. 1650. 0. 0. 0. .45 60. 12.3 B 22.7 12.1 *
* 30
* 31
* 32
*****
*
* TOTAL 140349. = 26.6 MILES MAX(V/C) = 0.51 LOWEST LOS = B AVG = 60. 13.7 22.7 12.1 *
*
*****

```

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|-----------------------------|--------------------|-----------------|-------------------|------------------|
| FREEWAY TRAVEL TIME = | 364. VEH-HRS | 727. PASS-HRS | 1167. VEH-HRS | 2335. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 364. VEH-HRS | 727. PASS-HRS | 1167. VEH-HRS | 2335. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 21822. VEH-MI. | 43644. PASS-MI. | 70049. VEH-MI. | 140099. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 60. MPH. | | 60. MPH. | |
| AVERAGE DENSITY = | 14. VPMP/L | | 15. VPMP/L | |
| TOTAL FUEL = | 960. GALLONS | | 3082. GALLONS | |
| TOTAL EMISSIONS = | 264. KILOGRAMS | | 849. KILOGRAMS | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 20.31 | 3 | 0.57 | 4 | 0.19 | 5 | 0.30 |
| 6 | 0.61 | 7 | 0.21 | 8 | 0.29 | 9 | 0.29 | 10 | 0.71 |
| 11 | 0.21 | 12 | 0.20 | 13 | 0.37 | 14 | 0.30 | 15 | 0.22 |
| 16 | 0.18 | 17 | 0.20 | 18 | 0.18 | 19 | 0.16 | 20 | 0.02 |
| 21 | 0.02 | 22 | 0.02 | 23 | 0.11 | 24 | 0.24 | 25 | 0.10 |
| 26 | 0.19 | 27 | 0.15 | 28 | 0.19 | 29 | 1.44 | 30 | 0.00 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 28.0 VEH-HRS ***** AVERAGE DELAY = 2.04 MIN/VEH *****

**
** FREEWAY TRAVEL TIME (MINUTES) **
**

* ORIGINS DESTINATIONS ACROSS *

| * DOWN | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|--------|------|-------|-------|-------|-------|-------|------|-------|
| * 1 * | 0.09 | 22.99 | 23.83 | 24.06 | 24.47 | 25.15 | 0.00 | 30.73 |
| * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 3 * | 0.00 | 0.00 | 0.59 | 0.81 | 1.23 | 1.91 | 0.00 | 7.49 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.06 | 0.47 | 1.16 | 0.00 | 6.73 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.53 | 0.00 | 6.10 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.82 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.64 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMI SS | | | | |
|--|--------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|--------|---------|-----------|---------|---------|----------|---------|------|------|------|
| * SEC | * LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VP/MP | * LEVEL | * MPG | * GS/VM | | | |
| * 1 | 4 | 500. | 5261. | 894. | 5261. | 5261. | 894. | 5261. | 10000. | 0. | 0. | .53 | 65. | 20.2 | C | 19.2 | 14.0 | | |
| * 2 | 3 | 99999. | 0. | 0. | 4367. | 0. | 0. | 4367. | 7000. | 0. | 0. | .62 | 60. | 24.3 | C | 21.6 | 12.3 | | |
| * 3 | 3 | 2830. | 0. | 0. | 4367. | 0. | 0. | 4367. | 7000. | 0. | 0. | .62 | 60. | 24.3 | C | 21.6 | 12.3 | | |
| * 4 | 3 | 930. | 0. | 0. | 4367. | 0. | 0. | 4367. | 7000. | 0. | 0. | .62 | 60. | 24.3 | C | 21.6 | 12.3 | | |
| * 5 | 3 | 1490. | 0. | 0. | 4367. | 0. | 0. | 4367. | 7000. | 0. | 0. | .62 | 60. | 24.3 | C | 21.6 | 12.3 | | |
| * 6 | 3 | 3020. | 0. | 0. | 4367. | 0. | 0. | 4367. | 7000. | 0. | 0. | .62 | 60. | 24.3 | C | 21.6 | 12.3 | | |
| * 7 | 3 | 1030. | 0. | 0. | 4367. | 0. | 0. | 4367. | 7000. | 0. | 0. | .62 | 60. | 24.3 | C | 21.6 | 12.3 | | |
| * 8 | 3 | 1440. | 0. | 0. | 4367. | 0. | 0. | 4367. | 7000. | 0. | 0. | .62 | 60. | 24.3 | C | 21.6 | 12.3 | | |
| * 9 | 3 | 1430. | 0. | 0. | 4367. | 0. | 0. | 4367. | 7000. | 0. | 0. | .62 | 60. | 24.3 | C | 21.6 | 12.3 | | |
| * 10 | 3 | 3480. | 0. | 0. | 4367. | 0. | 0. | 4367. | 7000. | 0. | 0. | .62 | 60. | 24.3 | C | 21.6 | 12.3 | | |
| * 11 | 3 | 1020. | 0. | 0. | 4367. | 0. | 0. | 4367. | 7000. | 0. | 0. | .62 | 60. | 24.3 | C | 21.6 | 12.3 | | |
| * 12 | 3 | 980. | 0. | 0. | 4367. | 0. | 0. | 4367. | 7000. | 0. | 0. | .62 | 60. | 24.3 | C | 21.6 | 12.3 | | |
| * 13 | 3 | 1800. | 0. | 0. | 4367. | 0. | 0. | 4367. | 7000. | 0. | 0. | .62 | 60. | 24.3 | C | 21.6 | 12.3 | | |
| * 14 | 3 | 1500. | 0. | 506. | 4367. | 0. | 506. | 4367. | 6896. | 0. | 0. | .63 | 60. | 24.3 | C | 21.6 | 12.3 | | |
| * 15 | 3 | 1300. | 0. | 0. | 3860. | 0. | 0. | 3860. | 6000. | 0. | 0. | .64 | 60. | 21.4 | C | 21.6 | 12.3 | | |
| * 16 | 3 | 1000. | 289. | 0. | 4150. | 289. | 0. | 4150. | 5960. | 0. | 0. | .70 | 60. | 23.1 | C | 21.6 | 12.3 | | |
| * 17 | 3 | 1100. | 0. | 0. | 4150. | 0. | 0. | 4150. | 6000. | 0. | 0. | .69 | 60. | 23.1 | C | 21.6 | 12.3 | | |
| * 18 | 3 | 1000. | 0. | 143. | 4150. | 0. | 143. | 4150. | 5973. | 0. | 0. | .69 | 60. | 23.1 | C | 21.6 | 12.3 | | |
| * 19 | 3 | 900. | 0. | 0. | 4007. | 0. | 0. | 4007. | 6000. | 0. | 0. | .67 | 60. | 22.3 | C | 21.6 | 12.3 | | |
| * 20 | 3 | 100. | 258. | 0. | 4265. | 258. | 0. | 4265. | 5963. | 0. | 0. | .72 | 60. | 23.7 | C | 21.6 | 12.3 | | |
| * 21 | 3 | 100. | 0. | 0. | 4265. | 0. | 0. | 4265. | 6000. | 0. | 0. | .71 | 60. | 23.7 | C | 21.6 | 12.3 | | |
| * 22 | 3 | 100. | 0. | 408. | 4265. | 0. | 408. | 4265. | 5928. | 0. | 0. | .72 | 60. | 23.7 | C | 21.6 | 12.3 | | |
| * 23 | 3 | 700. | 0. | 0. | 3857. | 0. | 0. | 3857. | 6000. | 0. | 0. | .64 | 60. | 21.4 | C | 21.6 | 12.3 | | |
| * 24 | 3 | 1500. | 0. | 561. | 3857. | 0. | 561. | 3857. | 5901. | 0. | 0. | .65 | 60. | 21.4 | C | 21.6 | 12.3 | | |
| * 25 | 3 | 800. | 0. | 0. | 3296. | 0. | 0. | 3296. | 6000. | 0. | 0. | .55 | 60. | 18.3 | C | 21.6 | 12.3 | | |
| * 26 | 3 | 1000. | 1277. | 0. | 4572. | 1277. | 0. | 4572. | 5757. | 0. | 0. | .79 | 60. | 25.4 | C | 21.6 | 12.3 | | |
| * 27 | 3 | 800. | 0. | 0. | 4572. | 0. | 0. | 4572. | 6000. | 0. | 0. | .76 | 60. | 25.4 | C | 21.6 | 12.3 | | |
| * 28 | 3 | 1000. | 0. | 285. | 4572. | 0. | 285. | 4572. | 5965. | 0. | 0. | .77 | 60. | 25.4 | C | 21.6 | 12.3 | | |
| * 29 | 3 | 8000. | 0. | 0. | 4287. | 0. | 0. | 3822. | 6000. | 0. | * | 5268. | 465. | .64 | 19. | 66.7 | F | 16.2 | 16.4 |
| * 30 | 4 | 100. | 878. | 0. | 5165. | 878. | 0. | 4700. | 8000. | 0. | ** | 100. | 465. | .59 | 6. | 185.3 | F | 9.3 | 27.0 |
| * 31 | 4 | 1000. | 800. | 0. | 5965. | 800. | 0. | 5500. | 5500. | 0. | 0. | 1.00 | 65. | 21.2 | E | 19.2 | 14.0 | | |
| * 32 | 4 | 2640. | 0. | 5965. | 5965. | 0. | 5500. | 5500. | 8000. | 0. | 0. | .69 | 65. | 21.2 | C | 20.0 | 13.7 | | |
| ***** | | | | | | | | | | | | | | | | | | | |
| * TOTAL 144589. = 27.4 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 54. 26.5 21.2 12.6 * | | | | | | | | | | | | | | | | | | | |
| ***** | | | | | | | | | | | | | | | | | | | |

| | | |
|-----------------------|---------------------------------|---------------------------------|
| | CURRENT TIME SLICE | CUMULATIVE VALUES |
| FREEWAY TRAVEL TIME = | 2223. VEH-HRS 2237. PASS-HRS | 2223. VEH-HRS 2237. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |

| | | | | | | | | | | | | | | | | | | | | | |
|---|----|---|-------|-------|-------|-------|-------|-------|-------|-------|----|----|-------|-------|-----|------|-------|------|------|------|---|
| * | 13 | 3 | 1800. | 0. | 0. | 4648. | 0. | 0. | 4648. | 7000. | 0. | 0. | 0. | .66 | 60. | 25.8 | C | 21.6 | 12.3 | * | |
| * | 14 | 3 | 1500. | 0. | 772. | 4648. | 0. | 772. | 4648. | 6842. | 0. | 0. | 0. | .68 | 60. | 25.8 | C | 21.6 | 12.3 | * | |
| * | 15 | 3 | 1300. | 0. | 0. | 3876. | 0. | 0. | 3876. | 6000. | 0. | 0. | 0. | .65 | 60. | 21.5 | C | 21.6 | 12.3 | * | |
| * | 16 | 3 | 1000. | 340. | 0. | 4216. | 340. | 0. | 4216. | 5961. | 0. | 0. | 0. | .71 | 60. | 23.4 | C | 21.6 | 12.3 | * | |
| * | 17 | 3 | 1100. | 0. | 0. | 4216. | 0. | 0. | 4216. | 6000. | 0. | 0. | 0. | .70 | 60. | 23.4 | C | 21.6 | 12.3 | * | |
| * | 18 | 3 | 1000. | 0. | 160. | 4216. | 0. | 160. | 4216. | 5970. | 0. | 0. | 0. | .71 | 60. | 23.4 | C | 21.6 | 12.3 | * | |
| * | 19 | 3 | 900. | 0. | 0. | 4056. | 0. | 0. | 4056. | 6000. | 0. | 0. | 0. | .68 | 60. | 22.5 | C | 21.6 | 12.3 | * | |
| * | 20 | 3 | 100. | 223. | 0. | 4279. | 223. | 0. | 4279. | 5973. | 0. | 0. | 0. | .72 | 60. | 23.8 | C | 21.6 | 12.3 | * | |
| * | 21 | 3 | 100. | 0. | 0. | 4279. | 0. | 0. | 4279. | 6000. | 0. | 0. | 0. | .71 | 60. | 23.8 | C | 21.6 | 12.3 | * | |
| * | 22 | 3 | 100. | 0. | 629. | 4279. | 0. | 629. | 4279. | 5889. | 0. | 0. | 0. | .73 | 60. | 23.8 | C | 21.6 | 12.3 | * | |
| * | 23 | 3 | 700. | 0. | 0. | 3650. | 0. | 0. | 3650. | 6000. | 0. | 0. | 0. | .61 | 60. | 20.3 | C | 21.6 | 12.3 | * | |
| * | 24 | 3 | 1500. | 0. | 782. | 3650. | 0. | 782. | 3650. | 5862. | 0. | 0. | 0. | .62 | 60. | 20.3 | C | 21.6 | 12.3 | * | |
| * | 25 | 3 | 800. | 0. | 0. | 2868. | 0. | 0. | 2298. | 6000. | 0. | * | 183. | .570. | .38 | 56. | 13.6 | F | 21.5 | 12.4 | * |
| * | 26 | 3 | 1000. | 1145. | 0. | 4013. | 1145. | 0. | 3443. | 5785. | 0. | ** | 1000. | .570. | .60 | 32. | 35.8 | F | 19.0 | 13.9 | * |
| * | 27 | 3 | 800. | 0. | 0. | 4013. | 0. | 0. | 3443. | 6000. | 0. | ** | 800. | .570. | .57 | 19. | 59.8 | F | 16.3 | 15.9 | * |
| * | 28 | 3 | 1000. | 0. | 303. | 4013. | 0. | 303. | 3443. | 5964. | 0. | ** | 1000. | .570. | .58 | 14. | 83.7 | F | 14.2 | 18.0 | * |
| * | 29 | 3 | 8000. | 0. | 0. | 3710. | 0. | 0. | 3140. | 6000. | 0. | ** | 8000. | .570. | .52 | 6. | 186.0 | F | 9.0 | 26.9 | * |
| * | 30 | 4 | 100. | 760. | 0. | 4470. | 760. | 0. | 3900. | 8000. | 0. | ** | 100. | .570. | .49 | 5. | 214.0 | F | 8.4 | 28.7 | * |
| * | 31 | 4 | 1000. | 1600. | 0. | 6070. | 1600. | 0. | 5500. | 5500. | 0. | 0. | 0. | 1.00 | 65. | 21.2 | E | 19.2 | 14.0 | * | |
| * | 32 | 4 | 2640. | 0. | 6070. | 6070. | 0. | 5500. | 5500. | 8000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 20.0 | 13.7 | * | |

 * TOTAL 144589. = 27.4 MI LES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 42. 35.1 20.3 13.0 *

| | | | | | | | | | |
|-----------------------------|---------|--------------------|---------|----------|---------|-------------------|---------|----------|--|
| | | CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | |
| FREEWAY TRAVEL TIME = | 2928. | VEH-HRS | 2943. | PASS-HRS | 5150. | VEH-HRS | 5180. | PASS-HRS | |
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS | |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS | |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS | |
| TOTAL SYSTEM TRAVEL TIME = | 2928. | VEH-HRS | 2943. | PASS-HRS | 5150. | VEH-HRS | 5180. | PASS-HRS | |
| TOTAL FRWAY TRAV DISTANCE = | 124066. | VEH-MI. | 124856. | PASS-MI. | 243584. | VEH-MI. | 245151. | PASS-MI. | |
| AVERAGE SYSTEM SPEED = | 42. | MPH. | | | 47. | MPH. | | | |
| AVERAGE DENSITY = | 35. | VPMP/L | | | 31. | VPMP/L | | | |
| TOTAL FUEL = | 6104. | GALLONS | | | 11753. | GALLONS | | | |
| TOTAL EMISSIONS = | 1614. | KILOGRAMS | | | 3120. | KILOGRAMS | | | |

***** MAINTLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|--------|------------|-------|------------|--------|------------|-------|
| 1 | 0.00 | 2 | 112.86 | 3 | 3.19 | 4 | 1.05 | 5 | 1.68 |
| 6 | 3.41 | 7 | 1.16 | 8 | 1.63 | 9 | 1.61 | 10 | 3.93 |
| 11 | 1.15 | 12 | 1.11 | 13 | 2.03 | 14 | 1.69 | 15 | 1.22 |
| 16 | 1.02 | 17 | 1.13 | 18 | 1.02 | 19 | 0.89 | 20 | 0.10 |
| 21 | 0.10 | 22 | 0.10 | 23 | 0.62 | 24 | 1.33 | 25 | 1.05 |
| 26 | 11.82 | 27 | 21.51 | 28 | 41.13 | 29 | 784.20 | 30 | 15.07 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 1018.8 VEH-HRS ***** AVERAGE DELAY = 18.42 MIN/VEH *****

 **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN

| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-------|------|-------|-------|-------|-------|-------|------|-------|
| * 1 * | 0.09 | 22.99 | 23.83 | 24.06 | 24.47 | 26.16 | 0.00 | 37.85 |
| * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 3 * | 0.00 | 0.00 | 0.59 | 0.81 | 1.23 | 2.91 | 0.00 | 14.61 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.06 | 0.47 | 2.16 | 0.00 | 13.85 |

```

+ * 5 * 0.00 0.00 0.00 0.00 0.00 1.52 0.00 13.22 *
+ * 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.81 *
+ * 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.64 *
* * *
*****

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 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED | VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS | | | |
|-----------|--------|--------------|--------------|--------------|---------|-------|--------|---------|---------|-----|--------|---------|-----|-------|--------|------|------|------|
| * SEC LNS | LENGTH | ORG DES SSEC | ORG DES SSEC | ORG DES SSEC | CAP. | EFF | LENGTH | RATE | RATIO | MPH | VP/MPL | LEVEL | MPG | GS/VM | | | | |
| * 1 4 | 500. | 4920. | 836. | 4920. | 4920. | 836. | 4920. | 10000. | 0. | 0. | 0. | .49 | 65. | 18.9 | C | 19.2 | 14.0 | |
| * 2 3 | 99999. | 0. | 0. | 4084. | 0. | 0. | 4084. | 7000. | 0. | 0. | 0. | .58 | 60. | 22.7 | C | 21.6 | 12.3 | |
| * 3 3 | 2830. | 0. | 0. | 4084. | 0. | 0. | 4084. | 7000. | 0. | 0. | 0. | .58 | 60. | 22.7 | C | 21.6 | 12.3 | |
| * 4 3 | 930. | 0. | 0. | 4084. | 0. | 0. | 4084. | 7000. | 0. | 0. | 0. | .58 | 60. | 22.7 | C | 21.6 | 12.3 | |
| * 5 3 | 1490. | 0. | 0. | 4084. | 0. | 0. | 4084. | 7000. | 0. | 0. | 0. | .58 | 60. | 22.7 | C | 21.6 | 12.3 | |
| * 6 3 | 3020. | 0. | 0. | 4084. | 0. | 0. | 4084. | 7000. | 0. | 0. | 0. | .58 | 60. | 22.7 | C | 21.6 | 12.3 | |
| * 7 3 | 1030. | 0. | 0. | 4084. | 0. | 0. | 4084. | 7000. | 0. | 0. | 0. | .58 | 60. | 22.7 | C | 21.6 | 12.3 | |
| * 8 3 | 1440. | 0. | 0. | 4084. | 0. | 0. | 4084. | 7000. | 0. | 0. | 0. | .58 | 60. | 22.7 | C | 21.6 | 12.3 | |
| * 9 3 | 1430. | 0. | 0. | 4084. | 0. | 0. | 4084. | 7000. | 0. | 0. | 0. | .58 | 60. | 22.7 | C | 21.6 | 12.3 | |
| * 10 3 | 3480. | 0. | 0. | 4084. | 0. | 0. | 4084. | 7000. | 0. | 0. | 0. | .58 | 60. | 22.7 | C | 21.6 | 12.3 | |
| * 11 3 | 1020. | 0. | 0. | 4084. | 0. | 0. | 4084. | 7000. | 0. | 0. | 0. | .58 | 60. | 22.7 | C | 21.6 | 12.3 | |
| * 12 3 | 980. | 0. | 0. | 4084. | 0. | 0. | 4084. | 7000. | 0. | 0. | 0. | .58 | 60. | 22.7 | C | 21.6 | 12.3 | |
| * 13 3 | 1800. | 0. | 0. | 4084. | 0. | 0. | 4084. | 7000. | 0. | 0. | 0. | .58 | 60. | 22.7 | C | 21.6 | 12.3 | |
| * 14 3 | 1500. | 0. | 606. | 4084. | 0. | 606. | 4084. | 6876. | 0. | 0. | 0. | .59 | 60. | 22.7 | C | 21.6 | 12.3 | |
| * 15 3 | 1300. | 0. | 0. | 3478. | 0. | 0. | 3478. | 6000. | 0. | 0. | 0. | .58 | 60. | 19.3 | C | 21.6 | 12.3 | |
| * 16 3 | 1000. | 303. | 0. | 3781. | 303. | 0. | 3781. | 5963. | 0. | 0. | 0. | .63 | 60. | 21.0 | C | 21.6 | 12.3 | |
| * 17 3 | 1100. | 0. | 0. | 3781. | 0. | 0. | 3781. | 6000. | 0. | 0. | 0. | .63 | 60. | 21.0 | C | 21.6 | 12.3 | |
| * 18 3 | 1000. | 0. | 126. | 3781. | 0. | 126. | 3781. | 5976. | 0. | 0. | 0. | .63 | 60. | 21.0 | C | 21.6 | 12.3 | |
| * 19 3 | 900. | 0. | 0. | 3655. | 0. | 0. | 3655. | 6000. | 0. | 0. | 0. | .61 | 60. | 20.3 | C | 21.6 | 12.3 | |
| * 20 3 | 100. | 222. | 0. | 3877. | 222. | 0. | 3877. | 5972. | 0. | 0. | 0. | .65 | 60. | 21.5 | C | 21.6 | 12.3 | |
| * 21 3 | 100. | 0. | 0. | 3877. | 0. | 0. | 3877. | 6000. | 0. | 0. | 0. | .65 | 60. | 21.5 | C | 21.6 | 12.3 | |
| * 22 3 | 100. | 0. | 558. | 3877. | 0. | 558. | 3877. | 5903. | 0. | 0. | 0. | .66 | 60. | 21.5 | C | 21.6 | 12.3 | |
| * 23 3 | 700. | 0. | 0. | 3319. | 0. | 0. | 3319. | 6000. | 0. | 0. | 0. | .55 | 60. | 18.4 | C | 21.6 | 12.3 | |
| * 24 3 | 1500. | 0. | 673. | 3319. | 0. | 673. | 3319. | 5883. | 0. | 0. | 0. | .56 | 60. | 18.4 | C | 21.6 | 12.3 | |
| * 25 3 | 800. | 0. | 0. | 2647. | 0. | 0. | 2647. | 6000. | 0. | 0. | 0. | .44 | 56. | 15.8 | B | 21.4 | 12.4 | |
| * 26 3 | 1000. | 1165. | 0. | 3812. | 1165. | 0. | 3812. | 5775. | 0. | 0. | 0. | .66 | 33. | 38.1 | E | 19.5 | 14.0 | |
| * 27 3 | 800. | 0. | 0. | 3812. | 0. | 0. | 3812. | 6000. | 0. | 0. | 0. | .64 | 21. | 61.5 | F | 16.9 | 16.2 | |
| * 28 3 | 1000. | 0. | 197. | 3812. | 0. | 197. | 3812. | 5977. | 0. | 0. | 0. | .64 | 15. | 82.8 | F | 15.1 | 18.3 | |
| * 29 3 | 8000. | 0. | 0. | 3615. | 0. | 0. | 4010. | 6000. | 0. | * | 6021. | -.395. | .67 | 8. | 160.0 | F | 11.0 | 24.5 |
| * 30 4 | 100. | 740. | 0. | 4355. | 740. | 0. | 4750. | 8000. | 0. | ** | 100. | -.395. | .59 | 6. | 186.2 | F | 9.3 | 27.1 |
| * 31 4 | 1000. | 750. | 0. | 5105. | 750. | 0. | 5500. | 5500. | 0. | 0. | 0. | 1.00 | 65. | 21.2 | E | 19.2 | 14.0 | |
| * 32 4 | 2640. | 0. | 5105. | 5105. | 0. | 5500. | 5500. | 8000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 20.0 | 13.7 | |

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* TOTAL 144589. = 27.4 MI L E S
* MAX(V/C) = 1.00 LOWEST LOS = F AVG = 44. 30.9 20.4 13.1
*
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| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 2558. VEH-HRS | 7708. VEH-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 2558. VEH-HRS | 7708. VEH-HRS |
| TOTAL FRWY TRAV DISTANCE = | 111726. VEH-MI. | 355310. VEH-MI. |
| AVERAGE SYSTEM SPEED = | 44. MPH. | 46. MPH. |
| AVERAGE DENSITY = | 31. VP/MPL | 31. VP/MPL |
| TOTAL FUEL = | 5487. GALLONS | 17240. GALLONS |
| TOTAL EMISSIONS = | 1466. KI LOGRAMS | 4587. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
 SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY

| | | | | | | | | | |
|----|-------|----|-------|----|-------|----|--------|----|-------|
| 1 | 0.00 | 2 | 99.15 | 3 | 2.81 | 4 | 0.92 | 5 | 1.48 |
| 6 | 2.99 | 7 | 1.02 | 8 | 1.43 | 9 | 1.42 | 10 | 3.45 |
| 11 | 1.01 | 12 | 0.97 | 13 | 1.78 | 14 | 1.49 | 15 | 1.10 |
| 16 | 0.92 | 17 | 1.01 | 18 | 0.92 | 19 | 0.80 | 20 | 0.09 |
| 21 | 0.09 | 22 | 0.09 | 23 | 0.56 | 24 | 1.21 | 25 | 1.03 |
| 26 | 10.67 | 27 | 19.67 | 28 | 37.75 | 29 | 630.43 | 30 | 12.72 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 839.0 VEH-HRS ***** AVERAGE DELAY = 12.57 MIN/VEH *****

US 101 Southbound

```

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A.D.MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQQ QQQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP LLL
FFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 2222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 11111111 2222222222 PPP LLLLLLLLLL
    
```

FREQ12PL

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 2 AND 26 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
 LOWER LIMB (AT V/C=1) = 25
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

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*****
*****
**
** FREEWAY AND ARTERIAL DESIGN FEATURES
**
*****
*****
** SUB NO. SSEC SSEC DESIGN ORG TRK SSEC PCT PCT DES SPECIAL FF.SPD. CAP. ART GRADE SUBSECTION LOCATION
** SEC LNS CAP LENGTH SPEED DES FAC GRAD TRK TRUCKS RAMP ALT. RTE ALT. RTE TYPE ALT. RTE
**
**
** 1
**
** 2 1 1650. 99999. 60 0 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Queue Capture
**
** 3 1 1650. 2740. 60 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 SR-85 Off to Shore On
**
** 4 1 1650. 600. 60 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Shore. On to Moffett Off
**
** 5 1 1650. 700. 60 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Moffett Off to On
**
** 6 1 1650. 2630. 60 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Moffett On to Ellis Off
**
** 7 1 1650. 2530. 60 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Ellis Off to On-ramp
**
** 8 1 1650. 1500. 60 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Ellis On-ramp
**
** 9 1 1650. 700. 60 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Ellis / US 237
**
** 10 1 1650. 1500. 60 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 SR-237 EB Off-Ramp
**
** 11 1 1650. 750. 60 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 SR-237 / SR-237
**
    
```


| | | | | | | | | | | | | | | | | | | |
|----|----|----|---|-------|-------|----|------|------|-----|---|----|-----|-----|------|------|-------------------------|-------------------------|----|
| ** | ** | 6 | 3 | 6000. | 2630. | 60 | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | GOOD | 0.0 | Moffett On to Ellis Off | ** | |
| ** | ** | 7 | 3 | 6000. | 2530. | 60 | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | GOOD | 0.0 | Ellis Off to On-ramp | ** | |
| ** | ** | 8 | 3 | 6000. | 1500. | 60 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0.0 | GOOD | 0.0 | Ellis On-ramp | ** |
| ** | ** | 9 | 3 | 6000. | 700. | 60 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0.0 | GOOD | 0.0 | Ellis / US 237 | ** |
| ** | ** | 10 | 3 | 6000. | 1500. | 60 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | GOOD | 0.0 | SR-237 EB Off-Ramp | ** |
| ** | ** | 11 | 3 | 6000. | 750. | 60 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | GOOD | 0.0 | SR-237 / SR-237 | ** |
| ** | ** | 12 | 4 | 8000. | 350. | 60 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0.0 | GOOD | 0.0 | SR-237 EB On-Ramp | ** |
| ** | ** | 13 | 4 | 8000. | 350. | 60 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0.0 | GOOD | 0.0 | US 237 / Mathilda | ** |
| ** | ** | 14 | 4 | 8000. | 350. | 60 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | GOOD | 0.0 | Mathilda Off-Ramp | ** |
| ** | ** | 15 | 3 | 6000. | 700. | 60 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | GOOD | 0.0 | Mathilda / Mathilda | ** |
| ** | ** | 16 | 3 | 6000. | 900. | 60 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0.0 | GOOD | 0.0 | Mathilda SB On-Ramp | ** |
| ** | ** | 17 | 3 | 6000. | 1400. | 60 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0.0 | GOOD | 0.0 | Mathilda NB On-Ramp | ** |
| ** | ** | 18 | 3 | 6000. | 200. | 60 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | GOOD | 0.0 | Mathilda / Fair Oaks | ** |
| ** | ** | 19 | 3 | 6000. | 1400. | 60 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | GOOD | 0.0 | Fair Oaks SB Off-Ramp | ** |
| ** | ** | 20 | 3 | 6000. | 900. | 60 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | GOOD | 0.0 | Fair Oaks SB/ Fair Oaks | ** |
| ** | ** | | | | | | | | | | | | | | | | ** | |

FREEWAY AND ARTERIAL DESIGN FEATURES

| ** | ** | SUB NO. | SSEC | SSEC | DESIGN | ORG | TRK | SSEC | PCT | PCT | DES | SPECIAL | FF.SPD. | CAP. | ART | GRADE | SUBSECTION | LOCATION | ** |
|----|----|---------|------|-------|--------|-------|-----|------|------|-----|--------|---------|---------|---------|------|---------|--------------------------|----------|----|
| ** | ** | SEC | LN | CAP | LENGTH | SPEED | DES | FAC | GRAD | TRK | TRUCKS | RAMP | ALT.RTE | ALT.RTE | TYPE | ALT.RTE | | | ** |
| ** | ** | 21 | 4 | 8000. | 100. | 60 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0.0 | GOOD | 0.0 | Fair Oaks SB On-Ramp | ** | |
| ** | ** | 22 | 4 | 8000. | 100. | 60 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | GOOD | 0.0 | Fair Oaks NB Off-Ramp | ** | |
| ** | ** | 23 | 3 | 6000. | 600. | 60 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | GOOD | 0.0 | Fair Oaks NB/ Fair Oaks | ** | |
| ** | ** | 24 | 3 | 6000. | 1500. | 60 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0.0 | GOOD | 0.0 | Oaks On-Ramp to Mid | ** | |
| ** | ** | 25 | 3 | 6000. | 1500. | 60 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0.0 | GOOD | 0.0 | Mid to Lawrence Off-ramp | ** | |
| ** | ** | 26 | 3 | 6000. | 8000. | 60 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | GOOD | 0.0 | HOV Dummy | ** | |
| ** | ** | 27 | 4 | 8000. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0.0 | GOOD | 0.0 | HOV Dummy | ** | |
| ** | ** | 28 | 4 | 7750. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0.0 | GOOD | 0.0 | Dummy Bottleneck | ** | |
| ** | ** | 29 | 4 | 7750. | 1000. | 65 | OD | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0.0 | GOOD | 0.0 | End of Network | ** | |


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FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A.D.MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP LLL
FFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 2222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 11111111 2222222222 PPP LLLLLLLLLL
    
```

FREQ12PL

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 2 AND 26 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
 LOWER LIMB (AT V/C=1) = 25
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

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*****
**
**          FREEWAY TRAVEL TIME (MINUTES)
**
*****
    
```

```

*****
* ORIGINS          DESTINATIONS ACROSS
* DOWN
*      1      2      3      4      5      6      7
+
* *****
* *
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 2 * 0.00 21.38 21.72 22.59 22.80 25.00 0.00
+
* 3 * 0.00 0.00 0.00 0.00 2.12 4.32 0.00
+
* 4 * 0.00 0.00 0.00 0.00 0.00 3.48 0.00
+
* 5 * 0.00 0.00 0.00 0.00 0.00 3.14 0.00
+
* 6 * 0.00 0.00 0.00 0.00 0.00 2.97 0.00
+
* 7 * 0.00 0.00 0.00 0.00 0.00 2.23 0.00
+
* 8 * 0.00 0.00 0.00 0.00 0.00 2.08 0.00
+
* 9 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 10 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
    
```

* 11 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | |
|-----------|----------|------------|------------|--------------------|--------|-------------|-----------|-----------|-----------------|---------|----------------|---------|-----------|-------------|------|------|
| * SEC LNS | * LENGTH | * ORG | * DES SSEC | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMPPL | * LEVEL | * MPG | * GS/VM | | |
| * 2 | 1 | 99999. | 1040. | 0. 1040. | 1040. | 0. 1040. | 1650. | 0. | 0. | 0. | .63 | 60. | 17.3 | B | 22.7 | 12.1 |
| * 3 | 1 | 2740. | 0. | 0. 1040. | 0. | 0. 1040. | 1650. | 0. | 0. | 0. | .63 | 60. | 17.3 | B | 22.7 | 12.1 |
| * 4 | 1 | 600. | 0. | 0. 1040. | 0. | 0. 1040. | 1650. | 0. | 0. | 0. | .63 | 60. | 17.3 | B | 22.7 | 12.1 |
| * 5 | 1 | 700. | 0. | 0. 1040. | 0. | 0. 1040. | 1650. | 0. | 0. | 0. | .63 | 60. | 17.3 | B | 22.7 | 12.1 |
| * 6 | 1 | 2630. | 0. | 0. 1040. | 0. | 0. 1040. | 1650. | 0. | 0. | 0. | .63 | 60. | 17.3 | B | 22.7 | 12.1 |
| * 7 | 1 | 2530. | 0. | 0. 1040. | 0. | 0. 1040. | 1650. | 0. | 0. | 0. | .63 | 60. | 17.3 | B | 22.7 | 12.1 |
| * 8 | 1 | 1500. | 19. | 0. 1059. | 19. | 0. 1059. | 1650. | 0. | 0. | 0. | .64 | 60. | 17.6 | B | 22.7 | 12.1 |
| * 9 | 1 | 700. | 0. | 0. 1059. | 0. | 0. 1059. | 1650. | 0. | 0. | 0. | .64 | 60. | 17.6 | B | 22.7 | 12.1 |
| * 10 | 1 | 1500. | 0. | 295. 1059. | 0. | 292. 1059. | 1650. | 0. | 0. | 0. | .64 | 60. | 17.6 | B | 22.7 | 12.1 |
| * 11 | 1 | 750. | 0. | 0. 764. | 0. | 0. 764. | 1650. | 0. | 0. | 0. | .46 | 60. | 12.7 | B | 22.7 | 12.1 |
| * 12 | 1 | 350. | 147. | 0. 911. | 147. | 0. 911. | 1650. | 0. | 0. | 0. | .55 | 60. | 15.2 | B | 22.7 | 12.1 |
| * 13 | 1 | 350. | 0. | 0. 911. | 0. | 0. 911. | 1650. | 0. | 0. | 0. | .55 | 60. | 15.2 | B | 22.7 | 12.1 |
| * 14 | 1 | 350. | 0. | 45. 911. | 0. | 45. 911. | 1650. | 0. | 0. | 0. | .55 | 60. | 15.2 | B | 22.7 | 12.1 |
| * 15 | 1 | 700. | 0. | 0. 865. | 0. | 0. 865. | 1650. | 0. | 0. | 0. | .52 | 60. | 14.4 | B | 22.7 | 12.1 |
| * 16 | 1 | 900. | 20. | 0. 885. | 20. | 0. 885. | 1650. | 0. | 0. | 0. | .54 | 60. | 14.8 | B | 22.7 | 12.1 |
| * 17 | 1 | 1400. | 64. | 0. 950. | 64. | 0. 950. | 1650. | 0. | 0. | 0. | .58 | 60. | 15.8 | B | 22.7 | 12.1 |
| * 18 | 1 | 200. | 0. | 0. 950. | 0. | 0. 950. | 1650. | 0. | 0. | 0. | .58 | 60. | 15.8 | B | 22.7 | 12.1 |
| * 19 | 1 | 1400. | 0. | 45. 950. | 0. | 45. 950. | 1650. | 0. | 0. | 0. | .58 | 60. | 15.8 | B | 22.7 | 12.1 |
| * 20 | 1 | 900. | 0. | 0. 905. | 0. | 0. 905. | 1650. | 0. | 0. | 0. | .55 | 60. | 15.1 | B | 22.7 | 12.1 |
| * 21 | 1 | 100. | 33. | 0. 939. | 33. | 0. 939. | 1650. | 0. | 0. | 0. | .57 | 60. | 15.6 | B | 22.7 | 12.1 |
| * 22 | 1 | 100. | 0. | 12. 939. | 0. | 12. 939. | 1650. | 0. | 0. | 0. | .57 | 60. | 15.6 | B | 22.7 | 12.1 |
| * 23 | 1 | 600. | 0. | 0. 927. | 0. | 0. 927. | 1650. | 0. | 0. | 0. | .56 | 60. | 15.4 | B | 22.7 | 12.1 |
| * 24 | 1 | 1500. | 98. | 0. 1025. | 98. | 0. 1025. | 1650. | 0. | 0. | 0. | .62 | 60. | 17.1 | B | 22.7 | 12.1 |
| * 25 | 1 | 1500. | 0. | 0. 1025. | 0. | 0. 1025. | 1650. | 0. | 0. | 0. | .62 | 60. | 17.1 | B | 22.7 | 12.1 |
| * 26 | 1 | 8000. | 0. | 1025. 1025. | 0. | 1025. 1025. | 1650. | 0. | 0. | 0. | .62 | 60. | 17.1 | B | 22.7 | 12.1 |
| * 27 | | | | | | | | | | | | | | | | |
| * 28 | | | | | | | | | | | | | | | | |
| * 29 | | | | | | | | | | | | | | | | |
| * TOTAL | 131999. | = | 25.0 | MILES | | | | | MAX(V/C) = 0.64 | | LOWEST LOS = B | | AVG = 60. | 17.2 | 22.7 | 12.1 |

| | CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | |
|-----------------------------|--------------------|------------|--------|----------|-------------------|------------|--------|----------|
| FREEWAY TRAVEL TIME = | 430. | VEH-HRS | 859. | PASS-HRS | 430. | VEH-HRS | 859. | PASS-HRS |
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 2. | VEH-HRS | 4. | PASS-HRS | 2. | VEH-HRS | 4. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 432. | VEH-HRS | 863. | PASS-HRS | 432. | VEH-HRS | 863. | PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 25776. | VEH-MI. | 51553. | PASS-MI. | 25776. | VEH-MI. | 51553. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 60. | MPH. | | | 60. | MPH. | | |
| AVERAGE DENSITY = | 17. | VPMPPL | | | 17. | VPMPPL | | |
| TOTAL FUEL = | 1135. | GALLONS | | | 1135. | GALLONS | | |
| TOTAL EMISSIONS = | 313. | KI LOGRAMS | | | 313. | KI LOGRAMS | | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 25.25 | 3 | 0.69 | 4 | 0.15 | 5 | 0.18 |
| 6 | 0.66 | 7 | 0.64 | 8 | 0.39 | 9 | 0.18 | 10 | 0.39 |
| 11 | 0.14 | 12 | 0.08 | 13 | 0.08 | 14 | 0.08 | 15 | 0.15 |
| 16 | 0.19 | 17 | 0.32 | 18 | 0.05 | 19 | 0.32 | 20 | 0.20 |
| 21 | 0.02 | 22 | 0.02 | 23 | 0.14 | 24 | 0.37 | 25 | 0.37 |
| 26 | 1.99 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

| | | | | | | | | | | |
|---|--|--------|------|------|------|------|------|------|------|---|
| + | | * 6 * | 0.00 | 0.00 | 0.00 | 0.57 | 0.78 | 0.00 | 3.34 | * |
| + | | * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.04 | 0.00 | 2.60 | * |
| + | | * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.45 | * |
| + | | * 9 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.37 | * |
| + | | * 10 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.35 | * |
| + | | * 11 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 | * |
| | | * * | | | | | | | | * |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMI SS | | | |
|-----------|--------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|-------|----------|-----------|---------|--------|----------|---------|-------|---------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 1 | 4 | 1370. | 5200. | 1040. | 5200. | 5200. | 1040. | 5200. | 8000. | 0. | 0. | 0. | .65 | 65. | 20.0 | C | 19.2 | 14.0 |
| * 2 | 3 | 99999. | 0. | 0. | 4160. | 0. | 0. | 4160. | 6000. | 0. | 0. | 0. | .69 | 60. | 23.1 | C | 21.6 | 12.3 |
| * 3 | 3 | 2740. | 0. | 0. | 4160. | 0. | 0. | 4160. | 6000. | 0. | 0. | 0. | .69 | 60. | 23.1 | C | 21.6 | 12.3 |
| * 4 | 3 | 600. | 0. | 0. | 4160. | 0. | 0. | 4160. | 6000. | 0. | 0. | 0. | .69 | 60. | 23.1 | C | 21.6 | 12.3 |
| * 5 | 3 | 700. | 0. | 0. | 4160. | 0. | 0. | 4160. | 6000. | 0. | 0. | 0. | .69 | 60. | 23.1 | C | 21.6 | 12.3 |
| * 6 | 3 | 2630. | 0. | 0. | 4160. | 0. | 0. | 4160. | 6000. | 0. | 0. | 0. | .69 | 60. | 23.1 | C | 21.6 | 12.3 |
| * 7 | 3 | 2530. | 0. | 0. | 4160. | 0. | 0. | 4160. | 6000. | 0. | 0. | 0. | .69 | 60. | 23.1 | C | 21.6 | 12.3 |
| * 8 | 3 | 1500. | 132. | 0. | 4292. | 132. | 0. | 4292. | 5981. | 0. | 0. | 0. | .72 | 60. | 23.8 | C | 21.6 | 12.3 |
| * 9 | 3 | 700. | 0. | 0. | 4292. | 0. | 0. | 4292. | 6000. | 0. | 0. | 0. | .72 | 60. | 23.8 | C | 21.6 | 12.3 |
| * 10 | 3 | 1500. | 0. | 1225. | 4292. | 0. | 1208. | 4292. | 5705. | 0. | 0. | 0. | .75 | 60. | 23.8 | C | 21.6 | 12.3 |
| * 11 | 3 | 750. | 0. | 0. | 3067. | 0. | 0. | 3067. | 6000. | 0. | 0. | 0. | .51 | 60. | 17.0 | B | 21.6 | 12.3 |
| * 12 | 4 | 350. | 704. | 0. | 3771. | 704. | 0. | 3771. | 7853. | 0. | 0. | 0. | .48 | 60. | 15.7 | B | 21.6 | 12.3 |
| * 13 | 4 | 350. | 0. | 0. | 3771. | 0. | 0. | 3771. | 8000. | 0. | 0. | 0. | .47 | 60. | 15.7 | B | 21.6 | 12.3 |
| * 14 | 4 | 350. | 0. | 241. | 3771. | 0. | 241. | 3771. | 7955. | 0. | 0. | 0. | .47 | 60. | 15.7 | B | 21.6 | 12.3 |
| * 15 | 3 | 700. | 0. | 0. | 3531. | 0. | 0. | 3531. | 6000. | 0. | 0. | 0. | .59 | 60. | 19.6 | C | 21.6 | 12.3 |
| * 16 | 3 | 900. | 90. | 0. | 3621. | 90. | 0. | 3621. | 5980. | 0. | 0. | 0. | .61 | 60. | 20.1 | C | 21.6 | 12.3 |
| * 17 | 3 | 1400. | 286. | 0. | 3906. | 286. | 0. | 3906. | 5936. | 0. | 0. | 0. | .66 | 60. | 21.7 | C | 21.6 | 12.3 |
| * 18 | 3 | 200. | 0. | 0. | 3906. | 0. | 0. | 3906. | 6000. | 0. | 0. | 0. | .65 | 60. | 21.7 | C | 21.6 | 12.3 |
| * 19 | 3 | 1400. | 0. | 264. | 3906. | 0. | 264. | 3906. | 5955. | 0. | 0. | 0. | .66 | 60. | 21.7 | C | 21.6 | 12.3 |
| * 20 | 3 | 900. | 0. | 0. | 3642. | 0. | 0. | 3642. | 6000. | 0. | 0. | 0. | .61 | 60. | 20.2 | C | 21.6 | 12.3 |
| * 21 | 4 | 100. | 137. | 0. | 3778. | 137. | 0. | 3778. | 7967. | 0. | 0. | 0. | .47 | 60. | 15.7 | B | 21.6 | 12.3 |
| * 22 | 4 | 100. | 0. | 70. | 3778. | 0. | 70. | 3778. | 7988. | 0. | 0. | 0. | .47 | 60. | 15.7 | B | 21.6 | 12.3 |
| * 23 | 3 | 600. | 0. | 0. | 3708. | 0. | 0. | 3708. | 6000. | 0. | 0. | 0. | .62 | 60. | 20.6 | C | 21.6 | 12.3 |
| * 24 | 3 | 1500. | 392. | 0. | 4100. | 392. | 0. | 4100. | 5902. | 0. | 0. | 0. | .69 | 60. | 22.8 | C | 21.6 | 12.3 |
| * 25 | 3 | 1500. | 0. | 0. | 4100. | 0. | 0. | 4100. | 6000. | 0. | 0. | 0. | .68 | 60. | 22.8 | C | 21.6 | 12.3 |
| * 26 | 3 | 8000. | 0. | 0. | 4100. | 0. | 0. | 4100. | 6000. | 0. | 0. | 0. | .68 | 60. | 22.8 | C | 21.6 | 12.3 |
| * 27 | 4 | 100. | 1025. | 0. | 5125. | 1025. | 0. | 5125. | 8000. | 0. | 0. | 0. | .64 | 65. | 19.7 | C | 19.2 | 14.0 |
| * 28 | 4 | 1000. | 0. | 0. | 5125. | 0. | 0. | 5125. | 7750. | 0. | 0. | 0. | .66 | 65. | 19.7 | C | 19.2 | 14.0 |
| * 29 | 4 | 1000. | 0. | 5125. | 5125. | 0. | 5125. | 5125. | 7750. | 0. | 0. | 0. | .66 | 65. | 19.7 | C | 19.2 | 14.0 |

TOTAL 135469. = 25.7 MILES MAX(V/C) = 0.75 LOWEST LOS = C AVG = 60. 22.8 21.5 12.4

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|-----------------------------|--------------------|------------------|-------------------|------------------|
| FREEWAY TRAVEL TIME = | 1773. VEH-HRS | 1784. PASS-HRS | 1773. VEH-HRS | 1784. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 8. VEH-HRS | 8. PASS-HRS | 8. VEH-HRS | 8. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1781. VEH-HRS | 1792. PASS-HRS | 1781. VEH-HRS | 1792. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 106648. VEH-MI. | 107357. PASS-MI. | 106648. VEH-MI. | 107357. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 60. MPH. | | 60. MPH. | |
| AVERAGE DENSITY = | 23. VPMP | | 23. VPMP | |
| TOTAL FUEL = | 4954. GALLONS | | 4954. GALLONS | |
| TOTAL EMISSIONS = | 1321. KILOGRAMS | | 1321. KILOGRAMS | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

Table with 10 columns: SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY. Rows 1-29 showing delay values for various subsections.

***** TOTAL DELAY = 132.4 VEH-HRS ***** AVERAGE DELAY = 1.92 MIN/VEH *****

***** RAMP DELAYS *****

Table with 10 columns: OFF-RAMP, SUBSECTION, DELAY, GAS GALS, HC KGMS, CO KGMS, NOX KGMS, TOTAL EMISSIONS KGMS. Row 2 OUTPUT POINT showing 16.0 VEH-HRS delay and other metrics.

**
** FREEWAY TRAVEL TIME (MINUTES) **
**

Table with 9 columns: ORIGINS, DESTINATIONS ACROSS (1-7). Rows 1-11 showing travel times between origins and destinations.

*
* TIME SLICE FREEWAY PERFORMANCE TABLE *
*

Table with 17 columns: SUB SEC, NO. LNS, SSEC LENGTH, O-D DATA ORG, DEMANDS DES, ADJUSTED VOLUMES ORG, WEAVE EFF, CONGEST LENGTH, STORAGE RATE, V/C RATIO, SPEED MPH, DENSITY VP/MPH, LOS LEVEL, FUEL MPG, EMISSIONS GS/VM. Rows 1-7 showing performance metrics for different subsections.

| | | | | | | | | | | | | | | | | | | | | |
|---|----|---|-------|-------|-------|-------|-------|-------|-------|-------|----|----|----|-----|-----|------|---|------|------|---|
| * | 8 | 3 | 1500. | 165. | 0. | 4909. | 165. | 0. | 4909. | 5975. | 0. | 0. | 0. | .82 | 59. | 27.7 | D | 21.9 | 12.2 | * |
| * | 9 | 3 | 700. | 0. | 0. | 4909. | 0. | 0. | 4909. | 6000. | 0. | 0. | 0. | .82 | 59. | 27.7 | D | 21.9 | 12.2 | * |
| * | 10 | 3 | 1500. | 0. | 1371. | 4909. | 0. | 1209. | 4909. | 5671. | 0. | 0. | 0. | .87 | 58. | 28.2 | D | 22.2 | 11.9 | * |
| * | 11 | 3 | 750. | 0. | 0. | 3539. | 0. | 0. | 3539. | 6000. | 0. | 0. | 0. | .59 | 60. | 19.7 | C | 21.6 | 12.3 | * |
| * | 12 | 4 | 350. | 989. | 0. | 4528. | 989. | 0. | 4528. | 7788. | 0. | 0. | 0. | .58 | 60. | 18.9 | C | 21.6 | 12.3 | * |
| * | 13 | 4 | 350. | 0. | 0. | 4528. | 0. | 0. | 4528. | 8000. | 0. | 0. | 0. | .57 | 60. | 18.9 | C | 21.6 | 12.3 | * |
| * | 14 | 4 | 350. | 0. | 302. | 4528. | 0. | 302. | 4528. | 7946. | 0. | 0. | 0. | .57 | 60. | 18.9 | C | 21.6 | 12.3 | * |
| * | 15 | 3 | 700. | 0. | 0. | 4226. | 0. | 0. | 4226. | 6000. | 0. | 0. | 0. | .70 | 60. | 23.5 | C | 21.6 | 12.3 | * |
| * | 16 | 3 | 900. | 101. | 0. | 4328. | 101. | 0. | 4328. | 5976. | 0. | 0. | 0. | .72 | 60. | 24.0 | C | 21.6 | 12.3 | * |
| * | 17 | 3 | 1400. | 446. | 0. | 4774. | 446. | 0. | 4774. | 5896. | 0. | 0. | 0. | .81 | 60. | 26.5 | D | 21.6 | 12.3 | * |
| * | 18 | 3 | 200. | 0. | 0. | 4774. | 0. | 0. | 4774. | 6000. | 0. | 0. | 0. | .80 | 60. | 26.5 | D | 21.6 | 12.3 | * |
| * | 19 | 3 | 1400. | 0. | 199. | 4774. | 0. | 199. | 4774. | 5969. | 0. | 0. | 0. | .80 | 60. | 26.5 | D | 21.6 | 12.3 | * |
| * | 20 | 3 | 900. | 0. | 0. | 4575. | 0. | 0. | 4575. | 6000. | 0. | 0. | 0. | .76 | 60. | 25.4 | C | 21.6 | 12.3 | * |
| * | 21 | 4 | 100. | 185. | 0. | 4760. | 185. | 0. | 4760. | 7955. | 0. | 0. | 0. | .60 | 60. | 19.8 | C | 21.6 | 12.3 | * |
| * | 22 | 4 | 100. | 0. | 104. | 4760. | 0. | 104. | 4760. | 7984. | 0. | 0. | 0. | .60 | 60. | 19.8 | C | 21.6 | 12.3 | * |
| * | 23 | 3 | 600. | 0. | 0. | 4656. | 0. | 0. | 4656. | 6000. | 0. | 0. | 0. | .78 | 60. | 25.9 | C | 21.6 | 12.3 | * |
| * | 24 | 3 | 1500. | 432. | 0. | 5088. | 432. | 0. | 5088. | 5892. | 0. | 0. | 0. | .86 | 58. | 29.2 | D | 22.2 | 12.0 | * |
| * | 25 | 3 | 1500. | 0. | 0. | 5088. | 0. | 0. | 5088. | 6000. | 0. | 0. | 0. | .85 | 59. | 29.0 | D | 22.1 | 12.0 | * |
| * | 26 | 3 | 8000. | 0. | 0. | 5088. | 0. | 0. | 5088. | 6000. | 0. | 0. | 0. | .85 | 59. | 29.0 | D | 22.1 | 12.0 | * |
| * | 27 | 4 | 100. | 1272. | 0. | 6360. | 1272. | 0. | 6360. | 8000. | 0. | 0. | 0. | .80 | 63. | 25.1 | C | 20.0 | 13.4 | * |
| * | 28 | 4 | 1000. | 0. | 0. | 6360. | 0. | 0. | 6360. | 7750. | 0. | 0. | 0. | .82 | 63. | 25.4 | C | 20.3 | 13.2 | * |
| * | 29 | 4 | 1000. | 0. | 6360. | 6360. | 0. | 6360. | 6360. | 7750. | 0. | 0. | 0. | .82 | 63. | 25.4 | C | 20.3 | 13.2 | * |

* TOTAL 135469. = 25.7 MI LES MAX(V/C) = 0.87 LOWEST LOS = D AVG = 60. 26.4 21.6 12.3 *

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|----------------------------|--------------------|------------------|-------------------|------------------|
| FREEWAY TRAVEL TIME = | 2055. VEH-HRS | 2068. PASS-HRS | 3828. VEH-HRS | 3852. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 97. VEH-HRS | 97. PASS-HRS | 105. VEH-HRS | 105. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 2151. VEH-HRS | 2165. PASS-HRS | 3932. VEH-HRS | 3957. PASS-HRS |
| TOTAL FRWY TRAV DISTANCE = | 123125. VEH-MI. | 123973. PASS-MI. | 229773. VEH-MI. | 231330. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 57. MPH. | | 60. MPH. | |
| AVERAGE DENSITY = | 26. VPMP | | 25. VPMP | |
| TOTAL FUEL = | 5731. GALLONS | | 10685. GALLONS | |
| TOTAL EMISSIONS = | 1532. KILOGRAMS | | 2853. KILOGRAMS | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|--------|------------|-------|------------|-------|------------|-------|
| 1 | 0.25 | 2 | 115.19 | 3 | 3.16 | 4 | 0.69 | 5 | 0.81 |
| 6 | 3.03 | 7 | 2.91 | 8 | 2.14 | 9 | 0.99 | 10 | 2.57 |
| 11 | 0.64 | 12 | 0.38 | 13 | 0.38 | 14 | 0.38 | 15 | 0.72 |
| 16 | 0.95 | 17 | 1.62 | 18 | 0.23 | 19 | 1.62 | 20 | 1.00 |
| 21 | 0.12 | 22 | 0.12 | 23 | 0.68 | 24 | 2.64 | 25 | 2.46 |
| 26 | 13.11 | 27 | 0.05 | 28 | 0.73 | 29 | 0.73 | | |

***** TOTAL DELAY = 160.3 VEH-HRS ***** AVERAGE DELAY = 2.01 MIN/VEH *****

***** RAMP DELAYS *****

| OFF-RAMP | OUTPUT POINT | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|----------|--------------|--------------------------|------------------|-------------|------------|------------|-------------|----------------------------|
| | 2 | 177. | 96.74 | 34.54 | 2.14 | 11.21 | 0.59 | 13.94 |

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FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A.D.MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQQ QQQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP LLL
FFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 2222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 11111111 2222222222 PPP LLLLLLLLLL
    
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FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 2 AND 26 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
 LOWER LIMB (AT V/C=1) = 25
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

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**
** SUB NO. SSEC SSEC DESIGN ORG TRK SSEC PCT PCT DES SPECIAL FF.SPD. CAP. ART GRADE SUBSECTION LOCATION **
** SEC LNS CAP LENGTH SPEED DES FAC GRAD TRK TRUCKS RAMP ALT. RTE ALT. RTE TYPE ALT. RTE **
**
*****
**
** 1 **
**
** 2 1 1650. 99999. 60 0 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Queue Capture **
**
** 3 1 1650. 2740. 60 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 SR-85 Off to Shore On **
**
** 4 1 1650. 600. 60 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Shore. On to Moffett Off **
**
** 5 1 1650. 700. 60 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Moffett Off to On **
**
** 6 1 1650. 2630. 60 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Moffett On to Ellis Off **
**
** 7 1 1650. 2530. 60 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Ellis Off to On-ramp **
**
** 8 1 1650. 1500. 60 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Ellis On-ramp **
**
** 9 1 1650. 700. 60 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Ellis / US 237 **
**
** 10 1 1650. 1500. 60 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 SR-237 EB Off-Ramp **
**
** 11 1 1650. 750. 60 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 SR-237 / SR-237 **
    
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**
** 12  1  1650.    350.  60    0  0.96  0.0  0    100  YES    0.0    0.    GOOD  0.0  SR-237 EB On-Ramp
**
** 13  1  1650.    350.  60    0  0.96  0.0  0    100  YES    0.0    0.    GOOD  0.0  US 237 / Mathilda
**
** 14  1  1650.    350.  60    D  0.96  0.0  0    100  NO     0.0    0.    GOOD  0.0  Mathilda Off-Ramp
**
** 15  1  1650.    700.  60    0  0.96  0.0  0    100  NO     0.0    0.    GOOD  0.0  Mathilda / Mathilda
**
** 16  1  1650.    900.  60    0  0.96  0.0  0    100  YES    0.0    0.    GOOD  0.0  Mathilda SB On-Ramp
**
** 17  1  1650.   1400.  60    0  0.96  0.0  0    100  YES    0.0    0.    GOOD  0.0  Mathilda NB On-Ramp
**
** 18  1  1650.    200.  60    0  0.96  0.0  0    100  NO     0.0    0.    GOOD  0.0  Mathilda / Fair Oaks
**
** 19  1  1650.   1400.  60    D  0.96  0.0  0    100  NO     0.0    0.    GOOD  0.0  Fair Oaks SB Off-Ramp
**
** 20  1  1650.    900.  60    0  0.96  0.0  0    100  NO     0.0    0.    GOOD  0.0  Fair Oaks SB/ Fair Oaks
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1 INSTITUTE OF TRANSPORTATION STUDIES          FREQ12PL  REL 3.01              10/19/2015  13:55              PAGE  3
UNIVERSITY OF CALIFORNIA, BERKELEY  SHORT TERM SIMULATION OF PRIORITY LANE

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| SUB NO. | SEC | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC PCT GRAD | PCT TRK | PCT DES TRUCKS | SPECIAL RAMP | FF. SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION LOCATION |
|---------|-----|----------|-------------|--------------|---------|---------|---------------|---------|----------------|--------------|-------------------|---------------|----------|----------------|--------------------------|
| 21 | 1 | 1650. | 100. | 60 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Fair Oaks SB On-Ramp |
| 22 | 1 | 1650. | 100. | 60 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks NB Off-Ramp |
| 23 | 1 | 1650. | 600. | 60 | 0 | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks NB/ Fair Oaks |
| 24 | 1 | 1650. | 1500. | 60 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Oaks On-Ramp to Mid |
| 25 | 1 | 1650. | 1500. | 60 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Mid to Lawrence Off-ramp |
| 26 | 1 | 1650. | 8000. | 60 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| 27 | | | | | | | | | | | | | | | |
| 28 | | | | | | | | | | | | | | | |
| 29 | | | | | | | | | | | | | | | |

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1 INSTITUTE OF TRANSPORTATION STUDIES          FREQ12PL  REL 3.01              10/19/2015  13:55              PAGE  4
UNIVERSITY OF CALIFORNIA, BERKELEY  SHORT TERM SIMULATION OF NON-PRIORITY LANES

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| SUB NO. | SEC | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC PCT GRAD | PCT TRK | PCT DES TRUCKS | SPECIAL RAMP | FF. SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION LOCATION |
|---------|-----|----------|-------------|--------------|---------|---------|---------------|---------|----------------|--------------|-------------------|---------------|----------|----------------|-------------------------|
| 1 | 4 | 8000. | 1370. | 65 | 0D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Seeding |
| 2 | 3 | 6000. | 99999. | 60 | 0 | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture |
| 3 | 3 | 6000. | 2740. | 60 | 0 | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-85 Off to Shore On |
| 4 | 3 | 6000. | 600. | 60 | 0 | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Shore. On to Moffet Off |
| 5 | 3 | 6000. | 700. | 60 | 0 | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Moffett Off to On |


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FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ      1111      222222      PPPPPPPP      EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A.D.MAY*Q  111111     222 222     PPPPPPPP     EEEEEEEEE
FFF      RRR      RRR      EEE      QQQQ      QQQQ      1111     222 222     PPP      PPP     EEE
FFF      RRR      RRR      EEE      QQQQ      QQQQ      1111     222 222     PPP      PPP     EEE
FFFFFFFF RRRRRRRR EEEEEEEEE QQQQ      QQQQ      1111     222 222     PPPPPPPP     EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE QQQQ      QQQQ      1111     2222      PPPPPPPP     EEEEEEEEE
FFF      RRR      RRR      EEE      QQQQ      QQQ QQQQ     1111     2222      PPP      PPP     EEE
FFF      RRR      RRR      EEE      Q*UC*      QQQQ      1111     222      PPP      PPP     EEE
FFF      RRR      RRR      EEEEEEEEE Q*REGENTS*Q  1111     222      PPP      PPP     EEEEEEEEE
FFF      RRR      RRR      EEEEEEEEE Q*1999*Q QQQ  11111111  22222222222  PPP      PPP     EEEEEEEEE
    
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FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
 LOWER LIMB (AT V/C=1) = 25
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

***** INPUT HAS BEEN COMPLETED *****

MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 4 IN TIME SLICE 1
 --- THE MAXIMUM METERING RATE WILL PREVAIL.

MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 9 IN TIME SLICE 1
 --- THE MAXIMUM METERING RATE WILL PREVAIL.

MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 10 IN TIME SLICE 1
 --- THE MAXIMUM METERING RATE WILL PREVAIL.

MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 4 IN TIME SLICE 2
 --- THE MAXIMUM METERING RATE WILL PREVAIL.

MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 4 IN TIME SLICE 3
 --- THE MAXIMUM METERING RATE WILL PREVAIL.

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QUEUE COLLISION IN SECTION 28 T2 =0.044
QUEUE COLLISION IN SECTION 10 T2 =0.941
QUEUE COLLISION IN SECTION 8 T2 =0.923
    
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*****
**
**          FREEWAY TRAVEL TIME (MINUTES)
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*****
* ORIGINS DESTINATIONS ACROSS
* DOWN
* 1 2 3 4 5 6
*
*
* 1 * 0.26 24.74 25.72 28.47 29.46 45.04
* 2 * 0.00 1.18 2.16 4.91 5.90 21.48
* 3 * 0.00 0.00 0.66 3.42 4.40 19.98
* 4 * 0.00 0.00 0.00 2.31 3.29 18.87
* 5 * 0.00 0.00 0.00 1.81 2.79 18.37
* 6 * 0.00 0.00 0.00 0.00 0.24 15.82
* 7 * 0.00 0.00 0.00 0.00 0.00 15.05
* 8 * 0.00 0.00 0.00 0.00 0.00 1.30
* 9 * 0.00 0.00 0.00 0.00 0.00 1.14
* 10 * 0.00 0.00 0.00 0.00 0.00 0.22
*
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TIME SLICE FREEWAY PERFORMANCE TABLE

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*****
*
*
*
* SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMI SS
* SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VP/PL LEVEL MPG GS/VM
*
* 1 4 1370. 7229. 1446. 7229. 7229. 1446. 7229. 8000. 0. 0. 0. .90 59. 30.6 D 21.9 12.1
* 2 3 99999. 0. 0. 5783. 0. 0. 5783. 6000. 0. 0. 0. .96 54. 36.0 E 23.5 11.3
* 3 3 2740. 0. 0. 5783. 0. 0. 5783. 6000. 0. 0. 0. .96 54. 36.0 E 23.5 11.3
* 4 3 600. 0. 0. 5783. 0. 0. 5783. 6000. 0. 0. 0. .96 54. 36.0 E 23.5 11.3
* 5 3 700. 0. 0. 5783. 0. 0. 5783. 6000. 0. 0. 0. .96 54. 36.0 E 23.5 11.3
* 6 3 2630. 0. 0. 5783. 0. 0. 3357. 6000. 0. * 199. 2426. .56 54. 20.9 F 23.5 11.3
* 7 3 2530. 0. 0. 5783. 0. 0. 3357. 6000. 0. ** 2530. 2426. .56 42. 26.5 F 22.3 11.8
* 8 3 1500. 258. 0. 6041. 240. 0. 3597. 5958. 0. ** 1500. 2361. .60 36. 33.7 F 21.9 12.1
* 9 3 700. 0. 0. 6041. 0. 0. 3597. 6000. 0. ** 700. 2361. .60 32. 37.8 F 21.0 12.5
* 10 3 1500. 0. 1172. 6041. 0. 1110. 3597. 5722. 0. ** 1500. 2125. .63 38. 31.6 F 22.3 11.9
* 11 3 750. 0. 0. 4869. 0. 0. 2487. 6000. 0. ** 750. 2125. .41 27. 30.6 F 19.3 13.6
* 12 4 350. 440. 0. 5309. 440. 0. 2927. 7910. 0. ** 350. 2125. .37 20. 36.2 F 18.6 14.0
* 13 4 350. 0. 0. 5309. 0. 0. 2927. 8000. 0. ** 350. 2125. .37 18. 41.0 F 18.1 14.3
* 14 4 350. 0. 358. 5309. 0. 341. 2927. 7923. 0. ** 350. 2125. .37 16. 45.1 F 17.7 14.7
* 15 3 700. 0. 0. 4951. 0. 0. 2586. 6000. 0. ** 700. 2125. .43 18. 48.4 F 17.3 14.9
* 16 3 900. 826. 0. 5777. 720. 0. 3306. 5816. 0. ** 900. 2125. .57 21. 53.6 F 17.5 14.7
* 17 3 1400. 360. 0. 6137. 360. 0. 3666. 5920. 0. ** 1400. 2125. .62 20. 60.8 F 17.6 14.9
* 18 3 200. 0. 0. 6137. 0. 0. 3666. 6000. 0. ** 200. 2125. .61 19. 65.7 F 16.9 15.4
* 19 3 1400. 0. 471. 6137. 0. 444. 3666. 5921. 0. ** 1400. 2125. .62 18. 68.7 F 16.7 15.7
* 20 3 900. 0. 0. 5666. 0. 0. 3222. 6000. 0. ** 900. 2125. .54 14. 78.2 F 14.8 17.2
* 21 4 100. 217. 0. 5883. 217. 0. 3439. 7947. 0. ** 100. 2125. .43 10. 89.5 F 13.9 18.1
* 22 4 100. 0. 127. 5883. 0. 120. 3439. 7979. 0. ** 100. 2125. .43 9. 91.4 F 13.8 18.2
* 23 3 600. 0. 0. 5756. 0. 0. 3319. 6000. 0. ** 600. 2125. .55 13. 85.6 F 14.3 17.7
* 24 3 1500. 176. 0. 5932. 176. 0. 3495. 5956. 0. ** 1500. 2125. .59 13. 90.6 F 14.2 18.0
* 25 3 1500. 0. 0. 5932. 0. 0. 3495. 6000. 0. ** 1500. 2125. .58 11. 102.1 F 13.4 19.1
* 26 3 8000. 0. 0. 5932. 0. 0. 3495. 6000. 0. ** 8000. 2125. .58 8. 140.1 F 11.1 22.7
* 27 4 100. 1483. 0. 7415. 1483. 0. 4978. 8000. 0. ** 100. 2125. .62 7. 170.9 F 10.1 25.7
* 28 4 1000. 1560. 0. 8975. 1212. 0. 6190. 7750. 0. ** 1000. 1560. .80 12. 125.7 F 14.4 20.9
* 29 4 1000. 1560. 10535. 10535. 1560. 7750. 7750. 7750. 0. 0. 0. 1.00 52. 37.1 E 23.8 11.1
*
*
* TOTAL 135469. = 25.7 MI LSES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 37. 45.0 21.6 12.2
*
*****

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TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | |
|-----------|--------|------------|----------------|----------------|------------|--------|----------|-----------|-----------|----------|---------|-----------|-------|---------|-------------|------|------|
| * SEC | * LNS | * LENGTH | * ORG DES SSEC | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VP/PL | * LEVEL | * MPG | * GS/VM | | | |
| * 1 | 4 | 1370. | 6699. 1340. | 6699. | 6699. | 1340. | 6699. | 8000. | 0. | 0. | 0. | .84 | 62. | 27.0 | D | 20.6 | 13.0 |
| * 2 | 3 | 9999. | 0. 0. | 5359. | 0. | 0. | 5359. | 6000. | 0. | 0. | 0. | .89 | 57. | 31.3 | D | 22.5 | 11.8 |
| * 3 | 3 | 2740. | 0. 0. | 5359. | 0. | 0. | 5092. | 6000. | 0. | ** 1592. | 267. | .85 | 46. | 37.2 | F | 21.7 | 12.4 |
| * 4 | 3 | 600. | 0. 0. | 5359. | 0. | 0. | 5092. | 6000. | 0. | ** 600. | 267. | .85 | 28. | 60.6 | F | 19.6 | 14.4 |
| * 5 | 3 | 700. | 0. 0. | 5359. | 0. | 0. | 5092. | 6000. | 0. | ** 700. | 267. | .85 | 24. | 71.5 | F | 18.7 | 15.4 |
| * 6 | 3 | 2630. | 0. 0. | 5359. | 0. | 0. | 5092. | 6000. | 0. | ** 2630. | 267. | .85 | 17. | 99.8 | F | 16.8 | 17.8 |
| * 7 | 3 | 2530. | 0. 0. | 5359. | 0. | 0. | 5092. | 6000. | 0. | ** 2530. | 267. | .85 | 14. | 119.6 | F | 15.7 | 19.5 |
| * 8 | 3 | 1500. | 312. 0. | 5671. | 280. 0. | 0. | 5372. | 5952. | 0. | ** 1500. | 267. | .90 | 17. | 104.6 | F | 17.2 | 17.7 |
| * 9 | 3 | 700. | 0. 0. | 5671. | 0. 0. | 0. | 5372. | 6000. | 0. | ** 700. | 267. | .90 | 17. | 107.4 | F | 17.0 | 17.9 |
| * 10 | 3 | 1500. | 0. 1175. | 5671. | 0. 1167. | 0. | 5372. | 5725. | 0. | ** 1500. | 267. | .94 | 20. | 91.7 | F | 18.3 | 16.3 |
| * 11 | 3 | 750. | 0. 0. | 4496. | 0. 0. | 0. | 4205. | 6000. | 0. | ** 750. | 267. | .70 | 9. | 158.2 | F | 11.7 | 24.1 |
| * 12 | 4 | 350. | 545. 0. | 5041. | 545. 0. | 0. | 4750. | 7895. | 0. | ** 350. | 267. | .60 | 7. | 181.7 | F | 9.5 | 26.9 |
| * 13 | 4 | 350. | 0. 0. | 5041. | 0. 0. | 0. | 4750. | 8000. | 0. | ** 350. | 267. | .59 | 6. | 186.2 | F | 9.3 | 27.1 |
| * 14 | 4 | 350. | 0. 390. | 5041. | 0. 388. | 0. | 4750. | 7920. | 0. | ** 350. | 267. | .60 | 6. | 182.8 | F | 9.4 | 26.9 |
| * 15 | 3 | 700. | 0. 0. | 4651. | 0. 0. | 0. | 4362. | 6000. | 0. | ** 700. | 267. | .73 | 10. | 151.4 | F | 12.6 | 23.3 |
| * 16 | 3 | 900. | 875. 0. | 5526. | 720. 0. | 0. | 5082. | 5815. | 0. | ** 900. | 267. | .87 | 15. | 109.5 | F | 16.5 | 18.6 |
| * 17 | 3 | 1400. | 405. 0. | 5931. | 400. 0. | 0. | 5482. | 5915. | 0. | ** 1400. | 267. | .93 | 19. | 97.7 | F | 17.9 | 16.8 |
| * 18 | 3 | 200. | 0. 0. | 5931. | 0. 0. | 0. | 5482. | 6000. | 0. | ** 200. | 267. | .91 | 18. | 102.6 | F | 17.5 | 17.3 |
| * 19 | 3 | 1400. | 0. 623. | 5931. | 0. 599. | 0. | 5482. | 5903. | 0. | ** 1400. | 267. | .93 | 19. | 97.1 | F | 17.9 | 16.7 |
| * 20 | 3 | 900. | 0. 0. | 5308. | 0. 0. | 0. | 4883. | 6000. | 0. | ** 900. | 267. | .81 | 13. | 128.7 | F | 14.7 | 20.7 |
| * 21 | 4 | 100. | 234. 0. | 5542. | 234. 0. | 0. | 5117. | 7944. | 0. | ** 100. | 267. | .64 | 7. | 171.8 | F | 10.2 | 25.8 |
| * 22 | 4 | 100. | 0. 199. | 5542. | 0. 191. | 0. | 5117. | 7969. | 0. | ** 100. | 267. | .64 | 7. | 172.9 | F | 10.2 | 25.9 |
| * 23 | 3 | 600. | 0. 0. | 5343. | 0. 0. | 0. | 4926. | 6000. | 0. | ** 600. | 267. | .82 | 13. | 126.8 | F | 14.8 | 20.5 |
| * 24 | 3 | 1500. | 160. 0. | 5503. | 160. 0. | 0. | 5086. | 5960. | 0. | ** 1500. | 267. | .85 | 14. | 117.5 | F | 15.9 | 19.3 |
| * 25 | 3 | 1500. | 0. 0. | 5503. | 0. 0. | 0. | 5086. | 6000. | 0. | ** 1500. | 267. | .85 | 14. | 119.8 | F | 15.7 | 19.5 |
| * 26 | 3 | 8000. | 0. 0. | 5503. | 0. 0. | 0. | 5086. | 6000. | 0. | ** 8000. | 267. | .85 | 14. | 119.8 | F | 15.7 | 19.5 |
| * 27 | 4 | 100. | 1376. 0. | 6879. | 1376. 0. | 0. | 6462. | 8000. | 0. | ** 100. | 267. | .81 | 12. | 130.3 | F | 14.5 | 20.9 |
| * 28 | 4 | 1000. | 520. 0. | 7399. | 768. 0. | 0. | 7230. | 7750. | 0. | ** 1000. | 267. | .93 | 19. | 94.5 | F | 18.1 | 16.6 |
| * 29 | 4 | 1000. | 520. 7919. | 7919. | 520. 7750. | 7750. | 7750. | 7750. | 0. | 0. | 0. | 1.00 | 52. | 37.1 | E | 23.8 | 11.1 |

TOTAL 135469. = 25.7 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 35. 50.1 20.6 13.3

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 3937. VEH-HRS | 7791. VEH-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| ON-RAMP MRG/CAP DELAY = | 444. VEH-HRS | 680. VEH-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 4381. VEH-HRS | 8471. VEH-HRS |
| TOTAL TRAVEL DISTANCE = | 137305. VEH-MI. | 281040. VEH-MI. |
| AVERAGE SYSTEM SPEED = | 31. MPH. | 36. MPH. |
| AVERAGE DENSITY = | 50. VP/PL | 48. VP/PL |
| TOTAL FUEL = | 6835. GALLONS | 13581. GALLONS |
| TOTAL EMISSIONS = | 1896. KILOGRAMS | 3682. KILOGRAMS |

***** MAINTENANCE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|--------|------------|--------|------------|-------|------------|-------|------------|-------|
| 1 | 1.31 | 2 | 215.67 | 3 | 18.04 | 4 | 12.16 | 5 | 18.54 |
| 6 | 111.38 | 7 | 134.34 | 8 | 65.70 | 9 | 31.75 | 10 | 54.69 |
| 11 | 58.24 | 12 | 43.34 | 13 | 44.53 | 14 | 43.63 | 15 | 51.31 |
| 16 | 42.65 | 17 | 55.38 | 18 | 8.46 | 19 | 54.84 | 20 | 52.98 |
| 21 | 11.53 | 22 | 11.61 | 23 | 34.61 | 24 | 77.96 | 25 | 79.90 |
| 26 | 426.11 | 27 | 7.99 | 28 | 50.52 | 29 | 5.53 | | |

***** TOTAL DELAY = 1824.7 VEH-HRS ***** AVERAGE DELAY = 21.36 MIN/VEH *****

| | | | | | | | | | | | | | | | | | | | | | |
|---|----|---|--------|-------|-------|-------|-------|-------|-------|-------|----|----|-------|-------|-----|-------|-------|------|------|------|---|
| * | 1 | 4 | 1370. | 5510. | 1102. | 5510. | 5510. | 1102. | 5510. | 8000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 19.2 | 14.0 | * | |
| * | 2 | 3 | 99999. | 0. | 0. | 4408. | 0. | 0. | 4408. | 6000. | 0. | 0. | 0. | .73 | 60. | 24.5 | C | 21.6 | 12.3 | * | |
| * | 3 | 3 | 2740. | 0. | 0. | 4408. | 0. | 0. | 4408. | 6000. | 0. | 0. | 0. | .73 | 52. | 28.0 | D | 21.3 | 12.6 | * | |
| * | 4 | 3 | 600. | 0. | 0. | 4408. | 0. | 0. | 4408. | 6000. | 0. | 0. | 0. | .73 | 38. | 38.6 | E | 20.2 | 13.6 | * | |
| * | 5 | 3 | 700. | 0. | 0. | 4408. | 0. | 0. | 4408. | 6000. | 0. | 0. | 0. | .73 | 34. | 43.3 | E | 19.8 | 14.0 | * | |
| * | 6 | 3 | 2630. | 0. | 0. | 4408. | 0. | 0. | 4408. | 6000. | 0. | 0. | 0. | .73 | 27. | 55.1 | F | 18.8 | 15.1 | * | |
| * | 7 | 3 | 2530. | 0. | 0. | 4408. | 0. | 0. | 4408. | 6000. | 0. | 0. | 0. | .73 | 20. | 72.4 | F | 17.5 | 16.7 | * | |
| * | 8 | 3 | 1500. | 218. | 0. | 4626. | 240. | 0. | 4648. | 5968. | 0. | 0. | 0. | .78 | 20. | 77.3 | F | 17.8 | 16.6 | * | |
| * | 9 | 3 | 700. | 0. | 0. | 4626. | 0. | 0. | 4648. | 6000. | 0. | 0. | 0. | .77 | 19. | 83.7 | F | 17.4 | 17.2 | * | |
| * | 10 | 3 | 1500. | 0. | 1059. | 4626. | 0. | 1064. | 4648. | 5749. | 0. | 0. | 0. | .81 | 20. | 77.2 | F | 18.1 | 16.4 | * | |
| * | 11 | 3 | 750. | 0. | 0. | 3567. | 0. | 0. | 4244. | 6000. | 0. | 0. | -660. | .71 | 9. | 151.8 | F | 12.1 | 23.5 | * | |
| * | 12 | 4 | 350. | 454. | 0. | 4021. | 454. | 0. | 4698. | 7914. | 0. | ** | 350. | -660. | .59 | 6. | 184.2 | F | 9.3 | 27.1 | * |
| * | 13 | 4 | 350. | 0. | 0. | 4021. | 0. | 0. | 4698. | 8000. | 0. | ** | 350. | -660. | .59 | 6. | 187.9 | F | 9.3 | 27.2 | * |
| * | 14 | 4 | 350. | 0. | 352. | 4021. | 0. | 353. | 4698. | 7927. | 0. | ** | 350. | -660. | .59 | 6. | 184.8 | F | 9.3 | 27.1 | * |
| * | 15 | 3 | 700. | 0. | 0. | 3669. | 0. | 0. | 4345. | 6000. | 0. | ** | 700. | -660. | .72 | 10. | 152.1 | F | 12.5 | 23.4 | * |
| * | 16 | 3 | 900. | 704. | 0. | 4373. | 720. | 0. | 5065. | 5853. | 0. | ** | 900. | -660. | .87 | 15. | 112.4 | F | 16.3 | 18.8 | * |
| * | 17 | 3 | 1400. | 389. | 0. | 4762. | 394. | 0. | 5459. | 5919. | 0. | ** | 1400. | -660. | .92 | 18. | 99.0 | F | 17.7 | 17.0 | * |
| * | 18 | 3 | 200. | 0. | 0. | 4762. | 0. | 0. | 5459. | 6000. | 0. | ** | 200. | -660. | .91 | 18. | 103.6 | F | 17.4 | 17.4 | * |
| * | 19 | 3 | 1400. | 0. | 521. | 4762. | 0. | 524. | 5459. | 5921. | 0. | ** | 1400. | -660. | .92 | 18. | 99.1 | F | 17.7 | 17.0 | * |
| * | 20 | 3 | 900. | 0. | 0. | 4241. | 0. | 0. | 4935. | 6000. | 0. | ** | 900. | -660. | .82 | 13. | 126.4 | F | 14.9 | 20.4 | * |
| * | 21 | 4 | 100. | 186. | 0. | 4427. | 186. | 0. | 5121. | 7956. | 0. | ** | 100. | -660. | .64 | 7. | 172.2 | F | 10.2 | 25.8 | * |
| * | 22 | 4 | 100. | 0. | 174. | 4427. | 0. | 174. | 5121. | 7973. | 0. | ** | 100. | -660. | .64 | 7. | 172.9 | F | 10.2 | 25.9 | * |
| * | 23 | 3 | 600. | 0. | 0. | 4253. | 0. | 0. | 4947. | 6000. | 0. | ** | 600. | -660. | .82 | 13. | 125.9 | F | 14.9 | 20.3 | * |
| * | 24 | 3 | 1500. | 192. | 0. | 4445. | 192. | 0. | 5139. | 5952. | 0. | ** | 1500. | -660. | .86 | 15. | 114.8 | F | 16.2 | 18.9 | * |
| * | 25 | 3 | 1500. | 0. | 0. | 4445. | 0. | 0. | 5139. | 6000. | 0. | ** | 1500. | -660. | .86 | 15. | 117.5 | F | 16.0 | 19.2 | * |
| * | 26 | 3 | 8000. | 0. | 0. | 4445. | 0. | 0. | 5139. | 6000. | 0. | ** | 8000. | -660. | .86 | 15. | 117.5 | F | 16.0 | 19.2 | * |
| * | 27 | 4 | 100. | 1111. | 0. | 5556. | 1111. | 0. | 6250. | 8000. | 0. | ** | 100. | -660. | .78 | 11. | 137.2 | F | 13.9 | 21.7 | * |
| * | 28 | 4 | 1000. | 750. | 0. | 6306. | 750. | 0. | 7000. | 7750. | 0. | ** | 1000. | -660. | .90 | 17. | 102.0 | F | 17.2 | 17.6 | * |
| * | 29 | 4 | 1000. | 750. | 7056. | 7056. | 750. | 7750. | 7750. | 7750. | 0. | 0. | 0. | 1.00 | 52. | 37.1 | E | 23.8 | 11.1 | * | |

 * TOTAL 135469. = 25.7 MI LES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 35. 42.1 19.9 13.8 *
 *

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|----------------------------|--------------------|------------------|-------------------|------------------|
| FREEWAY TRAVEL TIME = | 3352. VEH-HRS | 3385. PASS-HRS | 11143. VEH-HRS | 11245. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 394. VEH-HRS | 414. PASS-HRS | 1075. VEH-HRS | 1174. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 3747. VEH-HRS | 3799. PASS-HRS | 12218. VEH-HRS | 12419. PASS-HRS |
| TOTAL TRAV DISTANCE = | 117844. VEH-MI. | 118783. PASS-MI. | 398885. VEH-MI. | 401825. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 31. MPH. | | 36. MPH. | |
| AVERAGE DENSITY = | 42. VPMP/L | | 46. VPMP/L | |
| TOTAL FUEL = | 6050. GALLONS | | 19630. GALLONS | |
| TOTAL EMISSIONS = | 1686. KILOGRAMS | | 5368. KILOGRAMS | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|--------|------------|--------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 107.03 | 3 | 8.46 | 4 | 5.59 | 5 | 8.51 |
| 6 | 51.06 | 7 | 77.58 | 8 | 50.22 | 9 | 26.49 | 10 | 51.06 |
| 11 | 55.04 | 12 | 44.06 | 13 | 45.03 | 14 | 44.20 | 15 | 51.64 |
| 16 | 44.18 | 17 | 56.45 | 18 | 8.59 | 19 | 56.54 | 20 | 51.69 |
| 21 | 11.55 | 22 | 11.61 | 23 | 34.27 | 24 | 75.37 | 25 | 77.70 |
| 26 | 414.37 | 27 | 8.57 | 28 | 56.88 | 29 | 5.53 | | |

***** TOTAL DELAY = 1539.3 VEH-HRS ***** AVERAGE DELAY = 18.77 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH | DELAY | AVERAGE | GAS | HC | CO | NOX | TOTAL |
|-----------|--------------|---------|----------------|-------|-------|------|-------|-----------|
| | VEHICLES | VEH-HRS | METERING DELAY | GALS | KGMS | KGMS | KGMS | EMISSIONS |
| | | | MINUTES | | | | | KGMS |
| ON-RAMP 2 | RAMP | 28. | 39.00 | 8.73 | 13.93 | 0.86 | 4.52 | 5.62 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 28. | 39.00 | 8.73 | 13.93 | 0.86 | 4.52 | 5.62 |
| ON-RAMP 4 | RAMP | 245. | 253.00 | 15.73 | 90.34 | 5.60 | 29.31 | 36.47 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 245. | 253.00 | 15.73 | 90.34 | 5.60 | 29.31 | 36.47 |

| | | | | | | | | | | |
|---------|---|---------|------|--------|------|-------|------|-------|------|-------|
| ON-RAMP | 5 | RAMP | 0. | 2.50 | 0.10 | 0.89 | 0.06 | 0.29 | 0.02 | 0.36 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 0. | 2.50 | 0.10 | 0.89 | 0.06 | 0.29 | 0.02 | 0.36 |
| ON-RAMP | 9 | RAMP | 100. | 100.00 | 8.57 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 100.00 | 8.57 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |

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FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A.D.MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQQ QQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP LLL
FFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 2222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQ QQQQ 1111 2222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 11111111 2222222222 PPP LLLLLLLLLL
    
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FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 2 AND 26 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
 LOWER LIMB (AT V/C=1) = 25
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

```

*****
**
**          FREEWAY TRAVEL TIME (MINUTES)
**
*****
    
```

```

*****
* ORIGINS          DESTINATIONS ACROSS
* DOWN
*      1      2      3      4      5      6      7
*
+
* *****
*
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 2 * 0.00 21.38 21.72 22.59 22.80 25.00 0.00
+
* 3 * 0.00 0.00 0.00 0.00 2.12 4.32 0.00
+
* 4 * 0.00 0.00 0.00 0.00 0.00 3.48 0.00
+
* 5 * 0.00 0.00 0.00 0.00 0.00 3.14 0.00
+
* 6 * 0.00 0.00 0.00 0.00 0.00 2.97 0.00
+
* 7 * 0.00 0.00 0.00 0.00 0.00 2.23 0.00
+
* 8 * 0.00 0.00 0.00 0.00 0.00 2.08 0.00
+
* 9 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 10 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
    
```


* 11 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
 * *

 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | |
|-----------|---------|------------|----------------|----------------|----------------|--------|---------|-----------|-----------|-----------------|---------|----------------|---------|-----------|-------------|------|------|
| * SEC | * LNS | * LENGTH | * ORG DES SSEC | * ORG DES SSEC | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VP/MP | * LEVEL | * MPG | * GS/VM | | |
| * 1 | | | | | | | | | | | | | | | | | |
| * 2 | 1 | 99999 | 1446. 0. 1446. | 1446. 0. 1446. | 1446. 0. 1446. | 1650. | 0. | 0. | 0. | .88 | 60. | 24.1 | C | 22.7 | 12.1 | | |
| * 3 | 1 | 2740. | 0. 0. 1446. | 0. 0. 1446. | 0. 0. 1446. | 1650. | 0. | 0. | 0. | .88 | 60. | 24.1 | C | 22.7 | 12.1 | | |
| * 4 | 1 | 600. | 0. 0. 1446. | 0. 0. 1446. | 0. 0. 1446. | 1650. | 0. | 0. | 0. | .88 | 60. | 24.1 | C | 22.7 | 12.1 | | |
| * 5 | 1 | 700. | 0. 0. 1446. | 0. 0. 1446. | 0. 0. 1446. | 1650. | 0. | 0. | 0. | .88 | 60. | 24.1 | C | 22.7 | 12.1 | | |
| * 6 | 1 | 2630. | 0. 0. 1446. | 0. 0. 1446. | 0. 0. 1446. | 1650. | 0. | 0. | 0. | .88 | 60. | 24.1 | C | 22.7 | 12.1 | | |
| * 7 | 1 | 2530. | 0. 0. 1446. | 0. 0. 1446. | 0. 0. 1446. | 1650. | 0. | 0. | 0. | .88 | 60. | 24.1 | C | 22.7 | 12.1 | | |
| * 8 | 1 | 1500. | 42. 0. 1488. | 42. 0. 1488. | 0. 0. 1488. | 1650. | 0. | 0. | 0. | .90 | 60. | 24.8 | C | 22.7 | 12.1 | | |
| * 9 | 1 | 700. | 0. 0. 1488. | 0. 0. 1488. | 0. 0. 1488. | 1650. | 0. | 0. | 0. | .90 | 60. | 24.8 | C | 22.7 | 12.1 | | |
| * 10 | 1 | 1500. | 0. 278. 1488. | 0. 278. 1488. | 0. 278. 1488. | 1650. | 0. | 0. | 0. | .90 | 60. | 24.8 | C | 22.7 | 12.1 | | |
| * 11 | 1 | 750. | 0. 0. 1209. | 0. 0. 1209. | 0. 0. 1209. | 1650. | 0. | 0. | 0. | .73 | 60. | 20.2 | C | 22.7 | 12.1 | | |
| * 12 | 1 | 350. | 90. 0. 1299. | 90. 0. 1299. | 0. 0. 1299. | 1650. | 0. | 0. | 0. | .79 | 60. | 21.7 | C | 22.7 | 12.1 | | |
| * 13 | 1 | 350. | 0. 0. 1299. | 0. 0. 1299. | 0. 0. 1299. | 1650. | 0. | 0. | 0. | .79 | 60. | 21.7 | C | 22.7 | 12.1 | | |
| * 14 | 1 | 350. | 0. 77. 1299. | 0. 77. 1299. | 0. 77. 1299. | 1650. | 0. | 0. | 0. | .79 | 60. | 21.7 | C | 22.7 | 12.1 | | |
| * 15 | 1 | 700. | 0. 0. 1223. | 0. 0. 1223. | 0. 0. 1223. | 1650. | 0. | 0. | 0. | .74 | 60. | 20.4 | C | 22.7 | 12.1 | | |
| * 16 | 1 | 900. | 184. 0. 1406. | 184. 0. 1406. | 0. 0. 1406. | 1650. | 0. | 0. | 0. | .85 | 60. | 23.4 | C | 22.7 | 12.1 | | |
| * 17 | 1 | 1400. | 80. 0. 1486. | 80. 0. 1486. | 0. 0. 1486. | 1650. | 0. | 0. | 0. | .90 | 60. | 24.8 | C | 22.7 | 12.1 | | |
| * 18 | 1 | 200. | 0. 0. 1486. | 0. 0. 1486. | 0. 0. 1486. | 1650. | 0. | 0. | 0. | .90 | 60. | 24.8 | C | 22.7 | 12.1 | | |
| * 19 | 1 | 1400. | 0. 79. 1486. | 0. 79. 1486. | 0. 79. 1486. | 1650. | 0. | 0. | 0. | .90 | 60. | 24.8 | C | 22.7 | 12.1 | | |
| * 20 | 1 | 900. | 0. 0. 1408. | 0. 0. 1408. | 0. 0. 1408. | 1650. | 0. | 0. | 0. | .85 | 60. | 23.5 | C | 22.7 | 12.1 | | |
| * 21 | 1 | 100. | 53. 0. 1460. | 53. 0. 1460. | 0. 0. 1460. | 1650. | 0. | 0. | 0. | .89 | 60. | 24.3 | C | 22.7 | 12.1 | | |
| * 22 | 1 | 100. | 0. 21. 1460. | 0. 21. 1460. | 0. 21. 1460. | 1650. | 0. | 0. | 0. | .89 | 60. | 24.3 | C | 22.7 | 12.1 | | |
| * 23 | 1 | 600. | 0. 0. 1439. | 0. 0. 1439. | 0. 0. 1439. | 1650. | 0. | 0. | 0. | .87 | 60. | 24.0 | C | 22.7 | 12.1 | | |
| * 24 | 1 | 1500. | 44. 0. 1483. | 44. 0. 1483. | 0. 0. 1483. | 1650. | 0. | 0. | 0. | .90 | 60. | 24.7 | C | 22.7 | 12.1 | | |
| * 25 | 1 | 1500. | 0. 0. 1483. | 0. 0. 1483. | 0. 0. 1483. | 1650. | 0. | 0. | 0. | .90 | 60. | 24.7 | C | 22.7 | 12.1 | | |
| * 26 | 1 | 8000. | 0. 1483. 1483. | 0. 1483. 1483. | 0. 1483. 1483. | 1650. | 0. | 0. | 0. | .90 | 60. | 24.7 | C | 22.7 | 12.1 | | |
| * 27 | | | | | | | | | | | | | | | | | |
| * 28 | | | | | | | | | | | | | | | | | |
| * 29 | | | | | | | | | | | | | | | | | |
| * TOTAL | 131999. | = | 25.0 MI LES | | | | | | | MAX(V/C) = 0.90 | | LOWEST LOS = C | | AVG = 60. | 24.1 | 22.7 | 12.1 |

| | CURRENT TIME SLICE | | | CUMULATIVE VALUES | | |
|-----------------------------|--------------------|-----------------|--|-------------------|-----------------|--|
| FREEWAY TRAVEL TIME = | 603. VEH-HRS | 1206. PASS-HRS | | 603. VEH-HRS | 1206. PASS-HRS | |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | | 0. VEH-HRS | 0. PASS-HRS | |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | | 0. VEH-HRS | 0. PASS-HRS | |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | | 0. VEH-HRS | 0. PASS-HRS | |
| TOTAL SYSTEM TRAVEL TIME = | 603. VEH-HRS | 1206. PASS-HRS | | 603. VEH-HRS | 1206. PASS-HRS | |
| TOTAL FRWAY TRAV DISTANCE = | 36169. VEH-MI. | 72338. PASS-MI. | | 36169. VEH-MI. | 72338. PASS-MI. | |
| AVERAGE SYSTEM SPEED = | 60. MPH. | | | 60. MPH. | | |
| AVERAGE DENSITY = | 24. VP/MP | | | 24. VP/MP | | |
| TOTAL FUEL = | 1591. GALLONS | | | 1591. GALLONS | | |
| TOTAL EMISSIONS = | 438. KI LOGRAMS | | | 438. KI LOGRAMS | | |

***** MAINLINE DELAY (VEH-HRS) ***** DESI RED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 35.11 | 3 | 0.96 | 4 | 0.21 | 5 | 0.25 |
| 6 | 0.92 | 7 | 0.89 | 8 | 0.54 | 9 | 0.25 | 10 | 0.54 |
| 11 | 0.22 | 12 | 0.11 | 13 | 0.11 | 14 | 0.11 | 15 | 0.21 |
| 16 | 0.31 | 17 | 0.51 | 18 | 0.07 | 19 | 0.51 | 20 | 0.31 |
| 21 | 0.04 | 22 | 0.04 | 23 | 0.21 | 24 | 0.54 | 25 | 0.54 |
| 26 | 2.88 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 46.4 VEH-HRS ***** AVERAGE DELAY = 1.92 MIN/VEH *****

**
** FREEWAY TRAVEL TIME (MINUTES) **
**

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | * |
|-----------|---|-----------------------|-------|-------|-------|-------|-------|------|---|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | * |
| * | * | | | | | | | | * |
| * | * | | | | | | | | * |
| + * 1 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | * |
| + * 2 * | | 0.00 | 21.38 | 21.72 | 22.59 | 22.80 | 25.00 | 0.00 | * |
| + * 3 * | | 0.00 | 0.00 | 0.00 | 0.00 | 2.12 | 4.32 | 0.00 | * |
| + * 4 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.48 | 0.00 | * |
| + * 5 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.14 | 0.00 | * |
| + * 6 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.97 | 0.00 | * |
| + * 7 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.23 | 0.00 | * |
| + * 8 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.08 | 0.00 | * |
| + * 9 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | * |
| + * 10 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | * |
| + * 11 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | * |
| + * * | | | | | | | | | * |
| + * | | | | | | | | | * |

*
* TIME SLICE FREEWAY PERFORMANCE TABLE *
*

| * SUB NO. | * SEC LNS | * SSEC LENGTH | * O-D DATA ORG | * DEMANDS DES SSEC | * ADJUSTED VOLUMES ORG | * SSEC CAP. | * WEAVE EFF | * CONGEST LENGTH | * STORAGE RATE | * V/C RATIO | * SPEED MPH | * DENSITY VP/MP | * LOS LEVEL | * FUEL MPG | * EMISSIONS GS/VM | | | |
|-----------|-----------|---------------|----------------|--------------------|------------------------|-------------|-------------|------------------|----------------|-------------|-------------|-----------------|-------------|------------|-------------------|---|------|------|
| * 1 | | | | | | | | | | | | | | | | | | |
| * 2 | 1 | 99999 | 1340 | 0 | 1340 | 1340 | 0 | 1340 | 1650 | 0 | 0 | 0 | .81 | 60 | 22.3 | C | 22.7 | 12.1 |
| * 3 | 1 | 2740 | 0 | 0 | 1340 | 0 | 0 | 1340 | 1650 | 0 | 0 | 0 | .81 | 60 | 22.3 | C | 22.7 | 12.1 |
| * 4 | 1 | 600 | 0 | 0 | 1340 | 0 | 0 | 1340 | 1650 | 0 | 0 | 0 | .81 | 60 | 22.3 | C | 22.7 | 12.1 |
| * 5 | 1 | 700 | 0 | 0 | 1340 | 0 | 0 | 1340 | 1650 | 0 | 0 | 0 | .81 | 60 | 22.3 | C | 22.7 | 12.1 |
| * 6 | 1 | 2630 | 0 | 0 | 1340 | 0 | 0 | 1340 | 1650 | 0 | 0 | 0 | .81 | 60 | 22.3 | C | 22.7 | 12.1 |
| * 7 | 1 | 2530 | 0 | 0 | 1340 | 0 | 0 | 1340 | 1650 | 0 | 0 | 0 | .81 | 60 | 22.3 | C | 22.7 | 12.1 |
| * 8 | 1 | 1500 | 48 | 0 | 1388 | 48 | 0 | 1388 | 1650 | 0 | 0 | 0 | .84 | 60 | 23.1 | C | 22.7 | 12.1 |
| * 9 | 1 | 700 | 0 | 0 | 1388 | 0 | 0 | 1388 | 1650 | 0 | 0 | 0 | .84 | 60 | 23.1 | C | 22.7 | 12.1 |
| * 10 | 1 | 1500 | 0 | 275 | 1388 | 0 | 275 | 1388 | 1650 | 0 | 0 | 0 | .84 | 60 | 23.1 | C | 22.7 | 12.1 |
| * 11 | 1 | 750 | 0 | 0 | 1113 | 0 | 0 | 1113 | 1650 | 0 | 0 | 0 | .67 | 60 | 18.5 | C | 22.7 | 12.1 |
| * 12 | 1 | 350 | 105 | 0 | 1217 | 105 | 0 | 1217 | 1650 | 0 | 0 | 0 | .74 | 60 | 20.3 | C | 22.7 | 12.1 |
| * 13 | 1 | 350 | 0 | 0 | 1217 | 0 | 0 | 1217 | 1650 | 0 | 0 | 0 | .74 | 60 | 20.3 | C | 22.7 | 12.1 |
| * 14 | 1 | 350 | 0 | 80 | 1217 | 0 | 80 | 1217 | 1650 | 0 | 0 | 0 | .74 | 60 | 20.3 | C | 22.7 | 12.1 |
| * 15 | 1 | 700 | 0 | 0 | 1137 | 0 | 0 | 1137 | 1650 | 0 | 0 | 0 | .69 | 60 | 19.0 | C | 22.7 | 12.1 |
| * 16 | 1 | 900 | 185 | 0 | 1322 | 185 | 0 | 1322 | 1650 | 0 | 0 | 0 | .80 | 60 | 22.0 | C | 22.7 | 12.1 |
| * 17 | 1 | 1400 | 85 | 0 | 1408 | 85 | 0 | 1408 | 1650 | 0 | 0 | 0 | .85 | 60 | 23.5 | C | 22.7 | 12.1 |
| * 18 | 1 | 200 | 0 | 0 | 1408 | 0 | 0 | 1408 | 1650 | 0 | 0 | 0 | .85 | 60 | 23.5 | C | 22.7 | 12.1 |
| * 19 | 1 | 1400 | 0 | 97 | 1408 | 0 | 97 | 1408 | 1650 | 0 | 0 | 0 | .85 | 60 | 23.5 | C | 22.7 | 12.1 |
| * 20 | 1 | 900 | 0 | 0 | 1311 | 0 | 0 | 1311 | 1650 | 0 | 0 | 0 | .79 | 60 | 21.9 | C | 22.7 | 12.1 |
| * 21 | 1 | 100 | 56 | 0 | 1367 | 56 | 0 | 1367 | 1650 | 0 | 0 | 0 | .83 | 60 | 22.8 | C | 22.7 | 12.1 |
| * 22 | 1 | 100 | 0 | 31 | 1367 | 0 | 31 | 1367 | 1650 | 0 | 0 | 0 | .83 | 60 | 22.8 | C | 22.7 | 12.1 |
| * 23 | 1 | 600 | 0 | 0 | 1336 | 0 | 0 | 1336 | 1650 | 0 | 0 | 0 | .81 | 60 | 22.3 | C | 22.7 | 12.1 |
| * 24 | 1 | 1500 | 40 | 0 | 1376 | 40 | 0 | 1376 | 1650 | 0 | 0 | 0 | .83 | 60 | 22.9 | C | 22.7 | 12.1 |
| * 25 | 1 | 1500 | 0 | 0 | 1376 | 0 | 0 | 1376 | 1650 | 0 | 0 | 0 | .83 | 60 | 22.9 | C | 22.7 | 12.1 |

```

* 26 1 8000. 0. 1376. 1376. 0. 1376. 1376. 1650. 0. 0. 0. .83 60. 22.9 C 22.7 12.1 *
* 27 *
* 28 *
* 29 *
*
*****
* TOTAL 131999. = 25.0 MILES MAX(V/C) = 0.85 LOWEST LOS = C AVG = 60. 22.4 22.7 12.1 *
*
*****

```

```

CURRENT TIME SLICE CUMULATIVE VALUES
FREEWAY TRAVEL TIME = 559. VEH-HRS 1119. PASS-HRS 1162. VEH-HRS 2324. PASS-HRS
FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 559. VEH-HRS 1119. PASS-HRS 1162. VEH-HRS 2324. PASS-HRS
TOTAL FRWAY TRAV DISTANCE = 33555. VEH-MI. 67111. PASS-MI. 69724. VEH-MI. 139448. PASS-MI.
AVERAGE SYSTEM SPEED = 60. MPH. 60. MPH.
AVERAGE DENSITY = 22. VPML 23. VPML
TOTAL FUEL = 1476. GALLONS 3068. GALLONS
TOTAL EMISSIONS = 407. KILOGRAMS 845. KILOGRAMS

```

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 32.54 | 3 | 0.89 | 4 | 0.20 | 5 | 0.23 |
| 6 | 0.86 | 7 | 0.82 | 8 | 0.51 | 9 | 0.24 | 10 | 0.51 |
| 11 | 0.20 | 12 | 0.10 | 13 | 0.10 | 14 | 0.10 | 15 | 0.19 |
| 16 | 0.29 | 17 | 0.48 | 18 | 0.07 | 19 | 0.48 | 20 | 0.29 |
| 21 | 0.03 | 22 | 0.03 | 23 | 0.19 | 24 | 0.50 | 25 | 0.50 |
| 26 | 2.67 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 43.0 VEH-HRS ***** AVERAGE DELAY = 1.92 MIN/VEH *****

**
** FREEWAY TRAVEL TIME (MINUTES) **
**

```

*****
* ORIGINS DESTINATIONS ACROSS *
* DOWN 1 2 3 4 5 6 7 *
+
* * *****
* *
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 2 * 0.00 21.38 21.72 22.59 22.80 25.00 0.00
+
* 3 * 0.00 0.00 0.00 0.00 2.12 4.32 0.00
+
* 4 * 0.00 0.00 0.00 0.00 0.00 3.48 0.00
+
* 5 * 0.00 0.00 0.00 0.00 0.00 3.14 0.00
+
* 6 * 0.00 0.00 0.00 0.00 0.00 2.97 0.00
+
* 7 * 0.00 0.00 0.00 0.00 0.00 2.23 0.00
+
* 8 * 0.00 0.00 0.00 0.00 0.00 2.08 0.00
+
* 9 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 10 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 11 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
*
* *
*****

```

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS | |
|---------|---------|----------|---------|------------------|-------|-------------|---------|---------|-------|-----------------|----------------|-----------|------|--------|------|
| SEC LNS | LENGTH | ORG DES | SSEC | ORG DES SSEC | CAP. | EFF | LENGTH | RATE | RATIO | MPH | VP/MP | LEVEL | MPG | GS/VM | |
| 1 | | | | | | | | | | | | | | | |
| 2 | 1 | 99999. | 1102. | 0. 1102. | 1102. | 0. 1102. | 1650. | 0. | 0. | .67 | 60. | 18.4 | C | 22.7 | 12.1 |
| 3 | 1 | 2740. | 0. | 0. 1102. | 0. | 0. 1102. | 1650. | 0. | 0. | .67 | 60. | 18.4 | C | 22.7 | 12.1 |
| 4 | 1 | 600. | 0. | 0. 1102. | 0. | 0. 1102. | 1650. | 0. | 0. | .67 | 60. | 18.4 | C | 22.7 | 12.1 |
| 5 | 1 | 700. | 0. | 0. 1102. | 0. | 0. 1102. | 1650. | 0. | 0. | .67 | 60. | 18.4 | C | 22.7 | 12.1 |
| 6 | 1 | 2630. | 0. | 0. 1102. | 0. | 0. 1102. | 1650. | 0. | 0. | .67 | 60. | 18.4 | C | 22.7 | 12.1 |
| 7 | 1 | 2530. | 0. | 0. 1102. | 0. | 0. 1102. | 1650. | 0. | 0. | .67 | 60. | 18.4 | C | 22.7 | 12.1 |
| 8 | 1 | 1500. | 32. | 0. 1134. | 32. | 0. 1134. | 1650. | 0. | 0. | .69 | 60. | 18.9 | C | 22.7 | 12.1 |
| 9 | 1 | 700. | 0. | 0. 1134. | 0. | 0. 1134. | 1650. | 0. | 0. | .69 | 60. | 18.9 | C | 22.7 | 12.1 |
| 10 | 1 | 1500. | 0. | 251. 1134. | 0. | 251. 1134. | 1650. | 0. | 0. | .69 | 60. | 18.9 | C | 22.7 | 12.1 |
| 11 | 1 | 750. | 0. | 0. 883. | 0. | 0. 883. | 1650. | 0. | 0. | .54 | 60. | 14.7 | B | 22.7 | 12.1 |
| 12 | 1 | 350. | 86. | 0. 969. | 86. | 0. 969. | 1650. | 0. | 0. | .59 | 60. | 16.1 | B | 22.7 | 12.1 |
| 13 | 1 | 350. | 0. | 0. 969. | 0. | 0. 969. | 1650. | 0. | 0. | .59 | 60. | 16.1 | B | 22.7 | 12.1 |
| 14 | 1 | 350. | 0. | 73. 969. | 0. | 73. 969. | 1650. | 0. | 0. | .59 | 60. | 16.1 | B | 22.7 | 12.1 |
| 15 | 1 | 700. | 0. | 0. 896. | 0. | 0. 896. | 1650. | 0. | 0. | .54 | 60. | 14.9 | B | 22.7 | 12.1 |
| 16 | 1 | 900. | 147. | 0. 1043. | 147. | 0. 1043. | 1650. | 0. | 0. | .63 | 60. | 17.4 | B | 22.7 | 12.1 |
| 17 | 1 | 1400. | 81. | 0. 1125. | 81. | 0. 1125. | 1650. | 0. | 0. | .68 | 60. | 18.7 | C | 22.7 | 12.1 |
| 18 | 1 | 200. | 0. | 0. 1125. | 0. | 0. 1125. | 1650. | 0. | 0. | .68 | 60. | 18.7 | C | 22.7 | 12.1 |
| 19 | 1 | 1400. | 0. | 79. 1125. | 0. | 79. 1125. | 1650. | 0. | 0. | .68 | 60. | 18.7 | C | 22.7 | 12.1 |
| 20 | 1 | 900. | 0. | 0. 1045. | 0. | 0. 1045. | 1650. | 0. | 0. | .63 | 60. | 17.4 | B | 22.7 | 12.1 |
| 21 | 1 | 100. | 44. | 0. 1090. | 44. | 0. 1090. | 1650. | 0. | 0. | .66 | 60. | 18.2 | C | 22.7 | 12.1 |
| 22 | 1 | 100. | 0. | 27. 1090. | 0. | 27. 1090. | 1650. | 0. | 0. | .66 | 60. | 18.2 | C | 22.7 | 12.1 |
| 23 | 1 | 600. | 0. | 0. 1063. | 0. | 0. 1063. | 1650. | 0. | 0. | .64 | 60. | 17.7 | B | 22.7 | 12.1 |
| 24 | 1 | 1500. | 48. | 0. 1111. | 48. | 0. 1111. | 1650. | 0. | 0. | .67 | 60. | 18.5 | C | 22.7 | 12.1 |
| 25 | 1 | 1500. | 0. | 0. 1111. | 0. | 0. 1111. | 1650. | 0. | 0. | .67 | 60. | 18.5 | C | 22.7 | 12.1 |
| 26 | 1 | 8000. | 0. | 1111. 1111. | 0. | 1111. 1111. | 1650. | 0. | 0. | .67 | 60. | 18.5 | C | 22.7 | 12.1 |
| 27 | | | | | | | | | | | | | | | |
| 28 | | | | | | | | | | | | | | | |
| 29 | | | | | | | | | | | | | | | |
| TOTAL | 131999. | = | 25.0 | MILES | | | | | | MAX(V/C) = 0.69 | LOWEST LOS = C | AVG = 60. | 18.3 | 22.7 | 12.1 |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 458. VEH-HRS | 916. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 458. VEH-HRS | 916. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 27495. VEH-MI. | 54990. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 60. MPH. | 60. MPH. |
| AVERAGE DENSITY = | 18. VP/MP | 22. VP/MP |
| TOTAL FUEL = | 1210. GALLONS | 4278. GALLONS |
| TOTAL EMISSIONS = | 333. KILOGRAMS | 1178. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 26.76 | 3 | 0.73 | 4 | 0.16 | 5 | 0.19 |
| 6 | 0.70 | 7 | 0.68 | 8 | 0.41 | 9 | 0.19 | 10 | 0.41 |
| 11 | 0.16 | 12 | 0.08 | 13 | 0.08 | 14 | 0.08 | 15 | 0.15 |
| 16 | 0.23 | 17 | 0.38 | 18 | 0.05 | 19 | 0.38 | 20 | 0.23 |
| 21 | 0.03 | 22 | 0.03 | 23 | 0.15 | 24 | 0.40 | 25 | 0.40 |
| 26 | 2.16 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 35.2 VEH-HRS ***** AVERAGE DELAY = 1.92 MIN/VEH *****

SR 237 Westbound

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FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ      1111      222222      PPPPPPPP      EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A.D.MAY*Q 111111    222 222    PPPPPPPP    EEEEEEEEE
FFF      RRR  RRR  EEE      QQQQ      QQQQ      1111    222 222    PPP  PPP    EEE
FFF      RRR  RRR  EEE      QQQQ      QQQQ      1111    222 222    PPP  PPP    EEE
FFFFFFF  RRRRRRRR EEEEEEE  QQQQ      QQQQ      1111    222 222    PPPPPPPP    EEEEEEE
FFFFFFF  RRRRRRRR EEEEEEE  QQQQ      QQQQ      1111    2222    PPPPPPPP    EEEEEEE
FFF      RRR  RRR  EEE      QQQQ      QQQ QQQQ    1111    2222    PPP      EEE
FFF      RRR  RRR  EEE      Q*UC*      QQQQ      1111    222      PPP      EEE
FFF      RRR  RRR  EEEEEEEEE Q*REGENTS*Q 1111    222      PPP      EEEEEEEEE
FFF      RRR  RRR  EEEEEEEEE Q*1999*Q QQQ 1111111 2222222222 PPP      EEEEEEEEE
    
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FREQ12PE

1. THIS IS A SIMULATION ONLY EXECUTION.
2. THERE ARE 2.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
 LOWER LIMB (AT V/C=1) = 30
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.

FREEWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC | SSEC | DESIGN | ORG | TRK | SSEC | PCT | PCT | DES | SPECIAL | FF. SPD. | CAP. | ART | GRADE | SUBSECTION | LOCATION |
|---------|------|-------|--------|-----|-----|------|-----|--------|------|----------|----------|------|----------|-------|--------------------------|----------|
| SEC | LNS | CAP | LENGTH | DES | FAC | GRAD | TRK | TRUCKS | RAMP | ALT. RTE | ALT. RTE | TYPE | ALT. RTE | | | |
| 1 | 3 | 6000. | 1400. | 65 | 0 | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | DKS begin of network | |
| 2 | 3 | 6000. | 1500. | 65 | 0 | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence On-ramp | |
| 3 | 3 | 6000. | 1400. | 65 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence to Crossman | |
| 4 | 3 | 6000. | 1500. | 65 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Crossman On-Ramp | |
| 5 | 3 | 6000. | 1300. | 65 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Crossman / Mathilda | |
| 6 | 3 | 5020. | 500. | 65 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-Ramp | |
| 7 | 2 | 4000. | 2300. | 65 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | |
| 8 | 3 | 4230. | 700. | 65 | OD | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda / US 101 | |
| 9 | 2 | 4000. | 50. | 65 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bottleneck by-pass | |
| 10 | 2 | 2470. | 50. | 65 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bottleck | |
| 11 | 2 | 4000. | 1000. | 65 | OD | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US 101 / US 101 | |
| 12 | 2 | 4000. | 10. | 65 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Dummy end of travel time | |
| 13 | 2 | 4000. | 1500. | 65 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US 101 NB On-Ramp | |
| 14 | 2 | 4000. | 1500. | 65 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Maude Off-ramp | |
| 15 | 2 | 4000. | 100. | 65 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End of Network | |

***** INPUT HAS BEEN COMPLETED *****

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FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ      1111      222222      PPPPPPPP      EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A.D.MAY*Q  111111    222 222    PPPPPPPP      EEEEEEEEE
FFF      RRR  RRR  EEE      QQQQ      QQQQ      1111    222 222    PPP  PPP      EEE
FFF      RRR  RRR  EEE      QQQQ      QQQQ      1111    222 222    PPP  PPP      EEE
FFFFFFF  RRRRRRRR EEEEEEE  QQQQ      QQQQ      1111      222    PPPPPPPP      EEEEEEE
FFFFFFF  RRRRRRRR EEEEEEE  QQQQ      QQQQ      1111      222    PPPPPPPP      EEEEEEE
FFF      RRR  RRR  EEE      QQQQ      QQQ QQQQ    1111    2222    PPP      EEE
FFF      RRR  RRR  EEE      Q*UC*      QQQQ      1111    222    PPP      EEE
FFF      RRR  RRR  EEEEEEEEE Q*REGENTS*Q  1111    222    PPP      EEEEEEEEE
FFF      RRR  RRR  EEEEEEEEE Q*1999*Q QQQ  1111111  2222222222  PPP      EEEEEEEEE
    
```

FREQ12PE

1. THIS IS A SIMULATION ONLY EXECUTION.
2. THERE ARE 2.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
 LOWER LIMB (AT V/C=1) = 30
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.

***** INPUT HAS BEEN COMPLETED *****

```

*****
**                                     **
**          FREEWAY TRAVEL TIME (MINUTES)          **
**                                     **
*****
    
```

```

*****
* ORIGINS          DESTINATIONS ACROSS          *
* DOWN            *                             *
*                * 1 2 3 4 5 6                *
+                *                             *
*                *                             *
+                *                             *
* 1 * 1.36 2.06 2.13 2.31 2.86 2.88            *
+                *                             *
* 2 * 1.11 1.81 1.88 2.07 2.61 2.63            *
+                *                             *
* 3 * 0.60 1.30 1.37 1.55 2.10 2.12            *
+                *                             *
* 4 * 0.00 0.24 0.30 0.49 1.04 1.06            *
+                *                             *
* 5 * 0.00 0.00 0.00 0.17 0.72 0.74            *
+                *                             *
* 6 * 0.00 0.00 0.00 0.00 0.55 0.57            *
+                *                             *
*                *                             *
*****
    
```

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|-----------|----------|------------|-----------|--------------------|--------|---------|----------------|-----------|---------|---------|-----------|---------|--------|-------------|
| * SEC LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| 1 | 3 | 1400. | 4420. | 0. 4420. | 4420. | 0. | 0. | 0. | .74 | 64. | 22.9 | C | 19.2 | 13.9 |
| 2 | 3 | 1500. | 20. | 0. 4440. | 20. | 0. | 0. | 0. | .74 | 64. | 23.0 | C | 19.3 | 13.8 |
| 3 | 3 | 1400. | 0. | 0. 4440. | 0. | 0. | 0. | 0. | .74 | 64. | 23.0 | C | 19.3 | 13.8 |
| 4 | 3 | 1500. | 231. | 0. 4671. | 231. | 0. | 0. | 0. | .78 | 64. | 24.5 | C | 19.6 | 13.6 |
| 5 | 3 | 1300. | 0. | 0. 4671. | 0. | 0. | 0. | 0. | .78 | 64. | 24.5 | C | 19.6 | 13.6 |
| 6 | 3 | 500. | 0. | 890. 4671. | 0. | 890. | 4671. | 5020. | .93 | 57. | 27.1 | D | 22.1 | 11.9 |
| 7 | 2 | 2300. | 0. | 0. 3781. | 0. | 0. | 3741. | 4000. | * .94 | 56. | 33.3 | F | 22.4 | 11.7 |
| 8 | 3 | 700. | 189. | 1530. 3970. | 189. | 10. | 3930. | 4230. | ** .93 | 34. | 38.9 | F | 19.0 | 14.6 |
| 9 | 2 | 50. | 0. | 0. 2440. | 0. | 0. | 2400. | 4000. | ** .60 | 8. | 145.0 | F | 10.7 | 24.8 |
| 10 | 2 | 50. | 0. | 0. 2440. | 0. | 0. | 2400. | 2400. | 0. | 1.00 | 65. | E | 19.0 | 14.1 |
| 11 | 2 | 1000. | 0. | 0. 2440. | 0. | 0. | 2400. | 4000. | 0. | .60 | 65. | C | 19.0 | 14.1 |
| 12 | 2 | 10. | 0. | 0. 2440. | 0. | 0. | 2400. | 4000. | 0. | .60 | 65. | C | 19.0 | 14.1 |
| 13 | 2 | 1500. | 920. | 0. 3360. | 920. | 0. | 3320. | 4000. | 0. | .83 | 62. | D | 20.2 | 13.1 |
| 14 | 2 | 1500. | 0. | 730. 3360. | 0. | 721. | 3320. | 4000. | 0. | .83 | 62. | D | 20.2 | 13.1 |
| 15 | 2 | 100. | 0. | 2630. 2630. | 0. | 2599. | 2599. | 4000. | 0. | .65 | 65. | C | 19.0 | 14.1 |
| ***** | | | | | | | | | | | | | | |
| TOTAL | 14810. | = | 2.8 MILES | MAX(V/C) = 1.00 | | | LOWEST LOS = F | AVG = 59. | 26.6 | 19.9 | 13.3 | ***** | | |

| | | |
|----------------------------|------------------------------|------------------------------|
| | CURRENT TIME SLICE | CUMULATIVE VALUES |
| FREEWAY TRAVEL TIME = | 94. VEH-HRS 119. PASS-HRS | 94. VEH-HRS 119. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 190. VEH-HRS 239. PASS-HRS | 190. VEH-HRS 239. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 284. VEH-HRS 358. PASS-HRS | 284. VEH-HRS 358. PASS-HRS |
| TOTAL TRAV DISTANCE = | 5570. VEH-MI. 7019. PASS-MI. | 5570. VEH-MI. 7019. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 20. MPH. | 59. MPH. |
| AVERAGE DENSITY = | 27. VPMP | 27. VPMP |
| TOTAL FUEL = | 348. GALLONS | 348. GALLONS |
| TOTAL EMISSIONS = | 102. KILOGRAMS | 102. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.09 | 2 | 0.10 | 3 | 0.09 | 4 | 0.22 | 5 | 0.19 |
| 6 | 0.45 | 7 | 2.00 | 8 | 3.74 | 9 | 1.20 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.32 | 14 | 0.32 | 15 | 0.00 |

***** TOTAL DELAY = 8.7 VEH-HRS ***** AVERAGE DELAY = 0.15 MIN/VEH *****

***** RAMP DELAYS *****

| OFF-RAMP | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|----------------|-----------------------|---------------|----------|---------|---------|----------|----------------------|
| 2 OUTPUT POINT | 760. | 190.00 | 68.51 | 4.24 | 22.16 | 1.17 | 27.57 |

 ** **
 ** **
 ** **
 ** **

FREEWAY TRAVEL TIME (MINUTES)

| * ORIGINS | * DESTINATIONS ACROSS | | | | | |
|-----------|-----------------------|---|---|---|---|---|
| * DOWN | 1 | 2 | 3 | 4 | 5 | 6 |
| * * | | | | | | |

| | | | | | | |
|-------|------|------|------|------|------|------|
| * 1 * | 1.36 | 2.37 | 2.45 | 2.63 | 3.18 | 3.20 |
| * 2 * | 1.11 | 2.13 | 2.20 | 2.38 | 2.93 | 2.95 |
| * 3 * | 0.60 | 1.61 | 1.69 | 1.87 | 2.42 | 2.44 |
| * 4 * | 0.00 | 0.35 | 0.42 | 0.61 | 1.16 | 1.18 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.17 | 0.72 | 0.74 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.55 | 0.57 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | |
|-----------|----------|------------|-------------|--------------------|-------------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|------|
| * SEC LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP/L | * LEVEL | * MPG | * GS/VM | |
| * 1 3 | 1400. | 4420. | 0. 4420. | 4420. | 0. 4420. | 6000. | 0. | 0. | 0. | .74 | 64. | 22.9 | C | 19.2 | 13.9 |
| * 2 3 | 1500. | 20. | 0. 4440. | 20. | 0. 4440. | 6000. | 0. | 0. | 0. | .74 | 64. | 23.0 | C | 19.3 | 13.8 |
| * 3 3 | 1400. | 0. | 0. 4440. | 0. | 0. 4440. | 6000. | 0. | 0. | 0. | .74 | 64. | 23.0 | C | 19.3 | 13.8 |
| * 4 3 | 1500. | 231. | 0. 4671. | 231. | 0. 4671. | 6000. | 0. | 0. | 0. | .78 | 64. | 24.5 | C | 19.6 | 13.6 |
| * 5 3 | 1300. | 0. | 0. 4671. | 0. | 0. 4671. | 6000. | 0. | 0. | 0. | .78 | 64. | 24.5 | C | 19.6 | 13.6 |
| * 6 3 | 500. | 0. | 890. 4671. | 0. | 890. 4671. | 5020. | 0. | 0. | 0. | .93 | 57. | 27.1 | D | 22.1 | 11.9 |
| * 7 2 | 2300. | 0. | 0. 3781. | 0. | 0. 3741. | 4000. | 0. | * 1257. | 40. | .94 | 39. | 47.5 | F | 21.3 | 12.7 |
| * 8 3 | 700. | 189. | 1530. 3970. | 189. | 10. 3930. | 4230. | 0. | ** 700. | 40. | .93 | 23. | 57.9 | F | 19.1 | 15.1 |
| * 9 2 | 50. | 0. | 0. 2440. | 0. | 0. 2400. | 4000. | 0. | ** 50. | 40. | .60 | 8. | 153.8 | F | 10.4 | 25.5 |
| * 10 2 | 50. | 0. | 0. 2440. | 0. | 0. 2400. | 2400. | 0. | 0. | 0. | 1.00 | 65. | 18.5 | E | 19.0 | 14.1 |
| * 11 2 | 1000. | 0. | 0. 2440. | 0. | 0. 2400. | 4000. | 0. | 0. | 0. | .60 | 65. | 18.5 | C | 19.0 | 14.1 |
| * 12 2 | 10. | 0. | 0. 2440. | 0. | 0. 2400. | 4000. | 0. | 0. | 0. | .60 | 65. | 18.5 | C | 19.0 | 14.1 |
| * 13 2 | 1500. | 920. | 0. 3360. | 920. | 0. 3320. | 4000. | 0. | 0. | 0. | .83 | 62. | 26.7 | D | 20.2 | 13.1 |
| * 14 2 | 1500. | 0. | 730. 3360. | 0. | 721. 3320. | 4000. | 0. | 0. | 0. | .83 | 62. | 26.7 | D | 20.2 | 13.1 |
| * 15 2 | 100. | 0. | 2630. 2630. | 0. | 2599. 2599. | 4000. | 0. | 0. | 0. | .65 | 65. | 20.0 | C | 19.0 | 14.1 |

TOTAL 14810. = 2.8 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 53. 29.7 19.8 13.5

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 104. VEH-HRS | 132. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 570. VEH-HRS | 718. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 674. VEH-HRS | 850. PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 5566. VEH-MI. | 7014. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 8. MPH. | 56. MPH. |
| AVERAGE DENSITY = | 30. VPMP/L | 28. VPMP/L |
| TOTAL FUEL = | 486. GALLONS | 834. GALLONS |
| TOTAL EMISSIONS = | 158. KILOGRAMS | 260. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.09 | 2 | 0.10 | 3 | 0.09 | 4 | 0.22 | 5 | 0.19 |
| 6 | 0.45 | 7 | 8.22 | 8 | 7.50 | 9 | 1.28 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.32 | 14 | 0.32 | 15 | 0.00 |

***** TOTAL DELAY = 18.8 VEH-HRS ***** AVERAGE DELAY = 0.30 MIN/VEH *****

***** RAMP DELAYS *****

TOTAL

OFF-RAMP 2 OUTPUT POINT 1520. 570.00 205.54 12.71 66.47 3.52 82.70

1 INSTITUTE OF TRANSPORTATION STUDIES UNIVERSITY OF CALIFORNIA, BERKELEY FREQ12PE REL 3.01 SIMULATION BEFORE ENTRY CONTROL TIME SLICE 3 OF 4 10/20/2015 8:41 PAGE 8

QUEUE CLEAR SECTION 9 T2 =0.475

1 INSTITUTE OF TRANSPORTATION STUDIES UNIVERSITY OF CALIFORNIA, BERKELEY FREQ12PE REL 3.01 SIMULATION BEFORE ENTRY CONTROL TIME SLICE 3 OF 4 10/20/2015 8:41 PAGE 9

**
** FREEWAY TRAVEL TIME (MINUTES) **
**

Table with columns: ORIGINS DOWN, DESTINATIONS ACROSS (1-6). Contains travel time data for various origin-destination pairs.

1 INSTITUTE OF TRANSPORTATION STUDIES UNIVERSITY OF CALIFORNIA, BERKELEY FREQ12PE REL 3.01 SIMULATION BEFORE ENTRY CONTROL TIME SLICE 3 OF 4 10/20/2015 8:41 PAGE 10

TIME SLICE FREEWAY PERFORMANCE TABLE

Table with columns: SUB NO., SEC LNS, LENGTH, O-D DATA, DEMANDS, ADJUSTED VOLUMES, SSEC, WEAVE EFF, CONGEST LENGTH, STORAGE RATE, V/C RATIO, SPEED MPH, DENSITY VPMP, LOS LEVEL, FUEL MPG, EMISSIONS GS/VM. Includes a TOTAL row at the bottom.

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|----------------------------|--------------------|----------------|-------------------|-----------------|
| FREEWAY TRAVEL TIME = | 104. VEH-HRS | 131. PASS-HRS | 303. VEH-HRS | 381. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 920. VEH-HRS | 1159. PASS-HRS | 1680. VEH-HRS | 2117. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1024. VEH-HRS | 1290. PASS-HRS | 1983. VEH-HRS | 2498. PASS-HRS |
| TOTAL TRAV DISTANCE = | 5808. VEH-MI. | 7318. PASS-MI. | 16945. VEH-MI. | 21351. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 6. MPH. | | 56. MPH. | |
| AVERAGE DENSITY = | 30. VPMP/L | | 29. VPMP/L | |
| TOTAL FUEL = | 616. GALLONS | | 1450. GALLONS | |
| TOTAL EMISSIONS = | 209. KILOGRAMS | | 469. KILOGRAMS | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.10 | 2 | 0.11 | 3 | 0.11 | 4 | 0.30 | 5 | 0.26 |
| 6 | 0.57 | 7 | 4.54 | 8 | 4.56 | 9 | 0.97 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 1.41 | 14 | 1.41 | 15 | 0.00 |

***** TOTAL DELAY = 14.4 VEH-HRS ***** AVERAGE DELAY = 0.22 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-------------------------|--------------------------|------------------|-------------|------------|------------|-------------|----------------------------|
| OFF-RAMP 2 OUTPUT POINT | 2160. | 920.00 | 331.75 | 20.51 | 107.28 | 5.69 | 133.47 |

 ** FREEWAY TRAVEL TIME (MINUTES) **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN

| | 1 | 2 | 3 | 4 | 5 | 6 |
|-----|------|------|------|------|------|------|
| 1 * | 1.37 | 1.95 | 1.96 | 2.14 | 2.74 | 2.76 |
| 2 * | 1.12 | 1.70 | 1.71 | 1.89 | 2.49 | 2.51 |
| 3 * | 0.61 | 1.19 | 1.20 | 1.38 | 1.98 | 2.00 |
| 4 * | 0.00 | 0.12 | 0.13 | 0.31 | 0.92 | 0.93 |
| 5 * | 0.00 | 0.00 | 0.00 | 0.17 | 0.78 | 0.79 |
| 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.60 | 0.62 |

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

 * SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMISS *

| * SEC | LNS | LENGTH | ORG | DES | SSEC | ORG | DES | SSEC | CAP. | EFF | LENGTH | RATE | RATIO | MPH | VPMPL | LEVEL | MPG | GS/VM |
|-------|-----|--------|-------|-------|-------|-------|-------|-------|-------|-------|--------|------|-------|-----|-------|-------|------|-------|
| * | 1 | 3 | 1400. | 4455. | 0. | 4455. | 4455. | 0. | 4455. | 6000. | 0. | 0. | .74 | 64. | 23.1 | C | 19.3 | 13.8 |
| * | 2 | 3 | 1500. | 20. | 0. | 4475. | 20. | 0. | 4475. | 6000. | 0. | 0. | .75 | 64. | 23.2 | C | 19.3 | 13.8 |
| * | 3 | 3 | 1400. | 0. | 0. | 4475. | 0. | 0. | 4475. | 6000. | 0. | 0. | .75 | 64. | 23.2 | C | 19.3 | 13.8 |
| * | 4 | 3 | 1500. | 310. | 0. | 4785. | 310. | 0. | 4785. | 6000. | 0. | 0. | .80 | 63. | 25.2 | C | 19.8 | 13.5 |
| * | 5 | 3 | 1300. | 0. | 0. | 4785. | 0. | 0. | 4785. | 6000. | 0. | 0. | .80 | 63. | 25.2 | C | 19.8 | 13.5 |
| * | 6 | 3 | 500. | 0. | 1020. | 4785. | 0. | 1020. | 4785. | 5020. | 0. | 0. | .95 | 56. | 28.5 | D | 22.6 | 11.6 |
| * | 7 | 2 | 2300. | 0. | 0. | 3765. | 0. | 0. | 3765. | 4000. | 0. | 0. | .94 | 57. | 33.2 | D | 22.3 | 11.7 |
| * | 8 | 3 | 700. | 230. | 1290. | 3995. | 230. | 10. | 3995. | 4230. | 0. | 0. | .94 | 65. | 20.5 | C | 19.0 | 14.1 |
| * | 9 | 2 | 50. | 0. | 450. | 2705. | 0. | 450. | 2705. | 4000. | 0. | 0. | .68 | 65. | 20.8 | C | 19.0 | 14.1 |
| * | 10 | 2 | 50. | 0. | 0. | 2255. | 0. | 0. | 2255. | 2400. | 0. | 0. | .94 | 65. | 17.3 | B | 19.0 | 14.1 |
| * | 11 | 2 | 1000. | 450. | 0. | 2705. | 450. | 0. | 2705. | 4000. | 0. | 0. | .68 | 65. | 20.8 | C | 19.0 | 14.1 |
| * | 12 | 2 | 10. | 0. | 0. | 2705. | 0. | 0. | 2705. | 4000. | 0. | 0. | .68 | 65. | 20.8 | C | 19.0 | 14.1 |
| * | 13 | 2 | 1500. | 1050. | 0. | 3755. | 1050. | 0. | 3755. | 4000. | 0. | 0. | .94 | 57. | 33.0 | D | 22.3 | 11.8 |
| * | 14 | 2 | 1500. | 0. | 1191. | 3755. | 0. | 1191. | 3755. | 4000. | 0. | 0. | .94 | 57. | 33.0 | D | 22.3 | 11.8 |
| * | 15 | 2 | 100. | 0. | 2564. | 2564. | 0. | 2564. | 2564. | 4000. | 0. | 0. | .64 | 65. | 19.7 | C | 19.0 | 14.1 |

* TOTAL 14810. = 2.8 MILES MAX(V/C) = 0.95 LOWEST LOS = D AVG = 61. 27.0 20.4 13.0 *

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 94. VEH-HRS | 397. VEH-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| OFF-RAMP DELAY = | 1240. VEH-HRS | 2920. VEH-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1334. VEH-HRS | 3317. VEH-HRS |
| TOTAL TRAV DISTANCE = | 5773. VEH-MI. | 22718. VEH-MI. |
| AVERAGE SYSTEM SPEED = | 4. MPH. | 57. MPH. |
| AVERAGE DENSITY = | 27. VPMPPL | 28. VPMPPL |
| TOTAL FUEL = | 730. GALLONS | 2181. GALLONS |
| TOTAL EMISSIONS = | 255. KILOGRAMS | 724. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.10 | 2 | 0.11 | 3 | 0.11 | 4 | 0.30 | 5 | 0.26 |
| 6 | 0.57 | 7 | 1.84 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 1.17 | 14 | 1.17 | 15 | 0.00 |

***** TOTAL DELAY = 5.6 VEH-HRS ***** AVERAGE DELAY = 0.09 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH | DELAY | GAS | HC | CO | NOX | TOTAL |
|-------------------------|--------------|---------|--------|-------|--------|------|-----------|
| | VEHICLES | VEH-HRS | GALS | KGMS | KGMS | KGMS | EMISSIONS |
| OFF-RAMP 2 OUTPUT POINT | 2800. | 1240.00 | 447.14 | 27.64 | 144.60 | 7.66 | 179.90 |

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FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ      1111      222222      PPPPPPPP      EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A.D.MAY*Q 111111    222 222    PPPPPPPP    EEEEEEEEE
FFF      RRR  RRR  EEE      QQQQ      QQQQ      1111    222 222    PPP  PPP    EEE
FFF      RRR  RRR  EEE      QQQQ      QQQQ      1111    222 222    PPP  PPP    EEE
FFFFFFF  RRRRRRRR EEEEEEE   QQQQ      QQQQ      1111    222 222    PPPPPPPP    EEEEEEE
FFFFFFF  RRRRRRRR EEEEEEE   QQQQ      QQQQ      1111    2222    PPPPPPPP    EEEEEEE
FFF      RRR  RRR  EEE      QQQQ      QQQ QQQQ    1111    2222    PPP      EEE
FFF      RRR  RRR  EEE      Q*UC*      QQQQ      1111    222      PPP      EEE
FFF      RRR  RRR  EEEEEEEEE Q*REGENTS*Q 1111    222      PPP      EEEEEEEEE
FFF      RRR  RRR  EEEEEEEEE Q*1999*Q QQQ 11111111 2222222222 PPP      EEEEEEEEE
    
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FREQ12PE

1. THIS IS A SIMULATION ONLY EXECUTION.
2. THERE ARE 2.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
 LOWER LIMB (AT V/C=1) = 30
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.

FREEWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC | SSEC | DESIGN | ORG | TRK | SSEC | PCT | PCT | DES | SPECIAL | FF. SPD. | CAP. | ART | GRADE | SUBSECTION | LOCATION |
|---------|------|-------|--------|-----|-----|------|-----|--------|------|----------|----------|------|----------|-------|--------------------------|----------|
| SEC | LNS | CAP | LENGTH | DES | FAC | GRAD | TRK | TRUCKS | RAMP | ALT. RTE | ALT. RTE | TYPE | ALT. RTE | | | |
| 1 | 3 | 6000. | 1400. | 65 | 0 | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | DKS begin of network | |
| 2 | 3 | 6000. | 1500. | 65 | 0 | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence On-ramp | |
| 3 | 3 | 6000. | 1400. | 65 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence to Crossman | |
| 4 | 3 | 6000. | 1500. | 65 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Crossman On-Ramp | |
| 5 | 3 | 6000. | 1300. | 65 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Crossman / Mathilda | |
| 6 | 3 | 5020. | 500. | 65 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-Ramp | |
| 7 | 2 | 4000. | 2300. | 65 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | |
| 8 | 3 | 4230. | 700. | 65 | OD | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda / US 101 | |
| 9 | 2 | 4000. | 50. | 65 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bottleneck by-pass | |
| 10 | 2 | 2470. | 50. | 65 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bottleek | |
| 11 | 2 | 4000. | 1000. | 65 | OD | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US 101 / US 101 | |
| 12 | 2 | 4000. | 10. | 65 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Dummy end of travel time | |
| 13 | 2 | 4000. | 1500. | 65 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US 101 NB On-Ramp | |
| 14 | 2 | 4000. | 1500. | 65 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Maude Off-ramp | |
| 15 | 2 | 4000. | 100. | 65 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End of Network | |

***** INPUT HAS BEEN COMPLETED *****

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FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A.D.MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQ QQQ 1111 222 222 PPP PPP EEE
FFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQ QQQ QQQ 1111 222 PPP EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP EEEEEEEEE
    
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FREQ12PE

1. THIS IS A SIMULATION ONLY EXECUTION.
2. THERE ARE 2.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
 LOWER LIMB (AT V/C=1) = 30
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.

***** INPUT HAS BEEN COMPLETED *****

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*****
**                                     **
**          FREEWAY TRAVEL TIME (MINUTES)          **
**                                     **
*****
    
```

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*****
* ORIGINS          DESTINATIONS ACROSS          *
* DOWN            *                             *
*                 1     2     3     4     5     6     *
+
*                 *                             *
*                 *                             *
+
* 1 * 1.33 1.87 1.88 2.06 2.59 2.61          *
+
* 2 * 1.08 1.62 1.63 1.82 2.35 2.37          *
+
* 3 * 0.58 1.12 1.13 1.31 1.84 1.86          *
+
* 4 * 0.00 0.12 0.13 0.31 0.85 0.86          *
+
* 5 * 0.00 0.00 0.00 0.17 0.71 0.72          *
+
* 6 * 0.00 0.00 0.00 0.00 0.53 0.55          *
*                 *                             *
*****
    
```

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB SEC | NO. LNS | SSEC LENGTH | O-D ORG | DATA DES | DEMANDS SSEC | ADJUSTED ORG | VOLUMES DES | SSEC | SSEC CAP. | WEAVE EFF | CONGEST LENGTH | STORAGE RATE | V/C RATIO | SPEED MPH | DENSITY VPMP | LOS LEVEL | FUEL MPG | EMI SS GS/VM |
|---------|---------|-------------|---------|----------|--------------|--------------|-------------|-------|-----------|-----------|----------------|--------------|-----------|-----------|--------------|-----------|----------|--------------|
| 1 | 3 | 1400. | 3336. | 0. | 3336. | 3336. | 0. | 3336. | 6000. | 0. | 0. | 0. | .56 | 65. | 17.1 | B | 19.0 | 14.1 |
| 2 | 3 | 1500. | 40. | 0. | 3376. | 40. | 0. | 3376. | 6000. | 0. | 0. | 0. | .56 | 65. | 17.3 | B | 19.0 | 14.1 |
| 3 | 3 | 1400. | 0. | 0. | 3376. | 0. | 0. | 3376. | 6000. | 0. | 0. | 0. | .56 | 65. | 17.3 | B | 19.0 | 14.1 |
| 4 | 3 | 1500. | 550. | 0. | 3926. | 550. | 0. | 3926. | 6000. | 0. | 0. | 0. | .65 | 65. | 20.1 | C | 19.0 | 14.1 |
| 5 | 3 | 1300. | 0. | 0. | 3926. | 0. | 0. | 3926. | 6000. | 0. | 0. | 0. | .65 | 65. | 20.1 | C | 19.0 | 14.1 |
| 6 | 3 | 500. | 0. | 641. | 3926. | 0. | 641. | 3926. | 5020. | 0. | 0. | 0. | .78 | 65. | 20.1 | C | 19.0 | 14.1 |
| 7 | 2 | 2300. | 0. | 0. | 3285. | 0. | 0. | 3285. | 4000. | 0. | 0. | 0. | .82 | 63. | 26.3 | D | 20.1 | 13.2 |
| 8 | 3 | 700. | 690. | 1670. | 3975. | 690. | 10. | 3975. | 4230. | 0. | 0. | 0. | .94 | 65. | 20.4 | C | 19.0 | 14.1 |
| 9 | 2 | 50. | 0. | 50. | 2305. | 0. | 50. | 2305. | 4000. | 0. | 0. | 0. | .58 | 65. | 17.7 | B | 19.0 | 14.1 |
| 10 | 2 | 50. | 0. | 0. | 2255. | 0. | 0. | 2255. | 2470. | 0. | 0. | 0. | .91 | 65. | 17.3 | B | 19.0 | 14.1 |
| 11 | 2 | 1000. | 50. | 0. | 2305. | 50. | 0. | 2305. | 4000. | 0. | 0. | 0. | .58 | 65. | 17.7 | B | 19.0 | 14.1 |
| 12 | 2 | 10. | 0. | 0. | 2305. | 0. | 0. | 2305. | 4000. | 0. | 0. | 0. | .58 | 65. | 17.7 | B | 19.0 | 14.1 |
| 13 | 2 | 1500. | 660. | 0. | 2965. | 660. | 0. | 2965. | 4000. | 0. | 0. | 0. | .74 | 64. | 23.1 | C | 19.3 | 13.8 |
| 14 | 2 | 1500. | 0. | 260. | 2965. | 0. | 260. | 2965. | 4000. | 0. | 0. | 0. | .74 | 64. | 23.1 | C | 19.3 | 13.8 |
| 15 | 2 | 100. | 0. | 2705. | 2705. | 0. | 2705. | 2705. | 4000. | 0. | 0. | 0. | .68 | 65. | 20.8 | C | 19.0 | 14.1 |

TOTAL 14810. = 2.8 MILES MAX(V/C) = 0.94 LOWEST LOS = D AVG = 64. 20.7 19.2 13.9

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 73. VEH-HRS | 92. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 208. VEH-HRS | 261. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 280. VEH-HRS | 353. PASS-HRS |
| TOTAL TRAV DISTANCE = | 4685. VEH-MI. | 5903. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 17. MPH. | 64. MPH. |
| AVERAGE DENSITY = | 21. VPMP | 21. VPMP |
| TOTAL FUEL = | 319. GALLONS | 319. GALLONS |
| TOTAL EMISSIONS = | 95. KILOGRAMS | 95. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.44 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.07 | 14 | 0.07 | 15 | 0.00 |

***** TOTAL DELAY = 0.6 VEH-HRS ***** AVERAGE DELAY = 0.01 MIN/VEH *****

***** RAMP DELAYS *****

| OFF-RAMP | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|----------------|-----------------------|---------------|----------|---------|---------|----------|----------------------|
| 2 OUTPUT POINT | 830. | 207.50 | 74.82 | 4.63 | 24.20 | 1.28 | 30.10 |

 ** FREEWAY TRAVEL TIME (MINUTES) **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN *
 * 1 2 3 4 5 6 *
 * *****

| | | | | | | | | | | | | | | | | | | |
|---|---|---|---|------|------|------|------|------|------|--|--|--|--|--|--|--|--|---|
| + | * | * | | | | | | | | | | | | | | | | * |
| + | * | 1 | * | 1.33 | 1.87 | 1.88 | 2.06 | 2.59 | 2.61 | | | | | | | | | * |
| + | * | 2 | * | 1.08 | 1.62 | 1.63 | 1.82 | 2.35 | 2.37 | | | | | | | | | * |
| + | * | 3 | * | 0.58 | 1.12 | 1.13 | 1.31 | 1.84 | 1.86 | | | | | | | | | * |
| + | * | 4 | * | 0.00 | 0.12 | 0.13 | 0.31 | 0.85 | 0.86 | | | | | | | | | * |
| + | * | 5 | * | 0.00 | 0.00 | 0.00 | 0.17 | 0.71 | 0.72 | | | | | | | | | * |
| + | * | 6 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.53 | 0.55 | | | | | | | | | * |
| + | * | * | * | | | | | | | | | | | | | | | * |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | | |
|-----------|----------|------------|-----------|--------------------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|------|---|------|------|
| * SEC LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP/L | * LEVEL | * MPG | * GS/VM | | | | |
| * 1 | 3 | 1400. | 3336. | 0. | 3336. | 3336. | 0. | 3336. | 6000. | 0. | 0. | 0. | .56 | 65. | 17.1 | B | 19.0 | 14.1 |
| * 2 | 3 | 1500. | 40. | 0. | 3376. | 40. | 0. | 3376. | 6000. | 0. | 0. | 0. | .56 | 65. | 17.3 | B | 19.0 | 14.1 |
| * 3 | 3 | 1400. | 0. | 0. | 3376. | 0. | 0. | 3376. | 6000. | 0. | 0. | 0. | .56 | 65. | 17.3 | B | 19.0 | 14.1 |
| * 4 | 3 | 1500. | 550. | 0. | 3926. | 550. | 0. | 3926. | 6000. | 0. | 0. | 0. | .65 | 65. | 20.1 | C | 19.0 | 14.1 |
| * 5 | 3 | 1300. | 0. | 0. | 3926. | 0. | 0. | 3926. | 6000. | 0. | 0. | 0. | .65 | 65. | 20.1 | C | 19.0 | 14.1 |
| * 6 | 3 | 500. | 0. | 641. | 3926. | 0. | 641. | 3926. | 5020. | 0. | 0. | 0. | .78 | 65. | 20.1 | C | 19.0 | 14.1 |
| * 7 | 2 | 2300. | 0. | 0. | 3285. | 0. | 0. | 3285. | 4000. | 0. | 0. | 0. | .82 | 63. | 26.3 | D | 20.1 | 13.2 |
| * 8 | 3 | 700. | 690. | 1670. | 3975. | 690. | 10. | 3975. | 4230. | 0. | 0. | 0. | .94 | 65. | 20.4 | C | 19.0 | 14.1 |
| * 9 | 2 | 50. | 0. | 50. | 2305. | 0. | 50. | 2305. | 4000. | 0. | 0. | 0. | .58 | 65. | 17.7 | B | 19.0 | 14.1 |
| * 10 | 2 | 50. | 0. | 0. | 2255. | 0. | 0. | 2255. | 2470. | 0. | 0. | 0. | .91 | 65. | 17.3 | B | 19.0 | 14.1 |
| * 11 | 2 | 1000. | 50. | 0. | 2305. | 50. | 0. | 2305. | 4000. | 0. | 0. | 0. | .58 | 65. | 17.7 | B | 19.0 | 14.1 |
| * 12 | 2 | 10. | 0. | 0. | 2305. | 0. | 0. | 2305. | 4000. | 0. | 0. | 0. | .58 | 65. | 17.7 | B | 19.0 | 14.1 |
| * 13 | 2 | 1500. | 660. | 0. | 2965. | 660. | 0. | 2965. | 4000. | 0. | 0. | 0. | .74 | 64. | 23.1 | C | 19.3 | 13.8 |
| * 14 | 2 | 1500. | 0. | 260. | 2965. | 0. | 260. | 2965. | 4000. | 0. | 0. | 0. | .74 | 64. | 23.1 | C | 19.3 | 13.8 |
| * 15 | 2 | 100. | 0. | 2705. | 2705. | 0. | 2705. | 2705. | 4000. | 0. | 0. | 0. | .68 | 65. | 20.8 | C | 19.0 | 14.1 |

TOTAL 14810. = 2.8 MI LES MAX(V/C) = 0.94 LOWEST LOS = D AVG = 64. 20.7 19.2 13.9

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 73. VEH-HRS | 92. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 623. VEH-HRS | 784. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 695. VEH-HRS | 876. PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 4685. VEH-MI. | 5903. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 7. MPH. | 64. MPH. |
| AVERAGE DENSITY = | 21. VPMP/L | 21. VPMP/L |
| TOTAL FUEL = | 469. GALLONS | 788. GALLONS |
| TOTAL EMISSIONS = | 155. KILOGRAMS | 251. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.44 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.07 | 14 | 0.07 | 15 | 0.00 |

***** TOTAL DELAY = 0.6 VEH-HRS ***** AVERAGE DELAY = 0.01 MIN/VEH *****

***** RAMP DELAYS *****

TOTAL

QUEUE LENGTH DELAY GAS HC CO NOX EMISSIONS
 VEHICLES VEH-HRS GALS KGMS KGMS KGMS
 OFF-RAMP 2 OUTPUT POINT 1660. 622.50 224.47 13.88 72.59 3.85 90.31

 **
 ** FREeway TRAVEL TIME (MINUTES) **
 **

| * ORIGINS | * DESTINATIONS ACROSS | | | | | | * |
|-----------|-----------------------|------|------|------|------|------|---|
| * DOWN | 1 | 2 | 3 | 4 | 5 | 6 | * |
| * 1 * | 1.35 | 2.65 | 2.72 | 2.90 | 3.46 | 3.48 | * |
| * 2 * | 1.10 | 2.41 | 2.48 | 2.66 | 3.22 | 3.24 | * |
| * 3 * | 0.59 | 1.90 | 1.97 | 2.15 | 2.71 | 2.73 | * |
| * 4 * | 0.00 | 0.31 | 0.37 | 0.56 | 1.12 | 1.13 | * |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.17 | 0.73 | 0.75 | * |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.56 | 0.58 | * |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB | * NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|-------|-------|----------|------------|-----------|------------|-----------|---------|---------|-----------|-----------|----------|---------|-----------|-------|---------|-------------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VP/MP | * LEVEL |
| * 1 | * 3 | * 1400. | * 3695. | * 0. | * 3695. | * 3695. | * 0. | * 3695. | * 6000. | * 0. | * 0. | * 0. | * .62 | * 65. | * 18.9 | * C |
| * 2 | * 3 | * 1500. | * 40. | * 0. | * 3735. | * 40. | * 0. | * 3735. | * 6000. | * 0. | * 0. | * 0. | * .62 | * 65. | * 19.2 | * C |
| * 3 | * 3 | * 1400. | * 0. | * 0. | * 3735. | * 0. | * 0. | * 3735. | * 6000. | * 0. | * 0. | * 0. | * .62 | * 65. | * 19.2 | * C |
| * 4 | * 3 | * 1500. | * 620. | * 0. | * 4355. | * 620. | * 0. | * 4355. | * 6000. | * 0. | * 0. | * 0. | * .73 | * 65. | * 22.5 | * C |
| * 5 | * 3 | * 1300. | * 0. | * 0. | * 4355. | * 0. | * 0. | * 4355. | * 6000. | * 0. | * 0. | * 0. | * .73 | * 65. | * 22.5 | * C |
| * 6 | * 3 | * 500. | * 0. | * 890. | * 4355. | * 0. | * 890. | * 4169. | * 5020. | * 0. | * * | * 275. | * .83 | * 56. | * 24.6 | * F |
| * 7 | * 2 | * 2300. | * 0. | * 0. | * 3465. | * 0. | * 0. | * 3279. | * 4000. | * 0. | * ** | * 2300. | * .82 | * 26. | * 62.8 | * F |
| * 8 | * 3 | * 700. | * 730. | * 1489. | * 4195. | * 730. | * 10. | * 4009. | * 4230. | * 0. | * ** | * 700. | * .95 | * 26. | * 51.5 | * F |
| * 9 | * 2 | * 50. | * 0. | * 50. | * 2706. | * 0. | * 50. | * 2520. | * 4000. | * 0. | * ** | * 50. | * .86 | * 9. | * 145.5 | * F |
| * 10 | * 2 | * 50. | * 0. | * 0. | * 2656. | * 0. | * 0. | * 2470. | * 2470. | * 0. | * 0. | * 0. | * 1.00 | * 65. | * 19.0 | * E |
| * 11 | * 2 | * 1000. | * 50. | * 0. | * 2706. | * 50. | * 0. | * 2520. | * 4000. | * 0. | * 0. | * 0. | * .63 | * 65. | * 19.4 | * C |
| * 12 | * 2 | * 10. | * 0. | * 0. | * 2706. | * 0. | * 0. | * 2520. | * 4000. | * 0. | * 0. | * 0. | * .63 | * 65. | * 19.4 | * C |
| * 13 | * 2 | * 1500. | * 920. | * 0. | * 3626. | * 920. | * 0. | * 3440. | * 4000. | * 0. | * 0. | * 0. | * .86 | * 61. | * 28.2 | * D |
| * 14 | * 2 | * 1500. | * 0. | * 651. | * 3626. | * 0. | * 618. | * 3440. | * 4000. | * 0. | * 0. | * 0. | * .86 | * 61. | * 28.2 | * D |
| * 15 | * 2 | * 100. | * 0. | * 2975. | * 2975. | * 0. | * 2822. | * 2822. | * 4000. | * 0. | * 0. | * 0. | * .71 | * 65. | * 21.7 | * C |

* TOTAL 14810. = 2.8 MI LINES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 49. 30.6 19.3 14.0 *

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREeway TRAVEL TIME = | 105. VEH-HRS | 132. PASS-HRS |
| FREeway MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 1015. VEH-HRS | 1279. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1120. VEH-HRS | 1411. PASS-HRS |
| TOTAL TRAV DISTANCE = | 5148. VEH-MI. | 6486. PASS-MI. |

AVERAGE SYSTEM SPEED = 5. MPH. 58. MPH.
 AVERAGE DENSITY = 31. VPML 24. VPML
 TOTAL FUEL = 632. GALLONS 1420. GALLONS
 TOTAL EMISSIONS = 219. KILOGRAMS 470. KILOGRAMS

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.07 | 5 | 0.06 |
| 6 | 0.48 | 7 | 16.88 | 8 | 6.19 | 9 | 1.20 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.48 | 14 | 0.48 | 15 | 0.00 |

***** TOTAL DELAY = 25.8 VEH-HRS ***** AVERAGE DELAY = 0.46 MIN/VEH *****

***** RAMP DELAYS *****

| OFF-RAMP | 2 | OUTPUT POINT | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|----------|---|--------------|-----------------------|---------------|----------|---------|---------|----------|----------------------|
| | | | 2400. | 1014.88 | 365.96 | 22.62 | 118.34 | 6.27 | 147.24 |

 ** FREeway TRAVEL TIME (MINUTES) **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN 1 2 3 4 5 6 *

| | 1 | 2 | 3 | 4 | 5 | 6 |
|-------|------|------|------|------|------|------|
| * 1 * | 2.14 | 4.16 | 4.23 | 4.41 | 4.97 | 4.99 |
| * 2 * | 1.90 | 3.92 | 3.98 | 4.17 | 4.73 | 4.74 |
| * 3 * | 1.39 | 3.41 | 3.48 | 3.66 | 4.22 | 4.24 |
| * 4 * | 0.00 | 0.33 | 0.39 | 0.58 | 1.14 | 1.15 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.17 | 0.73 | 0.75 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.56 | 0.58 |

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|-----------|--------|------------|-----------|--------------------|---------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|
| * SEC | * LNS | * LENGTH | * ORG DES | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPML | * LEVEL | * MPG | * GS/VM |
| * 1 | * 3 | * 1400. | * 3695. | * 0. 3695. | * 3695. | * 0. | * 0. | * 0. | * .62 | * 65. | * 18.9 | * C | * 19.0 | * 14.1 |
| * 2 | * 3 | * 1500. | * 40. | * 0. 3735. | * 40. | * 0. | * 0. | * 0. | * .62 | * 65. | * 19.2 | * C | * 19.0 | * 14.1 |
| * 3 | * 3 | * 1400. | * 0. | * 0. 3735. | * 0. | * 0. | * 0. | * 0. | * .62 | * 65. | * 19.2 | * C | * 19.0 | * 14.1 |
| * 4 | * 3 | * 1500. | * 620. | * 0. 4355. | * 620. | * 0. | * 51. | * 186. | * .69 | * 64. | * 21.6 | * F | * 19.2 | * 13.9 |
| * 5 | * 3 | * 1300. | * 0. | * 0. 4355. | * 0. | * 0. | ** 1300. | * 186. | * .69 | * 19. | * 73.3 | * F | * 15.9 | * 17.9 |

| | | | | | | | | | | | | | | | | | | | | | |
|---|-------|--------|-------|------|-------|-------|------|-------|-------|-------|----|----|-----------------|----------------|-----------|------|-------|------|------|------|---|
| * | 6 | 3 | 500. | 0. | 890. | 4355. | 0. | 890. | 4169. | 5020. | 0. | ** | 500. | 186. | .83 | 16. | 85.4 | F | 16.5 | 18.2 | * |
| * | 7 | 2 | 2300. | 0. | 0. | 3465. | 0. | 0. | 3279. | 4000. | 0. | ** | 2300. | 186. | .82 | 15. | 105.9 | F | 16.3 | 18.7 | * |
| * | 8 | 3 | 700. | 730. | 1489. | 4195. | 730. | 10. | 4009. | 4230. | 0. | ** | 700. | 186. | .95 | 24. | 55.0 | F | 19.6 | 14.4 | * |
| * | 9 | 2 | 50. | 0. | 50. | 2706. | 0. | 50. | 2520. | 4000. | 0. | ** | 50. | 186. | .63 | 9. | 147.3 | F | 11.2 | 24.6 | * |
| * | 10 | 2 | 50. | 0. | 0. | 2656. | 0. | 0. | 2470. | 2470. | 0. | 0. | 0. | 1.00 | 65. | 19.0 | E | 19.0 | 14.1 | * | |
| * | 11 | 2 | 1000. | 50. | 0. | 2706. | 50. | 0. | 2520. | 4000. | 0. | 0. | 0. | .63 | 65. | 19.4 | C | 19.0 | 14.1 | * | |
| * | 12 | 2 | 10. | 0. | 0. | 2706. | 0. | 0. | 2520. | 4000. | 0. | 0. | 0. | .63 | 65. | 19.4 | C | 19.0 | 14.1 | * | |
| * | 13 | 2 | 1500. | 920. | 0. | 3626. | 920. | 0. | 3440. | 4000. | 0. | 0. | 0. | .86 | 61. | 28.2 | D | 20.8 | 12.7 | * | |
| * | 14 | 2 | 1500. | 0. | 651. | 3626. | 0. | 618. | 3440. | 4000. | 0. | 0. | 0. | .86 | 61. | 28.2 | D | 20.8 | 12.7 | * | |
| * | 15 | 2 | 100. | 0. | 2975. | 2975. | 0. | 2822. | 2822. | 4000. | 0. | 0. | 0. | .71 | 65. | 21.7 | C | 19.0 | 14.1 | * | |
| * | ***** | | | | | | | | | | | | | | | | | | | | |
| * | TOTAL | 14810. | = | 2.8 | MILES | | | | | | | | MAX(V/C) = 1.00 | LOWEST LOS = F | AVG = 34. | 43.8 | | 18.4 | 15.0 | * | |
| * | ***** | | | | | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 152. VEH-HRS | 402. VEH-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| OFF-RAMP DELAY = | 1385. VEH-HRS | 3230. VEH-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1536. VEH-HRS | 3631. VEH-HRS |
| TOTAL TRAVEL DISTANCE = | 5106. VEH-MI. | 19624. VEH-MI. |
| AVERAGE SYSTEM SPEED = | 3. MPH. | 49. MPH. |
| AVERAGE DENSITY = | 44. VPMP/L | 29. VPMP/L |
| TOTAL FUEL = | 777. GALLONS | 2196. GALLONS |
| TOTAL EMISSIONS = | 278. KILOGRAMS | 747. KILOGRAMS |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION BEFORE ENTRY CONTROL
 TIME SLICE 4 OF 6

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.10 | 5 | 19.61 |
| 6 | 9.10 | 7 | 35.16 | 8 | 6.85 | 9 | 1.21 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.48 | 14 | 0.48 | 15 | 0.00 |

***** TOTAL DELAY = 73.0 VEH-HRS ***** AVERAGE DELAY = 1.21 MIN/VEH *****

***** RAMP DELAYS *****

| OFF-RAMP | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|----------------|-----------------------|---------------|----------|---------|---------|----------|----------------------|
| 2 OUTPUT POINT | 3139. | 1384.63 | 499.30 | 30.86 | 161.46 | 8.56 | 200.88 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 10/20/2015 8:42 PAGE 14
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 TIME SLICE 5 OF 6

QUEUE CLEAR SECTION 9 T2 =0.445

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 10/20/2015 8:42 PAGE 15
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 TIME SLICE 5 OF 6

 ** **
 ** **
 ** **
 ** **

FREEWAY TRAVEL TIME (MINUTES)

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN *
 * 1 2 3 4 5 6 *

| | | | | | | |
|-------|------|------|------|------|------|------|
| * 1 * | 1.78 | 3.18 | 3.23 | 3.42 | 4.00 | 4.01 |
| * 2 * | 1.54 | 2.94 | 2.99 | 3.17 | 3.75 | 3.77 |

**
** FREeway TRAVEL TIME (MINUTES) **
**

| * ORIGINS | | DESTINATIONS ACROSS | | | | | |
|-----------|-----|---------------------|------|------|------|------|------|
| * DOWN | | | | | | | |
| * | * | 1 | 2 | 3 | 4 | 5 | 6 |
| * | * | | | | | | |
| + | | | | | | | |
| * | * | | | | | | |
| + | | | | | | | |
| * | 1 * | 1.33 | 1.86 | 1.87 | 2.05 | 2.59 | 2.61 |
| + | | | | | | | |
| * | 2 * | 1.08 | 1.62 | 1.62 | 1.81 | 2.35 | 2.37 |
| + | | | | | | | |
| * | 3 * | 0.58 | 1.11 | 1.12 | 1.30 | 1.84 | 1.86 |
| + | | | | | | | |
| * | 4 * | 0.00 | 0.12 | 0.13 | 0.31 | 0.86 | 0.87 |
| + | | | | | | | |
| * | 5 * | 0.00 | 0.00 | 0.00 | 0.17 | 0.72 | 0.73 |
| + | | | | | | | |
| * | 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.54 | 0.56 |
| + | | | | | | | |
| * | * | | | | | | |
| + | | | | | | | |

*
* TIME SLICE FREEWAY PERFORMANCE TABLE *
*

| * SUB | * NO. | * SSEC | * O-D DATA | | * DEMANDS | | * ADJUSTED VOLUMES | | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | |
|-------|-------|----------|------------|-------|-----------|-----------|--------------------|--------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMPPL | * LEVEL | * MPG | * GS/VM | |
| * | 1 | 3 | 1400. | 3182. | 0. | 3182. | 3182. | 0. | 3182. | 6000. | 0. | 0. | 0. | .53 | 65. | 16.3 | B | 19.0 | 14.1 |
| * | 2 | 3 | 1500. | 51. | 0. | 3233. | 51. | 0. | 3233. | 6000. | 0. | 0. | 0. | .54 | 65. | 16.6 | B | 19.0 | 14.1 |
| * | 3 | 3 | 1400. | 0. | 0. | 3233. | 0. | 0. | 3233. | 6000. | 0. | 0. | 0. | .54 | 65. | 16.6 | B | 19.0 | 14.1 |
| * | 4 | 3 | 1500. | 409. | 0. | 3642. | 409. | 0. | 3642. | 6000. | 0. | 0. | 0. | .61 | 65. | 18.7 | C | 19.0 | 14.1 |
| * | 5 | 3 | 1300. | 0. | 0. | 3642. | 0. | 0. | 3642. | 6000. | 0. | 0. | 0. | .61 | 65. | 18.7 | C | 19.0 | 14.1 |
| * | 6 | 3 | 500. | 0. | 580. | 3642. | 0. | 580. | 3642. | 5020. | 0. | 0. | 0. | .73 | 65. | 18.7 | C | 19.0 | 14.1 |
| * | 7 | 2 | 2300. | 0. | 0. | 3062. | 0. | 0. | 3062. | 4000. | 0. | 0. | 0. | .77 | 64. | 24.0 | C | 19.4 | 13.7 |
| * | 8 | 3 | 700. | 550. | 1209. | 3612. | 550. | 10. | 3612. | 4230. | 0. | 0. | 0. | .85 | 65. | 18.5 | C | 19.0 | 14.1 |
| * | 9 | 2 | 50. | 0. | 400. | 2403. | 0. | 400. | 2403. | 4000. | 0. | 0. | 0. | .60 | 65. | 18.5 | C | 19.0 | 14.1 |
| * | 10 | 2 | 50. | 0. | 0. | 2003. | 0. | 0. | 2003. | 2470. | 0. | 0. | 0. | .81 | 65. | 15.4 | B | 19.0 | 14.1 |
| * | 11 | 2 | 1000. | 400. | 0. | 2403. | 400. | 0. | 2403. | 4000. | 0. | 0. | 0. | .60 | 65. | 18.5 | C | 19.0 | 14.1 |
| * | 12 | 2 | 10. | 0. | 0. | 2403. | 0. | 0. | 2403. | 4000. | 0. | 0. | 0. | .60 | 65. | 18.5 | C | 19.0 | 14.1 |
| * | 13 | 2 | 1500. | 790. | 0. | 3193. | 790. | 0. | 3193. | 4000. | 0. | 0. | 0. | .80 | 63. | 25.3 | C | 19.8 | 13.4 |
| * | 14 | 2 | 1500. | 0. | 501. | 3193. | 0. | 501. | 3193. | 4000. | 0. | 0. | 0. | .80 | 63. | 25.3 | C | 19.8 | 13.4 |
| * | 15 | 2 | 100. | 0. | 2692. | 2692. | 0. | 2692. | 2692. | 4000. | 0. | 0. | 0. | .67 | 65. | 20.7 | C | 19.0 | 14.1 |
| * | | | | | | | | | | | | | | | | | | | |
| * | TOTAL | | 14810. | = | | 2.8 MILES | | | | | | | | | | | | | |
| * | | | | | | | | | | | | | | | | | | | |
| * | | | | | | | | | | | | | | | | | | | |
| * | | | | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | | | CUMULATIVE VALUES | | | | |
|----------------------------|--------------------|------------|-------|-------------------|--------|------------|--------|----------|
| FREEWAY TRAVEL TIME = | 70. | VEH-HRS | 89. | PASS-HRS | 588. | VEH-HRS | 741. | PASS-HRS |
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 2019. | VEH-HRS | 2544. | PASS-HRS | 6968. | VEH-HRS | 8780. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 2090. | VEH-HRS | 2633. | PASS-HRS | 7556. | VEH-HRS | 9521. | PASS-HRS |
| TOTAL TRAV DISTANCE = | 4537. | VEH-MI. | 5717. | PASS-MI. | 28974. | VEH-MI. | 36507. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 2. | MPH. | | | 49. | MPH. | | |
| AVERAGE DENSITY = | 20. | VPMPPL | | | 28. | VPMPPL | | |
| TOTAL FUEL = | 964. | GALLONS | | | 4033. | GALLONS | | |
| TOTAL EMISSIONS = | 356. | KI LOGRAMS | | | 1421. | KI LOGRAMS | | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.17 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.20 | 14 | 0.20 | 15 | 0.00 |

***** TOTAL DELAY = 0.6 VEH-HRS ***** AVERAGE DELAY = 0.01 MIN/VEH *****

***** RAMP DELAYS *****

| | | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS | |
|----------|---|--------------------------|------------------|-------------|------------|------------|-------------|----------------------------|--------|
| OFF-RAMP | 2 | OUTPUT POINT | 4338. | 2019.13 | 728.10 | 45.01 | 235.45 | 12.48 | 292.93 |

SR 237 Eastbound

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FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ      1111      222222      PPPPPPPP      LLL
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A.D.MAY*Q 111111    222 222    PPPPPPPP    LLL
FFF      RRR      RRR      EEE      QQQQQ      QQQQQ      1111      222 222    PPP      PPP    LLL
FFF      RRR      RRR      EEE      QQQQ      QQQQ      1111      222      PPP      PPP    LLL
FFFFFFF  RRRRRRRR EEEEEEE   QQQQ      QQQQ      1111      222      PPPPPPPP    LLL
FFFFFFF  RRRRRRRR EEEEEEE   QQQQ      QQQQ      1111      2222     PPPPPPPP    LLL
FFF      RRR      RRR      EEE      QQQQ      QQQ QQQQ    1111      2222     PPP      LLL
FFF      RRR      RRR      EEE      Q*UC*      QQQQ      1111      222      PPP      LLL
FFF      RRR      RRR      EEEEEEEEE Q*REGENTS*Q 1111      222      PPP      LLLLLLLLLL
FFF      RRR      RRR      EEEEEEEEE Q*1988*Q QQQ 11111111 2222222222 PPP      LLLLLLLLLL
    
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FREQ12PL

1. A TYPE 0 PRIORITY LANE BETWEEN SUBSECTIONS 9 AND 14 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 62
 LOWER LIMB (AT V/C=1) = 30
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

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**
** SUB NO.   SSEC  SSEC  DESIGN  ORG  TRK  SSEC  PCT  PCT  DES  SPECIAL  FF.SPD.  CAP.  ART  GRADE  SUBSECTION LOCATION
** SEC LNS   CAP   LENGTH SPEED  DES  FAC  GRAD  TRK  TRUCKS  RAMP   ALT. RTE  ALT. RTE  TYPE ALT. RTE
**
*****
**
** 1
**
** 2
**
** 3
**
** 4
**
** 5
**
** 6
**
** 7
**
** 8
**
** 9 1 1650.   800.   62    0  0.95  0.0  0  100   YES   0.0     0.    GOOD  0.0  Mathilda / Persian HOV
**
** 10 1 1650.  1400.  62    D  0.95  0.0  0  100   NO    0.0     0.    GOOD  0.0  Persian On-Ramp w/HOV
**
** 11 1 1650.  1400.  62    0.95  0.0  0  100   NO    0.0     0.    GOOD  0.0  West of Lawrence E
**
    
```

```

**
** 12 1 1650. 1500. 62 D 0.95 0.0 0 100 NO 0.0 0.0 GOOD 0.0 Lawrence Off-ramp
**
** 13 1 1650. 1500. 62 D 0.95 0.0 0 100 NO 0.0 0.0 GOOD 0.0 End of DKS
**
** 14 1 1650. 10000. 62 D 0.95 0.0 0 100 NO 0.0 0.0 GOOD 0.0 HOV Dummy
**
** 15
**

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FREeway AND ARTERIAL DESIGN FEATURES

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| SUB NO. | SEC | LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT DES TRUCKS | SPECIAL RAMP | FF SPD ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION | LOCATION |
|---------|------|----------|-----------|-------------|--------------|---------|---------|-----------|---------|----------------|--------------|-----------------|---------------|----------|---------------------------|------------|----------|
| ** 1 | ** 2 | ** 4000. | ** 1000. | ** 62 | ** 0 | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** NO | ** 0.0 | ** 0.0 | ** GOOD | ** 0.0 | ** Seeding | ** | ** |
| ** 2 | ** 3 | ** 4401. | ** 1000. | ** 62 | ** OD | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** YES | ** 0.0 | ** 0.0 | ** GOOD | ** 0.0 | ** Maude/US-101 | ** | ** |
| ** 3 | ** 2 | ** 4000. | ** 940. | ** 62 | ** 0 | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** NO | ** 0.0 | ** 0.0 | ** GOOD | ** 0.0 | ** US101SB / US101SB | ** | ** |
| ** 4 | ** 3 | ** 4840. | ** 700. | ** 62 | ** 0 | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** YES | ** 0.0 | ** 0.0 | ** GOOD | ** 0.0 | ** US101 SB On-ramp | ** | ** |
| ** 5 | ** 3 | ** 4840. | ** 700. | ** 62 | ** 0 | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** YES | ** 0.0 | ** 0.0 | ** GOOD | ** 0.0 | ** US 101 / Mathilda | ** | ** |
| ** 6 | ** 3 | ** 4840. | ** 700. | ** 62 | ** D | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** YES | ** 0.0 | ** 0.0 | ** GOOD | ** 0.0 | ** Mathilda Off-ramp | ** | ** |
| ** 7 | ** 2 | ** 4000. | ** 2300. | ** 62 | ** 0 | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** NO | ** 0.0 | ** 0.0 | ** GOOD | ** 0.0 | ** Mathilda / Mathilda | ** | ** |
| ** 8 | ** 2 | ** 4000. | ** 700. | ** 62 | ** OD | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** YES | ** 0.0 | ** 0.0 | ** GOOD | ** 0.0 | ** Mathilda On-Ramp | ** | ** |
| ** 9 | ** 2 | ** 4000. | ** 800. | ** 62 | ** 0 | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** YES | ** 0.0 | ** 0.0 | ** GOOD | ** 0.0 | ** Mathilda / Persian HOV | ** | ** |
| ** 10 | ** 2 | ** 4000. | ** 1400. | ** 62 | ** D | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** NO | ** 0.0 | ** 0.0 | ** GOOD | ** 0.0 | ** Persian On-Ramp w/HOV | ** | ** |
| ** 11 | ** 2 | ** 4000. | ** 1400. | ** 62 | ** 0 | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** NO | ** 0.0 | ** 0.0 | ** GOOD | ** 0.0 | ** West of Lawrence E | ** | ** |
| ** 12 | ** 2 | ** 4000. | ** 1500. | ** 62 | ** D | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** NO | ** 0.0 | ** 0.0 | ** GOOD | ** 0.0 | ** Lawrence Off-ramp | ** | ** |
| ** 13 | ** 2 | ** 4000. | ** 1500. | ** 62 | ** D | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** NO | ** 0.0 | ** 0.0 | ** GOOD | ** 0.0 | ** End of DKS | ** | ** |
| ** 14 | ** 2 | ** 4000. | ** 10000. | ** 62 | ** D | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** NO | ** 0.0 | ** 0.0 | ** GOOD | ** 0.0 | ** HOV Dummy | ** | ** |
| ** 15 | ** 3 | ** 5600. | ** 750. | ** 62 | ** OD | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** NO | ** 0.0 | ** 0.0 | ** GOOD | ** 0.0 | ** End of the network | ** | ** |

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FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ      1111      222222      PPPPPPPP      LLL
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A.D.MAY*Q  111111    222 222    PPPPPPPP    LLL
FFF      RRR   RRR   EEE      QQQQ      QQQQ      1111    222 222    PPP   PPP    LLL
FFF      RRR   RRR   EEE      QQQQ      QQQQ      1111    222 222    PPP   PPP    LLL
FFFFFFF  RRRRRRRR EEEEEEEE QQQQ      QQQQ      1111    222 222    PPPPPPPP    LLL
FFFFFFF  RRRRRRRR EEEEEEEE QQQQ      QQQQ      1111    2222    PPPPPPPP    LLL
FFF      RRR   RRR   EEE      QQQQ      QQQ QQQQ    1111    2222    PPP      LLL
FFF      RRR   RRR   EEE      Q*UC*      QQQQ      1111    222 222    PPP      LLL
FFF      RRR   RRR   EEEEEEEEE Q*REGENTS*Q  1111    222 222    PPP      LLLLLLLLLL
FFF      RRR   RRR   EEEEEEEEE Q*1988*Q QQQ  11111111 2222222222 PPP      LLLLLLLLLL
    
```

FREQ12PL

1. A TYPE 0 PRIORITY LANE BETWEEN SUBSECTIONS 9 AND 14 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 62
 LOWER LIMB (AT V/C=1) = 30
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

```

*****
**
**          FREEWAY TRAVEL TIME (MINUTES)
**
*****
    
```

```

*****
* ORIGINS          DESTINATIONS ACROSS
* DOWN
*      1      2      3      4      5      6      7      8
+
* *****
* *
+
* 1 *  0.00  0.00  0.00  0.00  0.00  0.00  0.00  0.00
+
* 2 *  0.00  0.00  0.00  0.00  0.00  0.00  0.00  0.00
+
* 3 *  0.00  0.00  0.00  0.00  0.00  0.00  0.00  0.00
+
* 4 *  0.00  0.00  0.00  0.00  0.00  0.00  0.00  0.00
+
* 5 *  0.00  0.00  0.00  0.00  0.00  0.00  2.90  0.00
+
* 6 *  0.00  0.00  0.00  0.00  0.00  0.00  0.00  0.00
+
* *
* *****
    
```


| | | | | | | | | | | | | | |
|---|---|---|---|------|------|------|------|------|------|------|------|------|------|
| + | * | 3 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * | 4 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * | 5 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.90 | 0.00 | 0.00 |
| + | * | 6 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * | * | * | | | | | | | | | | |

*
* TIME SLICE FREEWAY PERFORMANCE TABLE *
*

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | | |
|-----------|--------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|-------|----------|-----------|---------|--------|-------------|---------|-------|---------|--|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | |
| * 1 | | | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | | | |
| * 3 | | | | | | | | | | | | | | | | | | | |
| * 4 | | | | | | | | | | | | | | | | | | | |
| * 5 | | | | | | | | | | | | | | | | | | | |
| * 6 | | | | | | | | | | | | | | | | | | | |
| * 7 | | | | | | | | | | | | | | | | | | | |
| * 8 | | | | | | | | | | | | | | | | | | | |
| * 9 | 1 | 800. | 302. | 0. | 302. | 302. | 0. | 302. | 1650. | 0. | 0. | 0. | .18 | 65. | 4.6 | A | 20.0 | 13.7 | |
| * 10 | 1 | 1400. | 0. | 0. | 302. | 0. | 0. | 302. | 1650. | 0. | 0. | 0. | .18 | 65. | 4.6 | A | 20.0 | 13.7 | |
| * 11 | 1 | 1400. | 0. | 0. | 302. | 0. | 0. | 302. | 1650. | 0. | 0. | 0. | .18 | 65. | 4.6 | A | 20.0 | 13.7 | |
| * 12 | 1 | 1500. | 0. | 0. | 302. | 0. | 0. | 302. | 1650. | 0. | 0. | 0. | .18 | 65. | 4.6 | A | 20.0 | 13.7 | |
| * 13 | 1 | 1500. | 0. | 0. | 302. | 0. | 0. | 302. | 1650. | 0. | 0. | 0. | .18 | 65. | 4.6 | A | 20.0 | 13.7 | |
| * 14 | 1 | 10000. | 0. | 302. | 302. | 0. | 302. | 302. | 1650. | 0. | 0. | 0. | .18 | 65. | 4.6 | A | 20.0 | 13.7 | |
| * 15 | | | | | | | | | | | | | | | | | | | |

* TOTAL 16600. = 3.1 MILES MAX(V/C) = 0.18 LOWEST LOS = A AVG = 65. 4.6 20.0 13.7 *

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 15. VEH-HRS | 25. VEH-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 15. VEH-HRS | 25. VEH-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 948. VEH-MI. | 1896. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 65. MPH. | 65. MPH. |
| AVERAGE DENSITY = | 5. VPMP | 4. VPMP |
| TOTAL FUEL = | 47. GALLONS | 83. GALLONS |
| TOTAL EMISSIONS = | 13. KILOGRAMS | 23. KILOGRAMS |
| | 29. PASS-HRS | 51. PASS-HRS |
| | 0. PASS-HRS | 0. PASS-HRS |
| | 0. PASS-HRS | 0. PASS-HRS |
| | 0. PASS-HRS | 0. PASS-HRS |
| | 29. PASS-HRS | 51. PASS-HRS |
| | 1896. PASS-MI. | 3309. PASS-MI. |

***** MAI NLINE DELAY (VEH-HRS) ***** DESI RED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTI ON | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|-------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

**
**

** FREeway TRAVEL TIME (MINUTES) **
 ** **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|--|-----------------------|------|-------|-------|-------|-------|------|-------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | | 9.41 | 9.94 | 10.46 | 10.85 | 11.35 | 11.62 | 0.00 | 13.50 |
| * 2 * | | 0.17 | 0.71 | 1.23 | 1.62 | 2.12 | 2.39 | 0.00 | 4.27 |
| * 3 * | | 0.00 | 0.37 | 0.89 | 1.28 | 1.78 | 2.05 | 0.00 | 3.93 |
| * 4 * | | 0.00 | 0.00 | 0.12 | 0.51 | 1.02 | 1.28 | 0.00 | 3.16 |
| * 5 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 6 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.13 |

 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | |
|-----------|----------|------------|------------|--------------------|--------|-------------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|------|
| * SEC LNS | * LENGTH | * ORG | * DES SSEC | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | |
| * 1 | 2 | 52800. | 2499. | 0. 2499. | 2499. | 0. 2499. | 4000. | 0. | 0. | .62 | 65. | 19.2 | C | 19.0 | 14.1 |
| * 2 | 3 | 1000. | 219. | 850. 2718. | 219. | 850. 2718. | 4401. | 0. | 0. | .62 | 65. | 13.9 | B | 19.0 | 14.1 |
| * 3 | 2 | 940. | 0. | 0. 1868. | 0. | 0. 1868. | 4000. | 0. | 0. | .47 | 65. | 14.4 | B | 19.0 | 14.1 |
| * 4 | 3 | 700. | 1520. | 0. 3388. | 1520. | 0. 3388. | 4840. | 0. | 0. | .70 | 65. | 17.4 | B | 19.0 | 14.1 |
| * 5 | 3 | 700. | 0. | 0. 3388. | 0. | 0. 3388. | 4840. | 0. | 0. | .70 | 65. | 17.4 | B | 19.0 | 14.1 |
| * 6 | 3 | 700. | 0. | 660. 3388. | 0. | 660. 3388. | 4840. | 0. | 0. | .70 | 65. | 17.4 | B | 19.0 | 14.1 |
| * 7 | 2 | 2300. | 0. | 0. 2728. | 0. | 0. 2728. | 4000. | 0. | 0. | .68 | 65. | 21.0 | C | 19.0 | 14.1 |
| * 8 | 2 | 700. | 459. | 225. 3187. | 459. | 225. 3187. | 4400. | 0. | 0. | .72 | 65. | 24.7 | C | 19.2 | 13.9 |
| * 9 | 2 | 800. | 0. | 0. 2962. | 0. | 0. 2962. | 4400. | 0. | 0. | .67 | 65. | 22.8 | C | 19.0 | 14.0 |
| * 10 | 2 | 1400. | 0. | 189. 2962. | 0. | 189. 2962. | 4400. | 0. | 0. | .67 | 65. | 22.8 | C | 19.0 | 14.0 |
| * 11 | 2 | 1400. | 0. | 0. 2773. | 0. | 0. 2773. | 4000. | 0. | 0. | .69 | 65. | 21.3 | C | 19.0 | 14.1 |
| * 12 | 2 | 1500. | 0. | 189. 2773. | 0. | 189. 2773. | 4000. | 0. | 0. | .69 | 65. | 21.3 | C | 19.0 | 14.1 |
| * 13 | 2 | 1500. | 0. | 0. 2584. | 0. | 0. 2584. | 4000. | 0. | 0. | .65 | 65. | 19.9 | C | 19.0 | 14.1 |
| * 14 | 2 | 10000. | 0. | 0. 2584. | 0. | 0. 2584. | 4000. | 0. | 0. | .65 | 65. | 19.9 | C | 19.0 | 14.1 |
| * 15 | 3 | 750. | 225. | 2809. 2809. | 225. | 2809. 2809. | 5600. | 0. | 0. | .50 | 65. | 14.4 | B | 19.0 | 14.1 |

* TOTAL 77190. = 14.6 MILES MAX(V/C) = 0.72 LOWEST LOS = C AVG = 65. 19.4 19.0 14.1 *

| | CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | |
|-----------------------------|--------------------|------------|--------|----------|-------------------|------------|--------|----------|
| FREeway TRAVEL TIME = | 578. | VEH-HRS | 614. | PASS-HRS | 578. | VEH-HRS | 614. | PASS-HRS |
| FREeway MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 578. | VEH-HRS | 614. | PASS-HRS | 578. | VEH-HRS | 614. | PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 37581. | VEH-MI. | 39937. | PASS-MI. | 37581. | VEH-MI. | 39937. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 65. | MPH. | | | 65. | MPH. | | |
| AVERAGE DENSITY = | 19. | VPMP | | | 19. | VPMP | | |
| TOTAL FUEL = | 1980. | GALLONS | | | 1980. | GALLONS | | |
| TOTAL EMISSIONS = | 528. | KI LOGRAMS | | | 528. | KI LOGRAMS | | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.05 | 9 | 0.01 | 10 | 0.02 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |

***** TOTAL DELAY = 0.1 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 10/20/2015 17: 5 PAGE 11
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF NON-PRIORITY LANES
 TIME SLICE 2 OF 2

 ** **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 ** **

| ORIGINS | DESTINATIONS ACROSS | | | | | | | |
|---------|---------------------|-------|-------|-------|-------|-------|------|-------|
| DOWN | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| 1 | 10.00 | 10.53 | 11.11 | 11.53 | 12.10 | 12.38 | 0.00 | 14.39 |
| 2 | 0.17 | 0.71 | 1.28 | 1.71 | 2.28 | 2.56 | 0.00 | 4.56 |
| 3 | 0.00 | 0.37 | 0.94 | 1.37 | 1.94 | 2.22 | 0.00 | 4.22 |
| 4 | 0.00 | 0.00 | 0.14 | 0.57 | 1.14 | 1.42 | 0.00 | 3.42 |
| 5 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.13 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 10/20/2015 17: 5 PAGE 12
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF NON-PRIORITY LANES
 TIME SLICE 2 OF 2

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS | | | |
|---------|------|----------|--------------|------------------|-------|-------------|---------|---------|-------|-------|---------|-------|------|--------|---|------|------|
| SEC | LN | LENGTH | ORG DES SSEC | ORG DES SSEC | CAP. | EFF | LENGTH | RATE | RATIO | MPH | VP/MP | LEVEL | MPG | GS/VM | | | |
| 1 | 2 | 52800. | 3441. | 0. 3441. | 3441. | 0. | 3441. | 4000. | 0. | 0. | 0. | .86 | 61. | 28.2 | D | 20.8 | 12.7 |
| 2 | 3 | 1000. | 400. | 1200. 3841. | 400. | 1200. 3841. | 4401. | 0. | 0. | 0. | 0. | .87 | 65. | 19.7 | C | 19.0 | 14.1 |
| 3 | 2 | 940. | 0. | 0. 2641. | 0. | 0. 2641. | 4000. | 0. | 0. | 0. | 0. | .66 | 65. | 20.3 | C | 19.0 | 14.1 |
| 4 | 3 | 700. | 1700. | 0. 4341. | 1700. | 0. 4341. | 4840. | 0. | 0. | 0. | 0. | .90 | 65. | 22.3 | C | 19.0 | 14.1 |
| 5 | 3 | 700. | 0. | 0. 4341. | 0. | 0. 4341. | 4840. | 0. | 0. | 0. | 0. | .90 | 65. | 22.3 | C | 19.0 | 14.1 |
| 6 | 3 | 700. | 0. | 840. 4341. | 0. | 840. 4341. | 4840. | 0. | 0. | 0. | 0. | .90 | 65. | 22.3 | C | 19.0 | 14.1 |
| 7 | 2 | 2300. | 0. | 0. 3501. | 0. | 0. 3501. | 4000. | 0. | 0. | 0. | 0. | .88 | 60. | 29.0 | D | 21.1 | 12.5 |
| 8 | 2 | 700. | 750. | 302. 4251. | 750. | 302. 4251. | 4400. | 0. | 0. | 0. | 0. | .97 | 55. | 38.7 | E | 22.9 | 11.4 |
| 9 | 2 | 800. | 0. | 0. 3949. | 0. | 0. 3949. | 4400. | 0. | 0. | 0. | 0. | .90 | 59. | 33.3 | D | 21.6 | 12.2 |
| 10 | 2 | 1400. | 0. | 220. 3949. | 0. | 220. 3949. | 4400. | 0. | 0. | 0. | 0. | .90 | 59. | 33.3 | D | 21.6 | 12.2 |
| 11 | 2 | 1400. | 0. | 0. 3729. | 0. | 0. 3729. | 4000. | 0. | 0. | 0. | 0. | .93 | 57. | 32.5 | D | 22.1 | 11.9 |
| 12 | 2 | 1500. | 0. | 261. 3729. | 0. | 261. 3729. | 4000. | 0. | 0. | 0. | 0. | .93 | 57. | 32.5 | D | 22.1 | 11.9 |
| 13 | 2 | 1500. | 0. | 0. 3468. | 0. | 0. 3468. | 4000. | 0. | 0. | 0. | 0. | .87 | 61. | 28.5 | D | 21.0 | 12.6 |
| 14 | 2 | 10000. | 0. | 0. 3468. | 0. | 0. 3468. | 4000. | 0. | 0. | 0. | 0. | .87 | 61. | 28.5 | D | 21.0 | 12.6 |
| 15 | 3 | 750. | 302. | 3770. 3770. | 302. | 3770. 3770. | 5600. | 0. | 0. | 0. | 0. | .67 | 65. | 19.3 | C | 19.0 | 14.1 |

TOTAL 77190. = 14.6 MILES MAX(V/C) = 0.97 LOWEST LOS = E AVG = 61. 28.2 20.8 12.7

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|----------------------------|--------------------|---------------|-------------------|----------------|
| FREEWAY TRAVEL TIME = | 840. VEH-HRS | 893. PASS-HRS | 1418. VEH-HRS | 1507. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 840. VEH-HRS | 893. PASS-HRS | 1418. VEH-HRS | 1507. PASS-HRS |

| | | | | |
|-----------------------------|-----------------|------------------|-----------------|------------------|
| TOTAL FRWAY TRAV DISTANCE = | 51207. VEH-MI . | 54431. PASS-MI . | 88787. VEH-MI . | 94368. PASS-MI . |
| AVERAGE SYSTEM SPEED = | 61. MPH. | | 63. MPH. | |
| AVERAGE DENSITY = | 28. VPMP/L | | 24. VPMP/L | |
| TOTAL FUEL = | 2462. GALLONS | | 4443. GALLONS | |
| TOTAL EMISSIONS = | 652. KILOGRAMS | | 1181. KILOGRAMS | |

```

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION  DELAY  SUBSECTION  DELAY  SUBSECTION  DELAY  SUBSECTION  DELAY  SUBSECTION  DELAY
      1      34.02       2         0.00       3         0.00       4         0.00       5         0.00
      6         0.00       7         1.78       8         1.58       9         0.88      10         1.55
     11         2.05      12         2.19      13         1.05      14         7.01      15         0.00
***** TOTAL DELAY = 52.1 VEH-HRS ***** AVERAGE DELAY = 0.89 MIN/VEH *****
  
```

```

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ      1111      222222      PPPPPPPP      LLL
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A.D.MAY*Q 111111    222 222    PPPPPPPP    LLL
FFF      RRR      RRR      EEE      QQQQ      QQQQ      1111    222 222    PPP      PPP    LLL
FFF      RRR      RRR      EEE      QQQQ      QQQQ      1111    222 222    PPP      PPP    LLL
FFFFFFF  RRRRRRRR EEEEEEEE  QQQQ      QQQQ      1111    222 222    PPPPPPPP    LLL
FFFFFFF  RRRRRRRR EEEEEEEE  QQQQ      QQQQ      1111    2222    PPPPPPPP    LLL
FFF      RRR      RRR      EEE      QQQQ      QQQ QQQQ    1111    2222    PPP      LLL
FFF      RRR      RRR      EEE      Q*UC*      QQQQ      1111    222 222    PPP      LLL
FFF      RRR      RRR      EEEEEEEEE Q*REGENTS*Q 1111    222 222    PPP      LLLLLLLLLL
FFF      RRR      RRR      EEEEEEEEE Q*1988*Q QQQ 11111111 2222222222 PPP      LLLLLLLLLL
    
```

FREQ12PL

1. A TYPE 0 PRIORITY LANE BETWEEN SUBSECTIONS 9 AND 14 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 62
 LOWER LIMB (AT V/C=1) = 30
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

```

*****
*****
**
**
**
*****
*****
**
** SUB NO.   SSEC  SSEC  DESIGN  ORG  TRK  SSEC  PCT  PCT  DES  SPECIAL  FF.SPD.  CAP.  ART  GRADE  SUBSECTION LOCATION
** SEC LNS   CAP   LENGTH SPEED  DES  FAC  GRAD  TRK  TRUCKS  RAMP   ALT. RTE  ALT. RTE  TYPE ALT. RTE
**
*****
**
** 1
**
** 2
**
** 3
**
** 4
**
** 5
**
** 6
**
** 7
**
** 8
**
** 9 1 1650.   800.   62    0  0.95  0.0  0  100   YES   0.0     0.    GOOD  0.0  Mathilda / Persian HOV
**
** 10 1 1650.  1400.  62    D  0.95  0.0  0  100   NO    0.0     0.    GOOD  0.0  Persian On-Ramp w/HOV
**
** 11 1 1650.  1400.  62    0.95  0.0  0  100   NO    0.0     0.    GOOD  0.0  West of Lawrence E
**
    
```

```

** 12 1 1650. 1500. 62 D 0.95 0.0 0 100 NO 0.0 0.0 GOOD 0.0 Lawrence Off-ramp **
** 13 1 1650. 1500. 62 D 0.95 0.0 0 100 NO 0.0 0.0 GOOD 0.0 End of DKS **
** 14 1 1650. 10000. 62 D 0.95 0.0 0 100 NO 0.0 0.0 GOOD 0.0 HOV Dummy **
** 15 **

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*****

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*****
*****

```

FREEWAY AND ARTERIAL DESIGN FEATURES

```

*****
** SUB NO. SSEC SSEC DESIGN ORG TRK SSEC PCT PCT DES SPECIAL FF SPD CAP. ART GRADE SUBSECTION LOCATION **
** SEC LNS CAP LENGTH SPEED DES FAC GRAD TRK TRUCKS RAMP ALT. RTE ALT. RTE TYPE ALT. RTE **
** 1 2 4000. 1000. 62 0 0.95 0.0 5 0 NO 0.0 0.0 GOOD 0.0 Seeding **
** 2 3 4630. 1000. 62 OD 0.95 0.0 5 0 YES 0.0 0.0 GOOD 0.0 Maude/US-101 **
** 3 2 4000. 940. 62 0.95 0.0 5 0 NO 0.0 0.0 GOOD 0.0 US101SB / US101SB **
** 4 3 4390. 700. 62 0 0.95 0.0 5 0 YES 0.0 0.0 GOOD 0.0 US101 SB On-ramp **
** 5 3 4390. 700. 62 0.95 0.0 5 0 YES 0.0 0.0 GOOD 0.0 US 101 / Mathilda **
** 6 3 4390. 700. 62 D 0.95 0.0 5 0 YES 0.0 0.0 GOOD 0.0 Mathilda Off-ramp **
** 7 2 4000. 2300. 62 0.95 0.0 5 0 NO 0.0 0.0 GOOD 0.0 Mathilda / Mathilda **
** 8 2 4000. 700. 62 OD 0.95 0.0 5 0 YES 0.0 0.0 GOOD 0.0 Mathilda On-Ramp **
** 9 2 4000. 800. 62 0 0.95 0.0 5 0 YES 0.0 0.0 GOOD 0.0 Mathilda / Persian HOV **
** 10 2 4000. 1400. 62 D 0.95 0.0 5 0 NO 0.0 0.0 GOOD 0.0 Persian On-Ramp w/HOV **
** 11 2 4000. 1400. 62 0.95 0.0 5 0 NO 0.0 0.0 GOOD 0.0 West of Lawrence E **
** 12 2 4000. 1500. 62 D 0.95 0.0 5 0 NO 0.0 0.0 GOOD 0.0 Lawrence Off-ramp **
** 13 2 4000. 1500. 62 D 0.95 0.0 5 0 NO 0.0 0.0 GOOD 0.0 End of DKS **
** 14 2 4000. 10000. 62 D 0.95 0.0 5 0 NO 0.0 0.0 GOOD 0.0 HOV Dummy **
** 15 3 5600. 750. 62 OD 0.95 0.0 5 0 NO 0.0 0.0 GOOD 0.0 End of the network **

```

```

*****
*****

```

```

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ      1111      222222      PPPPPPPP      LLL
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A.D.MAY*Q 111111    222 222    PPPPPPPP    LLL
FFF      RRR      RRR      EEE      QQQQ      QQQQ      1111    222 222    PPP      PPP    LLL
FFF      RRR      RRR      EEE      QQQQ      QQQQ      1111    222 222    PPP      PPP    LLL
FFFFFFF  RRRRRRRR EEEEEEEE  QQQQ      QQQQ      1111    222 222    PPPPPPPP    LLL
FFFFFFF  RRRRRRRR EEEEEEEE  QQQQ      QQQQ      1111    222 222    PPPPPPPP    LLL
FFF      RRR      RRR      EEE      QQQQ      QQQQ      1111    222 222    PPP      PPP    LLL
FFF      RRR      RRR      EEE      Q*UC*      QQQQ      1111    222 222    PPP      PPP    LLL
FFF      RRR      RRR      EEEEEEEEE Q*REGENTS*Q 1111    222 222    PPP      PPP    LLLLLLLLLL
FFF      RRR      RRR      EEEEEEEEE Q*1988*Q QQQ 11111111 2222222222 PPP      PPP    LLLLLLLLLL
    
```

FREQ12PL

1. A TYPE 0 PRIORITY LANE BETWEEN SUBSECTIONS 9 AND 14 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 62
 LOWER LIMB (AT V/C=1) = 30
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

```

*****
**
**          FREEWAY TRAVEL TIME (MINUTES)
**
*****
    
```

```

*****
* ORIGINS          DESTINATIONS ACROSS
* DOWN
*      1      2      3      4      5      6      7      8
+
* *****
* *
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 2 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 3 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 4 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 5 * 0.00 0.00 0.00 0.00 0.00 0.00 3.04 0.00
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* *
* *****
    
```


** FREEWAY TRAVEL TIME (MINUTES) **
 ** **

```

*****
* ORIGINS          DESTINATIONS ACROSS          *
* DOWN            1       2       3       4       5       6       7       8          *
* *****
* *
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  *
* 2 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  *
* 3 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  *
* 4 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  *
* 5 * 0.00 0.00 0.00 0.00 0.00 0.00 3.04 0.00  *
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00  *
* *
* *****
  
```

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB NO. | * SSEC | * O-D DATA DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | | | | | |
|-----------|--------|--------------------|--------------------|----------------|---------|-----------|-----------|----------|---------|-----------|----------|---------|-------------|---------|-----|---|------|------|------|------|
| * SEC | * LNS | * LENGTH | * ORG DES SSEC | * ORG DES SSEC | * CAP | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP L | * LEVEL | * MPG | * GS/VM | | | | | | |
| * 1 | | | | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | | | | |
| * 3 | | | | | | | | | | | | | | | | | | | | |
| * 4 | | | | | | | | | | | | | | | | | | | | |
| * 5 | | | | | | | | | | | | | | | | | | | | |
| * 6 | | | | | | | | | | | | | | | | | | | | |
| * 7 | | | | | | | | | | | | | | | | | | | | |
| * 8 | | | | | | | | | | | | | | | | | | | | |
| * 9 | 1 | 800. | 559. | 0. | 559. | 559. | 0. | 559. | 1650. | 0. | 0. | 0. | .34 | 62. | 9.0 | A | 21.6 | 12.8 | | |
| * 10 | 1 | 1400. | 0. | 0. | 559. | 0. | 0. | 559. | 1650. | 0. | 0. | 0. | .34 | 62. | 9.0 | A | 21.6 | 12.8 | | |
| * 11 | 1 | 1400. | 0. | 0. | 559. | 0. | 0. | 559. | 1650. | 0. | 0. | 0. | .34 | 62. | 9.0 | A | 21.6 | 12.8 | | |
| * 12 | 1 | 1500. | 0. | 0. | 559. | 0. | 0. | 559. | 1650. | 0. | 0. | 0. | .34 | 62. | 9.0 | A | 21.6 | 12.8 | | |
| * 13 | 1 | 1500. | 0. | 0. | 559. | 0. | 0. | 559. | 1650. | 0. | 0. | 0. | .34 | 62. | 9.0 | A | 21.6 | 12.8 | | |
| * 14 | 1 | 10000. | 0. | 559. | 559. | 0. | 559. | 559. | 1650. | 0. | 0. | 0. | .34 | 62. | 9.0 | A | 21.6 | 12.8 | | |
| * 15 | | | | | | | | | | | | | | | | | | | | |
| * TOTAL | | 16600. | = | 3.1 | MILES | | | MAX(V/C) | = | 0.34 | LOWEST | LOS | = | A | AVG | = | 62. | 9.0 | 21.6 | 12.8 |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 28. VEH-HRS | 57. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 28. VEH-HRS | 57. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 1757. VEH-MI. | 3515. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 62. MPH. |
| AVERAGE DENSITY = | 9. VPMP L | 11. VPMP L |
| TOTAL FUEL = | 82. GALLONS | 305. GALLONS |
| TOTAL EMISSIONS = | 22. KI LOGRAMS | 84. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

TOTAL FRWAY TRAV DISTANCE = 11149. VEH-MI . 12294. PASS-MI . 11149. VEH-MI . 12294. PASS-MI .
 AVERAGE SYSTEM SPEED = 63. MPH. 63. MPH.
 AVERAGE DENSITY = 17. VPMLP 17. VPMLP
 TOTAL FUEL = 561. GALLONS 561. GALLONS
 TOTAL EMISSIONS = 149. KILOGRAMS 149. KILOGRAMS

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 10/20/2015 16:51 PAGE 13
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF NON-PRIORITY LANES
 TIME SLICE 1 OF 3

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.33 | 9 | 0.29 | 10 | 0.51 |
| 11 | 0.47 | 12 | 0.51 | 13 | 0.45 | 14 | 3.02 | 15 | 0.00 |

***** TOTAL DELAY = 5.6 VEH-HRS ***** AVERAGE DELAY = 0.15 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 10/20/2015 16:51 PAGE 14
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF NON-PRIORITY LANES
 TIME SLICE 2 OF 3

 **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN 1 2 3 4 5 6 7 8 *

 * * *
 * 1 * 0.35 0.88 1.42 1.82 2.35 2.63 0.00 4.59 *
 * 2 * 0.17 0.71 1.24 1.64 2.18 2.45 0.00 4.41 *
 * 3 * 0.00 0.37 0.90 1.30 1.84 2.11 0.00 4.08 *
 * 4 * 0.00 0.00 0.13 0.54 1.07 1.34 0.00 3.31 *
 * 5 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
 * 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.13 *
 * * *

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 10/20/2015 16:51 PAGE 15
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF NON-PRIORITY LANES
 TIME SLICE 2 OF 3

 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | |
|-----------|--------|------------|-----------|------------|-----------|---------|---------|-----------|-----------|-------|----------|-----------|---------|--------|-------------|---------|--------|---------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMLP | * LEVEL | * MPG | * GS/VM |
| * 1 | * 2 | * 1000. | * 2060. | * 0. | * 2060. | * 2060. | * 0. | * 2060. | * 4000. | * 0. | * 0. | * 0. | * .51 | * 65. | * 15.8 | * B | * 19.0 | * 14.1 |
| * 2 | * 3 | * 1000. | * 729. | * 650. | * 2789. | * 729. | * 650. | * 2789. | * 4630. | * 0. | * 0. | * 0. | * .60 | * 65. | * 14.3 | * B | * 19.0 | * 14.1 |
| * 3 | * 2 | * 940. | * 0. | * 0. | * 2139. | * 0. | * 0. | * 2139. | * 4000. | * 0. | * 0. | * 0. | * .53 | * 65. | * 16.5 | * B | * 19.0 | * 14.1 |
| * 4 | * 3 | * 700. | * 711. | * 0. | * 2850. | * 711. | * 0. | * 2850. | * 4390. | * 0. | * 0. | * 0. | * .65 | * 65. | * 14.6 | * B | * 19.0 | * 14.1 |
| * 5 | * 3 | * 700. | * 0. | * 0. | * 2850. | * 0. | * 0. | * 2850. | * 4390. | * 0. | * 0. | * 0. | * .65 | * 65. | * 14.6 | * B | * 19.0 | * 14.1 |
| * 6 | * 3 | * 700. | * 0. | * 240. | * 2850. | * 0. | * 240. | * 2850. | * 4390. | * 0. | * 0. | * 0. | * .65 | * 65. | * 14.6 | * B | * 19.0 | * 14.1 |
| * 7 | * 2 | * 2300. | * 0. | * 0. | * 2610. | * 0. | * 0. | * 2610. | * 4000. | * 0. | * 0. | * 0. | * .65 | * 65. | * 20.1 | * C | * 19.0 | * 14.1 |
| * 8 | * 2 | * 700. | * 919. | * 777. | * 3529. | * 919. | * 777. | * 3529. | * 4000. | * 0. | * 0. | * 0. | * .88 | * 60. | * 29.4 | * D | * 21.3 | * 12.4 |
| * 9 | * 2 | * 800. | * 0. | * 0. | * 2752. | * 0. | * 0. | * 2752. | * 4000. | * 0. | * 0. | * 0. | * .69 | * 62. | * 22.2 | * C | * 20.3 | * 13.0 |
| * 10 | * 2 | * 1400. | * 0. | * 319. | * 2752. | * 0. | * 319. | * 2752. | * 4000. | * 0. | * 0. | * 0. | * .69 | * 62. | * 22.2 | * C | * 20.3 | * 13.0 |
| * 11 | * 2 | * 1400. | * 0. | * 0. | * 2433. | * 0. | * 0. | * 2433. | * 4000. | * 0. | * 0. | * 0. | * .61 | * 62. | * 19.6 | * C | * 20.3 | * 13.0 |
| * 12 | * 2 | * 1500. | * 0. | * 220. | * 2433. | * 0. | * 220. | * 2433. | * 4000. | * 0. | * 0. | * 0. | * .61 | * 62. | * 19.6 | * C | * 20.3 | * 13.0 |
| * 13 | * 2 | * 1500. | * 0. | * 0. | * 2213. | * 0. | * 0. | * 2213. | * 4000. | * 0. | * 0. | * 0. | * .55 | * 62. | * 17.8 | * B | * 20.3 | * 13.0 |
| * 14 | * 2 | * 10000. | * 0. | * 0. | * 2213. | * 0. | * 0. | * 2213. | * 4000. | * 0. | * 0. | * 0. | * .55 | * 62. | * 17.8 | * B | * 20.3 | * 13.0 |

```

* 15 3 750. 777. 2990. 2990. 777. 2990. 2990. 5600. 0. 0. 0. .53 65. 15.3 B 19.0 14.1 *
*
*****
* TOTAL 25390. = 4.8 MILES MAX(V/C) = 0.88 LOWEST LOS = D AVG = 63. 18.3 19.9 13.4 *
*
*****

```

```

CURRENT TIME SLICE CUMULATIVE VALUES
FREEWAY TRAVEL TIME = 187. VEH-HRS 206. PASS-HRS 364. VEH-HRS 401. PASS-HRS
FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 187. VEH-HRS 206. PASS-HRS 364. VEH-HRS 401. PASS-HRS
TOTAL FRWAY TRAV DISTANCE = 11764. VEH-MI. 13014. PASS-MI. 22913. VEH-MI. 25308. PASS-MI.
AVERAGE SYSTEM SPEED = 63. MPH. 63. MPH.
AVERAGE DENSITY = 18. VPMPPL 18. VPMPPL
TOTAL FUEL = 591. GALLONS 1152. GALLONS
TOTAL EMISSIONS = 157. KI LOGRAMS 306. KI LOGRAMS

```

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.59 | 9 | 0.31 | 10 | 0.54 |
| 11 | 0.48 | 12 | 0.51 | 13 | 0.47 | 14 | 3.12 | 15 | 0.00 |

***** TOTAL DELAY = 6.0 VEH-HRS ***** AVERAGE DELAY = 0.15 MIN/VEH *****

 **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 **

```

*****
* ORIGINS DESTINATIONS ACROSS *
* DOWN 1 2 3 4 5 6 7 8 *
+
* *****
* *
+
* 1 * 0.35 0.88 1.41 1.81 2.34 2.62 0.00 4.58 *
+
* 2 * 0.17 0.71 1.23 1.63 2.17 2.44 0.00 4.40 *
+
* 3 * 0.00 0.37 0.89 1.29 1.83 2.10 0.00 4.07 *
+
* 4 * 0.00 0.00 0.12 0.53 1.06 1.33 0.00 3.30 *
+
* 5 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.13 *
+
* *
*****

```

 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *

```

* SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMISSIONS *
* SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMPPL LEVEL MPG GS/VM *

```



```

*****
*
* 1 2 1000. 1500. 0. 1500. 1500. 0. 1500. 4000. 0. 0. 0. .38 65. 11.5 B 19.0 14.1 *
* 2 3 1000. 550. 540. 2050. 550. 540. 2050. 4630. 0. 0. 0. .44 65. 10.5 A 19.0 14.1 *
* 3 2 940. 0. 0. 1510. 0. 0. 1510. 4000. 0. 0. 0. .38 65. 11.6 B 19.0 14.1 *
* 4 3 700. 571. 0. 2081. 571. 0. 2081. 4390. 0. 0. 0. .47 65. 10.7 A 19.0 14.1 *
* 5 3 700. 0. 0. 2081. 0. 0. 2081. 4390. 0. 0. 0. .47 65. 10.7 A 19.0 14.1 *
* 6 3 700. 0. 211. 2081. 0. 211. 2081. 4390. 0. 0. 0. .47 65. 10.7 A 19.0 14.1 *
* 7 2 2300. 0. 0. 1870. 0. 0. 1870. 4000. 0. 0. 0. .47 65. 14.4 B 19.0 14.1 *
* 8 2 700. 811. 559. 2681. 811. 559. 2681. 4000. 0. 0. 0. .67 65. 20.6 C 19.0 14.1 *
* 9 2 800. 0. 0. 2122. 0. 0. 2122. 4000. 0. 0. 0. .53 62. 17.1 B 20.3 13.0 *
* 10 2 1400. 0. 271. 2122. 0. 271. 2122. 4000. 0. 0. 0. .53 62. 17.1 B 20.3 13.0 *
* 11 2 1400. 0. 0. 1851. 0. 0. 1851. 4000. 0. 0. 0. .46 62. 14.9 B 20.3 13.0 *
* 12 2 1500. 0. 260. 1851. 0. 260. 1851. 4000. 0. 0. 0. .46 62. 14.9 B 20.3 13.0 *
* 13 2 1500. 0. 0. 1591. 0. 0. 1591. 4000. 0. 0. 0. .40 62. 12.8 B 20.3 13.0 *
* 14 2 10000. 0. 0. 1591. 0. 0. 1591. 4000. 0. 0. 0. .40 62. 12.8 B 20.3 13.0 *
* 15 3 750. 559. 2150. 2150. 559. 2150. 2150. 5600. 0. 0. 0. .38 65. 11.0 B 19.0 14.1 *
*
*
* TOTAL 25390. = 4.8 MI LES MAX(V/C) = 0.67 LOWEST LOS = C AVG = 63. 13.4 19.8 13.4 *
*
*****

```

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|-----------------------------|--------------------|----------------|-------------------|-----------------|
| FREEWAY TRAVEL TIME = | 136. VEH-HRS | 151. PASS-HRS | 501. VEH-HRS | 552. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 136. VEH-HRS | 151. PASS-HRS | 501. VEH-HRS | 552. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 8610. VEH-MI. | 9548. PASS-MI. | 31523. VEH-MI. | 34857. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 63. MPH. | | 63. MPH. | |
| AVERAGE DENSITY = | 13. VPMP/L | | 16. VPMP/L | |
| TOTAL FUEL = | 435. GALLONS | | 1587. GALLONS | |
| TOTAL EMISSIONS = | 116. KILOGRAMS | | 422. KILOGRAMS | |

```

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
   1      0.00     2      0.00     3      0.00     4      0.00     5      0.00
   6      0.00     7      0.00     8      0.00     9      0.24    10      0.42
  11      0.37    12      0.39    13      0.34    14      2.24    15      0.00

***** TOTAL DELAY = 4.0 VEH-HRS ***** AVERAGE DELAY = 0.14 MIN/VEH *****

```

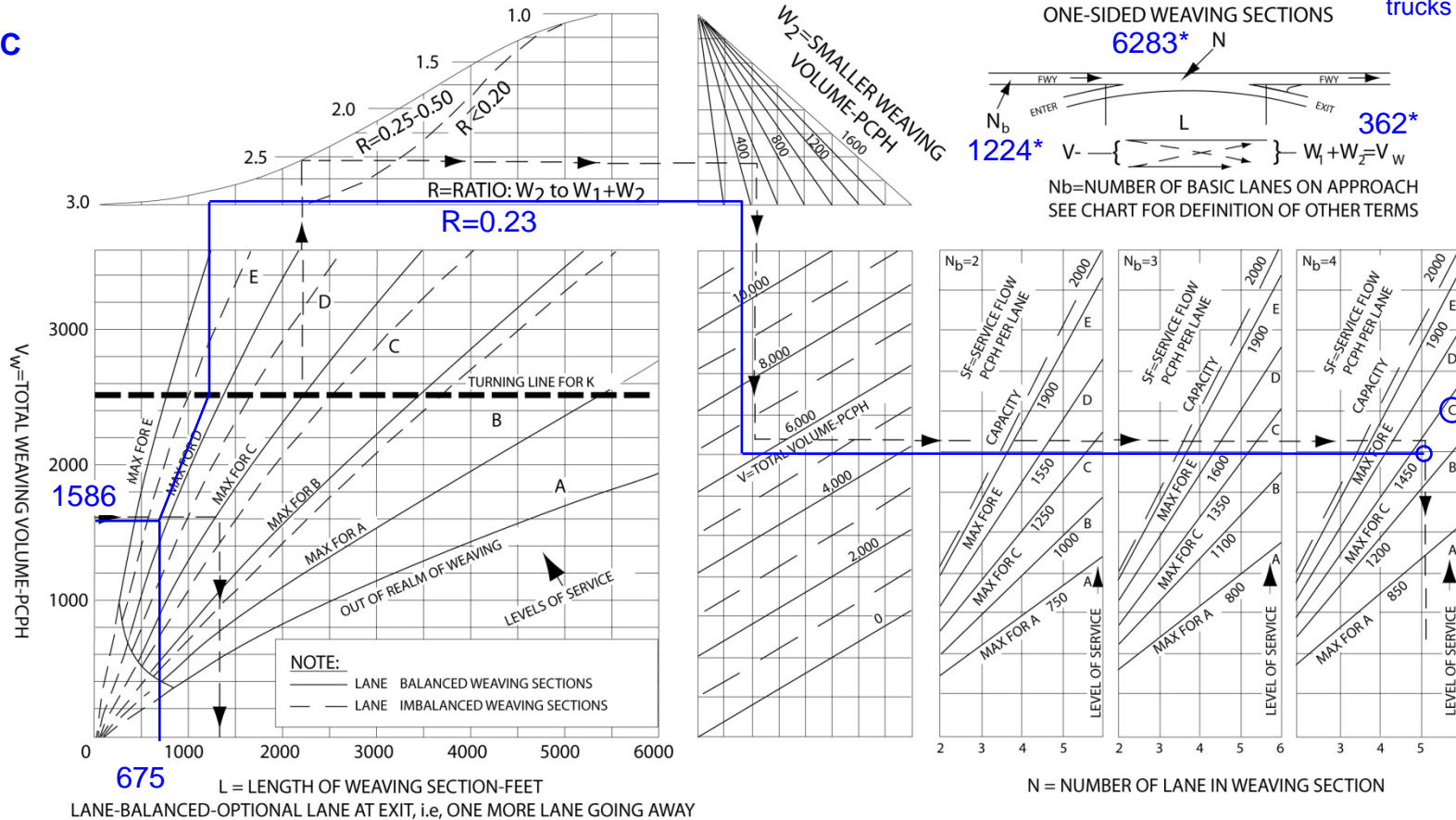
APPENDIX G – EXISTING LEISCH WEAVING ANALYSIS SHEETS



US 101, Southbound
 On: SR 237
 Off: Mathilda Ave
 Existing AM (8-9)

1 HOV (dashed) + 3 Mix
 1 Aux lane
 Imbalanced

LOS: C



Design Curve for Freeway and Collector Weaving
 Figure 504.7A

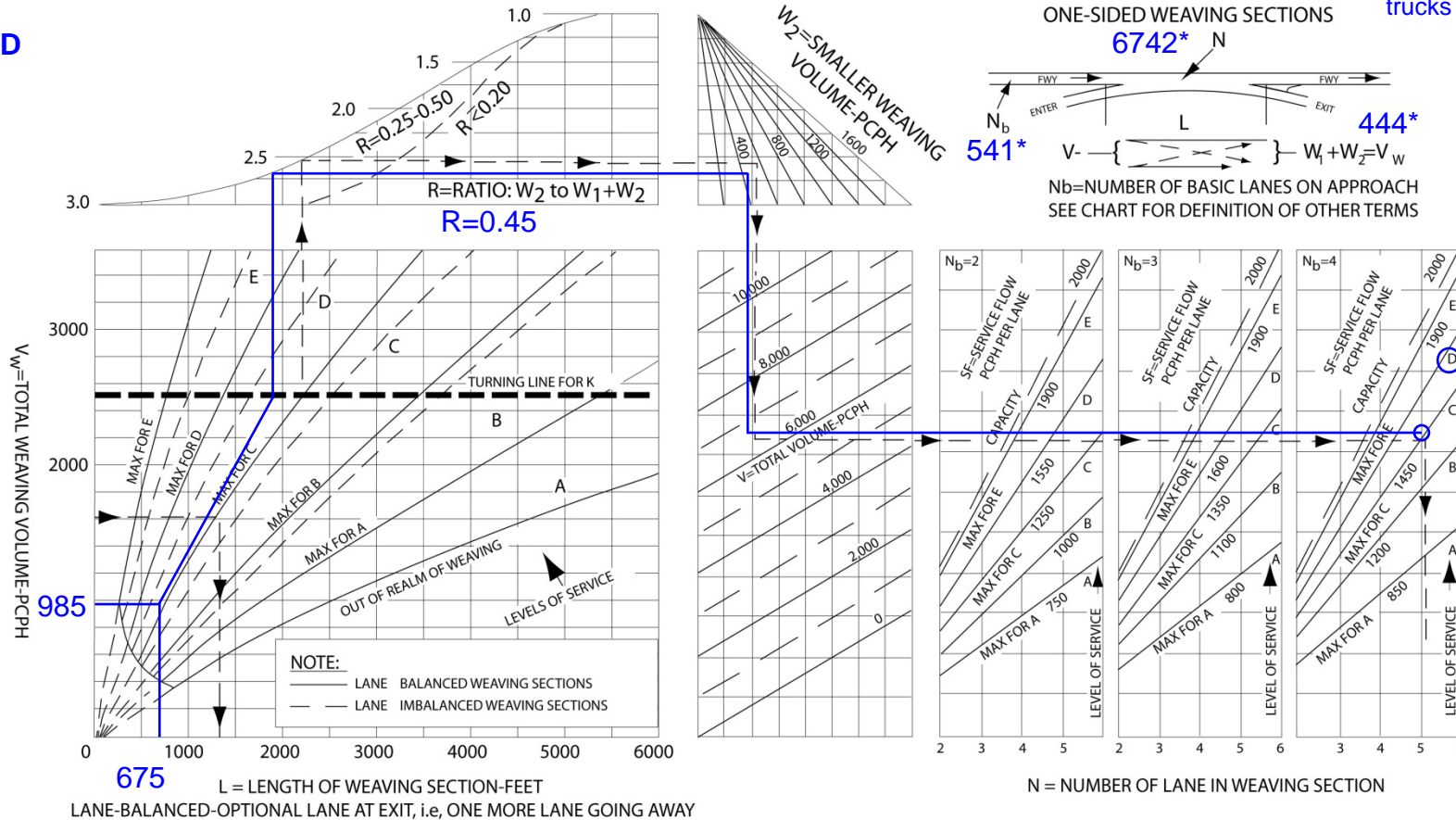
NOTE: EXTRAPOLATION OF CHART BEYOND THE BOUNDARIES GIVEN IS NOT ADVISED.

Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, $W_1 + W_2$ (or V_w) followed by projection to the right, intersecting the desired weaving LOS: a vertical drop from this point provides weaving distance $L = 1300$ ft. Returning to first intersection point of V_w with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K:" from here the solution line is extended vertically to intersect the K values curve, from which a horizontal extension meets the desired W_2 volume. Then a downward turn to total volume, V , from which the line is horizontally projected to the right, intersection (in this case) the desired LOS = C curve having an SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields a N of 5.2: this would be rounded to $N = 5$ lanes.

US 101, Southbound
 On: SR 237
 Off: Mathilda Ave
 Existing PM (4-5)

1 HOV (dashed) + 3 Mix
 1 Aux lane
 Imbalanced

LOS: D



Design Curve for Freeway and Collector Weaving
 Figure 504.7A

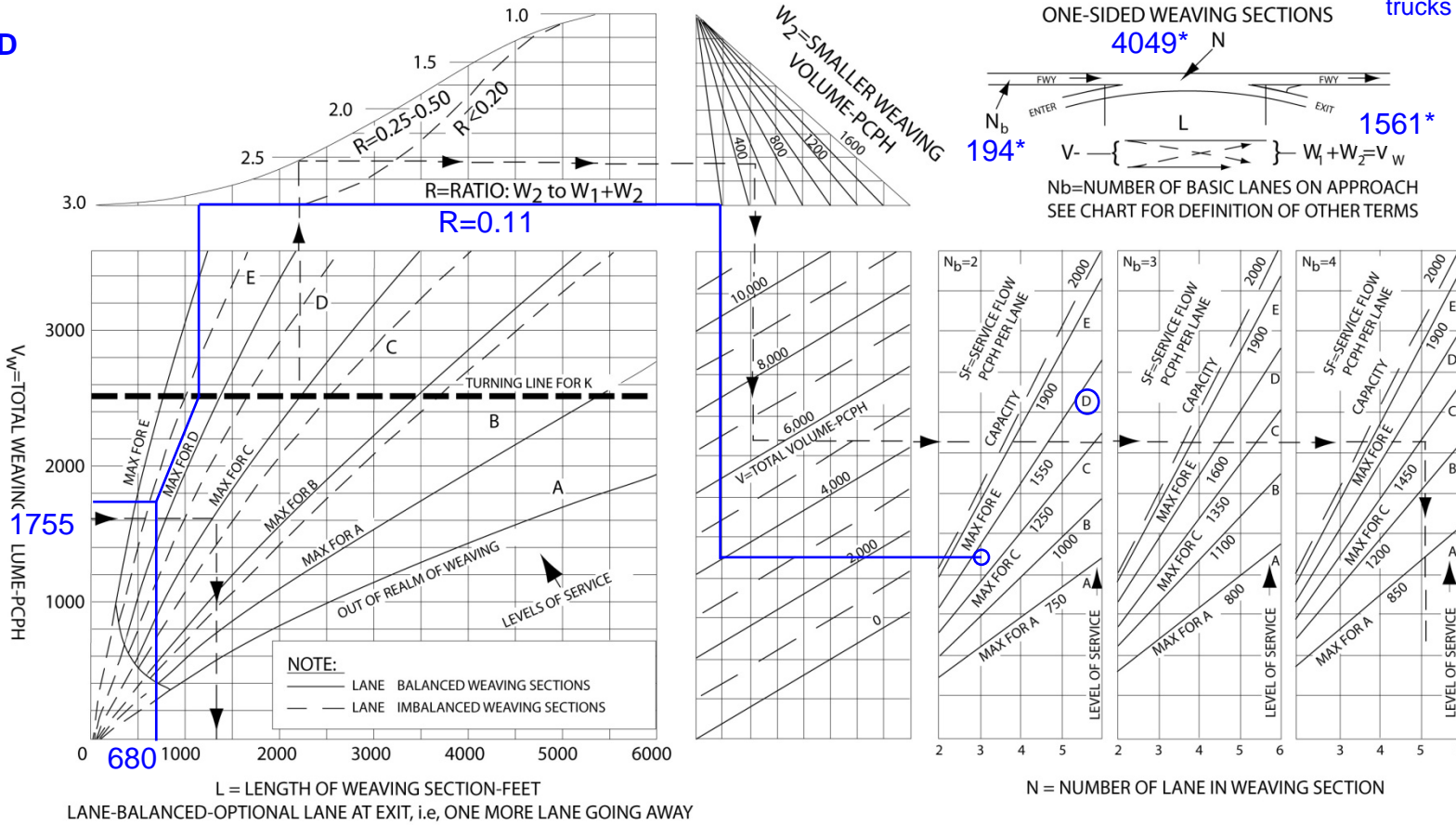
NOTE: EXTRAPOLATION OF CHART BEYOND THE BOUNDARIES GIVEN IS NOT ADVISED.

Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, W_1+W_2 (or V_w) followed by projection to the right, intersecting the desired weaving LOS; a vertical drop from this point provides weaving distance $L = 1300$ ft. Returning to first intersection point of V_w with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K;" from here the solution line is extended vertically to intersect the K values curve, from which a horizontal extension meets the desired W_2 volume. Then a downward turn to total volume, V , from which the line is horizontally projected to the right, intersection (in this case) the desired LOS = C curve having an SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields a N of 5.2; this would be rounded to $N = 5$ lanes.

SR 237 Westbound
 On: Mathilda Ave
 Off: US 101
 Existing AM (7-8)

2 Mix lanes
 1 Aux lane
 Imbalanced

LOS: D



*Volumes adjusted for 4% trucks

Design Curve for Freeway and Collector Weaving

Figure 504.7A

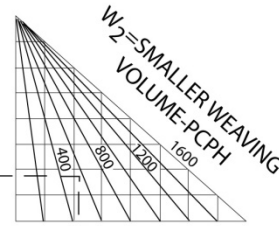
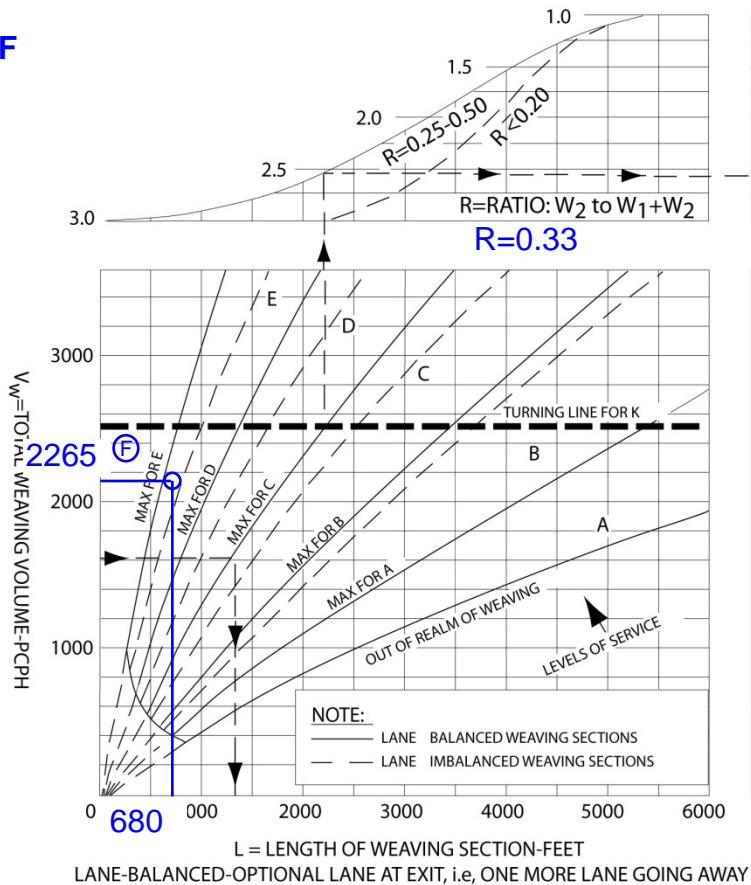
NOTE: EXTRAPOLATION OF CHART BEYOND THE BOUNDARIES GIVEN IS NOT ADVISED.

Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, W_1+W_2 (or V_w) followed by projection to the right, intersecting the desired weaving LOS; a vertical drop from this point provides weaving distance $L = 1300$ ft. Returning to first intersection point of V_w with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K;" from here the solution line is extended vertically to intersect the K values curve, from which a horizontal extension meets the desired W_2 volume. Then a downward turn to total volume, V , from which the line is horizontally projected to the right, intersection (in this case) the desired LOS = C curve having an SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields a N of 5.2; this would be rounded to $N = 5$ lanes.

SR 237 Westbound
 On: Mathilda Ave
 Off: US 101
 Existing PM (5-6)

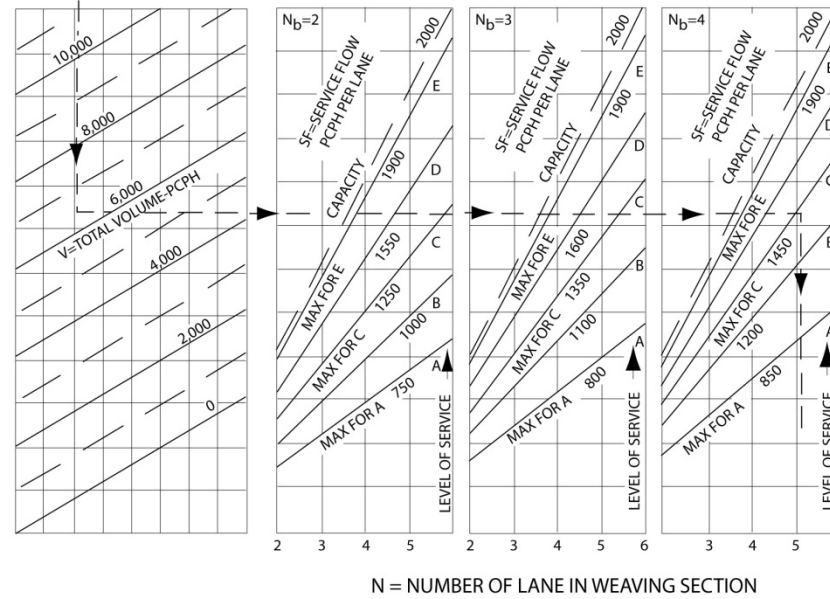
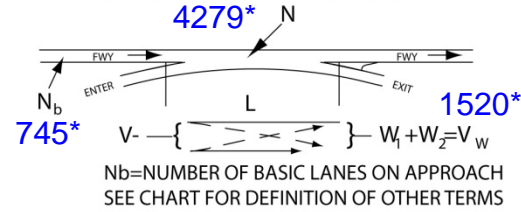
2 Mix lanes
 1 Aux lane
 Imbalanced

LOS: F



ANALYSIS NOMOGRAPH
 FOR DESIGN AND OPERATION OF
 ONE-SIDED WEAVING SECTIONS

*Volumes
 adjusted for 4%
 trucks



NOTE: EXTRAPOLATION OF CHART BEYOND THE BOUNDARIES GIVEN IS NOT ADVISED.

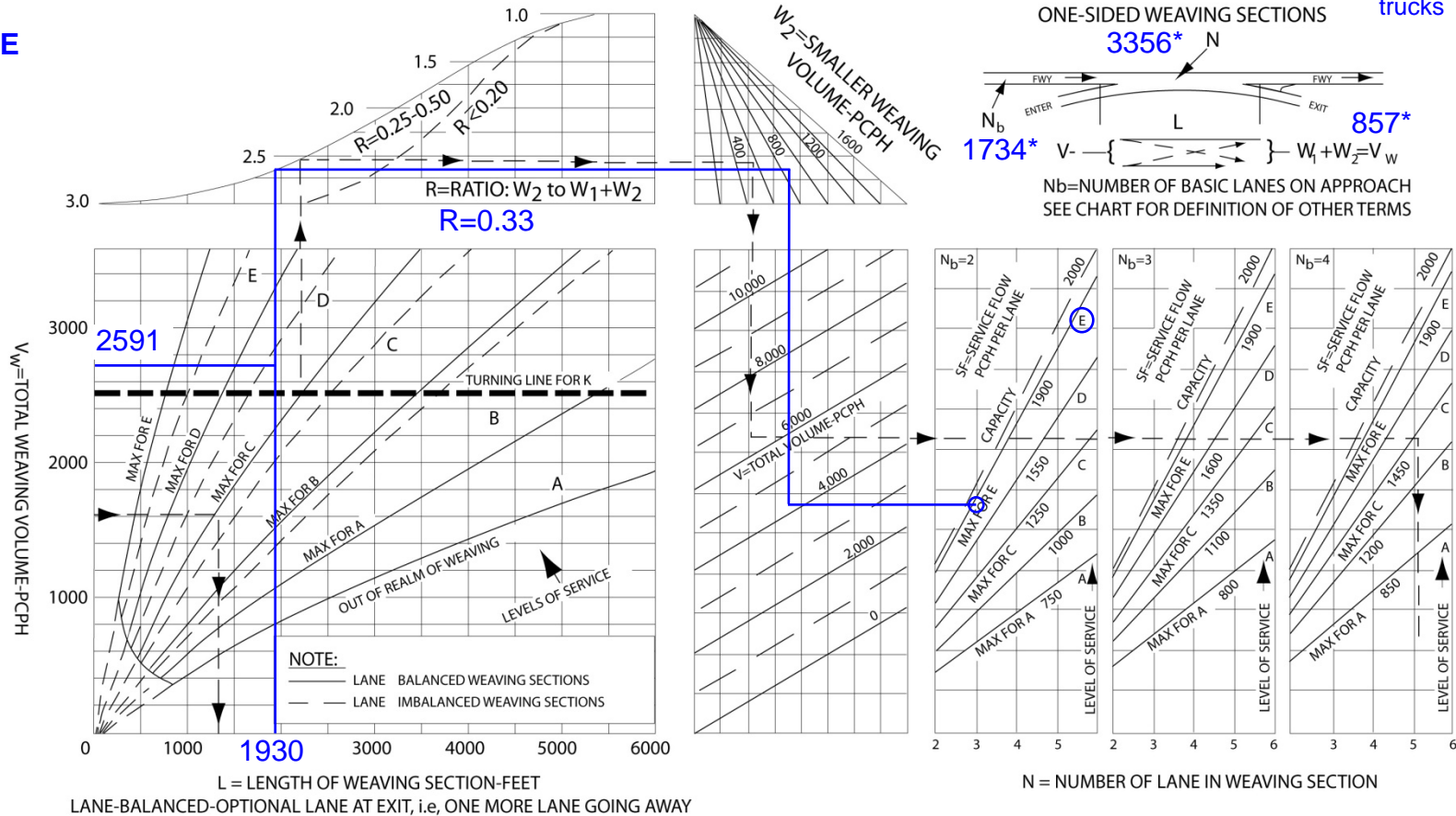
Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, W_1+W_2 (or V_w) followed by projection to the right, intersecting the desired weaving LOS; a vertical drop from this point provides weaving distance $L = 1300$ ft. Returning to first intersection point of V_w with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K;" from here the solution line is extended vertically to intersect the K values curve, from which a horizontal extension meets the desired W_2 volume. Then a downward turn to total volume, V , from which the line is horizontally projected to the right, intersection (in this case) the desired LOS = C curve having an SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields a N of 5.2; this would be rounded to $N = 5$ lanes.

Design Curve for Freeway and Collector Weaving
 Figure 504.7A

SR 237, Eastbound
 On: US 101
 Off: Mathilda Ave
 Existing AM (8-9)

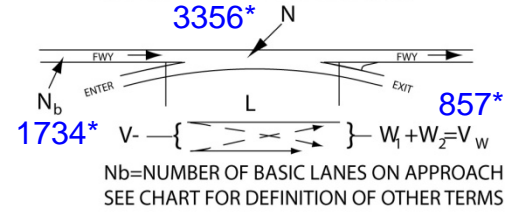
2 Mix lanes
 1 Aux lane
 Balanced

LOS: E



ANALYSIS NOMOGRAPH
 FOR DESIGN AND OPERATION OF
 ONE-SIDED WEAVING SECTIONS

*Volumes
 adjusted for 4%
 trucks



Design Curve for Freeway and Collector Weaving

Figure 504.7A

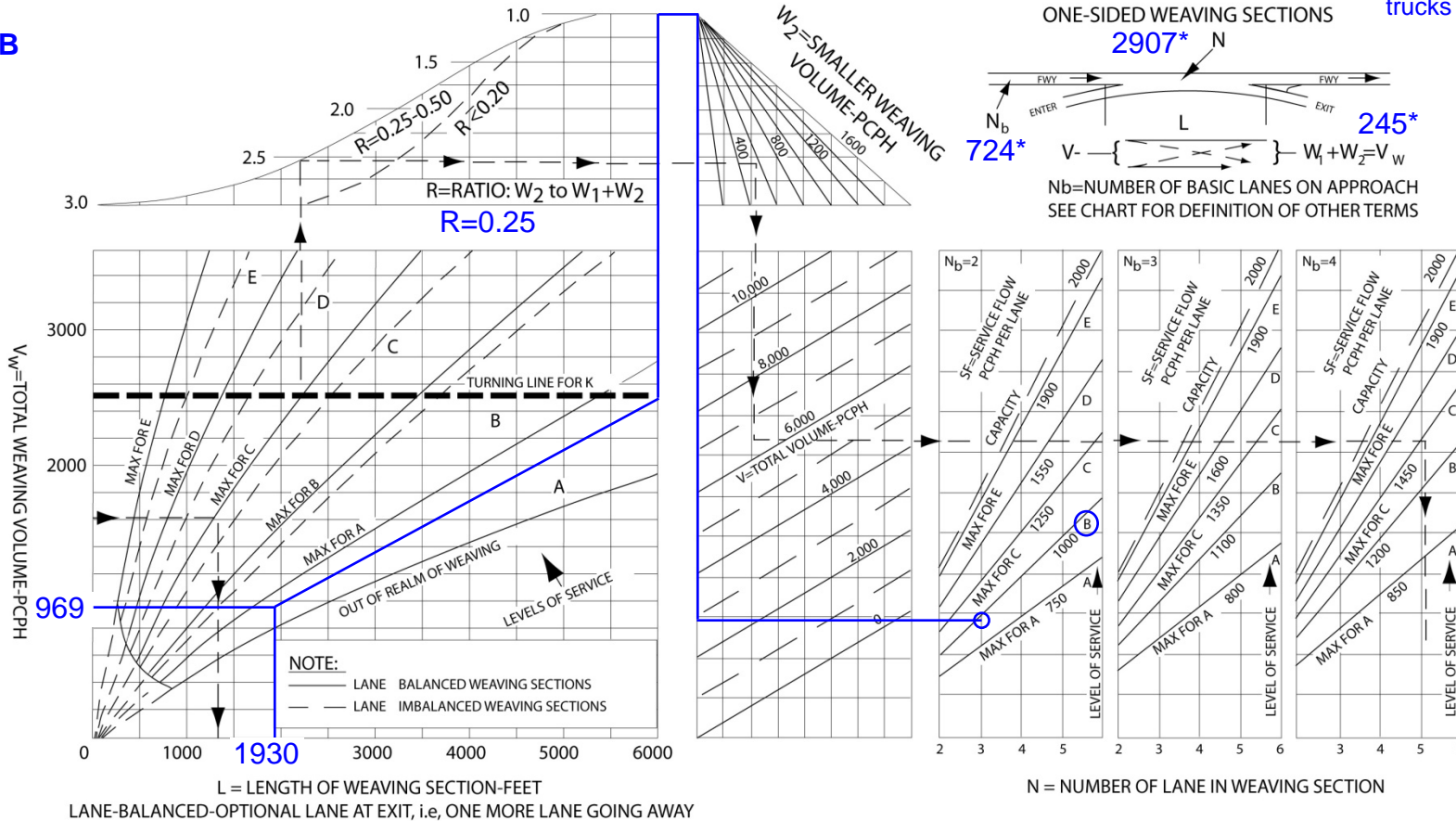
NOTE: EXTRAPOLATION OF CHART BEYOND THE BOUNDARIES GIVEN IS NOT ADVISED.

Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, W_1+W_2 (or V_w) followed by projection to the right, intersecting the desired weaving LOS; a vertical drop from this point provides weaving distance $L = 1300$ ft. Returning to first intersection point of V_w with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K;" from here the solution line is extended vertically to intersect the K values curve, from which a horizontal extension meets the desired W_2 volume. Then a downward turn to total volume, V , from which the line is horizontally projected to the right, intersection (in this case) the desired LOS = C curve having an SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields a N of 5.2; this would be rounded to $N = 5$ lanes.

SR 237, Eastbound
 On: US 101
 Off: Mathilda Ave
 Existing PM (5-6)

2 Mix lanes
 1 Aux lane
 Balanced

LOS: B



*Volumes adjusted for 4% trucks

Design Curve for Freeway and Collector Weaving

Figure 504.7A

NOTE: EXTRAPOLATION OF CHART BEYOND THE BOUNDARIES GIVEN IS NOT ADVISED.

Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, W_1+W_2 (or V_w) followed by projection to the right, intersecting the desired weaving LOS; a vertical drop from this point provides weaving distance $L = 1300$ ft. Returning to first intersection point of V_w with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K;" from here the solution line is extended vertically to intersect the K values curve, from which a horizontal extension meets the desired W_2 volume. Then a downward turn to total volume, V , from which the line is horizontally projected to the right, intersection (in this case) the desired LOS = C curve having an SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields a N of 5.2; this would be rounded to $N = 5$ lanes.

**APPENDIX H – TRAVEL DEMAND MODEL VALIDATION
MEMORANDUM**



MEMORANDUM

Date: October 14, 2015

To: Paul Ma, Caltrans
Phil Cox, Caltrans

From: Katie Leung, Matt Haynes and Ashley Brooks, Fehr & Peers
David Kobayashi and George Naylor, Valley Transportation Authority

Subject: Mathilda Avenue Improvements at SR 237 and US 101: Travel Demand Forecasting Model Validation Procedure and Results

SJ13-1460

A key step in conducting the transportation analysis for the Mathilda Avenue Improvements at SR 237 and US 101 Project is to determine the appropriate model to forecast traffic volumes within the study area. Two models were evaluated for potential application: the Santa Clara Valley Transportation Authority (VTA) travel demand model and the City of Sunnyvale travel demand model. The selected travel demand model will be used to forecast future traffic volumes to analyze the project alternatives and the potential effects of the project on the transportation network.

This memorandum describes steps taken to evaluate both models and associated validation results.

INTRODUCTION

The proposed Mathilda Avenue Improvements at SR 237 and US 101 Project is located within the City of Sunnyvale in Santa Clara County. **Figure 1** illustrates the project study area, which was identified based on input from the study team, Valley Transportation Authority (VTA), the City of Sunnyvale, and Caltrans staff. The Traffic Operations Analysis Report (TOAR) for this project will evaluate the following 14 intersections:



- | | |
|--|--|
| <ol style="list-style-type: none"> 1. Mathilda Avenue / Fifth Avenue 2. Mathilda Avenue / Innovation Way 3. Mathilda Avenue / Moffett Park Drive 4. Mathilda Avenue / SR 237 WB Ramps 5. Mathilda Avenue / SR 237 EB Ramps 6. Mathilda Avenue / Ross Drive 7. Mathilda Avenue US 101 NB Ramps (project intersection)* | <ol style="list-style-type: none"> 8. Mathilda Avenue / US 101 SB Ramps (project intersection)* 9. Mathilda Avenue / Ahwanee Avenue-Almanor Avenue 10. US 101 NB On-Ramp / Moffett Park Drive 11. Innovation Way / Moffett Park Drive 12. Innovation Way / Eleventh Avenue 13. Innovation Way / Juniper Networks Driveway 14. Bordeaux Drive / Innovation Way (future intersection)** |
|--|--|

* Project intersection is defined as an intersection to be evaluated under the Build Alternatives.

** Future intersection is defined as an intersection to be built as part of a separate project (Moffett Place) and will be assumed to be built under all 2040 analyses.

In addition, this study will evaluate the following mainline segments along US 101 and SR 237:

| US 101 | |
|---|---|
| Northbound | Southbound |
| <ul style="list-style-type: none"> • Lawrence Expressway to Fair Oaks Avenue • Fair Oaks Avenue to Mathilda Avenue • Mathilda Avenue to SR 237 Ramps • SR 237 Ramps to Ellis Street | <ul style="list-style-type: none"> • Ellis Street to SR 237 Ramps • SR 237 Ramps to Mathilda Avenue • Mathilda Avenue to Fair Oaks Avenue • Fair Oaks Avenue to Lawrence Expressway |
| SR 237 | |
| Westbound | Eastbound |
| <ul style="list-style-type: none"> • Lawrence Expressway to Fair Oaks Avenue • Fair Oaks Avenue to Mathilda Avenue • Mathilda Avenue to US 101 Ramps • US 101 Ramps to Maude Avenue | <ul style="list-style-type: none"> • Maude Avenue to US 101 Ramps • US 101 Ramps to Mathilda Avenue • Mathilda Avenue to Fair Oaks Avenue • Fair Oaks Avenue to Lawrence Expressway |

MODEL VALIDATION – 2010 CALIFORNIA REGIONAL TRANSPORTATION PLAN GUIDELINES

In order to evaluate the model's performance in replicating existing conditions, the model results were compared to the model validation thresholds from the *2010 California Regional Transportation Plan (RTP)*



Guidelines, California Transportation Commission, which provide guidelines for determining whether a model is valid and acceptable for forecasting future year traffic volumes.

It is important to note that the thresholds in the *RTP Guidelines* were developed to be applied to regional-scale models and not to a model that is being used only for a small project-specific study area; however, the thresholds can still provide a useful indication of how well the model results match the existing demand volumes in the study area. The goal is not necessarily to meet all of the thresholds but instead to confirm or improve the model's performance within the project's study area.

The model results were compared to 2013 AM and PM peak hour traffic counts collected throughout the project study area (some counts were collected in 2011, 2012, and 2014). Existing mainline and ramp demand volumes were obtained from Table 6 of the *Forecasted Traffic Demand Memorandum SR 237 Express Lanes Phase 2 Project* (February 2014), Caltrans 2013 census counts and Appendix C of the *Final Existing Conditions and Model Calibration Report US 101 Express Lanes* (January 2013). For each location, the peak hour count was identified for the AM period (between 7-9 AM) and the PM period (4-6 PM).

The model validation process involved the evaluation of model parameters in the roadway network files, as well as other key model components. The parameters were iteratively adjusted and compared with the following validation criteria drawn from the *2010 California Regional Transportation Plan Guidelines*:

- Correlation Coefficient: greater than 0.88
- Percent Root Mean Square Error: less than 40 percent
- 75 percent of links within Caltrans Deviation Allowance
- Model/Count ratio¹

The Caltrans Deviation Allowance is the difference between the model ADT volume and the actual ADT count divided by the actual ADT count. The Caltrans deviation thresholds shrink as the count increases as seen in Figure 3-9 of the Caltrans *Travel Forecasting Guidelines* (November 1992). The ADT thresholds found in the *Travel Forecasting Guidelines* document were adjusted to obtain peak hour thresholds based on the ratio between daily counts and peak hour counts from 24-hour tube counts performed in the area. In addition, the following Model/Count validation goals used by VTA for project-level validation were applied:

- Freeway Mainline and Expressways within seven percent
- Arterial and Collectors within 25 percent

¹ Although there is no specified threshold for this metric, VTA validation goals recommend a threshold of "within five percent" of the sum of all locations, "within 25 percent" of the sum of all arterials and local street, and "within seven percent" of the sum of all freeway mainlines and expressways and "within 25 percent" for ramps.



- Freeway Ramps within 25 percent
- All Facility Types within five percent.

MODEL PERFORMANCE AND VALIDATION PROCESS

VTA Travel Demand Model

A portion of the VTA model was transmitted to Fehr & Peers by VTA staff for use on the Mathilda Avenue Improvements at SR 237 and US 101 Project. These files included the vehicle trip tables, the highway network, and the scripts to rerun the trip assignment portion of the model. The model includes Year 2013, 2020, and 2040 scenarios consistent with the land use projections in Plan Bay Area and regional roadway improvements included in the Valley Transportation Plan (VTP) 2040.

The validation criteria for the model outputs as received from VTA staff were reviewed for the AM and PM peak hour model runs. The results are summarized below in **Table 1**. Link-level model validation results are also provided on **Figure 1** and **Figure 2**.

TABLE 1 – VTA MODEL BASE YEAR VALIDATION

| Criteria | AM Peak Hour | PM Peak Hour | Threshold |
|---|--------------|--------------|-------------------------|
| Model/Count Ratio | 0.93 | 0.96 | Within 5% ¹ |
| Model/Count Ratio (for arterials and local streets) | 0.83 | 0.82 | Within 25% ² |
| Model/Count Ratio (for ramps) | 0.93 | 0.94 | Within 25% ³ |
| Model/Count Ratio (for freeway mainline and expressways) | 0.97 | 1.02 | Within 7% ⁴ |
| Percent of Links within Caltrans Maximum Deviation | 76% | 75% | At least 75% |
| Percent Root Mean Square Error | 29% | 37% | Below 40% |
| Correlation Coefficient | 0.92 | 0.95 | At least 0.88 |
| Number of Validation Locations | 51 | 51 | N/A |

Note: **Bold** text indicates validation criteria met.

1. Although no specific threshold is specified in the 2010 *California Regional Transportation plan Guidelines*, per VTA a validation goal threshold of “within five percent” of the sum of all locations was used.
2. Per VTA validation goals, a threshold of “within 25 percent” of the sum of all arterials and local streets was used.
3. Per VTA validation goals, a threshold of “within 25 percent” of the sum of all ramps was used.
4. Per VTA validation goals, a threshold of “within seven percent” of the sum of all freeway mainline and expressways was used.

Source: Fehr & Peers, October 2015.



As received, the VTA model meets all of the validation thresholds in the AM and PM peak hours except for the model-to-count ratio during the AM peak hour. However on an overall basis the validation results are still acceptable because the VTA model meets or exceeds desired thresholds in all other categories. Therefore, the VTA model would be appropriate to use as the travel demand forecasting model for this project.

Sunnyvale Travel Demand Model

The same roadway links and freeway segments evaluated under the VTA model were also studied under the City of Sunnyvale travel demand model. However, the City of Sunnyvale model did not meet several of the validation criteria during the AM and PM peak hours as shown in **Table 2**. Because the VTA model performed well as shown in **Table 1**, no further testing was completed using the City of Sunnyvale model, and the VTA model was selected as the appropriate tool for forecasting future volumes.

TABLE 2 – SUNNYVALE MODEL BASE YEAR VALIDATION

| Criteria | AM Peak Hour | PM Peak Hour | Threshold |
|---|--------------|--------------|-------------------------|
| Model/Count Ratio | 0.93 | 1.07 | Within 5% ¹ |
| Model/Count Ratio (for arterials and local streets) | 0.91 | 0.97 | Within 25% ² |
| Model/Count Ratio (for ramps) | 1.02 | 1.00 | Within 25% ³ |
| Model/Count Ratio (for freeway mainline and expressways) | 0.93 | 1.12 | Within 7% ⁴ |
| Percent of Links within Caltrans Maximum Deviation | 63% | 59% | At least 75% |
| Percent Root Mean Square Error | 61% | 86% | Below 40% |
| Correlation Coefficient | 0.78 | 0.75 | At least 0.88 |
| Number of Validation Locations | 51 | 51 | N/A |

Note: **Bold** text indicates validation criteria met.

1. Although no specific threshold is specified in the 2010 *California Regional Transportation plan Guidelines*, per VTA a validation goal threshold of “within five percent” of the sum of all locations was used.
2. Per VTA validation goals, a threshold of “within 25 percent” of the sum of all arterials and local streets was used.
3. Per VTA validation goals, a threshold of “within 25 percent” of the sum of all ramps was used.
4. Per VTA validation goals, a threshold of “within seven percent” of the sum of all freeway mainline and expressways was used.

Source: Fehr & Peers, October 2015.

CONCLUSIONS

Based on the model validation results presented above in **Table 1**, the VTA travel demand model has been tested and found to be valid for use in the development of future year traffic forecasts on roadway segments



within the project study area. While the “as received” model already meets all validation criteria as outlined in the 2010 *RTP Guidelines*, minor modifications to the local area model network may be made, such as the location of centroid connectors, for conducting the future year traffic forecasts.

Next Steps

The primary purpose of the VTA model in the transportation analysis process is to develop traffic forecasts for the anticipated opening year of 2020 and for the design year of 2040. The design year forecasts will be developed by applying versions of the VTA model, calculating the growth in link volumes projected by the model between the base year and the design year, and adding that growth to the existing volumes. Opening year forecasts will be estimated through linear interpolation between the existing demand volumes and the design year forecasts.

Once future travel demand forecasts are developed, results will be documented in a forthcoming technical memorandum for agency review and approval. After future forecasts are approved, the opening and design year forecasts will be used for the traffic operations analysis to be conducted in the PA&ED phase of the project.

ATTACHMENTS

Figure 1: Study Area

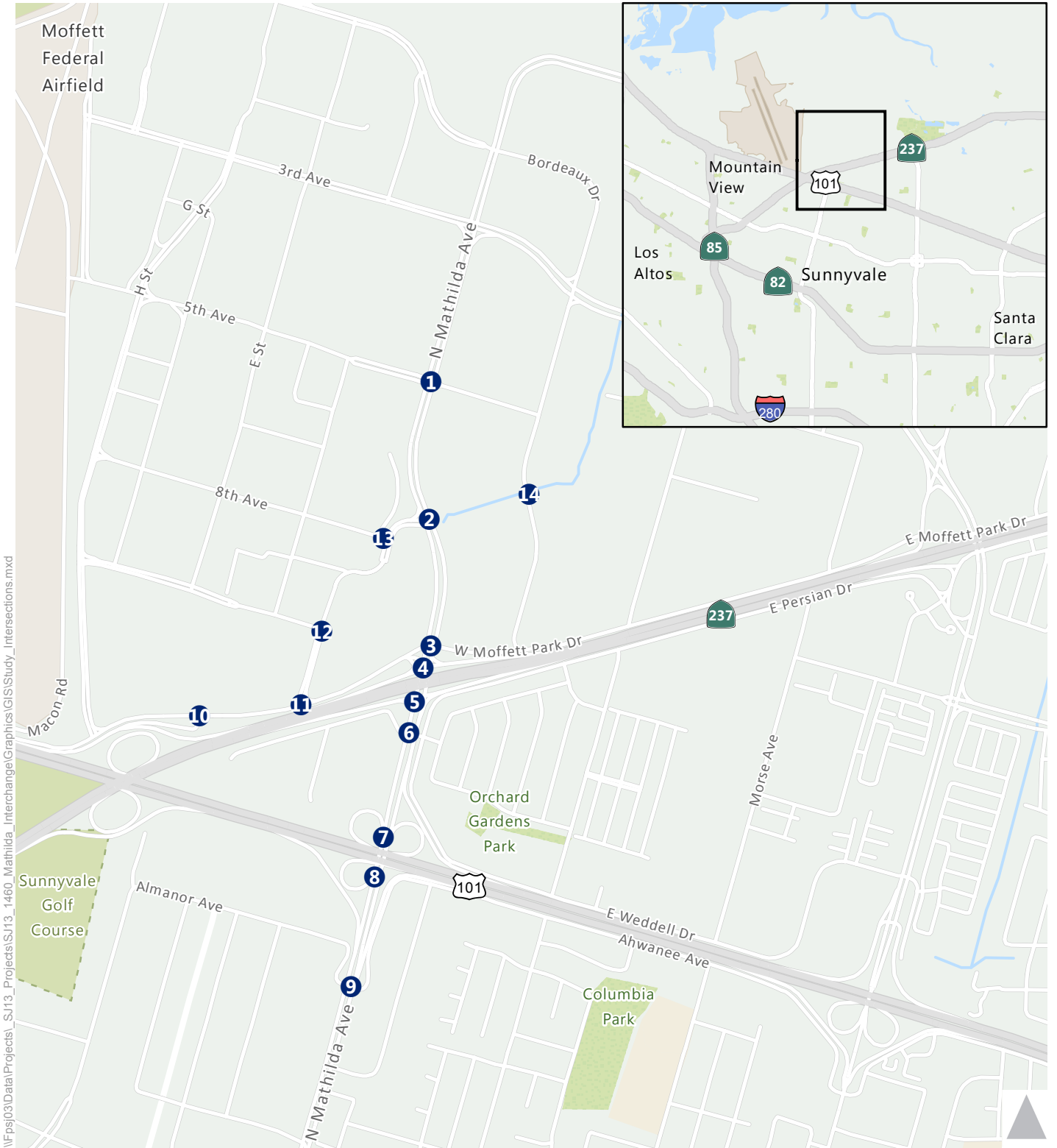
Figure 2: AM Peak Hour Link-Level Model Validation Results

Figure 3: PM Peak Hour Link-Level Model Validation Results

APPENDIX

Appendix A: VTA Model Link-Level Model Validation Results

Appendix B: Sunnyvale Model Link-Level Model Validation Results



● Study Intersections

Figure 1

Vicinity Map
Mathilda Avenue Improvements





Traffic Count Validation (AM Peak Hour)

— Within Deviation*

— Outside of Deviation*

*Deviation per Caltrans Deviation Allowance

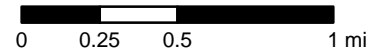
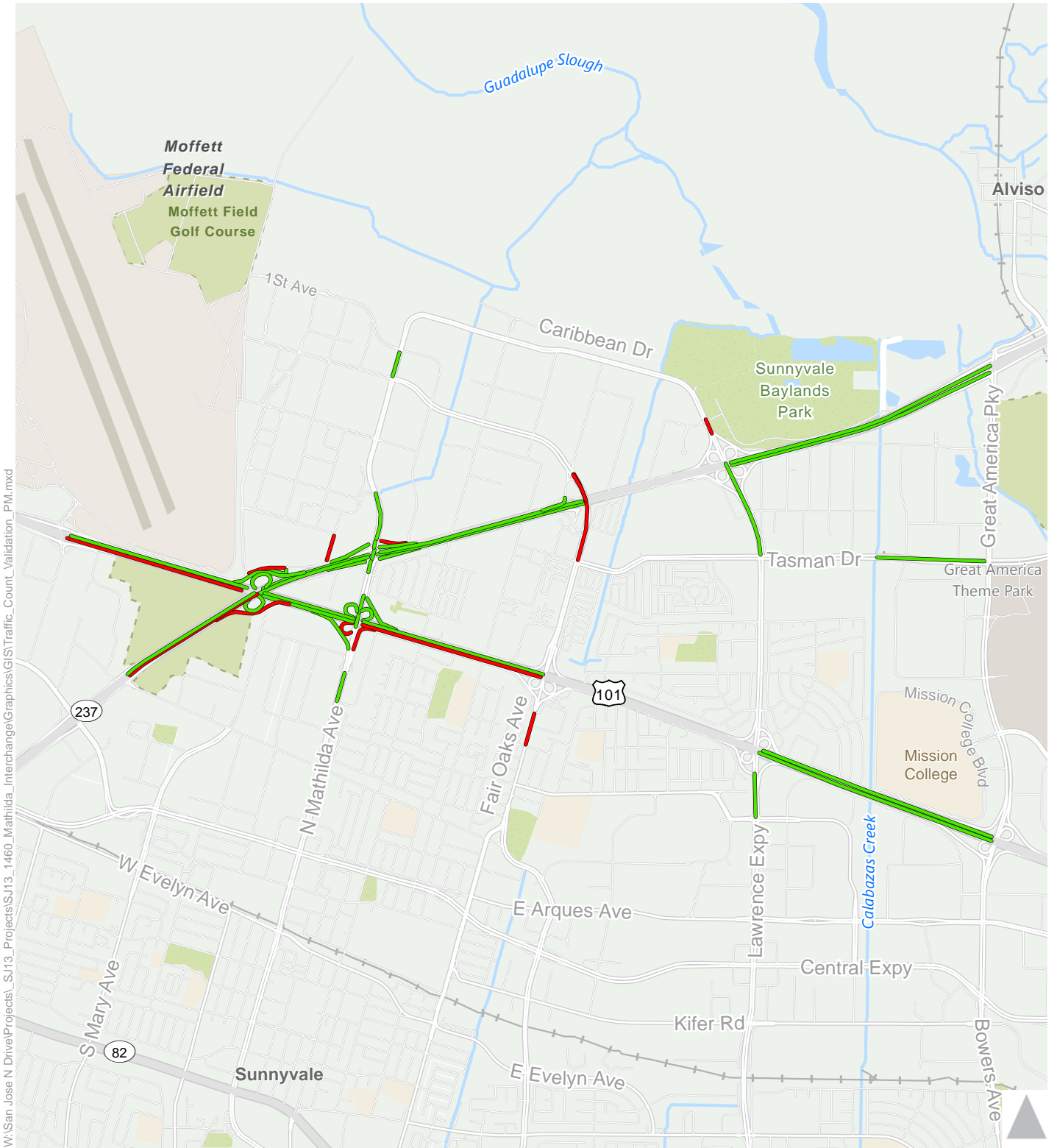


Figure 2
AM Peak Hour Link-Level Model Validation



W:\San Jose N Drive\Projects\SJ13_Projects\SJ13_1460_Mathilda_Interchange\Graphics\GIS\Traffic_Count_Validation_PM.mxd

Traffic Count Validation (PM Peak Hour)

— Within Deviation*

— Outside of Deviation*

*Deviation per Caltrans Deviation Allowance

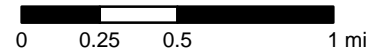


Figure 3
PM Peak Hour Link-Level Model Validation

APPENDIX I – BUILD ALTERNATIVE CONCEPTUAL DRAWINGS



Build Alternative 1

Existing northbound US 101 loop off-ramp would be closed and traffic shifted to the northbound US 101 diagonal off-ramp. Northbound US 101 diagonal off-ramp and loop on-ramp would be realigned and widened to terminate at a new signalized intersection on Mathilda Avenue. Left-turn access from southbound Mathilda Avenue to northbound US 101 loop on-ramp would be provided. This new ramp configuration would provide full access to northbound US 101 by adding access to northbound US 101 from southbound on Mathilda Avenue.

Southbound US 101 off-ramp and loop on-ramp would be realigned and widened to terminate at a new signalized intersection on Mathilda Avenue. Left-turn access from southbound US 101 off-ramp to northbound Mathilda Avenue would be provided. This new ramp configuration would provide full access to southbound US 101 by adding access to northbound on Mathilda Avenue from southbound US 101.

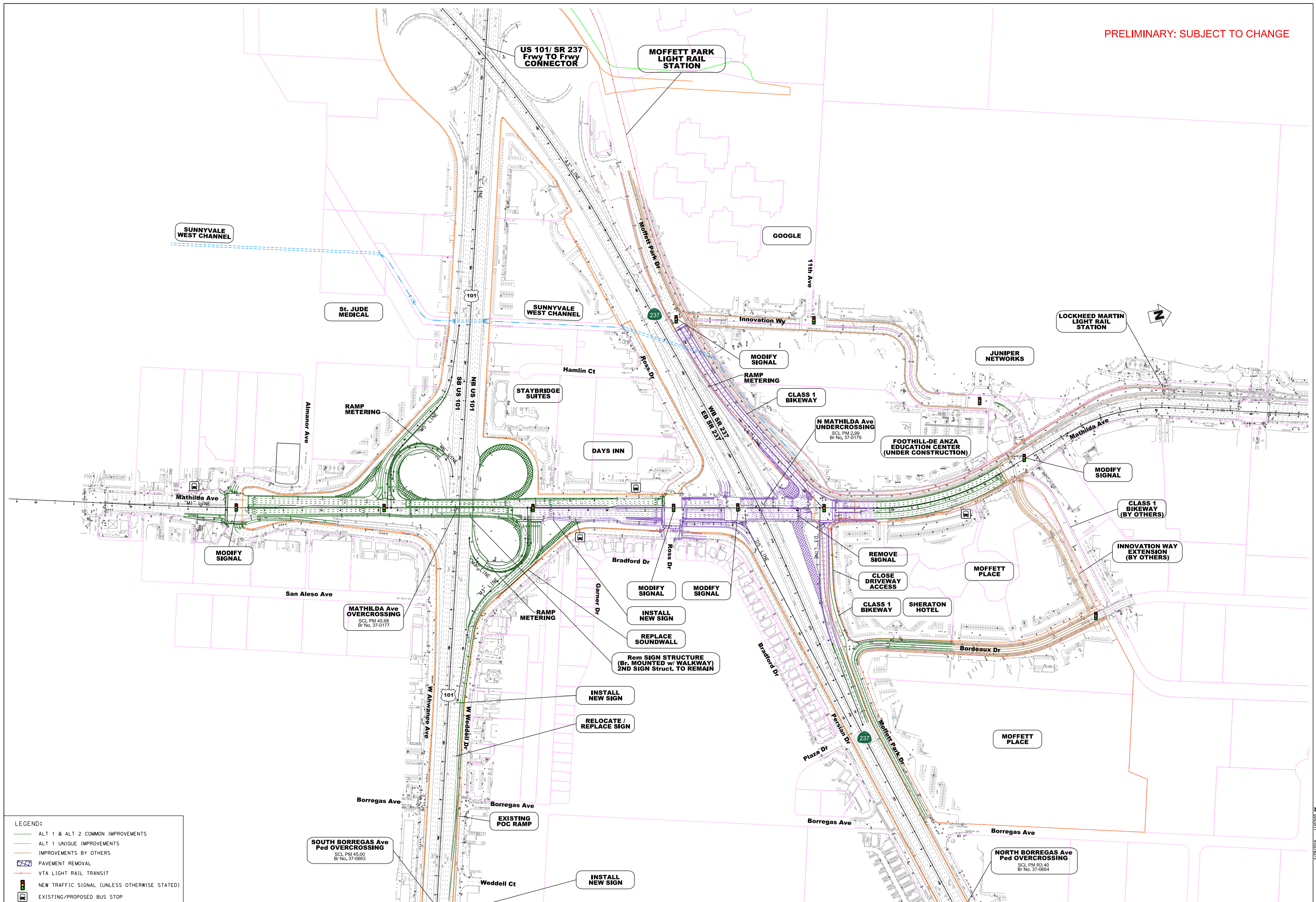
The westbound SR 237 off-ramp would be realigned with Moffett Park Drive on the east leg of the intersection and the signal at existing SR 237 westbound ramps would be removed. Moffett Park Drive access on the east side of Mathilda Avenue would be closed and traffic shifted to Bordeaux Drive and Innovation Way. Moffett Park Drive access west of Mathilda Avenue would remain open. Access to the westbound SR 237 on-ramp from northbound Mathilda Avenue would be accomplished with a U-turn movement at the new signalized intersection.

Build Alternative 2

Existing northbound US 101 loop off-ramp would be closed and traffic shifted to the northbound US 101 diagonal off-ramp. Northbound US 101 diagonal off-ramp and loop on-ramp would be realigned and widened to terminate at a new signalized intersection on Mathilda Avenue. Left-turn access from southbound Mathilda Avenue to northbound US 101 loop on-ramp would be provided. This new ramp configuration would provide full access to northbound US 101 by adding access to northbound US 101 from southbound on Mathilda Avenue.

Southbound US 101 off-ramp and loop on-ramp would be realigned and widened to terminate at a new signalized intersection on Mathilda Avenue. Left-turn access from southbound US 101 off-ramp to northbound Mathilda Avenue would be provided. This new ramp configuration would provide full access to southbound US 101 by adding access to northbound on Mathilda Avenue from southbound US 101.

Existing SR 237 ramps would be realigned and widened to accommodate a diverging diamond interchange configuration. Existing signalized intersections on Mathilda Avenue at the SR 237 ramps and Moffett Park Drive would be removed. New signalized intersections would be constructed at realigned SR 237 ramp termini. Traffic on Mathilda Avenue would be shifted to the opposite side of the road between SR 237 ramp termini to facilitate left-turn movements. Moffett Park Drive access on the east side of Mathilda Avenue would be closed and traffic shifted to Bordeaux Drive and Innovation Way. West Moffett Park Drive would remain open for westbound traffic.



wmh

SCALE IN FEET

80 40 0 80 160 240

US 101/ SR 237 Frwy TO Frwy CONNECTOR

MOFFETT PARK LIGHT RAIL STATION

SUNNYVALE WEST CHANNEL

GOOGLE

St. JUDE MEDICAL

SUNNYVALE WEST CHANNEL

LOCKHEED MARTIN LIGHT RAIL STATION

JUNIPER NETWORKS

RAMP METERING

STAYBRIDGE SUITES

DAYS INN

MODIFY SIGNAL

RAMP METERING

CLASS 1 BIKEWAY

N MATHILDA Ave UNDERCROSSING
SCL PM 2.99
Br No. 37-3179

FOOTHILL-DE ANZA EDUCATION CENTER (UNDER CONSTRUCTION)

MODIFY SIGNAL

CLASS 1 BIKEWAY (BY OTHERS)

INNOVATION WAY EXTENSION (BY OTHERS)

MODIFY SIGNAL

San Aleso Ave

MATHILDA Ave OVERCROSSING
SCL PM 45.68
Br No. 37-0177

Bradford Dr

INSTALL NEW SIGN

MODIFY SIGNAL

REMOVE SIGNAL

CLOSE DRIVEWAY ACCESS

CLASS 1 BIKEWAY

SHERATON HOTEL

MOFFETT PLACE

RAMP METERING

Rem SIGN STRUCTURE (Br. MOUNTED w/ WALKWAY) 2ND SIGN Struct. TO REMAIN

REPLACE SOUNDWALL

INSTALL NEW SIGN

RELOCATE / REPLACE SIGN

MOFFETT PLACE

SOUTH BORREGAS Ave Ped OVERCROSSING
SCL PM 45.00
Br No. 37-0663

INSTALL NEW SIGN

NORTH BORREGAS Ave Ped OVERCROSSING
SCL PM R3.40
Br No. 37-0664

LEGEND:

- ALT 1 & ALT 2 COMMON IMPROVEMENTS
- ALT 2 UNIQUE IMPROVEMENTS
- IMPROVEMENTS BY OTHERS
- PAVEMENT REMOVAL
- VTA LIGHT RAIL TRANSIT
- NEW TRAFFIC SIGNAL (UNLESS OTHERWISE STATED)
- EXISTING/PROPOSED BUS STOP
- RIGHT OF WAY LIMITS
- PARCEL LINE

wmh

SCALE IN FEET

80 40 0 80 160 240

MATHILDA Ave IMPROVEMENTS AT SR 237 AND US 101
SCL 237 - PM 2.7/3.3
SCL 101 - PM 45.4/45.8

ALTERNATIVE 2

FIGURE 2b

FEB 24, 2016

2/24/2016 11:04:25 AM

**APPENDIX J – TRAVEL DEMAND MODEL GROWTH RATE
CALCULATIONS**



VTA and City of Sunnyvale Models Trip Generation Growth Rates

VTA Model (AM)

| AM | 2015 | | 2040 | | Amount Difference | | Percent Difference | |
|-------------------|-------------|-------------|--------------|-------------|-------------------|-------------|--------------------|--------------|
| | Inbound | Outbound | Inbound | Outbound | Inbound | Outbound | Inbound | Outbound |
| West Moffett Park | 1831 | 246 | 2966 | 358 | 1136 | 113 | 62.0% | 45.8% |
| East Moffett Park | 1979 | 339 | 2843 | 422 | 863 | 83 | 43.6% | 24.5% |
| Triangle | 1217 | 1390 | 1344 | 1752 | 127 | 362 | 10.4% | 26.0% |
| NW Maude | 515 | 55 | 919 | 97 | 405 | 41 | 78.6% | 74.7% |
| NE Maude | 1535 | 2023 | 1509 | 2097 | -25 | 75 | -1.6% | 3.7% |
| SW Maude | 1277 | 1011 | 1351 | 1047 | 74 | 36 | 5.8% | 3.6% |
| SE Maude | 1223 | 1382 | 1699 | 2031 | 477 | 649 | 39.0% | 47.0% |
| TOTAL | 9576 | 6445 | 12632 | 7804 | 3056 | 1358 | 31.9% | 21.1% |

VTA Model (AM)

| AM | Annual Growth Rate (Compounded) | | | Annual Growth Rate (Linear) | | |
|-------------------|---------------------------------|-------------|-------------|-----------------------------|-------------|-------------|
| | Inbound | Outbound | Total | Inbound | Outbound | Total |
| West Moffett Park | 1.9% | 1.5% | 1.9% | 2.5% | 1.8% | 2.4% |
| East Moffett Park | 1.5% | 0.9% | 1.4% | 1.7% | 1.0% | 1.6% |
| Triangle | 0.4% | 0.9% | 0.7% | 0.4% | 1.0% | 0.7% |
| NW Maude | 2.3% | 2.3% | 2.3% | 3.1% | 3.0% | 3.1% |
| NE Maude | -0.1% | 0.1% | 0.1% | -0.1% | 0.1% | 0.1% |
| SW Maude | 0.2% | 0.1% | 0.2% | 0.2% | 0.1% | 0.2% |
| SE Maude | 1.3% | 1.6% | 1.4% | 1.6% | 1.9% | 1.7% |
| TOTAL | 1.1% | 0.8% | 1.0% | 1.3% | 0.8% | 1.1% |

Sunnyvale Model (AM)

| AM | 2015 | | 2035 | | Amount Difference | | Percent Difference | |
|-------------------|-------------|-------------|--------------|-------------|-------------------|-------------|--------------------|--------------|
| | Inbound | Outbound | Inbound | Outbound | Inbound | Outbound | Inbound | Outbound |
| West Moffett Park | 1945 | 320 | 2999 | 325 | 1054 | 6 | 54.2% | 1.7% |
| East Moffett Park | 2201 | 406 | 3688 | 438 | 1486 | 32 | 67.5% | 7.9% |
| Triangle | 1064 | 1225 | 1203 | 1767 | 139 | 542 | 13.1% | 44.2% |
| NW Maude | 813 | 126 | 1164 | 142 | 351 | 15 | 43.2% | 12.2% |
| NE Maude | 1018 | 1719 | 712 | 1240 | -305 | -479 | -30.0% | -27.9% |
| SW Maude | 1299 | 709 | 1484 | 540 | 185 | -170 | 14.2% | -23.9% |
| SE Maude | 480 | 955 | 331 | 805 | -148 | -150 | -30.9% | -15.7% |
| TOTAL | 8820 | 5460 | 11581 | 5256 | 2762 | -204 | 31.3% | -3.7% |

Sunnyvale Model (AM)

| AM | Annual Growth Rate (Compounded) | | | Annual Growth Rate (Linear) | | |
|-------------------|---------------------------------|--------------|-------------|-----------------------------|--------------|-------------|
| | Inbound | Outbound | Total | Inbound | Outbound | Total |
| West Moffett Park | 2.2% | 0.1% | 1.9% | 2.7% | 0.1% | 2.3% |
| East Moffett Park | 2.6% | 0.4% | 2.3% | 3.4% | 0.4% | 2.9% |
| Triangle | 0.6% | 1.8% | 1.3% | 0.7% | 2.2% | 1.5% |
| NW Maude | 1.8% | 0.6% | 1.7% | 2.2% | 0.6% | 1.9% |
| NE Maude | -1.8% | -1.6% | -1.7% | -1.5% | -1.4% | -1.4% |
| SW Maude | 0.7% | -1.4% | 0.0% | 0.7% | -1.2% | 0.0% |
| SE Maude | -1.8% | -0.9% | -1.2% | -1.5% | -0.8% | -1.0% |
| TOTAL | 1.4% | -0.2% | 0.8% | 1.6% | -0.2% | 0.9% |

VTA Model (PM)

| PM | 2015 | | 2040 | | Amount Difference | | Percent Difference | |
|-------------------|-------------|-------------|-------------|--------------|-------------------|-------------|--------------------|--------------|
| | Inbound | Outbound | Inbound | Outbound | Inbound | Outbound | Inbound | Outbound |
| West Moffett Park | 677 | 2243 | 980 | 3489 | 303 | 1247 | 44.7% | 55.6% |
| East Moffett Park | 661 | 2292 | 1162 | 3536 | 501 | 1243 | 75.7% | 54.2% |
| Triangle | 1270 | 1163 | 1639 | 1332 | 369 | 169 | 29.1% | 14.6% |
| NW Maude | 150 | 588 | 257 | 1035 | 108 | 447 | 71.8% | 76.1% |
| NE Maude | 1500 | 1128 | 1634 | 1177 | 134 | 49 | 8.9% | 4.4% |
| SW Maude | 1024 | 1317 | 1153 | 1490 | 129 | 174 | 12.6% | 13.2% |
| SE Maude | 1044 | 979 | 1718 | 1514 | 673 | 535 | 64.5% | 54.6% |
| TOTAL | 6326 | 9709 | 8543 | 13573 | 2217 | 3864 | 35.0% | 39.8% |

VTA Model (PM)

| PM | Annual Growth Rate (Compounded) | | | Annual Growth Rate (Linear) | | |
|-------------------|---------------------------------|-------------|-------------|-----------------------------|-------------|-------------|
| | Inbound | Outbound | Total | Inbound | Outbound | Total |
| West Moffett Park | 1.5% | 1.8% | 1.7% | 1.8% | 2.2% | 2.1% |
| East Moffett Park | 2.3% | 1.7% | 1.9% | 3.0% | 2.2% | 2.4% |
| Triangle | 1.0% | 0.5% | 0.8% | 1.2% | 0.6% | 0.9% |
| NW Maude | 2.2% | 2.3% | 2.3% | 2.9% | 3.0% | 3.0% |
| NE Maude | 0.3% | 0.2% | 0.3% | 0.4% | 0.2% | 0.3% |
| SW Maude | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% | 0.5% |
| SE Maude | 2.0% | 1.8% | 1.9% | 2.6% | 2.2% | 2.4% |
| TOTAL | 1.2% | 1.3% | 1.3% | 1.4% | 1.6% | 1.5% |

Sunnyvale Model (PM)

| PM | 2015 | | 2035 | | Amount Difference | | Percent Difference | |
|-------------------|-------------|-------------|-------------|--------------|-------------------|-------------|--------------------|--------------|
| | Inbound | Outbound | Inbound | Outbound | Inbound | Outbound | Inbound | Outbound |
| West Moffett Park | 424 | 2045 | 660 | 3020 | 236 | 975 | 55.7% | 47.6% |
| East Moffett Park | 526 | 2370 | 858 | 3833 | 332 | 1464 | 63.0% | 61.8% |
| Triangle | 1183 | 1079 | 1907 | 1430 | 724 | 351 | 61.2% | 32.5% |
| NW Maude | 241 | 843 | 294 | 1220 | 53 | 377 | 21.8% | 44.7% |
| NE Maude | 1359 | 841 | 1275 | 871 | -85 | 30 | -6.2% | 3.6% |
| SW Maude | 836 | 1373 | 747 | 1584 | -89 | 211 | -10.7% | 15.3% |
| SE Maude | 700 | 325 | 845 | 452 | 145 | 127 | 20.7% | 39.1% |
| TOTAL | 5270 | 8876 | 6586 | 12411 | 1316 | 3534 | 25.0% | 39.8% |

Sunnyvale Model (PM)

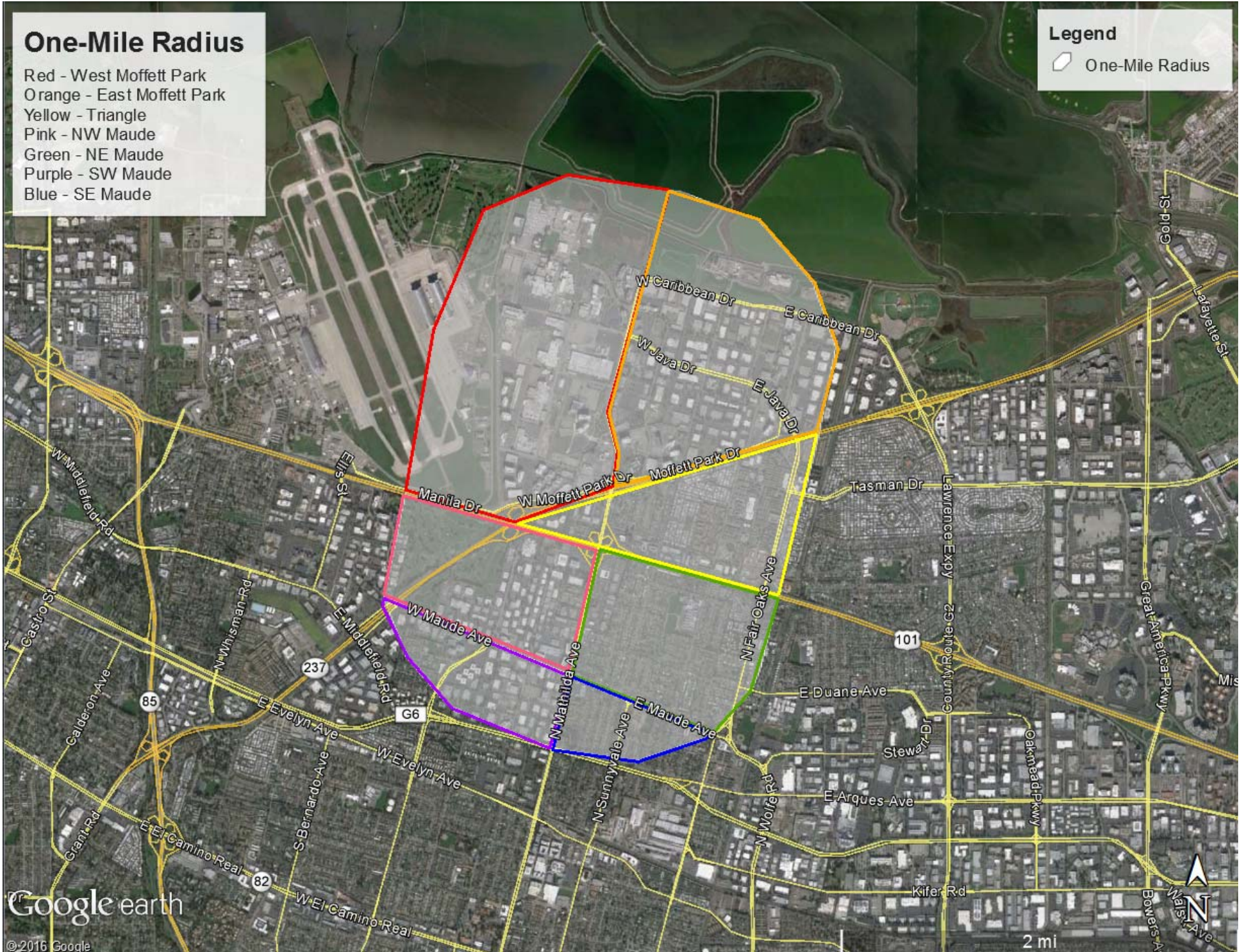
| PM | Annual Growth Rate (Compounded) | | | Annual Growth Rate (Linear) | | |
|-------------------|---------------------------------|-------------|-------------|-----------------------------|-------------|-------------|
| | Inbound | Outbound | Total | Inbound | Outbound | Total |
| West Moffett Park | 2.2% | 2.0% | 2.0% | 2.8% | 2.4% | 2.5% |
| East Moffett Park | 2.5% | 2.4% | 2.4% | 3.2% | 3.1% | 3.1% |
| Triangle | 2.4% | 1.4% | 2.0% | 3.1% | 1.6% | 2.4% |
| NW Maude | 1.0% | 1.9% | 1.7% | 1.1% | 2.2% | 2.0% |
| NE Maude | -0.3% | 0.2% | -0.1% | -0.3% | 0.2% | -0.1% |
| SW Maude | -0.6% | 0.7% | 0.3% | -0.5% | 0.8% | 0.3% |
| SE Maude | 0.9% | 1.7% | 1.2% | 1.0% | 2.0% | 1.3% |
| TOTAL | 1.1% | 1.7% | 1.5% | 1.2% | 2.0% | 1.7% |

One-Mile Radius

- Red - West Moffett Park
- Orange - East Moffett Park
- Yellow - Triangle
- Pink - NW Maude
- Green - NE Maude
- Purple - SW Maude
- Blue - SE Maude

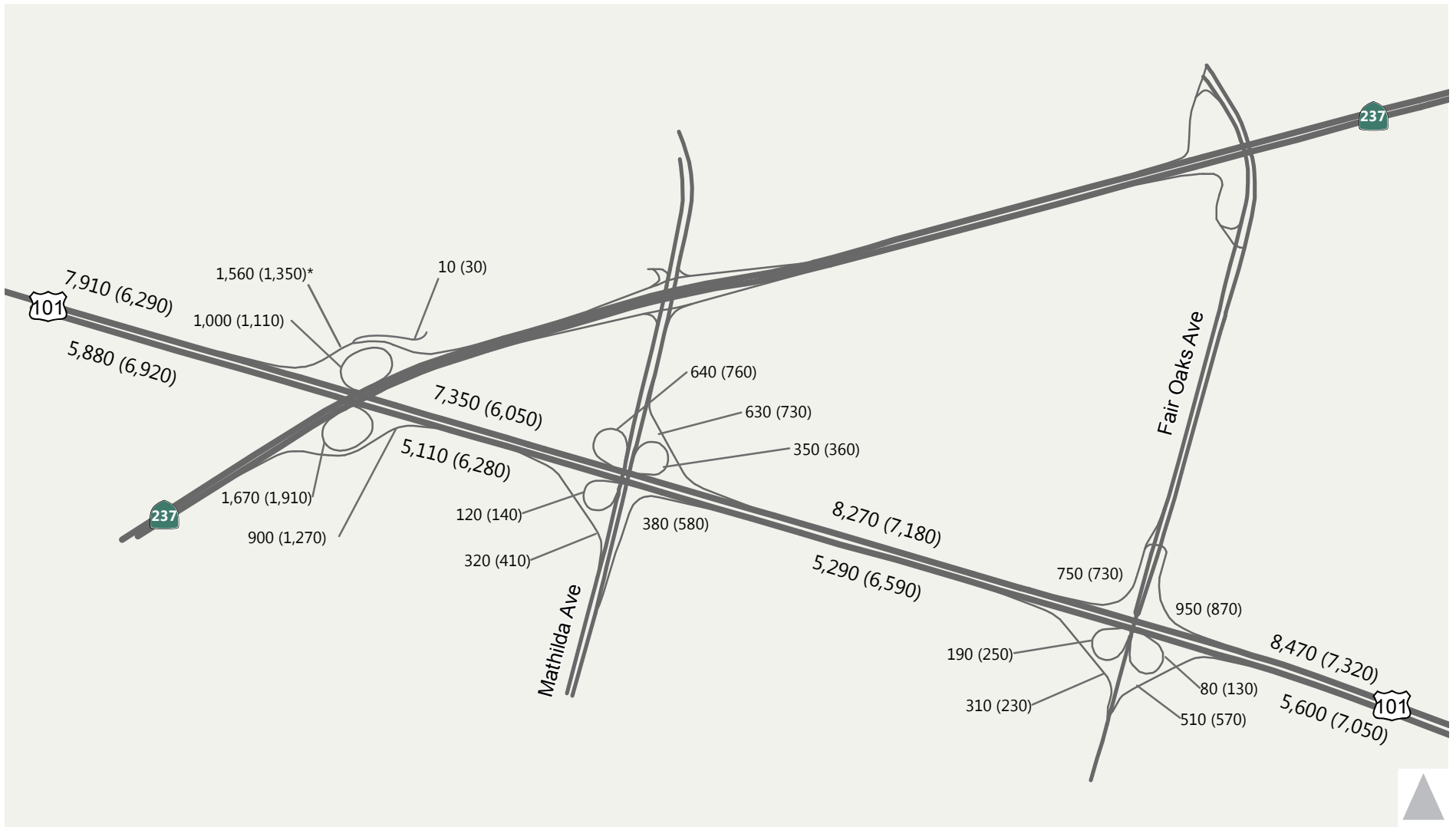
Legend

- One-Mile Radius



**APPENDIX K – 2018 AND 2040 FREEWAY AND RAMP DEMAND
VOLUMES**





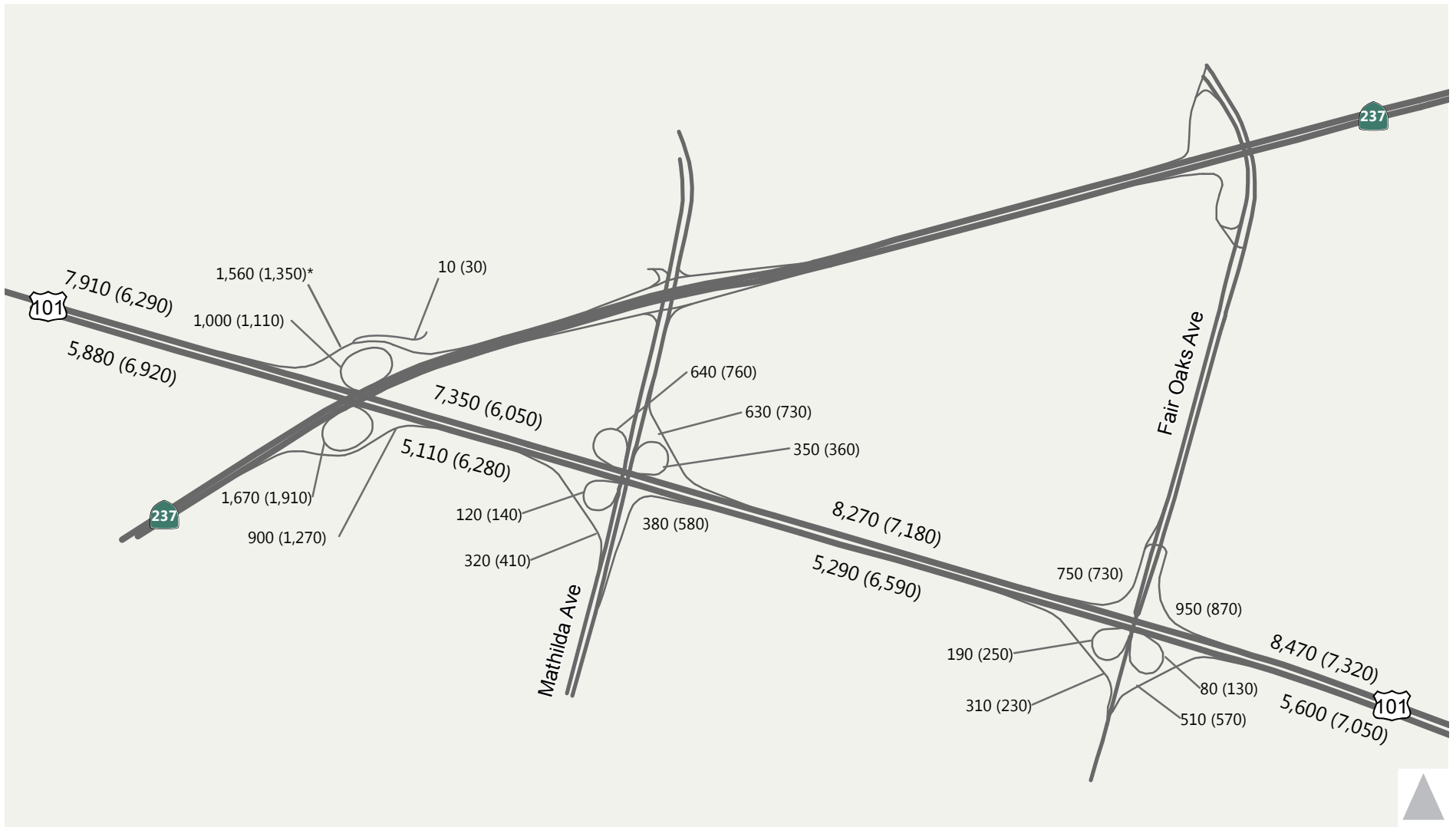
7:00 AM Volumes (8:00 AM Volumes)

* Ramp volume may differ from SR 237 ramp volume due to the slip ramp from Moffett Park Drive onto the SR 237 Off-Ramp/US 101 On-Ramp.

Figure 13A

Mathilda Interchange Project
 Freeway and Ramp Peak Hour Volumes - US Route 101
 2018 No Build - AM Peak Period





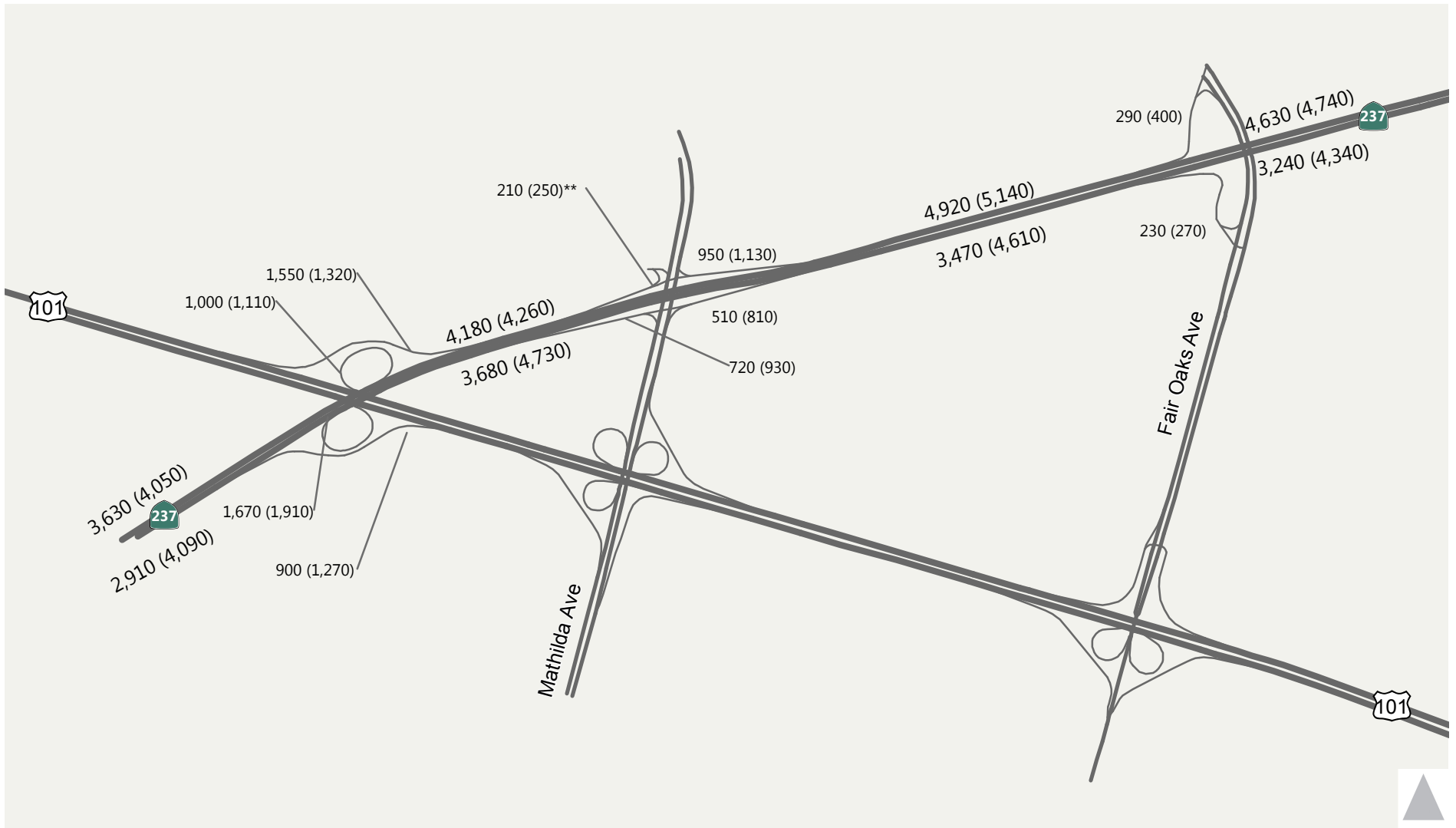
7:00 AM Volumes (8:00 AM Volumes)

* Ramp volume may differ from SR 237 ramp volume due to the slip ramp from Moffett Park Drive onto the SR 237 Off-Ramp/US 101 On-Ramp.

Figure 13A

Mathilda Interchange Project
 Freeway and Ramp Peak Hour Volumes - US Route 101
 2020 No Build - AM Peak Period





7:00 AM Volumes (8:00 AM Volumes)

** Ramp volume may not match ramp terminal intersection due to slip ramp from Moffett Park Drive.

Figure 13B
 Mathilda Interchange Project
 Freeway and Ramp Peak Hour Volumes - CA SR 237
 2018 No Build - AM Peak Period





7:00 AM Volumes (8:00 AM Volumes)

** Ramp volume may not match ramp terminal intersection due to slip ramp from Moffett Park Drive.

Figure 13B
 Mathilda Interchange Project
 Freeway and Ramp Peak Hour Volumes - CA SR 237
 2020 No Build - AM Peak Period





4:00 PM Volumes (5:00 PM Volumes) [6:00 PM Volumes]

* Ramp volume may differ from SR 237 ramp volume due to the slip ramp from Moffett Park Drive onto the SR 237 Off-Ramp/US 101 On-Ramp.

Figure 14A

Mathilda Interchange Project
 Freeway and Ramp Peak Hour Volumes - US Route 101
 2018 No Build - PM Peak Period





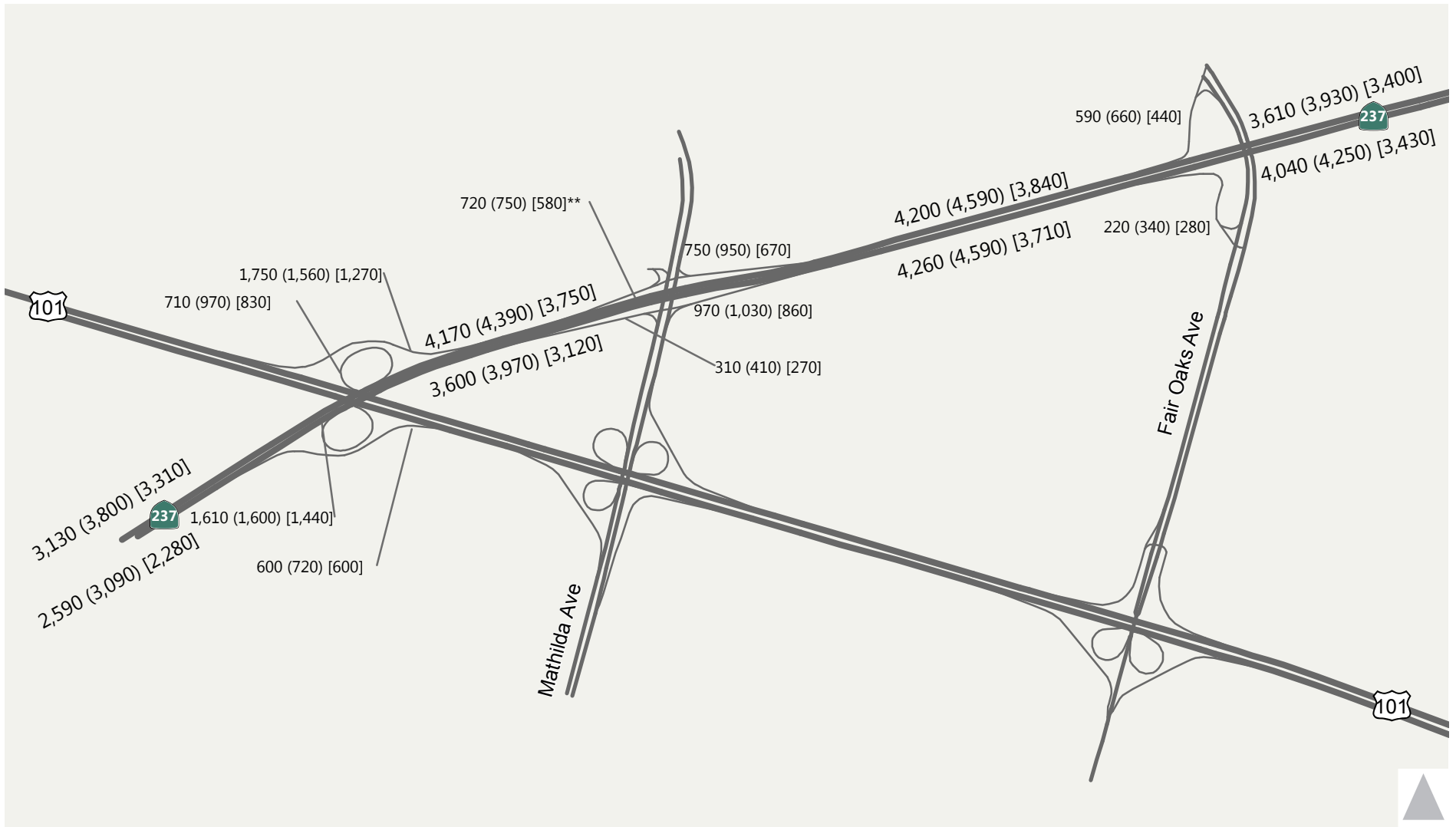
4:00 PM Volumes (5:00 PM Volumes) [6:00 PM Volumes]

* Ramp volume may differ from SR 237 ramp volume due to the slip ramp from Moffett Park Drive onto the SR 237 Off-Ramp/US 101 On-Ramp.

Figure 14A

Mathilda Interchange Project
 Freeway and Ramp Peak Hour Volumes - US Route 101
 2020 No Build - PM Peak Period



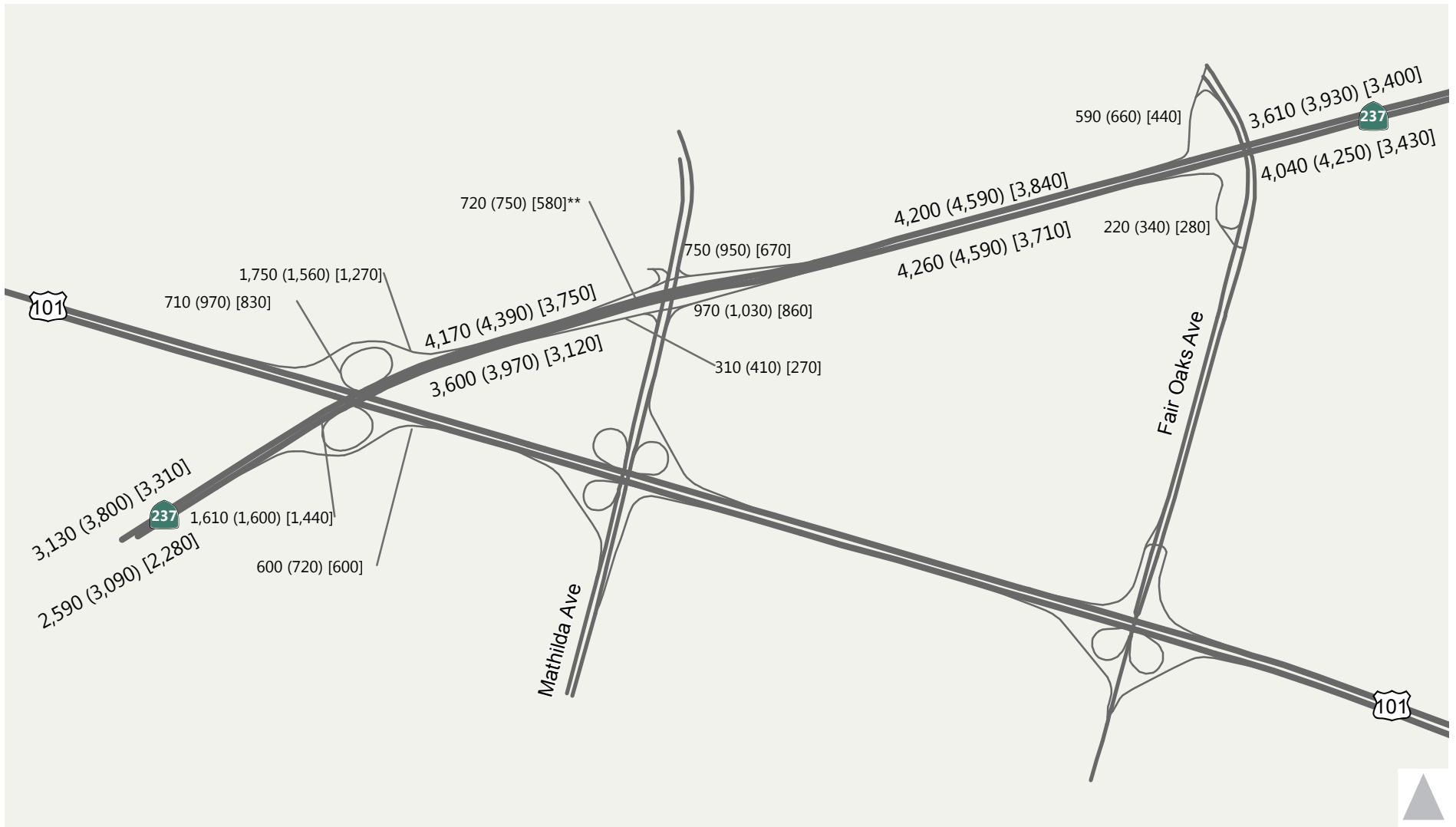


4:00 PM Volumes (5:00 PM Volumes) [6:00 PM Volumes]

** Ramp volume may not match ramp terminal intersection due to slip ramp from Moffett Park Drive.



Figure 14B
 Mathilda Interchange Project
 Freeway and Ramp Peak Hour Volumes - CA SR 237
 2018 No Build - PM Peak Period

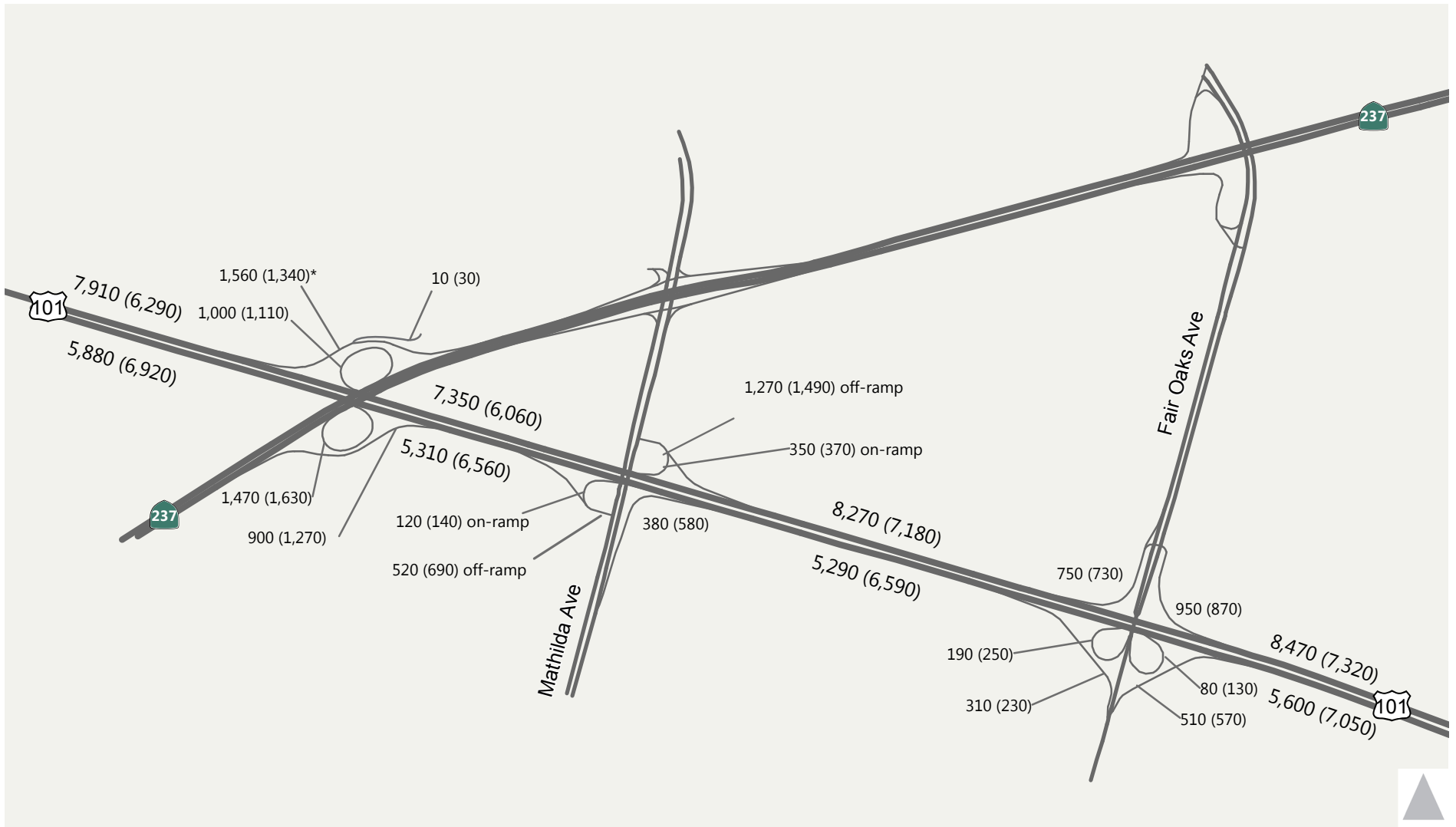


4:00 PM Volumes (5:00 PM Volumes) [6:00 PM Volumes]

** Ramp volume may not match ramp terminal intersection due to slip ramp from Moffett Park Drive.



Figure 14B
 Mathilda Interchange Project
 Freeway and Ramp Peak Hour Volumes - CA SR 237
 2018 No Build - PM Peak Period

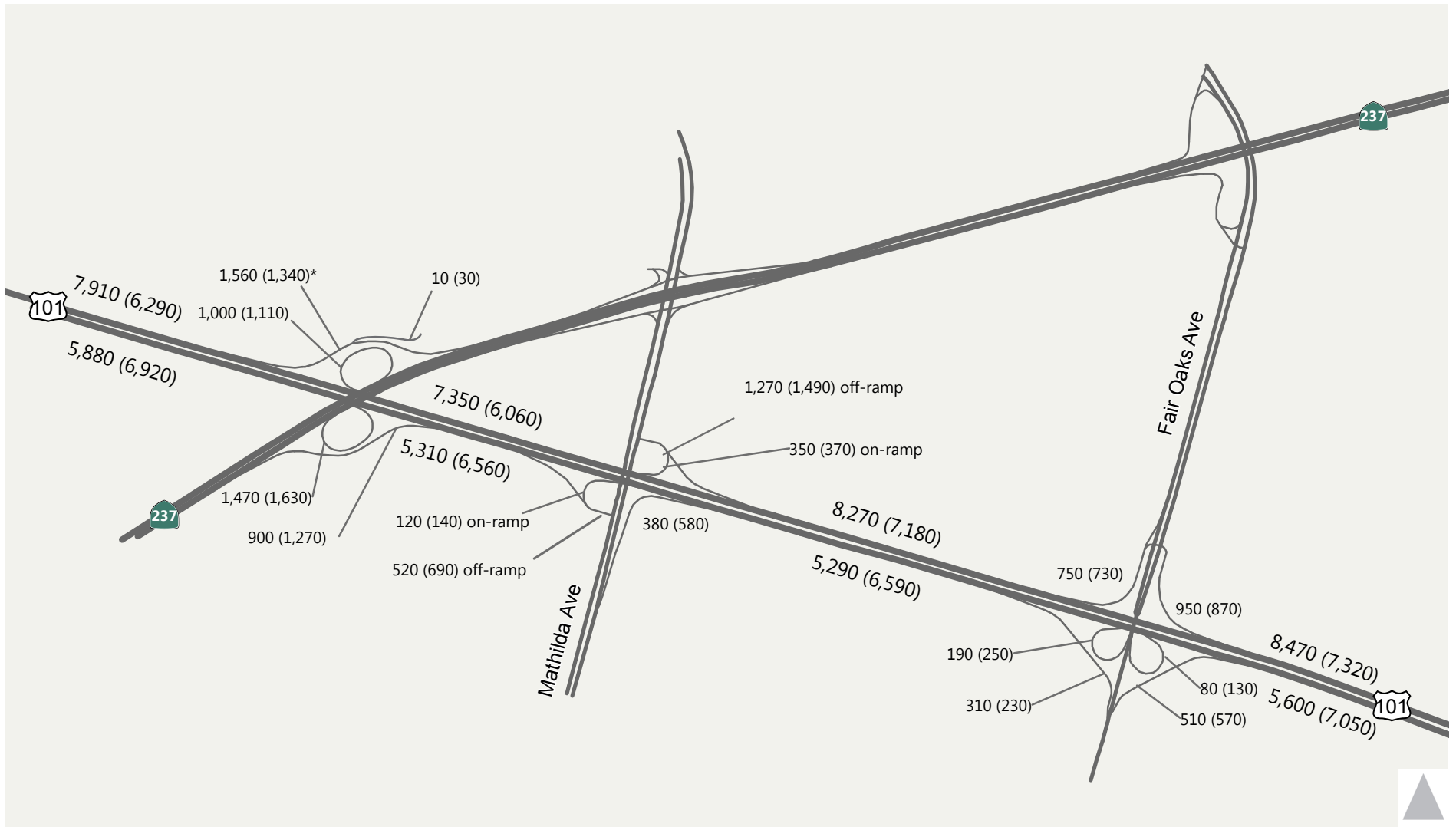


7:00 AM Volumes (8:00 AM Volumes)

* Ramp volume may differ from SR 237 ramp volume due to the slip ramp from Moffett Park Drive onto the SR 237 Off-Ramp/US 101 On-Ramp.

Figure 15A
 Mathilda Interchange Project
 Freeway and Ramp Peak Hour Volumes - US Route 101
 2018 Build- AM Peak Period





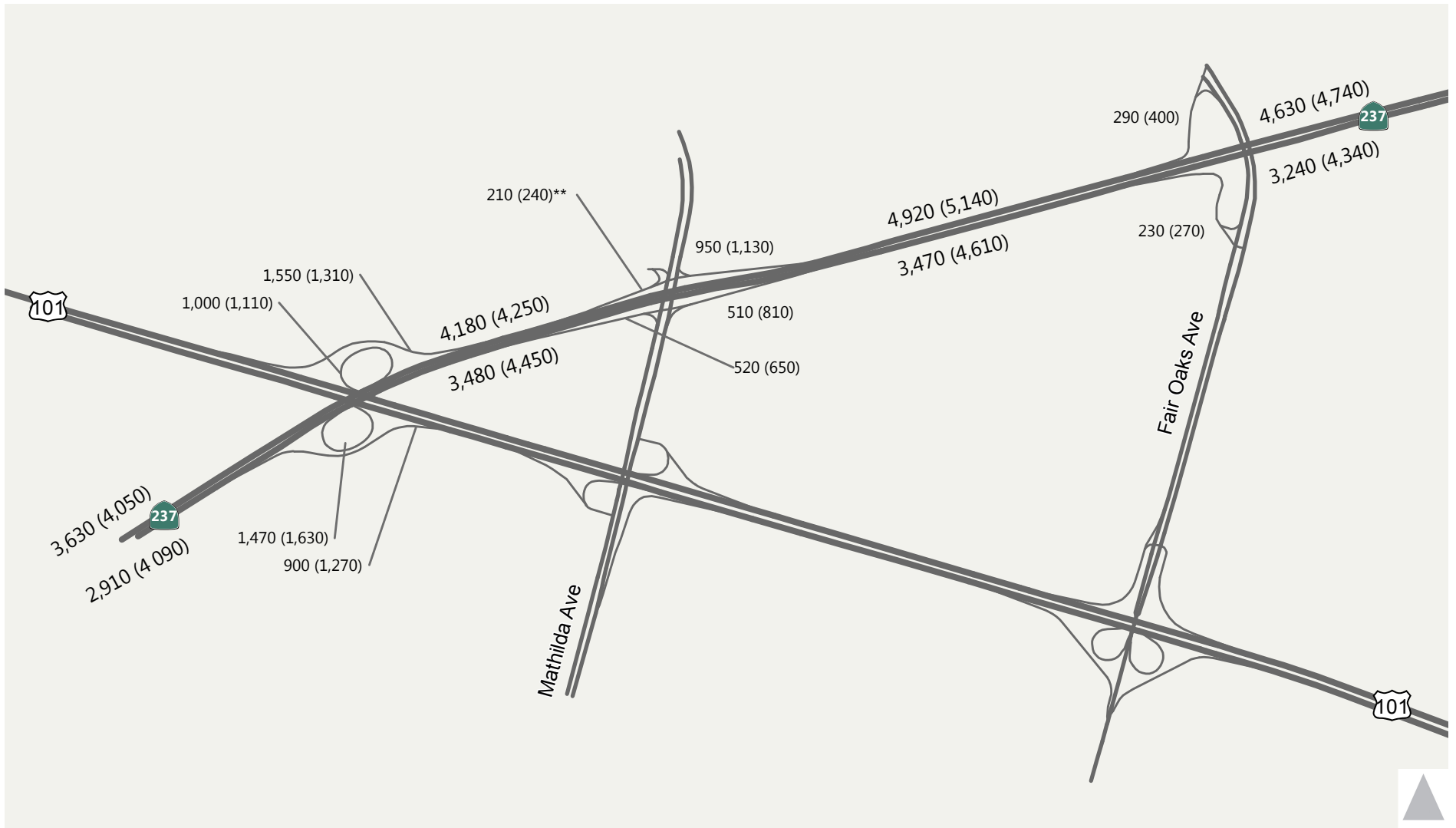
7:00 AM Volumes (8:00 AM Volumes)

* Ramp volume may differ from SR 237 ramp volume due to the slip ramp from Moffett Park Drive onto the SR 237 Off-Ramp/US 101 On-Ramp.

Figure 15A

Mathilda Interchange Project
 Freeway and Ramp Peak Hour Volumes - US Route 101
 2020 Build- AM Peak Period





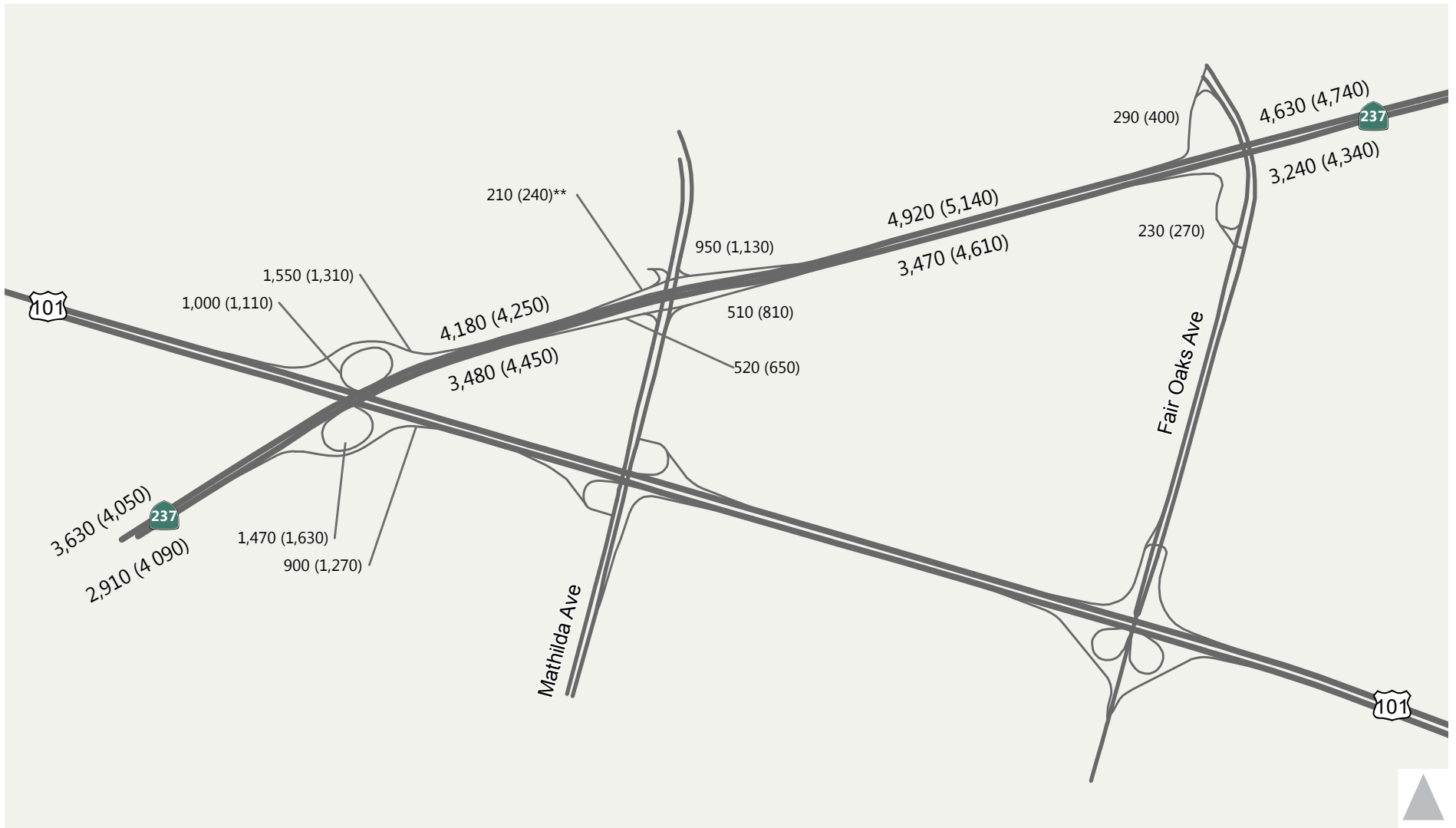
7:00 AM Volumes (8:00 AM Volumes)

** Ramp volume may not match ramp terminal intersection due to slip ramp from Moffett Park Drive.

Figure 15B

Mathilda Interchange Project
 Freeway and Ramp Peak Hour Volumes - CA SR 237
 2018 Build - AM Peak Period





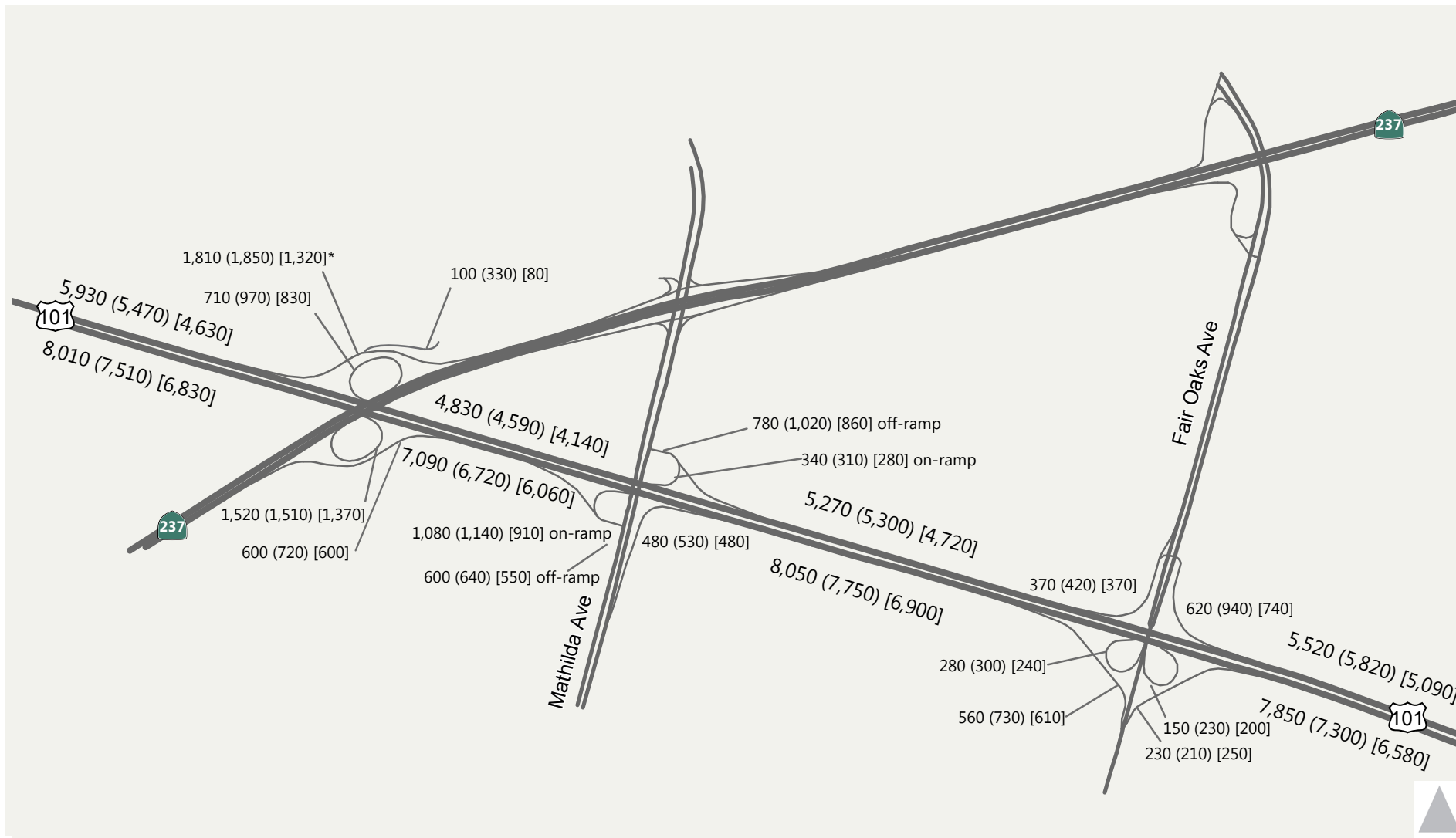
7:00 AM Volumes (8:00 AM Volumes)

** Ramp volume may not match ramp terminal intersection due to slip ramp from Moffett Park Drive.

Figure 15B

Mathilda Interchange Project
 Freeway and Ramp Peak Hour Volumes - CA SR 237
 2020 Build - AM Peak Period





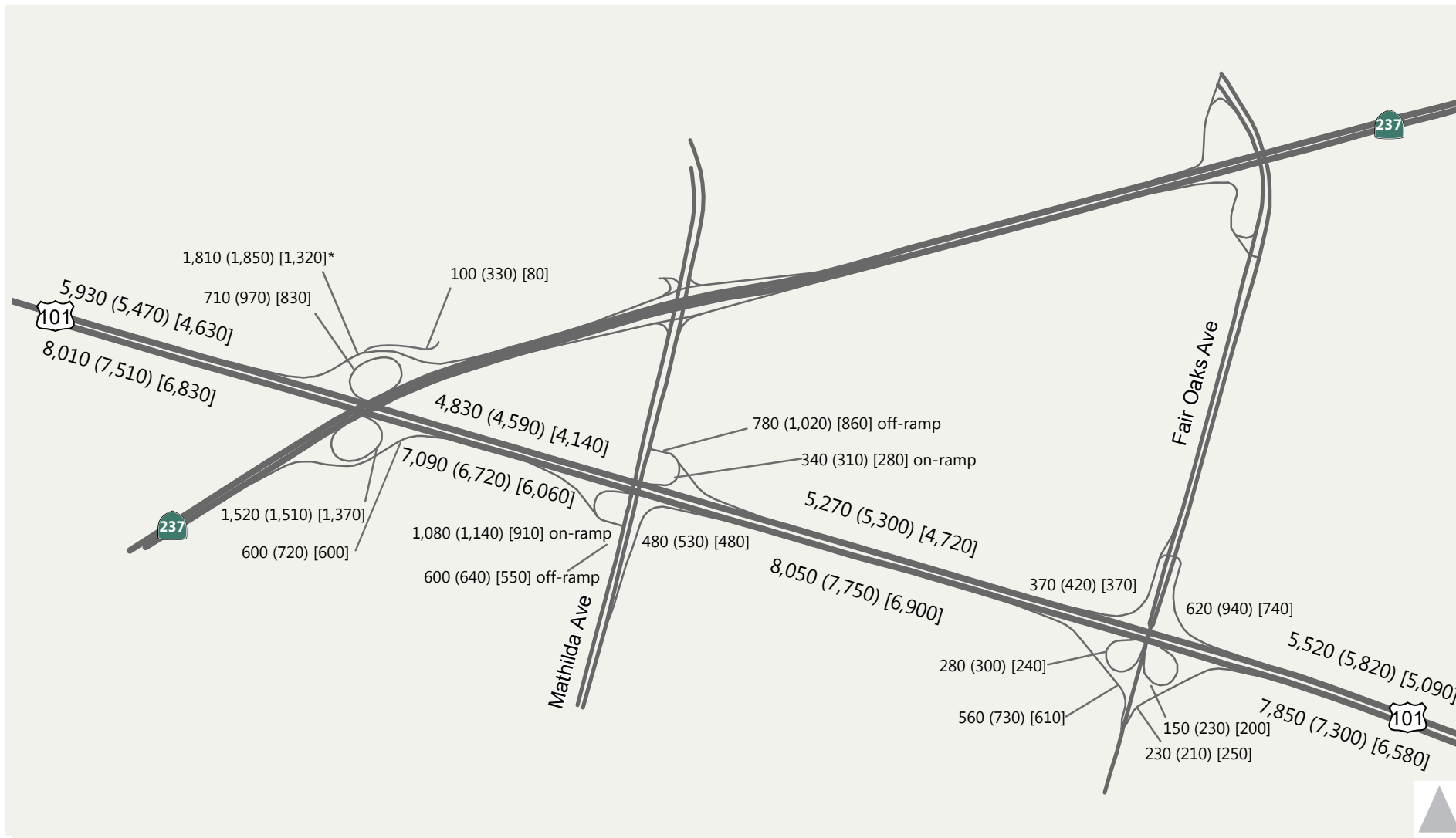
4:00 PM Volumes (5:00 PM Volumes) [6:00 PM Volumes]

* Ramp volume may differ from SR 237 ramp volume due to the slip ramp from Moffett Park Drive onto the SR 237 Off-Ramp/US 101 On-Ramp.

Figure 16A

Mathilda Interchange Project
 Freeway and Ramp Peak Hour Volumes - US Route 101
 2018 Build - PM Peak Period





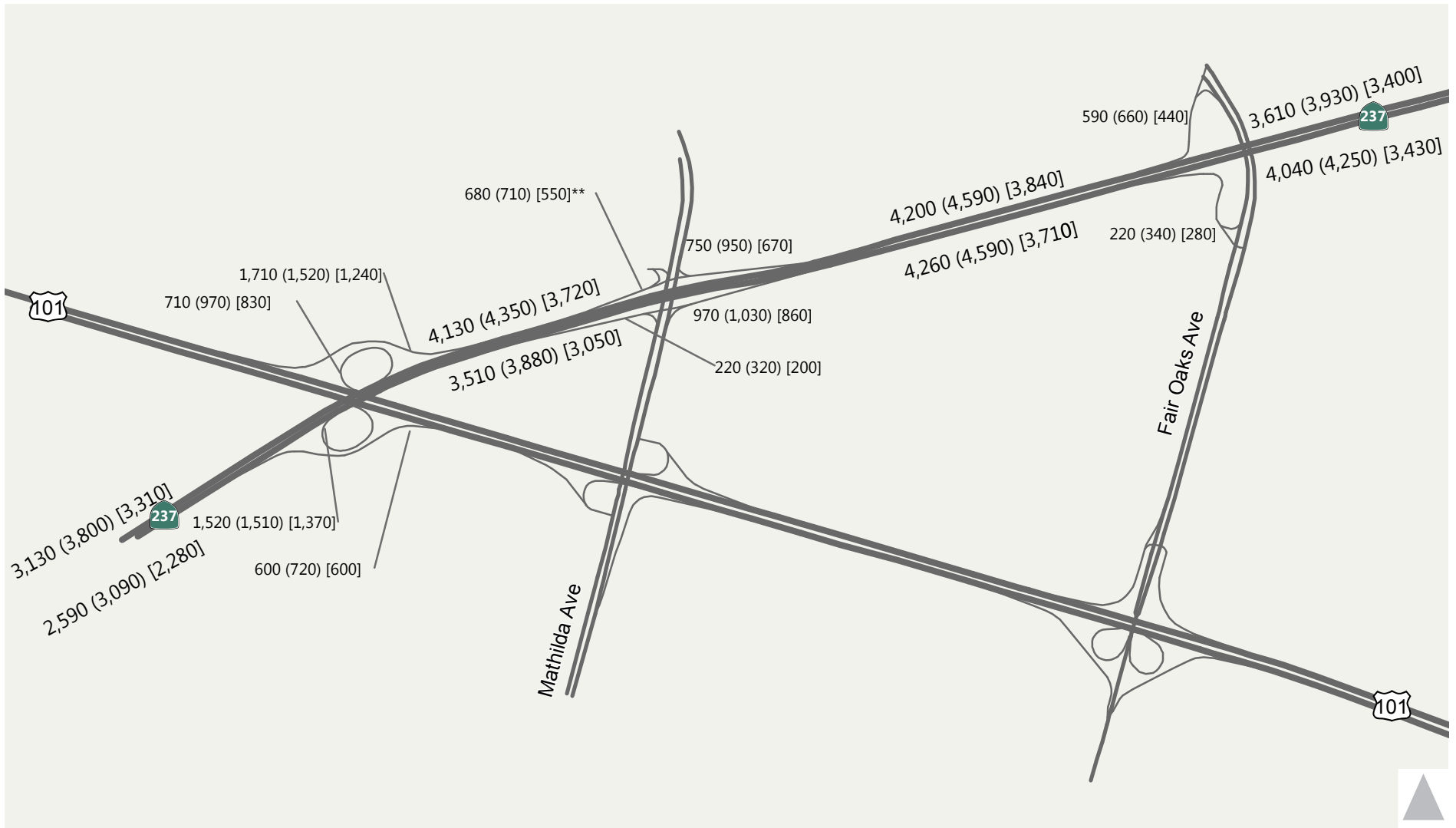
4:00 PM Volumes (5:00 PM Volumes) [6:00 PM Volumes]

* Ramp volume may differ from SR 237 ramp volume due to the slip ramp from Moffett Park Drive onto the SR 237 Off-Ramp/US 101 On-Ramp.

Figure 16A

Mathilda Interchange Project
 Freeway and Ramp Peak Hour Volumes - US Route 101
 2020 Build - PM Peak Period



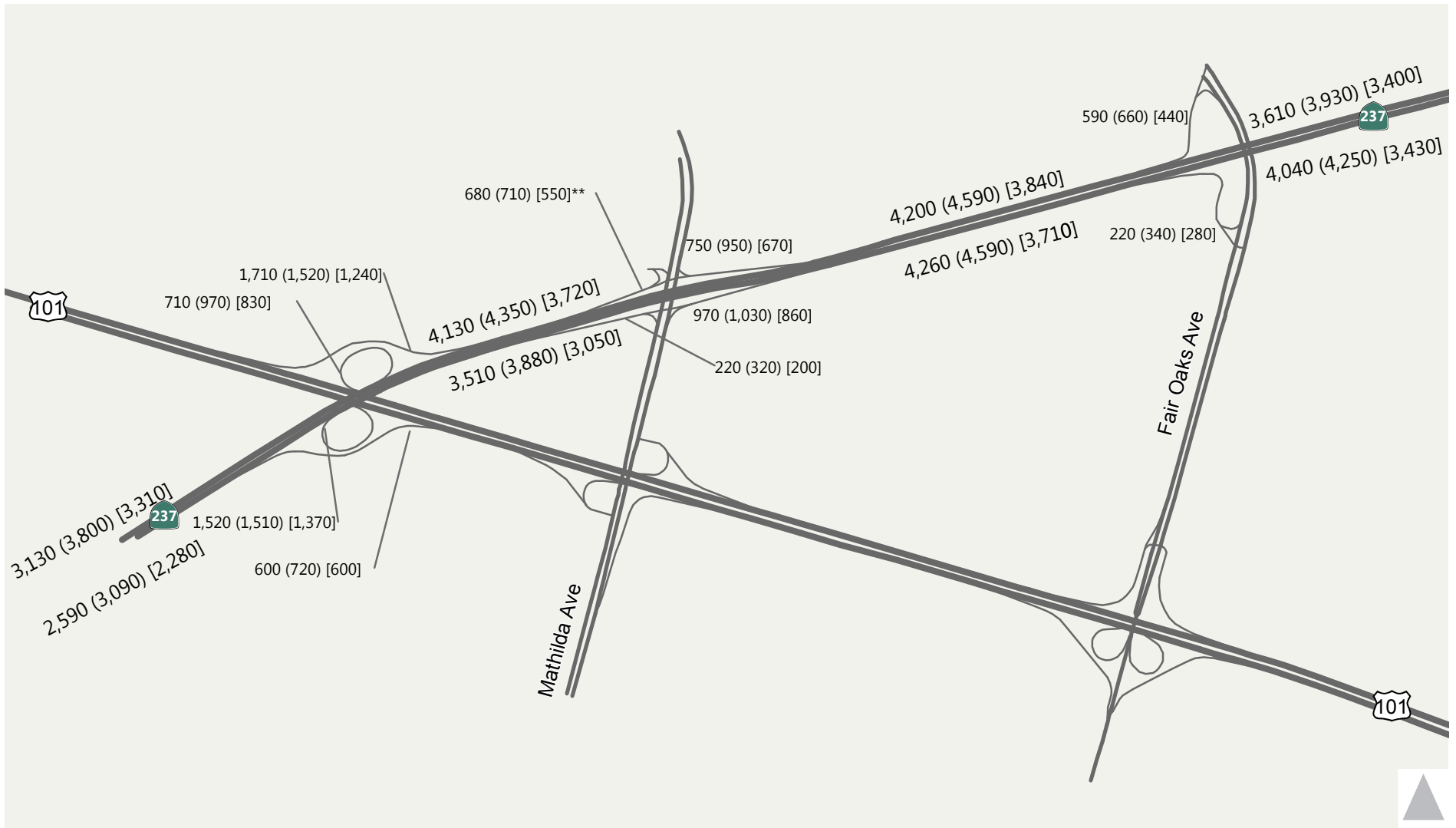


4:00 PM Volumes (5:00 PM Volumes) [6:00 PM Volumes]

** Ramp volume may not match ramp terminal intersection due to slip ramp from Moffett Park Drive.



Figure 16B
 Mathilda Interchange Project
 Freeway and Ramp Peak Hour Volumes - CA SR 237
 2018 Build - PM Peak Period

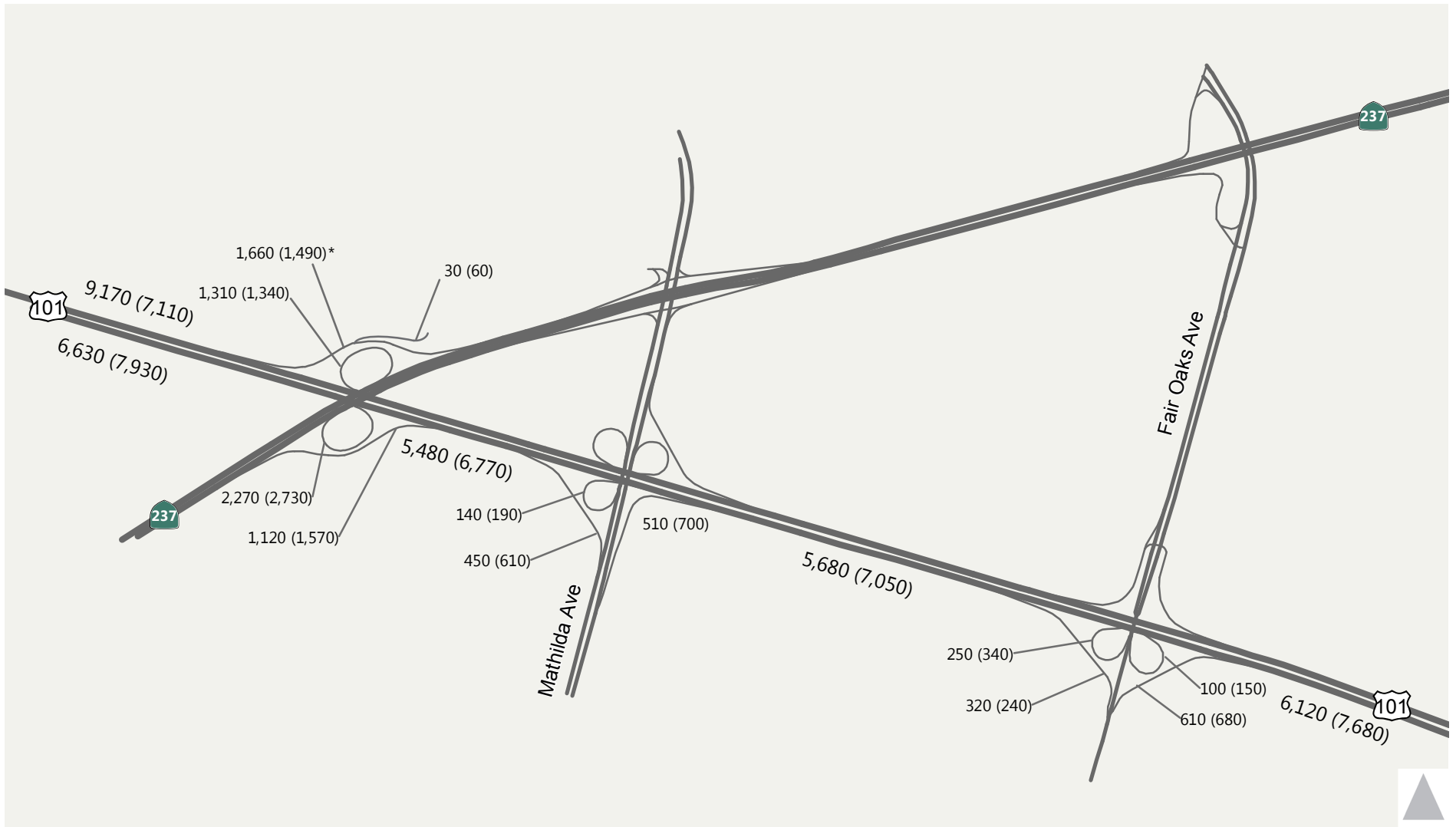


4:00 PM Volumes (5:00 PM Volumes) [6:00 PM Volumes]

** Ramp volume may not match ramp terminal intersection due to slip ramp from Moffett Park Drive.



Figure 16B
 Mathilda Interchange Project
 Freeway and Ramp Peak Hour Volumes - CA SR 237
 2020 Build - PM Peak Period



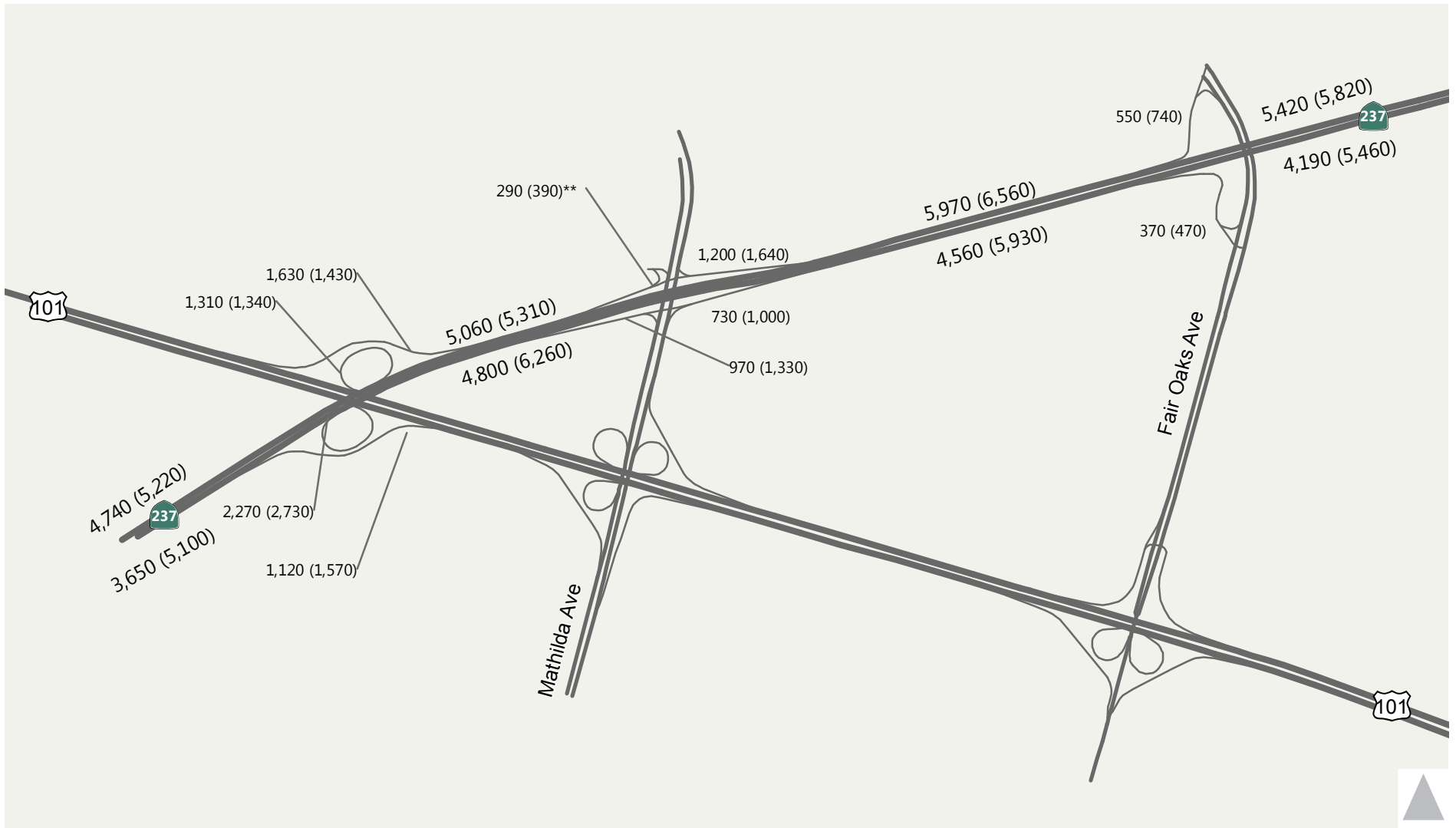
7:00 AM Volumes (8:00 AM Volumes)

* Ramp volume may differ from SR 237 ramp volume due to the slip ramp from Moffett Park Drive onto the SR 237 Off-Ramp/US 101 On-Ramp.

Figure 17A

Mathilda Interchange Project
 Freeway and Ramp Peak Hour Volumes - US Route 101
 2040 No Build - AM Peak Period





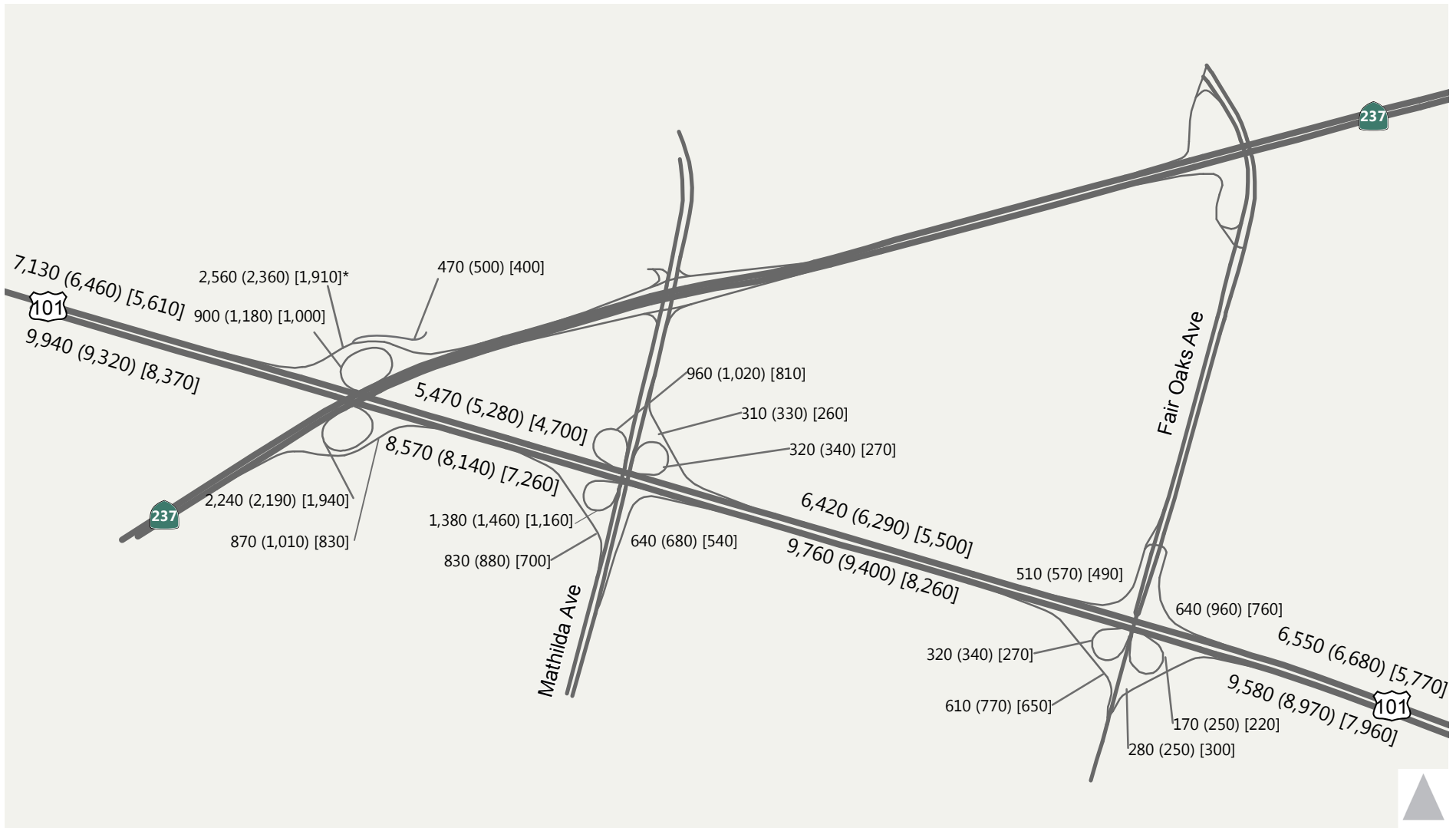
7:00 AM Volumes (8:00 AM Volumes)

** Ramp volume may not match ramp terminal intersection due to slip ramp from Moffett Park Drive.

Figure 17B

Mathilda Interchange Project
 Freeway and Ramp Peak Hour Volumes - CA SR 237
 2040 No Build - AM Peak Period





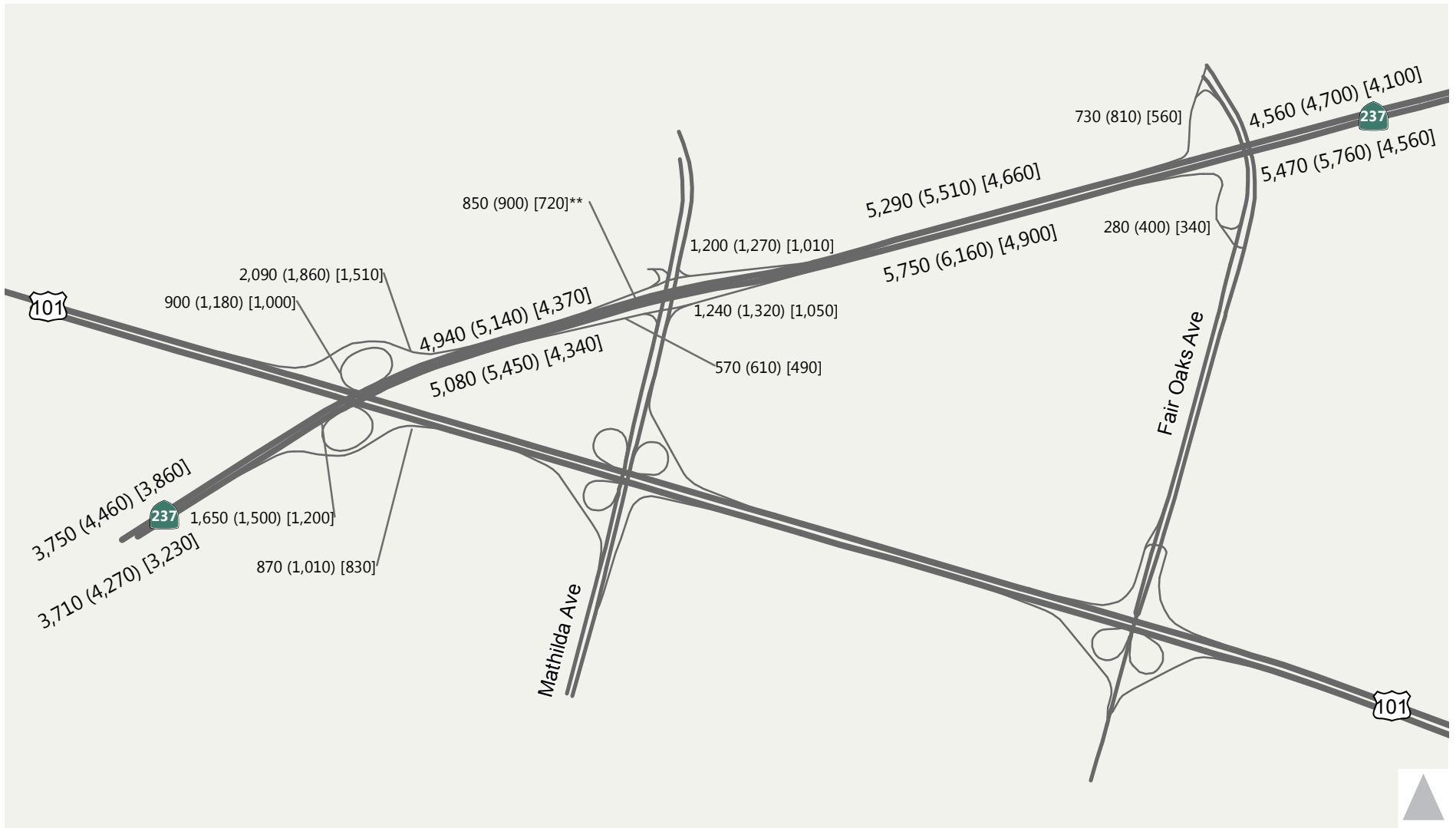
4:00 PM Volumes (5:00 PM Volumes) [6:00 PM Volumes]

* Ramp volume may differ from SR 237 ramp volume due to the slip ramp from Moffett Park Drive onto the SR 237 Off-Ramp/US 101 On-Ramp.

Figure 18A

Mathilda Interchange Project
 Freeway and Ramp Peak Hour Volumes - US Route 101
 2040 No Build - PM Peak Period





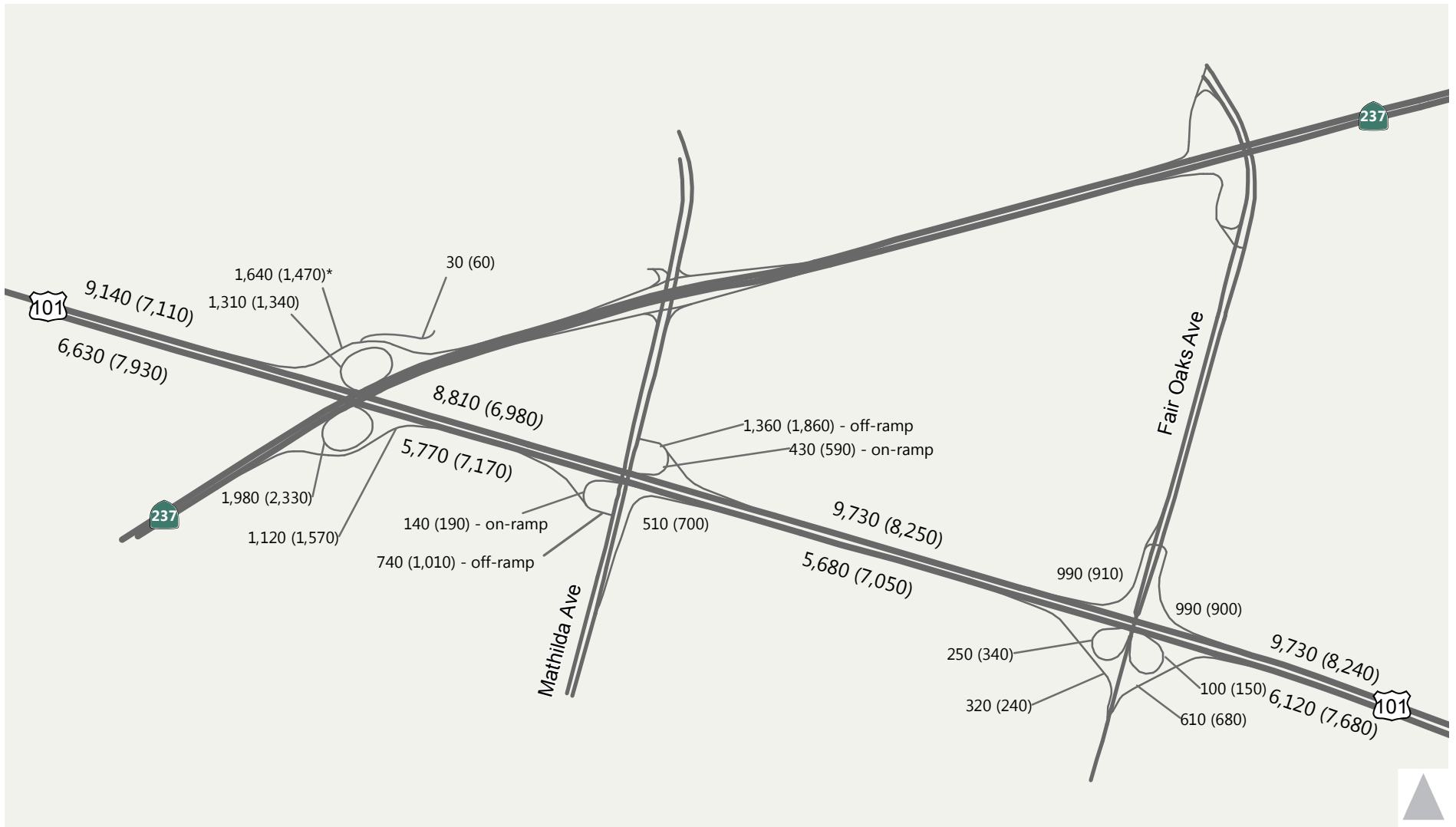
4:00 PM Volumes (5:00 PM Volumes) [6:00 PM Volumes]

** Ramp volume may not match ramp terminal intersection due to slip ramp from Moffett Park Drive.

Figure 18B

Mathilda Interchange Project
 Freeway and Ramp Peak Hour Volumes - CA SR 237
 2040 No Build - PM Peak Period





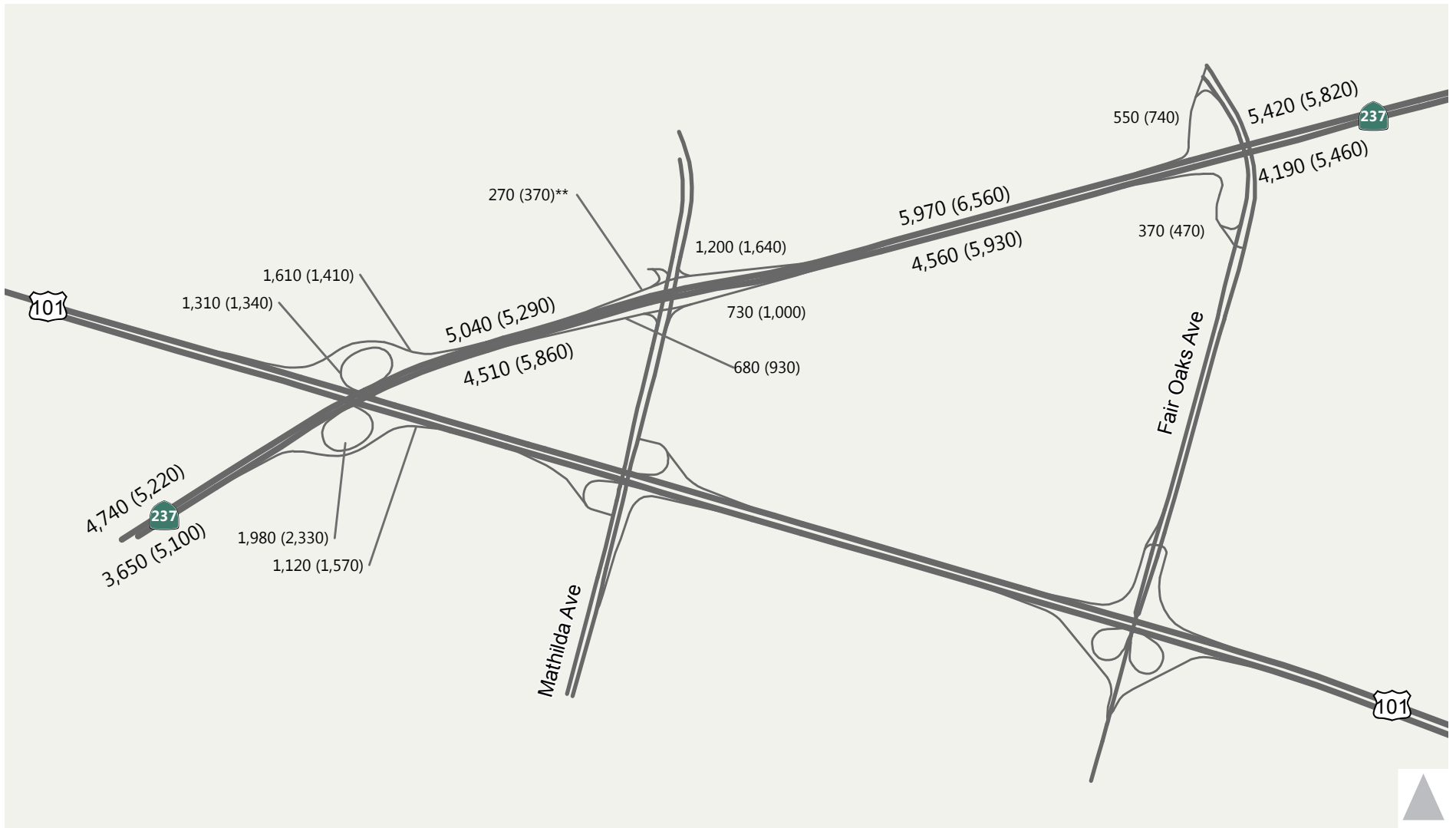
7:00 AM Volumes (8:00 AM Volumes)

* Ramp volume may differ from SR 237 ramp volume due to the slip ramp from Moffett Park Drive onto the SR 237 Off-Ramp/US 101 On-Ramp.

Figure 19A

Mathilda Interchange Project
 Freeway and Ramp Peak Hour Volumes - US Route 101
 2040 Build- AM Peak Period



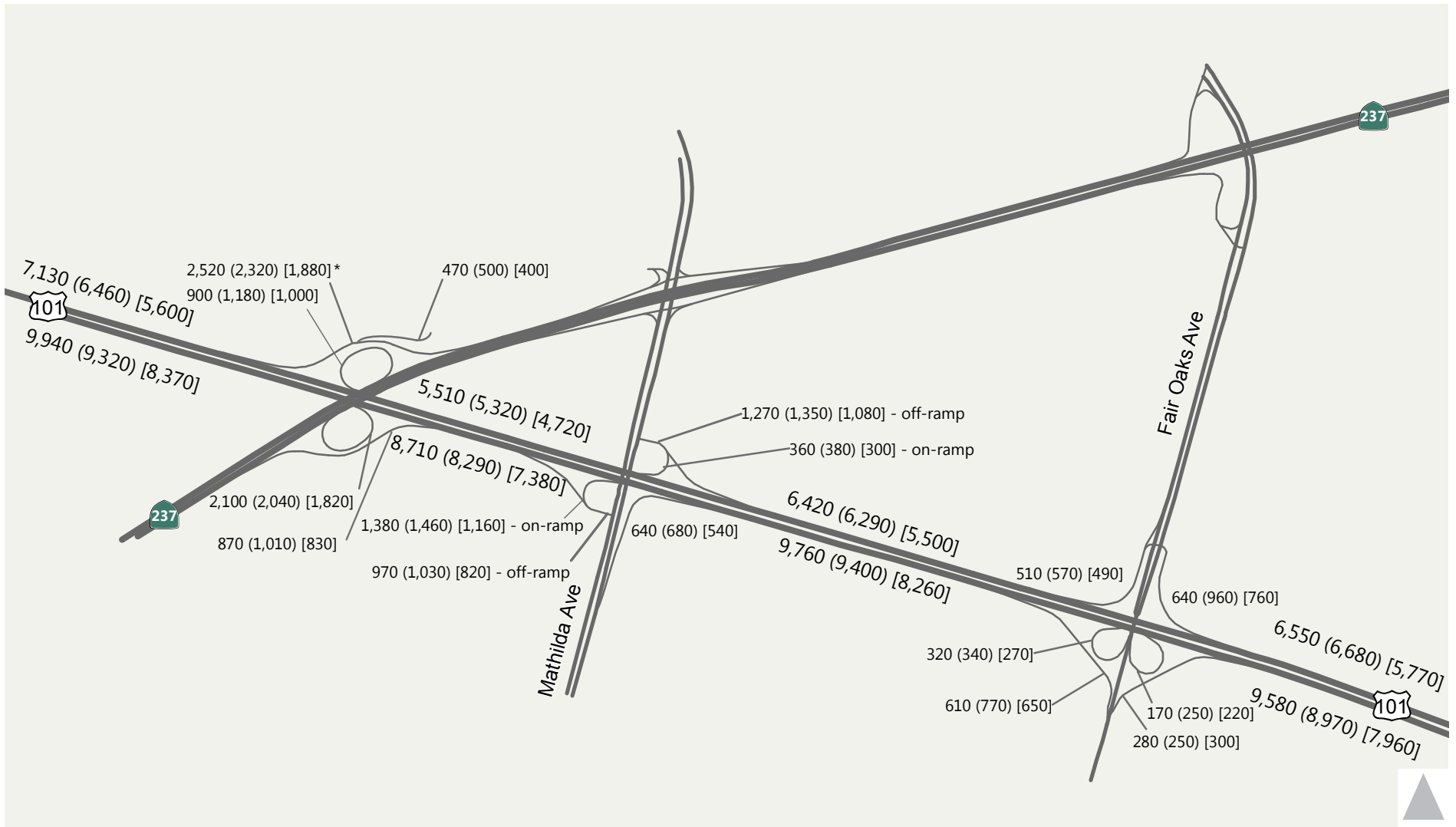


7:00 AM Volumes (8:00 AM Volumes)

** Ramp volume may not match ramp terminal intersection due to slip ramp from Moffett Park Drive.



Figure 19B
 Mathilda Interchange Project
 Freeway and Ramp Peak Hour Volumes - CA SR 237
 2040 Build - AM Peak Period



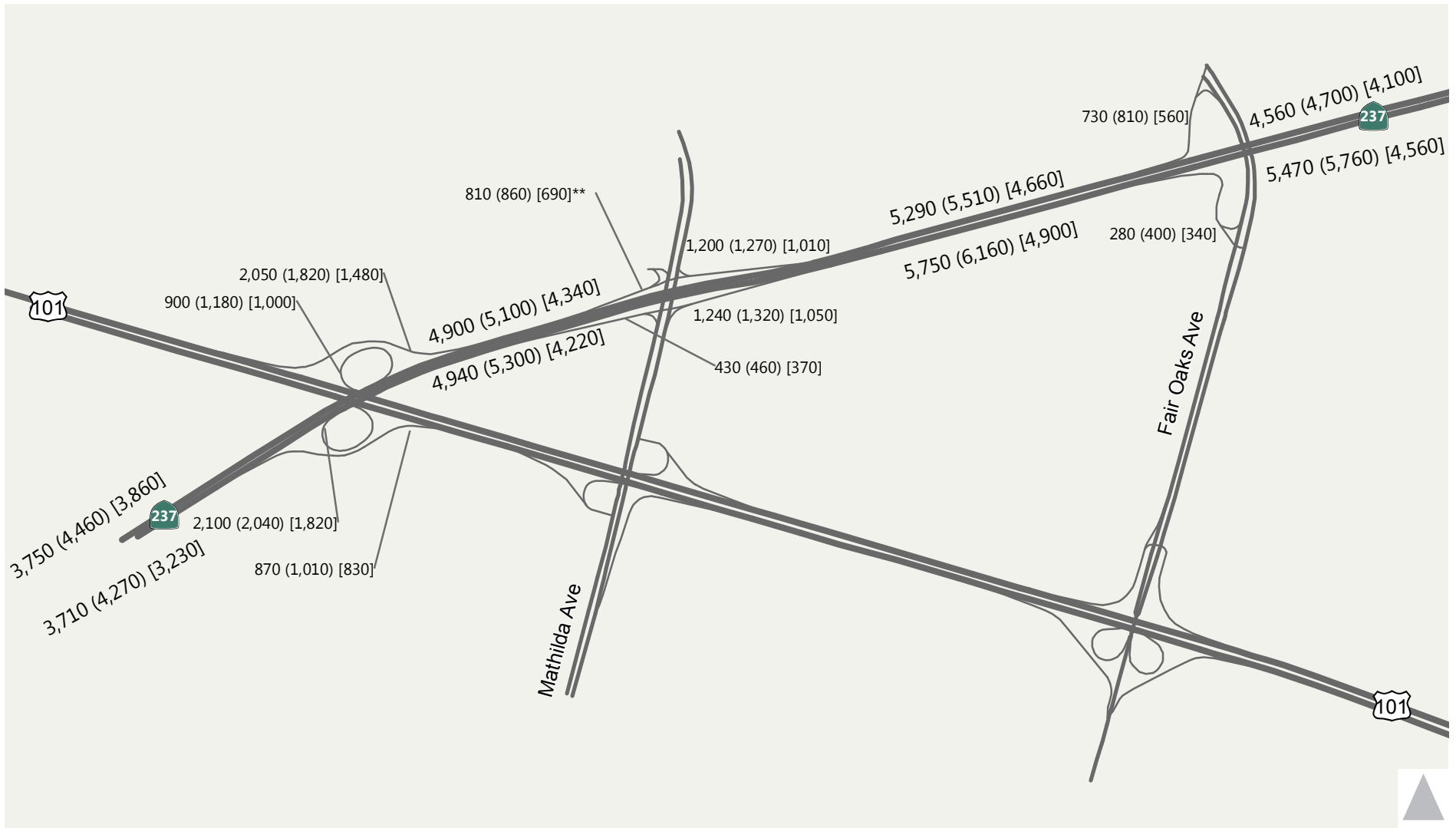
4:00 PM Volumes (5:00 PM Volumes) [6:00 PM Volumes]

* Ramp volume may differ from SR 237 ramp volume due to the slip ramp from Moffett Park Drive onto the SR 237 Off-Ramp/US 101 On-Ramp.

Figure 20A

Mathilda Interchange Project
 Freeway and Ramp Peak Hour Volumes - US Route 101
 2040 Build - PM Peak Period





4:00 PM Volumes (5:00 PM Volumes) [6:00 PM Volumes]

** Ramp volume may not match ramp terminal intersection due to slip ramp from Moffett Park Drive.

Figure 20B

Mathilda Interchange Project
 Freeway and Ramp Peak Hour Volumes - CA SR 237
 2040 Build - PM Peak Period

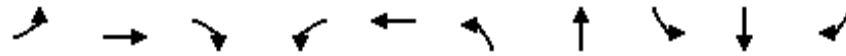


APPENDIX L – YEAR 2018 INTERSECTION CALCULATION SHEETS



Lanes, Volumes, Timings
1: Mathilda Ave & 5th Ave

3/4/2016

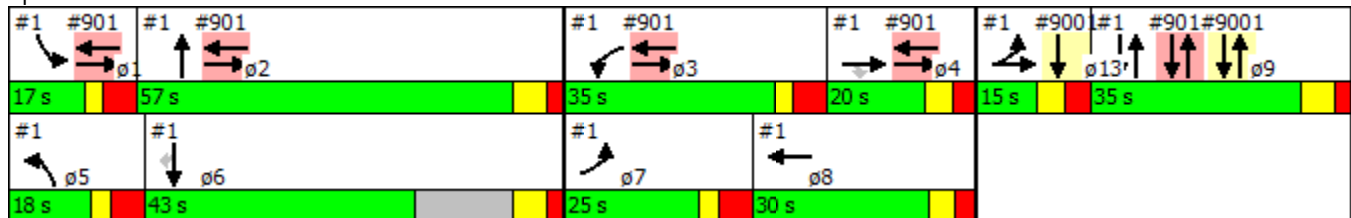


| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT | SBR | ø2 | ø7 |
|----------------------|------|------|--------|-------|-------|-------|-----|------|-----|--------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 20 | 10 | 30 | 30 | 10 | 80 | 860 | 10 | 370 | 70 | | |
| Turn Type | Prot | NA | custom | Prot | NA | Prot | NA | Prot | NA | custom | | |
| Protected Phases | 7 13 | 4 13 | | 3 | 8 | 5 | 2 9 | 1 | 6 9 | | 2 | 7 |
| Permitted Phases | | | 4 | | | | | | | 6 | | |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 5 | 2 | 1 | 6 | 6 | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 13.0 | 12.0 | 8.0 | 11.0 | | 10.0 | | 12.0 | 12.0 | 12.0 |
| Minimum Split (s) | | | 20.0 | 19.0 | 29.5 | 18.0 | | 17.0 | | 41.0 | 35.0 | 19.0 |
| Total Split (s) | | | 20.0 | 35.0 | 30.0 | 18.0 | | 17.0 | | 43.0 | 57.0 | 25.0 |
| Total Split (%) | | | 11.2% | 19.6% | 16.8% | 10.1% | | 9.5% | | 24.0% | 32% | 14% |
| Yellow Time (s) | | | 3.6 | 2.5 | 3.6 | 2.5 | | 2.5 | | 4.7 | 4.7 | 2.5 |
| All-Red Time (s) | | | 3.4 | 4.5 | 2.9 | 4.5 | | 4.5 | | 2.3 | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | | 0.0 | | |
| Total Lost Time (s) | | | 7.0 | 7.0 | 6.5 | 7.0 | | 7.0 | | 7.0 | | |
| Lead/Lag | | | Lag | Lead | Lag | Lead | | Lead | | Lag | Lag | Lead |
| Lead-Lag Optimize? | | | Yes | Yes | Yes | Yes | | Yes | | Yes | Yes | Yes |
| Recall Mode | | | None | None | None | None | | None | | Min | Min | None |

Intersection Summary

Cycle Length: 179
 Actuated Cycle Length: 84.7
 Natural Cycle: 160
 Control Type: Actuated-Uncoordinated

Splits and Phases: 1: Mathilda Ave & 5th Ave

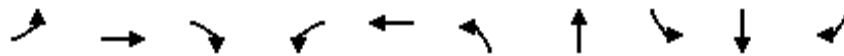


| Lane Group | ø9 | ø13 |
|----------------------|------|------|
| Lane Configurations | | |
| Volume (vph) | | |
| Turn Type | | |
| Protected Phases | 9 | 13 |
| Permitted Phases | | |
| Detector Phase | | |
| Switch Phase | | |
| Minimum Initial (s) | 28.0 | 8.0 |
| Minimum Split (s) | 35.0 | 15.0 |
| Total Split (s) | 35.0 | 15.0 |
| Total Split (%) | 20% | 8% |
| Yellow Time (s) | 4.7 | 3.6 |
| All-Red Time (s) | 2.3 | 3.4 |
| Lost Time Adjust (s) | | |
| Total Lost Time (s) | | |
| Lead/Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes |
| Recall Mode | None | None |
| Intersection Summary | | |

Lanes, Volumes, Timings

2: Mathilda Ave & Innovation Way

3/4/2016

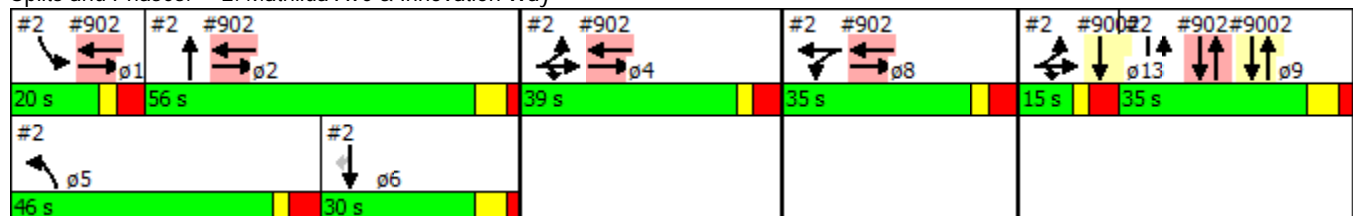


| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT | SBR | ø2 | ø4 |
|----------------------|-------|------|------|-------|-------|-------|------|-------|-----|--------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 20 | 0 | 50 | 20 | 10 | 730 | 990 | 10 | 290 | 130 | | |
| Turn Type | Split | NA | Prot | Split | NA | Prot | NA | Prot | NA | custom | | |
| Protected Phases | 4 13 | 4 13 | 4 13 | 8 | 8 | 5 | 2 9 | 1 | 6 9 | | 2 | 4 |
| Permitted Phases | | | | | | | | | | | | 6 |
| Detector Phase | 4 | 4 | 4 | 8 | 8 | 5 | 2 | 1 | 6 | 6 | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | | 10.0 | 10.0 | 13.0 | | 10.0 | | 12.0 | 12.0 | 14.0 |
| Minimum Split (s) | | | | 35.0 | 35.0 | 20.0 | | 16.8 | | 30.0 | 19.0 | 39.0 |
| Total Split (s) | | | | 35.0 | 35.0 | 46.0 | | 20.0 | | 30.0 | 56.0 | 39.0 |
| Total Split (%) | | | | 17.5% | 17.5% | 23.0% | | 10.0% | | 15.0% | 28% | 20% |
| Yellow Time (s) | | | | 2.5 | 2.5 | 2.5 | | 2.5 | | 4.7 | 4.7 | 2.5 |
| All-Red Time (s) | | | | 4.5 | 4.5 | 4.5 | | 4.3 | | 2.3 | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | | 0.0 | 0.0 | 0.0 | | 0.0 | | 0.0 | | |
| Total Lost Time (s) | | | | 7.0 | 7.0 | 7.0 | | 6.8 | | 7.0 | | |
| Lead/Lag | | | | | | | Lead | Lead | | Lag | Lag | |
| Lead-Lag Optimize? | | | | | | | Yes | Yes | | Yes | Yes | |
| Recall Mode | | | | None | None | None | | None | | Min | Min | None |

Intersection Summary

Cycle Length: 200
 Actuated Cycle Length: 112.3
 Natural Cycle: 175
 Control Type: Actuated-Uncoordinated

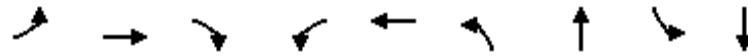
Splits and Phases: 2: Mathilda Ave & Innovation Way



| Lane Group | ø9 | ø13 |
|----------------------|------|------|
| Lane Configurations | | |
| Volume (vph) | | |
| Turn Type | | |
| Protected Phases | 9 | 13 |
| Permitted Phases | | |
| Detector Phase | | |
| Switch Phase | | |
| Minimum Initial (s) | 28.0 | 8.0 |
| Minimum Split (s) | 35.0 | 15.0 |
| Total Split (s) | 35.0 | 15.0 |
| Total Split (%) | 18% | 8% |
| Yellow Time (s) | 4.7 | 2.5 |
| All-Red Time (s) | 2.3 | 4.5 |
| Lost Time Adjust (s) | | |
| Total Lost Time (s) | | |
| Lead/Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes |
| Recall Mode | None | None |
| Intersection Summary | | |

Lanes, Volumes, Timings
 3: Mathilda Ave & Moffett Park Dr

3/4/2016

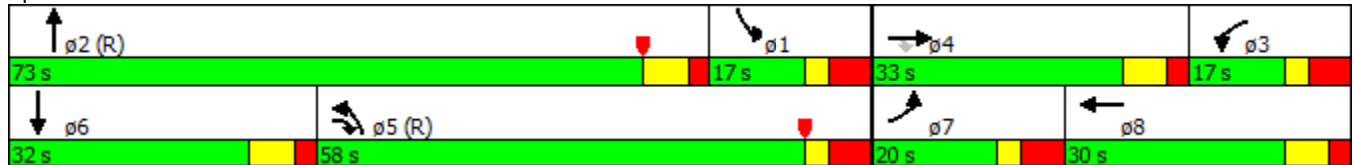


| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↶ | ↷ | ↷ | ↶↷ | ↷ | ↶↷ | ↑↑↷ | ↶ | ↑↑↑ |
| Volume (vph) | 40 | 60 | 50 | 80 | 210 | 710 | 1720 | 10 | 240 |
| Turn Type | Prot | NA | pm+ov | Prot | NA | Prot | NA | Prot | NA |
| Protected Phases | 7 | 4 | 5 | 3 | 8 | 5 | 2 | 1 | 6 |
| Permitted Phases | | | 4 | | | | | | |
| Detector Phase | 7 | 4 | 5 | 3 | 8 | 5 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | | |
| Minimum Initial (s) | 8.0 | 8.0 | 4.0 | 8.0 | 8.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | 15.0 | 15.0 | 11.0 | 15.0 | 30.0 | 11.0 | 32.9 | 11.0 | 10.9 |
| Total Split (s) | 20.0 | 33.0 | 58.0 | 17.0 | 30.0 | 58.0 | 73.0 | 17.0 | 32.0 |
| Total Split (%) | 14.3% | 23.6% | 41.4% | 12.1% | 21.4% | 41.4% | 52.1% | 12.1% | 22.9% |
| Yellow Time (s) | 2.5 | 4.7 | 2.5 | 2.5 | 4.5 | 2.5 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 4.5 | 2.3 | 4.5 | 4.5 | 2.5 | 4.5 | 2.2 | 4.5 | 2.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.9 | 7.0 | 6.9 |
| Lead/Lag | Lead | Lead | Lag | Lag | Lag | Lag | Lead | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | C-Max | None | None | C-Max | C-Max | None | None |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 110 (79%), Referenced to phase 2:NBT and 5:NBL, Start of Yellow
 Natural Cycle: 130
 Control Type: Actuated-Coordinated

Splits and Phases: 3: Mathilda Ave & Moffett Park Dr



Lanes, Volumes, Timings

4: Mathilda Ave & SR 237 Off/On Ramp/SR 237 EB On-Ramp

3/4/2016

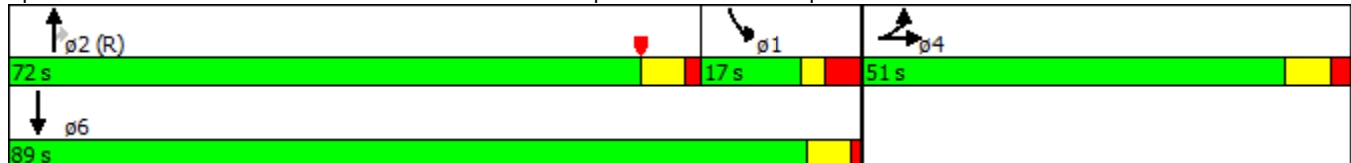


| Lane Group | EBL | EBT | NBT | NBR | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | |
| Volume (vph) | 860 | 0 | 2110 | 760 | 50 | 900 |
| Turn Type | Split | NA | NA | Perm | Prot | NA |
| Protected Phases | 4 | 4 | 2 | | 1 | 6 |
| Permitted Phases | | | | 2 | | |
| Detector Phase | 4 | 4 | 2 | 2 | 1 | 6 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | 12.0 | 12.0 | 20.7 | 20.7 | 10.4 | 10.7 |
| Total Split (s) | 51.0 | 51.0 | 72.0 | 72.0 | 17.0 | 89.0 |
| Total Split (%) | 36.4% | 36.4% | 51.4% | 51.4% | 12.1% | 63.6% |
| Yellow Time (s) | 4.8 | 4.8 | 4.7 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 2.2 | 2.2 | 1.5 | 1.5 | 3.9 | 1.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 6.2 | 6.2 | 6.4 | 5.9 |
| Lead/Lag | | | Lead | Lead | Lag | |
| Lead-Lag Optimize? | | | Yes | Yes | Yes | |
| Recall Mode | Max | Max | C-Max | C-Max | None | None |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 134 (96%), Referenced to phase 2:NBT, Start of Yellow
 Natural Cycle: 60
 Control Type: Actuated-Coordinated

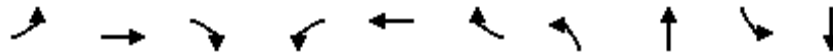
Splits and Phases: 4: Mathilda Ave & SR 237 Off/On Ramp/SR 237 EB On-Ramp



Lanes, Volumes, Timings

5: Mathilda Ave & Ross Dr

3/4/2016



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | | |
| Volume (vph) | 80 | 60 | 20 | 110 | 30 | 250 | 50 | 2540 | 50 | 880 |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | Prot | NA | Prot | NA |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | 1 | 6 |
| Permitted Phases | 4 | | 4 | 8 | | 8 | | | | |
| Detector Phase | 4 | 4 | 4 | 8 | 8 | 8 | 5 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 4.0 | 5.0 | 4.0 | 5.0 |
| Minimum Split (s) | 41.0 | 41.0 | 41.0 | 13.0 | 13.0 | 13.0 | 11.0 | 31.4 | 11.0 | 11.6 |
| Total Split (s) | 43.0 | 43.0 | 43.0 | 43.0 | 43.0 | 43.0 | 20.0 | 80.0 | 17.0 | 77.0 |
| Total Split (%) | 30.7% | 30.7% | 30.7% | 30.7% | 30.7% | 30.7% | 14.3% | 57.1% | 12.1% | 55.0% |
| Yellow Time (s) | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 2.5 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 3.4 | 3.4 | 3.4 | 3.4 | 3.4 | 3.4 | 4.5 | 1.7 | 4.5 | 1.9 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.4 | 7.0 | 6.6 |
| Lead/Lag | | | | | | | Lead | Lead | Lag | Lag |
| Lead-Lag Optimize? | | | | | | | Yes | Yes | Yes | Yes |
| Recall Mode | Max | Max | Max | None | None | None | None | C-Max | Max | None |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 0 (0%), Referenced to phase 2:NBT, Start of Yellow, Master Intersection
 Natural Cycle: 85
 Control Type: Actuated-Coordinated

Splits and Phases: 5: Mathilda Ave & Ross Dr



Lanes, Volumes, Timings
 8: Mathilda Ave & Almanor Ave/Ahwanee Ave

3/4/2016

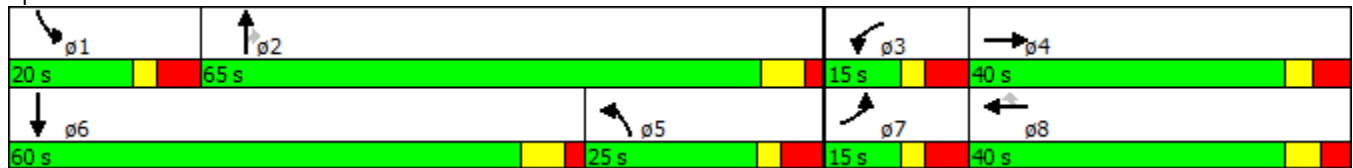


| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | | |
| Volume (vph) | 90 | 20 | 70 | 30 | 190 | 110 | 2650 | 50 | 160 | 1540 |
| Turn Type | Prot | NA | Prot | NA | Perm | Prot | NA | Perm | Prot | NA |
| Protected Phases | 7 | 4 | 3 | 8 | | 5 | 2 | | 1 | 6 |
| Permitted Phases | | | | | 8 | | | 2 | | |
| Detector Phase | 7 | 4 | 3 | 8 | 8 | 5 | 2 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 12.0 | 12.0 | 8.0 | 12.0 |
| Minimum Split (s) | 15.0 | 40.0 | 15.0 | 15.0 | 15.0 | 15.0 | 33.7 | 33.7 | 15.0 | 18.7 |
| Total Split (s) | 15.0 | 40.0 | 15.0 | 40.0 | 40.0 | 25.0 | 65.0 | 65.0 | 20.0 | 60.0 |
| Total Split (%) | 10.7% | 28.6% | 10.7% | 28.6% | 28.6% | 17.9% | 46.4% | 46.4% | 14.3% | 42.9% |
| Yellow Time (s) | 2.5 | 2.8 | 2.5 | 3.6 | 3.6 | 2.5 | 4.7 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 4.5 | 4.2 | 4.5 | 3.4 | 3.4 | 4.5 | 2.0 | 2.0 | 4.5 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.7 | 6.7 | 7.0 | 6.7 |
| Lead/Lag | Lead | Lag | Lead | Lag | Lag | Lag | Lag | Lag | Lead | Lead |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | None | Min | Min | None | Min |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 116
 Natural Cycle: 135
 Control Type: Actuated-Uncoordinated

Splits and Phases: 8: Mathilda Ave & Almanor Ave/Ahwanee Ave



Lanes, Volumes, Timings
 9: US 101 On-Ramp & Moffett Park Dr

3/4/2016



| Lane Group | EBT | EBR | WBL | WBT |
|----------------------|-------|-------|-------|--------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ |
| Volume (vph) | 180 | 10 | 20 | 920 |
| Turn Type | NA | Perm | Prot | NA |
| Protected Phases | 2 | | 1 | 6 |
| Permitted Phases | | 2 | | |
| Detector Phase | 2 | 2 | 1 | 6 |
| Switch Phase | | | | |
| Minimum Initial (s) | 15.0 | 15.0 | 6.0 | 15.0 |
| Minimum Split (s) | 20.0 | 20.0 | 10.5 | 20.0 |
| Total Split (s) | 62.0 | 62.0 | 13.0 | 75.0 |
| Total Split (%) | 82.7% | 82.7% | 17.3% | 100.0% |
| Yellow Time (s) | 4.0 | 4.0 | 3.5 | 4.0 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.0 | 5.0 | 4.5 | 5.0 |
| Lead/Lag | Lag | Lag | Lead | |
| Lead-Lag Optimize? | | | | |
| Recall Mode | Min | Min | None | Min |

Intersection Summary

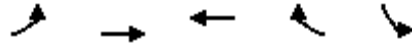
Cycle Length: 75
 Actuated Cycle Length: 41
 Natural Cycle: 40
 Control Type: Semi Act-Uncoord

Splits and Phases: 9: US 101 On-Ramp & Moffett Park Dr



Lanes, Volumes, Timings
 10: Moffett Park Dr & Innovation Way

3/4/2016

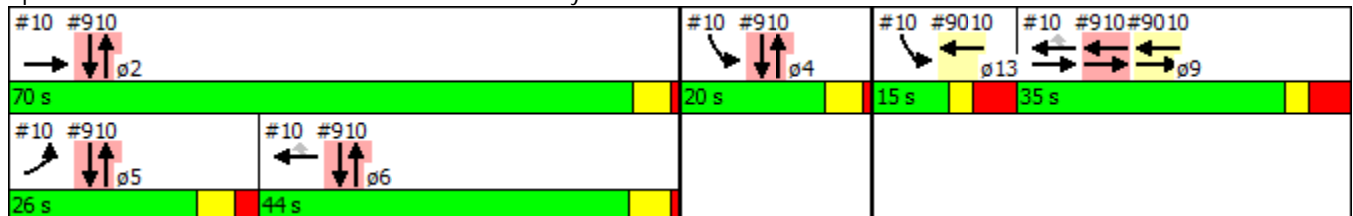


| Lane Group | EBL | EBT | WBT | WBR | SBL | ø2 | ø4 | ø6 | ø9 | ø13 |
|----------------------|-------|-----|-----|------|------|------|------|------|------|------|
| Lane Configurations | ↶ | ↕↕ | ↕↕ | ↷ | ↶↶↶ | | | | | |
| Volume (vph) | 50 | 130 | 830 | 200 | 40 | | | | | |
| Turn Type | Prot | NA | NA | Perm | Prot | | | | | |
| Protected Phases | 5 | 2 9 | 6 9 | | 4 13 | 2 | 4 | 6 | 9 | 13 |
| Permitted Phases | | | | 6 9 | | | | | | |
| Detector Phase | 5 | 2 | 6 | 6 9 | 4 | | | | | |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 8.0 | | | | | 10.0 | 10.0 | 10.0 | 28.0 | 8.0 |
| Minimum Split (s) | 14.5 | | | | | 14.9 | 15.0 | 15.5 | 35.0 | 15.0 |
| Total Split (s) | 26.0 | | | | | 70.0 | 20.0 | 44.0 | 35.0 | 15.0 |
| Total Split (%) | 18.6% | | | | | 50% | 14% | 31% | 25% | 11% |
| Yellow Time (s) | 4.0 | | | | | 3.9 | 4.0 | 4.5 | 2.5 | 2.5 |
| All-Red Time (s) | 2.5 | | | | | 1.0 | 1.0 | 1.0 | 4.5 | 4.5 |
| Lost Time Adjust (s) | 0.0 | | | | | | | | | |
| Total Lost Time (s) | 6.5 | | | | | | | | | |
| Lead/Lag | Lead | | | | | | | Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | | | | | | | Yes | Yes | Yes |
| Recall Mode | None | | | | | Min | None | Min | None | None |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 83.3
 Natural Cycle: 95
 Control Type: Actuated-Uncoordinated

Splits and Phases: 10: Moffett Park Dr & Innovation Way



Lanes, Volumes, Timings
 11: Innovation Way & 11th Ave

3/4/2016



| Lane Group | EBL | EBT | EBR | NBL | NBT | SBT |
|---------------------|-----|------|-----|-----|------|------|
| Lane Configurations | | | | | | |
| Volume (vph) | 20 | 0 | 60 | 180 | 20 | 90 |
| Sign Control | | Stop | | | Stop | Stop |

Intersection Summary

Control Type: Unsignalized

Lanes, Volumes, Timings
 12: Innovation Way & Juniper Driveway

3/4/2016



| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
|---------------------|------|-----|-----|------|------|-----|
| Lane Configurations | | | | | | |
| Volume (vph) | 40 | 10 | 10 | 30 | 450 | 420 |
| Sign Control | Stop | | | Stop | Stop | |

Intersection Summary

Control Type: Unsignalized

Lanes, Volumes, Timings
 13: Bordeaux Dr & Innovation Way/Driveway

3/4/2016

| | → | ↘ | ↙ | ↑ | ↓ |
|---------------------|------|-----|-----|------|------|
| Lane Group | EBT | EBR | NBL | NBT | SBT |
| Lane Configurations | ↔ | ↗ | ↖ | ↗ | ↖ |
| Volume (vph) | 0 | 30 | 10 | 110 | 50 |
| Sign Control | Stop | | | Stop | Stop |

Intersection Summary

Control Type: Unsignalized

Lanes, Volumes, Timings

33: Mathilda Ave & SR 237 WB On-Ramp/SR 237 WB Off-Ramp

3/4/2016

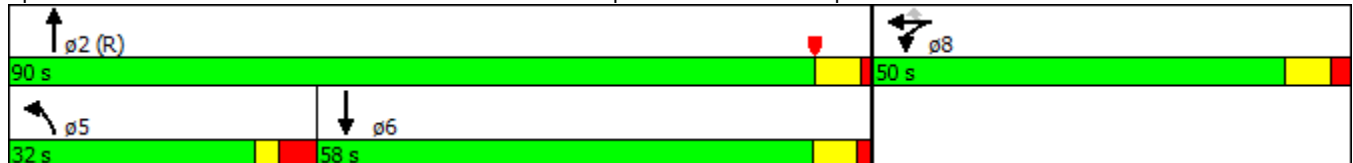


| Lane Group | WBL | WBT | WBR | NBL | NBT | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | |
| Volume (vph) | 670 | 0 | 410 | 140 | 2830 | 280 |
| Turn Type | Split | NA | Perm | Prot | NA | NA |
| Protected Phases | 8 | 8 | | 5 | 2 | 6 |
| Permitted Phases | | | 8 | | | |
| Detector Phase | 8 | 8 | 8 | 5 | 2 | 6 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | 11.0 | 11.0 | 11.0 | 10.3 | 20.0 | 10.3 |
| Total Split (s) | 50.0 | 50.0 | 50.0 | 32.0 | 90.0 | 58.0 |
| Total Split (%) | 35.7% | 35.7% | 35.7% | 22.9% | 64.3% | 41.4% |
| Yellow Time (s) | 4.8 | 4.8 | 4.8 | 2.5 | 4.7 | 4.7 |
| All-Red Time (s) | 2.2 | 2.2 | 2.2 | 3.8 | 1.3 | 1.6 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 6.3 | 6.0 | 6.3 |
| Lead/Lag | | | | Lead | | Lag |
| Lead-Lag Optimize? | | | | Yes | | Yes |
| Recall Mode | Max | Max | Max | None | C-Max | None |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 110 (79%), Referenced to phase 2:NBT, Start of Yellow
 Natural Cycle: 55
 Control Type: Actuated-Coordinated

Splits and Phases: 33: Mathilda Ave & SR 237 WB On-Ramp/SR 237 WB Off-Ramp



SimTraffic Post-Processor
Average Results from 10 Runs
Network Performance

Mathilda Avenue Improvements
2018 No Build AM Peak Hour

| Performance Measure | Average | Std. Dev. | Minimum | Maximum |
|---------------------------------|---------|-----------|---------|---------|
| Average Delay (seconds) | 445.9 | 36.5 | 379.6 | 481.4 |
| Total Delay (hours) | 1,319 | 113 | 1,112 | 1,446 |
| Average Stopped Delay (seconds) | 378.4 | 41.6 | 307.8 | 425.6 |
| Total Stopped Delay (hours) | 1120 | 127 | 902 | 1279 |
| Total Stops | 33,222 | 1,809 | 30,141 | 36,270 |
| Average Stops | 3.12 | 0.17 | 2.84 | 3.39 |
| Total Distance Traveled (miles) | 34,108 | 616 | 33,096 | 34,918 |
| Average Speed (mph) | 15.9 | 1.1 | 15.0 | 18.0 |
| Total Travel Time (hours) | 2,182.4 | 105.0 | 2,006.4 | 2,314.5 |
| Vehicles Entered | 8,945 | 65 | 8,866 | 9,080 |
| Vehicles Exited | 7,961 | 226 | 7,626 | 8,265 |
| Percent Demand Served | 89.0% | 2.7% | 85.6% | 93.2% |
| Fuel Used (gallons) | 1,152 | 17 | 1,128 | 1,179 |
| HC Emissions (grams) | 14,310 | 599 | 13,391 | 15,052 |
| CO Emissions (grams) | 422,519 | 11,819 | 406,443 | 437,804 |
| NOx Emissions (grams) | 52,287 | 1,560 | 50,273 | 54,184 |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2018 No Build AM Peak Hour

Intersection 1 **Mathilda Avenue/5th Avenue** **Signal**

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 80 | 66 | 82.3% | 36.2 | 4.4 | D |
| | Through | 860 | 686 | 79.8% | 13.5 | 2.3 | B |
| | Right Turn | 70 | 58 | 83.3% | 12.5 | 3.1 | B |
| | Subtotal | 1,010 | 810 | 80.2% | 15.3 | 2.2 | B |
| SB | Left Turn | 10 | 9 | 91.0% | 53.0 | 7.0 | D |
| | Through | 370 | 374 | 101.1% | 20.9 | 2.1 | C |
| | Right Turn | 70 | 71 | 101.4% | 9.6 | 1.2 | A |
| | Subtotal | 450 | 454 | 100.9% | 19.8 | 2.1 | B |
| EB | Left Turn | 20 | 18 | 91.5% | 29.2 | 4.3 | C |
| | Through | 10 | 10 | 104.0% | 26.6 | 6.1 | C |
| | Right Turn | 30 | 32 | 105.3% | 5.6 | 1.5 | A |
| | Subtotal | 60 | 60 | 100.5% | 16.4 | 3.2 | B |
| WB | Left Turn | 30 | 31 | 104.7% | 39.5 | 5.9 | D |
| | Through | 10 | 11 | 110.0% | 33.3 | 9.6 | C |
| | Right Turn | 10 | 11 | 107.0% | 8.9 | 3.3 | A |
| | Subtotal | 50 | 53 | 106.2% | 32.2 | 6.3 | C |
| Total | | 1,570 | 1,378 | 87.8% | 17.4 | 1.8 | B |

Intersection 2 **Mathilda Avenue/Innovation Way** **Signal**

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 730 | 577 | 79.0% | 101.0 | 175.1 | F |
| | Through | 990 | 789 | 79.7% | 18.8 | 6.5 | B |
| | Right Turn | 70 | 58 | 82.3% | 14.7 | 2.9 | B |
| | Subtotal | 1,790 | 1,424 | 79.5% | 47.0 | 58.6 | D |
| SB | Left Turn | 10 | 10 | 100.0% | 57.8 | 19.2 | E |
| | Through | 290 | 284 | 98.0% | 43.0 | 41.7 | D |
| | Right Turn | 130 | 126 | 96.8% | 24.1 | 22.7 | C |
| | Subtotal | 430 | 420 | 97.7% | 37.6 | 35.1 | D |
| EB | Left Turn | 20 | 17 | 86.0% | 45.3 | 18.9 | D |
| | Through | | | | | | |
| | Right Turn | 50 | 48 | 96.4% | 50.3 | 25.5 | D |
| | Subtotal | 70 | 65 | 93.4% | 49.0 | 23.7 | D |
| WB | Left Turn | 20 | 17 | 87.0% | 67.7 | 43.3 | E |
| | Through | 10 | 12 | 120.0% | 49.4 | 11.0 | D |
| | Right Turn | | | | | | |
| | Subtotal | 30 | 29 | 98.0% | 59.8 | 22.9 | E |
| Total | | 2,320 | 1,938 | 83.5% | 42.1 | 37.3 | D |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2018 No Build AM Peak Hour

Intersection 3

Mathilda Avenue/Moffett Park Drive/SR 237 WB Ramps

Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-------------------------|--------------------------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn (Moffett Park) | 710 | 538 | 75.8% | 35.1 | 15.7 | D |
| | Left Turn (SR 237 WB On-Ramp) | 140 | 95 | 68.0% | 65.2 | 4.7 | E |
| | Through | 2,830 | 2,181 | 77.1% | 39.7 | 26.4 | D |
| | Right Turn (Moffett Park) | 810 | 627 | 77.4% | 33.3 | 15.4 | C |
| | Subtotal | 4,490 | 3,441 | 76.7% | 38.5 | 21.9 | D |
| SB | Left Turn (Moffett Park) | 10 | 8 | 84.0% | 125.8 | 136.2 | F |
| | Through | 240 | 225 | 93.9% | 180.4 | 176.1 | F |
| | Right Turn (Moffett Park) | 110 | 97 | 88.5% | 189.3 | 203.9 | F |
| | Right Turn (SR 237 WB On-Ramp) | 90 | 84 | 93.2% | 172.8 | 176.0 | F |
| | Subtotal | 450 | 415 | 92.3% | 179.8 | 179.5 | F |
| EB (Moffett Park) | Left Turn | 40 | 34 | 85.0% | 98.6 | 109.8 | F |
| | Through | 60 | 59 | 98.8% | 59.9 | 6.4 | E |
| | Right Turn | 50 | 50 | 99.8% | 24.5 | 7.3 | C |
| | Subtotal | 150 | 143 | 95.9% | 56.7 | 22.1 | E |
| WB (Moffett Park) | Left Turn | 80 | 79 | 98.6% | 139.1 | 105.0 | F |
| | Through | 210 | 207 | 98.3% | 156.4 | 174.6 | F |
| | Right Turn | 30 | 27 | 90.0% | 153.9 | 212.2 | F |
| | Subtotal | 320 | 312 | 97.7% | 151.8 | 159.7 | F |
| WB (SR 237 WB Off-Ramp) | Left Turn | 670 | 567 | 84.6% | 450.6 | 331.5 | F |
| | Through | | | | | | F |
| | Right Turn | 410 | 349 | 85.1% | 545.8 | 348.0 | F |
| | Subtotal | 1,080 | 916 | 84.8% | 486.9 | 339.8 | F |
| Total | | 6,490 | 5,227 | 80.5% | 383.1 | 236.7 | F |

Intersection 4 **Mathilda Avenue/SR 237 EB Off-Ramp-SR 237 EB On-Ramp** **Signal**

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | 2,110 | 1,465 | 69.4% | 75.2 | 45.3 | E |
| | Right Turn | 760 | 528 | 69.5% | 8.1 | 9.5 | A |
| | Subtotal | 2,870 | 1,993 | 69.4% | 57.8 | 36.9 | E |
| SB | Left Turn | 50 | 46 | 91.0% | 67.7 | 12.0 | E |
| | Through | 900 | 785 | 87.2% | 16.8 | 1.7 | B |
| | Right Turn | | | | | | |
| | Subtotal | 950 | 830 | 87.4% | 19.5 | 1.7 | B |
| EB | Left Turn | 860 | 818 | 95.1% | 323.8 | 215.5 | F |
| | Through | | | | | | |
| | Right Turn | 70 | 67 | 95.0% | 354.5 | 192.9 | F |
| | Subtotal | 930 | 885 | 95.1% | 326.2 | 213.7 | F |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 4,750 | 3,708 | 78.1% | 116.3 | 80.9 | F |

Intersection 5 **Mathilda Avenue/Ross Drive** **Signal**

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 50 | 35 | 69.2% | 70.5 | 12.2 | E |
| | Through | 2,540 | 1,706 | 67.2% | 433.1 | 305.3 | F |
| | Right Turn | 100 | 64 | 63.5% | 125.8 | 84.0 | F |
| | Subtotal | 2,690 | 1,804 | 67.1% | 416.1 | 294.3 | F |
| SB | Left Turn | 50 | 42 | 84.4% | 66.6 | 9.0 | E |
| | Through | 880 | 771 | 87.6% | 22.9 | 2.0 | C |
| | Right Turn | 40 | 34 | 85.3% | 18.1 | 4.4 | B |
| | Subtotal | 970 | 848 | 87.4% | 24.8 | 2.3 | C |
| EB | Left Turn | 80 | 72 | 90.5% | 231.8 | 362.3 | F |
| | Through | 60 | 59 | 97.5% | 198.1 | 370.4 | F |
| | Right Turn | 20 | 19 | 96.5% | 157.7 | 327.0 | F |
| | Subtotal | 160 | 150 | 93.9% | 209.0 | 361.2 | F |
| WB | Left Turn | 110 | 96 | 87.3% | 354.9 | 232.5 | F |
| | Through | 30 | 26 | 85.3% | 371.2 | 338.8 | F |
| | Right Turn | 250 | 217 | 86.8% | 349.4 | 250.6 | F |
| | Subtotal | 390 | 339 | 86.8% | 352.0 | 249.4 | F |
| Total | | 4,210 | 3,141 | 74.6% | 285.7 | 191.3 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2018 No Build AM Peak Hour

Intersection 8

Mathilda Avenue/Almanor Avenue-Ahwanee Avenue

Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 110 | 79 | 71.7% | 699.7 | 334.2 | F |
| | Through | 2,650 | 1,906 | 71.9% | 741.6 | 363.6 | F |
| | Right Turn | 50 | 31 | 62.8% | 815.4 | 413.6 | F |
| | Subtotal | 2,810 | 2,016 | 71.8% | 741.1 | 363.1 | F |
| SB | Left Turn | 160 | 145 | 90.6% | 174.7 | 88.7 | F |
| | Through | 1,540 | 1,458 | 94.6% | 55.1 | 27.4 | E |
| | Right Turn | 300 | 289 | 96.4% | 34.2 | 9.1 | C |
| | Subtotal | 2,000 | 1,892 | 94.6% | 61.4 | 29.5 | E |
| EB | Left Turn | 90 | 80 | 89.0% | 293.7 | 506.1 | F |
| | Through | 20 | 19 | 97.0% | 167.9 | 326.7 | F |
| | Right Turn | 30 | 31 | 103.3% | 120.3 | 278.6 | F |
| | Subtotal | 140 | 131 | 93.2% | 227.6 | 402.9 | F |
| WB | Left Turn | 70 | 68 | 97.3% | 146.5 | 126.0 | F |
| | Through | 30 | 26 | 85.7% | 178.1 | 273.2 | F |
| | Right Turn | 190 | 182 | 95.8% | 142.3 | 230.2 | F |
| | Subtotal | 290 | 276 | 95.1% | 147.1 | 207.5 | F |
| Total | | 5,240 | 4,314 | 82.3% | 365.2 | 117.5 | F |

Intersection 9

US 101 On-Ramp/Moffett Park Drive

Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| EB | Left Turn | | | | | | |
| | Through | 180 | 181 | 100.6% | 2.1 | 0.3 | A |
| | Right Turn | 10 | 11 | 108.0% | 1.5 | 0.6 | A |
| | Subtotal | 190 | 192 | 100.9% | 2.0 | 0.3 | A |
| WB | Left Turn | 20 | 14 | 72.0% | 7.8 | 0.7 | A |
| | Through | 920 | 775 | 84.2% | 4.3 | 0.4 | A |
| | Right Turn | | | | | | |
| | Subtotal | 940 | 789 | 84.0% | 4.4 | 0.4 | A |
| Total | | 1,130 | 981 | 86.8% | 3.9 | 0.4 | A |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2018 No Build AM Peak Hour

Intersection 10 Innovation Way/Moffett Park Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | 40 | 34 | 84.0% | 31.6 | 6.2 | C |
| | Through | 110 | 101 | 92.0% | 29.7 | 3.2 | C |
| | Right Turn | | | | | | |
| | Subtotal | 150 | 135 | 89.9% | 30.1 | 3.8 | C |
| EB | Left Turn | 50 | 52 | 103.0% | 30.8 | 5.0 | C |
| | Through | 130 | 129 | 99.2% | 4.1 | 0.7 | A |
| | Right Turn | | | | | | |
| | Subtotal | 180 | 181 | 100.3% | 11.7 | 1.9 | B |
| WB | Left Turn | | | | | | |
| | Through | 830 | 690 | 83.1% | 12.6 | 2.1 | B |
| | Right Turn | 200 | 161 | 80.3% | 7.7 | 1.9 | A |
| | Subtotal | 1,030 | 851 | 82.6% | 11.7 | 2.1 | B |
| Total | | 1,360 | 1,166 | 85.7% | 13.7 | 0.9 | B |

Intersection 11 Innovation Way/11th Avenue All-way Stop

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 180 | 157 | 87.2% | 11.0 | 0.8 | B |
| | Through | 20 | 18 | 90.0% | 13.1 | 0.9 | B |
| | Right Turn | 40 | 35 | 87.3% | 7.9 | 0.6 | A |
| | Subtotal | 240 | 210 | 87.5% | 10.7 | 0.8 | B |
| SB | Left Turn | 10 | 7 | 67.0% | 6.7 | 0.5 | A |
| | Through | 90 | 78 | 86.4% | 13.6 | 0.6 | B |
| | Right Turn | 360 | 291 | 80.7% | 10.5 | 1.0 | B |
| | Subtotal | 460 | 375 | 81.5% | 11.1 | 0.9 | B |
| EB | Left Turn | 20 | 22 | 107.5% | 10.0 | 1.9 | A |
| | Through | | | | | | |
| | Right Turn | 60 | 57 | 94.3% | 6.9 | 1.3 | A |
| | Subtotal | 80 | 78 | 97.6% | 7.8 | 1.2 | A |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 780 | 663 | 85.0% | 10.5 | 0.8 | B |

Intersection 12

Innovation Way/Juniper Driveway

All-way Stop

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 10 | 11 | 109.0% | 6.3 | 0.7 | A |
| | Through | 30 | 29 | 96.7% | 8.1 | 0.3 | A |
| | Right Turn | | | | | | |
| | Subtotal | 40 | 40 | 99.8% | 7.6 | 0.3 | A |
| SB | Left Turn | | | | | | |
| | Through | 450 | 366 | 81.2% | 17.9 | 1.8 | C |
| | Right Turn | 420 | 346 | 82.5% | 11.4 | 1.2 | B |
| | Subtotal | 870 | 712 | 81.8% | 14.8 | 1.6 | B |
| EB | Left Turn | 40 | 38 | 95.5% | 8.8 | 1.8 | A |
| | Through | | | | | | |
| | Right Turn | 10 | 10 | 100.0% | 6.2 | 2.8 | A |
| | Subtotal | 50 | 48 | 96.4% | 8.4 | 1.7 | A |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 960 | 800 | 83.3% | 14.0 | 1.6 | B |

Intersection 13

Bordeaux Drive/Innovation Way

All-way Stop

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 10 | 8 | 84.0% | 4.5 | 0.4 | A |
| | Through | 110 | 275 | 249.5% | 2.4 | 0.2 | A |
| | Right Turn | | | | | | |
| | Subtotal | 120 | 283 | 235.8% | 2.5 | 0.2 | A |
| SB | Left Turn | | | | | | |
| | Through | 50 | 54 | 108.6% | 6.5 | 0.5 | A |
| | Right Turn | 10 | 11 | 109.0% | 4.2 | 0.6 | A |
| | Subtotal | 60 | 65 | 108.7% | 6.1 | 0.5 | A |
| EB | Left Turn | 20 | 15 | 75.5% | 4.6 | 0.1 | A |
| | Through | | | | | | |
| | Right Turn | 30 | 27 | 90.3% | 3.2 | 0.3 | A |
| | Subtotal | 50 | 42 | 84.4% | 3.7 | 0.2 | A |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 230 | 390 | 169.7% | 3.2 | 0.3 | A |

Intersection 1

Mathilda Avenue/5th Avenue

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 625 | 25 | 3 | 50 | 5 | 50 | 6 | 0% | 0% |
| | Through | 625 | 25 | 5 | 50 | 9 | 75 | 9 | 0% | 0% |
| | Right Turn | 625 | 25 | 2 | 25 | 5 | 50 | 7 | 0% | 0% |
| NB | Left Turn | 425 | 50 | 9 | 100 | 11 | 100 | 24 | 0% | 0% |
| | Through | 1,125 | 75 | 22 | 175 | 39 | 225 | 36 | 0% | 0% |
| | Through/Right | 1,125 | 100 | 27 | 225 | 40 | 275 | 35 | 0% | 0% |
| SB | Left Turn | 250 | 25 | 4 | 50 | 7 | 50 | 11 | 0% | 0% |
| | Through | 1,325 | 75 | 9 | 125 | 15 | 150 | 34 | 0% | 0% |
| | Right Turn | 250 | 25 | 2 | 25 | 11 | 50 | 24 | 0% | 0% |
| WB | Left Turn | 925 | 50 | 5 | 75 | 10 | 100 | 28 | 5% | 0% |
| | Through/Right | 75 | 25 | 5 | 75 | 8 | 75 | 8 | 2% | 0% |

Intersection 2

Mathilda Avenue/Innovation Way

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 200 | 25 | 2 | 25 | 4 | 50 | 8 | 0% | 4% |
| | Through/Right | 225 | 25 | 2 | 50 | 4 | 50 | 15 | 0% | 22% |
| | Right Turn | 225 | 25 | 5 | 50 | 9 | 50 | 20 | 0% | 7% |
| NB | Left Turn | 400 | 225 | 59 | 375 | 107 | 400 | 67 | 7% | 0% |
| | Through | 975 | 150 | 172 | 325 | 389 | 325 | 261 | 0% | 6% |
| | Through/Right | 975 | 200 | 155 | 375 | 333 | 375 | 227 | 0% | 5% |
| SB | Left Turn | 75 | 25 | 3 | 25 | 8 | 50 | 41 | 0% | 0% |
| | Through | 975 | 75 | 42 | 175 | 142 | 275 | 261 | 10% | 0% |
| | Right Turn | 225 | 75 | 10 | 125 | 27 | 150 | 49 | 0% | 0% |
| WB | Left Turn | 425 | 25 | 3 | 25 | 8 | 50 | 19 | 0% | 0% |
| | Shared | 225 | 25 | 2 | 25 | 9 | 50 | 16 | 0% | 0% |

Intersection 3

Mathilda Avenue/Moffett Park Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-------------------------|-----------------------------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB (Moffett Park) | Left Turn | 525 | 25 | 14 | 75 | 36 | 100 | 32 | 0% | 3% |
| | Through/Right | 1,125 | 50 | 6 | 125 | 15 | 150 | 24 | 0% | 2% |
| | Right Turn | 1,125 | 50 | 6 | 100 | 14 | 125 | 22 | 0% | 0% |
| NB | Left Turn (Moffett Park) | 125 | 25 | 5 | 50 | 6 | 50 | 11 | 0% | 15% |
| | Through | 300 | 225 | 40 | 325 | 29 | 350 | 35 | 0% | 55% |
| | Through/Right (Moffett Park) | 300 | 275 | 35 | 350 | 20 | 350 | 26 | 0% | 68% |
| | Left Turn (SR 237 WB On-Ramp) | 175 | 100 | 21 | 175 | 25 | 200 | 24 | 0% | 4% |
| SB | Left Turn (Moffett Park) | 175 | 25 | 3 | 50 | 6 | 50 | 5 | 0% | 0% |
| | Through | 1,100 | 225 | 150 | 500 | 406 | 550 | 391 | 3% | 12% |
| | Through/Right (Moffett Park) | 975 | 275 | 139 | 500 | 337 | 550 | 299 | 0% | 4% |
| | Through/Right (SR 237 WB On-Ramp) | 1,100 | 225 | 151 | 500 | 407 | 575 | 396 | 3% | 9% |
| WB (Moffett Park) | Left Turn | 300 | 100 | 91 | 250 | 162 | 300 | 154 | 0% | 0% |
| | Through/Right | 675 | 250 | 67 | 400 | 129 | 425 | 100 | 10% | 4% |
| WB (SR 237 WB Off-Ramp) | Left Turn | 1,075 | 1,100 | 159 | 1,300 | 123 | 1,200 | 12 | 12% | 47% |
| | Left/Through | 325 | 425 | 23 | 475 | 35 | 450 | 0 | 18% | 0% |
| | Right Turn | 325 | 375 | 8 | 400 | 12 | 375 | 0 | 69% | 0% |

Intersection 4

Mathilda Avenue/SR 237 EB Off-Ramp-SR 237 EB On-Ramp

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,025 | 1,375 | 791 | 2,900 | 1,378 | 3,225 | 1,541 | 55% | 0% |
| | Shared | 1,025 | 475 | 63 | 650 | 36 | 575 | 0 | 52% | 0% |
| NB | Through | 275 | 250 | 20 | 325 | 30 | 325 | 48 | 0% | 41% |
| | Right Turn | 275 | 175 | 46 | 375 | 31 | 325 | 18 | 0% | 22% |
| SB | Left Turn | 175 | 50 | 9 | 100 | 15 | 125 | 23 | 0% | 0% |
| | Through | 175 | 125 | 19 | 225 | 23 | 200 | 13 | 0% | 4% |
| | | | | | | | | | | |

Intersection 5

Mathilda Avenue/Ross Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 250 | 250 | 271 | 500 | 501 | 575 | 397 | 74% | 0% |
| | Through | 1,575 | 75 | 15 | 125 | 11 | 100 | 0 | 34% | 0% |
| | Right Turn | 50 | 25 | 7 | 75 | 13 | 75 | 6 | 2% | 0% |
| NB | Left Turn | 150 | 50 | 9 | 100 | 16 | 125 | 43 | 0% | 0% |
| | Through | 2,800 | 1,100 | 102 | 1,100 | 96 | 1,100 | 46 | 1% | 46% |
| | Through/Right | 450 | 550 | 2 | 550 | 6 | 575 | 0 | 0% | 87% |
| SB | Left Turn | 225 | 50 | 16 | 150 | 41 | 200 | 52 | 1% | 0% |
| | Through | 225 | 150 | 26 | 275 | 31 | 275 | 9 | 13% | 3% |
| | Through/Right | 225 | 150 | 27 | 275 | 25 | 275 | 13 | 0% | 4% |
| WB | Left Turn | 100 | 1,175 | 760 | 2,275 | 1,706 | 2,400 | 1,964 | 28% | 0% |
| | Through | 225 | 100 | 3 | 125 | 13 | 100 | 0 | 10% | 0% |
| | Right Turn | 100 | 75 | 2 | 100 | 7 | 100 | 0 | 70% | 0% |

Intersection 8

Mathilda Avenue/Almanor Avenue-Ahwanee Avenue

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,025 | 125 | 72 | 250 | 136 | 300 | 111 | 26% | 10% |
| | Through/Right | 125 | 50 | 12 | 125 | 34 | 200 | 51 | 0% | 0% |
| NB | Left Turn | 425 | 125 | 38 | 350 | 68 | 375 | 0 | 0% | 0% |
| | Through | 750 | 5,350 | 38 | 8,325 | 75 | 9,150 | 15 | 70% | 0% |
| | Right Turn | 75 | 25 | 8 | 75 | 17 | 100 | 3 | 0% | 0% |
| SB | Left Turn | 125 | 150 | 15 | 200 | 12 | 175 | 0 | 57% | 0% |
| | Through | 2,225 | 650 | 117 | 725 | 128 | 800 | 100 | 15% | 0% |
| | Through/Right | 2,225 | 325 | 36 | 475 | 49 | 500 | 38 | 0% | 0% |
| WB | Left Turn | 250 | 100 | 36 | 225 | 92 | 275 | 104 | 2% | 0% |
| | Through | 1,025 | 225 | 170 | 600 | 357 | 700 | 309 | 3% | 0% |
| | Right Turn | 75 | 100 | 6 | 150 | 6 | 125 | 0 | 46% | 0% |

Intersection 9

US 101 On-Ramp/Moffett Park Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Through | 850 | 25 | 4 | 50 | 14 | 75 | 26 | 0% | 0% |
| | Right Turn | 150 | 25 | 0 | 25 | 5 | 25 | 14 | 0% | 0% |
| WB | Left Turn | 850 | 25 | 2 | 50 | 4 | 50 | 11 | 0% | 0% |
| | Through | 850 | 25 | 30 | 100 | 184 | 200 | 386 | 0% | 0% |
| | | | | | | | | | | |
| | | | | | | | | | | |

Intersection 10

Innovation Way/Moffett Park Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 225 | 50 | 4 | 100 | 9 | 100 | 14 | 0% | 0% |
| | Through | 850 | 25 | 4 | 75 | 9 | 100 | 22 | 0% | 0% |
| SB | Left Turn | 575 | 25 | 3 | 50 | 6 | 50 | 10 | 0% | 0% |
| | Shared | 575 | 100 | 8 | 150 | 13 | 175 | 21 | 0% | 0% |
| WB | Through | 1,150 | 150 | 24 | 250 | 29 | 300 | 55 | 1% | 0% |
| | Right Turn | 1,150 | 50 | 12 | 125 | 40 | 225 | 55 | 0% | 0% |
| | | | | | | | | | | |

Intersection 11

Innovation Way/11th Avenue

All-way Stop

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 125 | 25 | 4 | 50 | 7 | 75 | 20 | 0% | 0% |
| | Through/Right | 325 | 25 | 2 | 50 | 4 | 50 | 8 | 0% | 0% |
| | Right Turn | 325 | 50 | 3 | 75 | 9 | 75 | 22 | 0% | 0% |
| NB | Left Turn | 125 | 25 | 5 | 50 | 6 | 75 | 8 | 0% | 0% |
| | Left/Through | 575 | 50 | 2 | 50 | 6 | 75 | 7 | 0% | 0% |
| | Through/Right | 575 | 25 | 1 | 50 | 4 | 50 | 14 | 0% | 0% |
| SB | Left/Through | 1,000 | 25 | 4 | 50 | 4 | 50 | 8 | 0% | 0% |
| | Through/Right | 1,000 | 75 | 14 | 125 | 21 | 150 | 23 | 0% | 0% |
| WB | Left Turn | 325 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | Through/Right | 325 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |

Intersection 12

Innovation Way/Juniper Driveway

All-way Stop

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 200 | 50 | 2 | 75 | 5 | 75 | 11 | 0% | 0% |
| | Right Turn | 200 | 25 | 2 | 50 | 4 | 50 | 0 | 0% | 0% |
| NB | Left Turn | 125 | 25 | 3 | 50 | 5 | 50 | 7 | 0% | 0% |
| | Through | 1,000 | 25 | 3 | 50 | 7 | 75 | 18 | 0% | 0% |
| SB | Through/Right | 300 | 225 | 34 | 250 | 32 | 275 | 27 | 0% | 2% |
| | Right Turn | 300 | 225 | 19 | 300 | 30 | 300 | 34 | 0% | 0% |
| | | | | | | | | | | |

Intersection 13

Bordeaux Drive/Innovation Way

All-way Stop

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left/Through | 375 | 25 | 3 | 50 | 3 | 50 | 7 | 0% | 0% |
| | Right Turn | 125 | 25 | 3 | 50 | 4 | 50 | 17 | 0% | 0% |
| NB | Left Turn | 325 | 25 | 3 | 50 | 5 | 50 | 1 | 0% | 0% |
| | Through/Right | 2,025 | 50 | 5 | 75 | 8 | 75 | 14 | 0% | 0% |
| SB | Left Turn | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | Through/Right | 725 | 50 | 1 | 50 | 3 | 75 | 5 | 0% | 0% |
| WB | Left/Through | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | Right Turn | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |

Arterial Level of Service: NB Mathilda Ave

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|----------------------|------|---------------|-----------------|------------|----------------|
| Ahwanee Ave | 8 | 124.4 | 135.1 | 0.1 | 4 |
| US 101 SB Diag. On-R | 702 | 31.8 | 38.4 | 0.1 | 8 |
| US 101 SB Loop On-Ra | 701 | 78.6 | 86.2 | 0.1 | 4 |
| US 101 NB Loop On-Ra | 602 | 70.0 | 75.6 | 0.1 | 3 |
| US 101 NB Diag.Off-R | 601 | 90.8 | 97.6 | 0.1 | 3 |
| Ross Dr | 5 | 97.0 | 104.5 | 0.1 | 3 |
| SR 237 EB On-Ramp | 4 | 64.7 | 70.2 | 0.1 | 3 |
| SR 237 WB Off-Ramp | 33 | 24.8 | 28.6 | 0.0 | 6 |
| Moffett Park Dr | 3 | 4.5 | 7.4 | 0.0 | 21 |
| Innovation Way | 2 | 17.9 | 34.6 | 0.2 | 22 |
| 5th Ave | 1 | 13.7 | 33.0 | 0.2 | 26 |
| | 107 | 4.3 | 26.6 | 0.3 | 37 |
| Total | | 622.5 | 737.8 | 1.5 | 7 |

Arterial Level of Service: SB Mathilda Ave

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|----------------------|------|---------------|-----------------|------------|----------------|
| 5th Ave | 1 | 13.3 | 35.6 | 0.3 | 28 |
| Innovation Way | 2 | 44.3 | 62.7 | 0.2 | 14 |
| Moffett Park Dr | 3 | 152.0 | 168.5 | 0.2 | 5 |
| SR 237 WB On-Ramp | 33 | 8.5 | 11.5 | 0.0 | 13 |
| SR 237 Off/On Ramp | 4 | 15.4 | 19.4 | 0.0 | 9 |
| Ross Dr | 5 | 23.8 | 28.8 | 0.1 | 8 |
| US 101 NB Diag.Off-R | 601 | 5.3 | 13.6 | 0.1 | 24 |
| US 101 NB Loop Off-R | 602 | 2.6 | 8.2 | 0.1 | 40 |
| US 101 SB Loop On-Ra | 701 | 2.8 | 8.9 | 0.1 | 27 |
| US 101 SB Off-Ramp | 702 | 6.8 | 13.5 | 0.1 | 28 |
| Almanor Ave | 8 | 38.8 | 46.9 | 0.1 | 6 |
| San Aleso Ave | 201 | 3.8 | 15.2 | 0.1 | 33 |
| Total | | 317.3 | 432.8 | 1.5 | 12 |

Arterial Level of Service: NB Innovation Way

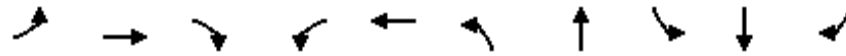
| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|------------------|------|---------------|-----------------|-----------|----------------|
| | 910 | 5.7 | 7.7 | 0.0 | 11 |
| | 38 | 1.3 | 6.4 | 0.0 | 23 |
| | 11 | 7.3 | 14.4 | 0.1 | 18 |
| | 200 | 2.4 | 18.1 | 0.2 | 32 |
| Juniper Driveway | 12 | 6.7 | 12.5 | 0.1 | 16 |
| Driveway | 217 | 2.7 | 5.6 | 0.0 | 24 |
| | 902 | 18.8 | 21.6 | 0.0 | 4 |
| Mathilda Ave | 2 | 25.0 | 27.8 | 0.0 | 3 |
| | 53 | 0.5 | 15.1 | 0.1 | 23 |
| Bordeaux Dr | 13 | 4.2 | 16.4 | 0.1 | 17 |
| Total | | 74.4 | 145.5 | 0.6 | 15 |

Arterial Level of Service: SB Innovation Way

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|------------------|------|---------------|-----------------|-----------|----------------|
| | 53 | 0.4 | 14.0 | 0.1 | 20 |
| Mathilda Ave | 2 | 48.8 | 60.8 | 0.1 | 6 |
| | 902 | 1.4 | 5.6 | 0.0 | 16 |
| Driveway | 217 | 1.5 | 3.5 | 0.0 | 23 |
| Juniper Driveway | 12 | 15.0 | 19.0 | 0.0 | 7 |
| | 200 | 3.0 | 9.5 | 0.1 | 21 |
| 11th Ave | 11 | 10.7 | 26.3 | 0.2 | 22 |
| | 38 | 3.2 | 11.0 | 0.1 | 24 |
| | 910 | 16.3 | 20.7 | 0.0 | 7 |
| Moffett Park Dr | 10 | 13.8 | 17.1 | 0.0 | 5 |
| Total | | 114.1 | 187.5 | 0.6 | 12 |

Lanes, Volumes, Timings
1: Mathilda Ave & 5th Ave

3/4/2016

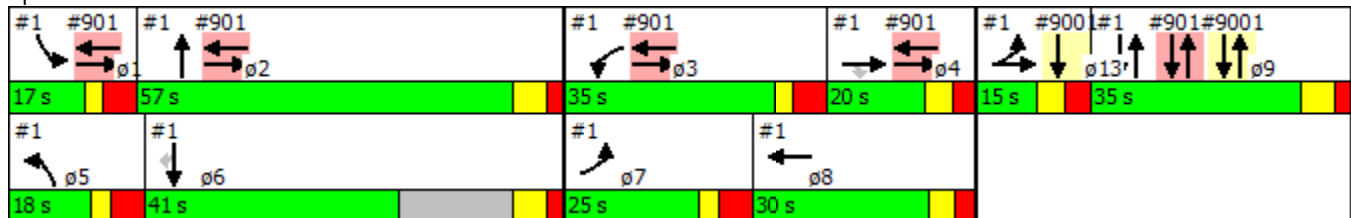


| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT | SBR | ø2 | ø7 |
|----------------------|------|------|--------|-------|-------|-------|-----|------|------|--------|------|------|
| Lane Configurations | ↔↔ | ↑ | ↔ | ↔↔ | ↔ | ↔↔ | ↔↔↔ | ↔ | ↔↔↔ | ↔ | | |
| Volume (vph) | 70 | 20 | 70 | 240 | 10 | 110 | 370 | 10 | 1110 | 10 | | |
| Turn Type | Prot | NA | custom | Prot | NA | Prot | NA | Prot | NA | custom | | |
| Protected Phases | 7 13 | 4 13 | | 3 | 8 | 5 | 2 9 | 1 | 6 9 | | 2 | 7 |
| Permitted Phases | | | 4 | | | | | | | 6 | | |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 5 | 2 | 1 | 6 | 6 | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 13.0 | 12.0 | 8.0 | 11.0 | | 10.0 | | 12.0 | 12.0 | 12.0 |
| Minimum Split (s) | | | 20.0 | 19.0 | 29.5 | 18.0 | | 17.0 | | 41.0 | 35.0 | 19.0 |
| Total Split (s) | | | 20.0 | 35.0 | 30.0 | 18.0 | | 17.0 | | 41.0 | 57.0 | 25.0 |
| Total Split (%) | | | 11.2% | 19.6% | 16.8% | 10.1% | | 9.5% | | 22.9% | 32% | 14% |
| Yellow Time (s) | | | 3.6 | 2.5 | 3.6 | 2.5 | | 2.5 | | 4.7 | 4.7 | 2.5 |
| All-Red Time (s) | | | 3.4 | 4.5 | 2.9 | 4.5 | | 4.5 | | 2.3 | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | | 0.0 | | |
| Total Lost Time (s) | | | 7.0 | 7.0 | 6.5 | 7.0 | | 7.0 | | 7.0 | | |
| Lead/Lag | | | Lag | Lead | Lag | Lead | | Lead | | Lag | Lag | Lead |
| Lead-Lag Optimize? | | | Yes | Yes | Yes | Yes | | Yes | | Yes | Yes | Yes |
| Recall Mode | | | None | None | None | None | | None | | Min | Min | None |

Intersection Summary

Cycle Length: 179
 Actuated Cycle Length: 107.1
 Natural Cycle: 160
 Control Type: Actuated-Uncoordinated

Splits and Phases: 1: Mathilda Ave & 5th Ave

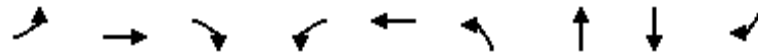


| Lane Group | ø9 | ø13 |
|----------------------|------|------|
| Lane Configurations | | |
| Volume (vph) | | |
| Turn Type | | |
| Protected Phases | 9 | 13 |
| Permitted Phases | | |
| Detector Phase | | |
| Switch Phase | | |
| Minimum Initial (s) | 28.0 | 8.0 |
| Minimum Split (s) | 35.0 | 15.0 |
| Total Split (s) | 35.0 | 15.0 |
| Total Split (%) | 20% | 8% |
| Yellow Time (s) | 4.7 | 3.6 |
| All-Red Time (s) | 2.3 | 3.4 |
| Lost Time Adjust (s) | | |
| Total Lost Time (s) | | |
| Lead/Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes |
| Recall Mode | None | None |
| Intersection Summary | | |

Lanes, Volumes, Timings

2: Mathilda Ave & Innovation Way

3/4/2016



| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBT | SBR | ø1 | ø2 | ø4 |
|----------------------|-------|------|------|-------|-------|-------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 140 | 10 | 680 | 40 | 0 | 90 | 380 | 1370 | 50 | | | |
| Turn Type | Split | NA | Prot | Split | NA | Prot | NA | NA | Perm | | | |
| Protected Phases | 4 13 | 4 13 | 4 13 | 8 | 8 | 5 | 2 9 | 6 9 | | 1 | 2 | 4 |
| Permitted Phases | | | | | | | | | 6 9 | | | |
| Detector Phase | 4 | 4 | 4 | 8 | 8 | 5 | 2 | 6 | 6 | | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | | 10.0 | 10.0 | 13.0 | | | | 10.0 | 12.0 | 14.0 |
| Minimum Split (s) | | | | 35.0 | 35.0 | 20.0 | | | | 16.8 | 19.0 | 39.0 |
| Total Split (s) | | | | 35.0 | 35.0 | 20.0 | | | | 17.8 | 45.2 | 52.0 |
| Total Split (%) | | | | 17.5% | 17.5% | 10.0% | | | | 9% | 23% | 26% |
| Yellow Time (s) | | | | 2.5 | 2.5 | 2.5 | | | | 2.5 | 4.7 | 2.5 |
| All-Red Time (s) | | | | 4.5 | 4.5 | 4.5 | | | | 4.3 | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | | 0.0 | 0.0 | 0.0 | | | | | | |
| Total Lost Time (s) | | | | 7.0 | 7.0 | 7.0 | | | | | | |
| Lead/Lag | | | | | | | Lead | | | Lead | Lag | |
| Lead-Lag Optimize? | | | | | | | Yes | | | Yes | Yes | |
| Recall Mode | | | | None | None | None | | | | None | Min | Max |

Intersection Summary

Cycle Length: 200
 Actuated Cycle Length: 152.3
 Natural Cycle: 175
 Control Type: Actuated-Uncoordinated

Splits and Phases: 2: Mathilda Ave & Innovation Way



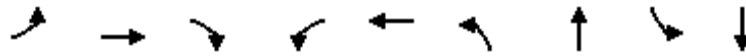
Lanes, Volumes, Timings
 2: Mathilda Ave & Innovation Way

3/4/2016

| Lane Group | ø6 | ø9 | ø13 |
|----------------------|------|------|------|
| Lane Configurations | | | |
| Volume (vph) | | | |
| Turn Type | | | |
| Protected Phases | 6 | 9 | 13 |
| Permitted Phases | | | |
| Detector Phase | | | |
| Switch Phase | | | |
| Minimum Initial (s) | 12.0 | 28.0 | 8.0 |
| Minimum Split (s) | 30.0 | 35.0 | 15.0 |
| Total Split (s) | 43.0 | 35.0 | 15.0 |
| Total Split (%) | 22% | 18% | 8% |
| Yellow Time (s) | 4.7 | 4.7 | 2.5 |
| All-Red Time (s) | 2.3 | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | |
| Total Lost Time (s) | | | |
| Lead/Lag | Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes | Yes |
| Recall Mode | Min | None | None |
| Intersection Summary | | | |

Lanes, Volumes, Timings
 3: Mathilda Ave & Moffett Park Dr

3/4/2016

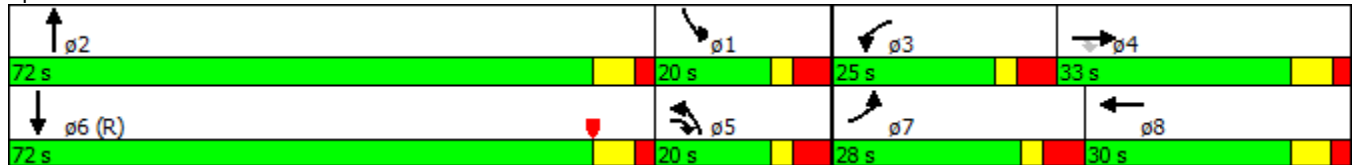


| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↶ | ↷ | ↷ | ↶↷ | ↷ | ↶↷ | ↶↷↷ | ↶ | ↶↶↶ |
| Volume (vph) | 70 | 190 | 450 | 310 | 260 | 100 | 420 | 50 | 1940 |
| Turn Type | Prot | NA | pm+ov | Prot | NA | Prot | NA | Prot | NA |
| Protected Phases | 7 | 4 | 5 | 3 | 8 | 5 | 2 | 1 | 6 |
| Permitted Phases | | | 4 | | | | | | |
| Detector Phase | 7 | 4 | 5 | 3 | 8 | 5 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | | |
| Minimum Initial (s) | 8.0 | 8.0 | 4.0 | 8.0 | 8.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | 15.0 | 15.0 | 11.0 | 15.0 | 30.0 | 11.0 | 34.9 | 11.0 | 10.9 |
| Total Split (s) | 28.0 | 33.0 | 20.0 | 25.0 | 30.0 | 20.0 | 72.0 | 20.0 | 72.0 |
| Total Split (%) | 18.7% | 22.0% | 13.3% | 16.7% | 20.0% | 13.3% | 48.0% | 13.3% | 48.0% |
| Yellow Time (s) | 2.5 | 4.7 | 2.5 | 2.5 | 4.5 | 2.5 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 4.5 | 2.3 | 4.5 | 4.5 | 2.5 | 4.5 | 2.2 | 4.5 | 2.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.9 | 7.0 | 6.9 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | Max | Max | Max | None | Max | Max | None | C-Max |

Intersection Summary

Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 0 (0%), Referenced to phase 6:SBT, Start of Yellow, Master Intersection
 Natural Cycle: 95
 Control Type: Actuated-Coordinated

Splits and Phases: 3: Mathilda Ave & Moffett Park Dr



Lanes, Volumes, Timings

4: Mathilda Ave & SR 237 Off/On Ramp/SR 237 EB On-Ramp

3/4/2016



| Lane Group | EBL | EBT | NBT | NBR | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | |
| Volume (vph) | 170 | 0 | 410 | 670 | 360 | 2670 |
| Turn Type | Split | NA | NA | Perm | Prot | NA |
| Protected Phases | 4 | 4 | 2 | | 1 | 6 |
| Permitted Phases | | | | 2 | | |
| Detector Phase | 4 | 4 | 2 | 2 | 1 | 6 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | 12.0 | 12.0 | 20.7 | 20.7 | 10.4 | 10.7 |
| Total Split (s) | 40.6 | 40.6 | 61.0 | 61.0 | 48.4 | 109.4 |
| Total Split (%) | 27.1% | 27.1% | 40.7% | 40.7% | 32.3% | 72.9% |
| Yellow Time (s) | 4.8 | 4.8 | 4.7 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 2.2 | 2.2 | 1.5 | 1.5 | 3.9 | 1.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 6.2 | 6.2 | 6.4 | 5.9 |
| Lead/Lag | | | Lag | Lag | Lead | |
| Lead-Lag Optimize? | | | Yes | Yes | Yes | |
| Recall Mode | Max | Max | None | None | Max | C-Max |

Intersection Summary

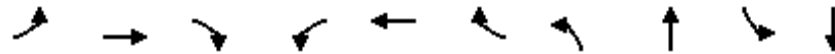
Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 50 (33%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 65
 Control Type: Actuated-Coordinated

Splits and Phases: 4: Mathilda Ave & SR 237 Off/On Ramp/SR 237 EB On-Ramp



Lanes, Volumes, Timings
5: Mathilda Ave & Ross Dr

3/4/2016

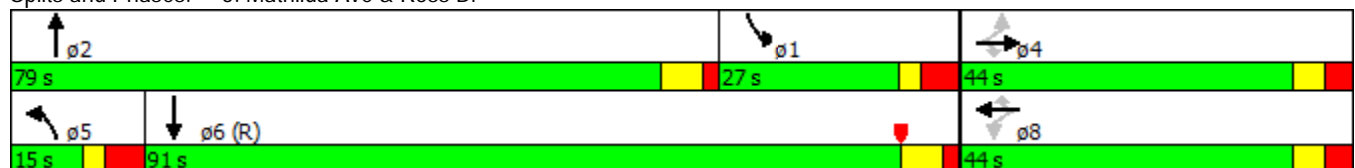


| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↖ | ↑ | ↗ | ↖ | ↑ | ↗ | ↖ | ↑↑↑↑ | ↖ | ↑↑↑ |
| Volume (vph) | 40 | 150 | 40 | 230 | 50 | 100 | 90 | 940 | 140 | 2620 |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | Prot | NA | Prot | NA |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | 1 | 6 |
| Permitted Phases | 4 | | 4 | 8 | | 8 | | | | |
| Detector Phase | 4 | 4 | 4 | 8 | 8 | 8 | 5 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 4.0 | 5.0 | 4.0 | 5.0 |
| Minimum Split (s) | 44.0 | 44.0 | 44.0 | 13.0 | 13.0 | 13.0 | 11.0 | 33.4 | 11.0 | 11.6 |
| Total Split (s) | 44.0 | 44.0 | 44.0 | 44.0 | 44.0 | 44.0 | 15.0 | 79.0 | 27.0 | 91.0 |
| Total Split (%) | 29.3% | 29.3% | 29.3% | 29.3% | 29.3% | 29.3% | 10.0% | 52.7% | 18.0% | 60.7% |
| Yellow Time (s) | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 2.5 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 3.4 | 3.4 | 3.4 | 3.4 | 3.4 | 3.4 | 4.5 | 1.7 | 4.5 | 1.9 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.4 | 7.0 | 6.6 |
| Lead/Lag | | | | | | | Lead | Lead | Lag | Lag |
| Lead-Lag Optimize? | | | | | | | Yes | Yes | Yes | Yes |
| Recall Mode | Max | Max | Max | Max | Max | Max | Max | Max | None | C-Max |

Intersection Summary

Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 35 (23%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 140
 Control Type: Actuated-Coordinated

Splits and Phases: 5: Mathilda Ave & Ross Dr



Lanes, Volumes, Timings
 8: Mathilda Ave & Almanor Ave/Ahwanee Ave

3/4/2016

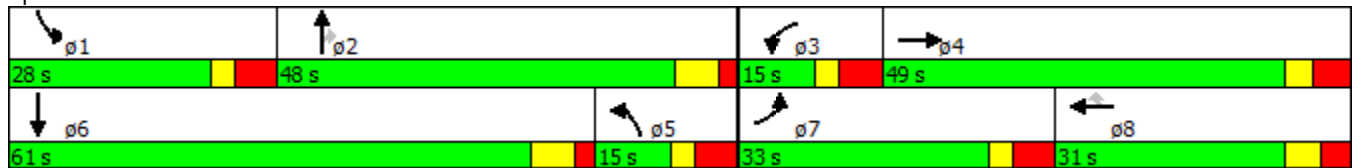


| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↖↗ | ↖ | ↖ | ↖ | ↖ | ↖ | ↑↑↑ | ↖ | ↖ | ↑↑↑ |
| Volume (vph) | 310 | 30 | 50 | 10 | 190 | 60 | 1380 | 40 | 180 | 2800 |
| Turn Type | Prot | NA | Prot | NA | Perm | Prot | NA | Perm | Prot | NA |
| Protected Phases | 7 | 4 | 3 | 8 | | 5 | 2 | | 1 | 6 |
| Permitted Phases | | | | | 8 | | | 2 | | |
| Detector Phase | 7 | 4 | 3 | 8 | 8 | 5 | 2 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 12.0 | 12.0 | 8.0 | 12.0 |
| Minimum Split (s) | 15.0 | 49.0 | 15.0 | 15.0 | 15.0 | 15.0 | 36.7 | 36.7 | 15.0 | 27.7 |
| Total Split (s) | 33.0 | 49.0 | 15.0 | 31.0 | 31.0 | 15.0 | 48.0 | 48.0 | 28.0 | 61.0 |
| Total Split (%) | 23.6% | 35.0% | 10.7% | 22.1% | 22.1% | 10.7% | 34.3% | 34.3% | 20.0% | 43.6% |
| Yellow Time (s) | 2.5 | 2.8 | 2.5 | 3.6 | 3.6 | 2.5 | 4.7 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 4.5 | 4.2 | 4.5 | 3.4 | 3.4 | 4.5 | 2.0 | 2.0 | 4.5 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.7 | 6.7 | 7.0 | 6.7 |
| Lead/Lag | Lead | Lag | Lead | Lag | Lag | Lag | Lag | Lag | Lead | Lead |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | None | Max | Max | None | Max |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 111.4
 Natural Cycle: 150
 Control Type: Actuated-Uncoordinated

Splits and Phases: 8: Mathilda Ave & Almanor Ave/Ahwanee Ave



Lanes, Volumes, Timings
 9: US 101 On Ramp & Moffett Park Dr

3/4/2016

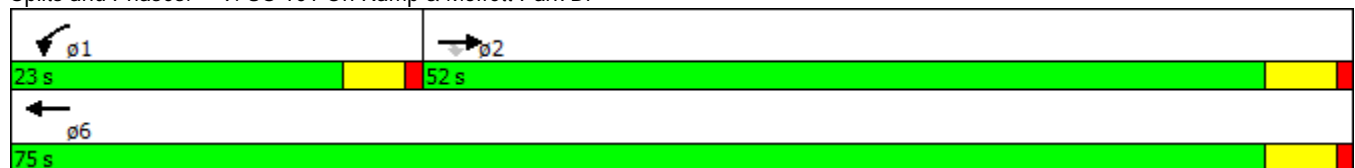


| Lane Group | EBT | EBR | WBL | WBT |
|----------------------|-------|-------|-------|--------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ |
| Volume (vph) | 790 | 90 | 230 | 320 |
| Turn Type | NA | Perm | Prot | NA |
| Protected Phases | 2 | | 1 | 6 |
| Permitted Phases | | 2 | | |
| Detector Phase | 2 | 2 | 1 | 6 |
| Switch Phase | | | | |
| Minimum Initial (s) | 15.0 | 15.0 | 6.0 | 15.0 |
| Minimum Split (s) | 20.0 | 20.0 | 10.5 | 20.0 |
| Total Split (s) | 52.0 | 52.0 | 23.0 | 75.0 |
| Total Split (%) | 69.3% | 69.3% | 30.7% | 100.0% |
| Yellow Time (s) | 4.0 | 4.0 | 3.5 | 4.0 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.0 | 5.0 | 4.5 | 5.0 |
| Lead/Lag | Lag | Lag | Lead | |
| Lead-Lag Optimize? | | | | |
| Recall Mode | Min | Min | Max | Min |

Intersection Summary

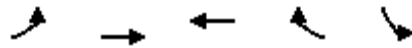
Cycle Length: 75
 Actuated Cycle Length: 60.1
 Natural Cycle: 50
 Control Type: Semi Act-Uncoord

Splits and Phases: 9: US 101 On Ramp & Moffett Park Dr



Lanes, Volumes, Timings
 10: Moffett Park Dr & Innovation Way

3/4/2016

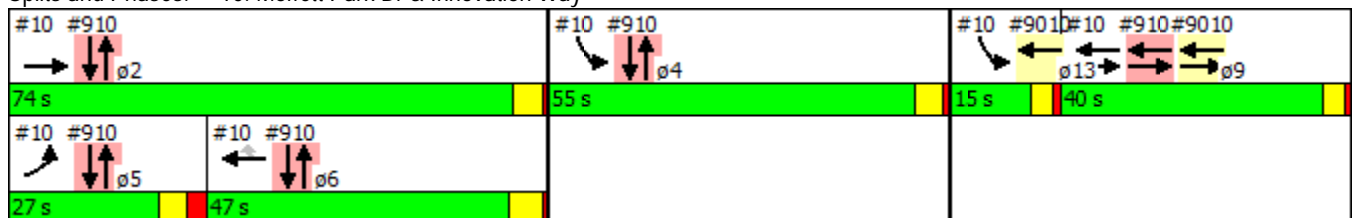


| Lane Group | EBL | EBT | WBT | WBR | SBL | ø2 | ø4 | ø9 | ø13 |
|----------------------|-------|-----|-----|--------|------|------|------|------|------|
| Lane Configurations | ↖ | ↑↑ | ↑↑ | ↗ | ↖↗ | | | | |
| Volume (vph) | 50 | 740 | 400 | 60 | 200 | | | | |
| Turn Type | Prot | NA | NA | custom | Prot | | | | |
| Protected Phases | 5 | 2 9 | 6 9 | | 4 13 | 2 | 4 | 9 | 13 |
| Permitted Phases | | | | 6 | | | | | |
| Detector Phase | 5 | 2 | 6 | 6 | 4 | | | | |
| Switch Phase | | | | | | | | | |
| Minimum Initial (s) | 8.0 | | | 10.0 | | 10.0 | 10.0 | 46.0 | 10.0 |
| Minimum Split (s) | 14.5 | | | 15.5 | | 14.9 | 15.0 | 50.0 | 14.0 |
| Total Split (s) | 27.0 | | | 47.0 | | 74.0 | 55.0 | 40.0 | 15.0 |
| Total Split (%) | 14.7% | | | 25.5% | | 40% | 30% | 22% | 8% |
| Yellow Time (s) | 4.0 | | | 4.5 | | 3.9 | 4.0 | 3.0 | 3.0 |
| All-Red Time (s) | 2.5 | | | 1.0 | | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | | | 0.0 | | | | | |
| Total Lost Time (s) | 6.5 | | | 5.5 | | | | | |
| Lead/Lag | Lead | | | Lag | | | | Lag | Lead |
| Lead-Lag Optimize? | Yes | | | Yes | | | | Yes | Yes |
| Recall Mode | None | | | Min | | Min | None | None | None |

Intersection Summary

















Cycle Length: 184
 Actuated Cycle Length: 64.3
 Natural Cycle: 110
 Control Type: Actuated-Uncoordinated

Splits and Phases: 10: Moffett Park Dr & Innovation Way



Lanes, Volumes, Timings
 11: Innovation Way & 11th Ave

3/4/2016

| |  |  |  |  |  |  |  |
|---------------------|---|---|---|---|---|---|---|
| Lane Group | EBL | EBT | EBR | WBL | NBL | NBT | SBT |
| Lane Configurations |  |  |  |  |  |   |   |
| Volume (vph) | 390 | 0 | 270 | 10 | 30 | 70 | 60 |
| Sign Control | | Stop | | | | Stop | Stop |

Intersection Summary

Control Type: Unsignalized

Lanes, Volumes, Timings
 12: Innovation Way & Juniper Driveway

3/4/2016



| Lane Group | EBL | EBR | NBT | SBT | SBR |
|---------------------|------|-----|------|------|-----|
| Lane Configurations | | | | | |
| Volume (vph) | 370 | 30 | 460 | 60 | 80 |
| Sign Control | Stop | | Stop | Stop | |

Intersection Summary

Control Type: Unsignalized

Lanes, Volumes, Timings
 13: Bordeaux Dr & Innovation Way/Driveway

3/4/2016

| | → | ↘ | ↙ | ↑ | ↓ |
|---------------------|------|-----|-----|------|------|
| Lane Group | EBT | EBR | NBL | NBT | SBT |
| Lane Configurations | ↖ | ↗ | ↘ | ↖ | ↗ |
| Volume (vph) | 10 | 10 | 10 | 30 | 140 |
| Sign Control | Stop | | | Stop | Stop |

Intersection Summary

Control Type: Unsignalized

Lanes, Volumes, Timings

33: Mathilda Ave & SR 237 WB On-Ramp/SR 237 WB Off-Ramp

3/4/2016

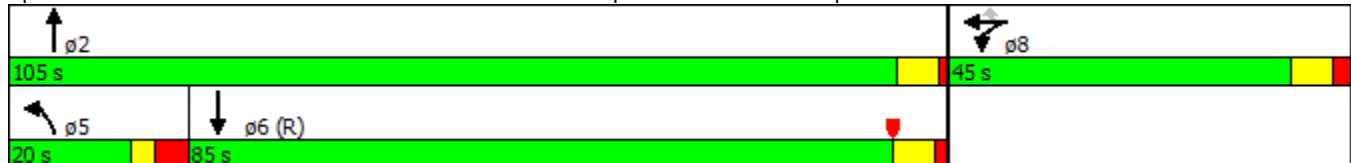


| Lane Group | WBL | WBT | WBR | NBL | NBT | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | |
| Volume (vph) | 760 | 0 | 190 | 90 | 490 | 2270 |
| Turn Type | Split | NA | Perm | Prot | NA | NA |
| Protected Phases | 8 | 8 | | 5 | 2 | 6 |
| Permitted Phases | | | 8 | | | |
| Detector Phase | 8 | 8 | 8 | 5 | 2 | 6 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | 11.0 | 11.0 | 11.0 | 10.3 | 19.0 | 10.3 |
| Total Split (s) | 45.0 | 45.0 | 45.0 | 20.0 | 105.0 | 85.0 |
| Total Split (%) | 30.0% | 30.0% | 30.0% | 13.3% | 70.0% | 56.7% |
| Yellow Time (s) | 4.8 | 4.8 | 4.8 | 2.5 | 4.7 | 4.7 |
| All-Red Time (s) | 2.2 | 2.2 | 2.2 | 3.8 | 1.3 | 1.6 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 6.3 | 6.0 | 6.3 |
| Lead/Lag | | | | Lead | | Lag |
| Lead-Lag Optimize? | | | | Yes | | Yes |
| Recall Mode | Max | Max | Max | Max | Max | C-Max |

Intersection Summary

Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 33 (22%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 90
 Control Type: Actuated-Coordinated

Splits and Phases: 33: Mathilda Ave & SR 237 WB On-Ramp/SR 237 WB Off-Ramp



SimTraffic Post-Processor
Average Results from 10 Runs
Network Performance

Mathilda Avenue Improvements
2018 No Build PM Peak Hour

| Performance Measure | Average | Std. Dev. | Minimum | Maximum |
|---------------------------------|---------|-----------|---------|---------|
| Average Delay (seconds) | 465.2 | 14.0 | 442.6 | 487.1 |
| Total Delay (hours) | 1,504 | 51 | 1,417 | 1,571 |
| Average Stopped Delay (seconds) | 400.5 | 14.3 | 378.4 | 425.8 |
| Total Stopped Delay (hours) | 1295 | 50 | 1212 | 1374 |
| Total Stops | 40,164 | 1,462 | 37,811 | 43,027 |
| Average Stops | 3.45 | 0.10 | 3.30 | 3.63 |
| Total Distance Traveled (miles) | 37,384 | 413 | 36,832 | 38,078 |
| Average Speed (mph) | 15.1 | 0.3 | 15.0 | 16.0 |
| Total Travel Time (hours) | 2,481.2 | 53.0 | 2,400.8 | 2,547.7 |
| Vehicles Entered | 9,858 | 131 | 9,720 | 10,047 |
| Vehicles Exited | 8,456 | 73 | 8,353 | 8,569 |
| Percent Demand Served | 85.8% | 0.7% | 84.9% | 87.3% |
| Fuel Used (gallons) | 1,275 | 15 | 1,252 | 1,301 |
| HC Emissions (grams) | 15,551 | 419 | 14,836 | 16,042 |
| CO Emissions (grams) | 432,243 | 5,149 | 423,246 | 440,545 |
| NOx Emissions (grams) | 55,081 | 1,066 | 53,393 | 56,321 |

Intersection 1 **Mathilda Avenue/5th Avenue** **Signal**

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 110 | 94 | 85.4% | 53.4 | 5.6 | D |
| | Through | 370 | 320 | 86.4% | 20.7 | 3.1 | C |
| | Right Turn | 40 | 34 | 84.3% | 14.3 | 6.2 | B |
| | Subtotal | 520 | 447 | 86.0% | 27.1 | 3.8 | C |
| SB | Left Turn | 10 | 8 | 83.0% | 366.1 | 122.8 | F |
| | Through | 1,110 | 921 | 83.0% | 373.1 | 139.4 | F |
| | Right Turn | 10 | 8 | 80.0% | 351.4 | 196.1 | F |
| | Subtotal | 1,130 | 938 | 83.0% | 372.8 | 139.5 | F |
| EB | Left Turn | 70 | 73 | 103.7% | 32.1 | 3.5 | C |
| | Through | 20 | 22 | 107.5% | 47.8 | 8.1 | D |
| | Right Turn | 70 | 69 | 98.7% | 15.9 | 4.5 | B |
| | Subtotal | 160 | 163 | 102.0% | 27.2 | 4.2 | C |
| WB | Left Turn | 240 | 213 | 88.9% | 190.1 | 104.7 | F |
| | Through | 10 | 9 | 93.0% | 185.7 | 64.6 | F |
| | Right Turn | 30 | 21 | 71.0% | 161.3 | 80.5 | F |
| | Subtotal | 280 | 244 | 87.1% | 187.2 | 100.1 | F |
| Total | | 2,090 | 1,792 | 85.7% | 227.0 | 73.8 | F |

Intersection 2 **Mathilda Avenue/Innovation Way** **Signal**

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 90 | 77 | 86.0% | 66.7 | 5.5 | E |
| | Through | 380 | 352 | 92.7% | 26.5 | 3.8 | C |
| | Right Turn | 40 | 36 | 90.8% | 20.9 | 7.3 | C |
| | Subtotal | 510 | 466 | 91.4% | 32.6 | 3.5 | C |
| SB | Left Turn | | | | | | |
| | Through | 1,370 | 1,112 | 81.2% | 327.2 | 25.7 | F |
| | Right Turn | 50 | 45 | 90.0% | 289.6 | 27.2 | F |
| | Subtotal | 1,420 | 1,157 | 81.5% | 325.7 | 25.4 | F |
| EB | Left Turn | 140 | 94 | 67.4% | 115.6 | 36.2 | F |
| | Through | 10 | 6 | 60.0% | 112.3 | 33.7 | F |
| | Right Turn | 680 | 475 | 69.8% | 119.6 | 42.1 | F |
| | Subtotal | 830 | 575 | 69.3% | 118.9 | 41.1 | F |
| WB | Left Turn | 40 | 39 | 96.3% | 123.7 | 57.0 | F |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | 40 | 39 | 96.3% | 123.7 | 57.0 | F |
| Total | | 2,800 | 2,237 | 79.9% | 206.1 | 12.1 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2018 No Build PM Peak Hour

Intersection 3

Mathilda Avenue/Moffett Park Drive/SR 237 WB Ramps

Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-------------------------|--------------------------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn (Moffett Park) | 100 | 92 | 91.7% | 45.6 | 6.4 | D |
| | Left Turn (SR 237 WB On-Ramp) | 90 | 78 | 86.3% | 79.4 | 2.3 | E |
| | Through | 490 | 450 | 91.8% | 41.4 | 4.3 | D |
| | Right Turn (Moffett Park) | 160 | 145 | 90.3% | 26.1 | 3.1 | C |
| | Subtotal | 840 | 764 | 90.9% | 42.9 | 3.3 | D |
| SB | Left Turn (Moffett Park) | 50 | 38 | 76.0% | 182.8 | 13.9 | F |
| | Through | 1,940 | 1,509 | 77.8% | 229.6 | 6.8 | F |
| | Right Turn (Moffett Park) | 100 | 82 | 82.1% | 244.3 | 7.9 | F |
| | Right Turn (SR 237 WB On-Ramp) | 430 | 333 | 77.5% | 223.2 | 7.4 | F |
| | Subtotal | 2,520 | 1,962 | 77.9% | 228.2 | 6.9 | F |
| EB (Moffett Park) | Left Turn | 70 | 55 | 78.4% | 292.4 | 31.9 | F |
| | Through | 190 | 145 | 76.3% | 282.5 | 46.0 | F |
| | Right Turn | 450 | 332 | 73.8% | 304.3 | 32.4 | F |
| | Subtotal | 710 | 532 | 74.9% | 297.1 | 35.7 | F |
| WB (Moffett Park) | Left Turn | 310 | 287 | 92.5% | 392.9 | 105.3 | F |
| | Through | 260 | 233 | 89.7% | 130.3 | 45.9 | F |
| | Right Turn | 20 | 20 | 100.5% | 121.2 | 47.4 | F |
| | Subtotal | 590 | 540 | 91.6% | 269.4 | 79.5 | F |
| WB (SR 237 WB Off-Ramp) | Left Turn | 760 | 675 | 88.8% | 465.4 | 130.2 | F |
| | Through | | | | | | F |
| | Right Turn | 190 | 177 | 92.9% | 414.8 | 130.3 | F |
| | Subtotal | 950 | 851 | 89.6% | 454.9 | 130.4 | F |
| Total | | 5,610 | 4,649 | 82.9% | 301.1 | 30.4 | F |

Intersection 4

Mathilda Avenue/SR 237 EB Off-Ramp-SR 237 EB On-Ramp

Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | 410 | 362 | 88.3% | 37.0 | 1.9 | D |
| | Right Turn | 670 | 586 | 87.4% | 9.8 | 0.3 | A |
| | Subtotal | 1,080 | 948 | 87.8% | 20.2 | 1.0 | C |
| SB | Left Turn | 360 | 295 | 82.1% | 35.8 | 1.8 | D |
| | Through | 2,670 | 2,173 | 81.4% | 13.9 | 0.2 | B |
| | Right Turn | | | | | | |
| | Subtotal | 3,030 | 2,469 | 81.5% | 16.6 | 0.4 | B |
| EB | Left Turn | 170 | 167 | 98.4% | 54.8 | 3.3 | D |
| | Through | | | | | | |
| | Right Turn | 180 | 179 | 99.2% | 20.4 | 2.6 | C |
| | Subtotal | 350 | 346 | 98.8% | 37.0 | 2.6 | D |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 4,460 | 3,762 | 84.3% | 19.4 | 0.5 | B |

Intersection 5

Mathilda Avenue/Ross Drive

Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 90 | 75 | 83.2% | 85.2 | 23.6 | F |
| | Through | 940 | 826 | 87.9% | 375.4 | 49.2 | F |
| | Right Turn | 270 | 245 | 90.6% | 91.2 | 2.4 | F |
| | Subtotal | 1,300 | 1,146 | 88.1% | 295.7 | 36.4 | F |
| SB | Left Turn | 140 | 117 | 83.3% | 40.7 | 3.3 | D |
| | Through | 2,620 | 2,154 | 82.2% | 11.6 | 0.5 | B |
| | Right Turn | 90 | 79 | 88.1% | 7.5 | 1.0 | A |
| | Subtotal | 2,850 | 2,350 | 82.4% | 12.9 | 0.6 | B |
| EB | Left Turn | 40 | 39 | 98.5% | 49.7 | 9.0 | D |
| | Through | 150 | 147 | 98.1% | 47.2 | 3.8 | D |
| | Right Turn | 40 | 36 | 89.5% | 36.0 | 6.5 | D |
| | Subtotal | 230 | 222 | 96.7% | 45.8 | 3.2 | D |
| WB | Left Turn | 230 | 177 | 77.1% | 641.9 | 105.9 | F |
| | Through | 50 | 39 | 77.0% | 652.8 | 111.2 | F |
| | Right Turn | 100 | 80 | 79.8% | 633.3 | 125.5 | F |
| | Subtotal | 380 | 296 | 77.8% | 641.5 | 110.8 | F |
| Total | | 4,760 | 4,013 | 84.3% | 141.4 | 11.0 | F |

Intersection 8

Mathilda Avenue/Almanor Avenue-Ahwanee Avenue

Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 60 | 52 | 86.7% | 222.0 | 94.3 | F |
| | Through | 1,380 | 1,174 | 85.1% | 253.9 | 115.2 | F |
| | Right Turn | 40 | 29 | 73.5% | 305.0 | 151.8 | F |
| | Subtotal | 1,480 | 1,255 | 84.8% | 253.8 | 114.9 | F |
| SB | Left Turn | 180 | 152 | 84.3% | 101.3 | 15.1 | F |
| | Through | 2,800 | 2,438 | 87.1% | 83.4 | 18.4 | F |
| | Right Turn | 70 | 61 | 87.6% | 34.9 | 12.7 | C |
| | Subtotal | 3,050 | 2,651 | 86.9% | 83.3 | 17.9 | F |
| EB | Left Turn | 310 | 288 | 92.8% | 221.8 | 147.4 | F |
| | Through | 30 | 25 | 83.7% | 211.4 | 142.3 | F |
| | Right Turn | 70 | 64 | 91.6% | 172.8 | 137.7 | F |
| | Subtotal | 410 | 377 | 91.9% | 212.8 | 144.7 | F |
| WB | Left Turn | 50 | 48 | 96.0% | 68.0 | 14.6 | E |
| | Through | 10 | 12 | 115.0% | 99.2 | 35.7 | F |
| | Right Turn | 190 | 188 | 99.1% | 79.8 | 34.2 | E |
| | Subtotal | 250 | 248 | 99.1% | 78.8 | 30.4 | E |
| Total | | 5,190 | 4,531 | 87.3% | 139.9 | 45.0 | F |

Intersection 9

US 101 On-Ramp/Moffett Park Drive

Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| EB | Left Turn | | | | | | |
| | Through | 790 | 587 | 74.3% | 104.6 | 25.8 | F |
| | Right Turn | 90 | 74 | 82.0% | 53.7 | 15.0 | D |
| | Subtotal | 880 | 660 | 75.0% | 98.9 | 24.3 | F |
| WB | Left Turn | 230 | 201 | 87.3% | 33.2 | 10.9 | C |
| | Through | 320 | 283 | 88.3% | 1.9 | 0.3 | A |
| | Right Turn | | | | | | |
| | Subtotal | 550 | 483 | 87.9% | 14.9 | 4.6 | B |
| Total | | 1,430 | 1,144 | 80.0% | 63.0 | 14.1 | E |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2018 No Build PM Peak Hour

Intersection 10 Innovation Way/Moffett Park Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | 200 | 176 | 88.0% | 229.7 | 97.8 | F |
| | Through | | | | | | |
| | Right Turn | 150 | 130 | 86.3% | 213.8 | 91.5 | F |
| | Subtotal | 350 | 305 | 87.3% | 223.0 | 95.7 | F |
| EB | Left Turn | 50 | 36 | 71.0% | 224.0 | 42.5 | F |
| | Through | 740 | 509 | 68.8% | 314.0 | 64.7 | F |
| | Right Turn | | | | | | |
| | Subtotal | 790 | 545 | 68.9% | 308.0 | 62.4 | F |
| WB | Left Turn | | | | | | |
| | Through | 400 | 354 | 88.4% | 20.2 | 3.6 | C |
| | Right Turn | 60 | 51 | 84.5% | 4.8 | 0.4 | A |
| | Subtotal | 460 | 404 | 87.9% | 18.2 | 3.1 | B |
| Total | | 1,600 | 1,254 | 78.4% | 190.5 | 30.0 | F |

Intersection 11 Innovation Way/11th Avenue All-way Stop

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 30 | 23 | 77.0% | 34.1 | 24.5 | D |
| | Through | 70 | 54 | 76.7% | 35.5 | 22.3 | E |
| | Right Turn | | | | | | |
| | Subtotal | 100 | 77 | 76.8% | 35.6 | 21.4 | E |
| SB | Left Turn | 10 | 9 | 85.0% | 19.1 | 16.9 | C |
| | Through | 60 | 58 | 96.3% | 73.7 | 79.2 | F |
| | Right Turn | 20 | 18 | 92.0% | 83.2 | 116.1 | F |
| | Subtotal | 90 | 85 | 94.1% | 71.5 | 81.9 | F |
| EB | Left Turn | 390 | 356 | 91.3% | 184.7 | 155.3 | F |
| | Through | | | | | | |
| | Right Turn | 270 | 246 | 91.0% | 165.5 | 160.6 | F |
| | Subtotal | 660 | 602 | 91.2% | 172.7 | 134.6 | F |
| WB | Left Turn | 10 | 9 | 90.0% | 105.6 | 82.2 | F |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | 10 | 9 | 90.0% | 105.6 | 82.2 | F |
| Total | | 860 | 772 | 89.8% | 144.4 | 107.3 | F |

Intersection 12 Innovation Way/Juniper Driveway All-way Stop

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | 460 | 361 | 78.5% | 454.4 | 257.2 | F |
| | Right Turn | | | | | | |
| | Subtotal | 460 | 361 | 78.5% | 454.4 | 257.2 | F |
| SB | Left Turn | | | | | | |
| | Through | 60 | 52 | 86.5% | 69.7 | 29.4 | F |
| | Right Turn | 80 | 68 | 85.3% | 35.6 | 11.5 | E |
| | Subtotal | 140 | 120 | 85.8% | 50.4 | 18.4 | F |
| EB | Left Turn | 370 | 212 | 57.4% | 813.5 | 254.5 | F |
| | Through | | | | | | |
| | Right Turn | 30 | 34 | 113.3% | 78.5 | 36.7 | F |
| | Subtotal | 400 | 246 | 61.6% | 709.0 | 217.2 | F |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 1,000 | 728 | 72.8% | 463.4 | 160.0 | F |

Intersection 13 Bordeaux Drive/Innovation Way All-way Stop

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 10 | 8 | 84.0% | 4.6 | 0.3 | A |
| | Through | 30 | 64 | 212.0% | 2.7 | 0.4 | A |
| | Right Turn | | | | | | |
| | Subtotal | 40 | 72 | 180.0% | 2.9 | 0.4 | A |
| SB | Left Turn | | | | | | |
| | Through | 140 | 133 | 94.6% | 21.1 | 19.4 | C |
| | Right Turn | 10 | 12 | 115.0% | 17.4 | 19.0 | C |
| | Subtotal | 150 | 144 | 96.0% | 20.8 | 19.2 | C |
| EB | Left Turn | 10 | 6 | 57.0% | 5.0 | 0.6 | A |
| | Through | 10 | 10 | 95.0% | 6.1 | 1.2 | A |
| | Right Turn | 10 | 10 | 97.0% | 3.4 | 0.7 | A |
| | Subtotal | 30 | 25 | 83.0% | 4.7 | 0.8 | A |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 220 | 241 | 109.5% | 13.5 | 10.5 | B |

Intersection 1

Mathilda Avenue/5th Avenue

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 625 | 50 | 17 | 100 | 25 | 150 | 29 | 5% | 0% |
| | Through | 625 | 25 | 5 | 50 | 7 | 75 | 7 | 0% | 0% |
| | Right Turn | 625 | 25 | 7 | 75 | 12 | 100 | 16 | 0% | 0% |
| NB | Left Turn | 425 | 75 | 6 | 125 | 9 | 125 | 18 | 0% | 0% |
| | Through | 1,125 | 75 | 8 | 125 | 16 | 175 | 32 | 0% | 0% |
| | Through/Right | 1,125 | 75 | 11 | 175 | 20 | 200 | 32 | 0% | 0% |
| SB | Left Turn | 250 | 50 | 22 | 175 | 54 | 300 | 1 | 0% | 0% |
| | Through | 1,325 | 1,100 | 288 | 1,925 | 423 | 2,050 | 342 | 74% | 0% |
| | Right Turn | 250 | 50 | 21 | 200 | 57 | 300 | 0 | 0% | 0% |
| WB | Left Turn | 925 | 325 | 127 | 700 | 276 | 975 | 316 | 77% | 0% |
| | Through/Right | 75 | 50 | 7 | 100 | 9 | 100 | 0 | 5% | 0% |

Intersection 2

Mathilda Avenue/Innovation Way

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 200 | 50 | 14 | 125 | 21 | 150 | 18 | 0% | 20% |
| | Through/Right | 225 | 25 | 1 | 50 | 6 | 50 | 12 | 0% | 64% |
| | Right Turn | 225 | 275 | 11 | 325 | 13 | 325 | 18 | 0% | 63% |
| NB | Left Turn | 400 | 50 | 7 | 75 | 15 | 100 | 22 | 0% | 0% |
| | Through | 975 | 75 | 13 | 150 | 19 | 175 | 27 | 0% | 0% |
| | Through/Right | 975 | 100 | 10 | 175 | 19 | 200 | 20 | 0% | 0% |
| SB | Left Turn | 75 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | Through | 975 | 1,125 | 58 | 1,275 | 84 | 1,200 | 16 | 85% | 38% |
| | Right Turn | 225 | 150 | 20 | 350 | 21 | 275 | 0 | 0% | 0% |
| WB | Left Turn | 425 | 25 | 13 | 75 | 36 | 100 | 57 | 0% | 0% |
| | Shared | 225 | 25 | 11 | 75 | 28 | 100 | 40 | 0% | 0% |

SimTraffic Post-Processor
Average Results from 10 Runs
Queue Length

Mathilda Avenue Improvements
2018 No Build
PM Peak Hour

Intersection 3

Mathilda Avenue/Moffett Park Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-------------------------|-----------------------------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB (Moffett Park) | Left Turn | 525 | 300 | 394 | 475 | 386 | 525 | 373 | 0% | 2% |
| | Through/Right | 1,125 | 1,075 | 96 | 1,325 | 108 | 1,175 | 41 | 0% | 33% |
| | Right Turn | 1,125 | 925 | 404 | 975 | 421 | 950 | 412 | 0% | 43% |
| NB | Left Turn (Moffett Park) | 125 | 25 | 3 | 50 | 7 | 50 | 11 | 0% | 1% |
| | Through | 300 | 100 | 11 | 200 | 22 | 225 | 44 | 0% | 27% |
| | Through/Right (Moffett Park) | 300 | 100 | 11 | 200 | 19 | 225 | 43 | 0% | 19% |
| | Left Turn (SR 237 WB On-Ramp) | 175 | 100 | 8 | 150 | 14 | 175 | 18 | 0% | 1% |
| SB | Left Turn (Moffett Park) | 175 | 50 | 11 | 125 | 29 | 175 | 48 | 0% | 0% |
| | Through | 1,100 | 1,125 | 19 | 1,200 | 21 | 1,175 | 19 | 70% | 65% |
| | Through/Right (Moffett Park) | 975 | 1,075 | 3 | 1,100 | 13 | 1,125 | 12 | 0% | 41% |
| WB (Moffett Park) | Through/Right (SR 237 WB On-Ramp) | 1,100 | 1,125 | 15 | 1,175 | 21 | 1,175 | 22 | 70% | 67% |
| | Left Turn | 300 | 800 | 204 | 1,275 | 271 | 1,400 | 258 | 78% | 0% |
| WB (Moffett Park) | Through/Right | 675 | 475 | 144 | 675 | 121 | 650 | 13 | 4% | 22% |
| | Left Turn | 1,075 | 3,150 | 1,106 | 4,675 | 1,360 | 4,675 | 1,320 | 67% | 0% |
| WB (SR 237 WB Off-Ramp) | Left/Through | 325 | 450 | 1 | 450 | 3 | 450 | 0 | 67% | 0% |
| | Right Turn | 325 | 325 | 27 | 500 | 14 | 375 | 0 | 3% | 0% |

Intersection 4

Mathilda Avenue/SR 237 EB Off-Ramp-SR 237 EB On-Ramp

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,025 | 75 | 9 | 125 | 23 | 150 | 47 | 0% | 0% |
| | Shared | 1,025 | 100 | 12 | 200 | 22 | 250 | 27 | 0% | 0% |
| NB | Through | 275 | 50 | 8 | 100 | 19 | 125 | 27 | 0% | 0% |
| | Right Turn | 275 | 75 | 9 | 200 | 22 | 250 | 46 | 0% | 0% |
| SB | Left Turn | 175 | 100 | 14 | 175 | 16 | 200 | 16 | 0% | 6% |
| | Through | 175 | 200 | 4 | 225 | 7 | 225 | 13 | 0% | 17% |
| | | | | | | | | | | |

Intersection 5

Mathilda Avenue/Ross Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 250 | 150 | 18 | 275 | 24 | 325 | 30 | 28% | 0% |
| | Through | 1,575 | 100 | 3 | 125 | 3 | 100 | 0 | 57% | 0% |
| | Right Turn | 50 | 50 | 8 | 75 | 8 | 75 | 3 | 11% | 0% |
| NB | Left Turn | 150 | 100 | 15 | 175 | 33 | 175 | 36 | 7% | 0% |
| | Through | 2,200 | 975 | 50 | 1,100 | 71 | 1,100 | 139 | 0% | 34% |
| | Through/Right | 450 | 525 | 4 | 550 | 5 | 550 | 12 | 0% | 76% |
| SB | Left Turn | 225 | 100 | 10 | 175 | 17 | 200 | 31 | 8% | 0% |
| | Through | 225 | 125 | 13 | 200 | 22 | 250 | 27 | 3% | 0% |
| | Through/Right | 225 | 125 | 11 | 200 | 23 | 275 | 40 | 0% | 1% |
| WB | Left Turn | 100 | 2,150 | 404 | 3,225 | 747 | 3,350 | 773 | 85% | 0% |
| | Through | 225 | 75 | 6 | 125 | 4 | 100 | 0 | 5% | 0% |
| | Right Turn | 100 | 50 | 4 | 100 | 5 | 100 | 0 | 7% | 0% |

Intersection 8

Mathilda Avenue/Almanor Avenue-Ahwanee Avenue

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,025 | 275 | 41 | 350 | 43 | 350 | 8 | 59% | 30% |
| | Through/Right | 125 | 125 | 14 | 250 | 24 | 225 | 0 | 5% | 0% |
| NB | Left Turn | 425 | 125 | 39 | 300 | 84 | 375 | 66 | 0% | 0% |
| | Through | 750 | 975 | 110 | 1,900 | 134 | 2,175 | 17 | 71% | 0% |
| | Right Turn | 75 | 25 | 4 | 100 | 9 | 100 | 0 | 0% | 0% |
| SB | Left Turn | 125 | 150 | 6 | 225 | 7 | 175 | 0 | 34% | 0% |
| | Through | 2,225 | 1,075 | 61 | 1,500 | 48 | 1,700 | 18 | 39% | 0% |
| | Through/Right | 2,225 | 350 | 52 | 500 | 37 | 525 | 13 | 0% | 0% |
| WB | Left Turn | 250 | 75 | 15 | 225 | 61 | 325 | 73 | 0% | 0% |
| | Through | 1,025 | 175 | 70 | 425 | 158 | 550 | 220 | 2% | 0% |
| | Right Turn | 75 | 100 | 8 | 150 | 5 | 125 | 0 | 49% | 0% |

Intersection 9

US 101 On-Ramp/Moffett Park Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Through | 850 | 650 | 97 | 1,100 | 56 | 900 | 4 | 57% | 12% |
| | Right Turn | 150 | 150 | 39 | 425 | 55 | 375 | 0 | 0% | 0% |
| WB | Left Turn | 850 | 125 | 22 | 250 | 59 | 325 | 90 | 0% | 0% |
| | Through | 850 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | | | | | | | | | | |
| | | | | | | | | | | |

Intersection 10

Innovation Way/Moffett Park Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 225 | 150 | 28 | 400 | 53 | 350 | 0 | 0% | 0% |
| | Through | 850 | 800 | 122 | 1,100 | 67 | 950 | 7 | 54% | 29% |
| SB | Left Turn | 575 | 250 | 35 | 525 | 39 | 525 | 33 | 0% | 8% |
| | Shared | 575 | 425 | 34 | 625 | 26 | 550 | 21 | 0% | 43% |
| WB | Through | 1,150 | 100 | 11 | 175 | 20 | 225 | 35 | 0% | 0% |
| | Right Turn | 1,150 | 25 | 3 | 50 | 33 | 100 | 95 | 0% | 0% |
| | | | | | | | | | | |

Intersection 11

Innovation Way/11th Avenue

All-way Stop

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 125 | 125 | 9 | 175 | 11 | 150 | 0 | 44% | 0% |
| | Through/Right | 325 | 650 | 503 | 1,575 | 1,119 | 1,800 | 1,211 | 2% | 0% |
| | Right Turn | 325 | 450 | 329 | 1,100 | 758 | 1,400 | 876 | 0% | 0% |
| NB | Left Turn | 125 | 25 | 3 | 25 | 10 | 50 | 18 | 0% | 0% |
| | Left/Through | 575 | 75 | 7 | 150 | 17 | 200 | 32 | 0% | 0% |
| | Through/Right | 575 | 25 | 7 | 50 | 23 | 100 | 43 | 0% | 0% |
| SB | Left/Through | 1,000 | 25 | 7 | 75 | 24 | 100 | 67 | 0% | 0% |
| | Through/Right | 1,000 | 75 | 43 | 175 | 111 | 200 | 119 | 0% | 0% |
| WB | Left Turn | 325 | 25 | 6 | 50 | 14 | 75 | 20 | 0% | 0% |
| | Through/Right | 325 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |

Intersection 12

Innovation Way/Juniper Driveway

All-way Stop

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 200 | 2,350 | 789 | 4,125 | 1,268 | 4,225 | 1,252 | 0% | 0% |
| | Right Turn | 200 | 475 | 151 | 1,075 | 182 | 1,025 | 165 | 0% | 0% |
| NB | Left Turn | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | Through | 1,000 | 675 | 212 | 1,075 | 241 | 1,000 | 177 | 90% | 18% |
| SB | Through/Right | 300 | 175 | 53 | 225 | 92 | 225 | 91 | 0% | 0% |
| | Right Turn | 300 | 75 | 48 | 175 | 86 | 200 | 96 | 0% | 0% |
| | | | | | | | | | | |

Intersection 13

Bordeaux Drive/Innovation Way

All-way Stop

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left/Through | 375 | 25 | 3 | 50 | 4 | 50 | 0 | 0% | 0% |
| | Right Turn | 125 | 25 | 2 | 50 | 5 | 50 | 7 | 0% | 0% |
| NB | Left Turn | 325 | 25 | 2 | 50 | 5 | 50 | 0 | 0% | 0% |
| | Through/Right | 2,025 | 25 | 3 | 50 | 5 | 50 | 16 | 0% | 0% |
| SB | Left Turn | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | Through/Right | 725 | 50 | 4 | 75 | 6 | 75 | 13 | 0% | 0% |
| WB | Left/Through | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | Right Turn | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |

Arterial Level of Service: NB Mathilda Ave

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|----------------------|------|---------------|-----------------|------------|----------------|
| Ahwanee Ave | 8 | 119.4 | 130.2 | 0.1 | 4 |
| US 101 SB Diag. On-R | 702 | 17.5 | 24.1 | 0.1 | 12 |
| US 101 SB Loop On-Ra | 701 | 79.5 | 87.3 | 0.1 | 4 |
| US 101 NB Loop On-Ra | 602 | 70.3 | 76.0 | 0.1 | 3 |
| US 101 NB Diag.Off-R | 601 | 125.5 | 132.3 | 0.1 | 2 |
| Ross Dr | 5 | 76.8 | 84.4 | 0.1 | 4 |
| SR 237 EB On-Ramp | 4 | 34.4 | 39.7 | 0.1 | 6 |
| SR 237 WB Off-Ramp | 33 | 11.5 | 15.3 | 0.0 | 11 |
| Moffett Park Dr | 3 | 33.9 | 36.6 | 0.0 | 4 |
| Innovation Way | 2 | 26.6 | 43.7 | 0.2 | 18 |
| 5th Ave | 1 | 21.5 | 40.4 | 0.2 | 21 |
| | 107 | 3.9 | 26.1 | 0.3 | 38 |
| Total | | 620.9 | 736.2 | 1.5 | 7 |

Arterial Level of Service: SB Mathilda Ave

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|----------------------|------|---------------|-----------------|------------|----------------|
| 5th Ave | 1 | 311.7 | 332.7 | 0.3 | 3 |
| Innovation Way | 2 | 314.1 | 330.8 | 0.2 | 3 |
| Moffett Park Dr | 3 | 210.9 | 227.5 | 0.2 | 3 |
| SR 237 WB On-Ramp | 33 | 3.4 | 6.4 | 0.0 | 23 |
| SR 237 Off/On Ramp | 4 | 4.1 | 8.2 | 0.0 | 21 |
| Ross Dr | 5 | 9.6 | 14.6 | 0.1 | 16 |
| US 101 NB Diag.Off-R | 601 | 21.0 | 29.2 | 0.1 | 11 |
| US 101 NB Loop Off-R | 602 | 10.3 | 16.0 | 0.1 | 20 |
| US 101 SB Loop On-Ra | 701 | 4.3 | 10.4 | 0.1 | 23 |
| US 101 SB Off-Ramp | 702 | 4.9 | 11.5 | 0.1 | 33 |
| Almanor Ave | 8 | 42.6 | 50.7 | 0.1 | 6 |
| San Aleso Ave | 201 | 6.7 | 18.1 | 0.1 | 28 |
| Total | | 943.6 | 1056.0 | 1.5 | 5 |

Arterial Level of Service: NB Innovation Way

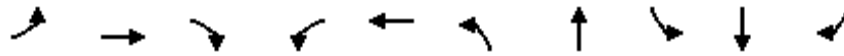
| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|------------------|------|---------------|-----------------|-----------|----------------|
| | 910 | 6.5 | 8.5 | 0.0 | 10 |
| | 38 | 1.0 | 7.2 | 0.0 | 21 |
| | 11 | 30.6 | 40.4 | 0.1 | 6 |
| | 200 | 154.0 | 166.9 | 0.2 | 3 |
| Juniper Driveway | 12 | 188.2 | 195.8 | 0.1 | 1 |
| Driveway | 217 | 39.0 | 43.1 | 0.0 | 3 |
| | 902 | 58.8 | 62.5 | 0.0 | 1 |
| Mathilda Ave | 2 | 10.5 | 12.7 | 0.0 | 7 |
| | 53 | 2.6 | 17.1 | 0.1 | 20 |
| Bordeaux Dr | 13 | 4.9 | 13.4 | 0.1 | 21 |
| Total | | 496.3 | 567.6 | 0.6 | 4 |

Arterial Level of Service: SB Innovation Way

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|------------------|------|---------------|-----------------|-----------|----------------|
| | 53 | 0.3 | 13.7 | 0.1 | 21 |
| Mathilda Ave | 2 | 115.6 | 127.5 | 0.1 | 3 |
| | 902 | 0.9 | 6.1 | 0.0 | 15 |
| Driveway | 217 | 0.3 | 2.8 | 0.0 | 27 |
| Juniper Driveway | 12 | 71.2 | 76.5 | 0.0 | 2 |
| | 200 | 1.9 | 10.9 | 0.1 | 19 |
| 11th Ave | 11 | 70.9 | 92.4 | 0.2 | 6 |
| | 38 | 81.1 | 94.1 | 0.1 | 3 |
| | 910 | 91.3 | 96.5 | 0.0 | 2 |
| Moffett Park Dr | 10 | 22.3 | 25.5 | 0.0 | 3 |
| Total | | 455.8 | 546.1 | 0.6 | 4 |

Lanes, Volumes, Timings
1: Mathilda Ave & 5th Ave

3/4/2016

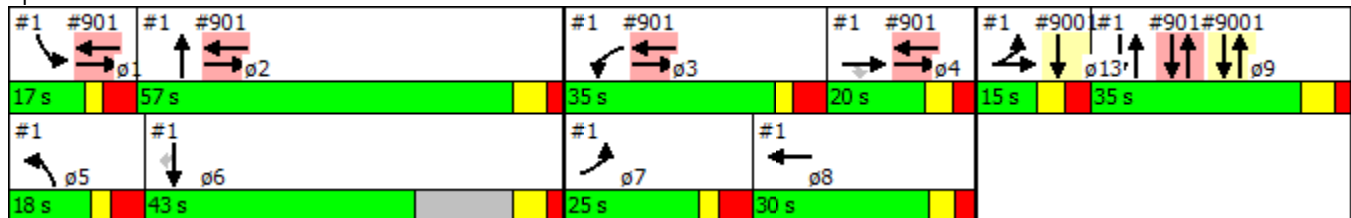


| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT | SBR | ø2 | ø7 |
|----------------------|------|------|--------|-------|-------|-------|-----|------|-----|--------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 20 | 10 | 30 | 30 | 10 | 80 | 870 | 10 | 370 | 70 | | |
| Turn Type | Prot | NA | custom | Prot | NA | Prot | NA | Prot | NA | custom | | |
| Protected Phases | 7 13 | 4 13 | | 3 | 8 | 5 | 2 9 | 1 | 6 9 | | 2 | 7 |
| Permitted Phases | | | 4 | | | | | | | 6 | | |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 5 | 2 | 1 | 6 | 6 | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 13.0 | 12.0 | 8.0 | 11.0 | | 10.0 | | 12.0 | 12.0 | 12.0 |
| Minimum Split (s) | | | 20.0 | 19.0 | 29.5 | 18.0 | | 17.0 | | 41.0 | 37.0 | 19.0 |
| Total Split (s) | | | 20.0 | 35.0 | 30.0 | 18.0 | | 17.0 | | 43.0 | 57.0 | 25.0 |
| Total Split (%) | | | 11.2% | 19.6% | 16.8% | 10.1% | | 9.5% | | 24.0% | 32% | 14% |
| Yellow Time (s) | | | 3.6 | 2.5 | 3.6 | 2.5 | | 2.5 | | 4.7 | 4.7 | 2.5 |
| All-Red Time (s) | | | 3.4 | 4.5 | 2.9 | 4.5 | | 4.5 | | 2.3 | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | | 0.0 | | |
| Total Lost Time (s) | | | 7.0 | 7.0 | 6.5 | 7.0 | | 7.0 | | 7.0 | | |
| Lead/Lag | | | Lag | Lead | Lag | Lead | | Lead | | Lag | Lag | Lead |
| Lead-Lag Optimize? | | | Yes | Yes | Yes | Yes | | Yes | | Yes | Yes | Yes |
| Recall Mode | | | None | None | None | None | | None | | None | Min | None |

Intersection Summary

Cycle Length: 179
 Actuated Cycle Length: 84.6
 Natural Cycle: 160
 Control Type: Actuated-Uncoordinated

Splits and Phases: 1: Mathilda Ave & 5th Ave



| Lane Group | ø9 | ø13 |
|----------------------|------|------|
| Lane Configurations | | |
| Volume (vph) | | |
| Turn Type | | |
| Protected Phases | 9 | 13 |
| Permitted Phases | | |
| Detector Phase | | |
| Switch Phase | | |
| Minimum Initial (s) | 28.0 | 8.0 |
| Minimum Split (s) | 35.0 | 15.0 |
| Total Split (s) | 35.0 | 15.0 |
| Total Split (%) | 20% | 8% |
| Yellow Time (s) | 4.7 | 3.6 |
| All-Red Time (s) | 2.3 | 3.4 |
| Lost Time Adjust (s) | | |
| Total Lost Time (s) | | |
| Lead/Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes |
| Recall Mode | None | None |
| Intersection Summary | | |

Lanes, Volumes, Timings
2: Mathilda Ave & Innovation Way

3/4/2016

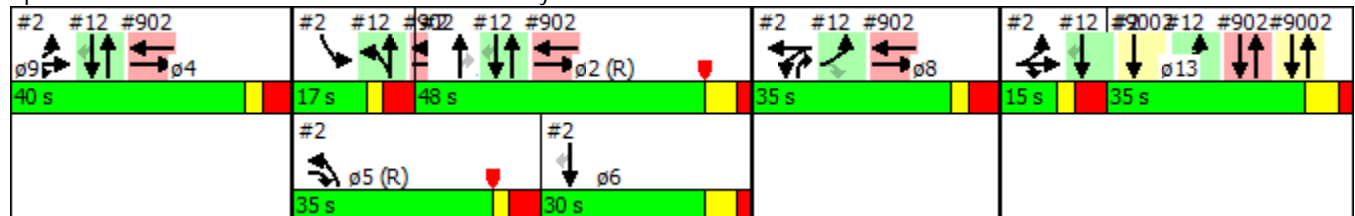


| Lane Group | EBT | EBR | WBL | WBT | NBL | NBT | NBR | SBL | SBT | SBR | ø2 | ø4 |
|----------------------|------|--------|-------|-------|-------|-----|-------|------|-----|------|-------|------|
| Lane Configurations | ↕ | ↕↕ | ↕ | ↕↕ | ↕↕ | ↕↕ | ↕ | ↕ | ↕↕↕ | ↕ | | |
| Volume (vph) | 60 | 50 | 210 | 110 | 520 | 970 | 880 | 20 | 280 | 130 | | |
| Turn Type | NA | pt+ov | Split | NA | Prot | NA | pm+ov | Prot | NA | Perm | | |
| Protected Phases | 4 13 | 4 13 5 | 8 | 8 | 5 | 2 9 | 8 | 1 | 6 9 | | 2 | 4 |
| Permitted Phases | | | | | | | 2 9 | | | 6 9 | | |
| Detector Phase | 4 | 4 | 8 | 8 | 5 | 2 | 2 | 1 | 6 | 6 | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 10.0 | 10.0 | 13.0 | | 10.0 | 10.0 | | | 12.0 | 14.0 |
| Minimum Split (s) | | | 35.0 | 35.0 | 20.0 | | 35.0 | 16.8 | | | 19.0 | 39.0 |
| Total Split (s) | | | 35.0 | 35.0 | 35.0 | | 35.0 | 17.0 | | | 48.0 | 40.0 |
| Total Split (%) | | | 18.4% | 18.4% | 18.4% | | 18.4% | 8.9% | | | 25% | 21% |
| Yellow Time (s) | | | 2.5 | 2.5 | 2.5 | | 2.5 | 2.5 | | | 4.7 | 2.5 |
| All-Red Time (s) | | | 4.5 | 4.5 | 4.5 | | 4.5 | 4.3 | | | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | | | | |
| Total Lost Time (s) | | | 7.0 | 7.0 | 7.0 | | 7.0 | 6.8 | | | | |
| Lead/Lag | | | | | Lead | | | Lead | | | Lag | |
| Lead-Lag Optimize? | | | | | Yes | | | Yes | | | Yes | |
| Recall Mode | | | None | None | C-Max | | None | None | | | C-Max | None |

Intersection Summary

Cycle Length: 190
 Actuated Cycle Length: 190
 Offset: 133 (70%), Referenced to phase 2:NBT and 5:NBL, Start of Yellow
 Natural Cycle: 175
 Control Type: Actuated-Coordinated

Splits and Phases: 2: Mathilda Ave & Innovation Way



Lanes, Volumes, Timings
 2: Mathilda Ave & Innovation Way

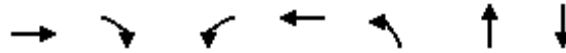
3/4/2016

| Lane Group | ø6 | ø9 | ø13 |
|----------------------|------|------|------|
| Lane Configurations | | | |
| Volume (vph) | | | |
| Turn Type | | | |
| Protected Phases | 6 | 9 | 13 |
| Permitted Phases | | | |
| Detector Phase | | | |
| Switch Phase | | | |
| Minimum Initial (s) | 12.0 | 28.0 | 8.0 |
| Minimum Split (s) | 30.0 | 35.0 | 15.0 |
| Total Split (s) | 30.0 | 35.0 | 15.0 |
| Total Split (%) | 16% | 18% | 8% |
| Yellow Time (s) | 4.7 | 4.7 | 2.5 |
| All-Red Time (s) | 2.3 | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | |
| Total Lost Time (s) | | | |
| Lead/Lag | Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes | Yes |
| Recall Mode | Min | None | None |
| Intersection Summary | | | |

Lanes, Volumes, Timings

3: Mathilda Ave & Moffett Park Dr/SR 237 WB Off-Ramp

3/4/2016

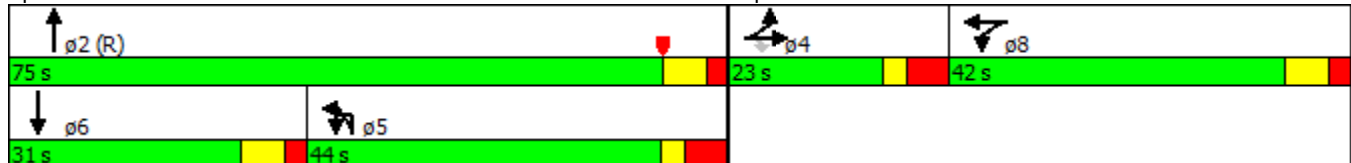


| Lane Group | EBT | EBR | WBL | WBT | NBL | NBT | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | |
| Volume (vph) | 0 | 70 | 670 | 200 | 710 | 2120 | 320 |
| Turn Type | NA | Perm | Split | NA | Prot | NA | NA |
| Protected Phases | 4 | | 8 | 8 | 5 | 2 | 6 |
| Permitted Phases | | 4 | | | | | |
| Detector Phase | 4 | 4 | 8 | 8 | 5 | 2 | 6 |
| Switch Phase | | | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 8.0 | 8.0 |
| Minimum Split (s) | 23.0 | 23.0 | 40.0 | 40.0 | 11.0 | 34.9 | 14.9 |
| Total Split (s) | 23.0 | 23.0 | 42.0 | 42.0 | 44.0 | 75.0 | 31.0 |
| Total Split (%) | 16.4% | 16.4% | 30.0% | 30.0% | 31.4% | 53.6% | 22.1% |
| Yellow Time (s) | 2.5 | 2.5 | 4.5 | 4.5 | 2.5 | 4.7 | 4.7 |
| All-Red Time (s) | 4.5 | 4.5 | 2.5 | 2.5 | 4.5 | 2.2 | 2.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.9 | 6.9 |
| Lead/Lag | | | | | Lag | | Lead |
| Lead-Lag Optimize? | | | | | Yes | | Yes |
| Recall Mode | Max | Max | Max | Max | None | C-Max | None |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 114 (81%), Referenced to phase 2:NBT, Start of Yellow
 Natural Cycle: 120
 Control Type: Actuated-Coordinated

Splits and Phases: 3: Mathilda Ave & Moffett Park Dr/SR 237 WB Off-Ramp



Lanes, Volumes, Timings
 4: Mathilda Ave & SR 237 EB Ramps

3/4/2016

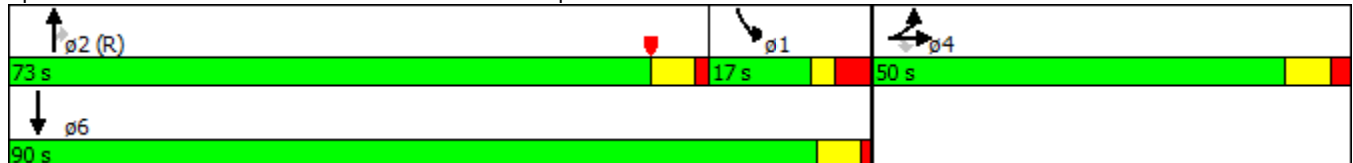


| Lane Group | EBL | EBT | EBR | NBT | NBR | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↶ | ↷ | ↸ | ↑↑↑↑ | ↷↸ | ↶ | ↑↑↑ |
| Volume (vph) | 590 | 0 | 60 | 2380 | 760 | 50 | 910 |
| Turn Type | Split | NA | Perm | NA | Perm | Prot | NA |
| Protected Phases | 4 | 4 | | 2 | | 1 | 6 |
| Permitted Phases | | | 4 | | 2 | | |
| Detector Phase | 4 | 4 | 4 | 2 | 2 | 1 | 6 |
| Switch Phase | | | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 4.0 | 8.0 | 8.0 | 4.0 | 8.0 |
| Minimum Split (s) | 12.0 | 12.0 | 12.0 | 20.7 | 20.7 | 10.4 | 13.9 |
| Total Split (s) | 50.0 | 50.0 | 50.0 | 73.0 | 73.0 | 17.0 | 90.0 |
| Total Split (%) | 35.7% | 35.7% | 35.7% | 52.1% | 52.1% | 12.1% | 64.3% |
| Yellow Time (s) | 4.8 | 4.8 | 4.8 | 4.7 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 2.2 | 2.2 | 2.2 | 1.5 | 1.5 | 3.9 | 1.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 6.2 | 6.2 | 6.4 | 5.9 |
| Lead/Lag | | | | Lead | Lead | Lag | |
| Lead-Lag Optimize? | | | | Yes | Yes | Yes | |
| Recall Mode | Max | Max | Max | C-Max | C-Max | None | Max |

Intersection Summary

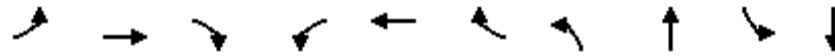
Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 135 (96%), Referenced to phase 2:NBT, Start of Yellow
 Natural Cycle: 60
 Control Type: Actuated-Coordinated

Splits and Phases: 4: Mathilda Ave & SR 237 EB Ramps



Lanes, Volumes, Timings
5: Mathilda Ave & Ross Dr

3/4/2016

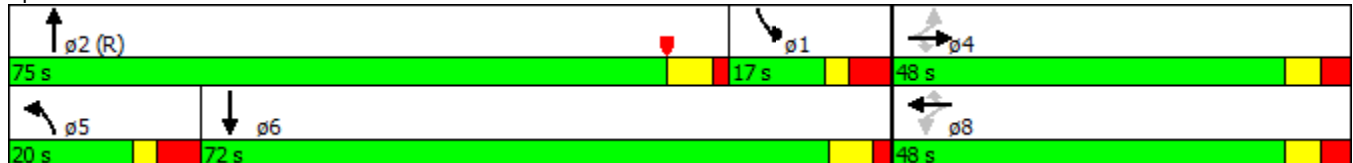


| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | | |
| Volume (vph) | 80 | 60 | 20 | 110 | 30 | 250 | 60 | 2810 | 50 | 890 |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | Prot | NA | Prot | NA |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | 1 | 6 |
| Permitted Phases | 4 | | 4 | 8 | | 8 | | | | |
| Detector Phase | 4 | 4 | 4 | 8 | 8 | 8 | 5 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 4.0 | 5.0 | 4.0 | 5.0 |
| Minimum Split (s) | 48.0 | 48.0 | 48.0 | 19.0 | 19.0 | 19.0 | 11.0 | 31.4 | 11.0 | 11.6 |
| Total Split (s) | 48.0 | 48.0 | 48.0 | 48.0 | 48.0 | 48.0 | 20.0 | 75.0 | 17.0 | 72.0 |
| Total Split (%) | 34.3% | 34.3% | 34.3% | 34.3% | 34.3% | 34.3% | 14.3% | 53.6% | 12.1% | 51.4% |
| Yellow Time (s) | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 2.5 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 3.4 | 3.4 | 3.4 | 3.4 | 3.4 | 3.4 | 4.5 | 1.7 | 4.5 | 1.9 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.4 | 7.0 | 6.6 |
| Lead/Lag | | | | | | | Lead | Lead | Lag | Lag |
| Lead-Lag Optimize? | | | | | | | Yes | Yes | Yes | Yes |
| Recall Mode | Max | Max | Max | None | None | None | None | C-Max | Max | None |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 0 (0%), Referenced to phase 2:NBT, Start of Yellow, Master Intersection
 Natural Cycle: 105
 Control Type: Actuated-Coordinated

Splits and Phases: 5: Mathilda Ave & Ross Dr



Lanes, Volumes, Timings
 6: Mathilda Ave & US 101 NB Ramps

3/4/2016



| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↖↖ | ↖↖ | ↑↑↑ | ↖ | ↖ | ↑↑↑ |
| Volume (vph) | 720 | 700 | 2270 | 360 | 10 | 1010 |
| Turn Type | Prot | pm+ov | NA | Perm | Prot | NA |
| Protected Phases | 8 | 1 | 2 | | 1 | 6 |
| Permitted Phases | | 8 | | 2 | | |
| Detector Phase | 8 | 1 | 2 | 2 | 1 | 6 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 8.0 | 4.0 | 8.0 | 8.0 | 4.0 | 4.0 |
| Minimum Split (s) | 14.9 | 9.7 | 39.9 | 39.9 | 9.7 | 10.9 |
| Total Split (s) | 44.0 | 16.0 | 80.0 | 80.0 | 16.0 | 96.0 |
| Total Split (%) | 31.4% | 11.4% | 57.1% | 57.1% | 11.4% | 68.6% |
| Yellow Time (s) | 4.7 | 3.5 | 4.7 | 4.7 | 3.5 | 4.7 |
| All-Red Time (s) | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.9 | 5.7 | 6.9 | 6.9 | 5.7 | 6.9 |
| Lead/Lag | | Lead | Lag | Lag | Lead | |
| Lead-Lag Optimize? | | Yes | Yes | Yes | Yes | |
| Recall Mode | None | None | C-Max | C-Max | None | None |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 118 (84%), Referenced to phase 2:NBT, Start of Yellow
 Natural Cycle: 90
 Control Type: Actuated-Coordinated

Splits and Phases: 6: Mathilda Ave & US 101 NB Ramps



Lanes, Volumes, Timings
 7: Mathilda Ave & US 101 SB Ramps

3/4/2016



| Lane Group | EBL | EBR | NBT | NBR | SBT |
|----------------------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | |
| Volume (vph) | 280 | 410 | 2350 | 580 | 1590 |
| Turn Type | Prot | Prot | NA | Perm | NA |
| Protected Phases | 7 | 7 | 2 | | 6 |
| Permitted Phases | | | | 2 | |
| Detector Phase | 7 | 7 | 2 | 2 | 6 |
| Switch Phase | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 8.0 | 8.0 | 8.0 |
| Minimum Split (s) | 10.9 | 10.9 | 14.9 | 14.9 | 14.9 |
| Total Split (s) | 40.0 | 40.0 | 100.0 | 100.0 | 100.0 |
| Total Split (%) | 28.6% | 28.6% | 71.4% | 71.4% | 71.4% |
| Yellow Time (s) | 4.7 | 4.7 | 4.7 | 4.7 | 4.7 |
| All-Red Time (s) | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.9 | 6.9 | 6.9 | 6.9 | 6.9 |
| Lead/Lag | | | | | |
| Lead-Lag Optimize? | | | | | |
| Recall Mode | None | None | C-Max | C-Max | None |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 117 (84%), Referenced to phase 2:NBT, Start of Yellow
 Natural Cycle: 60
 Control Type: Actuated-Coordinated

Splits and Phases: 7: Mathilda Ave & US 101 SB Ramps



Lanes, Volumes, Timings
 8: Mathilda Ave & Almanor Ave/Ahwanee Ave

3/4/2016

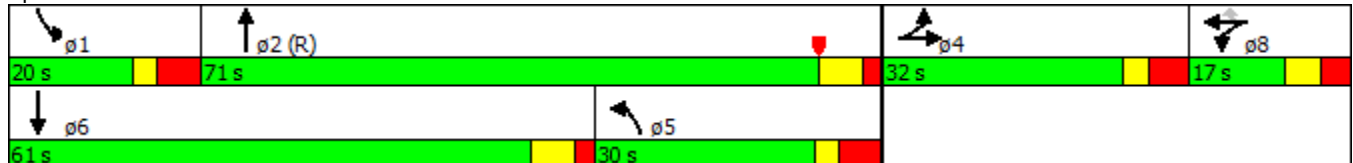


| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | |
| Volume (vph) | 90 | 20 | 70 | 30 | 190 | 110 | 2650 | 160 | 1540 |
| Turn Type | Split | NA | Split | NA | Perm | Prot | NA | Prot | NA |
| Protected Phases | 4 | 4 | 8 | 8 | | 5 | 2 | 1 | 6 |
| Permitted Phases | | | | | 8 | | | | |
| Detector Phase | 4 | 4 | 8 | 8 | 8 | 5 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | | |
| Minimum Initial (s) | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 12.0 | 8.0 | 12.0 |
| Minimum Split (s) | 32.0 | 32.0 | 15.0 | 15.0 | 15.0 | 15.0 | 36.7 | 15.0 | 27.7 |
| Total Split (s) | 32.0 | 32.0 | 17.0 | 17.0 | 17.0 | 30.0 | 71.0 | 20.0 | 61.0 |
| Total Split (%) | 22.9% | 22.9% | 12.1% | 12.1% | 12.1% | 21.4% | 50.7% | 14.3% | 43.6% |
| Yellow Time (s) | 2.8 | 2.8 | 3.6 | 3.6 | 3.6 | 2.5 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 4.2 | 4.2 | 3.4 | 3.4 | 3.4 | 4.5 | 2.0 | 4.5 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.7 | 7.0 | 6.7 |
| Lead/Lag | | | | | | Lag | Lag | Lead | Lead |
| Lead-Lag Optimize? | | | | | | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | None | C-Max | None | None |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 103 (74%), Referenced to phase 2:NBT, Start of Yellow
 Natural Cycle: 120
 Control Type: Actuated-Coordinated

Splits and Phases: 8: Mathilda Ave & Almanor Ave/Ahwanee Ave



Lanes, Volumes, Timings
 9: US 101 On-Ramp & Moffett Park Dr

3/4/2016

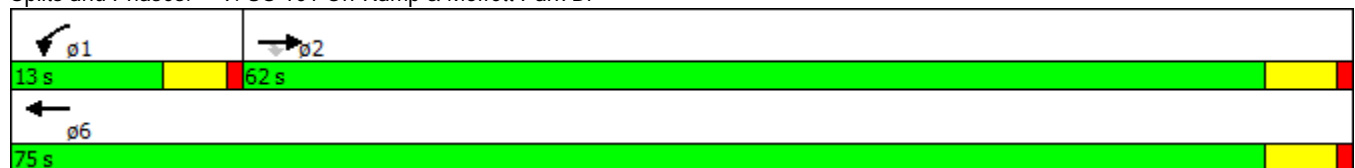


| Lane Group | EBT | EBR | WBL | WBT |
|----------------------|-------|-------|-------|--------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ |
| Volume (vph) | 180 | 10 | 20 | 880 |
| Turn Type | NA | Perm | Prot | NA |
| Protected Phases | 2 | | 1 | 6 |
| Permitted Phases | | 2 | | |
| Detector Phase | 2 | 2 | 1 | 6 |
| Switch Phase | | | | |
| Minimum Initial (s) | 15.0 | 15.0 | 6.0 | 15.0 |
| Minimum Split (s) | 20.0 | 20.0 | 10.5 | 20.0 |
| Total Split (s) | 62.0 | 62.0 | 13.0 | 75.0 |
| Total Split (%) | 82.7% | 82.7% | 17.3% | 100.0% |
| Yellow Time (s) | 4.0 | 4.0 | 3.5 | 4.0 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.0 | 5.0 | 4.5 | 5.0 |
| Lead/Lag | Lag | Lag | Lead | |
| Lead-Lag Optimize? | | | | |
| Recall Mode | Min | Min | None | Min |

Intersection Summary

Cycle Length: 75
 Actuated Cycle Length: 39.7
 Natural Cycle: 40
 Control Type: Semi Act-Uncoord

Splits and Phases: 9: US 101 On-Ramp & Moffett Park Dr



Lanes, Volumes, Timings
 10: Moffett Park Dr & Innovation Way

3/4/2016

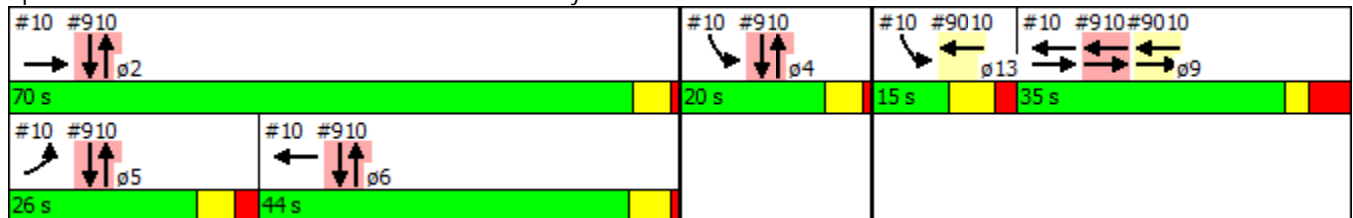


| Lane Group | EBL | EBT | WBT | SBL | ø2 | ø4 | ø6 | ø9 | ø13 |
|----------------------|-------|-----|-----|------|------|------|------|------|------|
| Lane Configurations | ↖ | ↑↑ | ↑↑↔ | ↘↘ | | | | | |
| Volume (vph) | 110 | 70 | 790 | 40 | | | | | |
| Turn Type | Prot | NA | NA | Prot | | | | | |
| Protected Phases | 5 | 2 9 | 6 9 | 4 13 | 2 | 4 | 6 | 9 | 13 |
| Permitted Phases | | | | | | | | | |
| Detector Phase | 5 | 2 | 6 | 4 | | | | | |
| Switch Phase | | | | | | | | | |
| Minimum Initial (s) | 8.0 | | | | 10.0 | 10.0 | 10.0 | 28.0 | 8.0 |
| Minimum Split (s) | 14.5 | | | | 14.9 | 15.0 | 27.5 | 35.0 | 15.0 |
| Total Split (s) | 26.0 | | | | 70.0 | 20.0 | 44.0 | 35.0 | 15.0 |
| Total Split (%) | 18.6% | | | | 50% | 14% | 31% | 25% | 11% |
| Yellow Time (s) | 4.0 | | | | 3.9 | 4.0 | 4.5 | 2.5 | 4.7 |
| All-Red Time (s) | 2.5 | | | | 1.0 | 1.0 | 1.0 | 4.5 | 2.3 |
| Lost Time Adjust (s) | 0.0 | | | | | | | | |
| Total Lost Time (s) | 6.5 | | | | | | | | |
| Lead/Lag | Lead | | | | | | Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | | | | | | Yes | Yes | Yes |
| Recall Mode | None | | | | Min | None | Min | None | None |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 79.8
 Natural Cycle: 110
 Control Type: Actuated-Uncoordinated

Splits and Phases: 10: Moffett Park Dr & Innovation Way



Lanes, Volumes, Timings
 11: Innovation Way & 11th Ave

3/4/2016



| Lane Group | EBL | EBT | EBR | NBL | NBT | SBL | SBT |
|---------------------|-----|------|-----|-----|------|-----|------|
| Lane Configurations | | | | | | | |
| Volume (vph) | 20 | 0 | 60 | 230 | 130 | 60 | 80 |
| Sign Control | | Stop | | | Stop | | Stop |

Intersection Summary

Control Type: Unsignalized

Lanes, Volumes, Timings
 12: Innovation Way & Juniper Driveway

3/4/2016

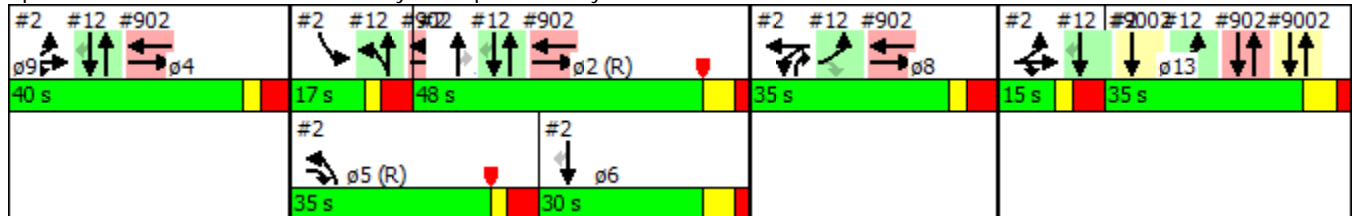


| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR | ø2 | ø4 | ø5 | ø6 | ø8 | ø9 |
|----------------------|------|------|------|-------|--------|--------|-------|------|-------|------|------|------|
| Lane Configurations | ↖ | ↗ | ↖ | ↑↑ | ↑ | ↗ | | | | | | |
| Volume (vph) | 40 | 10 | 60 | 90 | 390 | 370 | | | | | | |
| Turn Type | Prot | Perm | Prot | NA | NA | Perm | | | | | | |
| Protected Phases | 8 9 | | 1 | 1 2 4 | 2 4 13 | | 2 | 4 | 5 | 6 | 8 | 9 |
| Permitted Phases | | 8 9 | | | | 2 4 13 | | | | | | |
| Detector Phase | 8 | 8 | 1 | 1 2 4 | 2 4 | 2 4 | | | | | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 10.0 | | | | 12.0 | 14.0 | 13.0 | 12.0 | 10.0 | 28.0 |
| Minimum Split (s) | | | 16.8 | | | | 19.0 | 39.0 | 20.0 | 30.0 | 35.0 | 35.0 |
| Total Split (s) | | | 17.0 | | | | 48.0 | 40.0 | 35.0 | 30.0 | 35.0 | 35.0 |
| Total Split (%) | | | 8.9% | | | | 25% | 21% | 18% | 16% | 18% | 18% |
| Yellow Time (s) | | | 2.5 | | | | 4.7 | 2.5 | 2.5 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | | | 4.3 | | | | 2.3 | 4.5 | 4.5 | 2.3 | 4.5 | 2.3 |
| Lost Time Adjust (s) | | | 0.0 | | | | | | | | | |
| Total Lost Time (s) | | | 6.8 | | | | | | | | | |
| Lead/Lag | | | Lead | | | | Lag | Lead | Lag | Lag | Lag | Lag |
| Lead-Lag Optimize? | | | Yes | | | | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | | | None | | | | C-Max | None | C-Max | Min | None | None |

Intersection Summary

Cycle Length: 190
 Actuated Cycle Length: 190
 Offset: 133 (70%), Referenced to phase 2:NBT and 5:NBL, Start of Yellow
 Natural Cycle: 175
 Control Type: Actuated-Coordinated

Splits and Phases: 12: Innovation Way & Juniper Driveway



| | |
|----------------------|------|
| Lane Group | ø13 |
| Lane Configurations | |
| Volume (vph) | |
| Turn Type | |
| Protected Phases | 13 |
| Permitted Phases | |
| Detector Phase | |
| Switch Phase | |
| Minimum Initial (s) | 8.0 |
| Minimum Split (s) | 15.0 |
| Total Split (s) | 15.0 |
| Total Split (%) | 8% |
| Yellow Time (s) | 2.5 |
| All-Red Time (s) | 4.5 |
| Lost Time Adjust (s) | |
| Total Lost Time (s) | |
| Lead/Lag | Lead |
| Lead-Lag Optimize? | Yes |
| Recall Mode | None |
| Intersection Summary | |

Lanes, Volumes, Timings
 13: Bordeaux Dr & Innovation Way

3/4/2016

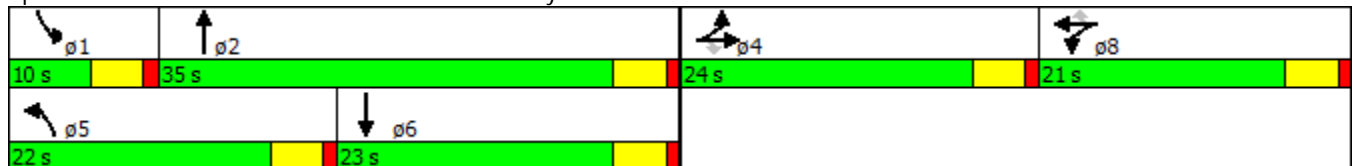


| Lane Group | EBT | EBR | NBL | NBT | SBT | ø1 | ø8 |
|----------------------|-------|-------|-------|-------|-------|------|------|
| Lane Configurations | ↖ | ↗ | ↖ | ↗ | ↗ | | |
| Volume (vph) | 0 | 540 | 250 | 110 | 50 | | |
| Turn Type | NA | Perm | Prot | NA | NA | | |
| Protected Phases | 4 | | 5 | 2 | 6 | 1 | 8 |
| Permitted Phases | | 4 | | | | | |
| Detector Phase | 4 | 4 | 5 | 2 | 6 | | |
| Switch Phase | | | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | 20.5 | 20.5 | 8.5 | 20.5 | 20.5 | 8.5 | 20.5 |
| Total Split (s) | 24.0 | 24.0 | 22.0 | 35.0 | 23.0 | 10.0 | 21.0 |
| Total Split (%) | 26.7% | 26.7% | 24.4% | 38.9% | 25.6% | 11% | 23% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | |
| Total Lost Time (s) | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | | |
| Lead/Lag | | | Lead | Lag | Lag | Lead | |
| Lead-Lag Optimize? | | | Yes | Yes | Yes | Yes | |
| Recall Mode | None | None | None | Min | Min | None | None |

Intersection Summary

Cycle Length: 90
 Actuated Cycle Length: 49.7
 Natural Cycle: 80
 Control Type: Actuated-Uncoordinated

Splits and Phases: 13: Bordeaux Dr & Innovation Way



**SimTraffic Post-Processor
Average Results from 10 Runs
Network Performance**

**Mathilda Avenue Improvements
Build 1 Year 2018
AM Peak Hour**

| Performance Measure | Average | Std. Dev. | Minimum | Maximum |
|---------------------------------|---------|-----------|---------|---------|
| Average Delay (seconds) | 168.7 | 9.2 | 159.1 | 188.7 |
| Total Delay (hours) | 493 | 26 | 461 | 542 |
| Average Stopped Delay (seconds) | 92.5 | 6.5 | 86.0 | 108.2 |
| Total Stopped Delay (hours) | 270 | 18 | 250 | 311 |
| Total Stops | 27,909 | 1,228 | 26,348 | 30,219 |
| Average Stops | 2.65 | 0.12 | 2.52 | 2.92 |
| Total Distance Traveled (miles) | 44,272 | 554 | 43,149 | 44,968 |
| Average Speed (mph) | 28.2 | 0.6 | 27.0 | 29.0 |
| Total Travel Time (hours) | 1,573.9 | 22.9 | 1,538.4 | 1,596.4 |
| Vehicles Entered | 8,974 | 88 | 8,847 | 9,114 |
| Vehicles Exited | 8,909 | 94 | 8,716 | 9,024 |
| Percent Demand Served | 99.3% | 0.8% | 97.9% | 100.4% |
| Fuel Used (gallons) | 1,237 | 12 | 1,219 | 1,253 |
| HC Emissions (grams) | 18,762 | 1,059 | 16,996 | 20,383 |
| CO Emissions (grams) | 533,677 | 19,496 | 502,096 | 561,324 |
| NOx Emissions (grams) | 73,035 | 2,795 | 67,784 | 77,047 |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Build 1 Year 2018
AM Peak Hour

| Intersection 1 | | Mathilda Avenue/5th Avenue | | | Signal | | |
|----------------|------------|----------------------------|---------------------|---------|-----------------------|-----------|-----|
| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | 80 | 75 | 93.4% | 37.6 | 4.5 | D |
| | Through | 870 | 842 | 96.7% | 13.4 | 1.9 | B |
| | Right Turn | 70 | 69 | 98.0% | 11.3 | 2.0 | B |
| | Subtotal | 1,020 | 985 | 96.6% | 15.1 | 1.8 | B |
| SB | Left Turn | 10 | 10 | 98.0% | 52.7 | 6.5 | D |
| | Through | 370 | 371 | 100.3% | 20.7 | 1.8 | C |
| | Right Turn | 70 | 67 | 95.9% | 9.0 | 0.5 | A |
| | Subtotal | 450 | 448 | 99.5% | 19.6 | 1.5 | B |
| EB | Left Turn | 20 | 20 | 100.0% | 30.6 | 5.4 | C |
| | Through | 10 | 8 | 83.0% | 33.6 | 8.7 | C |
| | Right Turn | 30 | 30 | 99.3% | 7.1 | 2.8 | A |
| | Subtotal | 60 | 58 | 96.8% | 19.0 | 3.6 | B |
| WB | Left Turn | 30 | 31 | 101.7% | 37.9 | 6.7 | D |
| | Through | 10 | 10 | 102.0% | 35.4 | 9.9 | D |
| | Right Turn | 10 | 10 | 95.0% | 8.9 | 3.9 | A |
| | Subtotal | 50 | 50 | 100.4% | 31.9 | 5.4 | C |
| Total | | 1,580 | 1,541 | 97.5% | 17.1 | 1.6 | B |

| Intersection 2 | | Mathilda Avenue/Innovation Way-Driveway | | | Signal | | |
|----------------|------------|---|---------------------|---------|-----------------------|-----------|-----|
| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | 520 | 520 | 100.0% | 51.7 | 3.6 | D |
| | Through | 970 | 943 | 97.2% | 32.4 | 3.1 | C |
| | Right Turn | 880 | 867 | 98.5% | 31.8 | 4.4 | C |
| | Subtotal | 2,370 | 2,330 | 98.3% | 36.5 | 2.5 | D |
| SB | Left Turn | 20 | 18 | 89.5% | 99.0 | 15.1 | F |
| | Through | 280 | 281 | 100.3% | 57.6 | 3.2 | E |
| | Right Turn | 130 | 127 | 97.7% | 20.9 | 3.7 | C |
| | Subtotal | 430 | 426 | 99.0% | 48.4 | 2.9 | D |
| EB | Left Turn | 20 | 18 | 88.0% | 57.3 | 17.1 | E |
| | Through | 60 | 63 | 105.3% | 53.3 | 4.7 | D |
| | Right Turn | 50 | 53 | 105.2% | 40.6 | 5.5 | D |
| | Subtotal | 130 | 133 | 102.6% | 48.6 | 5.5 | D |
| WB | Left Turn | 210 | 210 | 100.1% | 85.5 | 8.8 | F |
| | Through | 110 | 109 | 99.4% | 95.6 | 12.1 | F |
| | Right Turn | 30 | 30 | 101.0% | 78.0 | 12.9 | E |
| | Subtotal | 350 | 350 | 99.9% | 88.0 | 9.8 | F |
| Total | | 3,280 | 3,238 | 98.7% | 44.1 | 2.1 | D |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Build 1 Year 2018
AM Peak Hour

Intersection 3 Mathilda Avenue/Moffett Park Drive-SR 237 WB Off-Ramp Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | 850 | 823 | 96.9% | 55.0 | 5.8 | D |
| | Through | 2,120 | 2,046 | 96.5% | 36.1 | 2.8 | D |
| | Right Turn | | | | | | |
| | Subtotal | 2,970 | 2,869 | 96.6% | 41.5 | 3.6 | D |
| SB | Left Turn | | | | | | |
| | Through | 320 | 324 | 101.3% | 62.7 | 3.3 | E |
| | Right Turn | 220 | 218 | 99.2% | 70.0 | 12.8 | E |
| | Subtotal | 540 | 543 | 100.5% | 65.7 | 6.5 | E |
| EB | Left Turn | 40 | 41 | 102.8% | 52.2 | 6.0 | D |
| | Through | | | | | | |
| | Right Turn | 70 | 74 | 105.7% | 5.1 | 1.4 | A |
| | Subtotal | 110 | 115 | 104.6% | 21.9 | 3.4 | C |
| WB | Left Turn | 670 | 663 | 98.9% | 81.8 | 3.3 | F |
| | Through | 200 | 207 | 103.5% | 81.6 | 4.4 | F |
| | Right Turn | 210 | 220 | 104.5% | 75.0 | 3.1 | E |
| | Subtotal | 1,080 | 1,089 | 100.9% | 80.4 | 3.2 | F |
| Total | | 4,700 | 4,616 | 98.2% | 53.1 | 2.9 | D |

Intersection 4 Mathilda Avenue/SR 237 EB Ramps Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | | | | | | |
| | Through | 2,380 | 2,318 | 97.4% | 15.6 | 1.9 | B |
| | Right Turn | 760 | 751 | 98.8% | 2.6 | 0.1 | A |
| | Subtotal | 3,140 | 3,069 | 97.7% | 12.4 | 1.5 | B |
| SB | Left Turn | 50 | 46 | 92.6% | 94.5 | 6.8 | F |
| | Through | 910 | 871 | 95.7% | 40.8 | 2.2 | D |
| | Right Turn | | | | | | |
| | Subtotal | 960 | 917 | 95.6% | 43.5 | 2.0 | D |
| EB | Left Turn | 590 | 574 | 97.3% | 91.8 | 26.8 | F |
| | Through | | | | | | |
| | Right Turn | 60 | 58 | 96.7% | 31.9 | 13.8 | C |
| | Subtotal | 650 | 632 | 97.2% | 86.4 | 25.9 | F |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 4,750 | 4,618 | 97.2% | 28.7 | 4.1 | C |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Build 1 Year 2018
AM Peak Hour

Intersection 5 Mathilda Avenue/Ross Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | 60 | 59 | 99.0% | 87.2 | 5.9 | F |
| | Through | 2,810 | 2,733 | 97.3% | 28.5 | 3.2 | C |
| | Right Turn | 100 | 100 | 99.6% | 33.6 | 9.9 | C |
| | Subtotal | 2,970 | 2,892 | 97.4% | 29.9 | 3.4 | C |
| SB | Left Turn | 50 | 49 | 98.2% | 59.5 | 2.5 | E |
| | Through | 890 | 867 | 97.5% | 22.8 | 4.7 | C |
| | Right Turn | 30 | 30 | 98.3% | 11.0 | 3.6 | B |
| | Subtotal | 970 | 946 | 97.5% | 24.3 | 4.3 | C |
| EB | Left Turn | 80 | 81 | 101.3% | 53.0 | 5.0 | D |
| | Through | 60 | 62 | 103.3% | 47.1 | 6.2 | D |
| | Right Turn | 20 | 18 | 87.5% | 17.4 | 1.8 | B |
| | Subtotal | 160 | 161 | 100.3% | 46.9 | 4.2 | D |
| WB | Left Turn | 110 | 107 | 96.9% | 64.9 | 4.7 | E |
| | Through | 30 | 29 | 96.0% | 60.1 | 8.5 | E |
| | Right Turn | 250 | 253 | 101.2% | 50.8 | 3.1 | D |
| | Subtotal | 390 | 389 | 99.6% | 55.2 | 2.2 | E |
| Total | | 4,490 | 4,387 | 97.7% | 31.6 | 2.4 | C |

Intersection 6 Mathilda Avenue/US 101 NB Ramps Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | | | | | | |
| | Through | 2,270 | 2,201 | 97.0% | 25.0 | 2.9 | C |
| | Right Turn | 360 | 357 | 99.2% | 6.4 | 0.5 | A |
| | Subtotal | 2,630 | 2,558 | 97.3% | 22.4 | 2.7 | C |
| SB | Left Turn | 10 | 7 | 68.0% | 53.5 | 21.8 | D |
| | Through | 1,010 | 992 | 98.2% | 23.0 | 2.6 | C |
| | Right Turn | | | | | | |
| | Subtotal | 1,020 | 999 | 97.9% | 23.2 | 2.6 | C |
| EB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| WB | Left Turn | 720 | 719 | 99.9% | 116.0 | 32.9 | F |
| | Through | | | | | | |
| | Right Turn | 700 | 705 | 100.6% | 100.6 | 32.7 | F |
| | Subtotal | 1,420 | 1,424 | 100.3% | 108.3 | 32.7 | F |
| Total | | 5,070 | 4,981 | 98.2% | 47.2 | 9.7 | D |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Build 1 Year 2018
AM Peak Hour

Intersection 7 Mathilda Avenue/US 101 SB Ramps Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | | | | | | |
| | Through | 2,350 | 2,280 | 97.0% | 19.2 | 1.2 | B |
| | Right Turn | 580 | 566 | 97.6% | 15.4 | 0.5 | B |
| | Subtotal | 2,930 | 2,846 | 97.1% | 18.4 | 1.0 | B |
| SB | Left Turn | | | | | | |
| | Through | 1,590 | 1,575 | 99.1% | 12.9 | 3.6 | B |
| | Right Turn | 140 | 133 | 95.0% | 12.0 | 3.3 | B |
| | Subtotal | 1,730 | 1,708 | 98.7% | 12.8 | 3.5 | B |
| EB | Left Turn | 280 | 284 | 101.3% | 80.3 | 12.5 | F |
| | Through | | | | | | |
| | Right Turn | 410 | 397 | 96.8% | 28.0 | 4.1 | C |
| | Subtotal | 690 | 681 | 98.6% | 49.7 | 6.8 | D |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 5,350 | 5,234 | 97.8% | 20.7 | 1.9 | C |

Intersection 8 Mathilda Avenue/Almanor Avenue-Ahwanee Avenue Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | 110 | 102 | 92.3% | 108.7 | 33.5 | F |
| | Through | 2,650 | 2,564 | 96.8% | 111.7 | 31.2 | F |
| | Right Turn | 50 | 50 | 99.8% | 107.6 | 29.4 | F |
| | Subtotal | 2,810 | 2,716 | 96.6% | 111.5 | 31.2 | F |
| SB | Left Turn | 160 | 154 | 96.1% | 202.9 | 92.5 | F |
| | Through | 1,540 | 1,515 | 98.4% | 38.9 | 8.2 | D |
| | Right Turn | 300 | 295 | 98.4% | 41.9 | 8.8 | D |
| | Subtotal | 2,000 | 1,964 | 98.2% | 52.5 | 13.9 | D |
| EB | Left Turn | 90 | 90 | 100.3% | 68.2 | 7.0 | E |
| | Through | 20 | 19 | 94.0% | 69.7 | 8.9 | E |
| | Right Turn | 30 | 31 | 104.7% | 32.9 | 5.2 | C |
| | Subtotal | 140 | 141 | 100.4% | 60.6 | 6.1 | E |
| WB | Left Turn | 70 | 71 | 100.7% | 62.5 | 5.6 | E |
| | Through | 30 | 31 | 102.3% | 60.2 | 7.5 | E |
| | Right Turn | 190 | 191 | 100.7% | 21.8 | 1.6 | C |
| | Subtotal | 290 | 293 | 100.9% | 35.8 | 2.4 | D |
| Total | | 5,240 | 5,113 | 97.6% | 83.1 | 19.9 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Build 1 Year 2018
AM Peak Hour

Intersection 9 US 101 NB Slip Ramp/Moffett Park Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| EB | Left Turn | | | | | | |
| | Through | 180 | 178 | 98.6% | 1.8 | 0.2 | A |
| | Right Turn | 10 | 10 | 95.0% | 1.2 | 0.5 | A |
| | Subtotal | 190 | 187 | 98.4% | 1.7 | 0.2 | A |
| WB | Left Turn | 20 | 21 | 106.0% | 9.6 | 1.2 | A |
| | Through | 880 | 869 | 98.7% | 6.5 | 0.6 | A |
| | Right Turn | | | | | | |
| | Subtotal | 900 | 890 | 98.9% | 6.6 | 0.6 | A |
| Total | | 1,090 | 1,077 | 98.8% | 5.7 | 0.6 | A |

Intersection 10 Innovation Way/Moffett Park Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | 40 | 42 | 105.3% | 33.5 | 4.1 | C |
| | Through | | | | | | |
| | Right Turn | 110 | 107 | 97.1% | 29.0 | 2.4 | C |
| | Subtotal | 150 | 149 | 99.3% | 30.2 | 2.6 | C |
| EB | Left Turn | 110 | 105 | 95.1% | 34.0 | 1.4 | C |
| | Through | 70 | 74 | 105.9% | 4.3 | 0.7 | A |
| | Right Turn | | | | | | |
| | Subtotal | 180 | 179 | 99.3% | 21.7 | 1.2 | C |
| WB | Left Turn | | | | | | |
| | Through | 790 | 787 | 99.6% | 16.9 | 1.2 | B |
| | Right Turn | 340 | 338 | 99.5% | 18.6 | 1.8 | B |
| | Subtotal | 1,130 | 1,126 | 99.6% | 17.4 | 1.3 | B |
| Total | | 1,460 | 1,453 | 99.5% | 19.2 | 1.1 | B |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Build 1 Year 2018
AM Peak Hour

Intersection 11 Innovation Way/11th Avenue All-way Stop

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 230 | 228 | 99.0% | 11.3 | 1.0 | B |
| | Through | 130 | 130 | 99.8% | 10.5 | 0.6 | B |
| | Right Turn | 90 | 84 | 93.8% | 5.5 | 0.4 | A |
| | Subtotal | 450 | 442 | 98.2% | 10.0 | 0.7 | A |
| SB | Left Turn | 60 | 56 | 93.2% | 6.6 | 0.6 | A |
| | Through | 80 | 79 | 98.5% | 16.0 | 1.8 | C |
| | Right Turn | 260 | 258 | 99.3% | 15.3 | 1.8 | C |
| | Subtotal | 400 | 393 | 98.2% | 14.2 | 1.5 | B |
| EB | Left Turn | 20 | 21 | 105.0% | 10.6 | 2.9 | B |
| | Through | | | | | | |
| | Right Turn | 60 | 61 | 101.3% | 9.5 | 1.8 | A |
| | Subtotal | 80 | 82 | 102.3% | 9.8 | 1.5 | A |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 930 | 917 | 98.5% | 11.8 | 0.9 | B |

Intersection 12 Innovation Way/Juniper Networks Driveway Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 60 | 57 | 94.8% | 101.2 | 15.5 | F |
| | Through | 90 | 93 | 103.0% | 12.6 | 3.0 | B |
| | Right Turn | | | | | | |
| | Subtotal | 150 | 150 | 99.7% | 46.3 | 6.9 | D |
| SB | Left Turn | | | | | | |
| | Through | 390 | 386 | 99.1% | 7.1 | 0.5 | A |
| | Right Turn | 370 | 377 | 101.8% | 5.8 | 0.4 | A |
| | Subtotal | 760 | 763 | 100.4% | 6.4 | 0.3 | A |
| EB | Left Turn | 40 | 39 | 97.5% | 56.5 | 10.6 | E |
| | Through | | | | | | |
| | Right Turn | 10 | 10 | 96.0% | 7.1 | 3.9 | A |
| | Subtotal | 50 | 49 | 97.2% | 46.4 | 9.5 | D |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 960 | 961 | 100.1% | 14.7 | 1.4 | B |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Build 1 Year 2018
AM Peak Hour

| Intersection 13 | | Bordeaux Drive/Innovation Way | | | Signal | | |
|-----------------|------------|-------------------------------|---------------------|---------|-----------------------|-----------|-----|
| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | 250 | 244 | 97.4% | 21.4 | 1.3 | C |
| | Through | 110 | 109 | 99.4% | 10.3 | 0.9 | B |
| | Right Turn | | | | | | |
| | Subtotal | 360 | 353 | 98.0% | 18.0 | 0.9 | B |
| SB | Left Turn | | | | | | |
| | Through | 50 | 50 | 99.8% | 20.6 | 1.9 | C |
| | Right Turn | 90 | 95 | 105.9% | 10.1 | 1.3 | B |
| | Subtotal | 140 | 145 | 103.7% | 13.8 | 1.7 | B |
| EB | Left Turn | 270 | 272 | 100.7% | 14.2 | 1.2 | B |
| | Through | | | | | | |
| | Right Turn | 540 | 528 | 97.8% | 8.2 | 0.9 | A |
| | Subtotal | 810 | 800 | 98.7% | 10.2 | 0.8 | B |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 1,310 | 1,298 | 99.1% | 12.7 | 0.8 | B |

Intersection 1

Mathilda Avenue/5th Avenue

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 625 | 25 | 3 | 50 | 6 | 50 | 7 | 0% | 0% |
| | Through | 625 | 25 | 3 | 25 | 6 | 50 | 4 | 0% | 0% |
| | Right Turn | 625 | 25 | 3 | 25 | 9 | 50 | 20 | 0% | 0% |
| NB | Left Turn | 425 | 50 | 5 | 100 | 10 | 125 | 20 | 0% | 0% |
| | Through | 1,125 | 100 | 15 | 200 | 30 | 275 | 36 | 0% | 0% |
| | Through/Right | 1,125 | 100 | 18 | 250 | 37 | 300 | 40 | 0% | 0% |
| SB | Left Turn | 250 | 25 | 3 | 50 | 5 | 50 | 10 | 0% | 0% |
| | Through | 1,325 | 75 | 7 | 125 | 11 | 150 | 24 | 0% | 0% |
| | Right Turn | 250 | 25 | 2 | 25 | 11 | 50 | 29 | 0% | 0% |
| WB | Left Turn | 925 | 50 | 5 | 75 | 9 | 100 | 16 | 5% | 0% |
| | Through/Right | 75 | 25 | 4 | 75 | 9 | 75 | 10 | 2% | 0% |

Intersection 2

Mathilda Avenue/Innovation Way-Driveway

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|--------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left/Through | 225 | 125 | 10 | 150 | 18 | 175 | 27 | 0% | 0% |
| | Right Turn | 225 | 25 | 2 | 25 | 7 | 50 | 21 | 0% | 2% |
| NB | Left Turn | 725 | 200 | 26 | 325 | 49 | 375 | 58 | 0% | 0% |
| | Through | 975 | 275 | 45 | 525 | 129 | 725 | 281 | 0% | 0% |
| | Right Turn | 975 | 325 | 61 | 650 | 122 | 800 | 182 | 0% | 0% |
| SB | Left Turn | 75 | 25 | 5 | 75 | 11 | 125 | 33 | 1% | 0% |
| | Through | 975 | 100 | 8 | 150 | 16 | 200 | 38 | 16% | 0% |
| | Right Turn | 225 | 75 | 5 | 125 | 15 | 150 | 45 | 0% | 0% |
| WB | Left Turn | 425 | 300 | 31 | 500 | 54 | 600 | 48 | 15% | 0% |
| | Shared | 225 | 200 | 12 | 275 | 11 | 250 | 0 | 11% | 0% |

Intersection 3

Mathilda Avenue/Moffett Park Drive-SR 237 WB Off-Ramp

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|----------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Shared | 1,125 | 50 | 7 | 100 | 19 | 150 | 34 | 0% | 0% |
| | Right Turn | 1,125 | 25 | 3 | 50 | 10 | 75 | 17 | 0% | 0% |
| NB | Left Turn | 350 | 300 | 29 | 425 | 35 | 425 | 34 | 0% | 8% |
| | Through | 350 | 325 | 25 | 450 | 30 | 475 | 32 | 0% | 6% |
| | Right Diagonal | 350 | 175 | 6 | 225 | 9 | 200 | 12 | 0% | 58% |
| SB | Through | 975 | 150 | 24 | 325 | 65 | 450 | 97 | 0% | 0% |
| | Through/Right | 975 | 250 | 36 | 425 | 59 | 525 | 78 | 0% | 0% |
| WB | Left Turn | 525 | 275 | 20 | 375 | 25 | 400 | 46 | 0% | 0% |
| | Left/Through | 1,225 | 300 | 17 | 375 | 25 | 425 | 34 | 0% | 0% |
| | Through/Right | 1,225 | 275 | 14 | 375 | 28 | 425 | 44 | 0% | 0% |

Intersection 4

Mathilda Avenue/SR 237 EB Ramps

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|--------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,025 | 350 | 67 | 550 | 192 | 700 | 233 | 0% | 0% |
| | Left/Through | 1,025 | 250 | 66 | 475 | 207 | 625 | 255 | 5% | 0% |
| | Right Turn | 450 | 25 | 31 | 125 | 154 | 300 | 280 | 0% | 0% |
| NB | Through | 275 | 75 | 17 | 150 | 31 | 200 | 47 | 0% | 0% |
| | Right Turn | 275 | 25 | 8 | 50 | 24 | 50 | 32 | 0% | 0% |
| SB | Left Turn | 325 | 150 | 22 | 275 | 34 | 325 | 32 | 2% | 0% |
| | Through | 350 | 300 | 21 | 375 | 32 | 400 | 38 | 0% | 2% |
| | | | | | | | | | | |

SimTraffic Post-Processor
Average Results from 10 Runs
Queue Length
Intersection 5

Mathilda Avenue Improvements
Build 1 Year 2018
AM Peak Hour
Signal

Mathilda Avenue/Ross Drive

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 250 | 75 | 7 | 125 | 9 | 125 | 0 | 11% | 0% |
| | Through | 1,575 | 75 | 8 | 150 | 17 | 225 | 40 | 34% | 0% |
| | Right Turn | 50 | 25 | 4 | 50 | 13 | 75 | 25 | 2% | 0% |
| NB | Left Turn | 250 | 100 | 23 | 225 | 53 | 300 | 14 | 0% | 0% |
| | Through | 700 | 400 | 85 | 725 | 103 | 725 | 154 | 7% | 2% |
| | Through/Right | 225 | 250 | 11 | 300 | 17 | 275 | 0 | 24% | 0% |
| SB | Left Turn | 225 | 50 | 4 | 125 | 6 | 125 | 13 | 0% | 0% |
| | Through | 225 | 150 | 16 | 275 | 19 | 250 | 15 | 0% | 9% |
| | Through/Right | 225 | 175 | 12 | 300 | 14 | 275 | 5 | 0% | 12% |
| WB | Left Turn | 100 | 75 | 5 | 125 | 4 | 100 | 1 | 13% | 0% |
| | Through | 225 | 175 | 24 | 350 | 40 | 400 | 36 | 1% | 0% |
| | Right Turn | 100 | 100 | 3 | 125 | 5 | 125 | 0 | 34% | 0% |

Intersection 6

Mathilda Avenue/US 101 NB Ramps

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NB | Through | 575 | 375 | 35 | 525 | 61 | 575 | 102 | 0% | 1% |
| | Right Turn | 575 | 50 | 29 | 175 | 148 | 325 | 272 | 0% | 0% |
| SB | Left Turn | 375 | 25 | 4 | 50 | 11 | 50 | 18 | 0% | 0% |
| | Through | 700 | 175 | 30 | 325 | 64 | 425 | 141 | 0% | 0% |
| WB | Left Turn | 1,025 | 250 | 163 | 400 | 258 | 450 | 275 | 0% | 0% |
| | Right Turn | 1,025 | 150 | 7 | 175 | 12 | 175 | 14 | 0% | 51% |
| 0 | | | | | | | | | | |

SimTraffic Post-Processor
Average Results from 10 Runs
Queue Length
Intersection 7

Mathilda Avenue Improvements
Build 1 Year 2018
AM Peak Hour
Signal

Mathilda Avenue/US 101 SB Ramps

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,050 | 150 | 18 | 225 | 38 | 275 | 50 | 4% | 0% |
| | Right Turn | 1,050 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| NB | Through | 750 | 375 | 63 | 775 | 117 | 775 | 247 | 0% | 1% |
| | Right Turn | 750 | 200 | 67 | 700 | 130 | 775 | 24 | 0% | 0% |
| SB | Through | 575 | 125 | 29 | 250 | 60 | 300 | 127 | 0% | 0% |
| | Through/Right | 575 | 150 | 31 | 300 | 60 | 350 | 104 | 0% | 0% |
| | | | | | | | | | | |

Intersection 8

Mathilda Avenue/Almanor Avenue-Ahwanee Avenue

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,025 | 75 | 7 | 125 | 17 | 150 | 35 | 2% | 0% |
| | Through/Right | 125 | 50 | 5 | 100 | 12 | 125 | 24 | 0% | 0% |
| NB | Left Turn | 425 | 175 | 26 | 425 | 39 | 425 | 1 | 0% | 0% |
| | Through | 750 | 900 | 253 | 1,225 | 305 | 1,275 | 290 | 63% | 0% |
| | Through/Right | 750 | 325 | 2 | 325 | 10 | 325 | 0 | 36% | 0% |
| SB | Left Turn | 275 | 250 | 57 | 350 | 38 | 325 | 12 | 34% | 0% |
| | Through | 750 | 275 | 149 | 525 | 219 | 625 | 173 | 7% | 3% |
| | Through/Right | 750 | 275 | 62 | 500 | 112 | 575 | 109 | 0% | 0% |
| WB | Left Turn | 250 | 75 | 8 | 150 | 16 | 150 | 22 | 0% | 0% |
| | Through | 1,025 | 75 | 10 | 175 | 18 | 225 | 39 | 14% | 0% |
| | Right Turn | 75 | 100 | 3 | 125 | 5 | 125 | 0 | 32% | 0% |

US 101 NB Slip Ramp/Moffett Park Drive

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Through | 850 | 25 | 3 | 50 | 12 | 75 | 19 | 0% | 0% |
| | Right Turn | 150 | 25 | 0 | 25 | 5 | 25 | 14 | 0% | 0% |
| WB | Left Turn | 850 | 25 | 2 | 50 | 2 | 50 | 12 | 0% | 0% |
| | Through | 850 | 25 | 9 | 75 | 88 | 225 | 256 | 0% | 0% |
| | | | | | | | | | | |
| | | | | | | | | | | |

Intersection 10

Innovation Way/Moffett Park Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 225 | 75 | 6 | 150 | 11 | 175 | 24 | 0% | 0% |
| | Through | 850 | 25 | 3 | 50 | 8 | 75 | 15 | 0% | 0% |
| SB | Left Turn | 575 | 25 | 3 | 50 | 6 | 75 | 17 | 0% | 0% |
| | Shared | 575 | 125 | 6 | 175 | 10 | 200 | 18 | 0% | 0% |
| WB | Through | 1,150 | 150 | 18 | 275 | 27 | 350 | 38 | 0% | 0% |
| | Through/Right | 1,150 | 200 | 18 | 350 | 30 | 400 | 38 | 0% | 0% |
| | | | | | | | | | | |

SimTraffic Post-Processor
 Average Results from 10 Runs
 Queue Length
 Intersection 11

Mathilda Avenue Improvements
 Build 1 Year 2018
 AM Peak Hour
 All-way Stop

Innovation Way/11th Avenue

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 125 | 25 | 3 | 50 | 4 | 50 | 11 | 0% | 0% |
| | Left/Through | 325 | 25 | 1 | 25 | 5 | 50 | 7 | 0% | 0% |
| | Right Turn | 325 | 50 | 4 | 75 | 7 | 75 | 16 | 0% | 0% |
| NB | Left Turn | 125 | 75 | 4 | 100 | 9 | 150 | 19 | 1% | 0% |
| | Through | 575 | 50 | 6 | 125 | 28 | 150 | 59 | 0% | 0% |
| | Through/Right | 575 | 25 | 2 | 50 | 5 | 75 | 17 | 0% | 0% |
| SB | Left Turn | 175 | 50 | 2 | 75 | 8 | 75 | 17 | 0% | 0% |
| | Through | 1,000 | 25 | 3 | 50 | 11 | 75 | 37 | 0% | 0% |
| | Through/Right | 1,000 | 125 | 10 | 225 | 27 | 250 | 43 | 0% | 0% |
| WB | Left Turn | 325 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | Through/Right | 325 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |

Intersection 12

Innovation Way/Juniper Networks Driveway

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 200 | 50 | 10 | 100 | 18 | 125 | 22 | 0% | 0% |
| | Right Turn | 200 | 25 | 3 | 50 | 6 | 50 | 8 | 0% | 0% |
| NB | Left Turn | 125 | 75 | 8 | 150 | 14 | 150 | 18 | 14% | 0% |
| | Through | 1,000 | 25 | 10 | 100 | 36 | 150 | 65 | 0% | 0% |
| SB | Through | 300 | 75 | 6 | 125 | 17 | 175 | 23 | 0% | 2% |
| | Right Turn | 300 | 100 | 3 | 150 | 8 | 175 | 17 | 0% | 0% |
| | | | | | | | | | | |

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left/Through | 375 | 150 | 16 | 275 | 33 | 325 | 51 | 6% | 0% |
| | Right Turn | 125 | 125 | 7 | 150 | 3 | 150 | 0 | 6% | 0% |
| NB | Left Turn | 325 | 125 | 8 | 175 | 16 | 200 | 29 | 0% | 0% |
| | Through/Right | 2,025 | 50 | 4 | 75 | 9 | 100 | 22 | 0% | 0% |
| SB | Left Turn | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | Through/Right | 725 | 75 | 6 | 125 | 13 | 125 | 27 | 1% | 0% |
| WB | Left/Through | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | Right Turn | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |

Arterial Level of Service: NB Mathilda Ave

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|--------------------|------|---------------|-----------------|------------|----------------|
| Ahwanee Ave | 8 | 68.6 | 79.7 | 0.1 | 6 |
| | 7 | 18.6 | 31.4 | 0.2 | 18 |
| US 101 NB Ramps | 6 | 22.3 | 32.3 | 0.1 | 15 |
| Ross Dr | 5 | 22.6 | 34.3 | 0.1 | 15 |
| SR 237 EB Ramps | 4 | 13.4 | 18.7 | 0.1 | 12 |
| SR 237 WB On-Ramp | 33 | 9.3 | 12.8 | 0.0 | 13 |
| SR 237 WB Off-Ramp | 3 | 25.2 | 28.4 | 0.0 | 5 |
| Innovation Way | 2 | 33.3 | 49.9 | 0.2 | 16 |
| 5th Ave | 1 | 13.6 | 32.8 | 0.2 | 26 |
| | 107 | 4.4 | 26.5 | 0.3 | 37 |
| Total | | 231.3 | 346.7 | 1.4 | 15 |

Arterial Level of Service: SB Mathilda Ave

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|-------------------|------|---------------|-----------------|------------|----------------|
| 5th Ave | 1 | 13.8 | 36.0 | 0.3 | 27 |
| Innovation Way | 2 | 57.0 | 75.5 | 0.2 | 11 |
| Moffett Park Dr | 3 | 64.9 | 82.5 | 0.2 | 9 |
| SR 237 WB On-Ramp | 33 | 9.9 | 13.0 | 0.0 | 10 |
| SR 237 EB Ramps | 4 | 36.0 | 39.9 | 0.0 | 4 |
| Ross Dr | 5 | 22.3 | 27.1 | 0.1 | 9 |
| US 101 NB Ramps | 6 | 25.5 | 37.1 | 0.1 | 14 |
| US 101 SB Ramps | 7 | 13.7 | 24.5 | 0.1 | 20 |
| Almanor Ave | 8 | 35.9 | 48.5 | 0.2 | 11 |
| San Aleso Ave | 201 | 3.8 | 15.2 | 0.1 | 33 |
| Total | | 282.9 | 399.2 | 1.4 | 13 |

Arterial Level of Service: NB Innovation Way

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|------------------|------|---------------|-----------------|------------|----------------|
| | 910 | 2.3 | 6.4 | 0.0 | 13 |
| | 43 | 0.9 | 5.9 | 0.0 | 25 |
| | 11 | 7.6 | 15.1 | 0.1 | 17 |
| | 200 | 2.8 | 19.7 | 0.2 | 29 |
| Juniper Driveway | 12 | 10.0 | 15.8 | 0.1 | 13 |
| Driveway | 217 | 1.5 | 4.7 | 0.0 | 29 |
| | 902 | 28.0 | 30.3 | 0.0 | 2 |
| Mathilda Ave | 2 | 22.6 | 25.1 | 0.0 | 4 |
| | 52 | 2.0 | 15.7 | 0.1 | 21 |
| Bordeaux Dr | 13 | 14.2 | 26.4 | 0.1 | 11 |
| Total | | 92.0 | 165.1 | 0.6 | 13 |

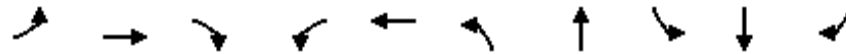
Arterial Level of Service: SB Innovation Way

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|------------------|------|---------------|-----------------|-----------|----------------|
| | 52 | - | - | 0.1 | - |
| Mathilda Ave | 2 | 92.9 | 105.0 | 0.1 | 3 |
| | 902 | 6.0 | 10.9 | 0.0 | 9 |
| Driveway | 217 | 0.5 | 2.7 | 0.0 | 27 |
| Juniper Driveway | 12 | 4.6 | 8.7 | 0.0 | 15 |
| | 200 | 1.4 | 7.9 | 0.1 | 26 |
| 11th Ave | 11 | 14.6 | 30.4 | 0.2 | 19 |
| | 43 | 3.1 | 10.6 | 0.1 | 25 |
| | 910 | 14.6 | 19.0 | 0.0 | 8 |
| Moffett Park Dr | 10 | 16.5 | 20.1 | 0.0 | 4 |
| Total | | 154.2 | 215.5 | 0.6 | 10 |

Lanes, Volumes, Timings

1: Mathilda Ave & 5th Ave

3/4/2016

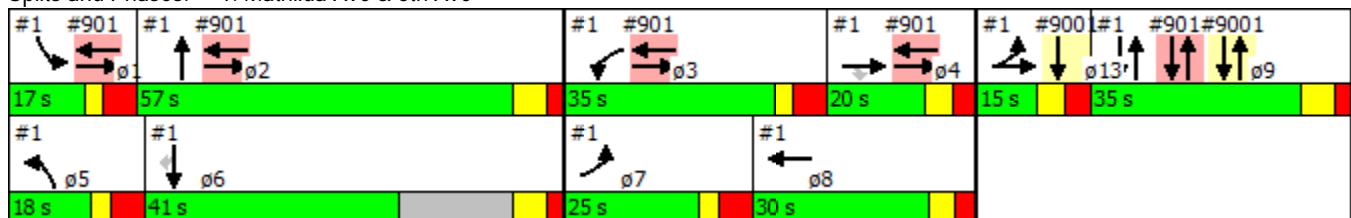


| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT | SBR | ø2 | ø7 |
|----------------------|------|------|--------|-------|-------|-------|-----|------|------|--------|------|------|
| Lane Configurations | ↔↔ | ↑ | ↔ | ↔↔ | ↔ | ↔↔ | ↔↔↔ | ↔ | ↔↔↔ | ↔ | | |
| Volume (vph) | 70 | 20 | 70 | 240 | 10 | 110 | 340 | 10 | 1110 | 10 | | |
| Turn Type | Prot | NA | custom | Prot | NA | Prot | NA | Prot | NA | custom | | |
| Protected Phases | 7 13 | 4 13 | | 3 | 8 | 5 | 2 9 | 1 | 6 9 | | 2 | 7 |
| Permitted Phases | | | 4 | | | | | | | 6 | | |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 5 | 2 | 1 | 6 | 6 | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 13.0 | 12.0 | 8.0 | 11.0 | | 10.0 | | 12.0 | 12.0 | 12.0 |
| Minimum Split (s) | | | 20.0 | 19.0 | 29.5 | 18.0 | | 17.0 | | 41.0 | 35.0 | 19.0 |
| Total Split (s) | | | 20.0 | 35.0 | 30.0 | 18.0 | | 17.0 | | 41.0 | 57.0 | 25.0 |
| Total Split (%) | | | 11.2% | 19.6% | 16.8% | 10.1% | | 9.5% | | 22.9% | 32% | 14% |
| Yellow Time (s) | | | 3.6 | 2.5 | 3.6 | 2.5 | | 2.5 | | 4.7 | 4.7 | 2.5 |
| All-Red Time (s) | | | 3.4 | 4.5 | 2.9 | 4.5 | | 4.5 | | 2.3 | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | | 0.0 | | |
| Total Lost Time (s) | | | 7.0 | 7.0 | 6.5 | 7.0 | | 7.0 | | 7.0 | | |
| Lead/Lag | | | Lag | Lead | Lag | Lead | | Lead | | Lag | Lag | Lead |
| Lead-Lag Optimize? | | | Yes | Yes | Yes | Yes | | Yes | | Yes | Yes | Yes |
| Recall Mode | | | None | None | None | None | | None | | None | Min | None |

Intersection Summary

Cycle Length: 179
 Actuated Cycle Length: 107.1
 Natural Cycle: 160
 Control Type: Actuated-Uncoordinated

Splits and Phases: 1: Mathilda Ave & 5th Ave



| Lane Group | ø9 | ø13 |
|----------------------|------|------|
| Lane Configurations | | |
| Volume (vph) | | |
| Turn Type | | |
| Protected Phases | 9 | 13 |
| Permitted Phases | | |
| Detector Phase | | |
| Switch Phase | | |
| Minimum Initial (s) | 28.0 | 8.0 |
| Minimum Split (s) | 35.0 | 15.0 |
| Total Split (s) | 35.0 | 15.0 |
| Total Split (%) | 20% | 8% |
| Yellow Time (s) | 4.7 | 3.6 |
| All-Red Time (s) | 2.3 | 3.4 |
| Lost Time Adjust (s) | | |
| Total Lost Time (s) | | |
| Lead/Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes |
| Recall Mode | None | None |
| Intersection Summary | | |

Lanes, Volumes, Timings
 2: Mathilda Ave & Innovation Way

3/4/2016

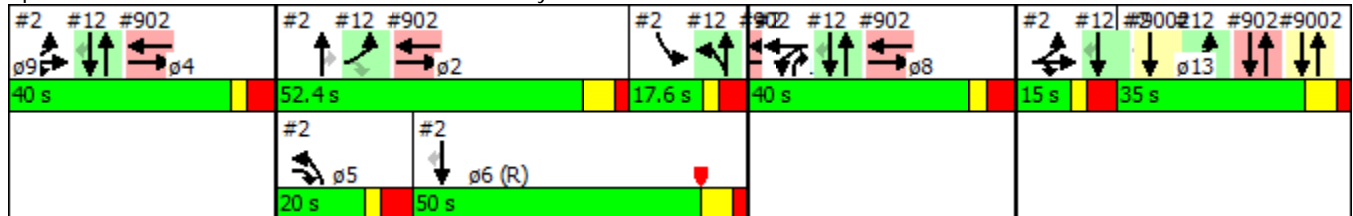


| Lane Group | EBT | EBR | WBL | WBT | NBL | NBT | NBR | SBL | SBT | SBR | ø2 | ø4 |
|----------------------|------|--------|-------|-------|-------|-----|-------|------|-------|------|------|------|
| Lane Configurations | ↖ ↗ | ↖ ↗ | ↖ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ | ↖ | ↖ ↗ ↘ | ↖ | | |
| Volume (vph) | 200 | 680 | 480 | 120 | 10 | 330 | 200 | 50 | 1320 | 50 | | |
| Turn Type | NA | pt+ov | Split | NA | Prot | NA | pm+ov | Prot | NA | Perm | | |
| Protected Phases | 4 13 | 4 13 5 | 8 | 8 | 5 | 2 9 | 8 | 1 | 6 9 | | 2 | 4 |
| Permitted Phases | | | | | | | 2 9 | | | | | 6 9 |
| Detector Phase | 4 | 4 | 8 | 8 | 5 | 2 | 2 | 1 | 6 | 6 | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 10.0 | 10.0 | 13.0 | | 10.0 | 10.0 | | | 12.0 | 14.0 |
| Minimum Split (s) | | | 35.0 | 35.0 | 20.0 | | 35.0 | 16.8 | | | 19.0 | 39.0 |
| Total Split (s) | | | 40.0 | 40.0 | 20.0 | | 40.0 | 17.6 | | | 52.4 | 40.0 |
| Total Split (%) | | | 20.0% | 20.0% | 10.0% | | 20.0% | 8.8% | | | 26% | 20% |
| Yellow Time (s) | | | 2.5 | 2.5 | 2.5 | | 2.5 | 2.5 | | | 4.7 | 2.5 |
| All-Red Time (s) | | | 4.5 | 4.5 | 4.5 | | 4.5 | 4.3 | | | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | | | | |
| Total Lost Time (s) | | | 7.0 | 7.0 | 7.0 | | 7.0 | 6.8 | | | | |
| Lead/Lag | | | | | Lead | | | Lag | | | Lead | |
| Lead-Lag Optimize? | | | | | Yes | | | Yes | | | Yes | |
| Recall Mode | | | None | None | None | | None | None | | | Max | None |

Intersection Summary

Cycle Length: 200
 Actuated Cycle Length: 200
 Offset: 0 (0%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 175
 Control Type: Actuated-Coordinated

Splits and Phases: 2: Mathilda Ave & Innovation Way



Lanes, Volumes, Timings
 2: Mathilda Ave & Innovation Way

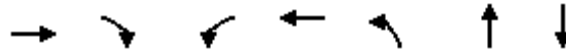
3/4/2016

| Lane Group | ø6 | ø9 | ø13 |
|----------------------|-------|------|------|
| Lane Configurations | | | |
| Volume (vph) | | | |
| Turn Type | | | |
| Protected Phases | 6 | 9 | 13 |
| Permitted Phases | | | |
| Detector Phase | | | |
| Switch Phase | | | |
| Minimum Initial (s) | 12.0 | 28.0 | 8.0 |
| Minimum Split (s) | 30.0 | 35.0 | 15.0 |
| Total Split (s) | 50.0 | 35.0 | 15.0 |
| Total Split (%) | 25% | 18% | 8% |
| Yellow Time (s) | 4.7 | 4.7 | 2.5 |
| All-Red Time (s) | 2.3 | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | |
| Total Lost Time (s) | | | |
| Lead/Lag | Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes | Yes |
| Recall Mode | C-Min | None | None |
| Intersection Summary | | | |

Lanes, Volumes, Timings

3: Mathilda Ave & Moffett Park Dr/SR 237 WB Off-Ramp

3/4/2016

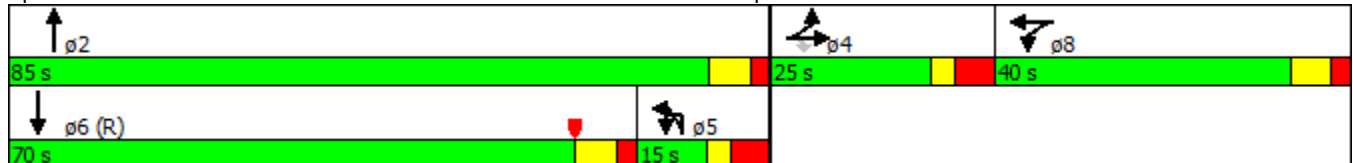


| Lane Group | EBT | EBR | WBL | WBT | NBL | NBT | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | |
| Volume (vph) | 0 | 680 | 760 | 110 | 100 | 390 | 2250 |
| Turn Type | NA | Perm | Split | NA | Prot | NA | NA |
| Protected Phases | 4 | | 8 | 8 | 5 | 2 | 6 |
| Permitted Phases | | 4 | | | | | |
| Detector Phase | 4 | 4 | 8 | 8 | 5 | 2 | 6 |
| Switch Phase | | | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 8.0 | 8.0 |
| Minimum Split (s) | 11.0 | 11.0 | 40.0 | 40.0 | 11.0 | 26.9 | 14.9 |
| Total Split (s) | 25.0 | 25.0 | 40.0 | 40.0 | 15.0 | 85.0 | 70.0 |
| Total Split (%) | 16.7% | 16.7% | 26.7% | 26.7% | 10.0% | 56.7% | 46.7% |
| Yellow Time (s) | 2.5 | 2.5 | 4.5 | 4.5 | 2.5 | 4.7 | 4.7 |
| All-Red Time (s) | 4.5 | 4.5 | 2.5 | 2.5 | 4.5 | 2.2 | 2.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.9 | 6.9 |
| Lead/Lag | | | | | Lag | | Lead |
| Lead-Lag Optimize? | | | | | Yes | | Yes |
| Recall Mode | Max | Max | Max | Max | Max | None | C-Max |

Intersection Summary

Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 0 (0%), Referenced to phase 6:SBT, Start of Yellow, Master Intersection
 Natural Cycle: 150
 Control Type: Actuated-Coordinated

Splits and Phases: 3: Mathilda Ave & Moffett Park Dr/SR 237 WB Off-Ramp



Lanes, Volumes, Timings
 4: Mathilda Ave & SR 237 EB Ramps

3/4/2016

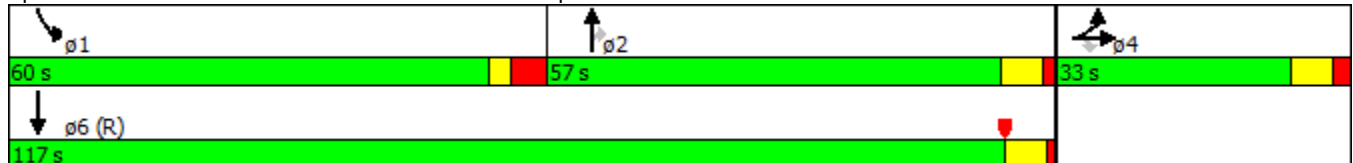


| Lane Group | EBL | EBT | EBR | NBT | NBR | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↙ | ↖ | ↗ | ↑↑↑↑ | ↗↖ | ↙ | ↑↑↑ |
| Volume (vph) | 120 | 0 | 150 | 460 | 670 | 360 | 2710 |
| Turn Type | Split | NA | Perm | NA | Perm | Prot | NA |
| Protected Phases | 4 | 4 | | 2 | | 1 | 6 |
| Permitted Phases | | | 4 | | 2 | | |
| Detector Phase | 4 | 4 | 4 | 2 | 2 | 1 | 6 |
| Switch Phase | | | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 4.0 | 8.0 | 8.0 | 4.0 | 8.0 |
| Minimum Split (s) | 11.0 | 11.0 | 11.0 | 18.2 | 18.2 | 10.4 | 13.9 |
| Total Split (s) | 33.0 | 33.0 | 33.0 | 57.0 | 57.0 | 60.0 | 117.0 |
| Total Split (%) | 22.0% | 22.0% | 22.0% | 38.0% | 38.0% | 40.0% | 78.0% |
| Yellow Time (s) | 4.8 | 4.8 | 4.8 | 4.7 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 2.2 | 2.2 | 2.2 | 1.5 | 1.5 | 3.9 | 1.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 6.2 | 6.2 | 6.4 | 5.9 |
| Lead/Lag | | | | Lag | Lag | Lead | |
| Lead-Lag Optimize? | | | | Yes | Yes | Yes | |
| Recall Mode | Max | Max | Max | None | None | None | C-Max |

Intersection Summary

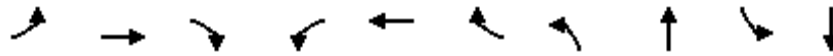
Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 6 (4%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 60
 Control Type: Actuated-Coordinated

Splits and Phases: 4: Mathilda Ave & SR 237 EB Ramps



Lanes, Volumes, Timings
5: Mathilda Ave & Ross Dr

3/4/2016

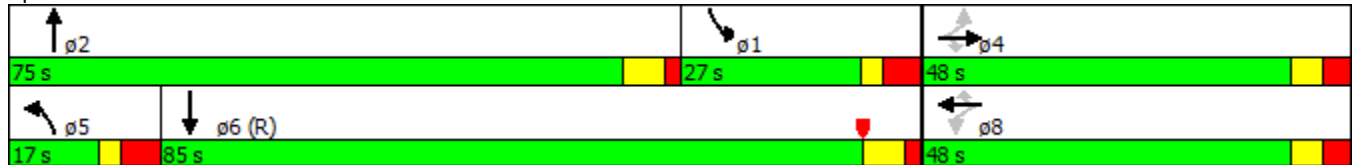


| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↖ | ↑ | ↗ | ↖ | ↑ | ↗ | ↖ | ↑↑↑↑ | ↗ | ↑↑↑ |
| Volume (vph) | 40 | 150 | 40 | 230 | 50 | 100 | 120 | 990 | 140 | 2660 |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | Prot | NA | Prot | NA |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | 1 | 6 |
| Permitted Phases | 4 | | 4 | 8 | | 8 | | | | |
| Detector Phase | 4 | 4 | 4 | 8 | 8 | 8 | 5 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 4.0 | 5.0 | 4.0 | 5.0 |
| Minimum Split (s) | 48.0 | 48.0 | 48.0 | 19.0 | 19.0 | 19.0 | 11.0 | 31.4 | 11.0 | 11.6 |
| Total Split (s) | 48.0 | 48.0 | 48.0 | 48.0 | 48.0 | 48.0 | 17.0 | 75.0 | 27.0 | 85.0 |
| Total Split (%) | 32.0% | 32.0% | 32.0% | 32.0% | 32.0% | 32.0% | 11.3% | 50.0% | 18.0% | 56.7% |
| Yellow Time (s) | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 2.5 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 3.4 | 3.4 | 3.4 | 3.4 | 3.4 | 3.4 | 4.5 | 1.7 | 4.5 | 1.9 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.4 | 7.0 | 6.6 |
| Lead/Lag | | | | | | | Lead | Lead | Lag | Lag |
| Lead-Lag Optimize? | | | | | | | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | Max | Max | Max | Max | None | None | C-Max |

Intersection Summary

Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 11 (7%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 145
 Control Type: Actuated-Coordinated

Splits and Phases: 5: Mathilda Ave & Ross Dr



Lanes, Volumes, Timings
 6: Mathilda Ave & US 101 NB Ramps

3/4/2016



| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↖↗ | ↖↗ | ↑↑↑ | ↖ | ↗ | ↑↑↑ |
| Volume (vph) | 800 | 220 | 1160 | 270 | 40 | 2890 |
| Turn Type | Prot | pm+ov | NA | Perm | Prot | NA |
| Protected Phases | 8 | 1 | 2 | | 1 | 6 |
| Permitted Phases | | 8 | | 2 | | |
| Detector Phase | 8 | 1 | 2 | 2 | 1 | 6 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 8.0 | 4.0 | 8.0 | 8.0 | 4.0 | 4.0 |
| Minimum Split (s) | 14.9 | 9.7 | 39.9 | 39.9 | 9.7 | 10.9 |
| Total Split (s) | 48.0 | 18.0 | 84.0 | 84.0 | 18.0 | 102.0 |
| Total Split (%) | 32.0% | 12.0% | 56.0% | 56.0% | 12.0% | 68.0% |
| Yellow Time (s) | 4.7 | 3.5 | 4.7 | 4.7 | 3.5 | 4.7 |
| All-Red Time (s) | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.9 | 5.7 | 6.9 | 6.9 | 5.7 | 6.9 |
| Lead/Lag | | Lead | Lag | Lag | Lead | |
| Lead-Lag Optimize? | | Yes | Yes | Yes | Yes | |
| Recall Mode | None | None | None | None | None | C-Max |

Intersection Summary

Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 6 (4%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 90
 Control Type: Actuated-Coordinated

Splits and Phases: 6: Mathilda Ave & US 101 NB Ramps



Lanes, Volumes, Timings
 7: Mathilda Ave & US 101 SB Ramps

3/4/2016

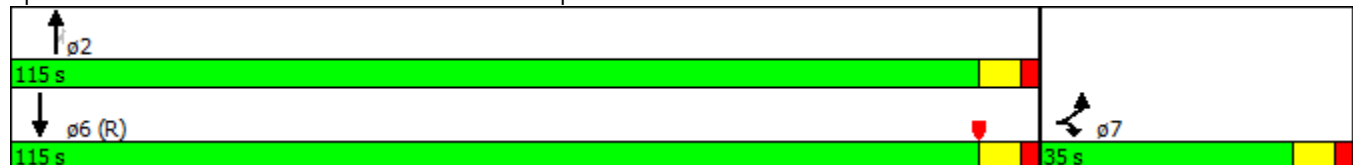


| Lane Group | EBL | EBR | NBT | NBR | SBT |
|----------------------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | |
| Volume (vph) | 80 | 500 | 1350 | 530 | 2550 |
| Turn Type | Prot | Prot | NA | Perm | NA |
| Protected Phases | 7 | 7 | 2 | | 6 |
| Permitted Phases | | | | 2 | |
| Detector Phase | 7 | 7 | 2 | 2 | 6 |
| Switch Phase | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 8.0 | 8.0 | 8.0 |
| Minimum Split (s) | 10.9 | 10.9 | 14.9 | 14.9 | 14.9 |
| Total Split (s) | 35.0 | 35.0 | 115.0 | 115.0 | 115.0 |
| Total Split (%) | 23.3% | 23.3% | 76.7% | 76.7% | 76.7% |
| Yellow Time (s) | 4.7 | 4.7 | 4.7 | 4.7 | 4.7 |
| All-Red Time (s) | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.9 | 6.9 | 6.9 | 6.9 | 6.9 |
| Lead/Lag | | | | | |
| Lead-Lag Optimize? | | | | | |
| Recall Mode | None | None | None | None | C-Max |

Intersection Summary

Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 7 (5%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 150
 Control Type: Actuated-Coordinated

Splits and Phases: 7: Mathilda Ave & US 101 SB Ramps



Lanes, Volumes, Timings
 8: Mathilda Ave & Almanor Ave/Ahwanee Ave

3/4/2016

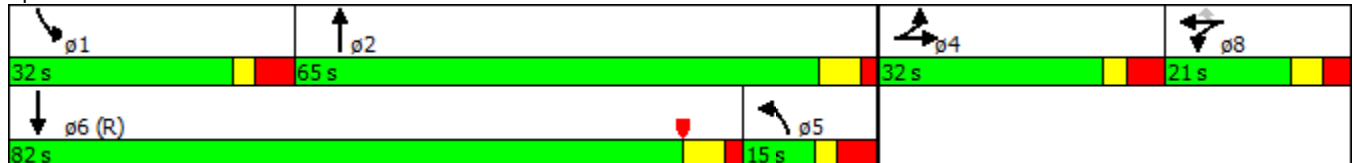


| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | |
| Volume (vph) | 310 | 30 | 50 | 10 | 190 | 60 | 1380 | 180 | 2800 |
| Turn Type | Split | NA | Split | NA | Perm | Prot | NA | Prot | NA |
| Protected Phases | 4 | 4 | 8 | 8 | | 5 | 2 | 1 | 6 |
| Permitted Phases | | | | | 8 | | | | |
| Detector Phase | 4 | 4 | 8 | 8 | 8 | 5 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | | |
| Minimum Initial (s) | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 12.0 | 8.0 | 12.0 |
| Minimum Split (s) | 32.0 | 32.0 | 15.0 | 15.0 | 15.0 | 15.0 | 36.7 | 15.0 | 18.7 |
| Total Split (s) | 32.0 | 32.0 | 21.0 | 21.0 | 21.0 | 15.0 | 65.0 | 32.0 | 82.0 |
| Total Split (%) | 21.3% | 21.3% | 14.0% | 14.0% | 14.0% | 10.0% | 43.3% | 21.3% | 54.7% |
| Yellow Time (s) | 2.8 | 2.8 | 3.6 | 3.6 | 3.6 | 2.5 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 4.2 | 4.2 | 3.4 | 3.4 | 3.4 | 4.5 | 2.0 | 4.5 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.7 | 7.0 | 6.7 |
| Lead/Lag | | | | | | Lag | Lag | Lead | Lead |
| Lead-Lag Optimize? | | | | | | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | None | None | None | C-Max |

Intersection Summary

Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 148 (99%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 120
 Control Type: Actuated-Coordinated

Splits and Phases: 8: Mathilda Ave & Almanor Ave/Ahwanee Ave



Lanes, Volumes, Timings
 9: US 101 On-Ramp & Moffett Park Dr

3/4/2016



| Lane Group | EBT | EBR | WBL | WBT |
|----------------------|-------|-------|-------|--------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ |
| Volume (vph) | 790 | 90 | 230 | 210 |
| Turn Type | NA | Perm | Prot | NA |
| Protected Phases | 2 | | 1 | 6 |
| Permitted Phases | | 2 | | |
| Detector Phase | 2 | 2 | 1 | 6 |
| Switch Phase | | | | |
| Minimum Initial (s) | 15.0 | 15.0 | 6.0 | 15.0 |
| Minimum Split (s) | 20.0 | 20.0 | 10.5 | 20.0 |
| Total Split (s) | 52.0 | 52.0 | 23.0 | 75.0 |
| Total Split (%) | 69.3% | 69.3% | 30.7% | 100.0% |
| Yellow Time (s) | 4.0 | 4.0 | 3.5 | 4.0 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.0 | 5.0 | 4.5 | 5.0 |
| Lead/Lag | Lag | Lag | Lead | |
| Lead-Lag Optimize? | | | | |
| Recall Mode | Min | Min | None | Min |

Intersection Summary

Cycle Length: 75
 Actuated Cycle Length: 52.7
 Natural Cycle: 50
 Control Type: Actuated-Uncoordinated

Splits and Phases: 9: US 101 On-Ramp & Moffett Park Dr



Lanes, Volumes, Timings
 10: Moffett Park Dr & Innovation Way

3/4/2016

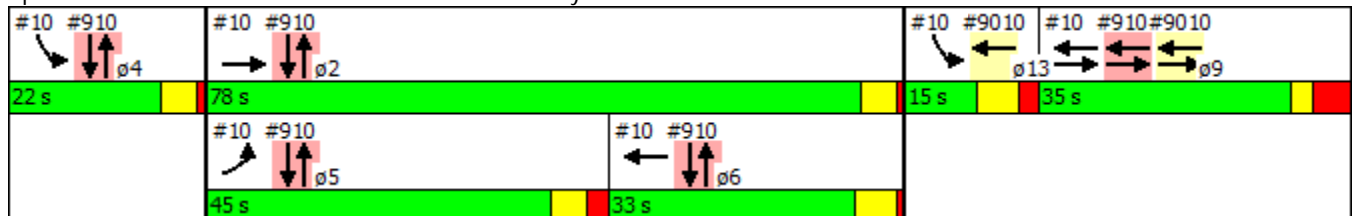


| Lane Group | EBL | EBT | WBT | SBL | ø2 | ø4 | ø6 | ø9 | ø13 |
|----------------------|-------|-----|-----|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | |
| Volume (vph) | 240 | 550 | 290 | 200 | | | | | |
| Turn Type | Prot | NA | NA | Prot | | | | | |
| Protected Phases | 5 | 2 9 | 6 9 | 4 13 | 2 | 4 | 6 | 9 | 13 |
| Permitted Phases | | | | | | | | | |
| Detector Phase | 5 | 2 | 6 | 4 | | | | | |
| Switch Phase | | | | | | | | | |
| Minimum Initial (s) | 8.0 | | | | 10.0 | 10.0 | 10.0 | 28.0 | 8.0 |
| Minimum Split (s) | 14.5 | | | | 14.9 | 15.0 | 27.5 | 35.0 | 15.0 |
| Total Split (s) | 45.0 | | | | 78.0 | 22.0 | 33.0 | 35.0 | 15.0 |
| Total Split (%) | 30.0% | | | | 52% | 15% | 22% | 23% | 10% |
| Yellow Time (s) | 4.0 | | | | 3.9 | 4.0 | 4.5 | 2.5 | 4.7 |
| All-Red Time (s) | 2.5 | | | | 1.0 | 1.0 | 1.0 | 4.5 | 2.3 |
| Lost Time Adjust (s) | 0.0 | | | | | | | | |
| Total Lost Time (s) | 6.5 | | | | | | | | |
| Lead/Lag | Lead | | | | | | Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | | | | | | Yes | Yes | Yes |
| Recall Mode | Max | | | | Min | None | Min | None | None |

Intersection Summary

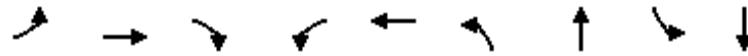
Cycle Length: 150
 Actuated Cycle Length: 101
 Natural Cycle: 110
 Control Type: Semi Act-Uncoord

Splits and Phases: 10: Moffett Park Dr & Innovation Way



Lanes, Volumes, Timings
 11: Innovation Way & 11th Ave

3/4/2016



| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT |
|---------------------|-----|------|-----|-----|------|-----|------|-----|------|
| Lane Configurations | | | | | | | | | |
| Volume (vph) | 390 | 0 | 270 | 10 | 0 | 60 | 290 | 80 | 60 |
| Sign Control | | Stop | | | Stop | | Stop | | Stop |

Intersection Summary

Control Type: Unsignalized

Lanes, Volumes, Timings

12: Innovation Way & Juniper Driveway

3/4/2016

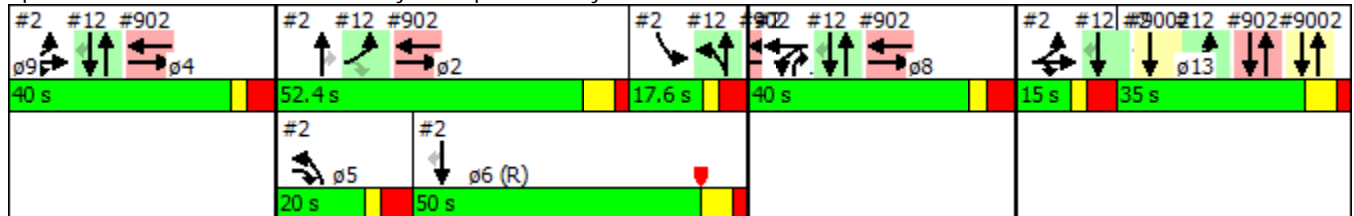


| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR | ø2 | ø4 | ø5 | ø6 | ø8 | ø9 |
|----------------------|------|------|------|-------|--------|--------|------|------|------|-------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 370 | 30 | 40 | 650 | 110 | 70 | | | | | | |
| Turn Type | Prot | Perm | Prot | NA | NA | Perm | | | | | | |
| Protected Phases | 2 9 | | 1 | 1 4 8 | 4 8 13 | | 2 | 4 | 5 | 6 | 8 | 9 |
| Permitted Phases | | 2 9 | | | | 4 8 13 | | | | | | |
| Detector Phase | 2 | 2 | 1 | 1 4 8 | 4 8 | 4 8 | | | | | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 10.0 | | | | 12.0 | 14.0 | 13.0 | 12.0 | 10.0 | 28.0 |
| Minimum Split (s) | | | 16.8 | | | | 19.0 | 39.0 | 20.0 | 30.0 | 35.0 | 35.0 |
| Total Split (s) | | | 17.6 | | | | 52.4 | 40.0 | 20.0 | 50.0 | 40.0 | 35.0 |
| Total Split (%) | | | 8.8% | | | | 26% | 20% | 10% | 25% | 20% | 18% |
| Yellow Time (s) | | | 2.5 | | | | 4.7 | 2.5 | 2.5 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | | | 4.3 | | | | 2.3 | 4.5 | 4.5 | 2.3 | 4.5 | 2.3 |
| Lost Time Adjust (s) | | | 0.0 | | | | | | | | | |
| Total Lost Time (s) | | | 6.8 | | | | | | | | | |
| Lead/Lag | | | Lag | | | | Lead | | Lead | Lag | | Lag |
| Lead-Lag Optimize? | | | Yes | | | | Yes | | Yes | Yes | | Yes |
| Recall Mode | | | None | | | | Max | None | None | C-Min | None | None |

Intersection Summary

Cycle Length: 200
 Actuated Cycle Length: 200
 Offset: 0 (0%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 175
 Control Type: Actuated-Coordinated

Splits and Phases: 12: Innovation Way & Juniper Driveway



| | |
|----------------------|------|
| Lane Group | ø13 |
| Lane Configurations | |
| Volume (vph) | |
| Turn Type | |
| Protected Phases | 13 |
| Permitted Phases | |
| Detector Phase | |
| Switch Phase | |
| Minimum Initial (s) | 8.0 |
| Minimum Split (s) | 15.0 |
| Total Split (s) | 15.0 |
| Total Split (%) | 8% |
| Yellow Time (s) | 2.5 |
| All-Red Time (s) | 4.5 |
| Lost Time Adjust (s) | |
| Total Lost Time (s) | |
| Lead/Lag | Lead |
| Lead-Lag Optimize? | Yes |
| Recall Mode | None |
| Intersection Summary | |

Lanes, Volumes, Timings
 13: Bordeaux Dr & Innovation Way

3/4/2016

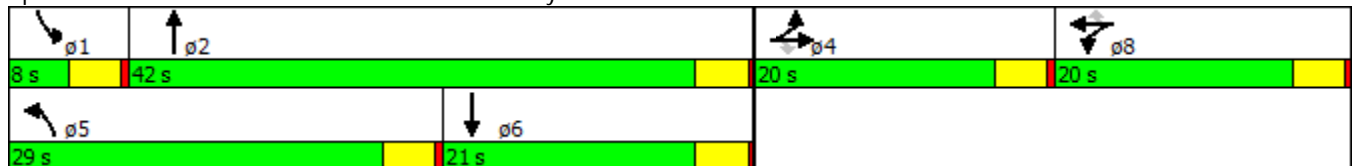


| Lane Group | EBT | EBR | NBL | NBT | SBT | ø1 | ø8 |
|----------------------|-------|-------|-------|-------|-------|------|------|
| Lane Configurations | ↖ | ↗ | ↖ | ↗ | ↗ | | |
| Volume (vph) | 10 | 140 | 450 | 30 | 140 | | |
| Turn Type | NA | Perm | Prot | NA | NA | | |
| Protected Phases | 4 | | 5 | 2 | 6 | 1 | 8 |
| Permitted Phases | | 4 | | | | | |
| Detector Phase | 4 | 4 | 5 | 2 | 6 | | |
| Switch Phase | | | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | 20.0 | 20.0 | 8.0 | 20.0 | 20.0 | 8.0 | 20.0 |
| Total Split (s) | 20.0 | 20.0 | 29.0 | 42.0 | 21.0 | 8.0 | 20.0 |
| Total Split (%) | 22.2% | 22.2% | 32.2% | 46.7% | 23.3% | 9% | 22% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | |
| Total Lost Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | |
| Lead/Lag | | | Lead | Lag | Lag | Lead | |
| Lead-Lag Optimize? | | | Yes | Yes | Yes | Yes | |
| Recall Mode | None | None | None | None | None | None | None |

Intersection Summary

Cycle Length: 90
 Actuated Cycle Length: 52.3
 Natural Cycle: 90
 Control Type: Actuated-Uncoordinated

Splits and Phases: 13: Bordeaux Dr & Innovation Way



SimTraffic Post-Processor
Average Results from 10 Runs
Network Performance

Mathilda Avenue Improvements
Build 1 Year 2018
PM Peak Hour

| Performance Measure | Average | Std. Dev. | Minimum | Maximum |
|---------------------------------|---------|-----------|---------|---------|
| Average Delay (seconds) | 399.9 | 22.9 | 350.9 | 425.1 |
| Total Delay (hours) | 1,293 | 84 | 1,112 | 1,401 |
| Average Stopped Delay (seconds) | 342.8 | 22.8 | 294.0 | 368.7 |
| Total Stopped Delay (hours) | 1108 | 82 | 931 | 1215 |
| Total Stops | 34,553 | 912 | 32,896 | 36,205 |
| Average Stops | 2.97 | 0.06 | 2.88 | 3.09 |
| Total Distance Traveled (miles) | 37,231 | 389 | 36,624 | 37,855 |
| Average Speed (mph) | 16.5 | 0.7 | 16.0 | 18.0 |
| Total Travel Time (hours) | 2,269.2 | 84.7 | 2,095.5 | 2,390.1 |
| Vehicles Entered | 9,863 | 139 | 9,605 | 10,063 |
| Vehicles Exited | 8,864 | 108 | 8,698 | 9,076 |
| Percent Demand Served | 89.9% | 1.3% | 87.2% | 91.9% |
| Fuel Used (gallons) | 1,241 | 24 | 1,201 | 1,279 |
| HC Emissions (grams) | 16,118 | 1,199 | 14,168 | 17,651 |
| CO Emissions (grams) | 454,835 | 20,618 | 418,517 | 481,637 |
| NOx Emissions (grams) | 60,315 | 2,803 | 55,524 | 64,177 |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Build 1 Year 2018
PM Peak Hour

Intersection 1 Mathilda Avenue/5th Avenue Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 110 | 95 | 86.4% | 54.4 | 10.3 | D |
| | Through | 340 | 311 | 91.4% | 18.4 | 2.7 | B |
| | Right Turn | 40 | 37 | 91.8% | 12.2 | 2.1 | B |
| | Subtotal | 490 | 442 | 90.3% | 25.7 | 3.0 | C |
| SB | Left Turn | 10 | 9 | 90.0% | 391.1 | 141.5 | F |
| | Through | 1,110 | 820 | 73.8% | 444.1 | 163.5 | F |
| | Right Turn | 10 | 6 | 63.0% | 362.1 | 199.1 | F |
| | Subtotal | 1,130 | 835 | 73.9% | 442.7 | 163.0 | F |
| EB | Left Turn | 70 | 67 | 96.3% | 35.2 | 3.8 | D |
| | Through | 20 | 21 | 103.5% | 58.2 | 12.4 | E |
| | Right Turn | 70 | 74 | 105.6% | 20.8 | 4.8 | C |
| | Subtotal | 160 | 162 | 101.3% | 31.4 | 5.1 | C |
| WB | Left Turn | 240 | 174 | 72.7% | 63.3 | 16.4 | E |
| | Through | 10 | 7 | 69.0% | 54.5 | 12.5 | D |
| | Right Turn | 30 | 23 | 75.7% | 32.2 | 14.5 | C |
| | Subtotal | 280 | 204 | 72.9% | 59.7 | 16.1 | E |
| Total | | 2,060 | 1,643 | 79.8% | 238.1 | 78.9 | F |

Intersection 2 Mathilda Avenue/Innovation Way-Driveway Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 10 | 8 | 83.0% | 111.7 | 26.4 | F |
| | Through | 330 | 310 | 93.8% | 46.4 | 6.8 | D |
| | Right Turn | 200 | 194 | 97.0% | 10.6 | 1.0 | B |
| | Subtotal | 540 | 512 | 94.8% | 33.9 | 4.7 | C |
| SB | Left Turn | 50 | 37 | 74.4% | 361.3 | 25.0 | F |
| | Through | 1,320 | 943 | 71.5% | 390.5 | 33.1 | F |
| | Right Turn | 50 | 37 | 73.0% | 332.6 | 45.6 | F |
| | Subtotal | 1,420 | 1,017 | 71.6% | 387.3 | 32.5 | F |
| EB | Left Turn | 140 | 122 | 87.1% | 84.1 | 6.2 | F |
| | Through | 200 | 176 | 88.0% | 83.6 | 6.2 | F |
| | Right Turn | 680 | 628 | 92.4% | 85.4 | 6.1 | F |
| | Subtotal | 1,020 | 926 | 90.8% | 84.9 | 6.1 | F |
| WB | Left Turn | 480 | 244 | 50.9% | 365.9 | 26.5 | F |
| | Through | 120 | 64 | 53.7% | 392.3 | 39.2 | F |
| | Right Turn | 20 | 10 | 48.0% | 382.1 | 91.4 | F |
| | Subtotal | 620 | 318 | 51.3% | 371.4 | 30.0 | F |
| Total | | 3,600 | 2,773 | 77.0% | 218.4 | 8.7 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Build 1 Year 2018
PM Peak Hour

Intersection 3 Mathilda Avenue/Moffett Park Drive-SR 237 WB Off-Ramp Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | 190 | 179 | 94.4% | 219.2 | 50.9 | F |
| | Through | 390 | 380 | 97.4% | 34.4 | 12.6 | C |
| | Right Turn | | | | | | |
| | Subtotal | 580 | 559 | 96.4% | 93.6 | 24.3 | F |
| SB | Left Turn | | | | | | |
| | Through | 2,250 | 1,661 | 73.8% | 178.8 | 6.9 | F |
| | Right Turn | 230 | 152 | 65.9% | 203.9 | 10.6 | F |
| | Subtotal | 2,480 | 1,812 | 73.1% | 180.9 | 7.1 | F |
| EB | Left Turn | 70 | 61 | 87.6% | 416.3 | 51.6 | F |
| | Through | | | | | | |
| | Right Turn | 680 | 567 | 83.3% | 353.3 | 46.1 | F |
| | Subtotal | 750 | 628 | 83.7% | 359.6 | 46.2 | F |
| WB | Left Turn | 760 | 704 | 92.7% | 218.5 | 29.8 | F |
| | Through | 110 | 112 | 101.7% | 65.2 | 13.4 | E |
| | Right Turn | 80 | 75 | 93.6% | 43.4 | 13.7 | D |
| | Subtotal | 950 | 891 | 93.8% | 184.6 | 23.1 | F |
| Total | | 4,760 | 3,890 | 81.7% | 197.8 | 11.6 | F |

Intersection 4 Mathilda Avenue/SR 237 EB Ramps Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | | | | | | |
| | Through | 460 | 447 | 97.2% | 22.6 | 11.6 | C |
| | Right Turn | 670 | 668 | 99.7% | 9.5 | 3.5 | A |
| | Subtotal | 1,130 | 1,115 | 98.7% | 14.7 | 6.0 | B |
| SB | Left Turn | 360 | 299 | 83.1% | 70.7 | 8.8 | E |
| | Through | 2,710 | 2,153 | 79.4% | 27.0 | 3.5 | C |
| | Right Turn | | | | | | |
| | Subtotal | 3,070 | 2,452 | 79.9% | 32.3 | 2.6 | C |
| EB | Left Turn | 120 | 121 | 100.8% | 68.6 | 12.4 | E |
| | Through | | | | | | |
| | Right Turn | 150 | 150 | 100.3% | 50.1 | 25.4 | D |
| | Subtotal | 270 | 271 | 100.5% | 58.2 | 12.3 | E |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 4,470 | 3,838 | 85.9% | 29.0 | 2.2 | C |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Build 1 Year 2018
PM Peak Hour

Intersection 5 Mathilda Avenue/Ross Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | 120 | 115 | 95.5% | 118.2 | 19.0 | F |
| | Through | 990 | 988 | 99.8% | 41.1 | 4.4 | D |
| | Right Turn | 270 | 266 | 98.4% | 42.9 | 5.1 | D |
| | Subtotal | 1,380 | 1,369 | 99.2% | 48.0 | 5.0 | D |
| SB | Left Turn | 140 | 115 | 81.9% | 40.0 | 3.9 | D |
| | Through | 2,660 | 2,136 | 80.3% | 27.4 | 3.1 | C |
| | Right Turn | 60 | 50 | 82.5% | 25.8 | 7.1 | C |
| | Subtotal | 2,860 | 2,300 | 80.4% | 28.0 | 3.0 | C |
| EB | Left Turn | 40 | 37 | 92.8% | 46.0 | 3.2 | D |
| | Through | 150 | 150 | 99.7% | 44.7 | 4.8 | D |
| | Right Turn | 40 | 42 | 103.8% | 27.8 | 6.3 | C |
| | Subtotal | 230 | 228 | 99.2% | 41.8 | 3.8 | D |
| WB | Left Turn | 230 | 231 | 100.6% | 174.1 | 50.2 | F |
| | Through | 50 | 49 | 98.0% | 159.3 | 50.6 | F |
| | Right Turn | 100 | 98 | 97.9% | 134.9 | 46.2 | F |
| | Subtotal | 380 | 378 | 99.6% | 162.1 | 49.6 | F |
| Total | | 4,850 | 4,275 | 88.2% | 46.9 | 3.8 | D |

Intersection 6 Mathilda Avenue/US 101 NB Ramps Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | | | | | | |
| | Through | 1,160 | 1,147 | 98.9% | 18.3 | 1.6 | B |
| | Right Turn | 270 | 275 | 101.7% | 4.9 | 0.3 | A |
| | Subtotal | 1,430 | 1,422 | 99.4% | 15.7 | 1.3 | B |
| SB | Left Turn | 40 | 33 | 82.5% | 81.0 | 6.4 | F |
| | Through | 2,890 | 2,379 | 82.3% | 52.9 | 4.1 | D |
| | Right Turn | | | | | | |
| | Subtotal | 2,930 | 2,412 | 82.3% | 53.3 | 4.0 | D |
| EB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| WB | Left Turn | 800 | 805 | 100.6% | 84.1 | 5.1 | F |
| | Through | | | | | | |
| | Right Turn | 220 | 219 | 99.5% | 61.2 | 4.3 | E |
| | Subtotal | 1,020 | 1,024 | 100.4% | 79.2 | 4.9 | E |
| Total | | 5,380 | 4,858 | 90.3% | 47.8 | 1.4 | D |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Build 1 Year 2018
PM Peak Hour

Intersection 7 Mathilda Avenue/US 101 SB Ramps Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | | | | | | |
| | Through | 1,350 | 1,339 | 99.2% | 6.6 | 0.6 | A |
| | Right Turn | 530 | 532 | 100.5% | 7.8 | 0.5 | A |
| | Subtotal | 1,880 | 1,871 | 99.5% | 6.9 | 0.5 | A |
| SB | Left Turn | | | | | | |
| | Through | 2,550 | 2,256 | 88.5% | 6.7 | 0.3 | A |
| | Right Turn | 1,140 | 929 | 81.5% | 14.5 | 2.4 | B |
| | Subtotal | 3,690 | 3,184 | 86.3% | 9.0 | 0.8 | A |
| EB | Left Turn | 80 | 82 | 102.8% | 90.6 | 4.7 | F |
| | Through | | | | | | |
| | Right Turn | 500 | 504 | 100.7% | 27.3 | 1.3 | C |
| | Subtotal | 580 | 586 | 101.0% | 36.2 | 1.3 | D |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 6,150 | 5,641 | 91.7% | 11.1 | 0.6 | B |

Intersection 8 Mathilda Avenue/Almanor Avenue-Ahwanee Avenue Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | 60 | 60 | 100.0% | 91.2 | 15.8 | F |
| | Through | 1,380 | 1,366 | 99.0% | 39.3 | 1.9 | D |
| | Right Turn | 40 | 45 | 111.5% | 27.3 | 3.4 | C |
| | Subtotal | 1,480 | 1,471 | 99.4% | 41.1 | 1.5 | D |
| SB | Left Turn | 180 | 169 | 94.1% | 78.1 | 5.5 | E |
| | Through | 2,800 | 2,524 | 90.1% | 22.8 | 0.9 | C |
| | Right Turn | 70 | 65 | 93.4% | 18.2 | 2.7 | B |
| | Subtotal | 3,050 | 2,759 | 90.5% | 26.1 | 0.8 | C |
| EB | Left Turn | 310 | 310 | 100.1% | 84.9 | 3.2 | F |
| | Through | 30 | 31 | 102.3% | 85.4 | 9.2 | F |
| | Right Turn | 70 | 72 | 103.1% | 55.5 | 7.0 | E |
| | Subtotal | 410 | 413 | 100.8% | 79.8 | 3.3 | E |
| WB | Left Turn | 50 | 48 | 95.4% | 63.4 | 8.3 | E |
| | Through | 10 | 8 | 84.0% | 65.9 | 14.8 | E |
| | Right Turn | 190 | 194 | 102.2% | 9.5 | 1.1 | A |
| | Subtotal | 250 | 250 | 100.1% | 21.6 | 2.0 | C |
| Total | | 5,190 | 4,893 | 94.3% | 34.9 | 0.8 | C |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Build 1 Year 2018
PM Peak Hour

Intersection 9 US 101 NB Slip Ramp/Moffett Park Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| EB | Left Turn | | | | | | |
| | Through | 790 | 789 | 99.9% | 8.0 | 4.7 | A |
| | Right Turn | 90 | 93 | 103.7% | 3.0 | 1.0 | A |
| | Subtotal | 880 | 883 | 100.3% | 7.5 | 4.3 | A |
| WB | Left Turn | 230 | 182 | 79.1% | 19.9 | 2.3 | B |
| | Through | 210 | 167 | 79.3% | 2.8 | 0.3 | A |
| | Right Turn | | | | | | |
| | Subtotal | 440 | 349 | 79.2% | 11.7 | 1.2 | B |
| Total | | 1,320 | 1,231 | 93.3% | 8.7 | 3.2 | A |

Intersection 10 Innovation Way/Moffett Park Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | 200 | 149 | 74.3% | 274.0 | 94.0 | F |
| | Through | | | | | | |
| | Right Turn | 150 | 113 | 75.1% | 257.3 | 87.8 | F |
| | Subtotal | 350 | 261 | 74.6% | 267.0 | 91.8 | F |
| EB | Left Turn | 240 | 237 | 98.8% | 42.3 | 23.2 | D |
| | Through | 550 | 525 | 95.5% | 72.7 | 56.7 | E |
| | Right Turn | | | | | | |
| | Subtotal | 790 | 762 | 96.5% | 63.4 | 46.5 | E |
| WB | Left Turn | | | | | | |
| | Through | 290 | 235 | 81.1% | 30.2 | 2.1 | C |
| | Right Turn | 150 | 125 | 83.3% | 19.9 | 3.1 | B |
| | Subtotal | 440 | 360 | 81.9% | 26.6 | 2.1 | C |
| Total | | 1,580 | 1,384 | 87.6% | 90.7 | 37.8 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Build 1 Year 2018
PM Peak Hour

Intersection 11 Innovation Way/11th Avenue All-way Stop

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 60 | 56 | 93.7% | 12.4 | 7.1 | B |
| | Through | 290 | 267 | 91.9% | 20.7 | 20.2 | C |
| | Right Turn | 30 | 28 | 92.0% | 13.7 | 19.5 | B |
| | Subtotal | 380 | 350 | 92.2% | 18.9 | 18.2 | C |
| SB | Left Turn | 80 | 56 | 69.4% | 10.8 | 3.2 | B |
| | Through | 60 | 45 | 74.3% | 35.5 | 18.1 | E |
| | Right Turn | | | | | | |
| | Subtotal | 140 | 100 | 71.5% | 21.3 | 7.2 | C |
| EB | Left Turn | 390 | 368 | 94.3% | 60.6 | 30.2 | F |
| | Through | | | | | | |
| | Right Turn | 270 | 221 | 82.0% | 166.7 | 131.0 | F |
| | Subtotal | 660 | 589 | 89.3% | 96.9 | 56.4 | F |
| WB | Left Turn | 10 | 9 | 92.0% | 33.0 | 38.6 | D |
| | Through | | | | | | |
| | Right Turn | 10 | 11 | 112.0% | 10.9 | 14.3 | B |
| | Subtotal | 20 | 20 | 102.0% | 21.2 | 22.6 | C |
| Total | | 1,200 | 1,060 | 88.3% | 61.7 | 28.8 | F |

Intersection 12 Innovation Way/Juniper Networks Driveway Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 40 | 38 | 95.0% | 337.7 | 152.9 | F |
| | Through | 650 | 609 | 93.8% | 149.3 | 75.4 | F |
| | Right Turn | | | | | | |
| | Subtotal | 690 | 647 | 93.8% | 159.9 | 78.7 | F |
| SB | Left Turn | | | | | | |
| | Through | 110 | 71 | 64.9% | 31.1 | 8.6 | C |
| | Right Turn | 70 | 39 | 56.1% | 5.9 | 1.7 | A |
| | Subtotal | 180 | 111 | 61.5% | 22.1 | 5.6 | C |
| EB | Left Turn | 370 | 317 | 85.6% | 453.6 | 154.1 | F |
| | Through | | | | | | |
| | Right Turn | 30 | 30 | 100.0% | 32.3 | 16.5 | C |
| | Subtotal | 400 | 347 | 86.7% | 416.8 | 141.1 | F |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 1,270 | 1,105 | 87.0% | 227.0 | 50.7 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Build 1 Year 2018
PM Peak Hour

Intersection 13 Bordeaux Drive/Innovation Way Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 450 | 210 | 46.7% | 1139.8 | 74.8 | F |
| | Through | 30 | 15 | 49.3% | 957.0 | 81.1 | F |
| | Right Turn | | | | | | |
| | Subtotal | 480 | 225 | 46.9% | 1127.8 | 75.3 | F |
| SB | Left Turn | | | | | | |
| | Through | 140 | 94 | 66.9% | 916.1 | 199.0 | F |
| | Right Turn | 160 | 102 | 63.9% | 923.4 | 207.9 | F |
| | Subtotal | 300 | 196 | 65.3% | 919.8 | 203.3 | F |
| EB | Left Turn | 30 | 27 | 89.0% | 25.8 | 4.4 | C |
| | Through | 10 | 9 | 87.0% | 25.4 | 7.9 | C |
| | Right Turn | 140 | 130 | 92.6% | 5.6 | 0.3 | A |
| | Subtotal | 180 | 165 | 91.7% | 9.9 | 1.0 | A |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 960 | 586 | 61.1% | 740.9 | 76.3 | F |

Intersection 1

Mathilda Avenue/5th Avenue

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 625 | 50 | 14 | 100 | 22 | 150 | 22 | 4% | 0% |
| | Through | 625 | 25 | 5 | 50 | 7 | 50 | 7 | 0% | 0% |
| | Right Turn | 625 | 50 | 7 | 75 | 11 | 125 | 12 | 0% | 0% |
| NB | Left Turn | 425 | 75 | 8 | 125 | 18 | 150 | 37 | 0% | 0% |
| | Through | 1,125 | 75 | 5 | 125 | 12 | 175 | 22 | 0% | 0% |
| | Through/Right | 1,125 | 75 | 6 | 150 | 16 | 200 | 23 | 0% | 0% |
| SB | Left Turn | 250 | 50 | 24 | 175 | 75 | 275 | 73 | 0% | 0% |
| | Through | 1,325 | 1,050 | 299 | 2,125 | 523 | 2,475 | 427 | 66% | 0% |
| | Right Turn | 250 | 50 | 10 | 175 | 36 | 300 | 1 | 0% | 0% |
| WB | Left Turn | 925 | 125 | 30 | 225 | 46 | 300 | 54 | 37% | 0% |
| | Through/Right | 75 | 50 | 7 | 100 | 10 | 100 | 0 | 2% | 0% |

Intersection 2

Mathilda Avenue/Innovation Way-Driveway

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|--------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left/Through | 225 | 225 | 15 | 325 | 17 | 325 | 19 | 0% | 24% |
| | Right Turn | 225 | 275 | 9 | 350 | 17 | 325 | 17 | 0% | 54% |
| NB | Left Turn | 725 | 25 | 2 | 25 | 9 | 25 | 21 | 0% | 0% |
| | Through | 975 | 125 | 9 | 225 | 16 | 275 | 35 | 0% | 0% |
| | Right Turn | 975 | 75 | 6 | 150 | 19 | 225 | 48 | 0% | 0% |
| SB | Left Turn | 75 | 75 | 9 | 150 | 13 | 150 | 0 | 6% | 0% |
| | Through | 975 | 1,150 | 47 | 1,300 | 65 | 1,225 | 18 | 88% | 43% |
| | Right Turn | 225 | 150 | 17 | 350 | 15 | 275 | 0 | 0% | 0% |
| WB | Left Turn | 425 | 750 | 1 | 775 | 2 | 775 | 6 | 76% | 65% |
| | Shared | 225 | 225 | 2 | 250 | 3 | 250 | 0 | 71% | 0% |

Intersection 3

Mathilda Avenue/Moffett Park Drive-SR 237 WB Off-Ramp

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|----------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Shared | 1,125 | 1,050 | 85 | 1,350 | 36 | 1,200 | 15 | 0% | 54% |
| | Right Turn | 1,125 | 1,025 | 85 | 1,350 | 38 | 1,200 | 16 | 0% | 51% |
| NB | Left Turn | 350 | 250 | 55 | 325 | 62 | 375 | 52 | 0% | 12% |
| | Through | 350 | 100 | 8 | 150 | 26 | 200 | 51 | 0% | 0% |
| | Right Diagonal | 350 | 175 | 15 | 225 | 12 | 200 | 16 | 0% | 80% |
| SB | Through | 975 | 1,050 | 3 | 1,075 | 7 | 1,075 | 9 | 0% | 32% |
| | Through/Right | 975 | 1,075 | 9 | 1,125 | 13 | 1,150 | 15 | 0% | 44% |
| WB | Left Turn | 525 | 575 | 45 | 650 | 37 | 600 | 0 | 52% | 0% |
| | Left/Through | 1,225 | 925 | 181 | 1,300 | 132 | 1,200 | 16 | 57% | 23% |
| | Through/Right | 1,225 | 175 | 23 | 275 | 41 | 350 | 69 | 0% | 0% |

Intersection 4

Mathilda Avenue/SR 237 EB Ramps

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|--------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,025 | 75 | 17 | 150 | 59 | 200 | 86 | 0% | 0% |
| | Left/Through | 1,025 | 50 | 20 | 125 | 69 | 150 | 102 | 0% | 0% |
| | Right Turn | 450 | 100 | 51 | 275 | 94 | 300 | 82 | 0% | 0% |
| NB | Through | 275 | 50 | 34 | 100 | 69 | 125 | 63 | 0% | 2% |
| | Right Turn | 275 | 50 | 31 | 125 | 69 | 225 | 71 | 1% | 1% |
| SB | Left Turn | 325 | 300 | 20 | 350 | 17 | 350 | 14 | 19% | 3% |
| | Through | 350 | 350 | 44 | 475 | 36 | 500 | 29 | 0% | 13% |
| | | | | | | | | | | |

SimTraffic Post-Processor
Average Results from 10 Runs
Queue Length
Intersection 5

Mathilda Avenue Improvements
Build 1 Year 2018
PM Peak Hour
Signal

Mathilda Avenue/Ross Drive

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 250 | 50 | 6 | 100 | 12 | 125 | 3 | 1% | 0% |
| | Through | 1,575 | 150 | 16 | 275 | 29 | 325 | 47 | 53% | 0% |
| | Right Turn | 50 | 50 | 8 | 100 | 13 | 100 | 0 | 11% | 0% |
| NB | Left Turn | 250 | 150 | 19 | 250 | 33 | 275 | 40 | 3% | 0% |
| | Through | 700 | 275 | 33 | 475 | 72 | 550 | 155 | 10% | 0% |
| | Through/Right | 225 | 225 | 7 | 300 | 13 | 275 | 0 | 33% | 0% |
| SB | Left Turn | 225 | 75 | 11 | 150 | 15 | 200 | 26 | 0% | 0% |
| | Through | 225 | 225 | 20 | 275 | 18 | 275 | 13 | 0% | 18% |
| | Through/Right | 225 | 275 | 21 | 325 | 15 | 300 | 12 | 0% | 60% |
| WB | Left Turn | 100 | 100 | 1 | 125 | 3 | 125 | 0 | 74% | 0% |
| | Through | 225 | 575 | 224 | 900 | 291 | 975 | 323 | 5% | 0% |
| | Right Turn | 100 | 50 | 6 | 100 | 8 | 100 | 2 | 5% | 0% |

Intersection 6

Mathilda Avenue/US 101 NB Ramps

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NB | Through | 575 | 200 | 14 | 275 | 23 | 325 | 41 | 0% | 0% |
| | Right Turn | 575 | 25 | 5 | 50 | 23 | 100 | 46 | 0% | 0% |
| SB | Left Turn | 375 | 75 | 17 | 225 | 71 | 400 | 125 | 0% | 0% |
| | Through | 700 | 550 | 73 | 700 | 45 | 725 | 29 | 21% | 0% |
| WB | Left Turn | 1,025 | 150 | 1 | 150 | 7 | 175 | 15 | 0% | 64% |
| | Right Turn | 1,025 | 75 | 7 | 125 | 13 | 125 | 15 | 0% | 6% |
| 0 | | | | | | | | | | |

Mathilda Avenue/US 101 SB Ramps

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,050 | 75 | 5 | 100 | 9 | 125 | 18 | 0% | 12% |
| | Right Turn | 1,050 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| NB | Through | 750 | 75 | 17 | 175 | 87 | 400 | 303 | 0% | 0% |
| | Right Turn | 750 | 25 | 11 | 75 | 109 | 225 | 318 | 0% | 0% |
| SB | Through | 575 | 100 | 10 | 150 | 20 | 175 | 34 | 0% | 0% |
| | Through/Right | 575 | 200 | 35 | 325 | 88 | 375 | 133 | 0% | 0% |
| | | | | | | | | | | |

Intersection 8

Mathilda Avenue/Almanor Avenue-Ahwanee Avenue

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,025 | 175 | 8 | 300 | 32 | 375 | 81 | 34% | 1% |
| | Through/Right | 125 | 100 | 11 | 225 | 20 | 225 | 0 | 3% | 0% |
| NB | Left Turn | 425 | 75 | 17 | 150 | 41 | 175 | 99 | 0% | 0% |
| | Through | 750 | 250 | 14 | 350 | 38 | 425 | 84 | 19% | 0% |
| | Through/Right | 750 | 200 | 18 | 325 | 21 | 325 | 4 | 3% | 0% |
| SB | Left Turn | 275 | 175 | 8 | 300 | 25 | 325 | 18 | 2% | 0% |
| | Through | 750 | 275 | 21 | 425 | 49 | 450 | 88 | 5% | 0% |
| | Through/Right | 750 | 200 | 12 | 350 | 27 | 375 | 41 | 0% | 0% |
| SB | Left Turn | 250 | 50 | 6 | 100 | 12 | 150 | 19 | 0% | 0% |
| | Through | 1,025 | 25 | 5 | 75 | 18 | 125 | 45 | 2% | 0% |
| | Right Turn | 75 | 75 | 4 | 100 | 7 | 125 | 6 | 13% | 0% |

US 101 NB Slip Ramp/Moffett Park Drive

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Through | 850 | 175 | 62 | 300 | 127 | 375 | 98 | 10% | 0% |
| | Right Turn | 150 | 50 | 28 | 125 | 109 | 175 | 140 | 0% | 0% |
| WB | Left Turn | 850 | 100 | 8 | 175 | 14 | 200 | 24 | 0% | 0% |
| | Through | 850 | 25 | 1 | 25 | 10 | 25 | 26 | 0% | 0% |
| | | | | | | | | | | |
| | | | | | | | | | | |

Intersection 10

Innovation Way/Moffett Park Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 225 | 175 | 45 | 350 | 94 | 325 | 47 | 2% | 0% |
| | Through | 850 | 300 | 166 | 625 | 351 | 650 | 268 | 32% | 3% |
| SB | Left Turn | 575 | 300 | 27 | 525 | 31 | 500 | 24 | 0% | 6% |
| | Shared | 575 | 375 | 20 | 600 | 24 | 550 | 17 | 0% | 33% |
| WB | Through | 1,150 | 75 | 8 | 150 | 14 | 175 | 30 | 0% | 0% |
| | Through/Right | 1,150 | 125 | 9 | 200 | 11 | 225 | 24 | 0% | 0% |
| | | | | | | | | | | |

SimTraffic Post-Processor
Average Results from 10 Runs
Queue Length
Intersection 11

Mathilda Avenue Improvements
Build 1 Year 2018
PM Peak Hour
All-way Stop

Innovation Way/11th Avenue

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 125 | 75 | 14 | 125 | 22 | 125 | 9 | 6% | 0% |
| | Left/Through | 325 | 300 | 205 | 900 | 668 | 1,300 | 866 | 8% | 0% |
| | Right Turn | 325 | 400 | 290 | 1,050 | 743 | 1,300 | 828 | 0% | 0% |
| NB | Left Turn | 125 | 50 | 7 | 75 | 27 | 100 | 45 | 0% | 0% |
| | Through | 575 | 125 | 30 | 200 | 77 | 275 | 93 | 4% | 0% |
| | Through/Right | 575 | 50 | 28 | 125 | 72 | 150 | 80 | 0% | 0% |
| SB | Left Turn | 175 | 50 | 5 | 75 | 11 | 100 | 21 | 0% | 0% |
| | Through | 1,000 | 25 | 3 | 50 | 7 | 75 | 21 | 0% | 0% |
| | Through/Right | 1,000 | 50 | 6 | 75 | 10 | 100 | 26 | 0% | 0% |
| WB | Left Turn | 325 | 25 | 5 | 50 | 12 | 50 | 22 | 0% | 0% |
| | Through/Right | 325 | 25 | 3 | 50 | 5 | 50 | 10 | 0% | 0% |

Intersection 12

Innovation Way/Juniper Networks Driveway

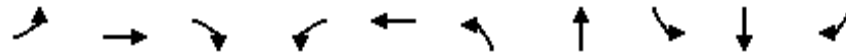
Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 200 | 1,450 | 457 | 2,325 | 743 | 2,375 | 677 | 0% | 0% |
| | Right Turn | 200 | 300 | 249 | 1,000 | 595 | 1,275 | 482 | 0% | 0% |
| NB | Left Turn | 125 | 100 | 18 | 200 | 9 | 175 | 0 | 32% | 0% |
| | Through | 1,000 | 525 | 220 | 825 | 251 | 875 | 229 | 64% | 6% |
| SB | Through | 300 | 150 | 22 | 225 | 48 | 225 | 75 | 0% | 0% |
| | Right Turn | 300 | 25 | 22 | 100 | 41 | 125 | 59 | 0% | 0% |
| 0 | | | | | | | | | | |

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left/Through | 375 | 50 | 3 | 75 | 12 | 100 | 30 | 0% | 0% |
| | Right Turn | 125 | 50 | 5 | 100 | 10 | 100 | 21 | 0% | 0% |
| NB | Left Turn | 325 | 850 | 22 | 925 | 39 | 900 | 0 | 93% | 0% |
| | Through/Right | 2,025 | 775 | 3 | 800 | 17 | 800 | 1 | 2% | 73% |
| SB | Left Turn | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | Through/Right | 725 | 2,750 | 616 | 4,875 | 707 | 4,475 | 530 | 91% | 20% |
| WB | Left/Through | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | Right Turn | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |

Lanes, Volumes, Timings
1: Mathilda Ave & 5th Ave

3/4/2016

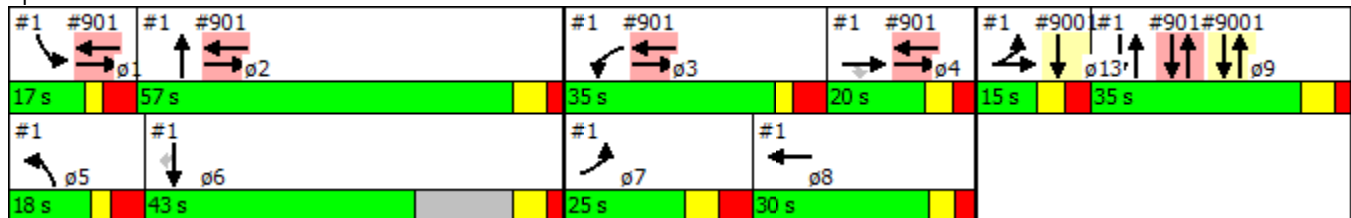


| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT | SBR | ø2 | ø7 |
|----------------------|------|------|--------|-------|-------|-------|-----|------|-----|--------|------|------|
| Lane Configurations | ↔↔ | ↑ | ↔ | ↔↔ | ↔ | ↔↔ | ↔↔↔ | ↔ | ↔↔↔ | ↔ | | |
| Volume (vph) | 20 | 10 | 30 | 30 | 10 | 80 | 870 | 10 | 370 | 70 | | |
| Turn Type | Prot | NA | custom | Prot | NA | Prot | NA | Prot | NA | custom | | |
| Protected Phases | 7 13 | 4 13 | | 3 | 8 | 5 | 2 9 | 1 | 6 9 | | 2 | 7 |
| Permitted Phases | | | 4 | | | | | | | 6 | | |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 5 | 2 | 1 | 6 | 6 | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 13.0 | 12.0 | 8.0 | 11.0 | | 10.0 | | 12.0 | 12.0 | 12.0 |
| Minimum Split (s) | | | 20.0 | 19.0 | 29.5 | 18.0 | | 17.0 | | 41.0 | 34.8 | 21.0 |
| Total Split (s) | | | 20.0 | 35.0 | 30.0 | 18.0 | | 17.0 | | 43.0 | 57.0 | 25.0 |
| Total Split (%) | | | 11.2% | 19.6% | 16.8% | 10.1% | | 9.5% | | 24.0% | 32% | 14% |
| Yellow Time (s) | | | 3.6 | 2.5 | 3.6 | 2.5 | | 2.5 | | 4.7 | 4.5 | 4.5 |
| All-Red Time (s) | | | 3.4 | 4.5 | 2.9 | 4.5 | | 4.5 | | 2.3 | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | | 0.0 | | |
| Total Lost Time (s) | | | 7.0 | 7.0 | 6.5 | 7.0 | | 7.0 | | 7.0 | | |
| Lead/Lag | | | Lag | Lead | Lag | Lead | | Lead | | Lag | Lag | Lead |
| Lead-Lag Optimize? | | | Yes | Yes | Yes | Yes | | Yes | | Yes | Yes | Yes |
| Recall Mode | | | None | None | None | None | | None | | None | Min | None |

Intersection Summary

Cycle Length: 179
 Actuated Cycle Length: 84.7
 Natural Cycle: 160
 Control Type: Actuated-Uncoordinated

Splits and Phases: 1: Mathilda Ave & 5th Ave



| Lane Group | ø9 | ø13 |
|----------------------|------|------|
| Lane Configurations | | |
| Volume (vph) | | |
| Turn Type | | |
| Protected Phases | 9 | 13 |
| Permitted Phases | | |
| Detector Phase | | |
| Switch Phase | | |
| Minimum Initial (s) | 28.0 | 8.0 |
| Minimum Split (s) | 35.0 | 15.0 |
| Total Split (s) | 35.0 | 15.0 |
| Total Split (%) | 20% | 8% |
| Yellow Time (s) | 4.7 | 3.6 |
| All-Red Time (s) | 2.3 | 3.4 |
| Lost Time Adjust (s) | | |
| Total Lost Time (s) | | |
| Lead/Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes |
| Recall Mode | None | None |
| Intersection Summary | | |

Lanes, Volumes, Timings
 2: Mathilda Ave & Innovation Way

3/4/2016

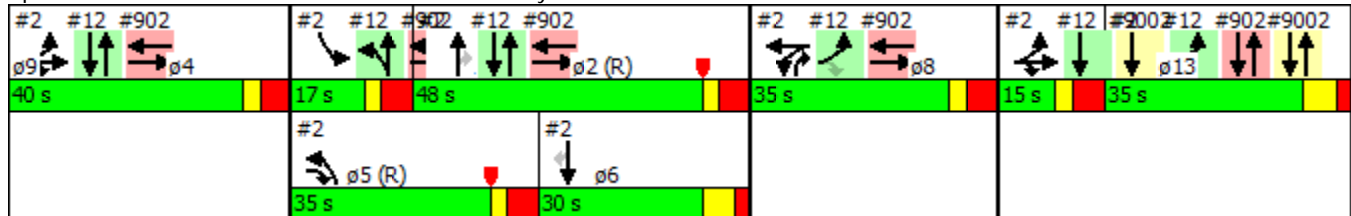


| Lane Group | EBT | EBR | WBL | WBT | NBL | NBT | NBR | SBL | SBT | SBR | ø2 | ø4 |
|----------------------|------|--------|-------|-------|-------|-----|-------|------|-----|------|-------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 60 | 70 | 210 | 110 | 720 | 930 | 880 | 20 | 280 | 130 | | |
| Turn Type | NA | pt+ov | Split | NA | Prot | NA | pm+ov | Prot | NA | Perm | | |
| Protected Phases | 4 13 | 4 13 5 | 8 | 8 | 5 | 2 9 | 8 | 1 | 6 9 | | 2 | 4 |
| Permitted Phases | | | | | | | 2 9 | | | | | 6 9 |
| Detector Phase | 4 | 4 | 8 | 8 | 5 | 2 | 2 | 1 | 6 | 6 | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 10.0 | 10.0 | 13.0 | | 10.0 | 10.0 | | | 12.0 | 14.0 |
| Minimum Split (s) | | | 35.0 | 35.0 | 20.0 | | 35.0 | 16.8 | | | 19.0 | 39.0 |
| Total Split (s) | | | 35.0 | 35.0 | 35.0 | | 35.0 | 17.0 | | | 48.0 | 40.0 |
| Total Split (%) | | | 18.4% | 18.4% | 18.4% | | 18.4% | 8.9% | | | 25% | 21% |
| Yellow Time (s) | | | 2.5 | 2.5 | 2.5 | | 2.5 | 2.5 | | | 2.5 | 2.5 |
| All-Red Time (s) | | | 4.5 | 4.5 | 4.5 | | 4.5 | 4.3 | | | 4.5 | 4.5 |
| Lost Time Adjust (s) | | | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | | | | |
| Total Lost Time (s) | | | 7.0 | 7.0 | 7.0 | | 7.0 | 6.8 | | | | |
| Lead/Lag | | | | | Lead | | | Lead | | | Lag | |
| Lead-Lag Optimize? | | | | | Yes | | | Yes | | | Yes | |
| Recall Mode | | | None | None | C-Max | | None | None | | | C-Max | None |

Intersection Summary

Cycle Length: 190
 Actuated Cycle Length: 190
 Offset: 0 (0%), Referenced to phase 2:NBT and 5:NBL, Start of Yellow
 Natural Cycle: 175
 Control Type: Actuated-Coordinated

Splits and Phases: 2: Mathilda Ave & Innovation Way



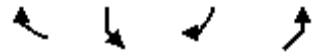
Lanes, Volumes, Timings
 2: Mathilda Ave & Innovation Way

3/4/2016

| Lane Group | ø6 | ø9 | ø13 |
|----------------------|------|------|------|
| Lane Configurations | | | |
| Volume (vph) | | | |
| Turn Type | | | |
| Protected Phases | 6 | 9 | 13 |
| Permitted Phases | | | |
| Detector Phase | | | |
| Switch Phase | | | |
| Minimum Initial (s) | 12.0 | 28.0 | 8.0 |
| Minimum Split (s) | 30.0 | 35.0 | 15.0 |
| Total Split (s) | 30.0 | 35.0 | 15.0 |
| Total Split (%) | 16% | 18% | 8% |
| Yellow Time (s) | 4.7 | 4.7 | 2.5 |
| All-Red Time (s) | 2.3 | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | |
| Total Lost Time (s) | | | |
| Lead/Lag | Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes | Yes |
| Recall Mode | None | None | None |
| Intersection Summary | | | |

Lanes, Volumes, Timings
 3: Mathilda Ave & SR 237 WB Off-Ramp

3/4/2016



| Lane Group | WBR | SBL | SBR2 | NEL | ø9 |
|----------------------|-------|-------|-------|-------|------|
| Lane Configurations | ↖ | ↖↖↖ | ↖ | ↖↖↖ | |
| Volume (vph) | 410 | 240 | 320 | 2120 | |
| Turn Type | Prot | Prot | Perm | Prot | |
| Protected Phases | 4 | 4 | | 2 | 9 |
| Permitted Phases | | | 4 | | |
| Detector Phase | 4 | 4 | 4 | 2 | |
| Switch Phase | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | 26.7 | 26.7 | 26.7 | 26.7 | 18.0 |
| Total Split (s) | 45.0 | 45.0 | 45.0 | 75.0 | 20.0 |
| Total Split (%) | 32.1% | 32.1% | 32.1% | 53.6% | 14% |
| Yellow Time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 2.0 |
| All-Red Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 0.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | 9.0 | 9.0 | 9.0 | 9.0 | |
| Lead/Lag | | | | | |
| Lead-Lag Optimize? | | | | | |
| Recall Mode | Max | Max | Max | C-Max | Max |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 110 (79%), Referenced to phase 2:NEL, Start of Yellow
 Natural Cycle: 110
 Control Type: Actuated-Coordinated

Splits and Phases: 3: Mathilda Ave & SR 237 WB Off-Ramp



Lanes, Volumes, Timings
 4: Mathilda Ave & SR 237 EB Off-Ramp

3/4/2016



| Lane Group | EBR | NBT | NBR2 | SWL | ø9 |
|----------------------|--------|-------|-------|-------|------|
| Lane Configurations | ↗ | ↑↑↑ | ↖ | ↑↑↑↑ | |
| Volume (vph) | 60 | 2380 | 760 | 860 | |
| Turn Type | custom | NA | Perm | Prot | |
| Protected Phases | 2 9 | 2 | | 4 | 9 |
| Permitted Phases | | | 2 | | |
| Detector Phase | 2 | 2 | 2 | 4 | |
| Switch Phase | | | | | |
| Minimum Initial (s) | | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | | 26.7 | 26.7 | 26.7 | 18.0 |
| Total Split (s) | | 75.0 | 75.0 | 45.0 | 20.0 |
| Total Split (%) | | 53.6% | 53.6% | 32.1% | 14% |
| Yellow Time (s) | | 3.0 | 3.0 | 3.0 | 2.0 |
| All-Red Time (s) | | 6.0 | 6.0 | 6.0 | 0.0 |
| Lost Time Adjust (s) | | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | | 9.0 | 9.0 | 9.0 | |
| Lead/Lag | | | | | |
| Lead-Lag Optimize? | | | | | |
| Recall Mode | | C-Max | C-Max | Max | Max |

Intersection Summary

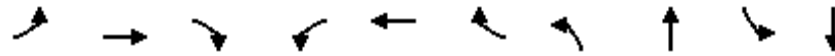
Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 110 (79%), Referenced to phase 2:NEL, Start of Yellow
 Natural Cycle: 110
 Control Type: Actuated-Coordinated

Splits and Phases: 4: Mathilda Ave & SR 237 EB Off-Ramp



Lanes, Volumes, Timings
5: Mathilda Ave & Ross Dr

3/4/2016

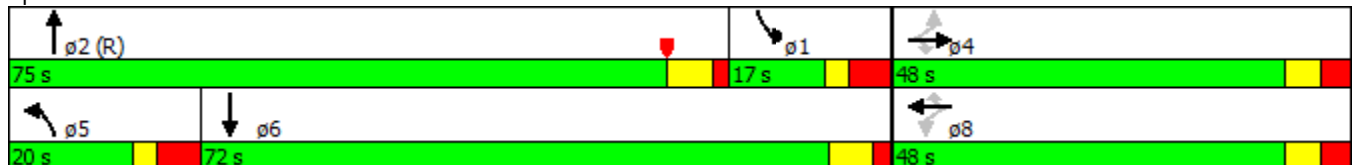


| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | | |
| Volume (vph) | 80 | 60 | 20 | 110 | 30 | 250 | 60 | 2810 | 50 | 840 |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | Prot | NA | Prot | NA |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | 1 | 6 |
| Permitted Phases | 4 | | 4 | 8 | | 8 | | | | |
| Detector Phase | 4 | 4 | 4 | 8 | 8 | 8 | 5 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 4.0 | 5.0 | 4.0 | 5.0 |
| Minimum Split (s) | 48.0 | 48.0 | 48.0 | 19.0 | 19.0 | 19.0 | 11.0 | 31.4 | 11.0 | 11.6 |
| Total Split (s) | 48.0 | 48.0 | 48.0 | 48.0 | 48.0 | 48.0 | 20.0 | 75.0 | 17.0 | 72.0 |
| Total Split (%) | 34.3% | 34.3% | 34.3% | 34.3% | 34.3% | 34.3% | 14.3% | 53.6% | 12.1% | 51.4% |
| Yellow Time (s) | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 2.5 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 3.4 | 3.4 | 3.4 | 3.4 | 3.4 | 3.4 | 4.5 | 1.7 | 4.5 | 1.9 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.4 | 7.0 | 6.6 |
| Lead/Lag | | | | | | | Lead | Lead | Lag | Lag |
| Lead-Lag Optimize? | | | | | | | Yes | Yes | Yes | Yes |
| Recall Mode | Min | Min | Min | Min | Min | Min | None | C-Max | None | None |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 0 (0%), Referenced to phase 2:NBT, Start of Yellow, Master Intersection
 Natural Cycle: 105
 Control Type: Actuated-Coordinated

Splits and Phases: 5: Mathilda Ave & Ross Dr



Lanes, Volumes, Timings
 6: Mathilda Ave & US 101 NB Ramps

3/4/2016



| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↖↖ | ↖↖ | ↑↑↑ | ↖ | ↖ | ↑↑↑ |
| Volume (vph) | 720 | 700 | 2270 | 360 | 10 | 960 |
| Turn Type | Prot | pm+ov | NA | Perm | Prot | NA |
| Protected Phases | 8 | 1 | 2 | | 1 | 6 |
| Permitted Phases | | 8 | | 2 | | |
| Detector Phase | 8 | 1 | 2 | 2 | 1 | 6 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 8.0 | 4.0 | 8.0 | 8.0 | 4.0 | 4.0 |
| Minimum Split (s) | 14.9 | 9.7 | 39.9 | 39.9 | 9.7 | 10.9 |
| Total Split (s) | 44.0 | 16.0 | 80.0 | 80.0 | 16.0 | 96.0 |
| Total Split (%) | 31.4% | 11.4% | 57.1% | 57.1% | 11.4% | 68.6% |
| Yellow Time (s) | 4.7 | 3.5 | 4.7 | 4.7 | 3.5 | 4.7 |
| All-Red Time (s) | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.9 | 5.7 | 6.9 | 6.9 | 5.7 | 6.9 |
| Lead/Lag | | Lead | Lag | Lag | Lead | |
| Lead-Lag Optimize? | | Yes | Yes | Yes | Yes | |
| Recall Mode | None | None | C-Max | C-Max | None | None |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 110 (79%), Referenced to phase 2:NBT, Start of Yellow
 Natural Cycle: 90
 Control Type: Actuated-Coordinated

Splits and Phases: 6: Mathilda Ave & US 101 NB Ramps



Lanes, Volumes, Timings
 7: Mathilda Ave & US 101 SB Ramps

3/4/2016



| Lane Group | EBL | EBR | NBT | NBR | SBT |
|----------------------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | |
| Volume (vph) | 280 | 410 | 2350 | 580 | 1540 |
| Turn Type | Prot | Prot | NA | Perm | NA |
| Protected Phases | 7 | 7 | 2 | | 6 |
| Permitted Phases | | | | 2 | |
| Detector Phase | 7 | 7 | 2 | 2 | 6 |
| Switch Phase | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 8.0 | 8.0 | 8.0 |
| Minimum Split (s) | 10.9 | 10.9 | 14.9 | 14.9 | 14.9 |
| Total Split (s) | 40.0 | 40.0 | 100.0 | 100.0 | 100.0 |
| Total Split (%) | 28.6% | 28.6% | 71.4% | 71.4% | 71.4% |
| Yellow Time (s) | 4.7 | 4.7 | 4.7 | 4.7 | 4.7 |
| All-Red Time (s) | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.9 | 6.9 | 6.9 | 6.9 | 6.9 |
| Lead/Lag | | | | | |
| Lead-Lag Optimize? | | | | | |
| Recall Mode | None | None | C-Max | C-Max | None |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 103 (74%), Referenced to phase 2:NBT, Start of Yellow
 Natural Cycle: 60
 Control Type: Actuated-Coordinated

Splits and Phases: 7: Mathilda Ave & US 101 SB Ramps



Lanes, Volumes, Timings
 8: Mathilda Ave & Almanor Ave/Ahwanee Ave

3/4/2016

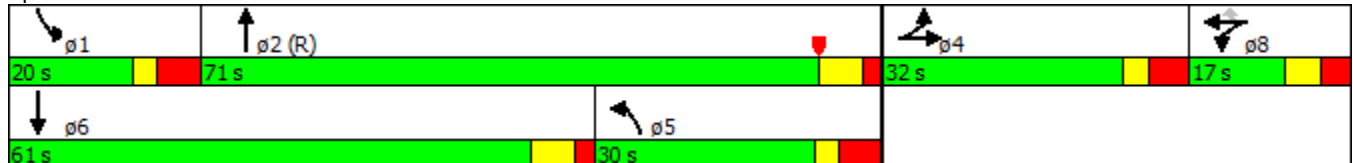


| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | |
| Volume (vph) | 90 | 20 | 70 | 30 | 190 | 110 | 2650 | 160 | 1490 |
| Turn Type | Split | NA | Split | NA | Perm | Prot | NA | Prot | NA |
| Protected Phases | 4 | 4 | 8 | 8 | | 5 | 2 | 1 | 6 |
| Permitted Phases | | | | | 8 | | | | |
| Detector Phase | 4 | 4 | 8 | 8 | 8 | 5 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | | |
| Minimum Initial (s) | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 12.0 | 8.0 | 12.0 |
| Minimum Split (s) | 32.0 | 32.0 | 15.0 | 15.0 | 15.0 | 15.0 | 36.7 | 15.0 | 18.7 |
| Total Split (s) | 32.0 | 32.0 | 17.0 | 17.0 | 17.0 | 30.0 | 71.0 | 20.0 | 61.0 |
| Total Split (%) | 22.9% | 22.9% | 12.1% | 12.1% | 12.1% | 21.4% | 50.7% | 14.3% | 43.6% |
| Yellow Time (s) | 2.8 | 2.8 | 3.6 | 3.6 | 3.6 | 2.5 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 4.2 | 4.2 | 3.4 | 3.4 | 3.4 | 4.5 | 2.0 | 4.5 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.7 | 7.0 | 6.7 |
| Lead/Lag | | | | | | Lag | Lag | Lead | Lead |
| Lead-Lag Optimize? | | | | | | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | None | C-Max | None | None |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 98 (70%), Referenced to phase 2:NBT, Start of Yellow
 Natural Cycle: 120
 Control Type: Actuated-Coordinated

Splits and Phases: 8: Mathilda Ave & Almanor Ave/Ahwanee Ave



Lanes, Volumes, Timings
 9: US 101 On-Ramp & Moffett Park Dr

3/4/2016

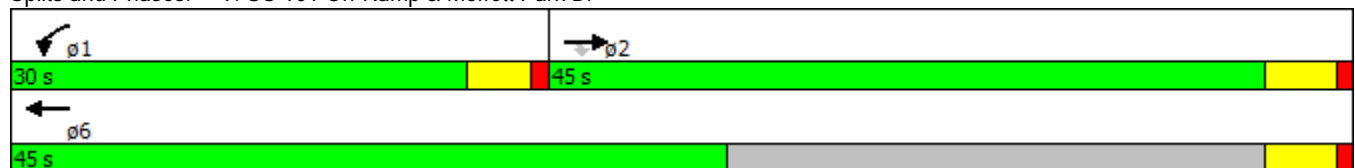


| Lane Group | EBT | EBR | WBL | WBT |
|----------------------|-------|-------|-------|-------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ |
| Volume (vph) | 180 | 10 | 20 | 890 |
| Turn Type | NA | Perm | Prot | NA |
| Protected Phases | 2 | | 1 | 6 |
| Permitted Phases | | 2 | | |
| Detector Phase | 2 | 2 | 1 | 6 |
| Switch Phase | | | | |
| Minimum Initial (s) | 15.0 | 15.0 | 6.0 | 15.0 |
| Minimum Split (s) | 20.0 | 20.0 | 10.5 | 20.0 |
| Total Split (s) | 45.0 | 45.0 | 30.0 | 45.0 |
| Total Split (%) | 60.0% | 60.0% | 40.0% | 60.0% |
| Yellow Time (s) | 4.0 | 4.0 | 3.5 | 4.0 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.0 | 5.0 | 4.5 | 5.0 |
| Lead/Lag | Lag | Lag | Lead | |
| Lead-Lag Optimize? | | | | |
| Recall Mode | Min | Min | None | Min |

Intersection Summary

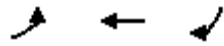
Cycle Length: 75
 Actuated Cycle Length: 40.1
 Natural Cycle: 40
 Control Type: Semi Act-Uncoord

Splits and Phases: 9: US 101 On-Ramp & Moffett Park Dr



Lanes, Volumes, Timings
 10: Moffett Park Dr & Innovation Way

3/4/2016



| Lane Group | EBL | WBT | SBR | ø4 | ø6 | ø9 |
|----------------------|-------|-----|-------|------|------|------|
| Lane Configurations | | | | | | |
| Volume (vph) | 180 | 690 | 220 | | | |
| Turn Type | Prot | NA | pt+ov | | | |
| Protected Phases | 5 | 6 9 | 4 5 | 4 | 6 | 9 |
| Permitted Phases | | | | | | |
| Detector Phase | 5 | 6 | 5 | | | |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 8.0 | | | 8.0 | 10.0 | 28.0 |
| Minimum Split (s) | 14.5 | | | 15.0 | 27.5 | 35.0 |
| Total Split (s) | 30.0 | | | 19.0 | 66.0 | 35.0 |
| Total Split (%) | 20.0% | | | 13% | 44% | 23% |
| Yellow Time (s) | 4.0 | | | 4.7 | 4.5 | 2.5 |
| All-Red Time (s) | 2.5 | | | 2.3 | 1.0 | 4.5 |
| Lost Time Adjust (s) | 0.0 | | | | | |
| Total Lost Time (s) | 6.5 | | | | | |
| Lead/Lag | Lead | | | | Lag | |
| Lead-Lag Optimize? | Yes | | | | Yes | |
| Recall Mode | None | | | None | Min | None |

Intersection Summary

Cycle Length: 150
 Actuated Cycle Length: 73.5
 Natural Cycle: 95
 Control Type: Actuated-Uncoordinated

Splits and Phases: 10: Moffett Park Dr & Innovation Way



Lanes, Volumes, Timings
 11: Innovation Way & 11th Ave

3/4/2016



| Lane Group | EBL | EBT | EBR | NBL | NBT | SBL | SBT |
|---------------------|-----|------|-----|-----|------|-----|------|
| Lane Configurations | | | | | | | |
| Volume (vph) | 20 | 0 | 30 | 130 | 190 | 60 | 190 |
| Sign Control | | Stop | | | Stop | | Stop |

Intersection Summary

Control Type: Unsignalized

Lanes, Volumes, Timings
 12: Innovation Way & Juniper Driveway

3/4/2016

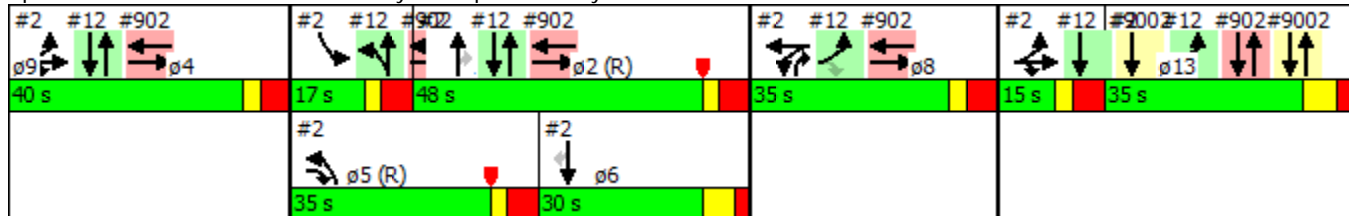


| Lane Group | EBL | EBR | NBL | NBT | SBT | ø2 | ø4 | ø5 | ø6 | ø8 | ø9 | ø13 |
|----------------------|------|------|------|-------|---------|-------|------|-------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 40 | 20 | 60 | 150 | 600 | | | | | | | |
| Turn Type | Prot | Perm | Prot | NA | NA | | | | | | | |
| Protected Phases | 8 9 | | 1 | 1 4 2 | 4 2 1 3 | 2 | 4 | 5 | 6 | 8 | 9 | 13 |
| Permitted Phases | | 8 9 | | | | | | | | | | |
| Detector Phase | 2 | 2 | 1 | 1 4 2 | 4 8 | | | | | | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 10.0 | | | 12.0 | 14.0 | 13.0 | 12.0 | 10.0 | 28.0 | 8.0 |
| Minimum Split (s) | | | 16.8 | | | 19.0 | 39.0 | 20.0 | 30.0 | 35.0 | 35.0 | 15.0 |
| Total Split (s) | | | 17.0 | | | 48.0 | 40.0 | 35.0 | 30.0 | 35.0 | 35.0 | 15.0 |
| Total Split (%) | | | 8.9% | | | 25% | 21% | 18% | 16% | 18% | 18% | 8% |
| Yellow Time (s) | | | 2.5 | | | 2.5 | 2.5 | 2.5 | 4.7 | 2.5 | 4.7 | 2.5 |
| All-Red Time (s) | | | 4.3 | | | 4.5 | 4.5 | 4.5 | 2.3 | 4.5 | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | 0.0 | | | | | | | | | |
| Total Lost Time (s) | | | 6.8 | | | | | | | | | |
| Lead/Lag | | | Lead | | | Lag | | Lead | Lag | | Lag | Lead |
| Lead-Lag Optimize? | | | Yes | | | Yes | | Yes | Yes | | Yes | Yes |
| Recall Mode | | | None | | | C-Max | None | C-Max | None | None | None | None |

Intersection Summary

Cycle Length: 190
 Actuated Cycle Length: 190
 Offset: 0 (0%), Referenced to phase 2:NBT and 5:NBL, Start of Yellow
 Natural Cycle: 175
 Control Type: Actuated-Coordinated

Splits and Phases: 12: Innovation Way & Juniper Driveway



Lanes, Volumes, Timings
 13: Bordeaux Dr & Innovation Way

3/4/2016

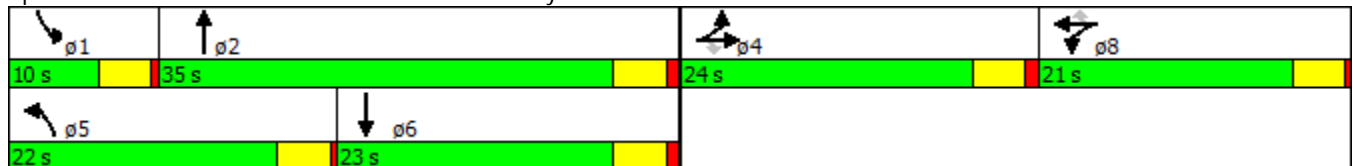


| Lane Group | EBT | EBR | NBL | NBT | SBT | ø1 | ø8 |
|----------------------|-------|-------|-------|-------|-------|------|------|
| Lane Configurations | ↖ | ↗ | ↙ | ↘ | ↘ | | |
| Volume (vph) | 0 | 580 | 250 | 110 | 50 | | |
| Turn Type | NA | Perm | Prot | NA | NA | | |
| Protected Phases | 4 | | 5 | 2 | 6 | 1 | 8 |
| Permitted Phases | | 4 | | | | | |
| Detector Phase | 4 | 4 | 5 | 2 | 6 | | |
| Switch Phase | | | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | 20.5 | 20.5 | 8.0 | 20.5 | 20.5 | 8.0 | 20.0 |
| Total Split (s) | 24.0 | 24.0 | 22.0 | 35.0 | 23.0 | 10.0 | 21.0 |
| Total Split (%) | 26.7% | 26.7% | 24.4% | 38.9% | 25.6% | 11% | 23% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.0 | 1.0 | 0.5 | 1.0 | 1.0 | 0.5 | 0.5 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | |
| Total Lost Time (s) | 4.5 | 4.5 | 4.0 | 4.5 | 4.5 | | |
| Lead/Lag | | | Lead | Lag | Lag | Lead | |
| Lead-Lag Optimize? | | | Yes | Yes | Yes | Yes | |
| Recall Mode | None | None | None | Min | Min | None | None |

Intersection Summary

Cycle Length: 90
 Actuated Cycle Length: 49.2
 Natural Cycle: 75
 Control Type: Actuated-Uncoordinated

Splits and Phases: 13: Bordeaux Dr & Innovation Way



**SimTraffic Post-Processor
Average Results from 10 Runs
Network Performance**

**Mathilda Avenue Improvements
2018 Build Alternative 2
AM Peak Hour**

| Performance Measure | Average | Std. Dev. | Minimum | Maximum |
|---------------------------------|---------|-----------|---------|---------|
| Average Delay (seconds) | 266.2 | 12.1 | 248.1 | 287.6 |
| Total Delay (hours) | 776 | 34 | 730 | 841 |
| Average Stopped Delay (seconds) | 183.9 | 11.4 | 164.9 | 203.2 |
| Total Stopped Delay (hours) | 536 | 32 | 485 | 595 |
| Total Stops | 36,256 | 842 | 34,974 | 37,891 |
| Average Stops | 3.45 | 0.08 | 3.31 | 3.60 |
| Total Distance Traveled (miles) | 43,270 | 321 | 42,714 | 43,853 |
| Average Speed (mph) | 23.8 | 0.6 | 23.0 | 25.0 |
| Total Travel Time (hours) | 1,816.1 | 30.8 | 1,777.7 | 1,880.3 |
| Vehicles Entered | 8,906 | 97 | 8,755 | 9,069 |
| Vehicles Exited | 8,442 | 95 | 8,312 | 8,603 |
| Percent Demand Served | 94.8% | 1.0% | 93.2% | 96.8% |
| Fuel Used (gallons) | 1,263 | 9 | 1,251 | 1,277 |
| HC Emissions (grams) | 18,817 | 1,165 | 16,991 | 20,486 |
| CO Emissions (grams) | 522,476 | 20,773 | 491,038 | 551,360 |
| NOx Emissions (grams) | 72,901 | 2,766 | 68,447 | 76,781 |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2018 Build Alternative 2
AM Peak Hour

Intersection 1 Mathilda Avenue/5th Avenue Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 80 | 70 | 87.5% | 39.7 | 6.1 | D |
| | Through | 870 | 821 | 94.4% | 14.3 | 1.1 | B |
| | Right Turn | 70 | 64 | 91.4% | 12.1 | 1.7 | B |
| | Subtotal | 1,020 | 955 | 93.6% | 16.1 | 1.0 | B |
| SB | Left Turn | 10 | 10 | 104.0% | 46.5 | 8.0 | D |
| | Through | 370 | 372 | 100.4% | 14.6 | 1.3 | B |
| | Right Turn | 70 | 73 | 104.0% | 1.7 | 0.5 | A |
| | Subtotal | 450 | 455 | 101.1% | 13.3 | 1.1 | B |
| EB | Left Turn | 20 | 20 | 100.0% | 32.0 | 3.4 | C |
| | Through | 10 | 10 | 100.0% | 29.5 | 8.9 | C |
| | Right Turn | 30 | 29 | 95.3% | 8.3 | 2.5 | A |
| | Subtotal | 60 | 59 | 97.7% | 20.3 | 3.8 | C |
| WB | Left Turn | 30 | 27 | 89.3% | 38.1 | 4.0 | D |
| | Through | 10 | 10 | 96.0% | 31.4 | 12.7 | C |
| | Right Turn | 10 | 9 | 87.0% | 6.2 | 2.9 | A |
| | Subtotal | 50 | 45 | 90.2% | 30.8 | 4.7 | C |
| Total | | 1,580 | 1,514 | 95.8% | 15.8 | 0.9 | B |

Intersection 2 Mathilda Avenue/Innovation Way Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 720 | 679 | 94.3% | 67.6 | 6.3 | E |
| | Through | 930 | 866 | 93.1% | 34.8 | 1.5 | C |
| | Right Turn | 880 | 831 | 94.5% | 31.3 | 1.7 | C |
| | Subtotal | 2,530 | 2,376 | 93.9% | 43.0 | 1.5 | D |
| SB | Left Turn | 20 | 21 | 104.0% | 94.5 | 19.6 | F |
| | Through | 280 | 271 | 96.8% | 63.1 | 6.5 | E |
| | Right Turn | 130 | 131 | 100.4% | 28.7 | 4.0 | C |
| | Subtotal | 430 | 422 | 98.2% | 54.3 | 5.0 | D |
| EB | Left Turn | 60 | 59 | 98.0% | 52.5 | 8.9 | D |
| | Through | 60 | 61 | 101.5% | 54.3 | 7.9 | D |
| | Right Turn | 70 | 73 | 104.6% | 42.7 | 5.1 | D |
| | Subtotal | 190 | 193 | 101.5% | 49.3 | 6.1 | D |
| WB | Left Turn | 210 | 191 | 90.7% | 290.9 | 39.4 | F |
| | Through | 110 | 104 | 94.8% | 315.9 | 40.4 | F |
| | Right Turn | 30 | 27 | 88.3% | 303.1 | 47.2 | F |
| | Subtotal | 350 | 321 | 91.8% | 300.2 | 39.9 | F |
| Total | | 3,500 | 3,312 | 94.6% | 69.7 | 4.0 | E |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2018 Build Alternative 2
AM Peak Hour

Intersection 3 Mathilda Avenue/Moffett Park Drive-SR 237 WB Ramps Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 850 | 790 | 93.0% | 7.3 | 1.3 | A |
| | Through | 2,120 | 1,948 | 91.9% | 29.9 | 1.2 | C |
| | Right Turn | | | | | | |
| | Subtotal | 2,970 | 2,738 | 92.2% | 23.4 | 1.2 | C |
| SB | Left Turn | | | | | | |
| | Through | 240 | 240 | 99.8% | 40.0 | 2.5 | D |
| | Right Turn | 320 | 305 | 95.4% | 29.9 | 5.2 | C |
| | Subtotal | 560 | 545 | 97.3% | 34.4 | 4.0 | C |
| EB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| WB | Left Turn | 670 | 669 | 99.8% | 42.2 | 2.0 | D |
| | Through | | | | | | |
| | Right Turn | 410 | 413 | 100.8% | 74.7 | 14.1 | E |
| | Subtotal | 1,080 | 1,082 | 100.2% | 54.6 | 6.6 | D |
| Total | | 4,610 | 4,365 | 94.8% | 32.5 | 2.9 | C |

Intersection 4 Mathilda Avenue/SR 237 EB On-Ramp Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | 2,380 | 2,155 | 90.5% | 33.5 | 0.7 | C |
| | Right Turn | 760 | 694 | 91.4% | 3.0 | 0.2 | A |
| | Subtotal | 3,140 | 2,849 | 90.7% | 26.1 | 0.6 | C |
| SB | Left Turn | 50 | 43 | 86.8% | 4.1 | 0.3 | A |
| | Through | 860 | 869 | 101.0% | 55.3 | 1.8 | E |
| | Right Turn | | | | | | |
| | Subtotal | 910 | 912 | 100.4% | 52.8 | 1.7 | D |
| EB | Left Turn | 590 | 599 | 101.5% | 63.2 | 8.0 | E |
| | Through | | | | | | |
| | Right Turn | 60 | 59 | 98.0% | 24.5 | 1.0 | C |
| | Subtotal | 650 | 658 | 101.2% | 59.7 | 7.4 | E |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 4,700 | 4,420 | 94.3% | 36.6 | 1.8 | D |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2018 Build Alternative 2
AM Peak Hour

Intersection 5 Mathilda Avenue/Ross Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 60 | 54 | 89.3% | 118.1 | 6.8 | F |
| | Through | 2,810 | 2,596 | 92.4% | 61.5 | 5.0 | E |
| | Right Turn | 100 | 97 | 96.7% | 39.0 | 6.6 | D |
| | Subtotal | 2,970 | 2,747 | 92.5% | 61.9 | 4.8 | E |
| SB | Left Turn | 50 | 51 | 101.6% | 40.4 | 6.9 | D |
| | Through | 840 | 842 | 100.2% | 18.2 | 3.2 | B |
| | Right Turn | 30 | 31 | 103.3% | 17.0 | 5.8 | B |
| | Subtotal | 920 | 924 | 100.4% | 19.3 | 3.0 | B |
| EB | Left Turn | 80 | 78 | 97.8% | 230.3 | 136.0 | F |
| | Through | 60 | 59 | 99.0% | 132.5 | 119.6 | F |
| | Right Turn | 20 | 20 | 101.5% | 105.7 | 126.6 | F |
| | Subtotal | 160 | 158 | 98.7% | 177.3 | 131.0 | F |
| WB | Left Turn | 110 | 76 | 69.1% | 678.6 | 159.2 | F |
| | Through | 30 | 24 | 79.0% | 683.6 | 229.3 | F |
| | Right Turn | 250 | 178 | 71.4% | 693.8 | 163.1 | F |
| | Subtotal | 390 | 278 | 71.3% | 689.4 | 164.3 | F |
| Total | | 4,440 | 4,106 | 92.5% | 98.6 | 9.5 | F |

Intersection 6 Mathilda Avenue/US 101 NB Ramps Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | 2,270 | 2,060 | 90.7% | 78.4 | 8.9 | E |
| | Right Turn | 360 | 326 | 90.6% | 11.4 | 1.3 | B |
| | Subtotal | 2,630 | 2,386 | 90.7% | 69.2 | 7.8 | E |
| SB | Left Turn | 10 | 11 | 105.0% | 31.3 | 7.4 | C |
| | Through | 960 | 927 | 96.5% | 15.3 | 0.7 | B |
| | Right Turn | | | | | | |
| | Subtotal | 970 | 937 | 96.6% | 15.5 | 0.7 | B |
| EB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| WB | Left Turn | 720 | 716 | 99.4% | 98.6 | 6.6 | F |
| | Through | | | | | | |
| | Right Turn | 700 | 705 | 100.7% | 82.4 | 6.7 | F |
| | Subtotal | 1,420 | 1,420 | 100.0% | 90.5 | 6.6 | F |
| Total | | 5,020 | 4,743 | 94.5% | 65.0 | 5.4 | E |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2018 Build Alternative 2
AM Peak Hour

Intersection 7 Mathilda Avenue/US 101 SB Ramps Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | 2,350 | 2,128 | 90.6% | 53.5 | 17.1 | D |
| | Right Turn | 580 | 545 | 94.0% | 15.7 | 2.9 | B |
| | Subtotal | 2,930 | 2,673 | 91.2% | 45.8 | 14.3 | D |
| SB | Left Turn | | | | | | |
| | Through | 1,540 | 1,515 | 98.4% | 7.9 | 3.1 | A |
| | Right Turn | 140 | 124 | 88.4% | 7.7 | 1.4 | A |
| | Subtotal | 1,680 | 1,639 | 97.6% | 7.9 | 2.9 | A |
| EB | Left Turn | 280 | 275 | 98.0% | 81.6 | 11.8 | F |
| | Through | | | | | | |
| | Right Turn | 410 | 416 | 101.4% | 27.3 | 3.7 | C |
| | Subtotal | 690 | 690 | 100.0% | 48.7 | 5.4 | D |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 5,300 | 5,003 | 94.4% | 33.7 | 7.4 | C |

Intersection 8 Mathilda Avenue-US 101 On-Ramp/Almanor Avenue-Ahwanee Avenue Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 110 | 102 | 92.7% | 240.7 | 33.2 | F |
| | Through | 2,650 | 2,423 | 91.4% | 251.7 | 35.9 | F |
| | Right Turn | 50 | 48 | 95.2% | 242.2 | 34.3 | F |
| | Subtotal | 2,810 | 2,573 | 91.6% | 251.0 | 35.8 | F |
| SB | Left Turn | 160 | 150 | 93.8% | 175.0 | 100.8 | F |
| | Through | 1,490 | 1,481 | 99.4% | 35.6 | 6.4 | D |
| | Right Turn | 300 | 299 | 99.5% | 35.7 | 6.3 | D |
| | Subtotal | 1,950 | 1,930 | 99.0% | 46.9 | 13.5 | D |
| EB | Left Turn | 90 | 94 | 104.9% | 56.5 | 3.1 | E |
| | Through | 20 | 21 | 104.5% | 59.3 | 8.6 | E |
| | Right Turn | 30 | 29 | 96.0% | 20.6 | 4.9 | C |
| | Subtotal | 140 | 144 | 102.9% | 49.8 | 3.1 | D |
| WB | Left Turn | 70 | 68 | 97.0% | 61.1 | 7.1 | E |
| | Through | 30 | 30 | 101.0% | 61.4 | 6.2 | E |
| | Right Turn | 190 | 193 | 101.7% | 12.8 | 2.2 | B |
| | Subtotal | 290 | 292 | 100.5% | 29.1 | 2.7 | C |
| Total | | 5,190 | 4,938 | 95.1% | 152.1 | 15.7 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2018 Build Alternative 2
AM Peak Hour

Intersection 9 Innovation Way-US 101 On-Ramp/Moffett Park Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| EB | Left Turn | | | | | | |
| | Through | 180 | 183 | 101.4% | 2.7 | 0.3 | A |
| | Right Turn | 10 | 11 | 110.0% | 1.7 | 0.5 | A |
| | Subtotal | 190 | 194 | 101.8% | 2.7 | 0.3 | A |
| WB | Left Turn | 20 | 19 | 93.5% | 9.2 | 0.5 | A |
| | Through | 890 | 835 | 93.8% | 4.8 | 0.4 | A |
| | Right Turn | | | | | | |
| | Subtotal | 910 | 854 | 93.8% | 4.9 | 0.4 | A |
| Total | | 1,100 | 1,047 | 95.2% | 4.5 | 0.4 | A |

Intersection 10 Innovation Way/Moffett Park Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | 220 | 206 | 93.5% | 26.8 | 2.8 | C |
| | Subtotal | 220 | 206 | 93.5% | 26.8 | 2.8 | C |
| EB | Left Turn | 180 | 184 | 102.0% | 27.6 | 3.4 | C |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | 180 | 184 | 102.0% | 27.6 | 3.4 | C |
| WB | Left Turn | | | | | | |
| | Through | 690 | 644 | 93.3% | 11.8 | 1.2 | B |
| | Right Turn | 240 | 228 | 95.0% | 11.6 | 1.6 | B |
| | Subtotal | 930 | 872 | 93.8% | 11.7 | 1.3 | B |
| Total | | 1,330 | 1,261 | 94.8% | 16.5 | 1.6 | B |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2018 Build Alternative 2
AM Peak Hour

Intersection 11 Innovation Way/11th Avenue All-way Stop

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 130 | 125 | 96.2% | 9.2 | 0.4 | A |
| | Through | 190 | 187 | 98.6% | 10.1 | 0.4 | B |
| | Right Turn | 80 | 82 | 102.5% | 5.3 | 0.4 | A |
| | Subtotal | 400 | 395 | 98.6% | 8.8 | 0.3 | A |
| SB | Left Turn | 60 | 58 | 96.5% | 8.0 | 0.6 | A |
| | Through | 190 | 177 | 92.9% | 11.8 | 0.4 | B |
| | Right Turn | 370 | 352 | 95.2% | 17.1 | 1.4 | C |
| | Subtotal | 620 | 587 | 94.6% | 14.6 | 1.0 | B |
| EB | Left Turn | 20 | 21 | 104.0% | 7.9 | 2.5 | A |
| | Through | | | | | | |
| | Right Turn | 30 | 29 | 97.0% | 7.4 | 2.0 | A |
| | Subtotal | 50 | 50 | 99.8% | 7.6 | 1.2 | A |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 1,070 | 1,031 | 96.4% | 12.1 | 0.6 | B |

Intersection 12 Innovation Way/Juniper Networks Driveway Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 60 | 57 | 95.3% | 99.2 | 13.3 | F |
| | Through | 150 | 151 | 100.4% | 12.7 | 2.0 | B |
| | Right Turn | | | | | | |
| | Subtotal | 210 | 208 | 99.0% | 36.6 | 5.3 | D |
| SB | Left Turn | | | | | | |
| | Through | 600 | 571 | 95.1% | 9.5 | 0.7 | A |
| | Right Turn | 360 | 348 | 96.6% | 8.3 | 0.7 | A |
| | Subtotal | 960 | 918 | 95.6% | 9.1 | 0.7 | A |
| EB | Left Turn | 40 | 41 | 102.8% | 58.8 | 8.4 | E |
| | Through | | | | | | |
| | Right Turn | 20 | 20 | 98.0% | 10.2 | 2.8 | B |
| | Subtotal | 60 | 61 | 101.2% | 42.9 | 5.3 | D |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 1,230 | 1,187 | 96.5% | 15.6 | 1.1 | B |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2018 Build Alternative 2
AM Peak Hour

Intersection 13 **Bordeaux Drive/Innovation Way** **Signal**

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 250 | 235 | 94.2% | 198.5 | 167.8 | F |
| | Through | 110 | 102 | 92.4% | 111.3 | 126.7 | F |
| | Right Turn | | | | | | |
| | Subtotal | 360 | 337 | 93.6% | 172.7 | 155.5 | F |
| SB | Left Turn | | | | | | |
| | Through | 50 | 48 | 96.6% | 34.3 | 8.3 | C |
| | Right Turn | 90 | 86 | 95.6% | 31.1 | 11.3 | C |
| | Subtotal | 140 | 134 | 95.9% | 32.3 | 10.0 | C |
| EB | Left Turn | 270 | 256 | 94.6% | 21.0 | 2.8 | C |
| | Through | | | | | | |
| | Right Turn | 580 | 552 | 95.1% | 12.5 | 1.6 | B |
| | Subtotal | 850 | 807 | 94.9% | 15.2 | 1.9 | B |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 1,350 | 1,278 | 94.7% | 57.4 | 40.1 | E |

Intersection 1 Mathilda Avenue/5th Avenue Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 625 | 25 | 4 | 75 | 6 | 100 | 8 | 0% | 0% |
| | Through | 625 | 25 | 4 | 50 | 8 | 75 | 7 | 0% | 0% |
| | Right Turn | 625 | 25 | 3 | 25 | 5 | 50 | 8 | 0% | 0% |
| NB | Left Turn | 425 | 50 | 8 | 100 | 13 | 100 | 16 | 0% | 0% |
| | Through | 1,125 | 100 | 10 | 200 | 25 | 275 | 63 | 0% | 0% |
| | Through/Right | 1,125 | 125 | 13 | 250 | 30 | 300 | 52 | 0% | 0% |
| SB | Left Turn | 250 | 25 | 3 | 50 | 6 | 50 | 11 | 0% | 0% |
| | Through | 1,325 | 75 | 8 | 125 | 18 | 150 | 30 | 0% | 0% |
| | Right Turn | 250 | 25 | 2 | 25 | 11 | 25 | 27 | 0% | 0% |
| WB | Left Turn | 925 | 25 | 4 | 75 | 9 | 75 | 18 | 4% | 0% |
| | Through/Right | 75 | 25 | 5 | 50 | 9 | 75 | 17 | 1% | 0% |

Intersection 2 Mathilda Avenue/Innovation Way Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|--------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left/Through | 225 | 150 | 8 | 200 | 15 | 250 | 22 | 0% | 1% |
| | Right Turn | 225 | 25 | 3 | 25 | 6 | 50 | 14 | 0% | 2% |
| NB | Left Turn | 725 | 350 | 33 | 575 | 72 | 600 | 91 | 0% | 0% |
| | Through | 975 | 225 | 20 | 425 | 79 | 550 | 286 | 0% | 0% |
| | Right Turn | 975 | 275 | 34 | 550 | 66 | 650 | 150 | 0% | 0% |
| SB | Left Turn | 75 | 25 | 7 | 75 | 20 | 100 | 41 | 1% | 0% |
| | Through | 975 | 125 | 13 | 200 | 21 | 250 | 40 | 9% | 0% |
| | Right Turn | 225 | 100 | 15 | 150 | 28 | 200 | 48 | 0% | 0% |
| WB | Left Turn | 425 | 725 | 60 | 850 | 60 | 800 | 22 | 10% | 31% |
| | Shared | 225 | 225 | 4 | 250 | 15 | 250 | 0 | 80% | 0% |

Intersection 3

Mathilda Avenue/Moffett Park Drive-SR 237 WB Ramps

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NB | Left Turn | 150 | 75 | 11 | 150 | 26 | 175 | 32 | 0% | 1% |
| | Through | 400 | 375 | 17 | 450 | 25 | 450 | 25 | 0% | 1% |
| SB | Through | 975 | 200 | 27 | 375 | 66 | 475 | 106 | 29% | 0% |
| WB | Left Turn | 1,075 | 200 | 33 | 250 | 66 | 325 | 81 | 0% | 0% |
| | Right Turn | 550 | 350 | 51 | 500 | 71 | 550 | 66 | 2% | 0% |
| 0 | | | | | | | | | | |

Intersection 4

Mathilda Avenue/SR 237 EB On-Ramp

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,050 | 225 | 24 | 325 | 36 | 400 | 40 | 0% | 0% |
| | Right Turn | 450 | 25 | 2 | 25 | 22 | 50 | 63 | 0% | 0% |
| NB | Through | 150 | 225 | 6 | 275 | 10 | 275 | 23 | 0% | 46% |
| | Right Turn | 150 | 25 | 5 | 25 | 44 | 75 | 127 | 0% | 0% |
| SB | Left Turn | 175 | 0 | 0 | 0 | 0 | 0 | 0 | 0% | 0% |
| | Through | 400 | 275 | 11 | 325 | 16 | 350 | 24 | 0% | 0% |
| | | | | | | | | | | |

Intersection 5

Mathilda Avenue/Ross Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 250 | 100 | 14 | 150 | 6 | 125 | 1 | 53% | 0% |
| | Through | 1,575 | 250 | 182 | 475 | 281 | 525 | 254 | 36% | 0% |
| | Right Turn | 50 | 25 | 3 | 50 | 10 | 100 | 6 | 2% | 0% |
| NB | Left Turn | 250 | 125 | 8 | 275 | 17 | 275 | 1 | 0% | 0% |
| | Through | 700 | 625 | 45 | 825 | 33 | 750 | 16 | 58% | 9% |
| | Through/Right | 700 | 525 | 43 | 800 | 25 | 725 | 17 | 0% | 1% |
| SB | Left Turn | 225 | 50 | 6 | 125 | 13 | 150 | 24 | 0% | 0% |
| | Through | 225 | 75 | 14 | 175 | 25 | 200 | 11 | 0% | 3% |
| | Through/Right | 225 | 100 | 14 | 225 | 18 | 250 | 23 | 0% | 6% |
| WB | Left Turn | 100 | 75 | 12 | 125 | 13 | 100 | 1 | 20% | 0% |
| | Through | 225 | 2,300 | 616 | 3,925 | 976 | 4,025 | 926 | 2% | 0% |
| | Right Turn | 100 | 100 | 1 | 125 | 3 | 125 | 0 | 90% | 0% |

Intersection 6

Mathilda Avenue/US 101 NB Ramps

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NB | Through | 575 | 625 | 38 | 750 | 50 | 700 | 20 | 0% | 27% |
| | Right Turn | 575 | 300 | 75 | 725 | 74 | 625 | 59 | 0% | 0% |
| SB | Left Turn | 375 | 25 | 2 | 50 | 6 | 75 | 13 | 0% | 0% |
| | Through | 700 | 200 | 20 | 325 | 24 | 325 | 55 | 0% | 0% |
| WB | Left Turn | 1,025 | 425 | 46 | 675 | 72 | 775 | 90 | 5% | 0% |
| | Right Turn | 1,025 | 375 | 12 | 450 | 16 | 400 | 15 | 0% | 0% |
| 0 | | | | | | | | | | |

Intersection 7

Mathilda Avenue/US 101 SB Ramps

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,050 | 150 | 14 | 200 | 25 | 275 | 40 | 5% | 0% |
| | Right Turn | 1,050 | 50 | 2 | 50 | 16 | 50 | 46 | 0% | 0% |
| NB | Through | 750 | 500 | 119 | 875 | 160 | 825 | 76 | 0% | 4% |
| | Right Turn | 750 | 325 | 149 | 850 | 210 | 800 | 189 | 0% | 4% |
| SB | Through | 575 | 50 | 24 | 125 | 67 | 175 | 81 | 0% | 0% |
| | Through/Right | 575 | 75 | 20 | 175 | 56 | 250 | 84 | 0% | 0% |
| | | | | | | | | | | |

Intersection 8

Mathilda Avenue-US 101 On-Ramp/Almanor Avenue-Ahwanee Avenue

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,025 | 75 | 5 | 125 | 8 | 125 | 10 | 1% | 0% |
| | Through/Right | 125 | 50 | 5 | 100 | 12 | 100 | 27 | 0% | 0% |
| NB | Left Turn | 425 | 250 | 31 | 600 | 38 | 500 | 0 | 0% | 0% |
| | Through | 725 | 2,000 | 296 | 3,150 | 406 | 3,375 | 416 | 65% | 0% |
| | Through/Right | 725 | 300 | 0 | 300 | 2 | 300 | 0 | 24% | 0% |
| SB | Left Turn | 275 | 225 | 54 | 325 | 40 | 325 | 1 | 26% | 0% |
| | Through | 750 | 300 | 139 | 550 | 206 | 575 | 175 | 6% | 3% |
| | Through/Right | 750 | 300 | 52 | 525 | 91 | 575 | 97 | 0% | 0% |
| WB | Left Turn | 250 | 75 | 10 | 150 | 27 | 175 | 66 | 0% | 0% |
| | Through | 1,025 | 50 | 15 | 150 | 39 | 225 | 90 | 12% | 0% |
| | Right Turn | 75 | 75 | 6 | 125 | 9 | 125 | 3 | 17% | 0% |

Intersection 9 Innovation Way-US 101 On-Ramp/Moffett Park Drive Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Through | 850 | 25 | 4 | 50 | 16 | 100 | 28 | 0% | 0% |
| | Right Turn | 150 | 25 | 1 | 25 | 6 | 25 | 16 | 0% | 0% |
| WB | Left Turn | 850 | 25 | 2 | 50 | 2 | 50 | 11 | 0% | 0% |
| | Through | 850 | 25 | 33 | 200 | 220 | 500 | 516 | 0% | 0% |
| | | | | | | | | | | |
| | | | | | | | | | | |

Intersection 10 Innovation Way/Moffett Park Drive Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 850 | 75 | 5 | 125 | 12 | 150 | 25 | 0% | 0% |
| SB | Right Turn | 575 | 50 | 6 | 75 | 9 | 100 | 16 | 0% | 0% |
| WB | Through | 1,150 | 100 | 10 | 200 | 38 | 250 | 83 | 0% | 0% |
| | Through/Right | 1,150 | 150 | 11 | 250 | 34 | 325 | 69 | 0% | 0% |
| | | | | | | | | | | |

Intersection 11

Innovation Way/11th Avenue

All-way Stop

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 125 | 25 | 3 | 50 | 6 | 50 | 12 | 0% | 0% |
| | Left/Through | 325 | 25 | 1 | 50 | 4 | 50 | 8 | 0% | 0% |
| | Right Turn | 325 | 25 | 2 | 50 | 4 | 75 | 4 | 0% | 0% |
| NB | Left Turn | 125 | 50 | 2 | 75 | 8 | 100 | 14 | 0% | 0% |
| | Through | 575 | 50 | 4 | 125 | 8 | 200 | 12 | 0% | 0% |
| | Through/Right | 575 | 50 | 2 | 75 | 7 | 75 | 13 | 0% | 0% |
| SB | Left Turn | 175 | 50 | 3 | 75 | 7 | 75 | 14 | 0% | 0% |
| | Through | 1,000 | 50 | 6 | 100 | 21 | 125 | 51 | 0% | 0% |
| | Through/Right | 1,000 | 150 | 13 | 250 | 24 | 300 | 51 | 0% | 0% |
| WB | Left Turn | 325 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | Through/Right | 325 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |

Intersection 12

Innovation Way/Juniper Networks Driveway

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 200 | 50 | 6 | 100 | 11 | 125 | 20 | 0% | 0% |
| | Right Turn | 200 | 25 | 3 | 50 | 5 | 50 | 13 | 0% | 0% |
| NB | Left Turn | 125 | 75 | 5 | 150 | 7 | 150 | 12 | 14% | 0% |
| | Through | 1,000 | 50 | 11 | 100 | 30 | 175 | 63 | 1% | 0% |
| SB | Through | 300 | 150 | 8 | 225 | 14 | 275 | 17 | 0% | 0% |
| | Through/Right | 300 | 150 | 8 | 175 | 18 | 175 | 29 | 0% | 4% |
| | | | | | | | | | | |

Intersection 13

Bordeaux Drive/Innovation Way

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left/Through | 375 | 175 | 19 | 325 | 31 | 375 | 8 | 9% | 0% |
| | Right Turn | 125 | 125 | 4 | 150 | 4 | 150 | 0 | 10% | 0% |
| NB | Left Turn | 325 | 350 | 83 | 525 | 91 | 550 | 60 | 35% | 0% |
| | Through/Right | 2,025 | 350 | 336 | 675 | 507 | 700 | 351 | 0% | 9% |
| SB | Left Turn | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | Through/Right | 725 | 100 | 14 | 175 | 27 | 225 | 44 | 9% | 0% |
| WB | Left/Through | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | Right Turn | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |

Arterial Level of Service: NB Mathilda Ave

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|--------------------|------|---------------|-----------------|-----------|----------------|
| Ahwanee Ave | 8 | 85.3 | 96.2 | 0.1 | 5 |
| | 7 | 52.7 | 65.1 | 0.2 | 8 |
| US 101 NB Ramps | 6 | 77.9 | 88.1 | 0.1 | 5 |
| Ross Dr | 5 | 59.2 | 70.7 | 0.1 | 8 |
| | 4 | 35.0 | 39.6 | 0.0 | 4 |
| SR 237 EB Off-Ramp | 43 | 1.5 | 5.8 | 0.0 | 20 |
| Mathilda Ave | 57 | 3.1 | 8.0 | 0.0 | 16 |
| Mathilda Ave | 3 | 19.2 | 23.3 | 0.0 | 6 |
| Innovation Way | 2 | 31.7 | 50.4 | 0.2 | 16 |
| 5th Ave | 1 | 14.8 | 34.0 | 0.2 | 25 |
| | 107 | 4.6 | 26.9 | 0.3 | 36 |
| Total | | 384.9 | 508.2 | 1.5 | 10 |

Arterial Level of Service: SB Mathilda Ave

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|-----------------|------|---------------|-----------------|-----------|----------------|
| 5th Ave | 1 | 14.6 | 35.9 | 0.3 | 27 |
| Innovation Way | 2 | 62.8 | 81.3 | 0.2 | 10 |
| | 3 | 38.8 | 68.8 | 0.2 | 11 |
| Ross Dr | 5 | 16.3 | 22.0 | 0.0 | 8 |
| US 101 NB Ramps | 6 | 16.7 | 28.2 | 0.1 | 19 |
| US 101 SB Ramps | 7 | 9.7 | 20.6 | 0.1 | 23 |
| Almanor Ave | 8 | 33.6 | 45.8 | 0.2 | 12 |
| San Aleso Ave | 201 | 4.3 | 15.7 | 0.1 | 32 |
| Total | | 196.7 | 318.4 | 1.4 | 15 |

Arterial Level of Service: NB Innovation Way

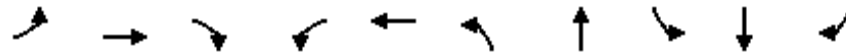
| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|------------------|------|---------------|-----------------|-----------|----------------|
| | 910 | 2.5 | 7.3 | 0.0 | 11 |
| | 53 | 0.6 | 5.4 | 0.0 | 27 |
| | 11 | 7.8 | 15.3 | 0.1 | 17 |
| | 200 | 3.0 | 19.8 | 0.2 | 29 |
| Juniper Driveway | 12 | 9.8 | 15.5 | 0.1 | 13 |
| Driveway | 217 | 2.3 | 5.5 | 0.0 | 24 |
| | 902 | 30.5 | 32.8 | 0.0 | 2 |
| Mathilda Ave | 2 | 20.9 | 22.6 | 0.0 | 4 |
| | 16 | 2.3 | 15.9 | 0.1 | 20 |
| Bordeaux Dr | 13 | 19.0 | 31.8 | 0.1 | 9 |
| Total | | 98.8 | 172.0 | 0.6 | 13 |

Arterial Level of Service: SB Innovation Way

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|------------------|------|---------------|-----------------|-----------|----------------|
| | 16 | - | - | 0.1 | - |
| Mathilda Ave | 2 | 217.8 | 229.3 | 0.1 | 1 |
| | 902 | 6.9 | 12.0 | 0.0 | 8 |
| Driveway | 217 | 1.1 | 3.0 | 0.0 | 24 |
| Juniper Driveway | 12 | 6.4 | 10.4 | 0.0 | 13 |
| | 200 | 2.0 | 8.5 | 0.1 | 24 |
| 11th Ave | 11 | 9.9 | 26.0 | 0.2 | 22 |
| | 53 | 2.9 | 10.4 | 0.1 | 25 |
| | 910 | 13.0 | 17.4 | 0.0 | 9 |
| Moffett Park Dr | 10 | 11.3 | 16.1 | 0.0 | 5 |
| Total | | 271.4 | 333.1 | 0.6 | 7 |

Lanes, Volumes, Timings
1: Mathilda Ave & 5th Ave

3/4/2016

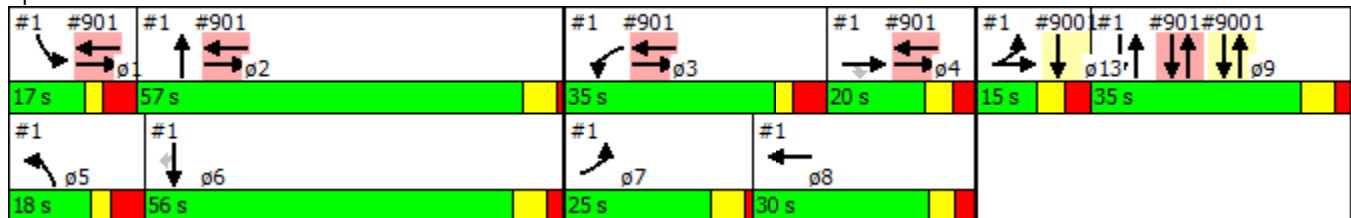


| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT | SBR | ø2 | ø7 |
|----------------------|------|------|--------|-------|-------|-------|-----|------|------|--------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 70 | 20 | 70 | 240 | 10 | 110 | 340 | 10 | 1110 | 10 | | |
| Turn Type | Prot | NA | custom | Prot | NA | Prot | NA | Prot | NA | custom | | |
| Protected Phases | 7 13 | 4 13 | | 3 | 8 | 5 | 2 9 | 1 | 6 9 | | 2 | 7 |
| Permitted Phases | | | 4 | | | | | | | 6 | | |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 5 | 2 | 1 | 6 | 6 | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 13.0 | 12.0 | 8.0 | 11.0 | | 10.0 | | 12.0 | 12.0 | 12.0 |
| Minimum Split (s) | | | 20.0 | 19.0 | 29.5 | 18.0 | | 17.0 | | 41.0 | 33.5 | 17.5 |
| Total Split (s) | | | 20.0 | 35.0 | 30.0 | 18.0 | | 17.0 | | 56.0 | 57.0 | 25.0 |
| Total Split (%) | | | 11.2% | 19.6% | 16.8% | 10.1% | | 9.5% | | 31.3% | 32% | 14% |
| Yellow Time (s) | | | 3.6 | 2.5 | 3.6 | 2.5 | | 2.5 | | 4.7 | 4.5 | 4.5 |
| All-Red Time (s) | | | 3.4 | 4.5 | 2.9 | 4.5 | | 4.5 | | 2.3 | 1.0 | 1.0 |
| Lost Time Adjust (s) | | | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | | 0.0 | | |
| Total Lost Time (s) | | | 7.0 | 7.0 | 6.5 | 7.0 | | 7.0 | | 7.0 | | |
| Lead/Lag | | | Lag | Lead | Lag | Lead | | Lead | | Lag | Lag | Lead |
| Lead-Lag Optimize? | | | Yes | Yes | Yes | Yes | | Yes | | Yes | Yes | Yes |
| Recall Mode | | | None | None | None | None | | None | | None | Min | None |

Intersection Summary

Cycle Length: 179
 Actuated Cycle Length: 107
 Natural Cycle: 160
 Control Type: Actuated-Uncoordinated

Splits and Phases: 1: Mathilda Ave & 5th Ave



| Lane Group | ø9 | ø13 |
|----------------------|------|------|
| Lane Configurations | | |
| Volume (vph) | | |
| Turn Type | | |
| Protected Phases | 9 | 13 |
| Permitted Phases | | |
| Detector Phase | | |
| Switch Phase | | |
| Minimum Initial (s) | 28.0 | 8.0 |
| Minimum Split (s) | 35.0 | 15.0 |
| Total Split (s) | 35.0 | 15.0 |
| Total Split (%) | 20% | 8% |
| Yellow Time (s) | 4.7 | 3.6 |
| All-Red Time (s) | 2.3 | 3.4 |
| Lost Time Adjust (s) | | |
| Total Lost Time (s) | | |
| Lead/Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes |
| Recall Mode | None | None |
| Intersection Summary | | |

Lanes, Volumes, Timings
 2: Mathilda Ave & Innovation Way

3/4/2016

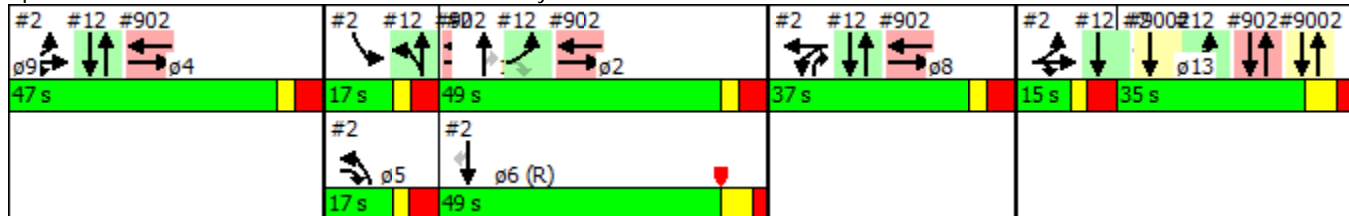


| Lane Group | EBT | EBR | WBL | WBT | NBL | NBT | NBR | SBL | SBT | SBR | ø2 | ø4 |
|----------------------|------|--------|-------|-------|------|-----|-------|------|------|------|------|------|
| Lane Configurations | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | ↖ ↗ | | |
| Volume (vph) | 200 | 1160 | 480 | 120 | 120 | 260 | 200 | 50 | 1320 | 50 | | |
| Turn Type | NA | pt+ov | Split | NA | Prot | NA | pm+ov | Prot | NA | Perm | | |
| Protected Phases | 4 13 | 4 13 5 | 8 | 8 | 5 | 2 9 | 8 | 1 | 6 9 | | 2 | 4 |
| Permitted Phases | | | | | | | 2 9 | | | | | 6 9 |
| Detector Phase | 4 | 4 | 8 | 8 | 5 | 2 | 8 | 1 | 6 | 6 | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 10.0 | 10.0 | 10.0 | | 10.0 | 7.0 | | | 12.0 | 14.0 |
| Minimum Split (s) | | | 35.0 | 35.0 | 17.0 | | 35.0 | 13.8 | | | 19.0 | 39.0 |
| Total Split (s) | | | 37.0 | 37.0 | 17.0 | | 37.0 | 17.0 | | | 49.0 | 47.0 |
| Total Split (%) | | | 18.5% | 18.5% | 8.5% | | 18.5% | 8.5% | | | 25% | 24% |
| Yellow Time (s) | | | 2.5 | 2.5 | 2.5 | | 2.5 | 2.5 | | | 2.5 | 2.5 |
| All-Red Time (s) | | | 4.5 | 4.5 | 4.5 | | 4.5 | 4.3 | | | 4.5 | 4.5 |
| Lost Time Adjust (s) | | | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | | | | |
| Total Lost Time (s) | | | 7.0 | 7.0 | 7.0 | | 7.0 | 6.8 | | | | |
| Lead/Lag | | | | | Lead | | | Lead | | | Lag | |
| Lead-Lag Optimize? | | | | | Yes | | | Yes | | | Yes | |
| Recall Mode | | | None | None | None | | None | None | | | None | None |

Intersection Summary

Cycle Length: 200
 Actuated Cycle Length: 200
 Offset: 0 (0%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 175
 Control Type: Actuated-Coordinated

Splits and Phases: 2: Mathilda Ave & Innovation Way



Lanes, Volumes, Timings
 2: Mathilda Ave & Innovation Way

3/4/2016

| Lane Group | ø6 | ø9 | ø13 |
|----------------------|-------|------|------|
| Lane Configurations | | | |
| Volume (vph) | | | |
| Turn Type | | | |
| Protected Phases | 6 | 9 | 13 |
| Permitted Phases | | | |
| Detector Phase | | | |
| Switch Phase | | | |
| Minimum Initial (s) | 12.0 | 28.0 | 8.0 |
| Minimum Split (s) | 30.0 | 35.0 | 15.0 |
| Total Split (s) | 49.0 | 35.0 | 15.0 |
| Total Split (%) | 25% | 18% | 8% |
| Yellow Time (s) | 4.7 | 4.7 | 2.5 |
| All-Red Time (s) | 2.3 | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | |
| Total Lost Time (s) | | | |
| Lead/Lag | Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes | Yes |
| Recall Mode | C-Max | None | None |
| Intersection Summary | | | |

Lanes, Volumes, Timings
 3: Mathilda Ave & SR 237 WB Off-Ramp

3/4/2016



| Lane Group | WBR | SBL | SBR2 | NEL | ø9 |
|----------------------|-------|-------|-------|-------|------|
| Lane Configurations | ↖ | ↙↘↗ | ↖ | ↙↘↗ | |
| Volume (vph) | 190 | 2110 | 850 | 390 | |
| Turn Type | Prot | Prot | Perm | Prot | |
| Protected Phases | 4 | 4 | | 2 | 9 |
| Permitted Phases | | | 4 | | |
| Detector Phase | 4 | 4 | 4 | 2 | |
| Switch Phase | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | 26.7 | 26.7 | 26.7 | 26.7 | 18.0 |
| Total Split (s) | 95.0 | 95.0 | 95.0 | 35.0 | 20.0 |
| Total Split (%) | 63.3% | 63.3% | 63.3% | 23.3% | 13% |
| Yellow Time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 2.0 |
| All-Red Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 0.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | 9.0 | 9.0 | 9.0 | 9.0 | |
| Lead/Lag | | | | | |
| Lead-Lag Optimize? | | | | | |
| Recall Mode | C-Max | C-Max | C-Max | None | Max |

Intersection Summary

Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 0 (0%), Referenced to phase 4:SBL, Start of Yellow, Master Intersection
 Natural Cycle: 110
 Control Type: Actuated-Coordinated

Splits and Phases: 3: Mathilda Ave & SR 237 WB Off-Ramp



Lanes, Volumes, Timings
 4: Mathilda Ave & SR 237 EB Off-Ramp

3/4/2016



| Lane Group | EBR | NBT | NBR2 | SWL | ø9 |
|----------------------|--------|-------|-------|-------|------|
| Lane Configurations | ↗ | ↑↑↑ | ↗ | ↑↑↑↑ | |
| Volume (vph) | 150 | 460 | 670 | 2510 | |
| Turn Type | custom | NA | Perm | Prot | |
| Protected Phases | 2 9 | 2 | | 4 | 9 |
| Permitted Phases | | | 2 | | |
| Detector Phase | 2 | 2 | 2 | 4 | |
| Switch Phase | | | | | |
| Minimum Initial (s) | | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | | 26.7 | 26.7 | 26.7 | 18.0 |
| Total Split (s) | | 35.0 | 35.0 | 95.0 | 20.0 |
| Total Split (%) | | 23.3% | 23.3% | 63.3% | 13% |
| Yellow Time (s) | | 3.0 | 3.0 | 3.0 | 2.0 |
| All-Red Time (s) | | 6.0 | 6.0 | 6.0 | 0.0 |
| Lost Time Adjust (s) | | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | | 9.0 | 9.0 | 9.0 | |
| Lead/Lag | | | | | |
| Lead-Lag Optimize? | | | | | |
| Recall Mode | | None | None | C-Max | Max |

Intersection Summary

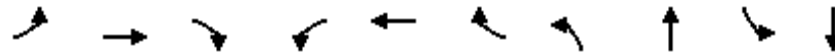
Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 0 (0%), Referenced to phase 4:SBL, Start of Yellow, Master Intersection
 Natural Cycle: 110
 Control Type: Actuated-Coordinated

Splits and Phases: 4: Mathilda Ave & SR 237 EB Off-Ramp



Lanes, Volumes, Timings
5: Mathilda Ave & Ross Dr

3/4/2016

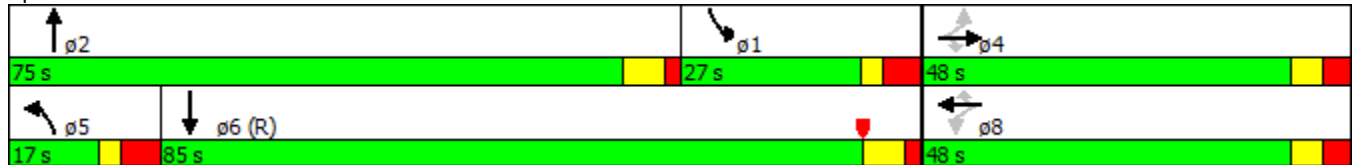


| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↖ | ↑ | ↗ | ↖ | ↑ | ↗ | ↖ | ↑↑↑↑ | ↗ | ↑↑↑ |
| Volume (vph) | 40 | 150 | 40 | 230 | 50 | 100 | 120 | 990 | 140 | 2460 |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | Prot | NA | Prot | NA |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | 1 | 6 |
| Permitted Phases | 4 | | 4 | 8 | | 8 | | | | |
| Detector Phase | 4 | 4 | 4 | 8 | 8 | 8 | 5 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 4.0 | 4.0 | 4.0 | 5.0 |
| Minimum Split (s) | 48.0 | 48.0 | 48.0 | 19.0 | 19.0 | 19.0 | 11.0 | 31.4 | 11.0 | 11.6 |
| Total Split (s) | 48.0 | 48.0 | 48.0 | 48.0 | 48.0 | 48.0 | 17.0 | 75.0 | 27.0 | 85.0 |
| Total Split (%) | 32.0% | 32.0% | 32.0% | 32.0% | 32.0% | 32.0% | 11.3% | 50.0% | 18.0% | 56.7% |
| Yellow Time (s) | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 2.5 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 3.4 | 3.4 | 3.4 | 3.4 | 3.4 | 3.4 | 4.5 | 1.7 | 4.5 | 1.9 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.4 | 7.0 | 6.6 |
| Lead/Lag | | | | | | | Lead | Lead | Lag | Lag |
| Lead-Lag Optimize? | | | | | | | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | Max | Max | Max | Max | None | None | C-Max |

Intersection Summary

Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 140 (93%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 135
 Control Type: Actuated-Coordinated

Splits and Phases: 5: Mathilda Ave & Ross Dr



Lanes, Volumes, Timings
 6: Mathilda Ave & US 101 NB Ramps

3/4/2016



| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↖↖ | ↖↖ | ↑↑↑ | ↖ | ↖ | ↑↑↑ |
| Volume (vph) | 800 | 220 | 1160 | 270 | 40 | 2690 |
| Turn Type | Prot | pm+ov | NA | Perm | Prot | NA |
| Protected Phases | 8 | 1 | 2 | | 1 | 6 |
| Permitted Phases | | 8 | | 2 | | |
| Detector Phase | 8 | 1 | 2 | 2 | 1 | 6 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 8.0 | 4.0 | 8.0 | 8.0 | 4.0 | 4.0 |
| Minimum Split (s) | 14.9 | 9.7 | 39.9 | 39.9 | 9.7 | 10.9 |
| Total Split (s) | 48.0 | 18.0 | 84.0 | 84.0 | 18.0 | 102.0 |
| Total Split (%) | 32.0% | 12.0% | 56.0% | 56.0% | 12.0% | 68.0% |
| Yellow Time (s) | 4.7 | 3.5 | 4.7 | 4.7 | 3.5 | 4.7 |
| All-Red Time (s) | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.9 | 5.7 | 6.9 | 6.9 | 5.7 | 6.9 |
| Lead/Lag | | Lead | Lag | Lag | Lead | |
| Lead-Lag Optimize? | | Yes | Yes | Yes | Yes | |
| Recall Mode | None | None | None | None | None | C-Max |

Intersection Summary

Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 120 (80%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 80
 Control Type: Actuated-Coordinated

Splits and Phases: 6: Mathilda Ave & US 101 NB Ramps



Lanes, Volumes, Timings
 7: Mathilda Ave & US 101 SB Ramps

3/4/2016



| Lane Group | EBL | EBR | NBT | NBR | SBT |
|----------------------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | |
| Volume (vph) | 80 | 500 | 1350 | 530 | 2350 |
| Turn Type | Prot | Prot | NA | Perm | NA |
| Protected Phases | 7 | 7 | 2 | | 6 |
| Permitted Phases | | | | 2 | |
| Detector Phase | 7 | 7 | 2 | 2 | 6 |
| Switch Phase | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | 10.9 | 10.9 | 22.9 | 22.9 | 22.9 |
| Total Split (s) | 35.0 | 35.0 | 115.0 | 115.0 | 115.0 |
| Total Split (%) | 23.3% | 23.3% | 76.7% | 76.7% | 76.7% |
| Yellow Time (s) | 4.7 | 4.7 | 4.7 | 4.7 | 4.7 |
| All-Red Time (s) | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.9 | 6.9 | 6.9 | 6.9 | 6.9 |
| Lead/Lag | | | | | |
| Lead-Lag Optimize? | | | | | |
| Recall Mode | None | None | None | None | C-Max |

Intersection Summary

Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 122 (81%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 120
 Control Type: Actuated-Coordinated

Splits and Phases: 7: Mathilda Ave & US 101 SB Ramps



Lanes, Volumes, Timings
 8: Mathilda Ave & Almanor Ave/Ahwanee Ave

3/4/2016

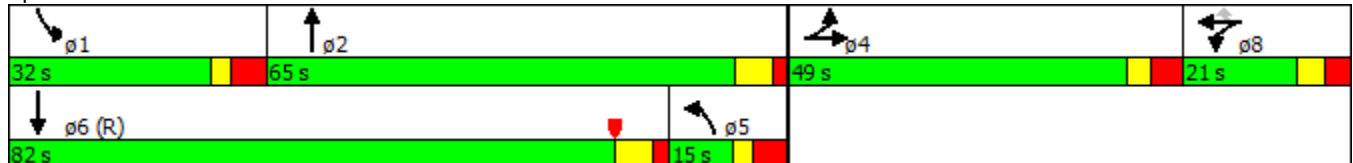


| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|------|-------|-------|-------|
| Lane Configurations | ↖↗ | ↖ | ↖ | ↖ | ↖ | ↖ | ↑↑↑ | ↖ | ↑↑↑ |
| Volume (vph) | 310 | 30 | 50 | 10 | 190 | 60 | 1380 | 180 | 2600 |
| Turn Type | Split | NA | Split | NA | Perm | Prot | NA | Prot | NA |
| Protected Phases | 4 | 4 | 8 | 8 | | 5 | 2 | 1 | 6 |
| Permitted Phases | | | | | 8 | | | | |
| Detector Phase | 4 | 4 | 8 | 8 | 8 | 5 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | | |
| Minimum Initial (s) | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 12.0 | 8.0 | 12.0 |
| Minimum Split (s) | 49.0 | 49.0 | 15.0 | 15.0 | 15.0 | 15.0 | 36.7 | 15.0 | 27.7 |
| Total Split (s) | 49.0 | 49.0 | 21.0 | 21.0 | 21.0 | 15.0 | 65.0 | 32.0 | 82.0 |
| Total Split (%) | 29.3% | 29.3% | 12.6% | 12.6% | 12.6% | 9.0% | 38.9% | 19.2% | 49.1% |
| Yellow Time (s) | 2.8 | 2.8 | 3.6 | 3.6 | 3.6 | 2.5 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 4.2 | 4.2 | 3.4 | 3.4 | 3.4 | 4.5 | 2.0 | 4.5 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.7 | 7.0 | 6.7 |
| Lead/Lag | | | | | | Lag | Lag | Lead | Lead |
| Lead-Lag Optimize? | | | | | | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | None | None | None | C-Max |

Intersection Summary

Cycle Length: 167
 Actuated Cycle Length: 167
 Offset: 0 (0%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 140
 Control Type: Actuated-Coordinated

Splits and Phases: 8: Mathilda Ave & Almanor Ave/Ahwanee Ave



Lanes, Volumes, Timings
 9: US 101 On-Ramp & Moffett Park Dr

3/4/2016

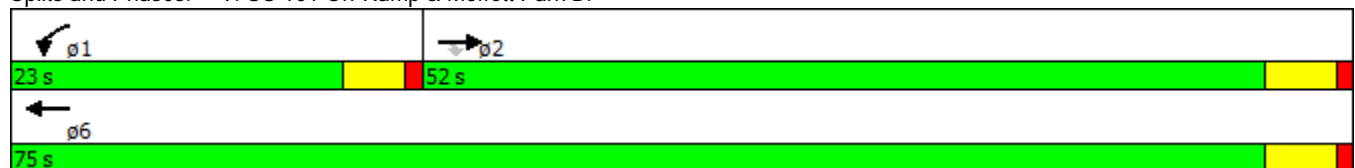


| Lane Group | EBT | EBR | WBL | WBT |
|----------------------|-------|-------|-------|--------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ |
| Volume (vph) | 790 | 90 | 230 | 220 |
| Turn Type | NA | Perm | Prot | NA |
| Protected Phases | 2 | | 1 | 6 |
| Permitted Phases | | 2 | | |
| Detector Phase | 2 | 2 | 1 | 6 |
| Switch Phase | | | | |
| Minimum Initial (s) | 15.0 | 15.0 | 6.0 | 15.0 |
| Minimum Split (s) | 20.0 | 20.0 | 10.5 | 20.0 |
| Total Split (s) | 52.0 | 52.0 | 23.0 | 75.0 |
| Total Split (%) | 69.3% | 69.3% | 30.7% | 100.0% |
| Yellow Time (s) | 4.0 | 4.0 | 3.5 | 4.0 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.0 | 5.0 | 4.5 | 5.0 |
| Lead/Lag | Lag | Lag | Lead | |
| Lead-Lag Optimize? | | | | |
| Recall Mode | Min | Min | None | Min |

Intersection Summary

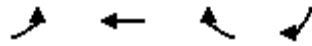
Cycle Length: 75
 Actuated Cycle Length: 52.2
 Natural Cycle: 50
 Control Type: Semi Act-Uncoord

Splits and Phases: 9: US 101 On-Ramp & Moffett Park Dr



Lanes, Volumes, Timings
 10: Moffett Park Dr & Innovation Way

3/4/2016

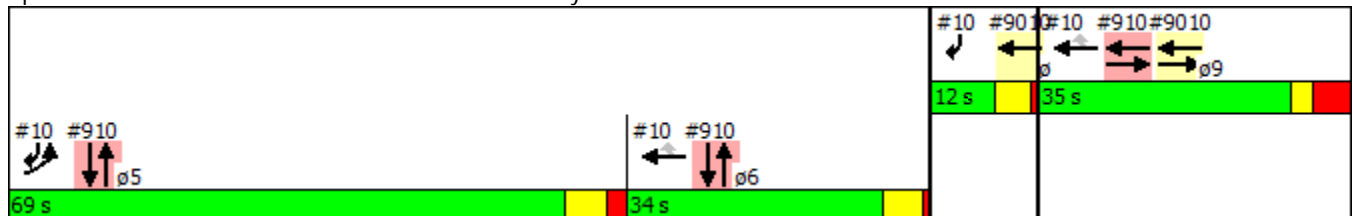


| Lane Group | EBL | WBT | WBR | SBR | ø4 | ø6 | ø9 |
|----------------------|-------|-----|------|-------|------|------|------|
| Lane Configurations | ↗↘ | ↑↑ | ↗ | ↗↘ | | | |
| Volume (vph) | 790 | 240 | 90 | 210 | | | |
| Turn Type | Prot | NA | Perm | pt+ov | | | |
| Protected Phases | 5 | 6 9 | | 4 5 | 4 | 6 | 9 |
| Permitted Phases | | | 6 9 | | | | |
| Detector Phase | 5 | 6 | 6 9 | 5 | | | |
| Switch Phase | | | | | | | |
| Minimum Initial (s) | 8.0 | | | | 4.0 | 10.0 | 28.0 |
| Minimum Split (s) | 15.0 | | | | 9.0 | 27.5 | 35.0 |
| Total Split (s) | 69.0 | | | | 12.0 | 34.0 | 35.0 |
| Total Split (%) | 46.0% | | | | 8% | 23% | 23% |
| Yellow Time (s) | 4.7 | | | | 4.0 | 4.5 | 2.5 |
| All-Red Time (s) | 2.3 | | | | 1.0 | 1.0 | 4.5 |
| Lost Time Adjust (s) | 0.0 | | | | | | |
| Total Lost Time (s) | 7.0 | | | | | | |
| Lead/Lag | Lead | | | | | Lag | |
| Lead-Lag Optimize? | Yes | | | | | Yes | |
| Recall Mode | Max | | | | None | Min | None |

Intersection Summary

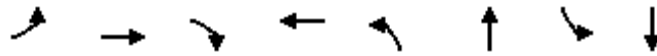
Cycle Length: 150
 Actuated Cycle Length: 132.7
 Natural Cycle: 100
 Control Type: Semi Act-Uncoord

Splits and Phases: 10: Moffett Park Dr & Innovation Way



Lanes, Volumes, Timings
 11: Innovation Way & 11th Ave

3/4/2016



| Lane Group | EBL | EBT | EBR | WBT | NBL | NBT | SBL | SBT |
|---------------------|-----|------|-----|------|-----|------|-----|------|
| Lane Configurations | | | | | | | | |
| Volume (vph) | 390 | 0 | 130 | 0 | 10 | 840 | 80 | 60 |
| Sign Control | | Stop | | Stop | | Stop | | Stop |

Intersection Summary

Control Type: Unsignalized

Lanes, Volumes, Timings
 12: Innovation Way & Juniper Driveway

3/4/2016

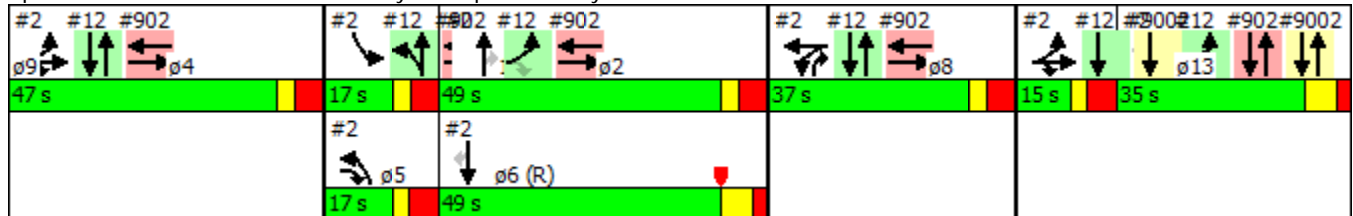


| Lane Group | EBL | EBR | NBL | NBT | SBT | ø2 | ø4 | ø5 | ø6 | ø8 | ø9 | ø13 |
|----------------------|------|------|------|-------|--------|------|------|------|-------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 370 | 40 | 40 | 1200 | 220 | | | | | | | |
| Turn Type | Prot | Perm | Prot | NA | NA | | | | | | | |
| Protected Phases | 2 9 | | 1 | 1 4 8 | 4 8 13 | 2 | 4 | 5 | 6 | 8 | 9 | 13 |
| Permitted Phases | | 2 9 | | | | | | | | | | |
| Detector Phase | 2 | 2 | 1 | 1 4 8 | 4 8 | | | | | | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 7.0 | | | 12.0 | 14.0 | 10.0 | 12.0 | 10.0 | 28.0 | 8.0 |
| Minimum Split (s) | | | 13.8 | | | 19.0 | 39.0 | 17.0 | 30.0 | 35.0 | 35.0 | 15.0 |
| Total Split (s) | | | 17.0 | | | 49.0 | 47.0 | 17.0 | 49.0 | 37.0 | 35.0 | 15.0 |
| Total Split (%) | | | 8.5% | | | 25% | 24% | 9% | 25% | 19% | 18% | 8% |
| Yellow Time (s) | | | 2.5 | | | 2.5 | 2.5 | 2.5 | 4.7 | 2.5 | 4.7 | 2.5 |
| All-Red Time (s) | | | 4.3 | | | 4.5 | 4.5 | 4.5 | 2.3 | 4.5 | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | 0.0 | | | | | | | | | |
| Total Lost Time (s) | | | 6.8 | | | | | | | | | |
| Lead/Lag | | | Lead | | | Lag | | Lead | Lag | | Lag | Lead |
| Lead-Lag Optimize? | | | Yes | | | Yes | | Yes | Yes | | Yes | Yes |
| Recall Mode | | | None | | | None | None | None | C-Max | None | None | None |

Intersection Summary

Cycle Length: 200
 Actuated Cycle Length: 200
 Offset: 0 (0%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 175
 Control Type: Actuated-Coordinated

Splits and Phases: 12: Innovation Way & Juniper Driveway



Lanes, Volumes, Timings
 13: Bordeaux Dr & Innovation Way

3/4/2016

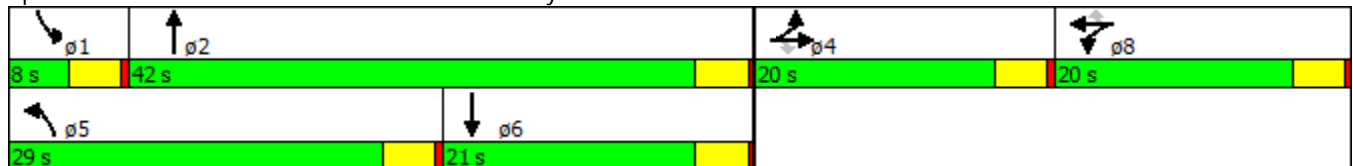


| Lane Group | EBT | EBR | NBL | NBT | SBT | ø1 | ø8 |
|----------------------|-------|-------|-------|-------|-------|------|------|
| Lane Configurations | ↖ | ↗ | ↖ | ↗ | ↗ | | |
| Volume (vph) | 10 | 140 | 450 | 30 | 140 | | |
| Turn Type | NA | Perm | Prot | NA | NA | | |
| Protected Phases | 4 | | 5 | 2 | 6 | 1 | 8 |
| Permitted Phases | | 4 | | | | | |
| Detector Phase | 4 | 4 | 5 | 2 | 6 | | |
| Switch Phase | | | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 8.0 | 20.0 |
| Total Split (s) | 20.0 | 20.0 | 29.0 | 42.0 | 21.0 | 8.0 | 20.0 |
| Total Split (%) | 22.2% | 22.2% | 32.2% | 46.7% | 23.3% | 9% | 22% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | | |
| Total Lost Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | | |
| Lead/Lag | | | Lead | Lag | Lag | Lead | |
| Lead-Lag Optimize? | | | Yes | Yes | Yes | Yes | |
| Recall Mode | None | None | None | None | None | None | None |

Intersection Summary

Cycle Length: 90
 Actuated Cycle Length: 52.3
 Natural Cycle: 90
 Control Type: Actuated-Uncoordinated

Splits and Phases: 13: Bordeaux Dr & Innovation Way



**SimTraffic Post-Processor
Average Results from 10 Runs
Network Performance**

**Mathilda Avenue Improvements
2018 Build Alternative 2
PM Peak Hour**

| Performance Measure | Average | Std. Dev. | Minimum | Maximum |
|---------------------------------|---------|-----------|---------|---------|
| Average Delay (seconds) | 347.1 | 14.6 | 319.7 | 363.0 |
| Total Delay (hours) | 1,107 | 56 | 1,002 | 1,181 |
| Average Stopped Delay (seconds) | 287.0 | 15.0 | 260.4 | 303.6 |
| Total Stopped Delay (hours) | 915 | 55 | 816 | 984 |
| Total Stops | 36,976 | 945 | 34,617 | 38,164 |
| Average Stops | 3.22 | 0.07 | 3.07 | 3.30 |
| Total Distance Traveled (miles) | 40,585 | 357 | 40,187 | 41,345 |
| Average Speed (mph) | 19.2 | 0.4 | 19.0 | 20.0 |
| Total Travel Time (hours) | 2,139.3 | 61.6 | 2,025.7 | 2,229.0 |
| Vehicles Entered | 9,739 | 120 | 9,569 | 9,974 |
| Vehicles Exited | 8,936 | 54 | 8,827 | 8,988 |
| Percent Demand Served | 91.8% | 1.0% | 90.1% | 93.0% |
| Fuel Used (gallons) | 1,268 | 20 | 1,234 | 1,303 |
| HC Emissions (grams) | 16,875 | 840 | 15,847 | 18,120 |
| CO Emissions (grams) | 463,624 | 14,946 | 446,547 | 485,264 |
| NOx Emissions (grams) | 64,966 | 2,137 | 62,528 | 67,888 |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2018 Build Alternative 2
PM Peak Hour

Intersection 1 Mathilda Avenue/5th Avenue Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 110 | 95 | 86.7% | 60.1 | 8.8 | E |
| | Through | 340 | 306 | 89.9% | 15.2 | 2.6 | B |
| | Right Turn | 40 | 35 | 88.5% | 8.3 | 2.8 | A |
| | Subtotal | 490 | 437 | 89.1% | 24.5 | 3.4 | C |
| SB | Left Turn | 10 | 8 | 79.0% | 230.8 | 101.6 | F |
| | Through | 1,110 | 929 | 83.7% | 269.3 | 107.1 | F |
| | Right Turn | 10 | 10 | 100.0% | 210.0 | 105.1 | F |
| | Subtotal | 1,130 | 947 | 83.8% | 268.6 | 106.5 | F |
| EB | Left Turn | 70 | 74 | 106.3% | 35.5 | 2.7 | D |
| | Through | 20 | 23 | 116.5% | 56.0 | 9.6 | E |
| | Right Turn | 70 | 66 | 94.7% | 19.7 | 2.7 | B |
| | Subtotal | 160 | 164 | 102.5% | 32.0 | 3.1 | C |
| WB | Left Turn | 240 | 217 | 90.5% | 205.2 | 111.2 | F |
| | Through | 10 | 10 | 100.0% | 211.5 | 112.5 | F |
| | Right Turn | 30 | 27 | 88.3% | 164.9 | 104.3 | F |
| | Subtotal | 280 | 254 | 90.6% | 200.7 | 109.4 | F |
| Total | | 2,060 | 1,801 | 87.4% | 177.3 | 62.2 | F |

Intersection 2 Mathilda Avenue/Innovation Way Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 120 | 111 | 92.1% | 85.4 | 9.0 | F |
| | Through | 260 | 256 | 98.3% | 37.1 | 5.9 | D |
| | Right Turn | 200 | 194 | 97.0% | 13.8 | 2.0 | B |
| | Subtotal | 580 | 560 | 96.6% | 38.7 | 3.2 | D |
| SB | Left Turn | 50 | 43 | 85.0% | 260.2 | 36.8 | F |
| | Through | 1,320 | 1,083 | 82.0% | 285.7 | 27.1 | F |
| | Right Turn | 50 | 47 | 93.4% | 320.7 | 25.3 | F |
| | Subtotal | 1,420 | 1,172 | 82.5% | 286.2 | 26.7 | F |
| EB | Left Turn | 210 | 165 | 78.5% | 60.0 | 3.5 | E |
| | Through | 200 | 160 | 80.0% | 61.4 | 5.5 | E |
| | Right Turn | 1,160 | 923 | 79.6% | 58.0 | 3.7 | E |
| | Subtotal | 1,570 | 1,248 | 79.5% | 58.7 | 3.9 | E |
| WB | Left Turn | 480 | 388 | 80.8% | 197.3 | 12.9 | F |
| | Through | 120 | 94 | 78.1% | 214.2 | 20.1 | F |
| | Right Turn | 20 | 16 | 80.5% | 202.8 | 22.0 | F |
| | Subtotal | 620 | 498 | 80.3% | 200.8 | 14.1 | F |
| Total | | 4,190 | 3,478 | 83.0% | 152.2 | 8.1 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2018 Build Alternative 2
PM Peak Hour

Intersection 3 Mathilda Avenue/Moffett Park Drive-SR 237 WB Ramps Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 190 | 180 | 94.5% | 1.9 | 0.6 | A |
| | Through | 390 | 373 | 95.7% | 38.1 | 2.1 | D |
| | Right Turn | | | | | | |
| | Subtotal | 580 | 553 | 95.3% | 26.3 | 1.6 | C |
| SB | Left Turn | | | | | | |
| | Through | 2,110 | 1,697 | 80.4% | 50.9 | 6.5 | D |
| | Right Turn | 850 | 692 | 81.4% | 97.4 | 7.3 | F |
| | Subtotal | 2,960 | 2,389 | 80.7% | 64.4 | 6.7 | E |
| EB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| WB | Left Turn | 760 | 740 | 97.4% | 176.0 | 48.4 | F |
| | Through | | | | | | |
| | Right Turn | 190 | 187 | 98.3% | 38.0 | 17.6 | D |
| | Subtotal | 950 | 927 | 97.6% | 148.2 | 42.2 | F |
| Total | | 4,490 | 3,869 | 86.8% | 79.0 | 14.5 | E |

Intersection 4 Mathilda Avenue/SR 237 EB On-Ramp Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | 460 | 456 | 99.1% | 74.9 | 2.5 | E |
| | Right Turn | 670 | 671 | 100.2% | 4.5 | 0.4 | A |
| | Subtotal | 1,130 | 1,127 | 99.8% | 33.0 | 1.2 | C |
| SB | Left Turn | 360 | 294 | 81.8% | 5.2 | 0.2 | A |
| | Through | 2,510 | 2,141 | 85.3% | 28.1 | 1.2 | C |
| | Right Turn | | | | | | |
| | Subtotal | 2,870 | 2,435 | 84.9% | 25.3 | 1.1 | C |
| EB | Left Turn | 120 | 97 | 80.6% | 171.0 | 127.9 | F |
| | Through | | | | | | |
| | Right Turn | 150 | 92 | 61.6% | 1042.9 | 334.5 | F |
| | Subtotal | 270 | 189 | 71.3% | 597.0 | 228.9 | F |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 4,270 | 3,752 | 88.7% | 56.4 | 12.6 | E |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2018 Build Alternative 2
PM Peak Hour

Intersection 5 Mathilda Avenue/Ross Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 120 | 120 | 100.3% | 168.8 | 43.2 | F |
| | Through | 990 | 993 | 100.3% | 50.8 | 14.6 | D |
| | Right Turn | 270 | 269 | 99.4% | 80.6 | 27.7 | F |
| | Subtotal | 1,380 | 1,382 | 100.1% | 66.9 | 17.8 | E |
| SB | Left Turn | 140 | 125 | 89.2% | 55.0 | 5.6 | D |
| | Through | 2,460 | 2,053 | 83.5% | 25.8 | 1.5 | C |
| | Right Turn | 60 | 51 | 85.5% | 22.6 | 4.6 | C |
| | Subtotal | 2,660 | 2,230 | 83.8% | 27.4 | 1.5 | C |
| EB | Left Turn | 40 | 38 | 94.3% | 47.6 | 6.5 | D |
| | Through | 150 | 153 | 102.0% | 46.4 | 4.2 | D |
| | Right Turn | 40 | 42 | 103.8% | 27.4 | 5.3 | C |
| | Subtotal | 230 | 232 | 101.0% | 43.1 | 4.0 | D |
| WB | Left Turn | 230 | 208 | 90.6% | 260.1 | 144.3 | F |
| | Through | 50 | 44 | 87.2% | 241.4 | 143.7 | F |
| | Right Turn | 100 | 92 | 92.0% | 231.0 | 152.3 | F |
| | Subtotal | 380 | 344 | 90.5% | 250.0 | 146.2 | F |
| Total | | 4,650 | 4,188 | 90.1% | 59.5 | 13.2 | E |

Intersection 6 Mathilda Avenue/US 101 NB Ramps Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | 1,160 | 1,168 | 100.7% | 18.4 | 4.3 | B |
| | Right Turn | 270 | 271 | 100.2% | 5.2 | 0.7 | A |
| | Subtotal | 1,430 | 1,438 | 100.6% | 15.9 | 3.6 | B |
| SB | Left Turn | 40 | 32 | 80.0% | 75.5 | 6.6 | E |
| | Through | 2,690 | 2,265 | 84.2% | 54.9 | 4.2 | D |
| | Right Turn | | | | | | |
| | Subtotal | 2,730 | 2,297 | 84.1% | 55.2 | 4.1 | E |
| EB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| WB | Left Turn | 800 | 806 | 100.8% | 99.7 | 20.2 | F |
| | Through | | | | | | |
| | Right Turn | 220 | 218 | 98.9% | 85.2 | 20.2 | F |
| | Subtotal | 1,020 | 1,024 | 100.4% | 96.6 | 20.3 | F |
| Total | | 5,180 | 4,759 | 91.9% | 52.3 | 6.1 | D |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2018 Build Alternative 2
PM Peak Hour

Intersection 7 Mathilda Avenue/US 101 SB Ramps Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | 1,350 | 1,352 | 100.1% | 7.6 | 1.7 | A |
| | Right Turn | 530 | 551 | 103.9% | 8.2 | 0.5 | A |
| | Subtotal | 1,880 | 1,903 | 101.2% | 7.8 | 1.3 | A |
| SB | Left Turn | | | | | | |
| | Through | 2,350 | 2,110 | 89.8% | 8.2 | 0.5 | A |
| | Right Turn | 1,140 | 957 | 83.9% | 17.1 | 2.7 | B |
| | Subtotal | 3,490 | 3,067 | 87.9% | 10.9 | 1.1 | B |
| EB | Left Turn | 80 | 81 | 101.6% | 82.0 | 4.8 | F |
| | Through | | | | | | |
| | Right Turn | 500 | 499 | 99.9% | 23.2 | 0.9 | C |
| | Subtotal | 580 | 581 | 100.1% | 31.5 | 1.3 | C |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 5,950 | 5,550 | 93.3% | 12.0 | 0.8 | B |

Intersection 8 Mathilda Avenue-US 101 On-Ramp/Almanor Avenue-Ahwanee Avenue Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 60 | 65 | 108.3% | 95.5 | 10.2 | F |
| | Through | 1,380 | 1,394 | 101.0% | 45.5 | 1.6 | D |
| | Right Turn | 40 | 40 | 99.3% | 33.8 | 2.5 | C |
| | Subtotal | 1,480 | 1,499 | 101.3% | 47.3 | 1.7 | D |
| SB | Left Turn | 180 | 167 | 92.9% | 82.6 | 3.8 | F |
| | Through | 2,600 | 2,375 | 91.4% | 29.6 | 2.6 | C |
| | Right Turn | 70 | 64 | 91.7% | 23.5 | 3.2 | C |
| | Subtotal | 2,850 | 2,607 | 91.5% | 32.9 | 2.4 | C |
| EB | Left Turn | 310 | 320 | 103.1% | 72.2 | 2.5 | E |
| | Through | 30 | 35 | 115.0% | 72.1 | 6.9 | E |
| | Right Turn | 70 | 73 | 103.6% | 47.8 | 4.1 | D |
| | Subtotal | 410 | 427 | 104.0% | 68.0 | 2.4 | E |
| WB | Left Turn | 50 | 50 | 99.4% | 61.3 | 7.3 | E |
| | Through | 10 | 11 | 114.0% | 61.5 | 7.8 | E |
| | Right Turn | 190 | 189 | 99.4% | 8.6 | 0.7 | A |
| | Subtotal | 250 | 250 | 100.0% | 21.5 | 2.5 | C |
| Total | | 4,990 | 4,782 | 95.8% | 40.0 | 1.6 | D |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2018 Build Alternative 2
PM Peak Hour

Intersection 9 Innovation Way-US 101 On-Ramp/Moffett Park Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| EB | Left Turn | | | | | | |
| | Through | 790 | 718 | 90.9% | 49.6 | 26.8 | D |
| | Right Turn | 90 | 85 | 94.9% | 24.6 | 12.8 | C |
| | Subtotal | 880 | 804 | 91.3% | 47.0 | 25.3 | D |
| WB | Left Turn | 230 | 221 | 96.1% | 26.6 | 5.5 | C |
| | Through | 220 | 218 | 99.0% | 2.4 | 0.3 | A |
| | Right Turn | | | | | | |
| | Subtotal | 450 | 439 | 97.5% | 14.6 | 3.0 | B |
| Total | | 1,330 | 1,242 | 93.4% | 35.2 | 17.1 | D |

Intersection 10 Innovation Way/Moffett Park Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | 210 | 201 | 95.8% | 11.7 | 2.4 | B |
| | Subtotal | 210 | 201 | 95.8% | 11.7 | 2.4 | B |
| EB | Left Turn | 790 | 665 | 84.1% | 165.7 | 81.8 | F |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | 790 | 665 | 84.1% | 165.7 | 81.8 | F |
| WB | Left Turn | | | | | | |
| | Through | 240 | 239 | 99.6% | 29.6 | 3.3 | C |
| | Right Turn | 90 | 44 | 48.9% | 67.3 | 26.7 | E |
| | Subtotal | 330 | 283 | 85.8% | 35.5 | 5.4 | D |
| Total | | 1,330 | 1,149 | 86.4% | 105.7 | 48.0 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2018 Build Alternative 2
PM Peak Hour

Intersection 11 Innovation Way/11th Avenue All-way Stop

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | 650 | 77.4% | 131.5 | 38.5 | F |
| | Through | 840 | 650 | 77.4% | 131.5 | 38.5 | F |
| | Right Turn | 20 | 17 | 86.0% | 127.3 | 37.0 | F |
| | Subtotal | 860 | 668 | 77.6% | 131.3 | 38.4 | F |
| SB | Left Turn | 80 | 71 | 88.1% | 27.4 | 4.4 | D |
| | Through | 60 | 56 | 92.5% | 18.0 | 4.4 | C |
| | Right Turn | 120 | 106 | 88.2% | 14.6 | 3.2 | B |
| | Subtotal | 260 | 232 | 89.2% | 19.3 | 3.2 | C |
| EB | Left Turn | 390 | 387 | 99.1% | 66.5 | 11.7 | F |
| | Through | | | | | | |
| | Right Turn | 130 | 126 | 97.2% | 24.5 | 2.9 | C |
| | Subtotal | 520 | 513 | 98.6% | 56.2 | 9.5 | F |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | 10 | 9 | 92.0% | 37.2 | 13.6 | E |
| | Subtotal | 10 | 9 | 92.0% | 37.2 | 13.6 | E |
| Total | | 1,650 | 1,422 | 86.2% | 85.0 | 19.3 | F |

Intersection 12 Innovation Way/Juniper Networks Driveway Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 40 | 35 | 88.0% | 254.1 | 23.4 | F |
| | Through | 1,200 | 996 | 83.0% | 231.4 | 22.1 | F |
| | Right Turn | | | | | | |
| | Subtotal | 1,240 | 1,031 | 83.2% | 232.2 | 22.0 | F |
| SB | Left Turn | | | | | | |
| | Through | 220 | 193 | 87.7% | 56.9 | 5.1 | E |
| | Right Turn | 70 | 58 | 83.1% | 43.3 | 6.4 | D |
| | Subtotal | 290 | 251 | 86.6% | 53.7 | 5.2 | D |
| EB | Left Turn | 370 | 251 | 67.7% | 809.8 | 308.3 | F |
| | Through | | | | | | |
| | Right Turn | 40 | 41 | 103.3% | 108.1 | 45.8 | F |
| | Subtotal | 410 | 292 | 71.2% | 707.8 | 266.4 | F |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 1,940 | 1,574 | 81.1% | 288.3 | 46.6 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2018 Build Alternative 2
PM Peak Hour

Intersection 13 Bordeaux Drive/Innovation Way Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 450 | 340 | 75.4% | 777.1 | 291.4 | F |
| | Through | 30 | 23 | 77.0% | 664.0 | 284.1 | F |
| | Right Turn | | | | | | |
| | Subtotal | 480 | 363 | 75.5% | 769.8 | 290.7 | F |
| SB | Left Turn | | | | | | |
| | Through | 140 | 131 | 93.3% | 219.0 | 79.6 | F |
| | Right Turn | 160 | 148 | 92.4% | 220.7 | 77.2 | F |
| | Subtotal | 300 | 279 | 92.8% | 219.8 | 78.0 | F |
| EB | Left Turn | 30 | 27 | 91.0% | 26.9 | 5.0 | C |
| | Through | 10 | 10 | 100.0% | 27.9 | 3.8 | C |
| | Right Turn | 140 | 120 | 85.5% | 8.5 | 0.7 | A |
| | Subtotal | 180 | 157 | 87.2% | 13.0 | 2.0 | B |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 960 | 798 | 83.1% | 427.3 | 141.5 | F |

Intersection 1 Mathilda Avenue/5th Avenue Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 625 | 75 | 14 | 125 | 22 | 175 | 20 | 6% | 0% |
| | Through | 625 | 50 | 4 | 75 | 6 | 75 | 12 | 0% | 0% |
| | Right Turn | 625 | 50 | 7 | 75 | 13 | 100 | 14 | 0% | 0% |
| NB | Left Turn | 425 | 75 | 6 | 125 | 10 | 125 | 24 | 0% | 0% |
| | Through | 1,125 | 50 | 6 | 125 | 11 | 150 | 25 | 0% | 0% |
| | Through/Right | 1,125 | 50 | 8 | 125 | 13 | 150 | 17 | 0% | 0% |
| SB | Left Turn | 250 | 50 | 18 | 150 | 65 | 300 | 1 | 0% | 0% |
| | Through | 1,325 | 800 | 247 | 1,450 | 352 | 1,350 | 224 | 67% | 13% |
| | Right Turn | 250 | 50 | 29 | 200 | 92 | 275 | 89 | 0% | 0% |
| WB | Left Turn | 925 | 350 | 167 | 675 | 362 | 700 | 254 | 75% | 6% |
| | Through/Right | 75 | 50 | 6 | 100 | 6 | 100 | 0 | 7% | 0% |

Intersection 2 Mathilda Avenue/Innovation Way Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|--------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left/Through | 225 | 250 | 5 | 350 | 10 | 350 | 15 | 0% | 45% |
| | Right Turn | 225 | 275 | 6 | 350 | 9 | 325 | 21 | 0% | 33% |
| NB | Left Turn | 725 | 75 | 9 | 125 | 21 | 150 | 34 | 0% | 0% |
| | Through | 975 | 100 | 11 | 175 | 19 | 200 | 39 | 0% | 0% |
| | Right Turn | 975 | 75 | 14 | 150 | 27 | 200 | 32 | 0% | 0% |
| SB | Left Turn | 75 | 75 | 12 | 150 | 22 | 150 | 0 | 14% | 0% |
| | Through | 975 | 1,125 | 82 | 1,275 | 90 | 1,200 | 16 | 82% | 37% |
| | Right Turn | 225 | 175 | 24 | 375 | 19 | 275 | 0 | 0% | 0% |
| WB | Left Turn | 425 | 775 | 3 | 800 | 6 | 800 | 5 | 25% | 48% |
| | Shared | 225 | 250 | 1 | 250 | 3 | 250 | 0 | 73% | 0% |

Intersection 3

Mathilda Avenue/Moffett Park Drive-SR 237 WB Ramps

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NB | Left Turn | 350 | 25 | 2 | 25 | 16 | 25 | 36 | 0% | 0% |
| | Through | 400 | 125 | 6 | 175 | 10 | 175 | 19 | 0% | 0% |
| SB | Through | 975 | 950 | 72 | 1,200 | 98 | 1,125 | 151 | 19% | 5% |
| WB | Left Turn | 1,075 | 650 | 154 | 975 | 232 | 1,025 | 240 | 13% | 0% |
| | Right Turn | 550 | 275 | 117 | 650 | 175 | 700 | 151 | 0% | 0% |
| | | | | | | | | | | |

Intersection 4

Mathilda Avenue/SR 237 EB On-Ramp

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|--------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,050 | 1,025 | 324 | 1,975 | 429 | 2,200 | 376 | 0% | 0% |
| | Right Turn | 450 | 950 | 105 | 1,575 | 98 | 1,775 | 59 | 75% | 0% |
| NB | Through | 150 | 125 | 7 | 200 | 13 | 200 | 33 | 0% | 2% |
| | Right Turn | 150 | 25 | 11 | 75 | 62 | 175 | 115 | 0% | 0% |
| SB | Left/Through | 400 | 25 | 2 | 50 | 15 | 75 | 45 | 0% | 0% |
| | Through | 400 | 350 | 11 | 400 | 12 | 375 | 19 | 0% | 6% |
| | | | | | | | | | | |

Intersection 5

Mathilda Avenue/Ross Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 250 | 50 | 10 | 125 | 15 | 125 | 0 | 1% | 0% |
| | Through | 1,575 | 150 | 20 | 275 | 50 | 325 | 94 | 57% | 0% |
| | Right Turn | 50 | 50 | 5 | 100 | 8 | 100 | 0 | 15% | 0% |
| NB | Left Turn | 250 | 150 | 26 | 250 | 36 | 250 | 21 | 13% | 0% |
| | Through | 700 | 350 | 118 | 600 | 256 | 625 | 249 | 10% | 1% |
| | Through/Right | 700 | 400 | 89 | 625 | 86 | 650 | 69 | 0% | 1% |
| SB | Left Turn | 225 | 125 | 8 | 200 | 13 | 225 | 10 | 0% | 1% |
| | Through | 225 | 175 | 11 | 225 | 13 | 250 | 20 | 0% | 6% |
| | Through/Right | 225 | 250 | 8 | 275 | 15 | 275 | 18 | 0% | 95% |
| WB | Left Turn | 100 | 100 | 1 | 125 | 2 | 100 | 0 | 78% | 0% |
| | Through | 225 | 875 | 509 | 1,400 | 827 | 1,400 | 670 | 3% | 0% |
| | Right Turn | 100 | 50 | 6 | 100 | 9 | 100 | 0 | 4% | 0% |

Intersection 6

Mathilda Avenue/US 101 NB Ramps

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NB | Through | 575 | 200 | 46 | 325 | 81 | 375 | 103 | 0% | 0% |
| | Right Turn | 575 | 25 | 4 | 50 | 25 | 75 | 57 | 0% | 0% |
| SB | Left Turn | 375 | 75 | 23 | 250 | 67 | 450 | 1 | 0% | 0% |
| | Through | 700 | 575 | 33 | 700 | 35 | 725 | 32 | 24% | 1% |
| WB | Left Turn | 1,025 | 400 | 92 | 575 | 118 | 625 | 110 | 14% | 0% |
| | Right Turn | 1,025 | 200 | 53 | 425 | 63 | 400 | 21 | 0% | 0% |
| | | | | | | | | | | |

Intersection 7

Mathilda Avenue/US 101 SB Ramps

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,050 | 100 | 5 | 125 | 8 | 125 | 17 | 0% | 0% |
| | Right Turn | 1,050 | 25 | 3 | 25 | 23 | 50 | 62 | 0% | 0% |
| NB | Through | 750 | 75 | 32 | 200 | 111 | 375 | 277 | 0% | 0% |
| | Right Turn | 750 | 25 | 11 | 100 | 107 | 250 | 314 | 0% | 0% |
| SB | Through | 575 | 100 | 23 | 250 | 65 | 350 | 121 | 0% | 0% |
| | Through/Right | 575 | 250 | 36 | 400 | 80 | 500 | 125 | 0% | 0% |
| | | | | | | | | | | |

Intersection 8

Mathilda Avenue-US 101 On-Ramp/Almanor Avenue-Ahwanee Avenue

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,025 | 175 | 12 | 275 | 26 | 325 | 62 | 32% | 0% |
| | Through/Right | 125 | 100 | 14 | 200 | 21 | 225 | 2 | 5% | 0% |
| NB | Left Turn | 425 | 75 | 11 | 150 | 20 | 175 | 31 | 0% | 0% |
| | Through | 750 | 300 | 14 | 425 | 33 | 475 | 68 | 23% | 0% |
| | Through/Right | 750 | 225 | 11 | 350 | 10 | 300 | 0 | 3% | 0% |
| SB | Left Turn | 275 | 200 | 15 | 325 | 18 | 325 | 1 | 2% | 0% |
| | Through | 750 | 300 | 34 | 450 | 49 | 525 | 75 | 11% | 0% |
| | Through/Right | 750 | 250 | 23 | 375 | 32 | 425 | 49 | 0% | 0% |
| WB | Left Turn | 250 | 50 | 8 | 100 | 15 | 125 | 26 | 0% | 0% |
| | Through | 1,025 | 25 | 5 | 75 | 20 | 100 | 42 | 2% | 0% |
| | Right Turn | 75 | 75 | 3 | 100 | 6 | 125 | 5 | 11% | 0% |

Intersection 9 Innovation Way-US 101 On-Ramp/Moffett Park Drive Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Through | 850 | 375 | 160 | 850 | 327 | 825 | 198 | 29% | 7% |
| | Right Turn | 150 | 100 | 38 | 300 | 107 | 350 | 96 | 0% | 0% |
| WB | Left Turn | 850 | 125 | 15 | 225 | 32 | 300 | 66 | 0% | 0% |
| | Through | 850 | 25 | 3 | 25 | 33 | 50 | 96 | 0% | 0% |
| | | | | | | | | | | |
| | | | | | | | | | | |

Intersection 10 Innovation Way/Moffett Park Drive Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 850 | 525 | 216 | 1,000 | 322 | 875 | 203 | 0% | 17% |
| SB | Right Turn | 575 | 25 | 5 | 50 | 11 | 100 | 20 | 0% | 0% |
| WB | Through | 1,150 | 100 | 8 | 150 | 20 | 175 | 33 | 0% | 0% |
| | Right Turn | 1,150 | 50 | 12 | 125 | 27 | 150 | 43 | 0% | 0% |
| | | | | | | | | | | |

Intersection 11

Innovation Way/11th Avenue

All-way Stop

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 125 | 125 | 9 | 175 | 6 | 150 | 0 | 9% | 0% |
| | Left/Through | 325 | 175 | 33 | 375 | 73 | 475 | 97 | 31% | 0% |
| | Right Turn | 325 | 75 | 4 | 100 | 20 | 150 | 63 | 0% | 0% |
| NB | Left Turn | 125 | 50 | 15 | 150 | 37 | 175 | 0 | 0% | 0% |
| | Through | 575 | 400 | 58 | 475 | 50 | 475 | 30 | 82% | 27% |
| | Through/Right | 575 | 300 | 40 | 400 | 33 | 375 | 6 | 0% | 59% |
| SB | Left Turn | 175 | 75 | 6 | 125 | 12 | 150 | 23 | 0% | 0% |
| | Through | 1,000 | 25 | 5 | 75 | 13 | 100 | 27 | 0% | 0% |
| | Through/Right | 1,000 | 75 | 11 | 150 | 20 | 175 | 25 | 0% | 0% |
| WB | Left Turn | 325 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | Through/Right | 325 | 25 | 3 | 50 | 6 | 50 | 15 | 0% | 0% |

Intersection 12

Innovation Way/Juniper Networks Driveway

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 200 | 2,575 | 988 | 3,875 | 1,341 | 3,850 | 1,169 | 0% | 0% |
| | Right Turn | 200 | 875 | 428 | 1,800 | 689 | 1,575 | 528 | 0% | 0% |
| NB | Left Turn | 125 | 75 | 10 | 150 | 20 | 175 | 1 | 0% | 0% |
| | Through | 1,000 | 1,100 | 50 | 1,225 | 61 | 1,175 | 34 | 72% | 39% |
| SB | Through | 300 | 200 | 11 | 225 | 23 | 250 | 36 | 0% | 0% |
| | Through/Right | 300 | 100 | 17 | 125 | 28 | 150 | 34 | 0% | 6% |
| | | | | | | | | | | |

Intersection 13

Bordeaux Drive/Innovation Way

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left/Through | 375 | 50 | 5 | 75 | 9 | 100 | 23 | 0% | 0% |
| | Right Turn | 125 | 50 | 3 | 100 | 6 | 100 | 16 | 0% | 0% |
| NB | Left Turn | 325 | 1,275 | 179 | 2,300 | 237 | 2,525 | 220 | 84% | 0% |
| | Through/Right | 2,025 | 925 | 98 | 1,150 | 154 | 1,025 | 1 | 0% | 44% |
| SB | Left Turn | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | Through/Right | 725 | 500 | 132 | 775 | 100 | 725 | 37 | 75% | 15% |
| WB | Left/Through | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | Right Turn | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |

Arterial Level of Service: NB Mathilda Ave

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|--------------------|------|---------------|-----------------|-----------|----------------|
| Ahwanee Ave | 8 | 32.6 | 43.7 | 0.1 | 12 |
| | 7 | 8.3 | 20.8 | 0.2 | 26 |
| US 101 NB Ramps | 6 | 16.6 | 27.0 | 0.1 | 18 |
| Ross Dr | 5 | 48.9 | 60.6 | 0.1 | 9 |
| | 4 | 79.8 | 84.3 | 0.0 | 2 |
| SR 237 EB Off-Ramp | 43 | 1.1 | 5.4 | 0.0 | 22 |
| Mathilda Ave | 57 | 0.5 | 5.4 | 0.0 | 24 |
| Mathilda Ave | 3 | 36.4 | 40.5 | 0.0 | 4 |
| Innovation Way | 2 | 32.7 | 56.8 | 0.2 | 14 |
| 5th Ave | 1 | 16.4 | 36.1 | 0.2 | 24 |
| | 107 | 3.3 | 25.4 | 0.3 | 39 |
| Total | | 276.7 | 406.1 | 1.5 | 13 |

Arterial Level of Service: SB Mathilda Ave

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|-----------------|------|---------------|-----------------|-----------|----------------|
| 5th Ave | 1 | 266.9 | 287.1 | 0.3 | 3 |
| Innovation Way | 2 | 276.4 | 298.1 | 0.2 | 3 |
| | 3 | 50.7 | 81.9 | 0.2 | 10 |
| Ross Dr | 5 | 20.6 | 27.4 | 0.0 | 6 |
| US 101 NB Ramps | 6 | 56.2 | 67.4 | 0.1 | 8 |
| US 101 SB Ramps | 7 | 7.0 | 17.8 | 0.1 | 27 |
| Almanor Ave | 8 | 27.6 | 40.0 | 0.2 | 14 |
| San Aleso Ave | 201 | 5.4 | 16.8 | 0.1 | 30 |
| Total | | 710.8 | 836.4 | 1.4 | 6 |

Arterial Level of Service: NB Innovation Way

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|------------------|------|---------------|-----------------|-----------|----------------|
| | 910 | 9.5 | 13.7 | 0.0 | 7 |
| | 53 | 24.3 | 28.9 | 0.0 | 5 |
| | 11 | 101.7 | 109.0 | 0.1 | 2 |
| | 200 | 155.5 | 171.1 | 0.2 | 3 |
| Juniper Driveway | 12 | 70.1 | 75.8 | 0.1 | 3 |
| Driveway | 217 | 10.7 | 13.9 | 0.0 | 10 |
| | 902 | 29.0 | 31.0 | 0.0 | 2 |
| Mathilda Ave | 2 | 10.9 | 13.5 | 0.0 | 7 |
| | 16 | 3.3 | 17.6 | 0.1 | 18 |
| Bordeaux Dr | 13 | 25.6 | 37.6 | 0.1 | 8 |
| Total | | 440.7 | 512.1 | 0.6 | 4 |

Arterial Level of Service: SB Innovation Way

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|------------------|------|---------------|-----------------|-----------|----------------|
| | 16 | - | - | 0.1 | - |
| Mathilda Ave | 2 | 136.2 | 147.7 | 0.1 | 2 |
| | 902 | 5.8 | 10.9 | 0.0 | 9 |
| Driveway | 217 | 0.5 | 2.5 | 0.0 | 27 |
| Juniper Driveway | 12 | 53.3 | 58.5 | 0.0 | 2 |
| | 200 | 2.4 | 8.8 | 0.1 | 23 |
| 11th Ave | 11 | 16.1 | 31.9 | 0.2 | 18 |
| | 53 | 3.2 | 10.6 | 0.1 | 24 |
| | 910 | 5.7 | 9.9 | 0.0 | 14 |
| Moffett Park Dr | 10 | 4.3 | 8.9 | 0.0 | 10 |
| Total | | 227.5 | 289.8 | 0.6 | 8 |

APPENDIX M – YEAR 2018 FREQ MAINLINE CALCULATION SHEETS



```

FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQQ QQQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP EEEEEEEEE
    
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FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 62
LOWER LIMB (AT V/C=1) = 30
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT DES TRUCKS | SPECIAL RAMP | FF. SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION LOCATION |
|---------|----------|----------|-------------|--------------|---------|---------|-----------|---------|----------------|--------------|-------------------|---------------|----------|----------------|------------------------|
| ** 1 | 3 | 6000. | 500. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Seeding |
| ** 2 | 3 | 6000. | 99999. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture |
| ** 3 | 2 | 4000. | 12000. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** 4 | 3 | 4430. | 350. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Maude On-Ramp |
| ** 5 | 3 | 4430. | 300. | 62 | | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Maude to US-101 |
| ** 6 | 3 | 4430. | 350. | 62 | D | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US-101 Off-ramp |
| ** 7 | 2 | 4000. | 940. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | US101SB / US101SB |
| ** 8 | 3 | 4930. | 700. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US101 SB On-ramp |
| ** 9 | 3 | 4930. | 700. | 62 | | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US 101 / Mathilda |
| ** 10 | 3 | 4930. | 700. | 62 | D | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-ramp |
| ** 11 | 2 | 4000. | 2300. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda |
| ** 12 | 3 | 4810. | 700. | 62 | OD | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda On-Ramp |
| ** 13 | 3 | 4270. | 800. | 62 | | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda / Persian HOV |
| ** 14 | 3 | 4270. | 1400. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks Off-Ramp |
| ** 15 | 2 | 4000. | 1400. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | West of Lawrence E |
| ** 16 | 2 | 4000. | 1500. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence Off-ramp |
| ** 17 | 2 | 4000. | 1500. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End of DKS |
| ** 18 | 2 | 4000. | 10000. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** 19 | 3 | 5600. | 750. | 62 | OD | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End of the network |

***** INPUT HAS BEEN COMPLETED *****

**
** FREeway TRAVEL TIME (MINUTES) **
**

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | |
|-----------|--|-----------------------|-------|-------|-------|-------|-------|-------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | | 20.80 | 21.36 | 21.91 | 22.31 | 22.84 | 23.12 | 25.09 |
| * 2 * | | 0.18 | 0.74 | 1.29 | 1.69 | 2.23 | 2.50 | 4.47 |
| * 3 * | | 0.00 | 0.38 | 0.93 | 1.34 | 1.87 | 2.14 | 4.11 |
| * 4 * | | 0.00 | 0.00 | 0.13 | 0.53 | 1.06 | 1.34 | 3.31 |
| * 5 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.14 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB | * NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | |
|---------|-------|----------|------------|-----------|------------|---------|---------|-----------|-----------|-----------------|---------|----------------|---------|-----------|-------------|--------|------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * ORG | * DES | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | |
| * 1 | * 3 | * 500. | * 2660. | * 0. | * 2660. | * 2660. | * 0. | * 0. | * 0. | * .44 | * 62. | * 14.3 | * B | * 20.3 | * 13.0 | | |
| * 2 | * 3 | * 99999. | * 0. | * 0. | * 2660. | * 0. | * 0. | * 0. | * 0. | * .44 | * 62. | * 14.3 | * B | * 20.3 | * 13.0 | | |
| * 3 | * 2 | * 12000. | * 0. | * 0. | * 2660. | * 0. | * 0. | * 0. | * 0. | * .67 | * 62. | * 21.5 | * C | * 20.3 | * 13.0 | | |
| * 4 | * 3 | * 350. | * 250. | * 0. | * 2910. | * 250. | * 0. | * 0. | * 0. | * .66 | * 62. | * 15.6 | * B | * 20.3 | * 13.0 | | |
| * 5 | * 3 | * 300. | * 0. | * 0. | * 2910. | * 0. | * 0. | * 0. | * 0. | * .66 | * 62. | * 15.6 | * B | * 20.3 | * 13.0 | | |
| * 6 | * 3 | * 350. | * 0. | * 900. | * 2910. | * 0. | * 900. | * 2910. | * 4430. | * 0. | * .66 | * 62. | * 15.6 | * B | * 20.3 | * 13.0 | |
| * 7 | * 2 | * 940. | * 0. | * 0. | * 2010. | * 0. | * 0. | * 2010. | * 4000. | * 0. | * .50 | * 62. | * 16.2 | * B | * 20.3 | * 13.0 | |
| * 8 | * 3 | * 700. | * 1670. | * 0. | * 3680. | * 1670. | * 0. | * 0. | * 0. | * .75 | * 62. | * 19.8 | * C | * 20.3 | * 13.0 | | |
| * 9 | * 3 | * 700. | * 0. | * 0. | * 3680. | * 0. | * 0. | * 3680. | * 4930. | * 0. | * .75 | * 62. | * 19.8 | * C | * 20.3 | * 13.0 | |
| * 10 | * 3 | * 700. | * 0. | * 720. | * 3680. | * 0. | * 720. | * 3680. | * 4930. | * 0. | * .75 | * 62. | * 19.8 | * C | * 20.3 | * 13.0 | |
| * 11 | * 2 | * 2300. | * 0. | * 0. | * 2960. | * 0. | * 0. | * 2960. | * 4000. | * 0. | * .74 | * 62. | * 23.9 | * C | * 20.3 | * 13.0 | |
| * 12 | * 3 | * 700. | * 360. | * 722. | * 3320. | * 360. | * 722. | * 3320. | * 4810. | * 0. | * .69 | * 62. | * 17.8 | * B | * 20.3 | * 13.0 | |
| * 13 | * 3 | * 800. | * 0. | * 0. | * 2598. | * 0. | * 0. | * 2598. | * 4270. | * 0. | * .61 | * 62. | * 14.0 | * B | * 20.3 | * 13.0 | |
| * 14 | * 3 | * 1400. | * 0. | * 230. | * 2598. | * 0. | * 230. | * 2598. | * 4270. | * 0. | * .61 | * 62. | * 14.0 | * B | * 20.3 | * 13.0 | |
| * 15 | * 2 | * 1400. | * 0. | * 0. | * 2368. | * 0. | * 0. | * 2368. | * 4000. | * 0. | * .59 | * 62. | * 19.1 | * C | * 20.3 | * 13.0 | |
| * 16 | * 2 | * 1500. | * 0. | * 200. | * 2368. | * 0. | * 200. | * 2368. | * 4000. | * 0. | * .59 | * 62. | * 19.1 | * C | * 20.3 | * 13.0 | |
| * 17 | * 2 | * 1500. | * 0. | * 0. | * 2168. | * 0. | * 0. | * 2168. | * 4000. | * 0. | * .54 | * 62. | * 17.5 | * B | * 20.3 | * 13.0 | |
| * 18 | * 2 | * 10000. | * 0. | * 0. | * 2168. | * 0. | * 0. | * 2168. | * 4000. | * 0. | * .54 | * 62. | * 17.5 | * B | * 20.3 | * 13.0 | |
| * 19 | * 3 | * 750. | * 722. | * 2890. | * 2890. | * 722. | * 2890. | * 2890. | * 5600. | * 0. | * .52 | * 62. | * 15.5 | * B | * 20.3 | * 13.0 | |
| * TOTAL | | 136889. | = | 25.9 | MILES | | | | | MAX(V/C) = 0.75 | | LOWEST LOS = C | | AVG = 62. | 15.6 | 20.3 | 13.0 |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 1102. VEH-HRS | 1349. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1102. VEH-HRS | 1349. PASS-HRS |
| TOTAL TRAV DISTANCE = | 68293. VEH-MI. | 83661. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 62. MPH. |
| AVERAGE DENSITY = | 16. VPMP | 16. VPMP |
| TOTAL FUEL = | 3357. GALLONS | 3357. GALLONS |
| TOTAL EMISSIONS = | 891. KI LOGRAMS | 891. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.19 | 2 | 37.50 | 3 | 4.50 | 4 | 0.14 | 5 | 0.12 |
| 6 | 0.14 | 7 | 0.27 | 8 | 0.36 | 9 | 0.36 | 10 | 0.36 |
| 11 | 0.96 | 12 | 0.33 | 13 | 0.29 | 14 | 0.51 | 15 | 0.47 |
| 16 | 0.50 | 17 | 0.46 | 18 | 3.06 | 19 | 0.31 | | |

***** TOTAL DELAY = 50.8 VEH-HRS ***** AVERAGE DELAY = 1.16 MIN/VEH *****

**
** FREEWAY TRAVEL TIME (MINUTES)
**

| * ORIGINS | * DESTINATIONS ACROSS | | | | | | |
|-----------|-----------------------|-------|-------|-------|-------|-------|-------|
| * DOWN | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 20.99 | 21.60 | 22.20 | 22.61 | 23.14 | 23.42 | 25.39 |
| * 2 * | 0.18 | 0.79 | 1.40 | 1.80 | 2.34 | 2.61 | 4.58 |
| * 3 * | 0.00 | 0.44 | 1.04 | 1.44 | 1.98 | 2.26 | 4.23 |
| * 4 * | 0.00 | 0.00 | 0.13 | 0.53 | 1.07 | 1.34 | 3.31 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.14 |

*
* TIME SLICE FREEWAY PERFORMANCE TABLE
*

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|-----------|----------|------------------|------------------|--------------------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|
| * SEC LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 1 3 | 500. | 3659. | 0. 3659. | 3659. 0. 3659. | 6000. | 0. | 0. | 0. | .61 | 62. | 19.7 | C | 20.3 | 13.0 |
| * 2 3 | 99999. | 0. | 0. 3659. | 0. 0. 3659. | 6000. | 0. | 0. | 0. | .61 | 62. | 19.7 | C | 20.3 | 13.0 |
| * 3 2 | 12000. | 0. | 0. 3659. | 0. 0. 3659. | 4000. | 0. | 0. | 0. | .91 | 57. | 32.0 | D | 22.2 | 11.8 |
| * 4 3 | 350. | 431. | 0. 4090. | 431. 0. 4090. | 4430. | 0. | 0. | 0. | .92 | 62. | 22.0 | C | 20.3 | 13.0 |
| * 5 3 | 300. | 0. | 0. 4090. | 0. 0. 4090. | 4430. | 0. | 0. | 0. | .92 | 62. | 22.0 | C | 20.3 | 13.0 |
| * 6 3 | 350. | 0. | 1270. 4090. | 0. 1270. 4090. | 4430. | 0. | 0. | 0. | .92 | 62. | 22.0 | C | 20.3 | 13.0 |
| * 7 2 | 940. | 0. | 0. 2820. | 0. 0. 2820. | 4000. | 0. | 0. | 0. | .70 | 62. | 22.7 | C | 20.3 | 13.0 |
| * 8 3 | 700. | 1911. | 0. 4731. | 1911. 0. 4731. | 4930. | 0. | 0. | 0. | .96 | 55. | 28.9 | D | 23.0 | 11.4 |
| * 9 3 | 700. | 0. | 0. 4731. | 0. 0. 4731. | 4930. | 0. | 0. | 0. | .96 | 55. | 28.9 | D | 23.0 | 11.4 |
| * 10 3 | 700. | 0. | 930. 4731. | 0. 930. 4731. | 4930. | 0. | 0. | 0. | .96 | 55. | 28.9 | D | 23.0 | 11.4 |
| * 11 2 | 2300. | 0. | 0. 3801. | 0. 0. 3801. | 4000. | 0. | 0. | 0. | .95 | 55. | 34.5 | D | 22.8 | 11.4 |
| * 12 3 | 700. | 574. 958. 4375. | 574. 958. 4375. | 4810. | 0. | 0. | 0. | 0. | .91 | 62. | 23.5 | C | 20.3 | 13.0 |
| * 13 3 | 800. | 0. | 0. 3417. | 0. 0. 3417. | 4270. | 0. | 0. | 0. | .80 | 62. | 18.4 | C | 20.3 | 13.0 |
| * 14 3 | 1400. | 0. | 270. 3417. | 0. 270. 3417. | 4270. | 0. | 0. | 0. | .80 | 62. | 18.4 | C | 20.3 | 13.0 |
| * 15 2 | 1400. | 0. | 0. 3147. | 0. 0. 3147. | 4000. | 0. | 0. | 0. | .79 | 61. | 25.7 | C | 20.7 | 12.8 |
| * 16 2 | 1500. | 0. | 270. 3147. | 0. 270. 3147. | 4000. | 0. | 0. | 0. | .79 | 61. | 25.7 | C | 20.7 | 12.8 |
| * 17 2 | 1500. | 0. | 0. 2877. | 0. 0. 2877. | 4000. | 0. | 0. | 0. | .72 | 62. | 23.2 | C | 20.3 | 13.0 |
| * 18 2 | 10000. | 0. | 0. 2877. | 0. 0. 2877. | 4000. | 0. | 0. | 0. | .72 | 62. | 23.2 | C | 20.3 | 13.0 |
| * 19 3 | 750. | 959. 3836. 3836. | 959. 3836. 3836. | 5600. | 0. | 0. | 0. | 0. | .69 | 62. | 20.6 | C | 20.3 | 13.0 |

*
* TOTAL 136889. = 25.9 MI LES MAX(V/C) = 0.96 LOWEST LOS = D AVG = 61. 21.6 20.6 12.9
*

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|----------------------------|--------------------|------------------|-------------------|------------------|
| FREWAY TRAVEL TIME = | 1524. VEH-HRS | 1869. PASS-HRS | 2626. VEH-HRS | 3218. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1524. VEH-HRS | 1869. PASS-HRS | 2626. VEH-HRS | 3218. PASS-HRS |
| TOTAL TRAV DISTANCE = | 93318. VEH-MI. | 114387. PASS-MI. | 161612. VEH-MI. | 198048. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 61. MPH. | | 62. MPH. | |

AVERAGE DENSITY = 22. VPMP
 TOTAL FUEL = 4532. GALLONS
 TOTAL EMISSIONS = 1201. KI LOGRAMS

SR-237_EB_AM_NP_2018_PE
 19. VPMP
 7890. GALLONS
 2092. KI LOGRAMS

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 SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 2

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***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.26 | 2 | 51.59 | 3 | 17.66 | 4 | 0.20 | 5 | 0.17 |
| 6 | 0.20 | 7 | 0.37 | 8 | 1.86 | 9 | 1.86 | 10 | 1.86 |
| 11 | 4.57 | 12 | 0.43 | 13 | 0.39 | 14 | 0.67 | 15 | 0.79 |
| 16 | 0.85 | 17 | 0.61 | 18 | 4.06 | 19 | 0.41 | | |

***** TOTAL DELAY = 88.8 VEH-HRS ***** AVERAGE DELAY = 1.46 MIN/VEH *****

** 19 **

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 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 1 OF 2

 ** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|-------|-----------------------|------|------|------|------|------|------|------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| + | * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.04 | 0.00 |
| + | * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 1 OF 2

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | |
|-----------|--------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|--------|---------|-----------|---------|--------|-------------|---|------|------|
| * SEC | * LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * SSEC | * CAP | * EFF | * LENGTH | * RATE | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | | |
| * 1 | | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | | |
| * 3 | | | | | | | | | | | | | | | | | | |
| * 4 | | | | | | | | | | | | | | | | | | |
| * 5 | | | | | | | | | | | | | | | | | | |
| * 6 | | | | | | | | | | | | | | | | | | |
| * 7 | | | | | | | | | | | | | | | | | | |
| * 8 | | | | | | | | | | | | | | | | | | |
| * 9 | | | | | | | | | | | | | | | | | | |
| * 10 | | | | | | | | | | | | | | | | | | |
| * 11 | | | | | | | | | | | | | | | | | | |
| * 12 | | | | | | | | | | | | | | | | | | |
| * 13 | 1 | 800. | 722. | 0. | 722. | 722. | 0. | 722. | 1650. | 0. | 0. | 0. | .44 | 62. | 11.6 | B | 21.6 | 12.8 |
| * 14 | 1 | 1400. | 0. | 0. | 722. | 0. | 0. | 722. | 1650. | 0. | 0. | 0. | .44 | 62. | 11.6 | B | 21.6 | 12.8 |
| * 15 | 1 | 1400. | 0. | 0. | 722. | 0. | 0. | 722. | 1650. | 0. | 0. | 0. | .44 | 62. | 11.6 | B | 21.6 | 12.8 |
| * 16 | 1 | 1500. | 0. | 0. | 722. | 0. | 0. | 722. | 1650. | 0. | 0. | 0. | .44 | 62. | 11.6 | B | 21.6 | 12.8 |
| * 17 | 1 | 1500. | 0. | 0. | 722. | 0. | 0. | 722. | 1650. | 0. | 0. | 0. | .44 | 62. | 11.6 | B | 21.6 | 12.8 |
| * 18 | 1 | 10000. | 0. | 722. | 722. | 0. | 722. | 722. | 1650. | 0. | 0. | 0. | .44 | 62. | 11.6 | B | 21.6 | 12.8 |
| * 19 | | | | | | | | | | | | | | | | | | |
| * TOTAL | | 16600. | = | 3.1 | MILES | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 37. VEH-HRS | 73. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 37. VEH-HRS | 73. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 2271. VEH-MI. | 4541. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 62. MPH. |
| AVERAGE DENSITY = | 12. VPMP | 12. VPMP |
| TOTAL FUEL = | 105. GALLONS | 105. GALLONS |
| TOTAL EMISSIONS = | 29. KILOGRAMS | 29. KILOGRAMS |

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 TIME SLICE 1 OF 2
 Page 2

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.08 | 14 | 0.14 | 15 | 0.14 |
| 16 | 0.15 | 17 | 0.15 | 18 | 1.02 | 19 | 0.00 | | |

***** TOTAL DELAY = 1.7 VEH-HRS ***** AVERAGE DELAY = 0.14 MIN/VEH *****

 ** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|------|-----------------------|------|------|------|------|------|------|------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| + * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.04 | 0.00 | 0.00 |
| + * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISS | | | | |
|-----------|--------|------------|-----------|--------------------|-----------|---------|-----------|-----------|---------|---------|-----------|---------|--------|---------|------|---|------|------|
| * SEC | * LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * CAP | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | | | |
| * 13 | 1 | 800. | 959. | 0. | 959. | 959. | 0. | 959. | 1650. | 0. | 0. | 0. | .58 | 62. | 15.5 | B | 21.6 | 12.8 |
| * 14 | 1 | 1400. | 0. | 0. | 959. | 0. | 0. | 959. | 1650. | 0. | 0. | 0. | .58 | 62. | 15.5 | B | 21.6 | 12.8 |
| * 15 | 1 | 1400. | 0. | 0. | 959. | 0. | 0. | 959. | 1650. | 0. | 0. | 0. | .58 | 62. | 15.5 | B | 21.6 | 12.8 |
| * 16 | 1 | 1500. | 0. | 0. | 959. | 0. | 0. | 959. | 1650. | 0. | 0. | 0. | .58 | 62. | 15.5 | B | 21.6 | 12.8 |
| * 17 | 1 | 1500. | 0. | 0. | 959. | 0. | 0. | 959. | 1650. | 0. | 0. | 0. | .58 | 62. | 15.5 | B | 21.6 | 12.8 |
| * 18 | 1 | 10000. | 0. | 959. | 959. | 0. | 959. | 959. | 1650. | 0. | 0. | 0. | .58 | 62. | 15.5 | B | 21.6 | 12.8 |
| * 19 | | | | | | | | | | | | | | | | | | |
| * TOTAL | 16600. | = | 3.1 | MI LBS | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
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| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 49. VEH-HRS | 97. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 49. VEH-HRS | 97. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 3014. VEH-MI. | 6029. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 62. MPH. |
| AVERAGE DENSITY = | 15. VPMP | 14. VPMP |
| TOTAL FUEL = | 140. GALLONS | 245. GALLONS |

TOTAL EMISSIONS = 38. KILOGRAMS

SR-237_EB_AM_NP_2018_PL
67. KILOGRAMS

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***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.11 | 14 | 0.19 | 15 | 0.19 |
| 16 | 0.20 | 17 | 0.20 | 18 | 1.35 | 19 | 0.00 | | |

***** TOTAL DELAY = 2.2 VEH-HRS ***** AVERAGE DELAY = 0.14 MIN/VEH *****

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FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQQ QQQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP EEEEEEEEE
    
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FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 62
LOWER LIMB (AT V/C=1) = 30
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREEWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT TRUCKS | DES TRUCKS | SPECIAL RAMP | FF. SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION LOCATION |
|---------|----------|----------|-------------|--------------|---------|---------|-----------|---------|------------|------------|--------------|-------------------|---------------|----------|----------------|------------------------|
| ** 1 | 3 | 6000. | 500. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Seeding |
| ** 2 | 3 | 6000. | 99999. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture |
| ** 3 | 2 | 4000. | 12000. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** 4 | 3 | 4430. | 350. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Maude On-Ramp |
| ** 5 | 3 | 4430. | 300. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Maude to US-101 |
| ** 6 | 3 | 4430. | 350. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US-101 Off-ramp |
| ** 7 | 2 | 4000. | 940. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | US101SB / US101SB |
| ** 8 | 3 | 4650. | 700. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US101 SB On-ramp |
| ** 9 | 3 | 4650. | 700. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US 101 / Mathilda |
| ** 10 | 3 | 4650. | 700. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-ramp |
| ** 11 | 2 | 4000. | 2300. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda |
| ** 12 | 3 | 4810. | 700. | 62 | OD | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda On-Ramp |
| ** 13 | 3 | 4270. | 800. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda / Persian HOV |
| ** 14 | 3 | 4270. | 1400. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks Off-Ramp |
| ** 15 | 2 | 4000. | 1400. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | West of Lawrence E |
| ** 16 | 2 | 4000. | 1500. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence Off-ramp |
| ** 17 | 2 | 4000. | 1500. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End of DKS |
| ** 18 | 2 | 4000. | 10000. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** 19 | 3 | 5600. | 750. | 62 | OD | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End of the network |

***** INPUT HAS BEEN COMPLETED *****

**
** FREeway TRAVEL TIME (MINUTES) **
**

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | |
|-----------|--|-----------------------|-------|-------|-------|-------|-------|-------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| + * 1 * | | 20.80 | 21.36 | 21.91 | 22.31 | 22.84 | 23.12 | 25.09 |
| + * 2 * | | 0.18 | 0.74 | 1.29 | 1.69 | 2.23 | 2.50 | 4.47 |
| + * 3 * | | 0.00 | 0.38 | 0.93 | 1.34 | 1.87 | 2.14 | 4.11 |
| + * 4 * | | 0.00 | 0.00 | 0.13 | 0.53 | 1.06 | 1.34 | 3.31 |
| + * 5 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.14 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | | | |
|------------------------------|----------|------------|-----------|------------|----------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-----------------|----------------|-----------|------|------|------|
| * SEC LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * SSEC | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | | | | |
| * 1 3 | 500. | 2661. | 0. 2661. | 2661. | 0. 2661. | 6000. | 0. | 0. | .44 | 62. | 14.3 | B | 20.3 | 13.0 | | | | | |
| * 2 3 | 99999. | 0. | 0. 2661. | 0. | 0. 2661. | 6000. | 0. | 0. | .44 | 62. | 14.3 | B | 20.3 | 13.0 | | | | | |
| * 3 2 | 12000. | 0. | 0. 2661. | 0. | 0. 2661. | 4000. | 0. | 0. | .67 | 62. | 21.5 | C | 20.3 | 13.0 | | | | | |
| * 4 3 | 350. | 250. | 0. 2911. | 250. | 0. 2911. | 4430. | 0. | 0. | .66 | 62. | 15.7 | B | 20.3 | 13.0 | | | | | |
| * 5 3 | 300. | 0. | 0. 2911. | 0. | 0. 2911. | 4430. | 0. | 0. | .66 | 62. | 15.7 | B | 20.3 | 13.0 | | | | | |
| * 6 3 | 350. | 0. | 0. 2911. | 0. | 0. 2911. | 4430. | 0. | 0. | .66 | 62. | 15.7 | B | 20.3 | 13.0 | | | | | |
| * 7 2 | 940. | 0. | 0. 2011. | 0. | 0. 2011. | 4000. | 0. | 0. | .50 | 62. | 16.2 | B | 20.3 | 13.0 | | | | | |
| * 8 3 | 700. | 1470. | 0. 3481. | 1470. | 0. 3481. | 4650. | 0. | 0. | .75 | 62. | 18.7 | C | 20.3 | 13.0 | | | | | |
| * 9 3 | 700. | 0. | 0. 3481. | 0. | 0. 3481. | 4650. | 0. | 0. | .75 | 62. | 18.7 | C | 20.3 | 13.0 | | | | | |
| * 10 3 | 700. | 0. | 0. 3481. | 0. | 0. 3481. | 4650. | 0. | 0. | .75 | 62. | 18.7 | C | 20.3 | 13.0 | | | | | |
| * 11 2 | 2300. | 0. | 0. 2960. | 0. | 0. 2960. | 4000. | 0. | 0. | .74 | 62. | 23.9 | C | 20.3 | 13.0 | | | | | |
| * 12 3 | 700. | 501. | 0. 3461. | 501. | 0. 3461. | 4810. | 0. | 0. | .72 | 62. | 18.6 | C | 20.3 | 13.0 | | | | | |
| * 13 3 | 800. | 0. | 0. 2703. | 0. | 0. 2703. | 4270. | 0. | 0. | .63 | 62. | 14.5 | B | 20.3 | 13.0 | | | | | |
| * 14 3 | 1400. | 0. | 0. 2703. | 0. | 0. 2703. | 4270. | 0. | 0. | .63 | 62. | 14.5 | B | 20.3 | 13.0 | | | | | |
| * 15 2 | 1400. | 0. | 0. 2473. | 0. | 0. 2473. | 4000. | 0. | 0. | .62 | 62. | 19.9 | C | 20.3 | 13.0 | | | | | |
| * 16 2 | 1500. | 0. | 0. 199. | 199. | 0. 2473. | 4000. | 0. | 0. | .62 | 62. | 19.9 | C | 20.3 | 13.0 | | | | | |
| * 17 2 | 1500. | 0. | 0. 2274. | 0. | 0. 2274. | 4000. | 0. | 0. | .57 | 62. | 18.3 | C | 20.3 | 13.0 | | | | | |
| * 18 2 | 10000. | 0. | 0. 2274. | 0. | 0. 2274. | 4000. | 0. | 0. | .57 | 62. | 18.3 | C | 20.3 | 13.0 | | | | | |
| * 19 3 | 750. | 758. | 0. 3032. | 3032. | 0. 3032. | 5600. | 0. | 0. | .54 | 62. | 16.3 | B | 20.3 | 13.0 | | | | | |
| * TOTAL 136889. = 25.9 MILES | | | | | | | | | | | | | | MAX(V/C) = 0.75 | LOWEST LOS = C | AVG = 62. | 15.7 | 20.3 | 13.0 |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 1107. VEH-HRS | 1354. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1107. VEH-HRS | 1354. PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 68607. VEH-MI. | 83969. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 62. MPH. |
| AVERAGE DENSITY = | 16. VPMP | 16. VPMP |
| TOTAL FUEL = | 3373. GALLONS | 3373. GALLONS |
| TOTAL EMISSIONS = | 895. KI LOGRAMS | 895. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.19 | 2 | 37.52 | 3 | 4.50 | 4 | 0.14 | 5 | 0.12 |
| 6 | 0.14 | 7 | 0.27 | 8 | 0.34 | 9 | 0.34 | 10 | 0.34 |
| 11 | 0.96 | 12 | 0.34 | 13 | 0.30 | 14 | 0.53 | 15 | 0.49 |
| 16 | 0.52 | 17 | 0.48 | 18 | 3.21 | 19 | 0.32 | | |

***** TOTAL DELAY = 51.1 VEH-HRS ***** AVERAGE DELAY = 1.16 MIN/VEH *****

**
** FREEWAY TRAVEL TIME (MINUTES)
**

| * ORIGINS * DOWN | * DESTINATIONS ACROSS | | | | | | |
|---------------------|-----------------------|-------|-------|-------|-------|-------|-------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 20.99 | 21.55 | 22.15 | 22.56 | 23.10 | 23.38 | 25.35 |
| * 2 * | 0.18 | 0.74 | 1.34 | 1.75 | 2.29 | 2.57 | 4.54 |
| * 3 * | 0.00 | 0.38 | 0.99 | 1.39 | 1.94 | 2.21 | 4.18 |
| * 4 * | 0.00 | 0.00 | 0.13 | 0.53 | 1.08 | 1.35 | 3.32 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.14 |

*
* TIME SLICE FREEWAY PERFORMANCE TABLE
*

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|-----------|----------|------------|-------------|--------------------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|
| * SEC LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 1 3 | 500. | 3662. | 0. 3662. | 3662. 0. 3662. | 6000. | 0. | 0. | 0. | .61 | 62. | 19.7 | C | 20.3 | 13.0 |
| * 2 3 | 99999. | 0. | 0. 3662. | 0. 0. 3662. | 6000. | 0. | 0. | 0. | .61 | 62. | 19.7 | C | 20.3 | 13.0 |
| * 3 2 | 12000. | 0. | 0. 3662. | 0. 0. 3662. | 4000. | 0. | 0. | 0. | .92 | 57. | 32.1 | D | 22.2 | 11.8 |
| * 4 3 | 350. | 430. | 0. 4092. | 430. 0. 4092. | 4430. | 0. | 0. | 0. | .92 | 62. | 22.0 | C | 20.3 | 13.0 |
| * 5 3 | 300. | 0. | 0. 4092. | 0. 0. 4092. | 4430. | 0. | 0. | 0. | .92 | 62. | 22.0 | C | 20.3 | 13.0 |
| * 6 3 | 350. | 0. | 1270. 4092. | 0. 1270. 4092. | 4430. | 0. | 0. | 0. | .92 | 62. | 22.0 | C | 20.3 | 13.0 |
| * 7 2 | 940. | 0. | 0. 2822. | 0. 0. 2822. | 4000. | 0. | 0. | 0. | .71 | 62. | 22.8 | C | 20.3 | 13.0 |
| * 8 3 | 700. | 1630. | 0. 4452. | 1630. 0. 4452. | 4650. | 0. | 0. | 0. | .96 | 62. | 23.9 | C | 20.3 | 13.0 |
| * 9 3 | 700. | 0. | 0. 4452. | 0. 0. 4452. | 4650. | 0. | 0. | 0. | .96 | 62. | 23.9 | C | 20.3 | 13.0 |
| * 10 3 | 700. | 0. | 650. 4452. | 0. 650. 4452. | 4650. | 0. | 0. | 0. | .96 | 62. | 23.9 | C | 20.3 | 13.0 |
| * 11 2 | 2300. | 0. | 0. 3802. | 0. 0. 3802. | 4000. | 0. | 0. | 0. | .95 | 55. | 34.5 | D | 22.8 | 11.4 |
| * 12 3 | 700. | 798. | 1015. 4600. | 798. 1015. 4600. | 4810. | 0. | 0. | 0. | .96 | 62. | 24.7 | C | 20.3 | 13.0 |
| * 13 3 | 800. | 0. | 0. 3585. | 0. 0. 3585. | 4270. | 0. | 0. | 0. | .84 | 62. | 19.3 | C | 20.3 | 13.0 |
| * 14 3 | 1400. | 0. | 271. 3585. | 0. 271. 3585. | 4270. | 0. | 0. | 0. | .84 | 62. | 19.3 | C | 20.3 | 13.0 |
| * 15 2 | 1400. | 0. | 0. 3314. | 0. 0. 3314. | 4000. | 0. | 0. | 0. | .83 | 60. | 27.4 | D | 21.2 | 12.5 |
| * 16 2 | 1500. | 0. | 271. 3314. | 0. 271. 3314. | 4000. | 0. | 0. | 0. | .83 | 60. | 27.4 | D | 21.2 | 12.5 |
| * 17 2 | 1500. | 0. | 0. 3043. | 0. 0. 3043. | 4000. | 0. | 0. | 0. | .76 | 62. | 24.5 | C | 20.3 | 13.0 |
| * 18 2 | 10000. | 0. | 0. 3043. | 0. 0. 3043. | 4000. | 0. | 0. | 0. | .76 | 62. | 24.5 | C | 20.3 | 13.0 |
| * 19 3 | 750. | 1014. | 4057. 4057. | 1014. 4057. 4057. | 5600. | 0. | 0. | 0. | .72 | 62. | 21.8 | C | 20.3 | 13.0 |

*
* TOTAL 136889. = 25.9 MILES MAX(V/C) = 0.96 LOWEST LOS = D AVG = 61. 21.7 20.6 12.9
*

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 1530. VEH-HRS | 1873. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1530. VEH-HRS | 1873. PASS-HRS |
| TOTAL TRAV DISTANCE = | 93857. VEH-MI. | 114929. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 61. MPH. | 62. MPH. |

AVERAGE DENSITY = 22. VPMPL
 TOTAL FUEL = 4567. GALLONS
 TOTAL EMISSIONS = 1211. KI LOGRAMS

SR-237_EB_AM_P1_2018_PE
 19. VPMPL
 7940. GALLONS
 2106. KI LOGRAMS

1 INSTITUTE OF TRANSPORTATION STUDIES
 UNIVERSITY OF CALIFORNIA, BERKELEY

FREQ12PE REL 3.01
 SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 2

3/31/2016 15:16

PAGE 9

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.26 | 2 | 51.63 | 3 | 17.77 | 4 | 0.20 | 5 | 0.17 |
| 6 | 0.20 | 7 | 0.37 | 8 | 0.44 | 9 | 0.44 | 10 | 0.44 |
| 11 | 4.58 | 12 | 0.45 | 13 | 0.40 | 14 | 0.71 | 15 | 1.04 |
| 16 | 1.11 | 17 | 0.64 | 18 | 4.29 | 19 | 0.43 | | |

***** TOTAL DELAY = 85.6 VEH-HRS ***** AVERAGE DELAY = 1.41 MIN/VEH *****

** 19 **

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/31/2016 15:16 PAGE 3
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 1 OF 2

 ** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|-------|-----------------------|------|------|------|------|------|------|------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| + | * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.04 | 0.00 |
| + | * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/31/2016 15:16 PAGE 4
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 1 OF 2

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | | |
|-----------|----------|------------|-----------|------------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|------|---|------|------|
| * SEC LNS | * LENGTH | * ORG | * DES | * ORG | * DES | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | | | |
| * 1 | | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | | |
| * 3 | | | | | | | | | | | | | | | | | | |
| * 4 | | | | | | | | | | | | | | | | | | |
| * 5 | | | | | | | | | | | | | | | | | | |
| * 6 | | | | | | | | | | | | | | | | | | |
| * 7 | | | | | | | | | | | | | | | | | | |
| * 8 | | | | | | | | | | | | | | | | | | |
| * 9 | | | | | | | | | | | | | | | | | | |
| * 10 | | | | | | | | | | | | | | | | | | |
| * 11 | | | | | | | | | | | | | | | | | | |
| * 12 | | | | | | | | | | | | | | | | | | |
| * 13 | 1 | 800. | 758. | 0. | 758. | 758. | 0. | 758. | 1650. | 0. | 0. | 0. | .46 | 62. | 12.2 | B | 21.6 | 12.8 |
| * 14 | 1 | 1400. | 0. | 0. | 758. | 0. | 0. | 758. | 1650. | 0. | 0. | 0. | .46 | 62. | 12.2 | B | 21.6 | 12.8 |
| * 15 | 1 | 1400. | 0. | 0. | 758. | 0. | 0. | 758. | 1650. | 0. | 0. | 0. | .46 | 62. | 12.2 | B | 21.6 | 12.8 |
| * 16 | 1 | 1500. | 0. | 0. | 758. | 0. | 0. | 758. | 1650. | 0. | 0. | 0. | .46 | 62. | 12.2 | B | 21.6 | 12.8 |
| * 17 | 1 | 1500. | 0. | 0. | 758. | 0. | 0. | 758. | 1650. | 0. | 0. | 0. | .46 | 62. | 12.2 | B | 21.6 | 12.8 |
| * 18 | 1 | 10000. | 0. | 758. | 758. | 0. | 758. | 758. | 1650. | 0. | 0. | 0. | .46 | 62. | 12.2 | B | 21.6 | 12.8 |
| * 19 | | | | | | | | | | | | | | | | | | |
| * TOTAL | 16600. | = | 3.1 MILES | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 38. VEH-HRS | 77. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 38. VEH-HRS | 77. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 2382. VEH-MI. | 4765. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | |
| AVERAGE DENSITY = | 12. VPMP | |
| TOTAL FUEL = | 111. GALLONS | |
| TOTAL EMISSIONS = | 30. KILOGRAMS | |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/31/2016 15:16 PAGE 5
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 1 OF 2
 Page 2

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.09 | 14 | 0.15 | 15 | 0.15 |
| 16 | 0.16 | 17 | 0.16 | 18 | 1.07 | 19 | 0.00 | | |

***** TOTAL DELAY = 1.8 VEH-HRS ***** AVERAGE DELAY = 0.14 MIN/VEH *****

 ** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|------|-----------------------|------|------|------|------|------|------|------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| + * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.04 | 0.00 |
| + * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|-----------|--------|------------|-----------|--------------------|-----------|----------|-----------------|-----------|---------|----------------|-----------|---------|-------------|-------------|
| * SEC | * LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * CAP | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 13 | 1 | 800. | 1014. | 0. 1014. | 1014. | 0. 1014. | 1650. | 0. | 0. | 0. | .61 | 62. | 16.4 | B 21.6 12.8 |
| * 14 | 1 | 1400. | 0. 1014. | 0. 1014. | 0. 1014. | 1650. | 0. | 0. | 0. | .61 | 62. | 16.4 | B 21.6 12.8 | |
| * 15 | 1 | 1400. | 0. 1014. | 0. 1014. | 0. 1014. | 1650. | 0. | 0. | 0. | .61 | 62. | 16.4 | B 21.6 12.8 | |
| * 16 | 1 | 1500. | 0. 1014. | 0. 1014. | 0. 1014. | 1650. | 0. | 0. | 0. | .61 | 62. | 16.4 | B 21.6 12.8 | |
| * 17 | 1 | 1500. | 0. 1014. | 0. 1014. | 0. 1014. | 1650. | 0. | 0. | 0. | .61 | 62. | 16.4 | B 21.6 12.8 | |
| * 18 | 1 | 10000. | 0. 1014. | 1014. | 0. 1014. | 1014. | 1650. | 0. | 0. | 0. | .61 | 62. | 16.4 | B 21.6 12.8 |
| * 19 | | | | | | | | | | | | | | |
| * TOTAL | 16600. | = | 3.1 MILES | | | | MAX(V/C) = 0.61 | | | LOWEST LOS = B | AVG = 62. | 16.4 | 21.6 | 12.8 |

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|-----------------------------|--------------------|----------------|-------------------|-----------------|
| FREWAY TRAVEL TIME = | 51. VEH-HRS | 103. PASS-HRS | 90. VEH-HRS | 180. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 51. VEH-HRS | 103. PASS-HRS | 90. VEH-HRS | 180. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 3189. VEH-MI. | 6377. PASS-MI. | 5571. VEH-MI. | 11142. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | | 62. MPH. | |
| AVERAGE DENSITY = | 16. VPMP | | 14. VPMP | |
| TOTAL FUEL = | 148. GALLONS | | 258. GALLONS | |

TOTAL EMISSIONS = 41. KILOGRAMS

SR-237_EB_AM_P1_2018_PL
71. KILOGRAMS

1 INSTITUTE OF TRANSPORTATION STUDIES
UNIVERSITY OF CALIFORNIA, BERKELEY

FREQ12PL REL 3.01
SHORT TERM SIMULATION OF PRIORITY LANE
TIME SLICE 2 OF 2

3/31/2016 15:16

PAGE 8

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.11 | 14 | 0.20 | 15 | 0.20 |
| 16 | 0.21 | 17 | 0.21 | 18 | 1.43 | 19 | 0.00 | | |

***** TOTAL DELAY = 2.4 VEH-HRS ***** AVERAGE DELAY = 0.14 MIN/VEH *****

```

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQQ QQQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP EEEEEEEEE
    
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FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 62
LOWER LIMB (AT V/C=1) = 30
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREEWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT DES TRUCKS | SPECIAL RAMP | FF. SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION LOCATION |
|---------|----------|----------|-------------|--------------|---------|---------|-----------|---------|----------------|--------------|-------------------|---------------|----------|----------------|------------------------|
| ** 1 | 3 | 6000. | 500. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Seeding |
| ** 2 | 3 | 6000. | 99999. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture |
| ** 3 | 2 | 4000. | 12000. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** 4 | 3 | 4430. | 350. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Maude On-Ramp |
| ** 5 | 3 | 4430. | 300. | 62 | | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Maude to US-101 |
| ** 6 | 3 | 4430. | 350. | 62 | D | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US-101 Off-ramp |
| ** 7 | 2 | 4000. | 940. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | US101SB / US101SB |
| ** 8 | 3 | 4650. | 700. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US101 SB On-ramp |
| ** 9 | 3 | 4650. | 700. | 62 | | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US 101 / Mathilda |
| ** 10 | 3 | 4650. | 700. | 62 | D | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-ramp |
| ** 11 | 2 | 4000. | 2300. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda |
| ** 12 | 3 | 4810. | 700. | 62 | OD | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda On-Ramp |
| ** 13 | 3 | 4270. | 800. | 62 | | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda / Persian HOV |
| ** 14 | 3 | 4270. | 1400. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks Off-Ramp |
| ** 15 | 2 | 4000. | 1400. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | West of Lawrence E |
| ** 16 | 2 | 4000. | 1500. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence Off-ramp |
| ** 17 | 2 | 4000. | 1500. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End of DKS |
| ** 18 | 2 | 4000. | 10000. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** 19 | 3 | 5600. | 750. | 62 | OD | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End of the network |

***** INPUT HAS BEEN COMPLETED *****

**
** FREeway TRAVEL TIME (MINUTES) **
**

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | |
|-----------|-------|-----------------------|-------|-------|-------|-------|-------|---|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 20.80 | 21.36 | 21.91 | 22.31 | 22.84 | 23.12 | 25.09 | |
| * 2 * | 0.18 | 0.74 | 1.29 | 1.69 | 2.23 | 2.50 | 4.47 | |
| * 3 * | 0.00 | 0.38 | 0.93 | 1.34 | 1.87 | 2.14 | 4.11 | |
| * 4 * | 0.00 | 0.00 | 0.13 | 0.53 | 1.06 | 1.34 | 3.31 | |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.14 | |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB | * NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | |
|---------|---------|----------|------------|-----------|-------------|-----------|-----------------|---------|----------------|-----------|-----------|---------|-----------|---------|--------|-------------|--------|--|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * ORG | * DES | * SSEC | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | |
| * 1 | * 3 | * 500. | * 2661. | * 0. | * 2661. | * 2661. | * 0. | * 2661. | * 6000. | * 0. | * 0. | * .44 | * 62. | * 14.3 | * B | * 20.3 | * 13.0 | |
| * 2 | * 3 | * 99999. | * 0. | * 0. | * 2661. | * 0. | * 0. | * 2661. | * 6000. | * 0. | * 0. | * .44 | * 62. | * 14.3 | * B | * 20.3 | * 13.0 | |
| * 3 | * 2 | * 12000. | * 0. | * 0. | * 2661. | * 0. | * 0. | * 2661. | * 4000. | * 0. | * 0. | * .67 | * 62. | * 21.5 | * C | * 20.3 | * 13.0 | |
| * 4 | * 3 | * 350. | * 250. | * 0. | * 2911. | * 250. | * 0. | * 2911. | * 4430. | * 0. | * 0. | * .66 | * 62. | * 15.7 | * B | * 20.3 | * 13.0 | |
| * 5 | * 3 | * 300. | * 0. | * 0. | * 2911. | * 0. | * 0. | * 2911. | * 4430. | * 0. | * 0. | * .66 | * 62. | * 15.7 | * B | * 20.3 | * 13.0 | |
| * 6 | * 3 | * 350. | * 0. | * 900. | * 2911. | * 0. | * 900. | * 2911. | * 4430. | * 0. | * 0. | * .66 | * 62. | * 15.7 | * B | * 20.3 | * 13.0 | |
| * 7 | * 2 | * 940. | * 0. | * 0. | * 2011. | * 0. | * 0. | * 2011. | * 4000. | * 0. | * 0. | * .50 | * 62. | * 16.2 | * B | * 20.3 | * 13.0 | |
| * 8 | * 3 | * 700. | * 1472. | * 0. | * 3483. | * 1472. | * 0. | * 3483. | * 4650. | * 0. | * 0. | * .75 | * 62. | * 18.7 | * C | * 20.3 | * 13.0 | |
| * 9 | * 3 | * 700. | * 0. | * 0. | * 3483. | * 0. | * 0. | * 3483. | * 4650. | * 0. | * 0. | * .75 | * 62. | * 18.7 | * C | * 20.3 | * 13.0 | |
| * 10 | * 3 | * 700. | * 0. | * 521. | * 3483. | * 0. | * 521. | * 3483. | * 4650. | * 0. | * 0. | * .75 | * 62. | * 18.7 | * C | * 20.3 | * 13.0 | |
| * 11 | * 2 | * 2300. | * 0. | * 0. | * 2962. | * 0. | * 0. | * 2962. | * 4000. | * 0. | * 0. | * .74 | * 62. | * 23.9 | * C | * 20.3 | * 13.0 | |
| * 12 | * 3 | * 700. | * 470. | * 751. | * 3432. | * 470. | * 751. | * 3432. | * 4810. | * 0. | * 0. | * .71 | * 62. | * 18.5 | * C | * 20.3 | * 13.0 | |
| * 13 | * 3 | * 800. | * 0. | * 0. | * 2681. | * 0. | * 0. | * 2681. | * 4270. | * 0. | * 0. | * .63 | * 62. | * 14.4 | * B | * 20.3 | * 13.0 | |
| * 14 | * 3 | * 1400. | * 0. | * 231. | * 2681. | * 0. | * 231. | * 2681. | * 4270. | * 0. | * 0. | * .63 | * 62. | * 14.4 | * B | * 20.3 | * 13.0 | |
| * 15 | * 2 | * 1400. | * 0. | * 0. | * 2450. | * 0. | * 0. | * 2450. | * 4000. | * 0. | * 0. | * .61 | * 62. | * 19.8 | * C | * 20.3 | * 13.0 | |
| * 16 | * 2 | * 1500. | * 0. | * 200. | * 2450. | * 0. | * 200. | * 2450. | * 4000. | * 0. | * 0. | * .61 | * 62. | * 19.8 | * C | * 20.3 | * 13.0 | |
| * 17 | * 2 | * 1500. | * 0. | * 0. | * 2250. | * 0. | * 0. | * 2250. | * 4000. | * 0. | * 0. | * .56 | * 62. | * 18.1 | * C | * 20.3 | * 13.0 | |
| * 18 | * 2 | * 10000. | * 0. | * 0. | * 2250. | * 0. | * 0. | * 2250. | * 4000. | * 0. | * 0. | * .56 | * 62. | * 18.1 | * C | * 20.3 | * 13.0 | |
| * 19 | * 3 | * 750. | * 750. | * 3000. | * 3000. | * 750. | * 3000. | * 3000. | * 5600. | * 0. | * 0. | * .54 | * 62. | * 16.1 | * B | * 20.3 | * 13.0 | |
| ***** | | | | | | | | | | | | | | | | | | |
| * TOTAL | 136889. | | = | | 25.9 MI LBS | | MAX(V/C) = 0.75 | | LOWEST LOS = C | | AVG = 62. | | 15.7 | | 20.3 | | 13.0 | |
| ***** | | | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 1105. VEH-HRS | 1353. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1105. VEH-HRS | 1353. PASS-HRS |
| TOTAL TRAV DISTANCE = | 68526. VEH-MI. | 83888. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH | 62. MPH |
| AVERAGE DENSITY = | 16. VPMP | 16. VPMP |
| TOTAL FUEL = | 3369. GALLONS | 3369. GALLONS |
| TOTAL EMISSIONS = | 894. KI LOGRAMS | 894. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.19 | 2 | 37.52 | 3 | 4.50 | 4 | 0.14 | 5 | 0.12 |
| 6 | 0.14 | 7 | 0.27 | 8 | 0.34 | 9 | 0.34 | 10 | 0.34 |
| 11 | 0.96 | 12 | 0.34 | 13 | 0.30 | 14 | 0.53 | 15 | 0.48 |
| 16 | 0.52 | 17 | 0.48 | 18 | 3.17 | 19 | 0.32 | | |

***** TOTAL DELAY = 51.0 VEH-HRS ***** AVERAGE DELAY = 1.16 MIN/VEH *****

**
** FREEWAY TRAVEL TIME (MINUTES)
**

| * ORIGINS | * DESTINATIONS ACROSS | | | | | | |
|-----------|-----------------------|-------|-------|-------|-------|-------|-------|
| * DOWN | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 20.99 | 21.55 | 22.15 | 22.55 | 23.10 | 23.37 | 25.34 |
| * 2 * | 0.18 | 0.74 | 1.34 | 1.75 | 2.29 | 2.56 | 4.54 |
| * 3 * | 0.00 | 0.38 | 0.99 | 1.39 | 1.93 | 2.21 | 4.18 |
| * 4 * | 0.00 | 0.00 | 0.13 | 0.53 | 1.08 | 1.35 | 3.32 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.14 |

*
* TIME SLICE FREEWAY PERFORMANCE TABLE
*

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|-----------|----------|-------------|-------------|-------------|-------------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|
| * SEC LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 1 3 | 500. | 3660. | 0. 3660. | 3660. | 0. 3660. | 6000. | 0. | 0. | 0. | .61 | 62. | 19.7 | C | 20.3 | 13.0 |
| * 2 3 | 99999. | 0. | 0. 3660. | 0. | 0. 3660. | 6000. | 0. | 0. | 0. | .61 | 62. | 19.7 | C | 20.3 | 13.0 |
| * 3 2 | 12000. | 0. | 0. 3660. | 0. | 0. 3660. | 4000. | 0. | 0. | 0. | .92 | 57. | 32.0 | D | 22.2 | 11.8 |
| * 4 3 | 350. | 430. | 0. 4090. | 430. | 0. 4090. | 4430. | 0. | 0. | 0. | .92 | 62. | 22.0 | C | 20.3 | 13.0 |
| * 5 3 | 300. | 0. | 0. 4090. | 0. | 0. 4090. | 4430. | 0. | 0. | 0. | .92 | 62. | 22.0 | C | 20.3 | 13.0 |
| * 6 3 | 350. | 0. | 1270. 4090. | 0. | 1270. 4090. | 4430. | 0. | 0. | 0. | .92 | 62. | 22.0 | C | 20.3 | 13.0 |
| * 7 2 | 940. | 0. | 0. 2820. | 0. | 0. 2820. | 4000. | 0. | 0. | 0. | .70 | 62. | 22.7 | C | 20.3 | 13.0 |
| * 8 3 | 700. | 1631. | 0. 4451. | 1631. | 0. 4451. | 4650. | 0. | 0. | 0. | .96 | 62. | 23.9 | C | 20.3 | 13.0 |
| * 9 3 | 700. | 0. | 0. 4451. | 0. | 0. 4451. | 4650. | 0. | 0. | 0. | .96 | 62. | 23.9 | C | 20.3 | 13.0 |
| * 10 3 | 700. | 0. | 650. 4451. | 0. | 650. 4451. | 4650. | 0. | 0. | 0. | .96 | 62. | 23.9 | C | 20.3 | 13.0 |
| * 11 2 | 2300. | 0. | 0. 3801. | 0. | 0. 3801. | 4000. | 0. | 0. | 0. | .95 | 55. | 34.5 | D | 22.8 | 11.4 |
| * 12 3 | 700. | 744. | 1002. 4545. | 744. | 1002. 4545. | 4810. | 0. | 0. | 0. | .94 | 62. | 24.4 | C | 20.3 | 13.0 |
| * 13 3 | 800. | 0. | 0. 3543. | 0. | 0. 3543. | 4270. | 0. | 0. | 0. | .83 | 62. | 19.0 | C | 20.3 | 13.0 |
| * 14 3 | 1400. | 0. | 270. 3543. | 0. | 270. 3543. | 4270. | 0. | 0. | 0. | .83 | 62. | 19.0 | C | 20.3 | 13.0 |
| * 15 2 | 1400. | 0. | 0. 3273. | 0. | 0. 3273. | 4000. | 0. | 0. | 0. | .82 | 61. | 27.0 | D | 21.0 | 12.6 |
| * 16 2 | 1500. | 0. | 270. 3273. | 0. | 270. 3273. | 4000. | 0. | 0. | 0. | .82 | 61. | 27.0 | D | 21.0 | 12.6 |
| * 17 2 | 1500. | 0. | 0. 3003. | 0. | 0. 3003. | 4000. | 0. | 0. | 0. | .75 | 62. | 24.2 | C | 20.3 | 13.0 |
| * 18 2 | 10000. | 0. | 0. 3003. | 0. | 0. 3003. | 4000. | 0. | 0. | 0. | .75 | 62. | 24.2 | C | 20.3 | 13.0 |
| * 19 3 | 750. | 1001. 4004. | 0. 4004. | 1001. 4004. | 0. 4004. | 5600. | 0. | 0. | 0. | .71 | 62. | 21.5 | C | 20.3 | 13.0 |

*
* TOTAL 136889. = 25.9 MILES MAX(V/C) = 0.96 LOWEST LOS = D AVG = 61. 21.7 20.5 12.9
*

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|----------------------------|--------------------|------------------|-------------------|------------------|
| FREWAY TRAVEL TIME = | 1526. VEH-HRS | 1870. PASS-HRS | 2632. VEH-HRS | 3223. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1526. VEH-HRS | 1870. PASS-HRS | 2632. VEH-HRS | 3223. PASS-HRS |
| TOTAL TRAV DISTANCE = | 93671. VEH-MI. | 114729. PASS-MI. | 162197. VEH-MI. | 198616. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 61. MPH. | | 62. MPH. | |

AVERAGE DENSITY = 22. VPMP
 TOTAL FUEL = 4559. GALLONS
 TOTAL EMISSIONS = 1209. KI LOGRAMS

SR-237_EB_AM_P2_2018_PE
 19. VPMP
 7928. GALLONS
 2103. KI LOGRAMS

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FREQ12PE REL 3.01
 SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 2

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***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.26 | 2 | 51.60 | 3 | 17.69 | 4 | 0.20 | 5 | 0.17 |
| 6 | 0.20 | 7 | 0.37 | 8 | 0.44 | 9 | 0.44 | 10 | 0.44 |
| 11 | 4.57 | 12 | 0.45 | 13 | 0.40 | 14 | 0.70 | 15 | 0.97 |
| 16 | 1.03 | 17 | 0.64 | 18 | 4.23 | 19 | 0.42 | | |

***** TOTAL DELAY = 85.2 VEH-HRS ***** AVERAGE DELAY = 1.41 MIN/VEH *****

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1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/31/2016 15:17 PAGE 3
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 1 OF 2

 ** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|--|-----------------------|------|------|------|------|------|------|------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 3 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 4 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 5 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.04 | 0.00 |
| * 6 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/31/2016 15:17 PAGE 4
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 1 OF 2

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | | |
|-----------|----------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|--------|---------|-----------|---------|--------|-------------|---|------|------|--|
| * SEC LNS | * LENGTH | * ORG | * DES | * ORG | * DES | * SSEC | * CAP | * EFF | * LENGTH | * RATE | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | | | |
| * 1 | | | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | | | |
| * 3 | | | | | | | | | | | | | | | | | | | |
| * 4 | | | | | | | | | | | | | | | | | | | |
| * 5 | | | | | | | | | | | | | | | | | | | |
| * 6 | | | | | | | | | | | | | | | | | | | |
| * 7 | | | | | | | | | | | | | | | | | | | |
| * 8 | | | | | | | | | | | | | | | | | | | |
| * 9 | | | | | | | | | | | | | | | | | | | |
| * 10 | | | | | | | | | | | | | | | | | | | |
| * 11 | | | | | | | | | | | | | | | | | | | |
| * 12 | | | | | | | | | | | | | | | | | | | |
| * 13 | 1 | 800. | 750. | 0. | 750. | 750. | 0. | 750. | 1650. | 0. | 0. | 0. | .45 | 62. | 12.1 | B | 21.6 | 12.8 | |
| * 14 | 1 | 1400. | 0. | 0. | 750. | 0. | 0. | 750. | 1650. | 0. | 0. | 0. | .45 | 62. | 12.1 | B | 21.6 | 12.8 | |
| * 15 | 1 | 1400. | 0. | 0. | 750. | 0. | 0. | 750. | 1650. | 0. | 0. | 0. | .45 | 62. | 12.1 | B | 21.6 | 12.8 | |
| * 16 | 1 | 1500. | 0. | 0. | 750. | 0. | 0. | 750. | 1650. | 0. | 0. | 0. | .45 | 62. | 12.1 | B | 21.6 | 12.8 | |
| * 17 | 1 | 1500. | 0. | 0. | 750. | 0. | 0. | 750. | 1650. | 0. | 0. | 0. | .45 | 62. | 12.1 | B | 21.6 | 12.8 | |
| * 18 | 1 | 10000. | 0. | 750. | 750. | 0. | 750. | 750. | 1650. | 0. | 0. | 0. | .45 | 62. | 12.1 | B | 21.6 | 12.8 | |
| * 19 | | | | | | | | | | | | | | | | | | | |
| * TOTAL | 16600. | = | 3.1 | MILES | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 38. VEH-HRS | 76. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 38. VEH-HRS | 76. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 2358. VEH-MI. | 4716. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 62. MPH. |
| AVERAGE DENSITY = | 12. VPMP | 12. VPMP |
| TOTAL FUEL = | 109. GALLONS | 109. GALLONS |
| TOTAL EMISSIONS = | 30. KILOGRAMS | 30. KILOGRAMS |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/31/2016 15:17 PAGE 5
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 1 OF 2
 Page 2

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.08 | 14 | 0.15 | 15 | 0.15 |
| 16 | 0.16 | 17 | 0.16 | 18 | 1.06 | 19 | 0.00 | | |

***** TOTAL DELAY = 1.8 VEH-HRS ***** AVERAGE DELAY = 0.14 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/31/2016 15:17 PAGE 6
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 2

 **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|-----|-----------------------|------|------|------|------|------|------|------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| + * | * | | | | | | | | |
| + * | * | | | | | | | | |
| + * | 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + * | 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + * | 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + * | 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + * | 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.04 | 0.00 |
| + * | 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + * | * | | | | | | | | |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/31/2016 15:17 PAGE 7
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 2

 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *

| * SUB | * NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | |
|---------|-------|----------|------------|-----------|--------------------|--------|---------|-----------|-----------|-----------------|----------------|-----------|-----------|--------|-------------|------|------|------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * ORG | * DES | * CAP. | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | | |
| * 1 | | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | | |
| * 3 | | | | | | | | | | | | | | | | | | |
| * 4 | | | | | | | | | | | | | | | | | | |
| * 5 | | | | | | | | | | | | | | | | | | |
| * 6 | | | | | | | | | | | | | | | | | | |
| * 7 | | | | | | | | | | | | | | | | | | |
| * 8 | | | | | | | | | | | | | | | | | | |
| * 9 | | | | | | | | | | | | | | | | | | |
| * 10 | | | | | | | | | | | | | | | | | | |
| * 11 | | | | | | | | | | | | | | | | | | |
| * 12 | | | | | | | | | | | | | | | | | | |
| * 13 | 1 | 800. | 1001. | 0. | 1001. | 1001. | 0. | 1001. | 1650. | 0. | 0. | 0. | .61 | 62. | 16.1 | B | 21.6 | 12.8 |
| * 14 | 1 | 1400. | 0. | 0. | 1001. | 0. | 0. | 1001. | 1650. | 0. | 0. | 0. | .61 | 62. | 16.1 | B | 21.6 | 12.8 |
| * 15 | 1 | 1400. | 0. | 0. | 1001. | 0. | 0. | 1001. | 1650. | 0. | 0. | 0. | .61 | 62. | 16.1 | B | 21.6 | 12.8 |
| * 16 | 1 | 1500. | 0. | 0. | 1001. | 0. | 0. | 1001. | 1650. | 0. | 0. | 0. | .61 | 62. | 16.1 | B | 21.6 | 12.8 |
| * 17 | 1 | 1500. | 0. | 0. | 1001. | 0. | 0. | 1001. | 1650. | 0. | 0. | 0. | .61 | 62. | 16.1 | B | 21.6 | 12.8 |
| * 18 | 1 | 10000. | 0. | 1001. | 1001. | 0. | 1001. | 1001. | 1650. | 0. | 0. | 0. | .61 | 62. | 16.1 | B | 21.6 | 12.8 |
| * 19 | | | | | | | | | | | | | | | | | | |
| * TOTAL | | 16600. | = | 3.1 | MI LBS | | | | | | | | | | | | | |
| | | | | | | | | | | MAX(V/C) = 0.61 | LOWEST LOS = B | | AVG = 62. | 16.1 | 21.6 | 12.8 | | |

| | CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | |
|-----------------------------|--------------------|---------|-------|----------|-------------------|---------|--------|----------|
| FREWAY TRAVEL TIME = | 51. | VEH-HRS | 102. | PASS-HRS | 89. | VEH-HRS | 178. | PASS-HRS |
| FREWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 51. | VEH-HRS | 102. | PASS-HRS | 89. | VEH-HRS | 178. | PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 3147. | VEH-MI. | 6294. | PASS-MI. | 5505. | VEH-MI. | 11010. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. | MPH. | | | 62. | MPH. | | |
| AVERAGE DENSITY = | 16. | VPMP | | | 14. | VPMP | | |
| TOTAL FUEL = | 146. | GALLONS | | | 255. | GALLONS | | |

TOTAL EMISSIONS = 40. KILOGRAMS

SR-237_EB_AM_P2_2018_PL
70. KILOGRAMS

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FREQ12PL REL 3.01
SHORT TERM SIMULATION OF PRIORITY LANE
TIME SLICE 2 OF 2

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***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.11 | 14 | 0.20 | 15 | 0.20 |
| 16 | 0.21 | 17 | 0.21 | 18 | 1.41 | 19 | 0.00 | | |

***** TOTAL DELAY = 2.3 VEH-HRS ***** AVERAGE DELAY = 0.14 MIN/VEH *****

```

FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFFF RRRRRRRR EEEEEEEEE Q* A. D. MAY* Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP EEE
FFFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP EEE
FFF RRR RRR EEE Q* UC* QQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE Q* REGENTS* Q 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q* 1999* Q Q 1111111 2222222222 PPP EEEEEEEEE

```

FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 62
LOWER LIMB (AT V/C=1) = 30
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65 MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

```

*****
**
** FREEWAY AND ARTERIAL DESIGN FEATURES
**
*****
**
** SUB NO. SSEC SSEC DESIGN ORG TRK SSEC PCT PCT DES SPECIAL FF. SPD. CAP. ART GRADE SUBSECTION LOCATION
** SEC LNS CAP LENGTH SPEED DES FAC GRAD TRK TRUCKS RAMP ALT. RTE ALT. RTE TYPE ALT. RTE
**
** 1 3 6000. 500. 62 0 0.95 0.0 5 0 NO 0.0 0. GOOD 0.0 Seeding
**
** 2 3 6000. 99999. 62 0.95 0.0 5 0 NO 0.0 0. GOOD 0.0 Queue Capture
**
** 3 2 4000. 12000. 62 0.95 0.0 5 0 NO 0.0 0. GOOD 0.0 HOV Dummy
**
** 4 3 4720. 350. 62 0 0.95 0.0 5 0 YES 0.0 0. GOOD 0.0 Maude On-ramp
**
** 5 3 4720. 300. 62 0.95 0.0 5 0 YES 0.0 0. GOOD 0.0 Maude to US-101
**
** 6 3 4720. 350. 62 D 0.95 0.0 5 0 YES 0.0 0. GOOD 0.0 US-101 Off-Ramp
**
** 7 2 4000. 940. 62 0.95 0.0 5 0 NO 0.0 0. GOOD 0.0 US101SB / US101SB
**
** 8 3 4410. 700. 62 0 0.95 0.0 5 0 YES 0.0 0. GOOD 0.0 US101 SB On-ramp
**
** 9 3 4410. 700. 62 0.95 0.0 5 0 YES 0.0 0. GOOD 0.0 US 101 / Mathilda
**
** 10 3 4410. 700. 62 D 0.95 0.0 5 0 YES 0.0 0. GOOD 0.0 Mathilda Off-ramp
**
** 11 2 4000. 2300. 62 0.95 0.0 5 0 NO 0.0 0. GOOD 0.0 Mathilda / Mathilda
**
** 12 3 5030. 700. 62 OD 0.95 0.0 5 0 YES 0.0 0. GOOD 0.0 Mathilda On-Ramp
**
** 13 3 4340. 800. 62 0.95 0.0 5 0 YES 0.0 0. GOOD 0.0 Mathilda / Persian HOV
**
** 14 3 4340. 1400. 62 D 0.95 0.0 5 0 NO 0.0 0. GOOD 0.0 Persian On-Ramp w/HOV
**
** 15 2 4000. 1400. 62 0.95 0.0 5 0 NO 0.0 0. GOOD 0.0 West of Lawrence E
**
** 16 2 4000. 1500. 62 D 0.95 0.0 5 0 NO 0.0 0. GOOD 0.0 Lawrence Off-ramp
**
** 17 2 4000. 1500. 62 D 0.95 0.0 5 0 NO 0.0 0. GOOD 0.0 End of DKS
**
** 18 2 4000. 5000. 62 0.95 0.0 5 0 NO 0.0 0. GOOD 0.0 HOV Dummy
**
** 19 2 4000. 5000. 62 0 0.95 0.0 5 0 NO 0.0 0. GOOD 0.0 Buffer
**
** 20 3 2500. 750. 62 OD 0.95 0.0 5 0 YES 0.0 0. GOOD 0.0 Dummy Queue Spillback
**
*****

```

***** INPUT HAS BEEN COMPLETED *****

**
** FREEWAY TRAVEL TIME (MINUTES) **
**

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | |
|-----------|--|-----------------------|-------|-------|-------|-------|-------|-------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | | 20.80 | 21.36 | 22.04 | 23.28 | 26.33 | 29.45 | 66.21 |
| * 2 * | | 0.18 | 0.74 | 1.42 | 2.66 | 5.71 | 8.83 | 45.59 |
| * 3 * | | 0.00 | 0.38 | 1.07 | 2.31 | 5.36 | 8.47 | 45.23 |
| * 4 * | | 0.00 | 0.00 | 0.22 | 1.45 | 4.51 | 7.62 | 44.38 |
| * 5 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 17.72 |
| * 6 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.14 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB | * NO. | * SSEC | * O-D | * DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | |
|---------|---------|----------|-------|--------|-----------|------------|-----------|--------|---------|-----------|-----------|--------|---------|-----------|--------|--------|-------------|------|------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * MPG | * GS/VM | | |
| * 1 | 3 | 500. | 1939. | 0. | 1939. | 1939. | 0. | 1939. | 6000. | 0. | 0. | 0. | .32 | 62. | 10.4 | A | 20.3 | 13.0 | |
| * 2 | 3 | 99999. | 0. | 0. | 1939. | 0. | 0. | 1939. | 6000. | 0. | 0. | 0. | .32 | 62. | 10.4 | A | 20.3 | 13.0 | |
| * 3 | 2 | 12000. | 0. | 0. | 1939. | 0. | 0. | 1939. | 4000. | 0. | 0. | 0. | .48 | 62. | 15.6 | B | 20.3 | 13.0 | |
| * 4 | 3 | 350. | 650. | 0. | 2589. | 550. | 0. | 2489. | 4720. | 0. | 0. | 0. | .53 | 62. | 13.4 | B | 20.3 | 13.0 | |
| * 5 | 3 | 300. | 0. | 0. | 2589. | 0. | 0. | 2489. | 4720. | 0. | 0. | 0. | .53 | 62. | 13.4 | B | 20.3 | 13.0 | |
| * 6 | 3 | 350. | 0. | 600. | 2589. | 0. | 577. | 2489. | 4720. | 0. | 0. | 0. | .53 | 62. | 13.4 | B | 20.3 | 13.0 | |
| * 7 | 2 | 940. | 0. | 0. | 1989. | 0. | 0. | 1912. | 4000. | 0. | 0. | 0. | .48 | 62. | 15.4 | B | 20.3 | 13.0 | |
| * 8 | 3 | 700. | 857. | 0. | 2846. | 857. | 0. | 2769. | 4410. | 0. | 0. | 0. | .63 | 62. | 14.9 | B | 20.3 | 13.0 | |
| * 9 | 3 | 700. | 0. | 0. | 2846. | 0. | 0. | 2769. | 4410. | 0. | 0. | 0. | .63 | 62. | 14.9 | B | 20.3 | 13.0 | |
| * 10 | 3 | 700. | 0. | 309. | 2846. | 0. | 301. | 2769. | 4410. | 0. | 0. | 0. | .63 | 62. | 14.9 | B | 20.3 | 13.0 | |
| * 11 | 2 | 2300. | 0. | 0. | 2537. | 0. | 0. | 887. | 4000. | 0. | * | 905. | 1582. | .22 | 56. | 7.9 | F | 20.2 | 13.1 |
| * 12 | 3 | 700. | 830. | 725. | 3367. | 730. | 689. | 1617. | 5030. | 0. | ** | 700. | 1582. | .32 | 37. | 14.7 | F | 19.4 | 13.6 |
| * 13 | 3 | 800. | 0. | 0. | 2642. | 0. | 0. | 928. | 4340. | 0. | ** | 800. | 1582. | .21 | 25. | 12.3 | F | 19.1 | 13.7 |
| * 14 | 3 | 1400. | 0. | 220. | 2642. | 0. | 209. | 928. | 4340. | 0. | ** | 1400. | 1582. | .21 | 18. | 17.0 | F | 18.4 | 14.2 |
| * 15 | 2 | 1400. | 0. | 0. | 2422. | 0. | 0. | 719. | 4000. | 0. | ** | 1400. | 1582. | .18 | 13. | 28.5 | F | 17.9 | 14.5 |
| * 16 | 2 | 1500. | 0. | 361. | 2422. | 0. | 343. | 719. | 4000. | 0. | ** | 1500. | 1582. | .18 | 10. | 37.7 | F | 17.1 | 15.2 |
| * 17 | 2 | 1500. | 0. | 0. | 2061. | 0. | 0. | 376. | 4000. | 0. | ** | 1500. | 1582. | .09 | 5. | 34.3 | F | 17.3 | 14.9 |
| * 18 | 2 | 5000. | 0. | 0. | 2061. | 0. | 0. | 376. | 4000. | 0. | ** | 5000. | 1582. | .09 | 3. | 63.0 | F | 15.3 | 16.7 |
| * 19 | 2 | 5000. | 724. | 0. | 2785. | 724. | 0. | 1100. | 4000. | 0. | ** | 5000. | 1582. | .28 | 3. | 170.2 | F | 9.8 | 24.9 |
| * 20 | 3 | 750. | 1400. | 4185. | 4185. | 1400. | 2500. | 2500. | 2500. | 0. | 0. | 0. | 1.00 | 62. | 13.4 | E | 20.3 | 13.0 | |
| * TOTAL | 136889. | = | 25.9 | MILES | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 1635. VEH-HRS | 1941. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 100. VEH-HRS | 100. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1735. VEH-HRS | 2041. PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 49554. VEH-MI. | 61792. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 29. MPH. | 30. MPH. |
| AVERAGE DENSITY = | 20. VPMP | 20. VPMP |
| TOTAL FUEL = | 2569. GALLONS | 2569. GALLONS |
| TOTAL EMISSIONS = | 683. KILOGRAMS | 683. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|--------|------------|--------|------------|-------|
| 1 | 0.14 | 2 | 27.34 | 3 | 3.28 | 4 | 0.12 | 5 | 0.11 |
| 6 | 0.12 | 7 | 0.25 | 8 | 0.27 | 9 | 0.27 | 10 | 0.27 |
| 11 | 2.63 | 12 | 4.89 | 13 | 8.66 | 14 | 23.47 | 15 | 32.28 |
| 16 | 45.28 | 17 | 61.85 | 18 | 301.45 | 19 | 359.87 | 20 | 0.26 |

***** TOTAL DELAY = 872.8 VEH-HRS ***** AVERAGE DELAY = 87.50 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-----------|-----------------------|---------------|--------------------------------|----------|---------|---------|----------|----------------------|
| ON-RAMP 2 | RAMP 100. | 50.00 | 4.62 | 18.03 | 1.11 | 5.83 | 0.31 | 7.25 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 100. | 50.00 | 4.62 | 18.03 | 1.11 | 5.83 | 0.31 | 7.25 |
| ON-RAMP 4 | RAMP 100. | 50.00 | 3.61 | 18.03 | 1.11 | 5.83 | 0.31 | 7.25 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 100. | 50.00 | 3.61 | 18.03 | 1.11 | 5.83 | 0.31 | 7.25 |

 ** FREEWAY TRAVEL TIME (MINUTES) **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN 1 2 3 4 5 6 7 *

| | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|
| * 1 * | 24.62 | 27.98 | 31.10 | 33.79 | 37.65 | 40.26 | 60.07 |
| * 2 * | 1.13 | 4.50 | 7.62 | 10.30 | 14.16 | 16.77 | 36.59 |
| * 3 * | 0.00 | 1.78 | 4.90 | 7.58 | 11.44 | 14.05 | 33.87 |
| * 4 * | 0.00 | 0.00 | 0.69 | 3.37 | 7.23 | 9.84 | 29.65 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 6.88 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.14 |

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | | | |
|-----------|--------|------------|-----------|------------|-----------|---------|---------|-----------|-----------|-------|----------|-----------|---------|--------|-------------|---------|--------|--------|---------|-----|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * LOS | * MPG | * GS/VM | |
| * 1 | * 3 | * 500. | * 2249. | * 0. | * 2249. | * 2249. | * 0. | * 2249. | * 6000. | * 0. | * 0. | * 0. | * .37 | * 62. | * 12.1 | * B | * 20.3 | * 13.0 | * * | |
| * 2 | * 3 | * 99999. | * 0. | * 0. | * 2249. | * 0. | * 0. | * 2249. | * 6000. | * 0. | * 0. | * 0. | * .37 | * 62. | * 12.1 | * B | * 20.3 | * 13.0 | * * | |
| * 3 | * 2 | * 12000. | * 0. | * 0. | * 2249. | * 0. | * 0. | * 1625. | * 4000. | * 0. | * * | * 5264. | * 624. | * .41 | * 27. | * 30.2 | * F | * 17.9 | * 14.5 | * * |
| * 4 | * 3 | * 350. | * 841. | * 0. | * 3090. | * 841. | * 0. | * 2466. | * 4720. | * 0. | * ** | * 350. | * 624. | * .52 | * 11. | * 77.6 | * F | * 12.2 | * 20.7 | * * |
| * 5 | * 3 | * 300. | * 0. | * 0. | * 3090. | * 0. | * 0. | * 2466. | * 4720. | * 0. | * ** | * 300. | * 624. | * .52 | * 10. | * 81.9 | * F | * 11.9 | * 21.3 | * * |
| * 6 | * 3 | * 350. | * 0. | * 720. | * 3090. | * 0. | * 720. | * 2466. | * 4720. | * 0. | * ** | * 350. | * 624. | * .52 | * 10. | * 86.4 | * F | * 11.6 | * 21.8 | * * |
| * 7 | * 2 | * 940. | * 0. | * 0. | * 2370. | * 0. | * 0. | * 1746. | * 4000. | * 0. | * ** | * 940. | * 624. | * .44 | * 7. | * 129.6 | * F | * 10.4 | * 23.5 | * * |
| * 8 | * 3 | * 700. | * 1445. | * 0. | * 3815. | * 1445. | * 0. | * 3191. | * 4410. | * 0. | * ** | * 700. | * 624. | * .72 | * 14. | * 75.4 | * F | * 14.9 | * 19.7 | * * |
| * 9 | * 3 | * 700. | * 0. | * 0. | * 3815. | * 0. | * 0. | * 3191. | * 4410. | * 0. | * ** | * 700. | * 624. | * .72 | * 13. | * 79.3 | * F | * 14.6 | * 20.2 | * * |
| * 10 | * 3 | * 700. | * 0. | * 409. | * 3815. | * 0. | * 409. | * 3191. | * 4410. | * 0. | * ** | * 700. | * 624. | * .72 | * 13. | * 83.3 | * F | * 14.3 | * 20.7 | * * |
| * 11 | * 2 | * 2300. | * 0. | * 0. | * 3406. | * 0. | * 0. | * 2782. | * 4000. | * 0. | * ** | * 2300. | * 624. | * .70 | * 11. | * 129.4 | * F | * 13.4 | * 22.2 | * * |
| * 12 | * 3 | * 700. | * 885. | * 808. | * 4291. | * 885. | * 812. | * 3667. | * 5030. | * 0. | * ** | * 700. | * 624. | * .73 | * 12. | * 105.4 | * F | * 13.8 | * 21.6 | * * |
| * 13 | * 3 | * 800. | * 0. | * 0. | * 3483. | * 0. | * 0. | * 2855. | * 4340. | * 0. | * ** | * 800. | * 624. | * .66 | * 9. | * 102.2 | * F | * 12.1 | * 23.7 | * * |
| * 14 | * 3 | * 1400. | * 0. | * 340. | * 3483. | * 0. | * 338. | * 2855. | * 4340. | * 0. | * ** | * 1400. | * 624. | * .66 | * 9. | * 102.2 | * F | * 12.1 | * 23.7 | * * |
| * 15 | * 2 | * 1400. | * 0. | * 0. | * 3143. | * 0. | * 0. | * 2517. | * 4000. | * 0. | * ** | * 1400. | * 624. | * .63 | * 9. | * 147.5 | * F | * 11.2 | * 24.7 | * * |
| * 16 | * 2 | * 1500. | * 0. | * 340. | * 3143. | * 0. | * 344. | * 2517. | * 4000. | * 0. | * ** | * 1500. | * 624. | * .63 | * 9. | * 147.5 | * F | * 11.2 | * 24.7 | * * |
| * 17 | * 2 | * 1500. | * 0. | * 499. | * 2803. | * 0. | * 481. | * 2172. | * 4000. | * 0. | * ** | * 1500. | * 624. | * .54 | * 7. | * 166.2 | * F | * 9.4 | * 27.0 | * * |
| * 18 | * 2 | * 5000. | * 0. | * 0. | * 2304. | * 0. | * 0. | * 1691. | * 4000. | * 0. | * ** | * 5000. | * 624. | * .42 | * 4. | * 192.4 | * F | * 8.3 | * 28.9 | * * |
| * 19 | * 2 | * 5000. | * 809. | * 0. | * 3113. | * 809. | * 0. | * 2500. | * 4000. | * 0. | * ** | * 5000. | * 624. | * .63 | * 8. | * 148.4 | * F | * 11.0 | * 24.8 | * * |
| * 20 | * 3 | * 750. | * 0. | * 3113. | * 3113. | * 0. | * 2500. | * 2500. | * 2500. | * 0. | * 0. | * 0. | * 1.00 | * 62. | * 13.4 | * E | * 20.3 | * 13.0 | * * | |

 * TOTAL 136889. = 25.9 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 26. 36.0 17.5 15.3 *

| | CURRENT TIME SLICE | | | CUMULATIVE VALUES | | | | |
|----------------------------|--------------------|------------|--------|-------------------|---------|------------|---------|----------|
| FREEWAY TRAVEL TIME = | 2264. | VEH-HRS | 2690. | PASS-HRS | 3899. | VEH-HRS | 4631. | PASS-HRS |
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 200. | VEH-HRS | 200. | PASS-HRS | 300. | VEH-HRS | 300. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 2464. | VEH-HRS | 2890. | PASS-HRS | 4199. | VEH-HRS | 4931. | PASS-HRS |
| TOTAL TRAV DISTANCE = | 59121. | VEH-MI. | 73522. | PASS-MI. | 108675. | VEH-MI. | 135313. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 24. | MPH. | | | 28. | MPH. | | |
| AVERAGE DENSITY = | 36. | VPMP/L | | | 28. | VPMP/L | | |
| TOTAL FUEL = | 3455. | GALLONS | | | 6024. | GALLONS | | |
| TOTAL EMISSIONS = | 931. | KI LOGRAMS | | | 1613. | KI LOGRAMS | | |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 2/29/2016 13:17 PAGE 9
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 3

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|--------|------------|--------|------------|-------|
| 1 | 0.16 | 2 | 31.71 | 3 | 107.32 | 4 | 14.26 | 5 | 12.94 |
| 6 | 15.94 | 7 | 45.46 | 8 | 24.41 | 9 | 25.82 | 10 | 27.22 |
| 11 | 94.70 | 12 | 34.44 | 13 | 39.78 | 14 | 69.62 | 15 | 67.93 |
| 16 | 72.78 | 17 | 84.94 | 18 | 339.81 | 19 | 244.57 | 20 | 0.26 |

***** TOTAL DELAY = 1354.1 VEH-HRS ***** AVERAGE DELAY = 37.42 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-----------|-----------------------|---------------|--------------------------------|----------|---------|---------|----------|----------------------|
| ON-RAMP 2 | RAMP 100. | 100.00 | 6.38 | 36.06 | 2.23 | 11.66 | 0.62 | 14.51 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 100. | 100.00 | 6.38 | 36.06 | 2.23 | 11.66 | 0.62 | 14.51 |
| ON-RAMP 4 | RAMP 100. | 100.00 | 6.09 | 36.06 | 2.23 | 11.66 | 0.62 | 14.51 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 100. | 100.00 | 6.09 | 36.06 | 2.23 | 11.66 | 0.62 | 14.51 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 2/29/2016 13:17 PAGE 10
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 3 OF 3

 ** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS DOWN | * DESTINATIONS ACROSS * | | | | | | |
|---------------------|-------------------------|-------|-------|-------|-------|-------|-------|
| * * 1 2 3 4 5 6 7 * | | | | | | | |
| * 1 * | 32.53 | 36.87 | 39.89 | 42.30 | 45.59 | 47.81 | 65.65 |
| * 2 * | 1.93 | 6.27 | 9.29 | 11.70 | 14.99 | 17.21 | 35.06 |
| * 3 * | 0.00 | 2.15 | 5.16 | 7.57 | 10.86 | 13.08 | 30.93 |
| * 4 * | 0.00 | 0.00 | 0.70 | 3.12 | 6.41 | 8.63 | 26.47 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 6.88 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.14 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 2/29/2016 13:17 PAGE 11
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 3 OF 3

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISS |
|-----------|--------|------------|-----------|------------|--------|---------|-----------|-----------|--------|---------|-----------|----------|---------|---------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP/L | * LEVEL | * MPG |
| ***** | ***** | ***** | ***** | ***** | ***** | ***** | ***** | ***** | ***** | ***** | ***** | ***** | ***** | ***** |

SR-237_EB_PM_NP_2018_PE.txt

| | | | | | | | | | | | | | | | | | | | | |
|-------|-------|---|--------|---------|-------|-------|--------|-----------------|-------|-------|----------------|-----------|-------|-------|------|------|---|------|------|---|
| * | 1 | 3 | 500. | 1650. | 0. | 1650. | 1650. | 0. | 1650. | 6000. | 0. | 0. | 0. | .28 | 62. | 8.9 | A | 20.3 | 13.0 | * |
| * | 2 | 3 | 99999. | 0. | 0. | 1650. | 0. | 0. | 1650. | 6000. | 0. | 0. | 0. | .28 | 62. | 8.9 | A | 20.3 | 13.0 | * |
| * | 3 | 2 | 12000. | 0. | 0. | 1650. | 0. | 0. | 1778. | 4000. | 0. | ** | 3325. | -128. | .44 | 11. | F | 13.2 | 19.0 | * |
| * | 4 | 3 | 350. | 629. | 0. | 2279. | 629. | 0. | 2407. | 4720. | 0. | ** | 350. | -128. | .51 | 6. | F | 8.9 | 27.8 | * |
| * | 5 | 3 | 300. | 0. | 0. | 2279. | 0. | 0. | 2407. | 4720. | 0. | ** | 300. | -128. | .51 | 6. | F | 8.9 | 27.8 | * |
| * | 6 | 3 | 350. | 0. | 600. | 2279. | 0. | 597. | 2407. | 4720. | 0. | ** | 350. | -128. | .51 | 6. | F | 8.9 | 27.8 | * |
| * | 7 | 2 | 940. | 0. | 0. | 1679. | 0. | 0. | 1810. | 4000. | 0. | ** | 940. | -128. | .45 | 5. | F | 8.3 | 28.9 | * |
| * | 8 | 3 | 700. | 1345. | 0. | 3024. | 1345. | 0. | 3155. | 4410. | 0. | ** | 700. | -128. | .72 | 11. | F | 13.6 | 22.0 | * |
| * | 9 | 3 | 700. | 0. | 0. | 3024. | 0. | 0. | 3155. | 4410. | 0. | ** | 700. | -128. | .72 | 11. | F | 13.6 | 22.0 | * |
| * | 10 | 3 | 700. | 0. | 270. | 3024. | 0. | 271. | 3155. | 4410. | 0. | ** | 700. | -128. | .72 | 11. | F | 13.6 | 22.0 | * |
| * | 11 | 2 | 2300. | 0. | 0. | 2754. | 0. | 0. | 2883. | 4000. | 0. | ** | 2300. | -128. | .72 | 11. | F | 13.7 | 21.9 | * |
| * | 12 | 3 | 700. | 740. | 615. | 3494. | 740. | 617. | 3623. | 5030. | 0. | ** | 700. | -128. | .72 | 11. | F | 13.7 | 21.9 | * |
| * | 13 | 3 | 800. | 0. | 0. | 2879. | 0. | 0. | 3006. | 4340. | 0. | ** | 800. | -128. | .69 | 10. | F | 13.2 | 22.6 | * |
| * | 14 | 3 | 1400. | 0. | 280. | 2879. | 0. | 280. | 3006. | 4340. | 0. | ** | 1400. | -128. | .69 | 10. | F | 13.2 | 22.6 | * |
| * | 15 | 2 | 1400. | 0. | 0. | 2599. | 0. | 0. | 2726. | 4000. | 0. | ** | 1400. | -128. | .68 | 10. | F | 13.0 | 22.9 | * |
| * | 16 | 2 | 1500. | 0. | 350. | 2599. | 0. | 348. | 2726. | 4000. | 0. | ** | 1500. | -128. | .68 | 10. | F | 13.0 | 22.9 | * |
| * | 17 | 2 | 1500. | 0. | 499. | 2249. | 0. | 494. | 2379. | 4000. | 0. | ** | 1500. | -128. | .59 | 8. | F | 10.3 | 25.7 | * |
| * | 18 | 2 | 5000. | 0. | 0. | 1750. | 0. | 0. | 1885. | 4000. | 0. | ** | 5000. | -128. | .47 | 5. | F | 8.5 | 28.6 | * |
| * | 19 | 2 | 5000. | 615. | 0. | 2365. | 615. | 0. | 2500. | 4000. | 0. | ** | 5000. | -128. | .63 | 8. | F | 11.0 | 24.8 | * |
| * | 20 | 3 | 750. | 0. | 2365. | 2365. | 0. | 2500. | 2500. | 2500. | 0. | 0. | 0. | 1.00 | 62. | 13.4 | E | 20.3 | 13.0 | * |
| ***** | | | | | | | | | | | | | | | | | | | | |
| * | TOTAL | | | 136889. | = | 25.9 | MI LES | MAX(V/C) = 1.00 | | | LOWEST LOS = F | AVG = 21. | 38.2 | 16.4 | 16.3 | * | | | | |
| ***** | | | | | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 2250. VEH-HRS | 2683. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 200. VEH-HRS | 200. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 2450. VEH-HRS | 2883. PASS-HRS |
| TOTAL TRAV DISTANCE = | 46962. VEH-MI. | 58112. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 19. MPH. | 25. MPH. |
| AVERAGE DENSITY = | 38. VPMP. | 31. VPMP. |
| TOTAL FUEL = | 2936. GALLONS | 8960. GALLONS |
| TOTAL EMISSIONS = | 794. KI LOGRAMS | 2408. KI LOGRAMS |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 2/29/2016 13:17 PAGE 12
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 3 OF 3

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|--------|------------|--------|------------|-------|
| 1 | 0.12 | 2 | 23.26 | 3 | 284.85 | 4 | 24.68 | 5 | 21.15 |
| 6 | 24.68 | 7 | 61.26 | 8 | 31.18 | 9 | 31.18 | 10 | 31.18 |
| 11 | 91.75 | 12 | 35.15 | 13 | 36.93 | 14 | 64.63 | 15 | 61.03 |
| 16 | 65.39 | 17 | 77.66 | 18 | 316.97 | 19 | 244.57 | 20 | 0.26 |

***** TOTAL DELAY = 1527.9 VEH-HRS ***** AVERAGE DELAY = 41.25 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-----------|-----------------------|---------------|--------------------------------|----------|---------|---------|----------|----------------------|
| ON-RAMP 2 | RAMP | 100. | 100.00 | 8.23 | 36.06 | 2.23 | 11.66 | 0.62 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 100.00 | 8.23 | 36.06 | 2.23 | 11.66 | 0.62 |
| ON-RAMP 4 | RAMP | 100. | 100.00 | 7.14 | 36.06 | 2.23 | 11.66 | 0.62 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 100.00 | 7.14 | 36.06 | 2.23 | 11.66 | 0.62 |

```

FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP LLL
FFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 1111111 222222222 PPP LLLLLLLLLL

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FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 13 AND 18 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 62
LOWER LIMB (AT V/C=1) = 30
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

FREWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC | SSEC | DESIGN | ORG | TRK | SSEC | PCT | PCT | DES | SPECIAL | FF.SPD. | CAP. | ART | GRADE | SUBSECTION | LOCATION |
|---------|------|-------|--------|-----|-----|------|-----|--------|------|---------|----------|----------|------|----------|-----------------------|----------|
| SEC | LNS | CAP | LENGTH | DES | FAC | GRAD | TRK | TRUCKS | RAMP | RAMP | ALT. RTE | ALT. RTE | TYPE | ALT. RTE | | |
| ** 1 | | | | | | | | | | | | | | | | ** |
| ** 2 | | | | | | | | | | | | | | | | ** |
| ** 3 | | | | | | | | | | | | | | | | ** |
| ** 4 | | | | | | | | | | | | | | | | ** |
| ** 5 | | | | | | | | | | | | | | | | ** |
| ** 6 | | | | | | | | | | | | | | | | ** |
| ** 7 | | | | | | | | | | | | | | | | ** |
| ** 8 | | | | | | | | | | | | | | | | ** |
| ** 9 | | | | | | | | | | | | | | | | ** |
| ** 10 | | | | | | | | | | | | | | | | ** |
| ** 11 | | | | | | | | | | | | | | | | ** |
| ** 12 | | | | | | | | | | | | | | | | ** |
| ** 13 | 1 | 1650. | 800. | 62 | 0 | 0.95 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda / Persian | HOV |
| ** 14 | 1 | 1650. | 1400. | 62 | D | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Persian On-Ramp w/HOV | |
| ** 15 | 1 | 1650. | 1400. | 62 | | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | West of Lawrence E | |
| ** 16 | 1 | 1650. | 1500. | 62 | D | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence Off-ramp | |
| ** 17 | 1 | 1650. | 1500. | 62 | D | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | End of DKS | |
| ** 18 | 1 | 1650. | 5000. | 62 | D | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | |
| ** 19 | | | | | | | | | | | | | | | | ** |

** 20 **

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 13:17 PAGE 3
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 1 OF 3

 ** FREeway TRAVEL TIME (MINUTES) **

| * ORIGINS DOWN | * DESTINATIONS ACROSS * | | | | | | | |
|----------------|-------------------------|------|------|------|------|------|------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.13 | 0.00 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 13:17 PAGE 4
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 1 OF 3

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | |
|-----------|--------|------------|-----------|------------|----------------|--------|---------|-----------------|----------------|-----------|---------|-----------|---------|--------|-------------|---|------|------|
| * SEC | * LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | | |
| * 1 | | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | | |
| * 3 | | | | | | | | | | | | | | | | | | |
| * 4 | | | | | | | | | | | | | | | | | | |
| * 5 | | | | | | | | | | | | | | | | | | |
| * 6 | | | | | | | | | | | | | | | | | | |
| * 7 | | | | | | | | | | | | | | | | | | |
| * 8 | | | | | | | | | | | | | | | | | | |
| * 9 | | | | | | | | | | | | | | | | | | |
| * 10 | | | | | | | | | | | | | | | | | | |
| * 11 | | | | | | | | | | | | | | | | | | |
| * 12 | | | | | | | | | | | | | | | | | | |
| * 13 | 1 | 800. | 724. | 0. | 724. | 724. | 0. | 724. | 1650. | 0. | 0. | 0. | .44 | 62. | 11.7 | B | 21.6 | 12.8 |
| * 14 | 1 | 1400. | 0. | 0. | 724. | 0. | 0. | 724. | 1650. | 0. | 0. | 0. | .44 | 62. | 11.7 | B | 21.6 | 12.8 |
| * 15 | 1 | 1400. | 0. | 0. | 724. | 0. | 0. | 724. | 1650. | 0. | 0. | 0. | .44 | 62. | 11.7 | B | 21.6 | 12.8 |
| * 16 | 1 | 1500. | 0. | 0. | 724. | 0. | 0. | 724. | 1650. | 0. | 0. | 0. | .44 | 62. | 11.7 | B | 21.6 | 12.8 |
| * 17 | 1 | 1500. | 0. | 0. | 724. | 0. | 0. | 724. | 1650. | 0. | 0. | 0. | .44 | 62. | 11.7 | B | 21.6 | 12.8 |
| * 18 | 1 | 5000. | 0. | 724. | 724. | 0. | 724. | 724. | 1650. | 0. | 0. | 0. | .44 | 62. | 11.7 | B | 21.6 | 12.8 |
| * 19 | | | | | | | | | | | | | | | | | | |
| * 20 | | | | | | | | | | | | | | | | | | |
| * TOTAL | | 11600. | = | 2.2 MILES | | | | MAX(V/C) = 0.44 | LOWEST LOS = B | AVG = 62. | 11.7 | | | 21.6 | 12.8 | | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 26. VEH-HRS | 51. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 26. VEH-HRS | 51. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 1591. VEH-MI. | 3183. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 62. MPH. |
| AVERAGE DENSITY = | 12. VPMP | 12. VPMP |
| TOTAL FUEL = | 74. GALLONS | 74. GALLONS |
| TOTAL EMISSIONS = | 20. KILOGRAMS | 20. KILOGRAMS |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 13:17 PAGE 5
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 Page 2

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.08 | 14 | 0.14 | 15 | 0.14 |
| 16 | 0.15 | 17 | 0.15 | 18 | 0.51 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 1.2 VEH-HRS ***** AVERAGE DELAY = 0.10 MIN/VEH *****

 ** FREeway TRAVEL TIME (MINUTES) **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|-------|-----------------------|------|------|------|------|------|------|------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| + | * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.13 | 0.00 |
| + | * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISS | | | | |
|-----------|--------|------------|-----------|---------------------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|---------|------|---|------|------|
| * SEC | * LNS | * LENGTH | * ORG DES | * SSEC ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMPL | * LEVEL | * MPG | * GS/VM | | | | |
| * 1 | | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | | |
| * 3 | | | | | | | | | | | | | | | | | | |
| * 4 | | | | | | | | | | | | | | | | | | |
| * 5 | | | | | | | | | | | | | | | | | | |
| * 6 | | | | | | | | | | | | | | | | | | |
| * 7 | | | | | | | | | | | | | | | | | | |
| * 8 | | | | | | | | | | | | | | | | | | |
| * 9 | | | | | | | | | | | | | | | | | | |
| * 10 | | | | | | | | | | | | | | | | | | |
| * 11 | | | | | | | | | | | | | | | | | | |
| * 12 | | | | | | | | | | | | | | | | | | |
| * 13 | 1 | 800. | 809. | 0. | 809. | 809. | 0. | 809. | 1650. | 0. | 0. | 0. | .49 | 62. | 13.1 | B | 21.6 | 12.8 |
| * 14 | 1 | 1400. | 0. | 0. | 809. | 0. | 0. | 809. | 1650. | 0. | 0. | 0. | .49 | 62. | 13.1 | B | 21.6 | 12.8 |
| * 15 | 1 | 1400. | 0. | 0. | 809. | 0. | 0. | 809. | 1650. | 0. | 0. | 0. | .49 | 62. | 13.1 | B | 21.6 | 12.8 |
| * 16 | 1 | 1500. | 0. | 0. | 809. | 0. | 0. | 809. | 1650. | 0. | 0. | 0. | .49 | 62. | 13.1 | B | 21.6 | 12.8 |
| * 17 | 1 | 1500. | 0. | 0. | 809. | 0. | 0. | 809. | 1650. | 0. | 0. | 0. | .49 | 62. | 13.1 | B | 21.6 | 12.8 |
| * 18 | 1 | 5000. | 0. | 809. | 809. | 0. | 809. | 809. | 1650. | 0. | 0. | 0. | .49 | 62. | 13.1 | B | 21.6 | 12.8 |
| * 19 | | | | | | | | | | | | | | | | | | |
| * 20 | | | | | | | | | | | | | | | | | | |
| * TOTAL | | 11600. | = | 2.2 | MILES | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 29. VEH-HRS | 57. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 29. VEH-HRS | 57. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 1778. VEH-MI. | 3555. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 62. MPH. |

AVERAGE DENSITY = 13. VP MPL
 TOTAL FUEL = 82. GALLONS
 TOTAL EMISSIONS = 23. KI LOGRAMS

SR-237_EB_PM_NP_2018_PL.txt
 12. VP MPL
 156. GALLONS
 43. KI LOGRAMS

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.09 | 14 | 0.16 | 15 | 0.16 |
| 16 | 0.17 | 17 | 0.17 | 18 | 0.57 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 1.3 VEH-HRS ***** AVERAGE DELAY = 0.10 MIN/VEH *****

 ** FREeway TRAVEL TIME (MINUTES) **

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | | |
|--------------|---------------------|------|------|------|------|------|------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| 1 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 4 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 5 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.13 | 0.00 |
| 6 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 7 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS | | | | | |
|---------|------|----------|---------|------------------|-------|-------|---------|---------|-------|-------|---------|------|-------|--------|--------|-------|------|-------|--|
| SEC | LNS | LENGTH | ORG | DES | SSEC | ORG | DES | SSEC | CAP. | EFF | LENGTH | RATE | RATIO | MPH | VP MPL | LEVEL | MPG | GS/VM | |
| 1 | | | | | | | | | | | | | | | | | | | |
| 2 | | | | | | | | | | | | | | | | | | | |
| 3 | | | | | | | | | | | | | | | | | | | |
| 4 | | | | | | | | | | | | | | | | | | | |
| 5 | | | | | | | | | | | | | | | | | | | |
| 6 | | | | | | | | | | | | | | | | | | | |
| 7 | | | | | | | | | | | | | | | | | | | |
| 8 | | | | | | | | | | | | | | | | | | | |
| 9 | | | | | | | | | | | | | | | | | | | |
| 10 | | | | | | | | | | | | | | | | | | | |
| 11 | | | | | | | | | | | | | | | | | | | |
| 12 | | | | | | | | | | | | | | | | | | | |
| 13 | 1 | 800. | 615. | 0. | 615. | 615. | 0. | 615. | 1650. | 0. | 0. | 0. | .37 | 62. | 9.9 | A | 21.6 | 12.8 | |
| 14 | 1 | 1400. | 0. | 0. | 615. | 0. | 0. | 615. | 1650. | 0. | 0. | 0. | .37 | 62. | 9.9 | A | 21.6 | 12.8 | |
| 15 | 1 | 1400. | 0. | 0. | 615. | 0. | 0. | 615. | 1650. | 0. | 0. | 0. | .37 | 62. | 9.9 | A | 21.6 | 12.8 | |
| 16 | 1 | 1500. | 0. | 0. | 615. | 0. | 0. | 615. | 1650. | 0. | 0. | 0. | .37 | 62. | 9.9 | A | 21.6 | 12.8 | |
| 17 | 1 | 1500. | 0. | 0. | 615. | 0. | 0. | 615. | 1650. | 0. | 0. | 0. | .37 | 62. | 9.9 | A | 21.6 | 12.8 | |
| 18 | 1 | 5000. | 0. | 615. | 615. | 0. | 615. | 615. | 1650. | 0. | 0. | 0. | .37 | 62. | 9.9 | A | 21.6 | 12.8 | |
| 19 | | | | | | | | | | | | | | | | | | | |
| 20 | | | | | | | | | | | | | | | | | | | |
| TOTAL | | 11600. | = | 2.2 | MILES | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | |

SR-237_EB_PM_NP_2018_PL.txt

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | | | |
|-----------------------------|--------------------|----------------|-------------------|----------------|--|--|
| FREEWAY TRAVEL TIME = | 22. VEH-HRS | 44. PASS-HRS | 76. VEH-HRS | 152. PASS-HRS | | |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | | |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | | |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | | |
| TOTAL SYSTEM TRAVEL TIME = | 22. VEH-HRS | 44. PASS-HRS | 76. VEH-HRS | 152. PASS-HRS | | |
| TOTAL FRWAY TRAV DISTANCE = | 1351. VEH-MI. | 2702. PASS-MI. | 4720. VEH-MI. | 9440. PASS-MI. | | |
| AVERAGE SYSTEM SPEED = | 62. MPH. | | 62. MPH. | | | |
| AVERAGE DENSITY = | 10. VPML | | 12. VPML | | | |
| TOTAL FUEL = | 63. GALLONS | | 219. GALLONS | | | |
| TOTAL EMISSIONS = | 17. KILOGRAMS | | 60. KILOGRAMS | | | |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 13:17 PAGE 11
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 3 OF 3

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.07 | 14 | 0.12 | 15 | 0.12 |
| 16 | 0.13 | 17 | 0.13 | 18 | 0.43 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 1.0 VEH-HRS ***** AVERAGE DELAY = 0.10 MIN/VEH *****


```

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE O*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP EEE
FFFFFFFF RRRRRRRR EEEEE QQQ QQQ 1111 222 PPPPPPPP EEEEE
FFFFFFFF RRRRRRRR EEEEE QQQ QQQ 1111 222 PPPPPPPP EEEEE
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP EEE
FFF RRR RRR EEE O*UC* QQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE O*REGENTS*Q 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QO 1111111 2222222222 PPP EEEEEEEEE
    
```

FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 62
LOWER LIMB (AT V/C=1) = 30
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREEWAY AND ARTERIAL DESIGN FEATURES

| ** SUB NO. | ** SEC | ** LNS | ** SSEC CAP | ** SSEC LENGTH | ** DESIGN SPEED | ** ORG DES | ** TRK FAC | ** SSEC GRAD | ** PCT TRK | ** PCT DES TRUCKS | ** SPECIAL RAMP | ** FF. SPD. ALT. RTE | ** CAP. ALT. RTE | ** ART TYPE | ** GRADE ALT. RTE | ** SUBSECTION | ** LOCATION |
|------------|--------|----------|-------------|----------------|-----------------|------------|------------|--------------|------------|-------------------|-----------------|----------------------|------------------|-------------|---------------------------|---------------|-------------|
| ** 1 | ** 3 | ** 6000. | ** 500. | ** 62 | ** 0 | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Seeding | ** | ** |
| ** 2 | ** 3 | ** 6000. | ** 99999. | ** 62 | ** 0 | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Queue Capture | ** | ** |
| ** 3 | ** 2 | ** 4000. | ** 12000. | ** 62 | ** 0 | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** HOV Dummy | ** | ** |
| ** 4 | ** 3 | ** 4720. | ** 350. | ** 62 | ** 0 | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Maude On-ramp | ** | ** |
| ** 5 | ** 3 | ** 4720. | ** 300. | ** 62 | ** 0 | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Maude to US-101 | ** | ** |
| ** 6 | ** 3 | ** 4720. | ** 350. | ** 62 | ** D | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** US-101 Off-Ramp | ** | ** |
| ** 7 | ** 2 | ** 4000. | ** 940. | ** 62 | ** 0 | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** US101SB / US101SB | ** | ** |
| ** 8 | ** 3 | ** 4410. | ** 700. | ** 62 | ** 0 | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** US101 SB On-ramp | ** | ** |
| ** 9 | ** 3 | ** 4410. | ** 700. | ** 62 | ** 0 | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** US 101 / Mathilda | ** | ** |
| ** 10 | ** 3 | ** 4410. | ** 700. | ** 62 | ** D | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Mathilda Off-ramp | ** | ** |
| ** 11 | ** 2 | ** 4000. | ** 2300. | ** 62 | ** 0 | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Mathilda / Mathilda | ** | ** |
| ** 12 | ** 3 | ** 5030. | ** 700. | ** 62 | ** OD | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Mathilda On-Ramp | ** | ** |
| ** 13 | ** 3 | ** 4340. | ** 800. | ** 62 | ** 0 | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Mathilda / Persian HOV | ** | ** |
| ** 14 | ** 3 | ** 4340. | ** 1400. | ** 62 | ** D | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Persian On-Ramp w/HOV | ** | ** |
| ** 15 | ** 2 | ** 4000. | ** 1400. | ** 62 | ** 0 | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** West of Lawrence E | ** | ** |
| ** 16 | ** 2 | ** 4000. | ** 1500. | ** 62 | ** D | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Lawrence Off-ramp | ** | ** |
| ** 17 | ** 2 | ** 4000. | ** 1500. | ** 62 | ** D | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** End of DKS | ** | ** |
| ** 18 | ** 2 | ** 4000. | ** 5000. | ** 62 | ** 0 | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** HOV Dummy | ** | ** |
| ** 19 | ** 2 | ** 4000. | ** 5000. | ** 62 | ** 0 | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Buffer | ** | ** |
| ** 20 | ** 3 | ** 2500. | ** 750. | ** 62 | ** OD | ** 0.95 | ** 0.0 | ** 5 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** End of the network | ** | ** |

***** INPUT HAS BEEN COMPLETED *****

MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 6 IN TIME SLICE 1
--- THE MAXIMUM METERING RATE WILL PREVAIL.

MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 4 IN TIME SLICE 2
--- THE MAXIMUM METERING RATE WILL PREVAIL.

**
** FREeway TRAVEL TIME (MINUTES) **
**

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | |
|-----------|--|-----------------------|-------|-------|-------|-------|-------|-------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | | 20.80 | 21.36 | 22.38 | 23.97 | 27.53 | 31.03 | 69.66 |
| * 2 * | | 0.18 | 0.74 | 1.76 | 3.35 | 6.91 | 10.42 | 49.04 |
| * 3 * | | 0.00 | 0.38 | 1.40 | 2.99 | 6.55 | 10.06 | 48.69 |
| * 4 * | | 0.00 | 0.00 | 0.30 | 1.90 | 5.46 | 8.96 | 47.59 |
| * 5 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 17.91 |
| * 6 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.14 |

*
* TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISS | | | | |
|--|--------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|-------|----------|-----------|---------|--------|---------|---------|-------|---------|------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | |
| * 1 | 3 | 500. | 1940. | 0. | 1940. | 1940. | 0. | 1940. | 6000. | 0. | 0. | 0. | .32 | 62. | 10.4 | A | 20.3 | 13.0 | |
| * 2 | 3 | 99999. | 0. | 0. | 1940. | 0. | 0. | 1940. | 6000. | 0. | 0. | 0. | .32 | 62. | 10.4 | A | 20.3 | 13.0 | |
| * 3 | 2 | 12000. | 0. | 0. | 1940. | 0. | 0. | 1940. | 4000. | 0. | 0. | 0. | .49 | 62. | 15.6 | B | 20.3 | 13.0 | |
| * 4 | 3 | 350. | 650. | 0. | 2590. | 550. | 0. | 2490. | 4720. | 0. | 0. | 0. | .53 | 62. | 13.4 | B | 20.3 | 13.0 | |
| * 5 | 3 | 300. | 0. | 0. | 2590. | 0. | 0. | 2490. | 4720. | 0. | 0. | 0. | .53 | 62. | 13.4 | B | 20.3 | 13.0 | |
| * 6 | 3 | 350. | 0. | 600. | 2590. | 0. | 577. | 2490. | 4720. | 0. | 0. | 0. | .53 | 62. | 13.4 | B | 20.3 | 13.0 | |
| * 7 | 2 | 940. | 0. | 0. | 1990. | 0. | 0. | 1913. | 4000. | 0. | 0. | 0. | .48 | 62. | 15.4 | B | 20.3 | 13.0 | |
| * 8 | 3 | 700. | 810. | 0. | 2800. | 810. | 0. | 2723. | 4410. | 0. | 0. | 0. | .62 | 62. | 14.6 | B | 20.3 | 13.0 | |
| * 9 | 3 | 700. | 0. | 0. | 2800. | 0. | 0. | 2723. | 4410. | 0. | 0. | 0. | .62 | 62. | 14.6 | B | 20.3 | 13.0 | |
| * 10 | 3 | 700. | 0. | 220. | 2800. | 0. | 214. | 2723. | 4410. | 0. | 0. | 0. | .62 | 62. | 14.6 | B | 20.3 | 13.0 | |
| * 11 | 2 | 2300. | 0. | 0. | 2580. | 0. | 0. | 805. | 4000. | 0. | ** | 2300. | 1705. | .20 | 37. | 11.0 | F | 19.8 | 13.4 |
| * 12 | 3 | 700. | 910. | 757. | 3490. | 810. | 720. | 1615. | 5030. | 0. | ** | 700. | 1705. | .32 | 26. | 20.5 | F | 18.5 | 14.1 |
| * 13 | 3 | 800. | 0. | 0. | 2733. | 0. | 0. | 895. | 4340. | 0. | ** | 800. | 1705. | .21 | 18. | 16.1 | F | 18.5 | 14.1 |
| * 14 | 3 | 1400. | 0. | 220. | 2733. | 0. | 209. | 895. | 4340. | 0. | ** | 1400. | 1705. | .21 | 14. | 20.6 | F | 17.9 | 14.5 |
| * 15 | 2 | 1400. | 0. | 0. | 2513. | 0. | 0. | 685. | 4000. | 0. | ** | 1400. | 1705. | .17 | 11. | 32.4 | F | 17.5 | 14.8 |
| * 16 | 2 | 1500. | 0. | 360. | 2513. | 0. | 342. | 685. | 4000. | 0. | ** | 1500. | 1705. | .17 | 8. | 41.3 | F | 16.8 | 15.4 |
| * 17 | 2 | 1500. | 0. | 0. | 2153. | 0. | 0. | 343. | 4000. | 0. | ** | 1500. | 1705. | .09 | 5. | 35.3 | F | 17.3 | 15.0 |
| * 18 | 2 | 5000. | 0. | 0. | 2153. | 0. | 0. | 343. | 4000. | 0. | ** | 5000. | 1705. | .09 | 3. | 62.5 | F | 15.3 | 16.6 |
| * 19 | 2 | 5000. | 757. | 0. | 2910. | 757. | 0. | 1100. | 4000. | 0. | ** | 5000. | 1705. | .28 | 3. | 172.0 | F | 9.7 | 25.0 |
| * 20 | 3 | 750. | 1400. | 4310. | 4310. | 1400. | 2500. | 2500. | 2500. | 0. | 0. | 0. | 1.00 | 62. | 13.4 | E | 20.3 | 13.0 | |
| ***** | | | | | | | | | | | | | | | | | | | |
| * TOTAL 136889. = 25.9 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 29. 19.9 19.5 13.5 * | | | | | | | | | | | | | | | | | | | |
| ***** | | | | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | |
|----------------------------|--------------------|---------|-------|----------|-------------------|---------|-------|----------|
| FREeway TRAVEL TIME = | 1702. | VEH-HRS | 2022. | PASS-HRS | 1702. | VEH-HRS | 2022. | PASS-HRS |
| FREeway MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 100. | VEH-HRS | 100. | PASS-HRS | 100. | VEH-HRS | 100. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1802. | VEH-HRS | 2122. | PASS-HRS | 1802. | VEH-HRS | 2122. | PASS-HRS |

| | | | | | | | | | | | | | | | | | | | | |
|-----|---|-------|------|-------|-------|------|-------|-------|-------|----|----|-------|------|------|-----|-------|---|------|------|---|
| *14 | 3 | 1400. | 0. | 341. | 3681. | 0. | 334. | 3423. | 4340. | 0. | ** | 1400. | 196. | .79 | 14. | 81.5 | F | 15.3 | 19.7 | * |
| *15 | 2 | 1400. | 0. | 0. | 3340. | 0. | 0. | 3089. | 4000. | 0. | ** | 1400. | 196. | .77 | 13. | 116.3 | F | 14.9 | 20.3 | * |
| *16 | 2 | 1500. | 0. | 341. | 3340. | 0. | 340. | 3089. | 4000. | 0. | ** | 1500. | 196. | .77 | 13. | 116.3 | F | 14.9 | 20.3 | * |
| *17 | 2 | 1500. | 0. | 1000. | 2999. | 0. | 952. | 2750. | 4000. | 0. | ** | 1500. | 196. | .69 | 10. | 134.8 | F | 13.1 | 22.8 | * |
| *18 | 2 | 5000. | 0. | 0. | 1999. | 0. | 0. | 1798. | 4000. | 0. | ** | 5000. | 196. | .45 | 5. | 186.6 | F | 8.3 | 28.9 | * |
| *19 | 2 | 5000. | 702. | 0. | 2701. | 702. | 0. | 2500. | 4000. | 0. | ** | 5000. | 196. | .63 | 8. | 148.4 | F | 11.0 | 24.8 | * |
| *20 | 3 | 750. | 0. | 2701. | 2701. | 0. | 2500. | 2500. | 2500. | 0. | 0. | 0. | 0. | 1.00 | 62. | 13.4 | E | 20.3 | 13.0 | * |

 * TOTAL 136889. = 25.9 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 31. 32.1 18.2 14.8 *

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------------------|----------------------------------|
| FREEWAY TRAVEL TIME = | 1988. VEH-HRS 2368. PASS-HRS | 3690. VEH-HRS 4391. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 232. VEH-HRS 232. PASS-HRS | 332. VEH-HRS 332. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 2220. VEH-HRS 2600. PASS-HRS | 4022. VEH-HRS 4723. PASS-HRS |
| TOTAL TRAV DISTANCE = | 60647. VEH-MI. 75404. PASS-MI. | 110113. VEH-MI. 137165. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 27. MPH. | 30. MPH. |
| AVERAGE DENSITY = | 32. VPMP/L | 26. VPMP/L |
| TOTAL FUEL = | 3417. GALLONS | 5986. GALLONS |
| TOTAL EMISSIONS = | 932. KI LOGRAMS | 1615. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|--------|------------|--------|------------|-------|
| 1 | 0.16 | 2 | 31.74 | 3 | 4.28 | 4 | 2.63 | 5 | 3.94 |
| 6 | 6.57 | 7 | 26.65 | 8 | 17.31 | 9 | 20.30 | 10 | 23.30 |
| 11 | 73.37 | 12 | 26.92 | 13 | 29.07 | 14 | 50.87 | 15 | 49.05 |
| 16 | 52.55 | 17 | 64.55 | 18 | 327.22 | 19 | 244.57 | 20 | 0.26 |

***** TOTAL DELAY = 1055.3 VEH-HRS ***** AVERAGE DELAY = 26.35 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MI MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-----------|-----------------------|---------------|-----------------------------------|----------|---------|---------|----------|----------------------|
| ON-RAMP 2 | RAMP 100. | 100.00 | 6.38 | 36.06 | 2.23 | 11.66 | 0.62 | 14.51 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 100. | 100.00 | 6.38 | 36.06 | 2.23 | 11.66 | 0.62 | 14.51 |
| ON-RAMP 4 | RAMP 164. | 132.00 | 7.44 | 47.60 | 2.94 | 15.39 | 0.82 | 19.15 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 164. | 132.00 | 7.44 | 47.60 | 2.94 | 15.39 | 0.82 | 19.15 |

 ** FREEWAY TRAVEL TIME (MINUTES) **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN *
 * 1 2 3 4 5 6 7 *

| | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|
| * 1 * | 21.01 | 22.83 | 24.77 | 26.46 | 28.78 | 30.37 | 47.57 |
| * 2 * | 0.38 | 2.20 | 4.14 | 5.83 | 8.16 | 9.74 | 26.94 |
| * 3 * | 0.00 | 1.12 | 3.07 | 4.75 | 7.08 | 8.66 | 25.86 |
| * 4 * | 0.00 | 0.00 | 0.48 | 2.17 | 4.50 | 6.08 | 23.28 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 6.88 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.14 |

TIME SLICE FREEWAY PERFORMANCE TABLE

Table with columns: SUB NO., SEC LNS, SSEC LENGTH, O-D DATA ORG, DEMANDS DES, SSEC, ADJUSTED VOLUMES ORG, SSEC CAP, WEAVE EFF, CONGEST LENGTH, STORAGE RATE, V/C RATIO, SPEED MPH, DENSITY VPMP, LOS LEVEL, FUEL MPG, EMISSIONS GS/VM. Includes a summary row: TOTAL 136889 = 25.9 MILES, MAX(V/C) = 1.00, LOWEST LOS = F, AVG = 28, 27.6, 17.8, 15.1.

Summary statistics table with columns: FREeway TRAVEL TIME, MERGE DELAY, MRG/CAP DELAY, OFF-RAMP DELAY, SYSTEM TRAVEL TIME, TRAV DISTANCE, AVERAGE SYSTEM SPEED, AVERAGE DENSITY, TOTAL FUEL, TOTAL EMISSIONS. Values are provided in VEH-HRS, PASS-HRS, VEH-MI., MPH, VPMP, GALLONS, and KILOGRAMS.

1 INSTITUTE OF TRANSPORTATION STUDIES UNIVERSITY OF CALIFORNIA, BERKELEY FREQ12PE REL 3.01 2/29/2016 15:51 PAGE 12 SIMULATION AFTER CONTROL, NO DIVERSION TIME SLICE 3 OF 3

Table showing MAINLINE DELAY (VEH-HRS) and DESIRED SPEED = 65.0. Columns include SUBSECTION, DELAY, and SUBSECTION DELAY. Values range from 0.12 to 49.69 VEH-HRS.

Table showing RAMP DELAYS with columns: RAMP, QUEUE LENGTH VEHICLES, DELAY VEH-HRS, AVERAGE METERING DELAY MI MINUTES, GAS GALS, HC KGMS, CO KGMS, NOX KGMS, TOTAL EMISSIONS KGMS. Includes data for ON-RAMP 2 and ON-RAMP 4.

```

FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP LLL
FFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 1111111 222222222 PPP LLLLLLLLLL
    
```

FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 13 AND 18 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 62
LOWER LIMB (AT V/C=1) = 30
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

FREEWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC | SSEC | DESIGN | ORG | TRK | SSEC | PCT | PCT | DES | SPECIAL | FF.SPD. | CAP. | ART | GRADE | SUBSECTION | LOCATION |
|---------|------|-------|--------|-----|-----|------|-----|--------|------|---------|----------|----------|------|----------|-----------------------|----------|
| SEC | LNS | CAP | LENGTH | DES | FAC | GRAD | TRK | TRUCKS | RAMP | RAMP | ALT. RTE | ALT. RTE | TYPE | ALT. RTE | | |
| ** 1 | | | | | | | | | | | | | | | | ** |
| ** 2 | | | | | | | | | | | | | | | | ** |
| ** 3 | | | | | | | | | | | | | | | | ** |
| ** 4 | | | | | | | | | | | | | | | | ** |
| ** 5 | | | | | | | | | | | | | | | | ** |
| ** 6 | | | | | | | | | | | | | | | | ** |
| ** 7 | | | | | | | | | | | | | | | | ** |
| ** 8 | | | | | | | | | | | | | | | | ** |
| ** 9 | | | | | | | | | | | | | | | | ** |
| ** 10 | | | | | | | | | | | | | | | | ** |
| ** 11 | | | | | | | | | | | | | | | | ** |
| ** 12 | | | | | | | | | | | | | | | | ** |
| ** 13 | 1 | 1650. | 800. | 62 | 0 | 0.95 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda / Persian | HOV |
| ** 14 | 1 | 1650. | 1400. | 62 | D | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Persian On-Ramp w/HOV | |
| ** 15 | 1 | 1650. | 1400. | 62 | | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | West of Lawrence E | |
| ** 16 | 1 | 1650. | 1500. | 62 | D | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence Off-ramp | |
| ** 17 | 1 | 1650. | 1500. | 62 | D | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | End of DKS | |
| ** 18 | 1 | 1650. | 5000. | 62 | D | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | |
| ** 19 | | | | | | | | | | | | | | | | ** |

** 20 **

FREEMWAY TRAVEL TIME (MINUTES)

Table with columns: ORIGINS DOWN, DESTINATIONS ACROSS (1-8). Rows 1-7 showing travel times.

TIME SLICE FREEMWAY PERFORMANCE TABLE

Table with columns: SUB NO., SSEC, O-D DATA DEMANDS, ADJUSTED VOLUMES, SSEC, WEAVE, CONGEST, STORAGE, V/C, SPEED DENSITY, LOS, FUEL, EMISSIONS.

Summary table with columns: FREEMWAY TRAVEL TIME, FREEMWAY MERGE DELAY, ON-RAMP MRG/CAP DELAY, OFF-RAMP DELAY, TOTAL SYSTEM TRAVEL TIME, TOTAL FRWAY TRAV DISTANCE, AVERAGE SYSTEM SPEED, AVERAGE DENSITY, TOTAL FUEL, TOTAL EMISSIONS.

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.09 | 14 | 0.15 | 15 | 0.15 |
| 16 | 0.16 | 17 | 0.16 | 18 | 0.53 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 1.2 VEH-HRS ***** AVERAGE DELAY = 0.10 MIN/VEH *****

 **
 ** FREeway TRAVEL TIME (MINUTES) **
 **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|-------|-----------------------|------|------|------|------|------|------|------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| + | * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.13 | 0.00 |
| + | * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISS | | | | |
|-----------|--------|------------|-----------|---------------------|--------|---------|-----------|-----------|---------|-----------------|----------------|---------|-----------|---------|------|---|------|------|
| * SEC | * LNS | * LENGTH | * ORG DES | * SSEC ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMPL | * LEVEL | * MPG | * GS/VM | | | | |
| * 1 | | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | | |
| * 3 | | | | | | | | | | | | | | | | | | |
| * 4 | | | | | | | | | | | | | | | | | | |
| * 5 | | | | | | | | | | | | | | | | | | |
| * 6 | | | | | | | | | | | | | | | | | | |
| * 7 | | | | | | | | | | | | | | | | | | |
| * 8 | | | | | | | | | | | | | | | | | | |
| * 9 | | | | | | | | | | | | | | | | | | |
| * 10 | | | | | | | | | | | | | | | | | | |
| * 11 | | | | | | | | | | | | | | | | | | |
| * 12 | | | | | | | | | | | | | | | | | | |
| * 13 | 1 | 800. | 702. | 0. | 702. | 702. | 0. | 702. | 1650. | 0. | 0. | 0. | .43 | 62. | 11.3 | B | 21.6 | 12.8 |
| * 14 | 1 | 1400. | 0. | 0. | 702. | 0. | 0. | 702. | 1650. | 0. | 0. | 0. | .43 | 62. | 11.3 | B | 21.6 | 12.8 |
| * 15 | 1 | 1400. | 0. | 0. | 702. | 0. | 0. | 702. | 1650. | 0. | 0. | 0. | .43 | 62. | 11.3 | B | 21.6 | 12.8 |
| * 16 | 1 | 1500. | 0. | 0. | 702. | 0. | 0. | 702. | 1650. | 0. | 0. | 0. | .43 | 62. | 11.3 | B | 21.6 | 12.8 |
| * 17 | 1 | 1500. | 0. | 0. | 702. | 0. | 0. | 702. | 1650. | 0. | 0. | 0. | .43 | 62. | 11.3 | B | 21.6 | 12.8 |
| * 18 | 1 | 5000. | 0. | 702. | 702. | 0. | 702. | 702. | 1650. | 0. | 0. | 0. | .43 | 62. | 11.3 | B | 21.6 | 12.8 |
| * 19 | | | | | | | | | | | | | | | | | | |
| * 20 | | | | | | | | | | | | | | | | | | |
| * TOTAL | | 11600. | = | 2.2 | MILES | | | | | | | | | | | | | |
| | | | | | | | | | | MAX(V/C) = 0.43 | LOWEST LOS = B | | AVG = 62. | | 11.3 | | 21.6 | 12.8 |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 25. VEH-HRS | 50. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 25. VEH-HRS | 50. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 1542. VEH-MI. | 3085. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 62. MPH. |

AVERAGE DENSITY = 11. VP MPL
TOTAL FUEL = 72. GALLONS
TOTAL EMISSIONS = 20. KI LOGRAMS

Table with columns: SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY. Includes summary rows for TOTAL DELAY and AVERAGE DELAY.

FREeway TRAVEL TIME (MINUTES)

Table with columns: ORIGINS DOWN, DESTINATIONS ACROSS (1-8). Shows travel times between various origins and destinations.

TIME SLICE FREEWAY PERFORMANCE TABLE

Table with columns: SUB NO., SSEC, O-D DATA, DEMANDS, ADJUSTED VOLUMES, SSEC, WEAVE, CONGEST, STORAGE, V/C, SPEED, DENSITY, LOS, FUEL, EMISSIONS. Includes a summary row for TOTAL performance metrics.

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| | CURRENT TIME SLICE | | CUMULATIVE VALUES | | | |
|-----------------------------|--------------------|----------------|-------------------|----------------|--|--|
| FREEWAY TRAVEL TIME = | 19. VEH-HRS | 38. PASS-HRS | 71. VEH-HRS | 142. PASS-HRS | | |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | | |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | | |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | | |
| TOTAL SYSTEM TRAVEL TIME = | 19. VEH-HRS | 38. PASS-HRS | 71. VEH-HRS | 142. PASS-HRS | | |
| TOTAL FRWAY TRAV DISTANCE = | 1188. VEH-MI. | 2375. PASS-MI. | 4392. VEH-MI. | 8784. PASS-MI. | | |
| AVERAGE SYSTEM SPEED = | 62. MPH. | | 62. MPH. | | | |
| AVERAGE DENSITY = | 9. VPML | | 11. VPML | | | |
| TOTAL FUEL = | 55. GALLONS | | 204. GALLONS | | | |
| TOTAL EMISSIONS = | 15. KILOGRAMS | | 56. KILOGRAMS | | | |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 3 OF 3

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.06 | 14 | 0.11 | 15 | 0.11 |
| 16 | 0.11 | 17 | 0.11 | 18 | 0.38 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 0.9 VEH-HRS ***** AVERAGE DELAY = 0.10 MIN/VEH *****

```

FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQO 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFFF RRRRRRRR EEEEEEEEE Q*A.D.MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQO QQQO 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQ QQQO 1111 222 PPP PPP EEE
FFFFFFFFF RRRRRRRR EEEEEEE QQQ QQQO 1111 222 PPPPPPPP EEEEEEE
FFFFFFFFF RRRRRRRR EEEEEEE QQQO QQQO 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQO QO QQQO 1111 2222 PPP EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QO 1111111 222222222 PPP EEEEEEEEE

```

FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 62
LOWER LIMB (AT V/C=1) = 30
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

```

*****
**                                     FREEWAY AND ARTERIAL DESIGN FEATURES                                     **
*****
** SUB NO.  SSEC  SSEC  DESIGN  ORG  TRK  SSEC  PCT  PCT  DES  SPECIAL  FF. SPD.  CAP.  ART  GRADE  SUBSECTION  LOCATION
** SEC  LNS   CAP   LENGTH  SPEED  DES  FAC  GRAD  TRK  TRUCKS  RAMP    ALT. RTE  ALT. RTE  TYPE  ALT. RTE  SECTION  LOC
**          *      *      *      *      *      *      *      *      *      *      *      *      *      *      *      *
** 1  3  6000.  500.  62   0  0.95  0.0  5   0   NO    0.0    0.   GOOD  0.0  Seeding  **
** 2  3  6000. 99999. 62   0  0.95  0.0  5   0   NO    0.0    0.   GOOD  0.0  Queue Capture  **
** 3  2  4000. 12000. 62   0  0.95  0.0  5   0   NO    0.0    0.   GOOD  0.0  HOV Dummy  **
** 4  3  4720.  350.  62   0  0.95  0.0  5   0   YES   0.0    0.   GOOD  0.0  Maude On-ramp  **
** 5  3  4720.  300.  62   0  0.95  0.0  5   0   YES   0.0    0.   GOOD  0.0  Maude to US-101  **
** 6  3  4720.  350.  62   D  0.95  0.0  5   0   YES   0.0    0.   GOOD  0.0  US-101 Off-Ramp  **
** 7  2  4000.  940.  62   0  0.95  0.0  5   0   NO    0.0    0.   GOOD  0.0  US101SB / US101SB  **
** 8  3  4410.  700.  62   0  0.95  0.0  5   0   YES   0.0    0.   GOOD  0.0  US101 SB On-ramp  **
** 9  3  4410.  700.  62   0  0.95  0.0  5   0   YES   0.0    0.   GOOD  0.0  US 101 / Mathilda  **
** 10 3  4410.  700.  62   D  0.95  0.0  5   0   YES   0.0    0.   GOOD  0.0  Mathilda Off-ramp  **
** 11 2  4000. 2300.  62   0  0.95  0.0  5   0   NO    0.0    0.   GOOD  0.0  Mathilda / Mathilda  **
** 12 3  5030.  700.  62   OD 0.95  0.0  5   0   YES   0.0    0.   GOOD  0.0  Mathilda On-Ramp  **
** 13 3  4340.  800.  62   0  0.95  0.0  5   0   YES   0.0    0.   GOOD  0.0  Mathilda / Persian HOV  **
** 14 3  4340. 1400.  62   D  0.95  0.0  5   0   NO    0.0    0.   GOOD  0.0  Persian On-Ramp w/HOV  **
** 15 2  4000. 1400.  62   0  0.95  0.0  5   0   NO    0.0    0.   GOOD  0.0  West of Lawrence E  **
** 16 2  4000. 1500.  62   D  0.95  0.0  5   0   NO    0.0    0.   GOOD  0.0  Lawrence Off-ramp  **
** 17 2  4000. 1500.  62   D  0.95  0.0  5   0   NO    0.0    0.   GOOD  0.0  End of DKS  **
** 18 2  4000. 5000.  62   0  0.95  0.0  5   0   NO    0.0    0.   GOOD  0.0  HOV Dummy  **
** 19 2  4000. 5000.  62   0  0.95  0.0  5   0   NO    0.0    0.   GOOD  0.0  Buffer  **
** 20 3  2500.  750.  62   OD 0.95  0.0  5   0   YES   0.0    0.   GOOD  0.0  End of the network  **
*****

```

***** INPUT HAS BEEN COMPLETED *****

MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 6 IN TIME SLICE 1
--- THE MAXIMUM METERING RATE WILL PREVAIL.

MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 4 IN TIME SLICE 2
--- THE MAXIMUM METERING RATE WILL PREVAIL.

**
** FREeway TRAVEL TIME (MINUTES)
**

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | |
|-----------|--|-----------------------|-------|-------|-------|-------|-------|-------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | | 20.80 | 21.36 | 22.38 | 23.97 | 27.53 | 31.03 | 69.66 |
| * 2 * | | 0.18 | 0.74 | 1.76 | 3.35 | 6.91 | 10.42 | 49.04 |
| * 3 * | | 0.00 | 0.38 | 1.40 | 2.99 | 6.55 | 10.06 | 48.69 |
| * 4 * | | 0.00 | 0.00 | 0.30 | 1.90 | 5.46 | 8.96 | 47.59 |
| * 5 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 17.91 |
| * 6 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.14 |

*
* TIME SLICE FREEWAY PERFORMANCE TABLE
*

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISS | | | | |
|-----------|--------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|-------|----------|-----------|---------|--------|---------|---------|-------|---------|------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | |
| * 1 | 3 | 500. | 1940. | 0. | 1940. | 1940. | 0. | 1940. | 6000. | 0. | 0. | 0. | .32 | 62. | 10.4 | A | 20.3 | 13.0 | |
| * 2 | 3 | 99999. | 0. | 0. | 1940. | 0. | 0. | 1940. | 6000. | 0. | 0. | 0. | .32 | 62. | 10.4 | A | 20.3 | 13.0 | |
| * 3 | 2 | 12000. | 0. | 0. | 1940. | 0. | 0. | 1940. | 4000. | 0. | 0. | 0. | .49 | 62. | 15.6 | B | 20.3 | 13.0 | |
| * 4 | 3 | 350. | 650. | 0. | 2590. | 550. | 0. | 2490. | 4720. | 0. | 0. | 0. | .53 | 62. | 13.4 | B | 20.3 | 13.0 | |
| * 5 | 3 | 300. | 0. | 0. | 2590. | 0. | 0. | 2490. | 4720. | 0. | 0. | 0. | .53 | 62. | 13.4 | B | 20.3 | 13.0 | |
| * 6 | 3 | 350. | 0. | 600. | 2590. | 0. | 577. | 2490. | 4720. | 0. | 0. | 0. | .53 | 62. | 13.4 | B | 20.3 | 13.0 | |
| * 7 | 2 | 940. | 0. | 0. | 1990. | 0. | 0. | 1913. | 4000. | 0. | 0. | 0. | .48 | 62. | 15.4 | B | 20.3 | 13.0 | |
| * 8 | 3 | 700. | 810. | 0. | 2800. | 810. | 0. | 2723. | 4410. | 0. | 0. | 0. | .62 | 62. | 14.6 | B | 20.3 | 13.0 | |
| * 9 | 3 | 700. | 0. | 0. | 2800. | 0. | 0. | 2723. | 4410. | 0. | 0. | 0. | .62 | 62. | 14.6 | B | 20.3 | 13.0 | |
| * 10 | 3 | 700. | 0. | 220. | 2800. | 0. | 214. | 2723. | 4410. | 0. | 0. | 0. | .62 | 62. | 14.6 | B | 20.3 | 13.0 | |
| * 11 | 2 | 2300. | 0. | 0. | 2580. | 0. | 0. | 805. | 4000. | 0. | ** | 2300. | 1705. | .20 | 37. | 11.0 | F | 19.8 | 13.4 |
| * 12 | 3 | 700. | 910. | 757. | 3490. | 810. | 720. | 1615. | 5030. | 0. | ** | 700. | 1705. | .32 | 26. | 20.5 | F | 18.5 | 14.1 |
| * 13 | 3 | 800. | 0. | 0. | 2733. | 0. | 0. | 895. | 4340. | 0. | ** | 800. | 1705. | .21 | 18. | 16.1 | F | 18.5 | 14.1 |
| * 14 | 3 | 1400. | 0. | 220. | 2733. | 0. | 209. | 895. | 4340. | 0. | ** | 1400. | 1705. | .21 | 14. | 20.6 | F | 17.9 | 14.5 |
| * 15 | 2 | 1400. | 0. | 0. | 2513. | 0. | 0. | 685. | 4000. | 0. | ** | 1400. | 1705. | .17 | 11. | 32.4 | F | 17.5 | 14.8 |
| * 16 | 2 | 1500. | 0. | 360. | 2513. | 0. | 342. | 685. | 4000. | 0. | ** | 1500. | 1705. | .17 | 8. | 41.3 | F | 16.8 | 15.4 |
| * 17 | 2 | 1500. | 0. | 0. | 2153. | 0. | 0. | 343. | 4000. | 0. | ** | 1500. | 1705. | .09 | 5. | 35.3 | F | 17.3 | 15.0 |
| * 18 | 2 | 5000. | 0. | 0. | 2153. | 0. | 0. | 343. | 4000. | 0. | ** | 5000. | 1705. | .09 | 3. | 62.5 | F | 15.3 | 16.6 |
| * 19 | 2 | 5000. | 757. | 0. | 2910. | 757. | 0. | 1100. | 4000. | 0. | ** | 5000. | 1705. | .28 | 3. | 172.0 | F | 9.7 | 25.0 |
| * 20 | 3 | 750. | 1400. | 4310. | 4310. | 1400. | 2500. | 2500. | 2500. | 0. | 0. | 0. | 1.00 | 62. | 13.4 | E | 20.3 | 13.0 | |

* TOTAL 136889. = 25.9 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 29. 19.9 19.5 13.5 *

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREeway TRAVEL TIME = | 1702. VEH-HRS | 2022. PASS-HRS |
| FREeway MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 100. VEH-HRS | 100. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1802. VEH-HRS | 2122. PASS-HRS |

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| | | | | |
|------------------------|----------------|-----------------|----------------|-----------------|
| TOTAL TRAV DISTANCE = | 49466. VEH-MI. | 61761. PASS-MI. | 49466. VEH-MI. | 61761. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 27. MPH. | | 29. MPH. | |
| AVERAGE DENSITY = | 20. VPMP. | | 20. VPMP. | |
| TOTAL FUEL = | 2569. GALLONS | | 2569. GALLONS | |
| TOTAL EMISSIONS = | 683. KILOGRAMS | | 683. KILOGRAMS | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|--------|------------|--------|------------|-------|
| 1 | 0.14 | 2 | 27.35 | 3 | 3.28 | 4 | 0.12 | 5 | 0.11 |
| 6 | 0.12 | 7 | 0.25 | 8 | 0.27 | 9 | 0.27 | 10 | 0.27 |
| 11 | 12.52 | 12 | 9.35 | 13 | 13.50 | 14 | 31.44 | 15 | 39.33 |
| 16 | 52.19 | 17 | 68.57 | 18 | 318.09 | 19 | 363.67 | 20 | 0.26 |

***** TOTAL DELAY = 941.1 VEH-HRS ***** AVERAGE DELAY = 100.77 MIN/VEH *****

***** RAMP DELAYS *****

| | | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|---------|---|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|
| ON-RAMP | 2 | RAMP | 100. | 4.62 | 18.03 | 1.11 | 5.83 | 0.31 | 7.25 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 4.62 | 18.03 | 1.11 | 5.83 | 0.31 | 7.25 |
| ON-RAMP | 4 | RAMP | 100. | 3.30 | 18.03 | 1.11 | 5.83 | 0.31 | 7.25 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 3.30 | 18.03 | 1.11 | 5.83 | 0.31 | 7.25 |

 ** FREEWAY TRAVEL TIME (MINUTES) **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN 1 2 3 4 5 6 7 *

| | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|
| * 1 * | 21.09 | 23.38 | 25.67 | 27.46 | 29.95 | 31.62 | 50.32 |
| * 2 * | 0.45 | 2.74 | 5.03 | 6.82 | 9.31 | 10.98 | 29.68 |
| * 3 * | 0.00 | 1.40 | 3.69 | 5.48 | 7.97 | 9.65 | 28.34 |
| * 4 * | 0.00 | 0.00 | 0.52 | 2.31 | 4.80 | 6.47 | 25.17 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 6.88 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.14 |

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB | * NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|-------|-------|----------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|----------|---------|-----------|-------|--------|-------------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL |
| * 1 | * 3 | * 500. | * 2250. | * 0. | * 2250. | * 2250. | * 0. | * 2250. | * 6000. | * 0. | * 0. | * 0. | * .38 | * 62. | * 12.1 | * B |
| * 2 | * 3 | * 99999. | * 0. | * 0. | * 2250. | * 0. | * 0. | * 2250. | * 6000. | * 0. | * 0. | * 0. | * .38 | * 62. | * 12.1 | * B |
| * 3 | * 2 | * 12000. | * 0. | * 0. | * 2250. | * 0. | * 0. | * 2050. | * 4000. | * 0. | * * | * 299. | * 200. | * .51 | * 61. | * 16.7 |
| * 4 | * 3 | * 350. | * 840. | * 0. | * 3090. | * 840. | * 0. | * 2890. | * 4720. | * 0. | * ** | * 350. | * 200. | * .61 | * 33. | * 29.0 |
| * 5 | * 3 | * 300. | * 0. | * 0. | * 3090. | * 0. | * 0. | * 2890. | * 4720. | * 0. | * ** | * 300. | * 200. | * .61 | * 25. | * 38.3 |
| * 6 | * 3 | * 350. | * 0. | * 720. | * 3090. | * 0. | * 720. | * 2890. | * 4720. | * 0. | * ** | * 350. | * 200. | * .61 | * 20. | * 47.8 |
| * 7 | * 2 | * 940. | * 0. | * 0. | * 2370. | * 0. | * 0. | * 2170. | * 4000. | * 0. | * ** | * 940. | * 200. | * .54 | * 12. | * 89.9 |
| * 8 | * 3 | * 700. | * 1367. | * 0. | * 3737. | * 1367. | * 0. | * 3537. | * 4410. | * 0. | * ** | * 700. | * 200. | * .80 | * 19. | * 61.4 |
| * 9 | * 3 | * 700. | * 0. | * 0. | * 3737. | * 0. | * 0. | * 3537. | * 4410. | * 0. | * ** | * 700. | * 200. | * .80 | * 17. | * 69.1 |
| * 10 | * 3 | * 700. | * 0. | * 320. | * 3737. | * 0. | * 320. | * 3537. | * 4410. | * 0. | * ** | * 700. | * 200. | * .80 | * 15. | * 76.8 |
| * 11 | * 2 | * 2300. | * 0. | * 0. | * 3417. | * 0. | * 0. | * 3217. | * 4000. | * 0. | * ** | * 2300. | * 200. | * .80 | * 15. | * 109.3 |
| * 12 | * 3 | * 700. | * 969. | * 702. | * 4386. | * 900. | * 699. | * 4117. | * 5030. | * 0. | * ** | * 700. | * 200. | * .82 | * 15. | * 89.0 |
| * 13 | * 3 | * 800. | * 0. | * 0. | * 3684. | * 0. | * 0. | * 3418. | * 4340. | * 0. | * ** | * 800. | * 200. | * .79 | * 14. | * 81.7 |

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| | | | | | | | | | | | | | | | | | | | | | |
|---|----|---|-------|------|-------|-------|------|-------|-------|-------|----|----|-------|------|-----|------|-------|------|------|------|---|
| * | 14 | 3 | 1400. | 0. | 340. | 3684. | 0. | 333. | 3418. | 4340. | 0. | ** | 1400. | 200. | .79 | 14. | 81.7 | F | 15.3 | 19.8 | * |
| * | 15 | 2 | 1400. | 0. | 0. | 3344. | 0. | 0. | 3085. | 4000. | 0. | ** | 1400. | 200. | .77 | 13. | 116.5 | F | 14.8 | 20.3 | * |
| * | 16 | 2 | 1500. | 0. | 340. | 3344. | 0. | 338. | 3085. | 4000. | 0. | ** | 1500. | 200. | .77 | 13. | 116.5 | F | 14.8 | 20.3 | * |
| * | 17 | 2 | 1500. | 0. | 1000. | 3004. | 0. | 951. | 2747. | 4000. | 0. | ** | 1500. | 200. | .69 | 10. | 134.9 | F | 13.1 | 22.8 | * |
| * | 18 | 2 | 5000. | 0. | 0. | 2004. | 0. | 0. | 1796. | 4000. | 0. | ** | 5000. | 200. | .45 | 5. | 186.7 | F | 8.3 | 28.9 | * |
| * | 19 | 2 | 5000. | 704. | 0. | 2708. | 704. | 0. | 2500. | 4000. | 0. | ** | 5000. | 200. | .63 | 8. | 148.4 | F | 11.0 | 24.8 | * |
| * | 20 | 3 | 750. | 0. | 2708. | 2708. | 0. | 2500. | 2500. | 2500. | 0. | 0. | 0. | 1.00 | 62. | 13.4 | E | 20.3 | 13.0 | * | |

 * TOTAL 136889. = 25.9 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 30. 32.2 18.2 14.8 *

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 1991. VEH-HRS | 2372. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 235. VEH-HRS | 235. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 2226. VEH-HRS | 2607. PASS-HRS |
| TOTAL TRAV DISTANCE = | 60610. VEH-MI. | 75359. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 27. MPH. | 30. MPH. |
| AVERAGE DENSITY = | 32. VPMP/L | 26. VPMP/L |
| TOTAL FUEL = | 3418. GALLONS | 5987. GALLONS |
| TOTAL EMISSIONS = | 932. KI LOGRAMS | 1615. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|--------|------------|--------|------------|-------|
| 1 | 0.16 | 2 | 31.72 | 3 | 4.58 | 4 | 2.99 | 5 | 4.22 |
| 6 | 6.86 | 7 | 27.24 | 8 | 17.51 | 9 | 20.46 | 10 | 23.41 |
| 11 | 73.67 | 12 | 27.01 | 13 | 29.17 | 14 | 51.06 | 15 | 49.19 |
| 16 | 52.70 | 17 | 64.66 | 18 | 327.45 | 19 | 244.57 | 20 | 0.26 |

***** TOTAL DELAY = 1058.9 VEH-HRS ***** AVERAGE DELAY = 26.46 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-----------|-----------------------|---------------|--------------------------------|----------|---------|---------|----------|----------------------|
| ON-RAMP 2 | RAMP 100. | 100.00 | 6.38 | 36.06 | 2.23 | 11.66 | 0.62 | 14.51 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 100. | 100.00 | 6.38 | 36.06 | 2.23 | 11.66 | 0.62 | 14.51 |
| ON-RAMP 4 | RAMP 169. | 134.50 | 7.55 | 48.50 | 3.00 | 15.68 | 0.83 | 19.51 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 169. | 134.50 | 7.55 | 48.50 | 3.00 | 15.68 | 0.83 | 19.51 |

 ** FREEWAY TRAVEL TIME (MINUTES) **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN 1 2 3 4 5 6 7 *

| | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|
| * 1 * | 21.05 | 22.95 | 24.97 | 26.68 | 29.01 | 30.60 | 47.81 |
| * 2 * | 0.41 | 2.31 | 4.33 | 6.05 | 8.38 | 9.96 | 27.18 |
| * 3 * | 0.00 | 1.17 | 3.19 | 4.91 | 7.23 | 8.82 | 26.03 |
| * 4 * | 0.00 | 0.00 | 0.50 | 2.22 | 4.54 | 6.13 | 23.34 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 6.88 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.14 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. SSEC | * LNS LENGTH | * O-D DATA ORG DES | * DEMANDS SSEC | * ADJUSTED ORG DES | * VOLUMES SSEC | * SSEC CAP. | * WEAVE EFF | * CONGEST LENGTH | * STORAGE RATE | * V/C RATIO | * SPEED MPH | * DENSITY VPMPPL | * LOS LEVEL | * FUEL MPG | * EMISSIONS GS/VM |
|----------------|--------------|--------------------|----------------|--------------------|----------------|-------------|-------------|------------------|----------------|-------------|-------------|------------------|-------------|------------|-------------------|
| * 1 3 | 500. | 1650. | 0. 1650. | 1650. | 0. 1650. | 6000. | 0. | 0. | 0. | .28 | 62. | 8.9 | A | 20.3 | 13.0 |
| * 2 3 | 99999. | 0. | 0. 1650. | 0. | 0. 1650. | 6000. | 0. | 0. | 0. | .28 | 62. | 8.9 | A | 20.3 | 13.0 |
| * 3 2 | 12000. | 0. | 0. 1650. | 0. | 0. 1650. | 4000. | 0. | 0. | 0. | .41 | 62. | 13.4 | B | 20.3 | 13.1 |
| * 4 3 | 350. | 629. | 0. 2279. | 629. | 0. 2279. | 4720. | 0. | 0. | 0. | .48 | 36. | 21.2 | C | 18.5 | 14.3 |
| * 5 3 | 300. | 0. | 0. 2279. | 0. | 0. 2279. | 4720. | 0. | 0. | 0. | .48 | 28. | 27.4 | D | 17.4 | 15.2 |
| * 6 3 | 350. | 0. | 600. 2279. | 0. | 597. 2279. | 4720. | 0. | 0. | 0. | .48 | 23. | 33.6 | D | 16.4 | 16.0 |
| * 7 2 | 940. | 0. | 0. 1679. | 0. | 0. 1682. | 4000. | 0. | 0. | 0. | .42 | 15. | 57.6 | F | 14.1 | 18.1 |
| * 8 3 | 700. | 1279. | 0. 2958. | 1279. | 0. 2958. | 4410. | 0. | 0. | 0. | .67 | 23. | 43.7 | E | 17.2 | 16.5 |
| * 9 3 | 700. | 0. | 0. 2958. | 0. | 0. 2961. | 4410. | 0. | 0. | 0. | .67 | 20. | 48.5 | F | 16.8 | 17.1 |
| * 10 3 | 700. | 0. | 199. 2958. | 0. | 200. 2961. | 4410. | 0. | 0. | 0. | .67 | 19. | 53.3 | F | 16.3 | 17.7 |
| * 11 2 | 2300. | 0. | 0. 2759. | 0. | 0. 2760. | 4000. | 0. | 0. | 0. | .69 | 17. | 80.2 | F | 16.2 | 18.1 |
| * 12 3 | 700. | 810. | 543. 3569. | 879. | 556. 3639. | 5030. | 0. | 0. | 0. | .72 | 16. | 76.1 | F | 16.1 | 18.6 |
| * 13 3 | 800. | 0. | 0. 3026. | 0. | 0. 3083. | 4340. | 0. | 0. | 0. | .71 | 15. | 68.8 | F | 15.8 | 19.1 |
| * 14 3 | 1400. | 0. | 281. 3026. | 0. | 286. 3455. | 4340. | 0. | * 1190. | -372. | .80 | 14. | 80.3 | F | 15.6 | 19.4 |
| * 15 2 | 1400. | 0. | 0. 2745. | 0. | 0. 3169. | 4000. | 0. | ** 1400. | -372. | .79 | 14. | 111.9 | F | 15.4 | 19.6 |
| * 16 2 | 1500. | 0. | 349. 2745. | 0. | 352. 3169. | 4000. | 0. | ** 1500. | -372. | .79 | 14. | 111.9 | F | 15.4 | 19.6 |
| * 17 2 | 1500. | 0. | 850. 2396. | 0. | 860. 2817. | 4000. | 0. | ** 1500. | -372. | .70 | 11. | 131.1 | F | 13.4 | 22.3 |
| * 18 2 | 5000. | 0. | 0. 1546. | 0. | 0. 1957. | 4000. | 0. | ** 5000. | -372. | .49 | 5. | 177.9 | F | 8.6 | 28.3 |
| * 19 2 | 5000. | 543. | 0. 2089. | 543. | 0. 2500. | 4000. | 0. | ** 5000. | -372. | .63 | 8. | 148.4 | F | 11.0 | 24.8 |
| * 20 3 | 750. | 0. | 2089. 2089. | 0. | 2500. 2500. | 2500. | 0. | 0. | 0. | 1.00 | 62. | 13.4 | E | 20.3 | 13.0 |
| * TOTAL | 136889. | = | 25.9 MILES | | | | | MAX(V/C) = 1.00 | LOWEST LOS = F | AVG = 28. | 27.8 | | | 17.8 | 15.2 |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 1696. VEH-HRS | 2006. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 235. VEH-HRS | 235. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1931. VEH-HRS | 2240. PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 47564. VEH-MI. | 58869. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 25. MPH. | 29. MPH. |
| AVERAGE DENSITY = | 28. VPMPPL | 27. VPMPPL |
| TOTAL FUEL = | 2760. GALLONS | 8747. GALLONS |
| TOTAL EMISSIONS = | 756. KILOGRAMS | 2371. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|--------|------------|--------|------------|-------|
| 1 | 0.12 | 2 | 23.26 | 3 | 3.23 | 4 | 1.91 | 5 | 2.74 |
| 6 | 4.49 | 7 | 16.98 | 8 | 11.92 | 9 | 14.07 | 10 | 16.23 |
| 11 | 56.29 | 12 | 24.85 | 13 | 26.80 | 14 | 49.75 | 15 | 46.43 |
| 16 | 49.75 | 17 | 62.18 | 18 | 308.50 | 19 | 244.57 | 20 | 0.26 |

***** TOTAL DELAY = 964.3 VEH-HRS ***** AVERAGE DELAY = 24.17 MIN/VEH *****

***** RAMP DELAYS *****

| ON-RAMP | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|---------|-----------------------|---------------|--------------------------------|----------|---------|---------|----------|----------------------|
| 2 | RAMP | 100. | 100.00 | 8.23 | 36.06 | 2.23 | 11.66 | 14.51 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 100.00 | 8.23 | 36.06 | 2.23 | 11.66 | 14.51 |
| 4 | RAMP | 100. | 134.50 | 8.24 | 48.50 | 3.00 | 15.68 | 19.51 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 134.50 | 8.24 | 48.50 | 3.00 | 15.68 | 19.51 |

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FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP LLL
FFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 1111111 222222222 PPP LLLLLLLLLL
    
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FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 13 AND 18 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 62
LOWER LIMB (AT V/C=1) = 30
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

FREWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC | SSEC | DESIGN | ORG | TRK | SSEC | PCT | PCT | DES | SPECIAL | FF.SPD. | CAP. | ART | GRADE | SUBSECTION | LOCATION |
|---------|------|-------|--------|-----|-----|------|-----|--------|------|---------|----------|----------|------|----------|-----------------------|----------|
| SEC | LNS | CAP | LENGTH | DES | FAC | GRAD | TRK | TRUCKS | RAMP | RAMP | ALT. RTE | ALT. RTE | TYPE | ALT. RTE | | |
| ** 1 | | | | | | | | | | | | | | | | ** |
| ** 2 | | | | | | | | | | | | | | | | ** |
| ** 3 | | | | | | | | | | | | | | | | ** |
| ** 4 | | | | | | | | | | | | | | | | ** |
| ** 5 | | | | | | | | | | | | | | | | ** |
| ** 6 | | | | | | | | | | | | | | | | ** |
| ** 7 | | | | | | | | | | | | | | | | ** |
| ** 8 | | | | | | | | | | | | | | | | ** |
| ** 9 | | | | | | | | | | | | | | | | ** |
| ** 10 | | | | | | | | | | | | | | | | ** |
| ** 11 | | | | | | | | | | | | | | | | ** |
| ** 12 | | | | | | | | | | | | | | | | ** |
| ** 13 | 1 | 1650. | 800. | 62 | 0 | 0.95 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda / Persian | HOV |
| ** 14 | 1 | 1650. | 1400. | 62 | D | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Persian On-Ramp w/HOV | |
| ** 15 | 1 | 1650. | 1400. | 62 | | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | West of Lawrence E | |
| ** 16 | 1 | 1650. | 1500. | 62 | D | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence Off-ramp | |
| ** 17 | 1 | 1650. | 1500. | 62 | D | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | End of DKS | |
| ** 18 | 1 | 1650. | 5000. | 62 | D | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | |
| ** 19 | | | | | | | | | | | | | | | | ** |

** 20 **

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 16:34 PAGE 3
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 1 OF 3

 ** FREeway TRAVEL TIME (MINUTES) **

| * ORIGINS | * DESTINATIONS ACROSS * | | | | | | | |
|-----------|-------------------------|------|------|------|------|------|------|------|
| * DOWN | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.13 | 0.00 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 16:34 PAGE 4
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 1 OF 3

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | |
|-----------|--------|------------|-----------|------------|----------------|--------|---------|-----------------|-----------|----------------|---------|-----------|---------|--------|-------------|------|------|------|
| * SEC | * LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPML | * LEVEL | * MPG | * GS/VM | | | |
| * 1 | | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | | |
| * 3 | | | | | | | | | | | | | | | | | | |
| * 4 | | | | | | | | | | | | | | | | | | |
| * 5 | | | | | | | | | | | | | | | | | | |
| * 6 | | | | | | | | | | | | | | | | | | |
| * 7 | | | | | | | | | | | | | | | | | | |
| * 8 | | | | | | | | | | | | | | | | | | |
| * 9 | | | | | | | | | | | | | | | | | | |
| * 10 | | | | | | | | | | | | | | | | | | |
| * 11 | | | | | | | | | | | | | | | | | | |
| * 12 | | | | | | | | | | | | | | | | | | |
| * 13 | 1 | 800. | 757. | 0. | 757. | 757. | 0. | 757. | 1650. | 0. | 0. | 0. | .46 | 62. | 12.2 | B | 21.6 | 12.8 |
| * 14 | 1 | 1400. | 0. | 0. | 757. | 0. | 0. | 757. | 1650. | 0. | 0. | 0. | .46 | 62. | 12.2 | B | 21.6 | 12.8 |
| * 15 | 1 | 1400. | 0. | 0. | 757. | 0. | 0. | 757. | 1650. | 0. | 0. | 0. | .46 | 62. | 12.2 | B | 21.6 | 12.8 |
| * 16 | 1 | 1500. | 0. | 0. | 757. | 0. | 0. | 757. | 1650. | 0. | 0. | 0. | .46 | 62. | 12.2 | B | 21.6 | 12.8 |
| * 17 | 1 | 1500. | 0. | 0. | 757. | 0. | 0. | 757. | 1650. | 0. | 0. | 0. | .46 | 62. | 12.2 | B | 21.6 | 12.8 |
| * 18 | 1 | 5000. | 0. | 757. | 757. | 0. | 757. | 757. | 1650. | 0. | 0. | 0. | .46 | 62. | 12.2 | B | 21.6 | 12.8 |
| * 19 | | | | | | | | | | | | | | | | | | |
| * 20 | | | | | | | | | | | | | | | | | | |
| * TOTAL | | 11600. | = | 2.2 | MILES | | | MAX(V/C) = 0.46 | | LOWEST LOS = B | | AVG = 62. | 12.2 | | 21.6 | 12.8 | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 27. VEH-HRS | 54. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 27. VEH-HRS | 54. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 1662. VEH-MI. | 3324. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 62. MPH. |
| AVERAGE DENSITY = | 12. VPML | 12. VPML |
| TOTAL FUEL = | 77. GALLONS | 77. GALLONS |
| TOTAL EMISSIONS = | 21. KILOGRAMS | 21. KILOGRAMS |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 Page 2

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.09 | 14 | 0.15 | 15 | 0.15 |
| 16 | 0.16 | 17 | 0.16 | 18 | 0.53 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 1.2 VEH-HRS ***** AVERAGE DELAY = 0.10 MIN/VEH *****

 **
 ** FREeway TRAVEL TIME (MINUTES) **
 **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|-------|-----------------------|------|------|------|------|------|------|------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| + | * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.13 | 0.00 |
| + | * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISS |
|-----------|--------|------------|-----------|---------------------|------------|----------|-----------|-----------|---------|---------|-----------|-------|---------|---------|
| * SEC | * LNS | * LENGTH | * ORG DES | * SSEC ORG DES SSEC | * CAP. EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | |
| * 1 | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | |
| * 3 | | | | | | | | | | | | | | |
| * 4 | | | | | | | | | | | | | | |
| * 5 | | | | | | | | | | | | | | |
| * 6 | | | | | | | | | | | | | | |
| * 7 | | | | | | | | | | | | | | |
| * 8 | | | | | | | | | | | | | | |
| * 9 | | | | | | | | | | | | | | |
| * 10 | | | | | | | | | | | | | | |
| * 11 | | | | | | | | | | | | | | |
| * 12 | | | | | | | | | | | | | | |
| * 13 | 1 | 800. | 704. | 0. 704. | 704. | 0. 704. | 1650. | 0. 0. | 0. 0. | .43 62. | 11.3 B | 21.6 | 12.8 | |
| * 14 | 1 | 1400. | 0. 704. | 0. 704. | 0. 704. | 1650. | 0. 0. | 0. 0. | .43 62. | 11.3 B | 21.6 | 12.8 | | |
| * 15 | 1 | 1400. | 0. 704. | 0. 704. | 0. 704. | 1650. | 0. 0. | 0. 0. | .43 62. | 11.3 B | 21.6 | 12.8 | | |
| * 16 | 1 | 1500. | 0. 704. | 0. 704. | 0. 704. | 1650. | 0. 0. | 0. 0. | .43 62. | 11.3 B | 21.6 | 12.8 | | |
| * 17 | 1 | 1500. | 0. 704. | 0. 704. | 0. 704. | 1650. | 0. 0. | 0. 0. | .43 62. | 11.3 B | 21.6 | 12.8 | | |
| * 18 | 1 | 5000. | 0. 704. | 0. 704. | 0. 704. | 1650. | 0. 0. | 0. 0. | .43 62. | 11.3 B | 21.6 | 12.8 | | |
| * 19 | | | | | | | | | | | | | | |
| * 20 | | | | | | | | | | | | | | |
| * TOTAL | 11600. | = | 2.2 MILES | | | | | | | | | | | |
| | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 25. VEH-HRS | 50. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 25. VEH-HRS | 50. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 1546. VEH-MI. | 3091. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 62. MPH. |

AVERAGE DENSITY = 11. VP MPL
TOTAL FUEL = 72. GALLONS
TOTAL EMISSIONS = 20. KI LOGRAMS

Table with columns: SUBSECTION, DELAY, DESIRED SPEED = 65.0. Rows 1-20 showing delay values for various subsections.

**
** FREEWAY TRAVEL TIME (MINUTES)
**

Table with columns: ORIGINS DOWN, DESTINATIONS ACROSS (1-8). Rows 1-7 showing travel times between origins and destinations.

TIME SLICE FREEWAY PERFORMANCE TABLE

Table with columns: SUB NO., SSEC, O-D DATA DEMANDS, ADJUSTED VOLUMES, SSEC WEAVE CONGEST STORAGE, V/C SPEED DENSITY LOS, FUEL EMISSIONS. Rows 1-20 showing performance metrics.

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| | CURRENT TIME SLICE | | CUMULATIVE VALUES | | | |
|-----------------------------|--------------------|----------------|-------------------|----------------|--|--|
| FREEWAY TRAVEL TIME = | 19. VEH-HRS | 38. PASS-HRS | 71. VEH-HRS | 142. PASS-HRS | | |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | | |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | | |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | | |
| TOTAL SYSTEM TRAVEL TIME = | 19. VEH-HRS | 38. PASS-HRS | 71. VEH-HRS | 142. PASS-HRS | | |
| TOTAL FRWAY TRAV DISTANCE = | 1193. VEH-MI. | 2387. PASS-MI. | 4401. VEH-MI. | 8802. PASS-MI. | | |
| AVERAGE SYSTEM SPEED = | 62. MPH. | | 62. MPH. | | | |
| AVERAGE DENSITY = | 9. VPMP. | | 11. VPMP. | | | |
| TOTAL FUEL = | 55. GALLONS | | 204. GALLONS | | | |
| TOTAL EMISSIONS = | 15. KILOGRAMS | | 56. KILOGRAMS | | | |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 16:34 PAGE 11
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 3 OF 3

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.06 | 14 | 0.11 | 15 | 0.11 |
| 16 | 0.11 | 17 | 0.11 | 18 | 0.38 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 0.9 VEH-HRS ***** AVERAGE DELAY = 0.10 MIN/VEH *****

```

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A.D.MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP LLL
FFFFFFFF RRRRRRRR EEEEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 1111111 222222222 PPP LLLLLLLLLL

```

FREQ12PL

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 3 AND 7 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 2.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 30
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

ON-RAMP CAPACITY LIMITS

```

1 2 3 4 5 6 7 8
6000.***** 1500. 1500.***** 2000. 1500. 1500.

```

OFF-RAMP CAPACITY LIMITS

```

1 2 3 4 5 6 7 8
***** 2000. 2000. 1500. 1500. 1500. 6000.

```

```

ON-RAMP 1 IS THE MAINLINE ORIGIN
OFF-RAMP 8 IS THE MAINLINE DESTINATION

```

```

***** ON-RAMPS 2 AND 5 ARE SYNTHETIC ORIGINS USED TO ENTER AND LEAVE THE PL LANE(S)
***** OFF-RAMPS 1 AND 2 ARE SYNTHETIC DESTINATIONS USED TO ENTER AND LEAVE THE PL LANE(S)

```

INPUT HAS BEEN COMPLETED

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*****
*****
**
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**

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FREeway AND ARTERIAL DESIgn FEATuRES

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**

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| ** SUB NO. | ** SSEC | ** SSEC | ** DESIGN | ** ORG | ** TRK | ** SSEC | ** PCT | ** PCT | ** DES | ** SPECIAL | ** FF.SPD. | ** CAP. | ** ART | ** GRADE | ** SUBSECTION | ** LOCATION |
|------------|---------|-----------|-----------|--------|--------|---------|--------|-----------|---------|-------------|-------------|---------|-------------|-------------|----------------------|-------------|
| ** SEC LNS | ** CAP | ** LENGTH | ** SPEED | ** DES | ** FAC | ** GRAD | ** TRK | ** TRUCKS | ** RAMP | ** ALT. RTE | ** ALT. RTE | ** TYPE | ** ALT. RTE | ** ALT. RTE | ** ALT. RTE | ** ALT. RTE |
| ** 1 | | | | | | | | | | | | | | | | |
| ** 2 | | | | | | | | | | | | | | | | |
| ** 3 | 1 | 1650. | 11000. | 62 | 0 | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | ** |
| ** 4 | 1 | 1650. | 1500. | 62 | 0 | 0.95 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Lawrence On-ramp | ** |
| ** 5 | 1 | 1650. | 1400. | 62 | | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence to Crossman | ** |
| ** 6 | 1 | 1650. | 1500. | 62 | 0 | 0.95 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Crossman On-Ramp | ** |
| ** 7 | 1 | 1650. | 1300. | 62 | D | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Crossman / Mathilda | ** |


```

* 20
*
*****
* TOTAL 16700. = 3.2 MILES MAX(V/C) = 0.73 LOWEST LOS = C AVG = 62. 19.3 21.6 12.8
*
*****

```

```

CURRENT TIME SLICE CUMULATIVE VALUES
FREEWAY TRAVEL TIME = 31. VEH-HRS 61. PASS-HRS 31. VEH-HRS 61. PASS-HRS
FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 31. VEH-HRS 61. PASS-HRS 31. VEH-HRS 61. PASS-HRS
TOTAL FRWAY TRAV DI STANCE = 1895. VEH-MI . 3790. PASS-MI . 1895. VEH-MI . 3790. PASS-MI .
AVERAGE SYSTEM SPEED = 62. MPH 62. MPH
AVERAGE DENSITY = 19. VPMP 19. VPMP
TOTAL FUEL = 88. GALLONS 88. GALLONS
TOTAL EMISSIONS = 24. KI LOGRAMS 24. KI LOGRAMS

```

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 13:42 PAGE 6
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 1 OF 4

```

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
1 0.00 2 0.00 3 0.93 4 0.13 5 0.12
6 0.13 7 0.11 8 0.00 9 0.00 10 0.00
11 0.00 12 0.00 13 0.00 14 0.00 15 0.00
16 0.00 17 0.00 18 0.00 19 0.00 20 0.00
***** TOTAL DELAY = 1.4 VEH-HRS ***** AVERAGE DELAY = 0.07 MIN/VEH *****

```

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 13:42 PAGE 7
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 4

```

*****
** FREEWAY TRAVEL TIME (MINUTES) **
*****

```

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | | |
|-----------------|---------------------|------|------|------|------|------|------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| 1 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | 0.00 | 3.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 4 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 5 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 7 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 8 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 13:42 PAGE 8
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 4

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS | | | |
|---------|------|----------|---------|------------------|-------|-------|---------|---------|-------|-------|---------|-------|------|--------|---|------|------|
| SEC | LNS | LENGTH | ORG | DES | ORG | DES | LENGTH | RATE | RATIO | MPH | VPMP | LEVEL | MPG | GS/VM | | | |
| 1 | | | | | | | | | | | | | | | | | |
| 2 | | | | | | | | | | | | | | | | | |
| 3 | 1 | 11000. | 1198. | 0. | 1198. | 1198. | 0. | 1198. | 1650. | 0. | 0. | .73 | 62. | 19.3 | C | 21.6 | 12.8 |
| 4 | 1 | 1500. | 0. | 0. | 1198. | 0. | 0. | 1198. | 1650. | 0. | 0. | .73 | 62. | 19.3 | C | 21.6 | 12.8 |
| 5 | 1 | 1400. | 0. | 0. | 1198. | 0. | 0. | 1198. | 1650. | 0. | 0. | .73 | 62. | 19.3 | C | 21.6 | 12.8 |
| 6 | 1 | 1500. | 0. | 0. | 1198. | 0. | 0. | 1198. | 1650. | 0. | 0. | .73 | 62. | 19.3 | C | 21.6 | 12.8 |
| 7 | 1 | 1300. | 0. | 1198. | 1198. | 0. | 1198. | 1198. | 1650. | 0. | 0. | .73 | 62. | 19.3 | C | 21.6 | 12.8 |
| 8 | | | | | | | | | | | | | | | | | |
| 9 | | | | | | | | | | | | | | | | | |

```

* 10
* 11
* 12
* 13
* 14
* 15
* 16
* 17
* 18
* 19
* 20
*****
* TOTAL 16700. = 3.2 MILES MAX(V/C) = 0.73 LOWEST LOS = C AVG = 62. 19.3 21.6 12.8
*****

```

```

CURRENT TIME SLICE CUMULATIVE VALUES
FREEWAY TRAVEL TIME = 31. VEH-HRS 61. PASS-HRS 61. VEH-HRS 122. PASS-HRS
FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 31. VEH-HRS 61. PASS-HRS 61. VEH-HRS 122. PASS-HRS
TOTAL FRWAY TRAV DISTANCE = 1895. VEH-MI. 3790. PASS-MI. 3790. VEH-MI. 7580. PASS-MI.
AVERAGE SYSTEM SPEED = 62. MPH. 62. MPH.
AVERAGE DENSITY = 19. VPMP. 19. VPMP.
TOTAL FUEL = 88. GALLONS 176. GALLONS
TOTAL EMISSIONS = 24. KILOGRAMS 48. KILOGRAMS

```

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 13:42 PAGE 9
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 4

```

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
1 0.00 2 0.00 3 0.93 4 0.13 5 0.12
6 0.13 7 0.11 8 0.00 9 0.00 10 0.00
11 0.00 12 0.00 13 0.00 14 0.00 15 0.00
16 0.00 17 0.00 18 0.00 19 0.00 20 0.00
***** TOTAL DELAY = 1.4 VEH-HRS ***** AVERAGE DELAY = 0.07 MIN/VEH *****

```

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 13:42 PAGE 10
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 3 OF 4

```

*****
**
** FREEWAY TRAVEL TIME (MINUTES) **
**
*****

```

```

*****
* ORIGINS DESTINATIONS ACROSS *
* DOWN 1 2 3 4 5 6 7 8 *
+
* * * * *
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 2 * 0.00 3.06 0.00 0.00 0.00 0.00 0.00 0.00
+
* 3 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 4 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 5 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 8 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* * * * *
*****

```

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 13:42 PAGE 11
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 3 OF 4

```

*****
* TIME SLICE FREEWAY PERFORMANCE TABLE *
*****
* SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMISSIONS *
* SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMP LEVEL MPG GS/VM *
*****

```



```

*
* 1
* 2
* 3 1 11000. 1227. 0. 1227. 1227. 0. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8
* 4 1 1500. 0. 0. 1227. 0. 0. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8
* 5 1 1400. 0. 0. 1227. 0. 0. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8
* 6 1 1500. 0. 0. 1227. 0. 0. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8
* 7 1 1300. 0. 1227. 1227. 0. 1227. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8
* 8
* 9
* 10
* 11
* 12
* 13
* 14
* 15
* 16
* 17
* 18
* 19
* 20
*****
*
* TOTAL 16700. = 3.2 MILES MAX(V/C) = 0.74 LOWEST LOS = C AVG = 62. 19.8 21.6 12.8
*
*****

```

```

CURRENT TIME SLICE CUMULATIVE VALUES
FREEWAY TRAVEL TIME = 31. VEH-HRS 63. PASS-HRS 92. VEH-HRS 185. PASS-HRS
FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 31. VEH-HRS 63. PASS-HRS 92. VEH-HRS 185. PASS-HRS
TOTAL FRWAY TRAV DISTANCE = 1941. VEH-MI. 3881. PASS-MI. 5731. VEH-MI. 11462. PASS-MI.
AVERAGE SYSTEM SPEED = 62. MPH. 62. MPH.
AVERAGE DENSITY = 20. VPML 19. VPML
TOTAL FUEL = 90. GALLONS 266. GALLONS
TOTAL EMISSIONS = 25. KILOGRAMS 73. KILOGRAMS

```

```

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
1 0.00 2 0.00 3 0.95 4 0.13 5 0.12
6 0.13 7 0.11 8 0.00 9 0.00 10 0.00
11 0.00 12 0.00 13 0.00 14 0.00 15 0.00
16 0.00 17 0.00 18 0.00 19 0.00 20 0.00
***** TOTAL DELAY = 1.4 VEH-HRS ***** AVERAGE DELAY = 0.07 MIN/VEH *****

```

```

*****
**
** FREeway TRAVEL TIME (MINUTES) **
**
*****

```

```

*****
* ORIGINS DESTINATIONS ACROSS *
* DOWN 1 2 3 4 5 6 7 8 *
+
* * * * *
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 2 * 0.00 3.06 0.00 0.00 0.00 0.00 0.00 0.00
+
* 3 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 4 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 5 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 8 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* * * * *
*****

```

 *
 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *
 *
 *
 * SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMISS *
 * SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMP L LEVEL MPG GS/VM *
 *
 * 1 *
 * 2 *
 * 3 1 11000. 1227. 0. 1227. 1227. 0. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8 *
 * 4 1 1500. 0. 0. 1227. 0. 0. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8 *
 * 5 1 1400. 0. 0. 1227. 0. 0. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8 *
 * 6 1 1500. 0. 0. 1227. 0. 0. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8 *
 * 7 1 1300. 0. 1227. 1227. 0. 1227. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8 *
 * 8 *
 * 9 *
 * 10 *
 * 11 *
 * 12 *
 * 13 *
 * 14 *
 * 15 *
 * 16 *
 * 17 *
 * 18 *
 * 19 *
 * 20 *
 *
 *
 * TOTAL 16700. = 3.2 MILES MAX(V/C) = 0.74 LOWEST LOS = C AVG = 62. 19.8 21.6 12.8 *
 *

| | | |
|-----------------------------|--------------------|-------------------|
| | CURRENT TIME SLICE | CUMULATIVE VALUES |
| FREEWAY TRAVEL TIME = | 31. VEH-HRS | 124. VEH-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 31. VEH-HRS | 124. VEH-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 1941. VEH-MI. | 3881. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 62. MPH. |
| AVERAGE DENSITY = | 20. VPMP L | 20. VPMP L |
| TOTAL FUEL = | 90. GALLONS | 356. GALLONS |
| TOTAL EMISSIONS = | 25. KI LOGRAMS | 98. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| | | | | | | | | | |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
| 1 | 0.00 | 2 | 0.00 | 3 | 0.95 | 4 | 0.13 | 5 | 0.12 |
| 6 | 0.13 | 7 | 0.11 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 1.4 VEH-HRS ***** AVERAGE DELAY = 0.07 MIN/VEH *****

 **
 ** FREeway TRAVEL TIME (MINUTES) **
 **

| | | | | | | | | | |
|---|--------------|---------------------|------|-------|-------|-------|-------|-------|-------|
| | ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | | |
| | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| + | | ***** | | | | | | | |
| + | | ***** | | | | | | | |
| + | * 1 * | 17.88 | 0.00 | 21.31 | 22.48 | 22.55 | 22.73 | 23.27 | 25.45 |
| + | * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 3 * | 0.00 | 0.00 | 1.33 | 2.50 | 2.57 | 2.76 | 3.29 | 5.47 |
| + | * 4 * | 0.00 | 0.00 | 0.78 | 1.95 | 2.02 | 2.20 | 2.74 | 4.92 |
| + | * 5 * | 0.00 | 0.00 | 0.15 | 1.32 | 1.39 | 1.58 | 2.11 | 4.30 |
| + | * 6 * | 0.00 | 0.00 | 0.00 | 0.32 | 0.40 | 0.58 | 1.11 | 3.30 |
| + | * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 | 0.71 | 2.89 |
| + | * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.53 | 2.72 |
| + | | ***** | | | | | | | |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB | * NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|-------|-------|----------|------------|-------------|------------|-------------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|
| * SEC | * LNS | * LENGTH | * ORG | * DES SSEC | * ORG | * DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMPPL | * LEVEL | * MPG | * GS/VM |
| * 1 | 3 | 500. | 4609. | 0. 4609. | 4609. | 0. 4609. | 6000. | 0. | 0. | 0. | .77 | 64. | 24.1 | C | 19.5 | 13.7 |
| * 2 | 3 | 99999. | 0. 1198. | 0. 4609. | 0. 1198. | 0. 4609. | 6000. | 0. | 0. | 0. | .77 | 64. | 24.1 | C | 19.5 | 13.7 |
| * 3 | 2 | 11000. | 0. | 0. 3431. | 0. | 0. 3431. | 4000. | 0. | 0. | 0. | .85 | 60. | 28.6 | D | 21.5 | 12.3 |
| * 4 | 2 | 1500. | 20. | 0. 3431. | 20. | 0. 3431. | 4000. | 0. | 0. | 0. | .86 | 60. | 28.8 | D | 21.5 | 12.3 |
| * 5 | 2 | 1400. | 0. | 0. 3431. | 0. | 0. 3431. | 4000. | 0. | 0. | 0. | .86 | 60. | 28.8 | D | 21.5 | 12.3 |
| * 6 | 2 | 1500. | 290. | 0. 3721. | 290. | 0. 3721. | 4000. | 0. | 0. | 0. | .93 | 56. | 33.0 | D | 22.5 | 11.7 |
| * 7 | 2 | 1300. | 0. | 0. 3721. | 0. | 0. 3542. | 4000. | 0. | * 1131. | 179. | .89 | 46. | 38.5 | F | 21.8 | 12.2 |
| * 8 | 3 | 500. | 1198. | 950. 4919. | 1198. | 950. 4740. | 5130. | 0. | ** 500. | 179. | .92 | 37. | 42.9 | F | 21.3 | 12.8 |
| * 9 | 2 | 2300. | 0. | 0. 3969. | 0. | 0. 3790. | 4000. | 0. | ** 2300. | 179. | .95 | 31. | 61.2 | F | 20.9 | 13.2 |
| * 10 | 3 | 250. | 160. | 0. 4129. | 160. | 0. 3950. | 4250. | 0. | ** 250. | 179. | .93 | 25. | 51.7 | F | 19.1 | 14.9 |
| * 11 | 3 | 200. | 0. | 0. 4129. | 0. | 0. 3950. | 4250. | 0. | ** 200. | 179. | .93 | 24. | 53.8 | F | 19.1 | 15.0 |
| * 12 | 3 | 250. | 0. | 1550. 4129. | 0. | 1550. 3950. | 4250. | 0. | ** 250. | 179. | .93 | 24. | 55.8 | F | 19.1 | 15.0 |
| * 13 | 2 | 50. | 0. | 0. 2579. | 0. | 0. 2400. | 4000. | 0. | ** 50. | 179. | .60 | 8. | 151.8 | F | 10.5 | 25.4 |
| * 14 | 2 | 50. | 0. | 0. 2579. | 0. | 0. 2400. | 2400. | 0. | 0. | 0. | 1.00 | 65. | 18.5 | E | 19.0 | 14.1 |
| * 15 | 2 | 1000. | 0. | 0. 2579. | 0. | 0. 2400. | 4000. | 0. | 0. | 0. | .60 | 65. | 18.5 | C | 19.0 | 14.1 |
| * 16 | 2 | 10. | 0. | 0. 2579. | 0. | 0. 2400. | 4000. | 0. | 0. | 0. | .60 | 65. | 18.5 | C | 19.0 | 14.1 |
| * 17 | 2 | 1500. | 616. | 0. 3195. | 616. | 0. 3016. | 4000. | 0. | 0. | 0. | .75 | 64. | 23.5 | C | 19.4 | 13.8 |
| * 18 | 2 | 1500. | 0. | 789. 3195. | 0. | 745. 3016. | 4000. | 0. | 0. | 0. | .75 | 64. | 23.5 | C | 19.4 | 13.8 |
| * 19 | 2 | 12000. | 0. | 0. 2406. | 0. | 0. 2271. | 4000. | 0. | 0. | 0. | .57 | 65. | 17.5 | B | 19.0 | 14.1 |
| * 20 | 3 | 500. | 0. | 2406. 2406. | 0. | 2271. 2271. | 6000. | 0. | 0. | 0. | .38 | 65. | 11.6 | B | 19.0 | 14.1 |

TOTAL 137309. = 26.0 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 62. 25.0 19.7 13.6

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 886. VEH-HRS | 1092. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 886. VEH-HRS | 1092. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 54474. VEH-MI. | 67235. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 62. MPH. |
| AVERAGE DENSITY = | 25. VPMPPL | 25. VPMPPL |
| TOTAL FUEL = | 2771. GALLONS | 2771. GALLONS |
| TOTAL EMISSIONS = | 738. KILOGRAMS | 738. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.06 | 2 | 11.98 | 3 | 4.88 | 4 | 0.69 | 5 | 0.65 |
| 6 | 1.26 | 7 | 2.89 | 8 | 2.71 | 9 | 14.20 | 10 | 2.25 |
| 11 | 1.91 | 12 | 2.53 | 13 | 1.26 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.09 | 18 | 0.09 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 47.5 VEH-HRS ***** AVERAGE DELAY = 0.73 MIN/VEH *****

 ** FREeway TRAVEL TIME (MINUTES) **

| * ORIGINS | * DESTINATIONS ACROSS * | | | | | | | |
|-----------|-------------------------|------|-------|-------|-------|-------|-------|-------|
| * DOWN | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 17.88 | 0.00 | 22.57 | 24.00 | 24.08 | 24.26 | 24.79 | 26.98 |
| * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 3 * | 0.00 | 0.00 | 2.60 | 4.02 | 4.10 | 4.28 | 4.81 | 7.00 |

| | | | | | | | | |
|-------|-------|------|-------|-------|-------|-------|-------|-------|
| * 1 * | 18.00 | 0.00 | 23.69 | 25.00 | 25.06 | 25.24 | 25.85 | 28.03 |
| * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 3 * | 0.00 | 0.00 | 3.39 | 4.70 | 4.75 | 4.94 | 5.54 | 7.73 |
| * 4 * | 0.00 | 0.00 | 1.54 | 2.85 | 2.91 | 3.09 | 3.70 | 5.89 |
| * 5 * | 0.00 | 0.00 | 0.21 | 1.52 | 1.58 | 1.76 | 2.37 | 4.55 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.32 | 0.37 | 0.56 | 1.16 | 3.35 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 | 0.78 | 2.97 |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.61 | 2.79 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED | VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS | | | | |
|---------|------|----------|--------------|--------------|---------|-------|--------|---------|---------|-----|-------|---------|------|-------|--------|-------|------|------|------|
| SEC | LNS | LENGTH | ORG DES SSEC | ORG DES SSEC | CAP. | EFF | LENGTH | RATE | RATIO | MPH | VPMPL | LEVEL | MPG | GS/VM | | | | | |
| * 1 | 3 | 500. | 4720. | 0. | 4720. | 4720. | 0. | 4720. | 6000. | 0. | 0. | 0. | .79 | 63. | 24.8 | C | 19.7 | 13.5 | |
| * 2 | 3 | 99999. | 0. | 1227. | 4720. | 0. | 1227. | 4720. | 6000. | 0. | 0. | 0. | .79 | 63. | 24.8 | C | 19.7 | 13.5 | |
| * 3 | 2 | 11000. | 0. | 0. | 3493. | 0. | 0. | 3354. | 4000. | 0. | ** | 1415. | 139. | .84 | 54. | 31.0 | F | 21.4 | 12.4 |
| * 4 | 2 | 1500. | 19. | 0. | 3512. | 19. | 0. | 3373. | 4000. | 0. | ** | 1500. | 139. | .84 | 19. | 88.3 | F | 17.5 | 16.9 |
| * 5 | 2 | 1400. | 0. | 0. | 3512. | 0. | 0. | 3373. | 4000. | 0. | ** | 1400. | 139. | .84 | 17. | 100.8 | F | 16.8 | 18.0 |
| * 6 | 2 | 1500. | 400. | 0. | 3912. | 400. | 0. | 3773. | 4000. | 0. | ** | 1500. | 139. | .94 | 24. | 79.0 | F | 19.5 | 14.6 |
| * 7 | 2 | 1300. | 0. | 0. | 3912. | 0. | 0. | 3773. | 4000. | 0. | ** | 1300. | 139. | .94 | 24. | 79.0 | F | 19.5 | 14.6 |
| * 8 | 3 | 500. | 1227. | 1130. | 5139. | 1227. | 1128. | 5000. | 5130. | 0. | ** | 500. | 130. | .97 | 27. | 61.7 | F | 20.4 | 13.6 |
| * 9 | 2 | 2300. | 0. | 0. | 4009. | 0. | 0. | 3872. | 4000. | 0. | ** | 2300. | 128. | .97 | 26. | 73.6 | F | 20.2 | 13.8 |
| * 10 | 3 | 250. | 194. | 0. | 4203. | 194. | 0. | 4066. | 4250. | 0. | ** | 250. | 128. | .96 | 25. | 53.9 | F | 19.9 | 14.1 |
| * 11 | 3 | 200. | 0. | 0. | 4203. | 0. | 0. | 4066. | 4250. | 0. | ** | 200. | 128. | .96 | 25. | 53.9 | F | 19.9 | 14.1 |
| * 12 | 3 | 250. | 0. | 1320. | 4203. | 0. | 1317. | 4066. | 4250. | 0. | ** | 250. | 128. | .96 | 25. | 53.9 | F | 19.9 | 14.1 |
| * 13 | 2 | 50. | 0. | 0. | 2883. | 0. | 349. | 2749. | 4000. | 0. | ** | 50. | 128. | .69 | 10. | 134.8 | F | 13.1 | 22.8 |
| * 14 | 2 | 50. | 0. | 0. | 2533. | 0. | 0. | 2400. | 2400. | 0. | 0. | 0. | 1.00 | 65. | 18.5 | E | 19.0 | 14.1 | |
| * 15 | 2 | 1000. | 350. | 0. | 2883. | 350. | 0. | 2750. | 4000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 19.0 | 14.1 | |
| * 16 | 2 | 10. | 0. | 0. | 2883. | 0. | 0. | 2750. | 4000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 19.0 | 14.1 | |
| * 17 | 2 | 1500. | 1045. | 0. | 3928. | 1045. | 0. | 3795. | 4000. | 0. | 0. | 0. | .95 | 56. | 33.8 | D | 22.5 | 11.6 | |
| * 18 | 2 | 1500. | 0. | 1270. | 3928. | 0. | 1227. | 3795. | 4000. | 0. | 0. | 0. | .95 | 56. | 33.8 | D | 22.5 | 11.6 | |
| * 19 | 2 | 12000. | 0. | 0. | 2658. | 0. | 0. | 2568. | 4000. | 0. | 0. | 0. | .64 | 65. | 19.8 | C | 19.0 | 14.1 | |
| * 20 | 3 | 500. | 0. | 2658. | 2658. | 0. | 2568. | 2568. | 6000. | 0. | 0. | 0. | .43 | 65. | 13.2 | B | 19.0 | 14.1 | |

TOTAL 137309. = 26.0 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 57. 28.7 19.7 13.6

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 992. VEH-HRS | 1209. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 992. VEH-HRS | 1209. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 56238. VEH-MI. | 69443. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 57. MPH. | 59. MPH. |
| AVERAGE DENSITY = | 29. VPMPL | 27. VPMPL |
| TOTAL FUEL = | 2851. GALLONS | 8405. GALLONS |
| TOTAL EMISSIONS = | 762. KI LOGRAMS | 2244. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.08 | 2 | 16.67 | 3 | 11.23 | 4 | 17.84 | 5 | 19.85 |
| 6 | 14.20 | 7 | 12.31 | 8 | 5.12 | 9 | 19.09 | 10 | 2.35 |
| 11 | 1.88 | 12 | 2.35 | 13 | 1.08 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 1.30 | 18 | 1.30 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 126.6 VEH-HRS ***** AVERAGE DELAY = 2.02 MIN/VEH *****

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|-------|-----------------------|-------|-------|-------|-------|-------|-------|---|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 18.00 | 0.00 | 24.92 | 26.23 | 26.29 | 26.47 | 27.08 | 29.26 | |
| * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| * 3 * | 0.00 | 0.00 | 3.51 | 4.82 | 4.88 | 5.06 | 5.67 | 7.86 | |
| * 4 * | 0.00 | 0.00 | 1.54 | 2.85 | 2.91 | 3.09 | 3.70 | 5.89 | |
| * 5 * | 0.00 | 0.00 | 0.21 | 1.52 | 1.58 | 1.76 | 2.37 | 4.55 | |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.32 | 0.37 | 0.56 | 1.16 | 3.35 | |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 | 0.78 | 2.97 | |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.61 | 2.79 | |

 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *
 * SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMI SS *
 * SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMP LEVEL MPG GS/VM *

| | | | | | | | | | | | | | | | | | | | |
|------|---|--------|-------|-------|-------|-------|-------|-------|-------|----|----|-------|------|-----|------|-------|------|------|------|
| * 1 | 3 | 500. | 4720. | 0. | 4720. | 4720. | 0. | 4720. | 6000. | 0. | 0. | 0. | .79 | 63. | 24.8 | C | 19.7 | 13.5 | |
| * 2 | 3 | 99999. | 0. | 1227. | 4720. | 0. | 1227. | 4720. | 6000. | 0. | 0. | 0. | .79 | 63. | 24.8 | C | 19.7 | 13.5 | |
| * 3 | 2 | 11000. | 0. | 0. | 3493. | 0. | 0. | 3354. | 4000. | 0. | * | 3948. | 139. | .84 | 37. | 45.8 | F | 20.2 | 13.6 |
| * 4 | 2 | 1500. | 19. | 0. | 3512. | 19. | 0. | 3373. | 4000. | 0. | ** | 1500. | 139. | .84 | 17. | 100.8 | F | 16.8 | 18.0 |
| * 5 | 2 | 1400. | 0. | 0. | 3512. | 0. | 0. | 3373. | 4000. | 0. | ** | 1400. | 139. | .84 | 17. | 100.8 | F | 16.8 | 18.0 |
| * 6 | 2 | 1500. | 400. | 0. | 3912. | 400. | 0. | 3773. | 4000. | 0. | ** | 1500. | 139. | .94 | 24. | 79.0 | F | 19.5 | 14.6 |
| * 7 | 2 | 1300. | 0. | 0. | 3912. | 0. | 0. | 3773. | 4000. | 0. | ** | 1300. | 139. | .94 | 24. | 79.0 | F | 19.5 | 14.6 |
| * 8 | 3 | 500. | 1227. | 1130. | 5139. | 1227. | 1128. | 5000. | 5130. | 0. | ** | 500. | 130. | .97 | 27. | 61.7 | F | 20.4 | 13.6 |
| * 9 | 2 | 2300. | 0. | 0. | 4009. | 0. | 0. | 3872. | 4000. | 0. | ** | 2300. | 128. | .97 | 26. | 73.6 | F | 20.2 | 13.8 |
| * 10 | 3 | 250. | 194. | 0. | 4203. | 194. | 0. | 4066. | 4250. | 0. | ** | 250. | 128. | .96 | 25. | 53.9 | F | 19.9 | 14.1 |
| * 11 | 3 | 200. | 0. | 0. | 4203. | 0. | 0. | 4066. | 4250. | 0. | ** | 200. | 128. | .96 | 25. | 53.9 | F | 19.9 | 14.1 |
| * 12 | 3 | 250. | 0. | 1320. | 4203. | 0. | 1317. | 4066. | 4250. | 0. | ** | 250. | 128. | .96 | 25. | 53.9 | F | 19.9 | 14.1 |
| * 13 | 2 | 50. | 0. | 0. | 2883. | 0. | 349. | 2749. | 4000. | 0. | ** | 50. | 128. | .69 | 10. | 134.8 | F | 13.1 | 22.8 |
| * 14 | 2 | 50. | 0. | 0. | 2533. | 0. | 0. | 2400. | 2400. | 0. | 0. | 0. | 1.00 | 65. | 18.5 | E | 19.0 | 14.1 | |
| * 15 | 2 | 1000. | 350. | 0. | 2883. | 350. | 0. | 2750. | 4000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 19.0 | 14.1 | |
| * 16 | 2 | 10. | 0. | 0. | 2883. | 0. | 0. | 2750. | 4000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 19.0 | 14.1 | |
| * 17 | 2 | 1500. | 1045. | 0. | 3928. | 1045. | 0. | 3795. | 4000. | 0. | 0. | 0. | .95 | 56. | 33.8 | D | 22.5 | 11.6 | |
| * 18 | 2 | 1500. | 0. | 1270. | 3928. | 0. | 1227. | 3795. | 4000. | 0. | 0. | 0. | .95 | 56. | 33.8 | D | 22.5 | 11.6 | |
| * 19 | 2 | 12000. | 0. | 0. | 2658. | 0. | 0. | 2568. | 4000. | 0. | 0. | 0. | .64 | 65. | 19.8 | C | 19.0 | 14.1 | |
| * 20 | 3 | 500. | 0. | 2658. | 2658. | 0. | 2568. | 2568. | 6000. | 0. | 0. | 0. | .43 | 65. | 13.2 | B | 19.0 | 14.1 | |

 *
 * TOTAL 137309. = 26.0 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 55. 30.0 19.6 13.6 *

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|-----------------------------|--------------------|-----------------|-------------------|------------------|
| FREWAY TRAVEL TIME = | 1026. VEH-HRS | 1244. PASS-HRS | 3834. VEH-HRS | 4684. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1026. VEH-HRS | 1244. PASS-HRS | 3834. VEH-HRS | 4684. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 56205. VEH-MI. | 69410. PASS-MI. | 221321. VEH-MI. | 273247. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 55. MPH. | | 58. MPH. | |
| AVERAGE DENSITY = | 30. VPMP | | 28. VPMP | |
| TOTAL FUEL = | 2861. GALLONS | | 11266. GALLONS | |
| TOTAL EMISSIONS = | 767. KILOGRAMS | | 3011. KILOGRAMS | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.08 | 2 | 16.67 | 3 | 42.96 | 4 | 21.27 | 5 | 19.85 |
| 6 | 14.20 | 7 | 12.31 | 8 | 5.12 | 9 | 19.09 | 10 | 2.35 |
| 11 | 1.88 | 12 | 2.35 | 13 | 1.08 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 1.30 | 18 | 1.30 | 19 | 0.00 | 20 | 0.00 |

SR-237_WB_AM_NP_MOD_2018_PL.txt

***** TOTAL DELAY = 161.8 VEH-HRS ***** AVERAGE DELAY = 2.65 MIN/VEH *****

| | | | | | | | |
|----------|----------|----------|---------------|--------------|--------------|------------|----------|
| FFFFFFFF | RRRRRRRR | EEEEEEEE | QQQQQQ | 1111 | 222222 | PPPPPPPP | LLL |
| FFFFFFFF | RRRRRRRR | EEEEEEEE | O*A. D. MAY*O | 111111 | 222 222 | PPPPPPPP | LLL |
| FFF | RRR | RRR | EEE | QQQQQ | QQQQQ | 1111 | 222 222 |
| FFF | RRR | RRR | EEE | QQQQ | QQQQ | 1111 | 222 |
| FFFFFFFF | RRRRRRRR | EEEEEEEE | QQQQ | QQQQ | 1111 | 222 | PPPPPPPP |
| FFFFFFFF | RRRRRRRR | EEEEEEEE | QQQQ | QQQQ | 1111 | 2222 | PPPPPPPP |
| FFF | RRR | RRR | EEE | QQO | QQO | 1111 | 2222 |
| FFF | RRR | RRR | EEE | O*UC* | QQQQ | 1111 | 222 |
| FFF | RRR | RRR | EEEEEEEE | O*REGENTS*OQ | 1111 | 222 | PPP |
| FFF | RRR | RRR | EEEEEEEE | O*1988*Q | QQO 11111111 | 2222222222 | PPP |

FREQ12PL

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 3 AND 7 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 2.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 30
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65 MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

ON-RAMP CAPACITY LIMITS

| | | | | | | | |
|------|-------|------|------|-------|------|------|------|
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| 6000 | ***** | 1500 | 1500 | ***** | 2000 | 1500 | 1500 |

OFF-RAMP CAPACITY LIMITS

| | | | | | | | |
|-------|-------|------|------|------|------|------|------|
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| ***** | ***** | 2000 | 2000 | 1500 | 1500 | 1500 | 6000 |

ON-RAMP 1 IS THE MAINLINE ORIGIN
OFF-RAMP 8 IS THE MAINLINE DESTINATION

***** ON-RAMPS 2 AND 5 ARE SYNTHETIC ORIGINS USED TO ENTER AND LEAVE THE PL LANE(S)
***** OFF-RAMPS 1 AND 2 ARE SYNTHETIC DESTINATIONS USED TO ENTER AND LEAVE THE PL LANE(S)

INPUT HAS BEEN COMPLETED

```
*****  
*****  
**  
**  
** FREEWAY AND ARTERIAL DESIGN FEATURES **  
**  
*****  
*****  
** SUB NO. SSEC SSEC DESIGN ORG TRK SSEC PCT PCT DES SPECIAL FF. SPD. CAP. ART GRADE SUBSECTION LOCATION **  
** SEC LNS CAP LENGTH SPEED DES FAC GRAD TRK TRUCKS RAMP ALT. RTE ALT. RTE TYPE ALT. RTE **  
**  
** 1 **  
** 2 **  
** 3 1 1650. 11000. 62 0 0.95 0.0 0 100 NO 0.0 0.0 GOOD 0.0 HOV Dummy **  
** 4 1 1650. 1500. 62 0 0.95 0.0 0 100 YES 0.0 0.0 GOOD 0.0 Lawrence On-ramp **  
** 5 1 1650. 1400. 62 0 0.95 0.0 0 100 NO 0.0 0.0 GOOD 0.0 Lawrence to Crossman **  
** 6 1 1650. 1500. 62 0 0.95 0.0 0 100 YES 0.0 0.0 GOOD 0.0 Crossman On-Ramp **  
** 7 1 1650. 1300. 62 0 0.95 0.0 0 100 NO 0.0 0.0 GOOD 0.0 Crossman / Mathilda **
```


** 8 **
** 9 **
** 10 **
** 11 **
** 12 **
** 13 **
** 14 **
** 15 **
** 16 **
** 17 **
** 18 **
** 19 **
** 20 **

** FREEWAY TRAVEL TIME (MINUTES) **

Table with columns: ORIGIN DOWN, DESTINATIONS ACROSS (1-8). Rows 1-8 showing travel times for each destination.

TIME SLICE FREEWAY PERFORMANCE TABLE

Table with columns: SUB NO., SSEC, O-D DATA, DEMANDS, ADJUSTED VOLUMES, SSEC, WEAVE, CONGEST, STORAGE, V/C, SPEED, DENSITY, LOS, FUEL, EMISSIONS. Rows 1-19 showing performance metrics.

* 20 *

 * TOTAL 16700. = 3.2 MILES MAX(V/C) = 0.73 LOWEST LOS = C AVG = 62. 19.3 21.6 12.8 *

| | | | | |
|------------------------------|--------------------|----------------|-------------------|----------------|
| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
| FREEWAY TRAVEL TIME = | 31. VEH-HRS | 61. PASS-HRS | 31. VEH-HRS | 61. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 31. VEH-HRS | 61. PASS-HRS | 31. VEH-HRS | 61. PASS-HRS |
| TOTAL FRWAY TRAV DI STANCE = | 1895. VEH-MI. | 3790. PASS-MI. | 1895. VEH-MI. | 3790. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | | 62. MPH. | |
| AVERAGE DENSITY = | 19. VPMP. | | 19. VPMP. | |
| TOTAL FUEL = | 88. GALLONS | | 88. GALLONS | |
| TOTAL EMISSIONS = | 24. KILOGRAMS | | 24. KILOGRAMS | |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 15:54 PAGE 6
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 1 OF 4

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.93 | 4 | 0.13 | 5 | 0.12 |
| 6 | 0.13 | 7 | 0.11 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 1.4 VEH-HRS ***** AVERAGE DELAY = 0.07 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 15:54 PAGE 7
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 4

 ** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|---|-----------------------|------|------|------|------|------|------|------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| + | * | | | | | | | | |
| + | * | | | | | | | | |
| + | * | 1 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * | 2 | 0.00 | 3.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * | 3 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * | 4 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * | 5 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * | 6 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * | 7 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * | 8 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * | | | | | | | | |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 15:54 PAGE 8
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 4

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|-----------|--------|------------|-----------|------------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * ORG | * DES | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 1 | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | |
| * 3 | 1 | 11000. | 1198. | 0. | 1198. | 1198. | 0. | 1198. | 1650. | 0. | 0. | .73 | 62. | 19.3 |
| * 4 | 1 | 1500. | 0. | 0. | 1198. | 0. | 0. | 1198. | 1650. | 0. | 0. | .73 | 62. | 19.3 |
| * 5 | 1 | 1400. | 0. | 0. | 1198. | 0. | 0. | 1198. | 1650. | 0. | 0. | .73 | 62. | 19.3 |
| * 6 | 1 | 1500. | 0. | 0. | 1198. | 0. | 0. | 1198. | 1650. | 0. | 0. | .73 | 62. | 19.3 |
| * 7 | 1 | 1300. | 0. | 1198. | 1198. | 0. | 1198. | 1198. | 1650. | 0. | 0. | .73 | 62. | 19.3 |
| * 8 | | | | | | | | | | | | | | |
| * 9 | | | | | | | | | | | | | | |

```

*10
* 11
* 12
* 13
* 14
* 15
* 16
* 17
* 18
* 19
* 20
*****
*
* TOTAL 16700. = 3.2 MILES MAX(V/C) = 0.73 LOWEST LOS = C AVG = 62. 19.3 21.6 12.8
*
*****

```

```

CURRENT TIME SLICE CUMULATIVE VALUES
FREEWAY TRAVEL TIME = 31. VEH-HRS 61. PASS-HRS 61. VEH-HRS 122. PASS-HRS
FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 31. VEH-HRS 61. PASS-HRS 61. VEH-HRS 122. PASS-HRS
TOTAL FRWAY TRAV DISTANCE = 1895. VEH-MI. 3790. PASS-MI. 3790. VEH-MI. 7580. PASS-MI.
AVERAGE SYSTEM SPEED = 62. MPH. 62. MPH.
AVERAGE DENSITY = 19. VPMP. 19. VPMP.
TOTAL FUEL = 88. GALLONS 176. GALLONS
TOTAL EMISSIONS = 24. KILOGRAMS 48. KILOGRAMS

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1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 15:54 PAGE 9
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 4

```

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
1 0.00 2 0.00 3 0.93 4 0.13 5 0.12
6 0.13 7 0.11 8 0.00 9 0.00 10 0.00
11 0.00 12 0.00 13 0.00 14 0.00 15 0.00
16 0.00 17 0.00 18 0.00 19 0.00 20 0.00
***** TOTAL DELAY = 1.4 VEH-HRS ***** AVERAGE DELAY = 0.07 MIN/VEH *****

```

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 15:54 PAGE 10
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 3 OF 4

```

*****
**
** FREEWAY TRAVEL TIME (MINUTES) **
**
*****

```

```

*****
* ORIGINS DESTINATIONS ACROSS *
* DOWN 1 2 3 4 5 6 7 8 *
+
* * * * *
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 2 * 0.00 3.06 0.00 0.00 0.00 0.00 0.00 0.00
+
* 3 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 4 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 5 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 8 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* *
*****

```

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 15:54 PAGE 11
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 3 OF 4

```

*****
*
* TIME SLICE FREEWAY PERFORMANCE TABLE
*
*****
* SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMISSIONS *
* SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMP LEVEL MPG GS/VM *
*****

```

```

*
* 1
* 2
* 3 1 11000. 1227. 0. 1227. 1227. 0. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8
* 4 1 1500. 0. 0. 1227. 0. 0. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8
* 5 1 1400. 0. 0. 1227. 0. 0. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8
* 6 1 1500. 0. 0. 1227. 0. 0. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8
* 7 1 1300. 0. 1227. 1227. 0. 1227. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8
* 8
* 9
* 10
* 11
* 12
* 13
* 14
* 15
* 16
* 17
* 18
* 19
* 20
*****
*
* TOTAL 16700. = 3.2 MILES MAX(V/C) = 0.74 LOWEST LOS = C AVG = 62. 19.8 21.6 12.8
*
*****

```

```

CURRENT TIME SLICE CUMULATIVE VALUES
FREEWAY TRAVEL TIME = 31. VEH-HRS 63. PASS-HRS 92. VEH-HRS 185. PASS-HRS
FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 31. VEH-HRS 63. PASS-HRS 92. VEH-HRS 185. PASS-HRS
TOTAL FRWAY TRAV DISTANCE = 1941. VEH-MI. 3881. PASS-MI. 5731. VEH-MI. 11462. PASS-MI.
AVERAGE SYSTEM SPEED = 62. MPH. 62. MPH.
AVERAGE DENSITY = 20. VPML 19. VPML
TOTAL FUEL = 90. GALLONS 266. GALLONS
TOTAL EMISSIONS = 25. KILOGRAMS 73. KILOGRAMS

```

```

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
1 0.00 2 0.00 3 0.95 4 0.13 5 0.12
6 0.13 7 0.11 8 0.00 9 0.00 10 0.00
11 0.00 12 0.00 13 0.00 14 0.00 15 0.00
16 0.00 17 0.00 18 0.00 19 0.00 20 0.00
***** TOTAL DELAY = 1.4 VEH-HRS ***** AVERAGE DELAY = 0.07 MIN/VEH *****

```

```

*****
**
** FREeway TRAVEL TIME (MINUTES) **
**
*****

```

```

*****
* ORIGINS DESTINATIONS ACROSS *
* DOWN 1 2 3 4 5 6 7 8 *
+
* * * * *
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 2 * 0.00 3.06 0.00 0.00 0.00 0.00 0.00 0.00
+
* 3 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 4 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 5 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 8 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* *
*****

```

 *
 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *
 *
 *
 * SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMISS *
 * SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMP L LEVEL MPG GS/VM *
 *
 * 1 *
 * 2 *
 * 3 1 11000. 1227. 0. 1227. 1227. 0. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8 *
 * 4 1 1500. 0. 0. 1227. 0. 0. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8 *
 * 5 1 1400. 0. 0. 1227. 0. 0. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8 *
 * 6 1 1500. 0. 0. 1227. 0. 0. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8 *
 * 7 1 1300. 0. 1227. 1227. 0. 1227. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8 *
 * 8 *
 * 9 *
 * 10 *
 * 11 *
 * 12 *
 * 13 *
 * 14 *
 * 15 *
 * 16 *
 * 17 *
 * 18 *
 * 19 *
 * 20 *
 *
 *
 * TOTAL 16700. = 3.2 MILES MAX(V/C) = 0.74 LOWEST LOS = C AVG = 62. 19.8 21.6 12.8 *
 *

| | | |
|-----------------------------|------------------------------|-------------------------------|
| | CURRENT TIME SLICE | CUMULATIVE VALUES |
| FREEWAY TRAVEL TIME = | 31. VEH-HRS 63. PASS-HRS | 124. VEH-HRS 247. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 31. VEH-HRS 63. PASS-HRS | 124. VEH-HRS 247. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 1941. VEH-MI. 3881. PASS-MI. | 7672. VEH-MI. 15343. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 62. MPH. |
| AVERAGE DENSITY = | 20. VPMP L | 20. VPMP L |
| TOTAL FUEL = | 90. GALLONS | 356. GALLONS |
| TOTAL EMISSIONS = | 25. KI LOGRAMS | 98. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| | | | | | | | | | |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
| 1 | 0.00 | 2 | 0.00 | 3 | 0.95 | 4 | 0.13 | 5 | 0.12 |
| 6 | 0.13 | 7 | 0.11 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 1.4 VEH-HRS ***** AVERAGE DELAY = 0.07 MIN/VEH *****

 **
 ** FREeway TRAVEL TIME (MINUTES) **
 **

| | | | | | | | | | |
|---|---------|---------------------|------|-------|-------|-------|-------|-------|-------|
| | ORIGINS | DESTINATIONS ACROSS | | | | | | | |
| | DOWN | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| + | * | ***** | | | | | | | |
| + | * | ***** | | | | | | | |
| + | * 1 * | 17.88 | 0.00 | 21.44 | 22.69 | 22.76 | 22.95 | 23.48 | 25.67 |
| + | * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 3 * | 0.00 | 0.00 | 1.46 | 2.71 | 2.79 | 2.97 | 3.50 | 5.69 |
| + | * 4 * | 0.00 | 0.00 | 0.91 | 2.16 | 2.23 | 2.41 | 2.95 | 5.13 |
| + | * 5 * | 0.00 | 0.00 | 0.18 | 1.43 | 1.50 | 1.68 | 2.22 | 4.40 |
| + | * 6 * | 0.00 | 0.00 | 0.00 | 0.33 | 0.40 | 0.59 | 1.12 | 3.30 |
| + | * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 | 0.71 | 2.89 |
| + | * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.53 | 2.72 |
| + | * | ***** | | | | | | | |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB * SEC | * NO. * LNS | * SSEC * LENGTH | * O-D DATA * ORG DES SSEC | * DEMANDS * SSEC | * ADJUSTED * ORG DES SSEC | * VOLUMES * SSEC | * SSEC * CAP. | * WEAVE * EFF | * CONGEST * LENGTH | * STORAGE * RATE | * V/C * RATIO | * SPEED * MPH | * DENSITY * VPMP | * LOS * LEVEL | * FUEL * MPG | * EMISSIONS * GS/VM |
|----------------|----------------|--------------------|------------------------------|---------------------|------------------------------|---------------------|------------------|------------------|-----------------------|---------------------|------------------|------------------|---------------------|------------------|-----------------|------------------------|
| * 1 | 3 | 500. | 4609. | 0. 4609. | 4609. | 0. 4609. | 6000. | 0. | 0. | 0. | .77 | 64. | 24.1 | C | 19.5 | 13.7 |
| * 2 | 3 | 9999. | 0. 1198. | 0. 4609. | 0. 1198. | 0. 4609. | 6000. | 0. | 0. | 0. | .77 | 64. | 24.1 | C | 19.5 | 13.7 |
| * 3 | 2 | 11000. | 0. 0. | 0. 3411. | 0. 0. | 0. 3411. | 4000. | 0. | 0. | 0. | .85 | 60. | 28.6 | D | 21.5 | 12.3 |
| * 4 | 2 | 1500. | 20. 0. | 0. 3431. | 20. 0. | 0. 3431. | 4000. | 0. | 0. | 0. | .86 | 60. | 28.8 | D | 21.5 | 12.3 |
| * 5 | 2 | 1400. | 0. 0. | 0. 3431. | 0. 0. | 0. 3431. | 4000. | 0. | 0. | 0. | .86 | 60. | 28.8 | D | 21.5 | 12.3 |
| * 6 | 2 | 1500. | 290. 0. | 0. 3721. | 290. 0. | 0. 3492. | 4000. | 0. | * 737. | 229. | .87 | 53. | 33.2 | F | 22.2 | 11.8 |
| * 7 | 2 | 1300. | 0. 0. | 0. 3721. | 0. 0. | 0. 3492. | 4000. | 0. | ** 1300. | 229. | .87 | 36. | 48.0 | F | 20.9 | 13.1 |
| * 8 | 3 | 500. | 1198. 950. | 0. 4919. | 1198. 950. | 0. 4690. | 5130. | 0. | ** 500. | 229. | .91 | 32. | 48.6 | F | 20.7 | 13.4 |
| * 9 | 2 | 2300. | 0. 0. | 0. 3969. | 0. 0. | 0. 3740. | 4000. | 0. | ** 2300. | 229. | .94 | 28. | 66.0 | F | 20.4 | 13.7 |
| * 10 | 3 | 250. | 210. 0. | 0. 4179. | 210. 0. | 0. 3950. | 4250. | 0. | ** 250. | 229. | .93 | 25. | 53.1 | F | 19.1 | 15.0 |
| * 11 | 3 | 200. | 0. 0. | 0. 4179. | 0. 0. | 0. 3950. | 4250. | 0. | ** 200. | 229. | .93 | 24. | 54.7 | F | 19.1 | 15.0 |
| * 12 | 3 | 250. | 0. 1550. | 0. 4179. | 0. 1550. | 0. 3950. | 4250. | 0. | ** 250. | 229. | .93 | 23. | 56.3 | F | 19.1 | 15.0 |
| * 13 | 2 | 50. | 0. 0. | 0. 2629. | 0. 0. | 0. 2400. | 4000. | 0. | ** 50. | 229. | .60 | 8. | 152.2 | F | 10.5 | 25.4 |
| * 14 | 2 | 50. | 0. 0. | 0. 2629. | 0. 0. | 0. 2400. | 2400. | 0. | 0. | 0. | 1.00 | 65. | 18.5 | E | 19.0 | 14.1 |
| * 15 | 2 | 1000. | 0. 0. | 0. 2629. | 0. 0. | 0. 2400. | 4000. | 0. | 0. | 0. | .60 | 65. | 18.5 | C | 19.0 | 14.1 |
| * 16 | 2 | 10. | 0. 0. | 0. 2629. | 0. 0. | 0. 2400. | 4000. | 0. | 0. | 0. | .60 | 65. | 18.5 | C | 19.0 | 14.1 |
| * 17 | 2 | 1500. | 608. 0. | 0. 3237. | 608. 0. | 0. 3008. | 4000. | 0. | 0. | 0. | .75 | 64. | 23.4 | C | 19.3 | 13.8 |
| * 18 | 2 | 1500. | 0. 789. | 0. 3237. | 0. 789. | 0. 3008. | 4000. | 0. | 0. | 0. | .75 | 64. | 23.4 | C | 19.3 | 13.8 |
| * 19 | 2 | 12000. | 0. 0. | 0. 2448. | 0. 0. | 0. 2275. | 4000. | 0. | 0. | 0. | .57 | 65. | 17.5 | B | 19.0 | 14.1 |
| * 20 | 3 | 500. | 0. 2448. | 0. 2448. | 0. 2275. | 0. 2275. | 6000. | 0. | 0. | 0. | .38 | 65. | 11.7 | B | 19.0 | 14.1 |

TOTAL 137309. = 26.0 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 61. 25.2 19.6 13.6

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 892. VEH-HRS | 1099. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 892. VEH-HRS | 1099. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 54457. VEH-MI. | 67215. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 61. MPH. | 61. MPH. |
| AVERAGE DENSITY = | 25. VPMP | 25. VPMP |
| TOTAL FUEL = | 2773. GALLONS | 2773. GALLONS |
| TOTAL EMISSIONS = | 739. KILOGRAMS | 739. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.06 | 2 | 11.98 | 3 | 4.88 | 4 | 0.69 | 5 | 0.65 |
| 6 | 1.92 | 7 | 5.46 | 8 | 3.57 | 9 | 16.51 | 10 | 2.35 |
| 11 | 1.97 | 12 | 2.57 | 13 | 1.27 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.09 | 18 | 0.09 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 54.0 VEH-HRS ***** AVERAGE DELAY = 0.84 MIN/VEH *****

 ** FREeway TRAVEL TIME (MINUTES) **

| * ORIGINS * DOWN | * DESTINATIONS ACROSS * | | | | | | | |
|---------------------|-------------------------|------|-------|-------|-------|-------|-------|-------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 17.88 | 0.00 | 23.25 | 24.73 | 24.80 | 24.99 | 25.52 | 27.71 |
| * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 3 * | 0.00 | 0.00 | 3.27 | 4.75 | 4.82 | 5.01 | 5.54 | 7.72 |

| | | | | | | | | |
|-------|------|------|------|------|------|------|------|------|
| * 4 * | 0.00 | 0.00 | 1.96 | 3.44 | 3.51 | 3.70 | 4.23 | 6.41 |
| * 5 * | 0.00 | 0.00 | 0.27 | 1.75 | 1.82 | 2.00 | 2.54 | 4.72 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.35 | 0.42 | 0.61 | 1.14 | 3.33 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 | 0.71 | 2.89 |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.53 | 2.72 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | | |
|-----------|--------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|-------|----------|-----------|---------|--------|-------------|---------|-------|---------|------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | |
| * 1 | 3 | 500. | 4609. | 0. | 4609. | 4609. | 0. | 4609. | 6000. | 0. | 0. | 0. | .77 | 64. | 24.1 | C | 19.5 | 13.7 | |
| * 2 | 3 | 99999. | 0. | 1198. | 4609. | 0. | 1198. | 4609. | 6000. | 0. | 0. | 0. | .77 | 64. | 24.1 | C | 19.5 | 13.7 | |
| * 3 | 2 | 11000. | 0. | 0. | 3411. | 0. | 0. | 3182. | 4000. | 0. | * | 238. | .229. | .80 | 60. | 26.7 | F | 21.5 | 12.3 |
| * 4 | 2 | 1500. | 20. | 0. | 3431. | 20. | 0. | 3202. | 4000. | 0. | ** | 1500. | .229. | .80 | 33. | 48.0 | F | 19.7 | 14.1 |
| * 5 | 2 | 1400. | 0. | 0. | 3431. | 0. | 0. | 3202. | 4000. | 0. | ** | 1400. | .229. | .80 | 20. | 80.3 | F | 17.4 | 16.8 |
| * 6 | 2 | 1500. | 290. | 0. | 3721. | 290. | 0. | 3492. | 4000. | 0. | ** | 1500. | .229. | .87 | 19. | 91.7 | F | 17.7 | 16.7 |
| * 7 | 2 | 1300. | 0. | 0. | 3721. | 0. | 0. | 3492. | 4000. | 0. | ** | 1300. | .229. | .87 | 19. | 94.4 | F | 17.5 | 17.0 |
| * 8 | 3 | 500. | 1198. | 950. | 4919. | 1198. | 950. | 4690. | 5130. | 0. | ** | 500. | .229. | .91 | 21. | 73.0 | F | 18.7 | 15.6 |
| * 9 | 2 | 2300. | 0. | 0. | 3969. | 0. | 0. | 3740. | 4000. | 0. | ** | 2300. | .229. | .94 | 23. | 80.8 | F | 19.2 | 14.9 |
| * 10 | 3 | 250. | 210. | 0. | 4179. | 210. | 0. | 3950. | 4250. | 0. | ** | 250. | .229. | .93 | 23. | 58.1 | F | 19.1 | 15.1 |
| * 11 | 3 | 200. | 0. | 0. | 4179. | 0. | 0. | 3950. | 4250. | 0. | ** | 200. | .229. | .93 | 23. | 58.1 | F | 19.1 | 15.1 |
| * 12 | 3 | 250. | 0. | 1550. | 4179. | 0. | 1550. | 3950. | 4250. | 0. | ** | 250. | .229. | .93 | 23. | 58.1 | F | 19.1 | 15.1 |
| * 13 | 2 | 50. | 0. | 0. | 2629. | 0. | 0. | 2400. | 4000. | 0. | ** | 50. | .229. | .60 | 8. | 153.8 | F | 10.4 | 25.5 |
| * 14 | 2 | 50. | 0. | 0. | 2629. | 0. | 0. | 2400. | 2400. | 0. | 0. | 0. | 1.00 | 65. | 18.5 | E | 19.0 | 14.1 | |
| * 15 | 2 | 1000. | 0. | 0. | 2629. | 0. | 0. | 2400. | 4000. | 0. | 0. | 0. | .60 | 65. | 18.5 | C | 19.0 | 14.1 | |
| * 16 | 2 | 10. | 0. | 0. | 2629. | 0. | 0. | 2400. | 4000. | 0. | 0. | 0. | .60 | 65. | 18.5 | C | 19.0 | 14.1 | |
| * 17 | 2 | 1500. | 608. | 0. | 3237. | 608. | 0. | 3008. | 4000. | 0. | 0. | 0. | .75 | 64. | 23.4 | C | 19.3 | 13.8 | |
| * 18 | 2 | 1500. | 0. | 789. | 3237. | 0. | 733. | 3008. | 4000. | 0. | 0. | 0. | .75 | 64. | 23.4 | C | 19.3 | 13.8 | |
| * 19 | 2 | 12000. | 0. | 0. | 2448. | 0. | 0. | 2275. | 4000. | 0. | 0. | 0. | .57 | 65. | 17.5 | B | 19.0 | 14.1 | |
| * 20 | 3 | 500. | 0. | 2448. | 2448. | 0. | 2275. | 2275. | 6000. | 0. | 0. | 0. | .38 | 65. | 11.7 | B | 19.0 | 14.1 | |

TOTAL 137309. = 26.0 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 57. 27.2 19.5 13.7

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 949. VEH-HRS | 1841. VEH-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 949. VEH-HRS | 1841. VEH-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 54355. VEH-MI. | 67106. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 57. MPH | 59. MPH |
| AVERAGE DENSITY = | 27. VPMP | 26. VPMP |
| TOTAL FUEL = | 2788. GALLONS | 5561. GALLONS |
| TOTAL EMISSIONS = | 746. KILOGRAMS | 1485. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.06 | 2 | 11.98 | 3 | 5.01 | 4 | 6.99 | 5 | 15.12 |
| 6 | 18.47 | 7 | 16.62 | 8 | 6.95 | 9 | 22.68 | 10 | 2.69 |
| 11 | 2.15 | 12 | 2.69 | 13 | 1.28 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.09 | 18 | 0.09 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 112.9 VEH-HRS ***** AVERAGE DELAY = 1.87 MIN/VEH *****

 ** FREWAY TRAVEL TIME (MINUTES) **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN *
 * 1 2 3 4 5 6 7 8 *

Table with 10 columns showing simulation results for 8 different lanes, including values for delay, volume, and other metrics.

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 15:54 PAGE 23
UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF NON-PRIORITY LANES
TIME SLICE 3 OF 4

TIME SLICE FREEWAY PERFORMANCE TABLE

Table with 16 columns: SUB NO., SSEC, O-D DATA DEMANDS, ADJUSTED VOLUMES, SSEC, WEAVE, CONGEST, STORAGE, V/C, SPEED, DENSITY, LOS, FUEL, EMISSIONS. Contains detailed performance data for 20 different freeway sections.

TOTAL 137309. = 26.0 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 55. 29.8 19.6 13.6

Summary table with 4 columns: FREeway TRAVEL TIME, FREeway MERGE DELAY, ON-RAMP DELAY, OFF-RAMP DELAY, TOTAL SYSTEM TRAVEL TIME, TOTAL FRWAY TRAV DISTANCE, AVERAGE SYSTEM SPEED, AVERAGE DENSITY, TOTAL FUEL, TOTAL EMISSIONS.

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 15:54 PAGE 24
UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF NON-PRIORITY LANES
TIME SLICE 3 OF 4

Table with 10 columns showing MAINTENANCE DELAY (VEH-HRS) and DESIRED SPEED = 65.0. Includes subsection delays and total delay.

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 15:54 PAGE 25
UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF NON-PRIORITY LANES
TIME SLICE 4 OF 4

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|-------|-----------------------|-------|-------|-------|-------|-------|-------|---|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 18.00 | 0.00 | 26.58 | 27.95 | 28.00 | 28.19 | 28.79 | 30.98 | |
| * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| * 3 * | 0.00 | 0.00 | 3.69 | 5.06 | 5.12 | 5.30 | 5.91 | 8.09 | |
| * 4 * | 0.00 | 0.00 | 1.63 | 3.00 | 3.05 | 3.24 | 3.84 | 6.03 | |
| * 5 * | 0.00 | 0.00 | 0.22 | 1.59 | 1.65 | 1.83 | 2.44 | 4.62 | |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.32 | 0.37 | 0.56 | 1.17 | 3.35 | |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 | 0.78 | 2.97 | |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.61 | 2.79 | |

 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | |
|-----------|--------|------------|-----------|------------|----------------|--------|---------|-----------|-----------|---------|----------|-----------|---------|--------|-------------|---|------|------|
| * SEC | * LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VP/MPH | * LEVEL | * MPG | * GS/VM | | | |
| * 1 | 3 | 500. | 4720. | 0. | 4720. | 4720. | 0. | 4720. | 6000. | 0. | 0. | 0. | .79 | 63. | 24.8 | C | 19.7 | 13.5 |
| * 2 | 3 | 99999. | 0. | 1227. | 4720. | 0. | 1227. | 4720. | 6000. | 0. | 0. | 0. | .79 | 63. | 24.8 | C | 19.7 | 13.5 |
| * 3 | 2 | 11000. | 0. | 0. | 3493. | 0. | 0. | 3297. | 4000. | 0. | * 7091. | 195. | .82 | 26. | 64.5 | F | 18.8 | 15.2 |
| * 4 | 2 | 1500. | 19. | 0. | 3512. | 19. | 0. | 3316. | 4000. | 0. | ** 1500. | 195. | .83 | 16. | 103.9 | F | 16.4 | 18.4 |
| * 5 | 2 | 1400. | 0. | 0. | 3512. | 0. | 0. | 3316. | 4000. | 0. | ** 1400. | 195. | .83 | 16. | 103.9 | F | 16.4 | 18.4 |
| * 6 | 2 | 1500. | 400. | 0. | 3912. | 400. | 0. | 3716. | 4000. | 0. | ** 1500. | 195. | .93 | 23. | 82.1 | F | 19.1 | 15.1 |
| * 7 | 2 | 1300. | 0. | 0. | 3912. | 0. | 0. | 3716. | 4000. | 0. | ** 1300. | 195. | .93 | 23. | 82.1 | F | 19.1 | 15.1 |
| * 8 | 3 | 500. | 1227. | 1130. | 5139. | 1227. | 1128. | 4944. | 5130. | 0. | ** 500. | 186. | .96 | 26. | 63.8 | F | 20.1 | 13.9 |
| * 9 | 2 | 2300. | 0. | 0. | 4009. | 0. | 0. | 3815. | 4000. | 0. | ** 2300. | 185. | .95 | 25. | 76.7 | F | 19.8 | 14.2 |
| * 10 | 3 | 250. | 241. | 0. | 4250. | 241. | 0. | 4056. | 4250. | 0. | ** 250. | 185. | .95 | 25. | 54.2 | F | 19.8 | 14.2 |
| * 11 | 3 | 200. | 0. | 0. | 4250. | 0. | 0. | 4056. | 4250. | 0. | ** 200. | 185. | .95 | 25. | 54.2 | F | 19.8 | 14.2 |
| * 12 | 3 | 250. | 0. | 1310. | 4250. | 0. | 1307. | 4056. | 4250. | 0. | ** 250. | 185. | .95 | 25. | 54.2 | F | 19.8 | 14.2 |
| * 13 | 2 | 50. | 0. | 0. | 2590. | 0. | 0. | 2400. | 2400. | 0. | ** 50. | 185. | .69 | 10. | 134.8 | F | 13.1 | 22.8 |
| * 14 | 2 | 50. | 0. | 0. | 2590. | 0. | 0. | 2400. | 2400. | 0. | 0. | 0. | 1.00 | 65. | 18.5 | E | 19.0 | 14.1 |
| * 15 | 2 | 1000. | 350. | 0. | 2940. | 350. | 0. | 2750. | 4000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 19.0 | 14.1 |
| * 16 | 2 | 10. | 0. | 0. | 2940. | 0. | 0. | 2750. | 4000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 19.0 | 14.1 |
| * 17 | 2 | 1500. | 1038. | 0. | 3978. | 1038. | 0. | 3788. | 4000. | 0. | 0. | 0. | .95 | 56. | 33.6 | D | 22.4 | 11.7 |
| * 18 | 2 | 1500. | 0. | 1270. | 3978. | 0. | 1209. | 3788. | 4000. | 0. | 0. | 0. | .95 | 56. | 33.6 | D | 22.4 | 11.7 |
| * 19 | 2 | 12000. | 0. | 0. | 2708. | 0. | 0. | 2579. | 4000. | 0. | 0. | 0. | .64 | 65. | 19.8 | C | 19.0 | 14.1 |
| * 20 | 3 | 500. | 0. | 2708. | 2708. | 0. | 2579. | 2579. | 6000. | 0. | 0. | 0. | .43 | 65. | 13.2 | B | 19.0 | 14.1 |

 *
 * TOTAL 137309. = 26.0 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 52. 31.7 19.5 13.8 *

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|-----------------------------------|-------------------------------------|
| FREWAY TRAVEL TIME = | 1072. VEH-HRS 1289. PASS-HRS | 3935. VEH-HRS 4788. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1072. VEH-HRS 1289. PASS-HRS | 3935. VEH-HRS 4788. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 56105. VEH-MI. 69308. PASS-MI. | 221085. VEH-MI. 273001. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 52. MPH. | 56. MPH. |
| AVERAGE DENSITY = | 32. VP/MPH | 28. VP/MPH |
| TOTAL FUEL = | 2873. GALLONS | 11293. GALLONS |
| TOTAL EMISSIONS = | 772. KILOGRAMS | 3024. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.08 | 2 | 16.67 | 3 | 83.99 | 4 | 22.27 | 5 | 20.79 |
| 6 | 15.21 | 7 | 13.18 | 8 | 5.46 | 9 | 20.63 | 10 | 2.38 |
| 11 | 1.90 | 12 | 2.38 | 13 | 1.08 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 1.27 | 18 | | 19 | 0.00 | 20 | 0.00 |

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***** TOTAL DELAY = 208.5 VEH-HRS ***** AVERAGE DELAY = 3.53 MIN/VEH *****


```

**
** 8
** 9
** 10
** 11
** 12
** 13
** 14
** 15
** 16
** 17
** 18
** 19
** 20
**
*****
*****

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```

*****
**
**          FREeway TRAVEL TIME (MINUTES)
**
*****

```

```

*****
* ORIGIN S                    DESTINATIONS ACROSS
* DOWN
*                    1       2       3       4       5       6       7       8
+
*
*
* 1 *    0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
* 2 *    0.00 3.06 0.00 0.00 0.00 0.00 0.00 0.00
* 3 *    0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
* 4 *    0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
* 5 *    0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
* 6 *    0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
* 7 *    0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
* 8 *    0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
*
*
*****

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*****
*
*
*          TIME SLICE FREEWAY PERFORMANCE TABLE
*
*****

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* SUB NO.    SSEC    O-D DATA DEMANDS    ADJUSTED VOLUMES    SSEC    WEAVE    CONGEST    STORAGE    V/C    SPEED    DENSITY    LOS    FUEL    EMISS
* SEC LNS    LENGTH    ORG    DES    SSEC    ORG    DES    SSEC    CAP.    EFF    LENGTH    RATE    RATIO    MPH    VPMP    LEVEL    MPG    GS/VM
*
* 1
* 2
* 3 1    11000.    1199.    0. 1199.    1199.    0. 1199.    1650.    0.    0.    0.    .73    62.    19.3    C    21.6    12.8
* 4 1    1500.    0. 0. 1199.    0.    0. 1199.    1650.    0.    0.    0.    .73    62.    19.3    C    21.6    12.8
* 5 1    1400.    0. 0. 1199.    0.    0. 1199.    1650.    0.    0.    0.    .73    62.    19.3    C    21.6    12.8
* 6 1    1500.    0. 0. 1199.    0.    0. 1199.    1650.    0.    0.    0.    .73    62.    19.3    C    21.6    12.8
* 7 1    1300.    0. 1199. 1199.    0. 1199. 1199.    1650.    0.    0.    0.    .73    62.    19.3    C    21.6    12.8
* 8
* 9
* 10
* 11
* 12
* 13
* 14
* 15
* 16
* 17
* 18
* 19

```

```

* 20
*
*****
* TOTAL 16700. = 3.2 MILES MAX(V/C) = 0.73 LOWEST LOS = C AVG = 62. 19.3 21.6 12.8
*
*****

```

```

CURRENT TIME SLICE CUMULATIVE VALUES
FREEWAY TRAVEL TIME = 31. VEH-HRS 61. PASS-HRS 31. VEH-HRS 61. PASS-HRS
FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 31. VEH-HRS 61. PASS-HRS 31. VEH-HRS 61. PASS-HRS
TOTAL FRWAY TRAV DI STANCE = 1896. VEH-MI . 3791. PASS-MI . 1896. VEH-MI . 3791. PASS-MI .
AVERAGE SYSTEM SPEED = 62. MPH 62. MPH
AVERAGE DENSITY = 19. VPML 19. VPML
TOTAL FUEL = 88. GALLONS 88. GALLONS
TOTAL EMISSIONS = 24. KI LOGRAMS 24. KI LOGRAMS

```

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 16:36 PAGE 6
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 1 OF 4

```

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
1 0.00 2 0.00 3 0.93 4 0.13 5 0.12
6 0.13 7 0.11 8 0.00 9 0.00 10 0.00
11 0.00 12 0.00 13 0.00 14 0.00 15 0.00
16 0.00 17 0.00 18 0.00 19 0.00 20 0.00
***** TOTAL DELAY = 1.4 VEH-HRS ***** AVERAGE DELAY = 0.07 MIN/VEH *****

```

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 16:36 PAGE 7
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 4

```

*****
** FREEWAY TRAVEL TIME (MINUTES) **
*****

```

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | | |
|-----------------|---------------------|------|------|------|------|------|------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| 1 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | 0.00 | 3.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 4 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 5 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 7 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 8 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 16:36 PAGE 8
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 4

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS | | | |
|---------|------|----------|---------|------------------|-------|-------|---------|---------|-------|-------|---------|-------|------|--------|---|------|------|
| SEC | LNS | LENGTH | ORG | DES | SSEC | EFF | LENGTH | RATE | RATIO | MPH | VPML | LEVEL | MPG | GS/VM | | | |
| 1 | | | | | | | | | | | | | | | | | |
| 2 | | | | | | | | | | | | | | | | | |
| 3 | 1 | 11000. | 1199. | 0. | 1199. | 1199. | 0. | 1199. | 1650. | 0. | 0. | .73 | 62. | 19.3 | C | 21.6 | 12.8 |
| 4 | 1 | 1500. | 0. | 0. | 1199. | 0. | 0. | 1199. | 1650. | 0. | 0. | .73 | 62. | 19.3 | C | 21.6 | 12.8 |
| 5 | 1 | 1400. | 0. | 0. | 1199. | 0. | 0. | 1199. | 1650. | 0. | 0. | .73 | 62. | 19.3 | C | 21.6 | 12.8 |
| 6 | 1 | 1500. | 0. | 0. | 1199. | 0. | 0. | 1199. | 1650. | 0. | 0. | .73 | 62. | 19.3 | C | 21.6 | 12.8 |
| 7 | 1 | 1300. | 0. | 1199. | 1199. | 0. | 1199. | 1199. | 1650. | 0. | 0. | .73 | 62. | 19.3 | C | 21.6 | 12.8 |
| 8 | | | | | | | | | | | | | | | | | |
| 9 | | | | | | | | | | | | | | | | | |

```

* 10
* 11
* 12
* 13
* 14
* 15
* 16
* 17
* 18
* 19
* 20
*****
* TOTAL 16700. = 3.2 MILES MAX(V/C) = 0.73 LOWEST LOS = C AVG = 62. 19.3 21.6 12.8
*****

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CURRENT TIME SLICE CUMULATIVE VALUES
FREEWAY TRAVEL TIME = 31. VEH-HRS 61. PASS-HRS 61. VEH-HRS 122. PASS-HRS
FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 31. VEH-HRS 61. PASS-HRS 61. VEH-HRS 122. PASS-HRS
TOTAL FRWAY TRAV DISTANCE = 1896. VEH-MI. 3791. PASS-MI. 3791. VEH-MI. 7582. PASS-MI.
AVERAGE SYSTEM SPEED = 62. MPH. 62. MPH.
AVERAGE DENSITY = 19. VPML 19. VPML
TOTAL FUEL = 88. GALLONS 176. GALLONS
TOTAL EMISSIONS = 24. KILOGRAMS 48. KILOGRAMS

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1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 16:36 PAGE 9
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 4

```

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
1 0.00 2 0.00 3 0.93 4 0.13 5 0.12
6 0.13 7 0.11 8 0.00 9 0.00 10 0.00
11 0.00 12 0.00 13 0.00 14 0.00 15 0.00
16 0.00 17 0.00 18 0.00 19 0.00 20 0.00
***** TOTAL DELAY = 1.4 VEH-HRS ***** AVERAGE DELAY = 0.07 MIN/VEH *****

```

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 16:36 PAGE 10
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 3 OF 4

```

*****
**
** FREEWAY TRAVEL TIME (MINUTES) **
**
*****

```

```

*****
* ORIGINS DESTINATIONS ACROSS *
* DOWN 1 2 3 4 5 6 7 8 *
+
* * * * *
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 2 * 0.00 3.06 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 3 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 4 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 5 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 8 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* * * * *
*****

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1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 16:36 PAGE 11
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 3 OF 4

TIME SLICE FREEWAY PERFORMANCE TABLE

```

*****
* SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMISS *
* SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPML LEVEL MPG GS/VM *
*****

```

```

*
* 1
* 2
* 3 1 11000. 1227. 0. 1227. 1227. 0. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8
* 4 1 1500. 0. 0. 1227. 0. 0. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8
* 5 1 1400. 0. 0. 1227. 0. 0. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8
* 6 1 1500. 0. 0. 1227. 0. 0. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8
* 7 1 1300. 0. 1227. 1227. 0. 1227. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8
* 8
* 9
* 10
* 11
* 12
* 13
* 14
* 15
* 16
* 17
* 18
* 19
* 20
*****
*
* TOTAL 16700. = 3.2 MILES MAX(V/C) = 0.74 LOWEST LOS = C AVG = 62. 19.8 21.6 12.8
*
*****

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```

CURRENT TIME SLICE CUMULATIVE VALUES
FREEWAY TRAVEL TIME = 31. VEH-HRS 63. PASS-HRS 92. VEH-HRS 185. PASS-HRS
FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 31. VEH-HRS 63. PASS-HRS 92. VEH-HRS 185. PASS-HRS
TOTAL FRWAY TRAV DISTANCE = 1941. VEH-MI. 3881. PASS-MI. 5732. VEH-MI. 11464. PASS-MI.
AVERAGE SYSTEM SPEED = 62. MPH. 62. MPH.
AVERAGE DENSITY = 20. VPML 19. VPML
TOTAL FUEL = 90. GALLONS 266. GALLONS
TOTAL EMISSIONS = 25. KILOGRAMS 73. KILOGRAMS

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***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
1 0.00 2 0.00 3 0.95 4 0.13 5 0.12
6 0.13 7 0.11 8 0.00 9 0.00 10 0.00
11 0.00 12 0.00 13 0.00 14 0.00 15 0.00
16 0.00 17 0.00 18 0.00 19 0.00 20 0.00
***** TOTAL DELAY = 1.4 VEH-HRS ***** AVERAGE DELAY = 0.07 MIN/VEH *****

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```

*****
**
** FREeway TRAVEL TIME (MINUTES) **
**
*****

```

```

*****
* ORIGINS DESTINATIONS ACROSS *
* DOWN 1 2 3 4 5 6 7 8 *
+
* * * * *
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 2 * 0.00 3.06 0.00 0.00 0.00 0.00 0.00 0.00
+
* 3 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 4 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 5 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 8 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* * * * *
*****

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*****
*
*
*          TIME SLICE FREEWAY PERFORMANCE TABLE
*
*****
* SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMISS
* SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMP L LEVEL MPG GS/VM
*
* 1
* 2
* 3 1 11000. 1227. 0. 1227. 1227. 0. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8
* 4 1 1500. 0. 0. 1227. 0. 0. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8
* 5 1 1400. 0. 0. 1227. 0. 0. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8
* 6 1 1500. 0. 0. 1227. 0. 0. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8
* 7 1 1300. 0. 1227. 1227. 0. 1227. 1227. 1650. 0. 0. 0. .74 62. 19.8 C 21.6 12.8
* 8
* 9
* 10
* 11
* 12
* 13
* 14
* 15
* 16
* 17
* 18
* 19
* 20
*
*****
*
* TOTAL 16700. = 3.2 MILES MAX(V/C) = 0.74 LOWEST LOS = C AVG = 62. 19.8 21.6 12.8
*
*****

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CURRENT TIME SLICE          CUMULATIVE VALUES
FREEWAY TRAVEL TIME =      31. VEH-HRS          63. PASS-HRS          124. VEH-HRS          248. PASS-HRS
FREEWAY MERGE DELAY =      0. VEH-HRS           0. PASS-HRS           0. VEH-HRS           0. PASS-HRS
ON-RAMP MRG/CAP DELAY =    0. VEH-HRS           0. PASS-HRS           0. VEH-HRS           0. PASS-HRS
OFF-RAMP DELAY =          0. VEH-HRS           0. PASS-HRS           0. VEH-HRS           0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 31. VEH-HRS          63. PASS-HRS          124. VEH-HRS          248. PASS-HRS
TOTAL FRWAY TRAV DISTANCE = 1941. VEH-MI.        3881. PASS-MI.        7673. VEH-MI.        15345. PASS-MI.
AVERAGE SYSTEM SPEED =    62. MPH
AVERAGE DENSITY =         20. VPMP L
TOTAL FUEL =                90. GALLONS
TOTAL EMISSIONS =          25. KI LOGRAMS

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1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 16:36 PAGE 15
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 4 OF 4

```

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
1 0.00 2 0.00 3 0.95 4 0.13 5 0.12
6 0.13 7 0.11 8 0.00 9 0.00 10 0.00
11 0.00 12 0.00 13 0.00 14 0.00 15 0.00
16 0.00 17 0.00 18 0.00 19 0.00 20 0.00
***** TOTAL DELAY = 1.4 VEH-HRS ***** AVERAGE DELAY = 0.07 MIN/VEH *****

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1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 16:36 PAGE 16
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF NON-PRIORITY LANES
 TIME SLICE 1 OF 4

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*****
**
**          FREeway TRAVEL TIME (MINUTES)
**
*****

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*****
* ORIGINS DESTINATIONS ACROSS
* DOWN
* 1 2 3 4 5 6 7 8
*
* 1 * 17.88 0.00 21.42 22.65 22.73 22.91 23.44 25.63
* 2 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
* 3 * 0.00 0.00 1.44 2.67 2.75 2.93 3.46 5.65
* 4 * 0.00 0.00 0.88 2.12 2.19 2.38 2.91 5.09
* 5 * 0.00 0.00 0.17 1.41 1.48 1.67 2.20 4.38
* 6 * 0.00 0.00 0.00 0.33 0.40 0.59 1.12 3.30
* 7 * 0.00 0.00 0.00 0.00 0.00 0.17 0.71 2.89
* 8 * 0.00 0.00 0.00 0.00 0.00 0.00 0.53 2.72
*

```


TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB * SEC | * NO. * LNS | * SSEC * LENGTH | * O-D DATA * ORG DES SSEC | * DEMANDS * SSEC | * ADJUSTED * ORG DES SSEC | * VOLUMES * SSEC | * SSEC * CAP. | * WEAVE * EFF | * CONGEST * LENGTH | * STORAGE * RATE | * V/C * RATIO | * SPEED * MPH | * DENSITY * VPMP | * LOS * LEVEL | * FUEL * MPG | * EMISSIONS * GS/VM |
|----------------|----------------|--------------------|------------------------------|---------------------|------------------------------|---------------------|------------------|------------------|-----------------------|---------------------|------------------|------------------|---------------------|------------------|-----------------|------------------------|
| * 1 | 3 | 500. | 4610. | 0. 4610. | 4610. | 0. 4610. | 6000. | 0. | 0. | 0. | .77 | 64. | 24.1 | C | 19.5 | 13.7 |
| * 2 | 3 | 99999. | 0. 1199. | 4610. | 0. | 1199. 4610. | 6000. | 0. | 0. | 0. | .77 | 64. | 24.1 | C | 19.5 | 13.7 |
| * 3 | 2 | 11000. | 0. 0. | 3431. | 0. | 0. 3431. | 4000. | 0. | 0. | 0. | .85 | 60. | 28.6 | D | 21.5 | 12.3 |
| * 4 | 2 | 1500. | 20. 0. | 3431. | 20. | 0. 3431. | 4000. | 0. | 0. | 0. | .86 | 59. | 28.8 | D | 21.5 | 12.3 |
| * 5 | 2 | 1400. | 0. 0. | 3431. | 0. | 0. 3431. | 4000. | 0. | 0. | 0. | .86 | 59. | 28.8 | D | 21.5 | 12.3 |
| * 6 | 2 | 1500. | 290. 0. | 3721. | 290. | 0. 3501. | 4000. | 0. | * 585. | 220. | .88 | 54. | 32.5 | F | 22.3 | 11.8 |
| * 7 | 2 | 1300. | 0. 0. | 3721. | 0. | 0. 3501. | 4000. | 0. | ** 1300. | 220. | .88 | 38. | 46.6 | F | 21.0 | 12.9 |
| * 8 | 3 | 500. | 1199. 950. | 4920. | 1199. 950. | 4700. 5130. | 0. | ** 500. | 220. | .92 | 33. | 47.7 | F | 20.8 | 13.3 | |
| * 9 | 2 | 2300. | 0. 0. | 3970. | 0. | 0. 3750. | 4000. | 0. | ** 2300. | 220. | .94 | 29. | 65.2 | F | 20.5 | 13.6 |
| * 10 | 3 | 250. | 200. 0. | 4170. | 200. | 0. 3950. | 4250. | 0. | ** 250. | 220. | .93 | 25. | 52.9 | F | 19.1 | 14.9 |
| * 11 | 3 | 200. | 0. 0. | 4170. | 0. | 0. 3950. | 4250. | 0. | ** 200. | 220. | .93 | 24. | 54.6 | F | 19.1 | 15.0 |
| * 12 | 3 | 250. | 0. 1550. | 4170. | 0. | 1550. 3950. | 4250. | 0. | ** 250. | 220. | .93 | 23. | 56.3 | F | 19.1 | 15.0 |
| * 13 | 2 | 50. | 0. 0. | 2620. | 0. | 0. 2400. | 4000. | 0. | ** 50. | 220. | .60 | 8. | 152.1 | F | 10.5 | 25.4 |
| * 14 | 2 | 50. | 0. 0. | 2620. | 0. | 0. 2400. | 2400. | 0. | 0. | 0. | 1.00 | 65. | 18.5 | E | 19.0 | 14.1 |
| * 15 | 2 | 1000. | 0. 0. | 2620. | 0. | 0. 2400. | 4000. | 0. | 0. | 0. | .60 | 65. | 18.5 | C | 19.0 | 14.1 |
| * 16 | 2 | 10. | 0. 0. | 2620. | 0. | 0. 2400. | 4000. | 0. | 0. | 0. | .60 | 65. | 18.5 | C | 19.0 | 14.1 |
| * 17 | 2 | 1500. | 608. 0. | 3228. | 608. | 0. 3008. | 4000. | 0. | 0. | 0. | .75 | 64. | 23.4 | C | 19.3 | 13.8 |
| * 18 | 2 | 1500. | 0. 790. | 3228. | 0. | 736. 3008. | 4000. | 0. | 0. | 0. | .75 | 64. | 23.4 | C | 19.3 | 13.8 |
| * 19 | 2 | 12000. | 0. 0. | 2438. | 0. | 0. 2272. | 4000. | 0. | 0. | 0. | .57 | 65. | 17.5 | B | 19.0 | 14.1 |
| * 20 | 3 | 500. | 0. 2438. | 2438. | 0. | 2272. 2272. | 6000. | 0. | 0. | 0. | .38 | 65. | 11.7 | B | 19.0 | 14.1 |

TOTAL 137309. = 26.0 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 61. 25.1 19.6 13.6

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 891. VEH-HRS | 1098. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 891. VEH-HRS | 1098. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 54468. VEH-MI. | 67229. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 61. MPH. | 61. MPH. |
| AVERAGE DENSITY = | 25. VPMP | 25. VPMP |
| TOTAL FUEL = | 2773. GALLONS | 2773. GALLONS |
| TOTAL EMISSIONS = | 739. KILOGRAMS | 739. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.06 | 2 | 12.02 | 3 | 4.89 | 4 | 0.69 | 5 | 0.65 |
| 6 | 1.68 | 7 | 5.07 | 8 | 3.44 | 9 | 16.12 | 10 | 2.33 |
| 11 | 1.96 | 12 | 2.56 | 13 | 1.27 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.09 | 18 | 0.09 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 52.9 VEH-HRS ***** AVERAGE DELAY = 0.82 MIN/VEH *****

 ** FREeway TRAVEL TIME (MINUTES) **

| * ORIGINS * DOWN | * DESTINATIONS ACROSS * | | | | | | | |
|---------------------|-------------------------|------|-------|-------|-------|-------|-------|-------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 17.88 | 0.00 | 23.13 | 24.60 | 24.67 | 24.86 | 25.39 | 27.57 |
| * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 3 * | 0.00 | 0.00 | 3.15 | 4.62 | 4.69 | 4.88 | 5.41 | 7.59 |

| | | | | | | | | |
|-------|------|------|------|------|------|------|------|------|
| * 4 * | 0.00 | 0.00 | 1.93 | 3.40 | 3.47 | 3.66 | 4.19 | 6.38 |
| * 5 * | 0.00 | 0.00 | 0.26 | 1.73 | 1.81 | 1.99 | 2.52 | 4.71 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.35 | 0.42 | 0.61 | 1.14 | 3.33 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 | 0.71 | 2.89 |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.53 | 2.72 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED | VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS | | | | |
|---------|------|----------|---------|----------|---------|-------|-------|---------|---------|-----|--------|---------|-------|------|--------|-------|------|-------|------|
| SEC | LNS | LENGTH | ORG | DES | SSEC | ORG | DES | SSEC | CAP. | EFF | LENGTH | RATE | RATIO | MPH | VP/MPH | LEVEL | MPG | GS/VM | |
| * 1 | 3 | 500. | 4610. | 0. | 4610. | 4610. | 0. | 4610. | 6000. | 0. | 0. | 0. | .77 | 64. | 24.1 | C | 19.5 | 13.7 | |
| * 2 | 3 | 99999. | 0. | 1199. | 4610. | 0. | 1199. | 4610. | 6000. | 0. | 0. | 0. | .77 | 64. | 24.1 | C | 19.5 | 13.7 | |
| * 3 | 2 | 11000. | 0. | 0. | 3411. | 0. | 0. | 3411. | 4000. | 0. | 0. | 0. | .85 | 60. | 28.6 | D | 21.5 | 12.3 | |
| * 4 | 2 | 1500. | 20. | 0. | 3431. | 20. | 0. | 3211. | 4000. | 0. | ** | 1500. | .220. | .80 | 37. | 43.5 | F | 20.1 | 13.7 |
| * 5 | 2 | 1400. | 0. | 0. | 3431. | 0. | 0. | 3211. | 4000. | 0. | ** | 1400. | .220. | .80 | 21. | 76.4 | F | 17.7 | 16.4 |
| * 6 | 2 | 1500. | 290. | 0. | 3721. | 290. | 0. | 3501. | 4000. | 0. | ** | 1500. | .220. | .88 | 19. | 89.9 | F | 17.9 | 16.6 |
| * 7 | 2 | 1300. | 0. | 0. | 3721. | 0. | 0. | 3501. | 4000. | 0. | ** | 1300. | .220. | .88 | 19. | 93.8 | F | 17.6 | 16.9 |
| * 8 | 3 | 500. | 1199. | 950. | 4920. | 1199. | 950. | 4700. | 5130. | 0. | ** | 500. | .220. | .92 | 22. | 72.6 | F | 18.7 | 15.5 |
| * 9 | 2 | 2300. | 0. | 0. | 3970. | 0. | 0. | 3750. | 4000. | 0. | ** | 2300. | .220. | .94 | 23. | 80.3 | F | 19.3 | 14.8 |
| * 10 | 3 | 250. | 200. | 0. | 4170. | 200. | 0. | 3950. | 4250. | 0. | ** | 250. | .220. | .93 | 23. | 58.1 | F | 19.1 | 15.1 |
| * 11 | 3 | 200. | 0. | 0. | 4170. | 0. | 0. | 3950. | 4250. | 0. | ** | 200. | .220. | .93 | 23. | 58.1 | F | 19.1 | 15.1 |
| * 12 | 3 | 250. | 0. | 1550. | 4170. | 0. | 1550. | 3950. | 4250. | 0. | ** | 250. | .220. | .93 | 23. | 58.1 | F | 19.1 | 15.1 |
| * 13 | 2 | 50. | 0. | 0. | 2620. | 0. | 0. | 2400. | 4000. | 0. | ** | 50. | .220. | .60 | 8. | 153.8 | F | 10.4 | 25.5 |
| * 14 | 2 | 50. | 0. | 0. | 2620. | 0. | 0. | 2400. | 2400. | 0. | 0. | 0. | 1.00 | 65. | 18.5 | E | 19.0 | 14.1 | |
| * 15 | 2 | 1000. | 0. | 0. | 2620. | 0. | 0. | 2400. | 4000. | 0. | 0. | 0. | .60 | 65. | 18.5 | C | 19.0 | 14.1 | |
| * 16 | 2 | 10. | 0. | 0. | 2620. | 0. | 0. | 2400. | 4000. | 0. | 0. | 0. | .60 | 65. | 18.5 | C | 19.0 | 14.1 | |
| * 17 | 2 | 1500. | 608. | 0. | 3228. | 608. | 0. | 3008. | 4000. | 0. | 0. | 0. | .75 | 64. | 23.4 | C | 19.3 | 13.8 | |
| * 18 | 2 | 1500. | 0. | 790. | 3228. | 0. | 736. | 3008. | 4000. | 0. | 0. | 0. | .75 | 64. | 23.4 | C | 19.3 | 13.8 | |
| * 19 | 2 | 12000. | 0. | 0. | 2438. | 0. | 0. | 2272. | 4000. | 0. | 0. | 0. | .57 | 65. | 17.5 | B | 19.0 | 14.1 | |
| * 20 | 3 | 500. | 0. | 2438. | 2438. | 0. | 2272. | 2272. | 6000. | 0. | 0. | 0. | .38 | 65. | 11.7 | B | 19.0 | 14.1 | |

TOTAL 137309. = 26.0 MILES

MAX(V/C) = 1.00 LOWEST LOS = F AVG = 57. 27.2

19.5 13.7

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 946. VEH-HRS | 1837. VEH-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 946. VEH-HRS | 1837. VEH-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 54372. VEH-MI. | 108840. VEH-MI. |
| AVERAGE SYSTEM SPEED = | 57. MPH | 59. MPH |
| AVERAGE DENSITY = | 27. VP/MPH | 26. VP/MPH |
| TOTAL FUEL = | 2787. GALLONS | 5560. GALLONS |
| TOTAL EMISSIONS = | 746. KILOGRAMS | 1485. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.06 | 2 | 12.02 | 3 | 4.89 | 4 | 5.63 | 5 | 14.07 |
| 6 | 17.97 | 7 | 16.47 | 8 | 6.89 | 9 | 22.41 | 10 | 2.69 |
| 11 | 2.15 | 12 | 2.69 | 13 | 1.28 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.09 | 18 | 0.09 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 109.4 VEH-HRS ***** AVERAGE DELAY = 1.80 MIN/VEH *****

 ** FREeway TRAVEL TIME (MINUTES) **

| ORIGINS | DESTINATIONS ACROSS | | | | | | | |
|---------|---------------------|---|---|---|---|---|---|---|
| DOWN | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |

| | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * | * |
|---|---|-------|------|-------|-------|-------|-------|-------|-------|---|---|---|---|---|---|---|---|---|---|
| 1 | * | 18.00 | 0.00 | 24.56 | 25.91 | 25.97 | 26.15 | 26.76 | 28.95 | | | | | | | | | | |
| 2 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | | | | | | | | | |
| 3 | * | 0.00 | 0.00 | 3.64 | 5.00 | 5.05 | 5.24 | 5.84 | 8.03 | | | | | | | | | | |
| 4 | * | 0.00 | 0.00 | 1.60 | 2.96 | 3.01 | 3.20 | 3.80 | 5.99 | | | | | | | | | | |
| 5 | * | 0.00 | 0.00 | 0.22 | 1.57 | 1.63 | 1.81 | 2.42 | 4.60 | | | | | | | | | | |
| 6 | * | 0.00 | 0.00 | 0.00 | 0.32 | 0.37 | 0.56 | 1.17 | 3.35 | | | | | | | | | | |
| 7 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 | 0.78 | 2.97 | | | | | | | | | | |
| 8 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.61 | 2.79 | | | | | | | | | | |

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED | VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS | | | | |
|---------|------|----------|---------|----------|---------|-------|-------|---------|---------|-----|--------|---------|-------|------|--------|-------|------|-------|------|
| SEC | LNS | LENGTH | ORG | DES | SSEC | ORG | DES | SSEC | CAP. | EFF | LENGTH | RATE | RATIO | MPH | VPMPL | LEVEL | MPG | GS/VM | |
| * 1 | 3 | 500. | 4720. | 0. | 4720. | 4720. | 0. | 4720. | 6000. | 0. | 0. | 0. | .79 | 63. | 24.8 | C | 19.7 | 13.5 | |
| * 2 | 3 | 99999. | 0. | 1227. | 4720. | 0. | 1227. | 4720. | 6000. | 0. | 0. | 0. | .79 | 63. | 24.8 | C | 19.7 | 13.5 | |
| * 3 | 2 | 11000. | 0. | 0. | 3493. | 0. | 0. | 3312. | 4000. | 0. | ** | 3208. | 181. | .83 | 43. | 38.7 | F | 20.7 | 13.0 |
| * 4 | 2 | 1500. | 19. | 0. | 3512. | 19. | 0. | 3331. | 4000. | 0. | ** | 1500. | 181. | .83 | 16. | 103.1 | F | 16.5 | 18.3 |
| * 5 | 2 | 1400. | 0. | 0. | 3512. | 0. | 0. | 3331. | 4000. | 0. | ** | 1400. | 181. | .83 | 16. | 103.1 | F | 16.5 | 18.3 |
| * 6 | 2 | 1500. | 401. | 0. | 3913. | 401. | 0. | 3732. | 4000. | 0. | ** | 1500. | 181. | .93 | 23. | 81.3 | F | 19.2 | 15.0 |
| * 7 | 2 | 1300. | 0. | 0. | 3913. | 0. | 0. | 3732. | 4000. | 0. | ** | 1300. | 181. | .93 | 23. | 81.3 | F | 19.2 | 15.0 |
| * 8 | 3 | 500. | 1227. | 1130. | 5140. | 1227. | 1128. | 4959. | 5130. | 0. | ** | 500. | 171. | .97 | 26. | 63.2 | F | 20.2 | 13.8 |
| * 9 | 2 | 2300. | 0. | 0. | 4010. | 0. | 0. | 3831. | 4000. | 0. | ** | 2300. | 169. | .96 | 25. | 75.9 | F | 19.9 | 14.1 |
| * 10 | 3 | 250. | 226. | 0. | 4236. | 226. | 0. | 4057. | 4250. | 0. | ** | 250. | 169. | .95 | 25. | 54.2 | F | 19.8 | 14.2 |
| * 11 | 3 | 200. | 0. | 0. | 4236. | 0. | 0. | 4057. | 4250. | 0. | ** | 200. | 169. | .95 | 25. | 54.2 | F | 19.8 | 14.2 |
| * 12 | 3 | 250. | 0. | 1311. | 4236. | 0. | 1308. | 4057. | 4250. | 0. | ** | 250. | 169. | .95 | 25. | 54.2 | F | 19.8 | 14.2 |
| * 13 | 2 | 50. | 0. | 350. | 2925. | 0. | 349. | 2749. | 4000. | 0. | ** | 50. | 169. | .69 | 10. | 134.8 | F | 13.1 | 22.8 |
| * 14 | 2 | 50. | 0. | 0. | 2575. | 0. | 0. | 2400. | 2400. | 0. | 0. | 0. | 1.00 | 65. | 18.5 | E | 19.0 | 14.1 | |
| * 15 | 2 | 1000. | 350. | 0. | 2925. | 350. | 0. | 2750. | 4000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 19.0 | 14.1 | |
| * 16 | 2 | 10. | 0. | 0. | 2925. | 0. | 0. | 2750. | 4000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 19.0 | 14.1 | |
| * 17 | 2 | 1500. | 1038. | 0. | 3963. | 1038. | 0. | 3788. | 4000. | 0. | 0. | 0. | .95 | 56. | 33.6 | D | 22.4 | 11.7 | |
| * 18 | 2 | 1500. | 0. | 1271. | 3963. | 0. | 1215. | 3788. | 4000. | 0. | 0. | 0. | .95 | 56. | 33.6 | D | 22.4 | 11.7 | |
| * 19 | 2 | 12000. | 0. | 0. | 2692. | 0. | 0. | 2573. | 4000. | 0. | 0. | 0. | .64 | 65. | 19.8 | C | 19.0 | 14.1 | |
| * 20 | 3 | 500. | 0. | 2692. | 2692. | 0. | 2573. | 2573. | 6000. | 0. | 0. | 0. | .43 | 65. | 13.2 | B | 19.0 | 14.1 | |

TOTAL 137309. = 26.0 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 55. 29.6 19.7 13.6

| | CURRENT TIME SLICE | | CUMULATIVE VALUES |
|-----------------------------|--------------------|-----------------|-------------------------------------|
| FREWAY TRAVEL TIME = | 1016. VEH-HRS | 1234. PASS-HRS | 2853. VEH-HRS 3488. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1016. VEH-HRS | 1234. PASS-HRS | 2853. VEH-HRS 3488. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 56183. VEH-MI. | 69385. PASS-MI. | 165022. VEH-MI. 203739. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 55. MPH | | 58. MPH |
| AVERAGE DENSITY = | 30. VPMPL | | 27. VPMPL |
| TOTAL FUEL = | 2858. GALLONS | | 8418. GALLONS |
| TOTAL EMISSIONS = | 765. KI LOGRAMS | | 2250. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.08 | 2 | 16.67 | 3 | 28.81 | 4 | 22.02 | 5 | 20.55 |
| 6 | 14.94 | 7 | 12.94 | 8 | 5.37 | 9 | 20.21 | 10 | 2.37 |
| 11 | 1.90 | 12 | 2.37 | 13 | 1.08 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 1.27 | 18 | 1.27 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 151.9 VEH-HRS ***** AVERAGE DELAY = 2.49 MIN/VEH *****

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|-------|-----------------------|-------|-------|-------|-------|-------|-------|---|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 18.00 | 0.00 | 26.20 | 27.55 | 27.61 | 27.79 | 28.40 | 30.58 | |
| * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| * 3 * | 0.00 | 0.00 | 3.64 | 5.00 | 5.05 | 5.24 | 5.84 | 8.03 | |
| * 4 * | 0.00 | 0.00 | 1.60 | 2.96 | 3.01 | 3.20 | 3.80 | 5.99 | |
| * 5 * | 0.00 | 0.00 | 0.22 | 1.57 | 1.63 | 1.81 | 2.42 | 4.60 | |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.32 | 0.37 | 0.56 | 1.17 | 3.35 | |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 | 0.78 | 2.97 | |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.61 | 2.79 | |

 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | |
|-----------|----------|------------|-------------|------------|-------------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|------|
| * SEC LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | |
| * 1 3 | 500. | 4720. | 0. 4720. | 4720. | 0. 4720. | 6000. | 0. | 0. | 0. | .79 | 63. | 24.8 | C | 19.7 | 13.5 | |
| * 2 3 | 99999. | 0. | 1227. 4720. | 0. | 1227. 4720. | 6000. | 0. | 0. | 0. | .79 | 63. | 24.8 | C | 19.7 | 13.5 | |
| * 3 2 | 11000. | 0. | 0. 3493. | 0. | 0. 3312. | 4000. | 0. | * 6415. | 181. | .83 | 27. | 60.4 | F | 19.1 | 14.8 | |
| * 4 2 | 1500. | 19. | 0. 3512. | 19. | 0. 3331. | 4000. | 0. | ** 1500. | 181. | .83 | 16. | 103.1 | F | 16.5 | 18.3 | |
| * 5 2 | 1400. | 0. | 0. 3512. | 0. | 0. 3331. | 4000. | 0. | ** 1400. | 181. | .83 | 16. | 103.1 | F | 16.5 | 18.3 | |
| * 6 2 | 1500. | 401. | 0. 3913. | 401. | 0. 3732. | 4000. | 0. | ** 1500. | 181. | .93 | 23. | 81.3 | F | 19.2 | 15.0 | |
| * 7 2 | 1300. | 0. | 0. 3913. | 0. | 0. 3732. | 4000. | 0. | ** 1300. | 181. | .93 | 23. | 81.3 | F | 19.2 | 15.0 | |
| * 8 3 | 500. | 1227. | 1130. 5140. | 1227. | 1128. 4959. | 5130. | 0. | ** 500. | 171. | .97 | 26. | 63.2 | F | 20.2 | 13.8 | |
| * 9 2 | 2300. | 0. | 0. 4010. | 0. | 0. 3831. | 4000. | 0. | ** 2300. | 169. | .96 | 25. | 75.9 | F | 19.9 | 14.1 | |
| * 10 3 | 250. | 226. | 0. 4236. | 226. | 0. 4057. | 4250. | 0. | ** 250. | 169. | .95 | 25. | 54.2 | F | 19.8 | 14.2 | |
| * 11 3 | 200. | 0. | 0. 4236. | 0. | 0. 4057. | 4250. | 0. | ** 200. | 169. | .95 | 25. | 54.2 | F | 19.8 | 14.2 | |
| * 12 3 | 250. | 0. | 1311. 4236. | 0. | 1308. 4057. | 4250. | 0. | ** 250. | 169. | .95 | 25. | 54.2 | F | 19.8 | 14.2 | |
| * 13 2 | 50. | 0. | 0. 2925. | 0. | 0. 349. | 2749. | 4000. | 0. | ** 50. | 169. | .69 | 10. | 134.8 | F | 13.1 | 22.8 |
| * 14 2 | 50. | 0. | 0. 2575. | 0. | 0. 2400. | 2400. | 0. | 0. | 0. | 1.00 | 65. | 18.5 | E | 19.0 | 14.1 | |
| * 15 2 | 1000. | 350. | 0. 2925. | 350. | 0. 2750. | 4000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 19.0 | 14.1 | |
| * 16 2 | 10. | 0. | 0. 2925. | 0. | 0. 2750. | 4000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 19.0 | 14.1 | |
| * 17 2 | 1500. | 1038. | 0. 3963. | 1038. | 0. 3788. | 4000. | 0. | 0. | 0. | .95 | 56. | 33.6 | D | 22.4 | 11.7 | |
| * 18 2 | 1500. | 0. | 1271. 3963. | 0. | 1215. 3788. | 4000. | 0. | 0. | 0. | .95 | 56. | 33.6 | D | 22.4 | 11.7 | |
| * 19 2 | 12000. | 0. | 0. 2692. | 0. | 0. 2573. | 4000. | 0. | 0. | 0. | .64 | 65. | 19.8 | C | 19.0 | 14.1 | |
| * 20 3 | 500. | 0. | 2692. 2692. | 0. | 2573. 2573. | 6000. | 0. | 0. | 0. | .43 | 65. | 13.2 | B | 19.0 | 14.1 | |

 *
 * TOTAL 137309. = 26.0 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 53. 31.3 19.6 13.7 *
 *

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 1061. VEH-HRS | 3914. VEH-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1061. VEH-HRS | 3914. VEH-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 56127. VEH-MI. | 221150. VEH-MI. |
| AVERAGE SYSTEM SPEED = | 53. MPH. | 56. MPH. |
| AVERAGE DENSITY = | 31. VPMP | 28. VPMP |
| TOTAL FUEL = | 2870. GALLONS | 11288. GALLONS |
| TOTAL EMISSIONS = | 771. KILOGRAMS | 3021. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.08 | 2 | 16.67 | 3 | 74.93 | 4 | 22.02 | 5 | 20.55 |
| 6 | 14.94 | 7 | 12.94 | 8 | 5.37 | 9 | 20.21 | 10 | 2.37 |
| 11 | 1.90 | 12 | 2.37 | 13 | 1.08 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 1.27 | 18 | 1.27 | 19 | 0.00 | 20 | 0.00 |

SR-237_WB_AM_P2_MOD_2018_PL.txt

***** TOTAL DELAY = 198.0 VEH-HRS ***** AVERAGE DELAY = 3.33 MIN/VEH *****

| | | | | | | | |
|----------|----------|----------|---------------|-------------|---------|------------|-----|
| FFFFFFFF | RRRRRRRR | EEEEEEEE | Q | 1111 | 222222 | PPPPPPPP | LLL |
| FFFFFFFF | RRRRRRRR | EEEEEEEE | O*A. D. MAY*O | 111111 | 222 222 | PPPPPPPP | LLL |
| FFF | RRR | RRR | EEE | Q | 1111 | 222 222 | PPP |
| FFF | RRR | RRR | EEE | Q | 1111 | 222 | PPP |
| FFFFFFFF | RRRRRRRR | EEEEEEEE | Q | 1111 | 222 | PPPPPPPP | LLL |
| FFFFFFFF | RRRRRRRR | EEEEEEEE | Q | 1111 | 2222 | PPPPPPPP | LLL |
| FFF | RRR | RRR | EEE | Q | 1111 | 2222 | PPP |
| FFF | RRR | RRR | EEE | O*UC* | 1111 | 222 | PPP |
| FFF | RRR | RRR | EEE | O*REGENTS*O | 1111 | 222 | PPP |
| FFF | RRR | RRR | EEE | Q*1988*Q | 1111111 | 2222222222 | PPP |

FREQ12PL

- 1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 3 AND 7 WILL BE SIMULATED.
- 2. SHORT TERM CONSEQUENCES ARE REQUESTED.
- 3. THERE ARE 2.0 TIME SLICES PER HOUR.
- 4. WEAVING ANALYSIS IS NOT ENGAGED.
- 5. NO ALTERNATE ROUTE IS PROVIDED.
- 6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 30
- 7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
- 8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
- 9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
- 10. NUMBER OF PRIORITY LANES = 1.
- 11. PRIORITY CUTOFF LIMIT = 2.

ON-RAMP CAPACITY LIMITS

| | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| 6000. | ***** | 1500. | 1500. | ***** | 2000. | 1500. | 1500. |

OFF-RAMP CAPACITY LIMITS

| | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| ***** | ***** | 2000. | 2000. | 1500. | 1500. | 1500. | 6000. |

ON-RAMP 1 IS THE MAINLINE ORIGIN
OFF-RAMP 8 IS THE MAINLINE DESTINATION

***** ON-RAMPS 2 AND 5 ARE SYNTHETIC ORIGINS USED TO ENTER AND LEAVE THE PL LANE(S)
***** OFF-RAMPS 1 AND 2 ARE SYNTHETIC DESTINATIONS USED TO ENTER AND LEAVE THE PL LANE(S)

INPUT HAS BEEN COMPLETED

```

*****
*****
**
**
**                      FREEWAY AND ARTERIAL DESIGN FEATURES                      **
**
*****
*****
** SUB NO.   SSEC   SSEC   DESIGN   ORG   TRK   SSEC PCT   PCT DES SPECIAL   FF. SPD.   CAP.   ART   GRADE   SUBSECTI ON LOCATI ON   **
** SEC LNS   CAP    LENGTH SPEED   DES   FAC   GRAD TRK   TRUCKS  RAMP   ALT. RTE   ALT. RTE   TYPE   ALT. RTE                   **
**
*****
** 1
**
** 2
**
** 3  1  1500.  11000.  62   0  0.95  0.0  0  100   NO   0.0   0.0   GOOD   0.0  HOV Dummy                **
**
** 4  1  1500.   1500.  62   0  0.95  0.0  0  100   NO   0.0   0.0   GOOD   0.0  Lawrence On-ramp           **
**
** 5  1  1500.   1400.  62   0  0.95  0.0  0  100   NO   0.0   0.0   GOOD   0.0  Lawrence to Crossman       **
**
** 6  1  1500.   1500.  62   0  0.95  0.0  0  100   YES  0.0   0.0   GOOD   0.0  Crossman On-Ramp           **
**
** 7  1  1500.   1300.  62   0  0.95  0.0  0  100   NO   0.0   0.0   GOOD   0.0  Crossman / Mathilda        **

```

** 8 **
** 9 **
** 10 **
** 11 **
** 12 **
** 13 **
** 14 **
** 15 **
** 16 **
** 17 **
** 18 **
** 19 **
** 20 **

** FREEWAY TRAVEL TIME (MINUTES) **

Table with columns: ORIGINS DOWN, DESTINATIONS ACROSS (1-8). Rows 1-8 showing travel times between origins and destinations.

TIME SLICE FREEWAY PERFORMANCE TABLE

Table with columns: SUB NO, SSEC, O-D DATA DEMANDS, ADJUSTED VOLUMES, SSEC, WEAVE EFF, CONGEST LENGTH, STORAGE RATE, V/C RATIO, SPEED, DENSITY, LOS, FUEL MPG, EMISSIONS GS/VM. Rows 1-19.

```

* 20
*
*****
* TOTAL 16700. = 3.2 MILES MAX(V/C) = 0.38 LOWEST LOS = A AVG = 62. 9.2 21.6 12.8
*
*****

```

```

CURRENT TIME SLICE CUMULATIVE VALUES
FREEWAY TRAVEL TIME = 15. VEH-HRS 29. PASS-HRS 15. VEH-HRS 29. PASS-HRS
FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 15. VEH-HRS 29. PASS-HRS 15. VEH-HRS 29. PASS-HRS
TOTAL FRWAY TRAV DI STANCE = 903. VEH-MI . 1807. PASS-MI . 903. VEH-MI . 1807. PASS-MI .
AVERAGE SYSTEM SPEED = 62. MPH 62. MPH
AVERAGE DENSITY = 9. VPMP 9. VPMP
TOTAL FUEL = 42. GALLONS 42. GALLONS
TOTAL EMISSIONS = 12. KI LOGRAMS 12. KI LOGRAMS

```

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/ 3/2016 15: 8 PAGE 6
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 1 OF 6

```

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
1 0.00 2 0.00 3 0.44 4 0.06 5 0.06
6 0.06 7 0.05 8 0.00 9 0.00 10 0.00
11 0.00 12 0.00 13 0.00 14 0.00 15 0.00
16 0.00 17 0.00 18 0.00 19 0.00 20 0.00
***** TOTAL DELAY = 0.7 VEH-HRS ***** AVERAGE DELAY = 0.07 MIN/VEH *****

```

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/ 3/2016 15: 8 PAGE 7
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 6

```

*****
** FREEWAY TRAVEL TIME (MINUTES) **
*****

```

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | | |
|--------------|---------------------|------|------|------|------|------|------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| 1 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | 0.00 | 3.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 4 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 5 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 7 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 8 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/ 3/2016 15: 8 PAGE 8
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 6

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS | | | |
|---------|------|----------|---------|----------|------|-------|---------|---------|-------|-------|---------|-------|------|--------|---|------|------|
| SEC | LNS | LENGTH | ORG | DES | ORG | DES | LENGTH | RATE | RATIO | MPH | VPMP | LEVEL | MPG | GS/VM | | | |
| 1 | | | | | | | | | | | | | | | | | |
| 2 | | | | | | | | | | | | | | | | | |
| 3 | 1 | 11000. | 571. | 0. | 571. | 571. | 0. | 571. | 1500. | 0. | 0. | .38 | 62. | 9.2 | A | 21.6 | 12.8 |
| 4 | 1 | 1500. | 0. | 0. | 571. | 0. | 0. | 571. | 1500. | 0. | 0. | .38 | 62. | 9.2 | A | 21.6 | 12.8 |
| 5 | 1 | 1400. | 0. | 0. | 571. | 0. | 0. | 571. | 1500. | 0. | 0. | .38 | 62. | 9.2 | A | 21.6 | 12.8 |
| 6 | 1 | 1500. | 0. | 0. | 571. | 0. | 0. | 571. | 1500. | 0. | 0. | .38 | 62. | 9.2 | A | 21.6 | 12.8 |
| 7 | 1 | 1300. | 0. | 571. | 571. | 0. | 571. | 571. | 1500. | 0. | 0. | .38 | 62. | 9.2 | A | 21.6 | 12.8 |
| 8 | | | | | | | | | | | | | | | | | |
| 9 | | | | | | | | | | | | | | | | | |


```

*10
* 11
* 12
* 13
* 14
* 15
* 16
* 17
* 18
* 19
* 20
*
*****
*
* TOTAL 16700. = 3.2 MILES MAX(V/C) = 0.38 LOWEST LOS = A AVG = 62. 9.2 21.6 12.8
*
*****

```

```

CURRENT TIME SLICE CUMULATIVE VALUES
FREEWAY TRAVEL TIME = 15. VEH-HRS 29. PASS-HRS 29. VEH-HRS 58. PASS-HRS
FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 15. VEH-HRS 29. PASS-HRS 29. VEH-HRS 58. PASS-HRS
TOTAL FRWAY TRAV DISTANCE = 903. VEH-MI. 1807. PASS-MI. 1807. VEH-MI. 3613. PASS-MI.
AVERAGE SYSTEM SPEED = 62. MPH. 62. MPH.
AVERAGE DENSITY = 9. VPMP. 9. VPMP.
TOTAL FUEL = 42. GALLONS 84. GALLONS
TOTAL EMISSIONS = 12. KILOGRAMS 23. KILOGRAMS

```

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/ 3/2016 15: 8 PAGE 9
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 6

```

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
1 0.00 2 0.00 3 0.44 4 0.06 5 0.06
6 0.06 7 0.05 8 0.00 9 0.00 10 0.00
11 0.00 12 0.00 13 0.00 14 0.00 15 0.00
16 0.00 17 0.00 18 0.00 19 0.00 20 0.00
***** TOTAL DELAY = 0.7 VEH-HRS ***** AVERAGE DELAY = 0.07 MIN/VEH *****

```

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/ 3/2016 15: 8 PAGE 10
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 3 OF 6

```

*****
**
** FREeway TRAVEL TIME (MINUTES) **
**
*****

```

```

*****
* ORIGINS DESTINATIONS ACROSS *
* DOWN 1 2 3 4 5 6 7 8 *
+
* * * * *
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 2 * 0.00 3.06 0.00 0.00 0.00 0.00 0.00 0.00
+
* 3 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 4 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 5 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 8 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* *
*****

```

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/ 3/2016 15: 8 PAGE 11
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 3 OF 6

```

*****
*
* TIME SLICE FREEWAY PERFORMANCE TABLE
*
*****
* SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMISS *
* SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMP. LEVEL MPG GS/VM *
*****

```

```

*
* 1
* 2
* 3 1 11000. 621. 0. 621. 621. 0. 621. 1500. 0. 0. 0. .41 62. 10.0 A 21.6 12.8
* 4 1 1500. 0. 0. 621. 0. 0. 621. 1500. 0. 0. 0. .41 62. 10.0 A 21.6 12.8
* 5 1 1400. 0. 0. 621. 0. 0. 621. 1500. 0. 0. 0. .41 62. 10.0 A 21.6 12.8
* 6 1 1500. 0. 0. 621. 0. 0. 621. 1500. 0. 0. 0. .41 62. 10.0 A 21.6 12.8
* 7 1 1300. 0. 621. 621. 0. 621. 621. 1500. 0. 0. 0. .41 62. 10.0 A 21.6 12.8
* 8
* 9
* 10
* 11
* 12
* 13
* 14
* 15
* 16
* 17
* 18
* 19
* 20
*****
*
* TOTAL 16700. = 3.2 MILES MAX(V/C) = 0.41 LOWEST LOS = A AVG = 62. 10.0 21.6 12.8
*
*****

```

```

CURRENT TIME SLICE CUMULATIVE VALUES
FREEWAY TRAVEL TIME = 16. VEH-HRS 32. PASS-HRS 45. VEH-HRS 90. PASS-HRS
FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 16. VEH-HRS 32. PASS-HRS 45. VEH-HRS 90. PASS-HRS
TOTAL FRWAY TRAV DISTANCE = 982. VEH-MI. 1963. PASS-MI. 2788. VEH-MI. 5576. PASS-MI.
AVERAGE SYSTEM SPEED = 62. MPH. 62. MPH.
AVERAGE DENSITY = 10. VPML 9. VPML
TOTAL FUEL = 46. GALLONS 129. GALLONS
TOTAL EMISSIONS = 13. KILOGRAMS 36. KILOGRAMS

```

```

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
1 0.00 2 0.00 3 0.48 4 0.07 5 0.06
6 0.07 7 0.06 8 0.00 9 0.00 10 0.00
11 0.00 12 0.00 13 0.00 14 0.00 15 0.00
16 0.00 17 0.00 18 0.00 19 0.00 20 0.00
***** TOTAL DELAY = 0.7 VEH-HRS ***** AVERAGE DELAY = 0.07 MIN/VEH *****

```

```

*****
**
** FREeway TRAVEL TIME (MINUTES) **
**
*****

```

```

*****
* ORIGINS DESTINATIONS ACROSS *
* DOWN 1 2 3 4 5 6 7 8 *
+
* * * * *
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 2 * 0.00 3.06 0.00 0.00 0.00 0.00 0.00 0.00
+
* 3 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 4 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 5 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 8 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* * * * *
*****

```

 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *

 * SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMISS *
 * SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMP L LEVEL MPG GS/VM *

 * 1 *
 * 2 *
 * 3 1 11000. 621. 0. 621. 621. 0. 621. 1500. 0. 0. 0. .41 62. 10.0 A 21.6 12.8 *
 * 4 1 1500. 0. 0. 621. 0. 0. 621. 1500. 0. 0. 0. .41 62. 10.0 A 21.6 12.8 *
 * 5 1 1400. 0. 0. 621. 0. 0. 621. 1500. 0. 0. 0. .41 62. 10.0 A 21.6 12.8 *
 * 6 1 1500. 0. 0. 621. 0. 0. 621. 1500. 0. 0. 0. .41 62. 10.0 A 21.6 12.8 *
 * 7 1 1300. 0. 621. 621. 0. 621. 621. 1500. 0. 0. 0. .41 62. 10.0 A 21.6 12.8 *
 * 8 *
 * 9 *
 * 10 *
 * 11 *
 * 12 *
 * 13 *
 * 14 *
 * 15 *
 * 16 *
 * 17 *
 * 18 *
 * 19 *
 * 20 *

 * TOTAL 16700. = 3.2 MILES MAX(V/C) = 0.41 LOWEST LOS = A AVG = 62. 10.0 21.6 12.8 *

| | | |
|-----------------------------|-----------------------------|------------------------------|
| | CURRENT TIME SLICE | CUMULATIVE VALUES |
| FREEWAY TRAVEL TIME = | 16. VEH-HRS 32. PASS-HRS | 61. VEH-HRS 122. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 16. VEH-HRS 32. PASS-HRS | 61. VEH-HRS 122. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 982. VEH-MI. 1963. PASS-MI. | 3770. VEH-MI. 7539. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 62. MPH. |
| AVERAGE DENSITY = | 10. VPMP L | 10. VPMP L |
| TOTAL FUEL = | 46. GALLONS | 175. GALLONS |
| TOTAL EMISSIONS = | 13. KI LOGRAMS | 48. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| | | | | | | | | | |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
| 1 | 0.00 | 2 | 0.00 | 3 | 0.48 | 4 | 0.07 | 5 | 0.06 |
| 6 | 0.07 | 7 | 0.06 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 0.7 VEH-HRS ***** AVERAGE DELAY = 0.07 MIN/VEH *****

 **
 ** FREeway TRAVEL TIME (MINUTES) **
 **

| | | | |
|-------|-----------|---|---|
| ***** | * ORIGINS | DESTINATIONS ACROSS | * |
| + | * DOWN | | * |
| | | 1 2 3 4 5 6 7 8 | |
| + | * 1 * | 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | * |
| + | * 2 * | 0.00 3.06 0.00 0.00 0.00 0.00 0.00 0.00 | * |
| + | * 3 * | 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | * |
| + | * 4 * | 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | * |
| + | * 5 * | 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | * |
| + | * 6 * | 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | * |
| + | * 7 * | 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | * |
| + | * 8 * | 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 | * |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB * SEC | * NO. * LNS | * SSEC * LENGTH | * O-D DATA * ORG DES | * DEMANDS * SSEC | * ADJUSTED * ORG DES | * VOLUMES * SSEC | * SSEC * CAP. | * WEAVE * EFF | * CONGEST * LENGTH | * STORAGE * RATE | * V/C * RATIO | * SPEED * MPH | * DENSITY * VPMP | * LOS * LEVEL | * FUEL * MPG | * EMISS * GS/VM | |
|----------------|----------------|--------------------|-------------------------|---------------------|-------------------------|---------------------|------------------|------------------|-----------------------|---------------------|------------------|------------------|---------------------|------------------|-----------------|--------------------|------|
| * 1 | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | |
| * 3 | 1 | 11000. | 536. | 0. | 536. | 536. | 0. | 536. | 1500. | 0. | 0. | .36 | 62. | 8.6 | A | 21.6 | 12.8 |
| * 4 | 1 | 1500. | 0. | 0. | 536. | 0. | 0. | 536. | 1500. | 0. | 0. | .36 | 62. | 8.6 | A | 21.6 | 12.8 |
| * 5 | 1 | 1400. | 0. | 0. | 536. | 0. | 0. | 536. | 1500. | 0. | 0. | .36 | 62. | 8.6 | A | 21.6 | 12.8 |
| * 6 | 1 | 1500. | 0. | 0. | 536. | 0. | 0. | 536. | 1500. | 0. | 0. | .36 | 62. | 8.6 | A | 21.6 | 12.8 |
| * 7 | 1 | 1300. | 0. | 536. | 536. | 0. | 536. | 536. | 1500. | 0. | 0. | .36 | 62. | 8.6 | A | 21.6 | 12.8 |
| * 8 | | | | | | | | | | | | | | | | | |
| * 9 | | | | | | | | | | | | | | | | | |
| * 10 | | | | | | | | | | | | | | | | | |
| * 11 | | | | | | | | | | | | | | | | | |
| * 12 | | | | | | | | | | | | | | | | | |
| * 13 | | | | | | | | | | | | | | | | | |
| * 14 | | | | | | | | | | | | | | | | | |
| * 15 | | | | | | | | | | | | | | | | | |
| * 16 | | | | | | | | | | | | | | | | | |
| * 17 | | | | | | | | | | | | | | | | | |
| * 18 | | | | | | | | | | | | | | | | | |
| * 19 | | | | | | | | | | | | | | | | | |
| * 20 | | | | | | | | | | | | | | | | | |
| * TOTAL | 16700. | = | 3.2 | MILES | | | | | | | | MAX(V/C) = 0.36 | LOWEST LOS = A | AVG = 62. | 8.6 | 21.6 | 12.8 |

| | | | |
|-----------------------------|--------------------|----------------|------------------------------|
| | CURRENT TIME SLICE | | CUMULATIVE VALUES |
| FREEWAY TRAVEL TIME = | 14. VEH-HRS | 27. PASS-HRS | 74. VEH-HRS 149. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 14. VEH-HRS | 27. PASS-HRS | 74. VEH-HRS 149. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 848. VEH-MI. | 1695. PASS-MI. | 4617. VEH-MI. 9235. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | | 62. MPH. |
| AVERAGE DENSITY = | 9. VPMP | | 9. VPMP |
| TOTAL FUEL = | 39. GALLONS | | 214. GALLONS |
| TOTAL EMISSIONS = | 11. KILOGRAMS | | 59. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.42 | 4 | 0.06 | 5 | 0.05 |
| 6 | 0.06 | 7 | 0.05 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 0.6 VEH-HRS ***** AVERAGE DELAY = 0.07 MIN/VEH *****

 ** FREeway TRAVEL TIME (MINUTES) **

| * ORIGINS * DOWN | * DESTINATIONS ACROSS * | | | | | | | |
|---------------------|-------------------------|------|------|------|------|------|------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 3.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

```

SR-237_WB_PM_NP_MOD_2018_PL_2.txt
* 4 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
* 5 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
* 8 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
* *
*****

```

 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *
 * SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMISS *
 * SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMP LEVEL MPG GS/VM *
 *
 * 1 *
 * 2 *
 * 3 1 11000. 536. 0. 536. 536. 0. 536. 1500. 0. 0. 0. .36 62. 8.6 A 21.6 12.8 *
 * 4 1 1500. 0. 0. 536. 0. 0. 536. 1500. 0. 0. 0. .36 62. 8.6 A 21.6 12.8 *
 * 5 1 1400. 0. 0. 536. 0. 0. 536. 1500. 0. 0. 0. .36 62. 8.6 A 21.6 12.8 *
 * 6 1 1500. 0. 0. 536. 0. 0. 536. 1500. 0. 0. 0. .36 62. 8.6 A 21.6 12.8 *
 * 7 1 1300. 0. 536. 536. 0. 536. 536. 1500. 0. 0. 0. .36 62. 8.6 A 21.6 12.8 *
 * 8 *
 * 9 *
 * 10 *
 * 11 *
 * 12 *
 * 13 *
 * 14 *
 * 15 *
 * 16 *
 * 17 *
 * 18 *
 * 19 *
 * 20 *
 *
 *
 * TOTAL 16700. = 3.2 MILES MAX(V/C) = 0.36 LOWEST LOS = A AVG = 62. 8.6 21.6 12.8 *
 *

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 14. VEH-HRS | 88. VEH-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 14. VEH-HRS | 88. VEH-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 848. VEH-MI. | 5465. VEH-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH | 62. MPH |
| AVERAGE DENSITY = | 9. VPMP | 9. VPMP |
| TOTAL FUEL = | 39. GALLONS | 254. GALLONS |
| TOTAL EMISSIONS = | 11. KILOGRAMS | 70. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.42 | 4 | 0.06 | 5 | 0.05 |
| 6 | 0.06 | 7 | 0.05 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 0.6 VEH-HRS ***** AVERAGE DELAY = 0.07 MIN/VEH *****

 **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN *
 * 1 2 3 4 5 6 7 8 *
 Page 8

Table with 8 columns of numerical data, likely representing traffic metrics for different lanes or segments.

TIME SLICE FREEWAY PERFORMANCE TABLE

Table with 15 columns: SUB NO., SSEC, O-D DATA, DEMANDS, ADJUSTED VOLUMES, SSEC, WEAVE, CONGEST, STORAGE, V/C, SPEED, DENSITY, LOS, FUEL, EMISSIONS. It lists performance metrics for various freeway segments.

TOTAL 137309. = 26.0 MILES MAX(V/C) = 0.91 LOWEST LOS = D AVG = 64. 19.6 19.2 13.9

Summary table with columns for CURRENT TIME SLICE and CUMULATIVE VALUES, including metrics like FREeway TRAVEL TIME, MERGE DELAY, RAMP DELAY, SYSTEM TRAVEL TIME, DISTANCE, AVERAGE SPEED, FUEL, and EMISSIONS.

Table showing MAINTENANCE DELAY (VEH-HRS) and DESIRED SPEED = 65.0. It lists delays for subsections 1 through 20.

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|-------|-----------------------|-------|-------|-------|-------|-------|-------|---|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 17.57 | 0.00 | 20.76 | 21.31 | 21.32 | 21.50 | 22.03 | 24.22 | |
| * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| * 3 * | 0.00 | 0.00 | 1.17 | 1.72 | 1.73 | 1.92 | 2.45 | 4.63 | |
| * 4 * | 0.00 | 0.00 | 0.64 | 1.19 | 1.20 | 1.38 | 1.92 | 4.10 | |
| * 5 * | 0.00 | 0.00 | 0.09 | 0.64 | 0.65 | 0.83 | 1.36 | 3.55 | |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.12 | 0.13 | 0.31 | 0.85 | 3.03 | |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 | 0.71 | 2.89 | |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.53 | 2.71 | |

 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | |
|-----------|--------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|--------|---------|-----------|--------|---------|-------------|---------|------|------|
| * SEC | * LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | |
| * 1 | 3 | 500. | 3570. | 0. | 3570. | 3570. | 0. | 3570. | 6000. | 0. | 0. | 0. | .60 | 65. | 18.3 | C | 19.0 | 14.1 |
| * 2 | 3 | 99999. | 0. | 571. | 3570. | 0. | 571. | 3570. | 6000. | 0. | 0. | 0. | .60 | 65. | 18.3 | C | 19.0 | 14.1 |
| * 3 | 2 | 11000. | 0. | 0. | 2999. | 0. | 0. | 2999. | 4000. | 0. | 0. | 0. | .75 | 62. | 24.2 | C | 20.3 | 13.0 |
| * 4 | 2 | 1500. | 40. | 0. | 3039. | 40. | 0. | 3039. | 4000. | 0. | 0. | 0. | .76 | 62. | 24.5 | C | 20.3 | 13.0 |
| * 5 | 2 | 1400. | 0. | 0. | 3039. | 0. | 0. | 3039. | 4000. | 0. | 0. | 0. | .76 | 62. | 24.5 | C | 20.3 | 13.0 |
| * 6 | 2 | 1500. | 590. | 0. | 3629. | 590. | 0. | 3629. | 4000. | 0. | 0. | 0. | .91 | 57. | 31.6 | D | 22.1 | 11.9 |
| * 7 | 2 | 1300. | 0. | 0. | 3629. | 0. | 0. | 3629. | 4000. | 0. | 0. | 0. | .91 | 57. | 31.6 | D | 22.1 | 11.9 |
| * 8 | 3 | 500. | 571. | 750. | 4200. | 571. | 750. | 4200. | 4950. | 0. | 0. | 0. | .85 | 65. | 21.5 | C | 19.0 | 14.1 |
| * 9 | 2 | 2300. | 0. | 0. | 3450. | 0. | 0. | 3450. | 4000. | 0. | 0. | 0. | .86 | 61. | 28.3 | D | 20.9 | 12.7 |
| * 10 | 3 | 250. | 551. | 0. | 4001. | 551. | 0. | 4001. | 4750. | 0. | 0. | 0. | .84 | 65. | 20.5 | C | 19.0 | 14.1 |
| * 11 | 3 | 200. | 0. | 0. | 4001. | 0. | 0. | 4001. | 4750. | 0. | 0. | 0. | .84 | 65. | 20.5 | C | 19.0 | 14.1 |
| * 12 | 3 | 250. | 0. | 1750. | 4001. | 0. | 1750. | 4001. | 4750. | 0. | 0. | 0. | .84 | 65. | 20.5 | C | 19.0 | 14.1 |
| * 13 | 2 | 50. | 0. | 0. | 2251. | 0. | 0. | 2251. | 4000. | 0. | 0. | 0. | .56 | 65. | 17.3 | B | 19.0 | 14.1 |
| * 14 | 2 | 50. | 0. | 0. | 2251. | 0. | 0. | 2251. | 2470. | 0. | 0. | 0. | .91 | 65. | 17.3 | B | 19.0 | 14.1 |
| * 15 | 2 | 1000. | 0. | 0. | 2251. | 0. | 0. | 2251. | 4000. | 0. | 0. | 0. | .56 | 65. | 17.3 | B | 19.0 | 14.1 |
| * 16 | 2 | 10. | 0. | 0. | 2251. | 0. | 0. | 2251. | 4000. | 0. | 0. | 0. | .56 | 65. | 17.3 | B | 19.0 | 14.1 |
| * 17 | 2 | 1500. | 691. | 0. | 2942. | 691. | 0. | 2942. | 4000. | 0. | 0. | 0. | .74 | 64. | 22.8 | C | 19.2 | 13.9 |
| * 18 | 2 | 1500. | 0. | 300. | 2942. | 0. | 300. | 2942. | 4000. | 0. | 0. | 0. | .74 | 64. | 22.8 | C | 19.2 | 13.9 |
| * 19 | 2 | 12000. | 0. | 0. | 2642. | 0. | 0. | 2642. | 4000. | 0. | 0. | 0. | .66 | 65. | 20.3 | C | 19.0 | 14.1 |
| * 20 | 3 | 500. | 0. | 2642. | 2642. | 0. | 2642. | 2642. | 6000. | 0. | 0. | 0. | .44 | 65. | 13.5 | B | 19.0 | 14.1 |

 *
 * TOTAL 137309. = 26.0 MILES MAX(V/C) = 0.91 LOWEST LOS = D AVG = 64. 19.6 19.2 13.9 *
 *

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|---|
| FREWAY TRAVEL TIME = | 687. VEH-HRS | 785. PASS-HRS 1375. VEH-HRS 1570. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 687. VEH-HRS | 785. PASS-HRS 1375. VEH-HRS 1570. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 44311. VEH-MI. | 50642. PASS-MI. 88622. VEH-MI. 101285. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 64. MPH. | 64. MPH. |
| AVERAGE DENSITY = | 20. VPMP | 20. VPMP |
| TOTAL FUEL = | 2310. GALLONS | 4620. GALLONS |
| TOTAL EMISSIONS = | 616. KILOGRAMS | 1232. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 2.33 | 4 | 0.32 | 5 | 0.30 |
| 6 | 1.04 | 7 | 0.90 | 8 | 0.00 | 9 | 0.76 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.06 | 18 | 0.06 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 5.8 VEH-HRS ***** AVERAGE DELAY = 0.11 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/ 3/2016 15: 8 PAGE 28
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF NON-PRIORITY LANES
 TIME SLICE 3 OF 6

 **
 ** FREEWAY TRAVEL TIME (MINUTES)
 **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|-------|-----------------------|-------|-------|-------|-------|-------|-------|---|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 17.57 | 0.00 | 20.88 | 22.04 | 22.11 | 22.29 | 22.84 | 25.02 | |
| * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| * 3 * | 0.00 | 0.00 | 1.25 | 2.41 | 2.48 | 2.66 | 3.21 | 5.39 | |
| * 4 * | 0.00 | 0.00 | 0.71 | 1.87 | 1.93 | 2.12 | 2.66 | 4.85 | |
| * 5 * | 0.00 | 0.00 | 0.10 | 1.26 | 1.32 | 1.51 | 2.05 | 4.24 | |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.40 | 0.47 | 0.65 | 1.19 | 3.38 | |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 | 0.72 | 2.91 | |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.54 | 2.73 | |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/ 3/2016 15: 8 PAGE 29
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF NON-PRIORITY LANES
 TIME SLICE 3 OF 6

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB | * NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | |
|--|-------|----------|------------|-----------|------------|-----------|---------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|--------|--------|--------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * CAP. | * EFF | * LENGTH | * RATE | * MPH | * VP/PL | * LEVEL | * MPG | * GS/VM | | | |
| * 1 | * 3 | * 500. | * 3879. | * 0. | * 3879. | * 3879. | * 0. | * 3879. | * 6000. | * 0. | * 0. | * .65 | * 65. | * 19.9 | * C | * 19.0 | * 14.1 | | |
| * 2 | * 3 | * 99999. | * 0. | * 621. | * 3879. | * 0. | * 621. | * 3879. | * 6000. | * 0. | * 0. | * .65 | * 65. | * 19.9 | * C | * 19.0 | * 14.1 | | |
| * 3 | * 2 | * 11000. | * 0. | * 0. | * 3258. | * 0. | * 0. | * 3258. | * 4000. | * 0. | * 0. | * .81 | * 61. | * 26.8 | * D | * 21.0 | * 12.6 | | |
| * 4 | * 2 | * 1500. | * 50. | * 0. | * 3308. | * 50. | * 0. | * 3308. | * 4000. | * 0. | * 0. | * .83 | * 60. | * 27.4 | * D | * 21.2 | * 12.5 | | |
| * 5 | * 2 | * 1400. | * 0. | * 0. | * 3308. | * 0. | * 0. | * 3308. | * 4000. | * 0. | * 0. | * .83 | * 60. | * 27.4 | * D | * 21.2 | * 12.5 | | |
| * 6 | * 2 | * 1500. | * 660. | * 0. | * 3968. | * 660. | * 0. | * 3968. | * 4000. | * 0. | * 0. | * .99 | * 52. | * 38.0 | * E | * 23.5 | * 11.2 | | |
| * 7 | * 2 | * 1300. | * 0. | * 0. | * 3968. | * 0. | * 0. | * 3968. | * 4000. | * 0. | * 0. | * .99 | * 52. | * 38.0 | * E | * 23.5 | * 11.2 | | |
| * 8 | * 3 | * 500. | * 621. | * 950. | * 4589. | * 621. | * 950. | * 4589. | * 4950. | * 0. | * 0. | * .93 | * 58. | * 26.5 | * D | * 22.1 | * 11.9 | | |
| * 9 | * 2 | * 2300. | * 0. | * 0. | * 3639. | * 0. | * 0. | * 3482. | * 4000. | * 0. | * 2217. | * 157. | * .87 | * 34. | * 50.5 | * F | * 20.2 | * 13.7 | |
| * 10 | * 3 | * 250. | * 572. | * 0. | * 4211. | * 572. | * 0. | * 4054. | * 4750. | * 0. | * ** | * 250. | * 157. | * .85 | * 22. | * 62.4 | * F | * 17.5 | * 16.7 |
| * 11 | * 3 | * 200. | * 0. | * 0. | * 4211. | * 0. | * 0. | * 4054. | * 4750. | * 0. | * ** | * 200. | * 157. | * .85 | * 20. | * 67.8 | * F | * 17.3 | * 17.0 |
| * 12 | * 3 | * 250. | * 0. | * 1560. | * 4211. | * 0. | * 1560. | * 4054. | * 4750. | * 0. | * ** | * 250. | * 157. | * .85 | * 18. | * 73.2 | * F | * 17.2 | * 17.3 |
| * 13 | * 2 | * 50. | * 0. | * 24. | * 2651. | * 0. | * 24. | * 2494. | * 4000. | * 0. | * ** | * 50. | * 157. | * .62 | * 9. | * 146.6 | * F | * 11.1 | * 24.7 |
| * 14 | * 2 | * 50. | * 0. | * 0. | * 2627. | * 0. | * 0. | * 2470. | * 2470. | * 0. | * 0. | * 0. | * 1.00 | * 65. | * 19.0 | * E | * 19.0 | * 14.1 | |
| * 15 | * 2 | * 1000. | * 25. | * 0. | * 2652. | * 25. | * 0. | * 2495. | * 4000. | * 0. | * 0. | * .62 | * 65. | * 19.2 | * C | * 19.0 | * 14.1 | | |
| * 16 | * 2 | * 10. | * 0. | * 0. | * 2652. | * 0. | * 0. | * 2495. | * 4000. | * 0. | * 0. | * .62 | * 65. | * 19.2 | * C | * 19.0 | * 14.1 | | |
| * 17 | * 2 | * 1500. | * 757. | * 0. | * 3409. | * 757. | * 0. | * 3252. | * 4000. | * 0. | * 0. | * .81 | * 63. | * 25.9 | * C | * 20.0 | * 13.3 | | |
| * 18 | * 2 | * 1500. | * 0. | * 689. | * 3409. | * 0. | * 657. | * 3252. | * 4000. | * 0. | * 0. | * .81 | * 63. | * 25.9 | * C | * 20.0 | * 13.3 | | |
| * 19 | * 2 | * 12000. | * 0. | * 0. | * 2720. | * 0. | * 0. | * 2595. | * 4000. | * 0. | * 0. | * .65 | * 65. | * 20.0 | * C | * 19.0 | * 14.1 | | |
| * 20 | * 3 | * 500. | * 0. | * 2720. | * 2720. | * 0. | * 2595. | * 2595. | * 6000. | * 0. | * 0. | * .43 | * 65. | * 13.3 | * B | * 19.0 | * 14.1 | | |
| ***** | | | | | | | | | | | | | | | | | | | |
| * TOTAL 137309. = 26.0 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 62. 21.9 19.3 13.9 * | | | | | | | | | | | | | | | | | | | |
| ***** | | | | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 766. VEH-HRS | 875. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 766. VEH-HRS | 875. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 47798. VEH-MI. | 54621. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 64. MPH. |
| AVERAGE DENSITY = | 22. VP/PL | 20. VP/PL |
| TOTAL FUEL = | 2481. GALLONS | 7101. GALLONS |
| TOTAL EMISSIONS = | 662. KI LOGRAMS | 1894. KI LOGRAMS |

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***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 3.70 | 4 | 0.55 | 5 | 0.51 |
| 6 | 2.13 | 7 | 1.85 | 8 | 0.43 | 9 | 10.65 | 10 | 2.99 |
| 11 | 2.69 | 12 | 3.73 | 13 | 1.21 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.25 | 18 | 0.25 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 30.9 VEH-HRS ***** AVERAGE DELAY = 0.51 MIN/VEH *****

 ** FREeway TRAVEL TIME (MINUTES) **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN *
 * 1 2 3 4 5 6 7 8 *

| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|---|-------|------|-------|-------|-------|-------|-------|-------|
| 1 | 17.57 | 0.00 | 21.46 | 23.34 | 23.41 | 23.60 | 24.14 | 26.33 |
| 2 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3 | 0.00 | 0.00 | 1.83 | 3.72 | 3.78 | 3.97 | 4.51 | 6.70 |
| 4 | 0.00 | 0.00 | 1.23 | 3.11 | 3.18 | 3.37 | 3.91 | 6.10 |
| 5 | 0.00 | 0.00 | 0.26 | 2.15 | 2.21 | 2.40 | 2.94 | 5.13 |
| 6 | 0.00 | 0.00 | 0.00 | 0.46 | 0.53 | 0.71 | 1.26 | 3.44 |
| 7 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 | 0.72 | 2.91 |
| 8 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.54 | 2.73 |

 TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB * SEC | NO. LNS | SSEC LENGTH | O-D DATA ORG DES | DEMANDS SSEC | ADJUSTED ORG DES | VOLUMES SSEC | SSEC CAP. | WEAVE EFF | CONGEST LENGTH | STORAGE RATE | V/C RATIO | SPEED MPH | DENSITY VPMP | LOS LEVEL | FUEL MPG | EMISS GS/VM | | | |
|----------------|------------|----------------|---------------------|-----------------|---------------------|-----------------|--------------|--------------|-------------------|-----------------|--------------|--------------|-----------------|--------------|-------------|----------------|------|------|------|
| * 1 | 3 | 500. | 3879. | 0. | 3879. | 3879. | 0. | 3879. | 6000. | 0. | 0. | 0. | .65 | 65. | 19.9 | C | 19.0 | 14.1 | |
| * 2 | 3 | 99999. | 0. | 621. | 3879. | 0. | 621. | 3879. | 6000. | 0. | 0. | 0. | .65 | 65. | 19.9 | C | 19.0 | 14.1 | |
| * 3 | 2 | 11000. | 0. | 0. | 3258. | 0. | 0. | 3258. | 4000. | 0. | 0. | 0. | .81 | 61. | 26.8 | D | 21.0 | 12.6 | |
| * 4 | 2 | 1500. | 50. | 0. | 3308. | 50. | 0. | 3308. | 4000. | 0. | 0. | 0. | .83 | 60. | 27.4 | D | 21.2 | 12.5 | |
| * 5 | 2 | 1400. | 0. | 0. | 3308. | 0. | 0. | 3151. | 4000. | 0. | * | 673. | 157. | .79 | 50. | 31.6 | F | 20.7 | 13.0 |
| * 6 | 2 | 1500. | 660. | 0. | 3968. | 660. | 0. | 3811. | 4000. | 0. | ** | 1500. | 157. | .95 | 36. | 53.0 | F | 21.8 | 12.4 |
| * 7 | 2 | 1300. | 0. | 0. | 3968. | 0. | 0. | 3811. | 4000. | 0. | ** | 1300. | 157. | .95 | 30. | 63.7 | F | 20.9 | 13.2 |
| * 8 | 3 | 500. | 621. | 950. | 4589. | 621. | 950. | 4432. | 4950. | 0. | ** | 500. | 157. | .90 | 22. | 68.3 | F | 18.6 | 15.6 |
| * 9 | 2 | 2300. | 0. | 0. | 3639. | 0. | 0. | 3482. | 4000. | 0. | ** | 2300. | 157. | .87 | 18. | 94.8 | F | 17.5 | 17.1 |
| * 10 | 3 | 250. | 572. | 0. | 4211. | 572. | 0. | 4054. | 4750. | 0. | ** | 250. | 157. | .85 | 17. | 78.1 | F | 17.0 | 17.6 |
| * 11 | 3 | 200. | 0. | 0. | 4211. | 0. | 0. | 4054. | 4750. | 0. | ** | 200. | 157. | .85 | 17. | 78.1 | F | 17.0 | 17.6 |
| * 12 | 3 | 250. | 0. | 1560. | 4211. | 0. | 1560. | 4054. | 4750. | 0. | ** | 250. | 157. | .85 | 17. | 78.1 | F | 17.0 | 17.6 |
| * 13 | 2 | 50. | 0. | 24. | 2651. | 0. | 24. | 2494. | 4000. | 0. | ** | 50. | 157. | .62 | 8. | 148.7 | F | 11.0 | 24.8 |
| * 14 | 2 | 50. | 0. | 0. | 2627. | 0. | 0. | 2470. | 2470. | 0. | 0. | 0. | 1.00 | 65. | 19.0 | E | 19.0 | 14.1 | |
| * 15 | 2 | 1000. | 25. | 0. | 2652. | 25. | 0. | 2495. | 4000. | 0. | 0. | 0. | .62 | 65. | 19.2 | C | 19.0 | 14.1 | |
| * 16 | 2 | 10. | 0. | 0. | 2652. | 0. | 0. | 2495. | 4000. | 0. | 0. | 0. | .62 | 65. | 19.2 | C | 19.0 | 14.1 | |
| * 17 | 2 | 1500. | 757. | 0. | 3409. | 757. | 0. | 3252. | 4000. | 0. | 0. | 0. | .81 | 63. | 25.9 | C | 20.0 | 13.3 | |
| * 18 | 2 | 1500. | 0. | 689. | 3409. | 0. | 657. | 3252. | 4000. | 0. | 0. | 0. | .81 | 63. | 25.9 | C | 20.0 | 13.3 | |
| * 19 | 2 | 12000. | 0. | 0. | 2720. | 0. | 0. | 2595. | 4000. | 0. | 0. | 0. | .65 | 65. | 20.0 | C | 19.0 | 14.1 | |
| * 20 | 3 | 500. | 0. | 2720. | 2720. | 0. | 2595. | 2595. | 6000. | 0. | 0. | 0. | .43 | 65. | 13.3 | B | 19.0 | 14.1 | |

 * TOTAL 137309. = 26.0 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 59. 23.3 19.2 14.0 *

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 806. VEH-HRS | 919. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 806. VEH-HRS | 919. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 47742. VEH-MI. | 54560. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 59. MPH. | 62. MPH. |

AVERAGE DENSITY = 23. VPML
 TOTAL FUEL = 2492. GALLONS
 TOTAL EMISSIONS = 667. KILOGRAMS

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 21. VPML
 9593. GALLONS
 2561. KILOGRAMS

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 TIME SLICE 4 OF 6

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 3.70 | 4 | 0.55 | 5 | 2.05 |
| 6 | 6.90 | 7 | 8.58 | 8 | 6.50 | 9 | 29.65 | 10 | 4.07 |
| 11 | 3.25 | 12 | 4.07 | 13 | 1.23 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.25 | 18 | 0.25 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 71.0 VEH-HRS ***** AVERAGE DELAY = 1.17 MIN/VEH *****

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 TIME SLICE 5 OF 6

QUEUE CLEAR SECTION 13 T2= 0.465

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 TIME SLICE 5 OF 6

 ** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGIN | * DESTINATIONS ACROSS * | | | | | | | |
|----------|-------------------------|------|-------|-------|-------|-------|-------|-------|
| * DOWN | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 17.57 | 0.00 | 21.13 | 22.59 | 22.64 | 22.82 | 23.40 | 25.61 |
| * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 3 * | 0.00 | 0.00 | 1.54 | 3.00 | 3.05 | 3.24 | 3.81 | 6.02 |
| * 4 * | 0.00 | 0.00 | 0.99 | 2.45 | 2.50 | 2.68 | 3.26 | 5.46 |
| * 5 * | 0.00 | 0.00 | 0.20 | 1.66 | 1.72 | 1.90 | 2.47 | 4.68 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.43 | 0.48 | 0.67 | 1.24 | 3.45 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 | 0.75 | 2.96 |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.57 | 2.78 |

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TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | |
|-----------|--------|------------|-----------|------------|-----------|---------|---------|-----------|-----------|-------|----------|-----------|---------|--------|-------------|---------|--------|---------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPML | * LEVEL | * MPG | * GS/VM |
| * 1 | * 3 | * 500. | * 3350. | * 0. | * 3350. | * 3350. | * 0. | * 3350. | * 6000. | * 0. | * 0. | * 0. | * .56 | * 65. | * 17.2 | * B | * 19.0 | * 14.1 |
| * 2 | * 3 | * 99999. | * 0. | * 536. | * 3350. | * 0. | * 536. | * 3350. | * 6000. | * 0. | * 0. | * .56 | * 65. | * 17.2 | * B | * 19.0 | * 14.1 | * 14.1 |
| * 3 | * 2 | * 11000. | * 0. | * 0. | * 2814. | * 0. | * 0. | * 2814. | * 4000. | * 0. | * 0. | * 0. | * .70 | * 62. | * 22.7 | * C | * 20.3 | * 13.0 |
| * 4 | * 2 | * 1500. | * 51. | * 0. | * 2865. | * 51. | * 0. | * 2865. | * 4000. | * 0. | * 0. | * 0. | * .72 | * 62. | * 23.1 | * C | * 20.3 | * 13.0 |
| * 5 | * 2 | * 1400. | * 0. | * 0. | * 2865. | * 0. | * 0. | * 2865. | * 4000. | * 0. | * 0. | * 0. | * .72 | * 57. | * 25.2 | * C | * 20.2 | * 13.2 |
| * 6 | * 2 | * 1500. | * 440. | * 0. | * 3305. | * 440. | * 0. | * 3305. | * 4000. | * 0. | * 0. | * 0. | * .83 | * 44. | * 37.2 | * E | * 20.6 | * 13.1 |
| * 7 | * 2 | * 1300. | * 0. | * 0. | * 3305. | * 0. | * 0. | * 3305. | * 4000. | * 0. | * 0. | * 0. | * .83 | * 37. | * 44.7 | * E | * 20.3 | * 13.5 |
| * 8 | * 3 | * 500. | * 536. | * 671. | * 3841. | * 536. | * 671. | * 3841. | * 4950. | * 0. | * 0. | * 0. | * .78 | * 28. | * 45.6 | * F | * 18.0 | * 15.8 |
| * 9 | * 2 | * 2300. | * 0. | * 0. | * 3170. | * 0. | * 0. | * 3170. | * 4000. | * 0. | * 0. | * 0. | * .79 | * 25. | * 62.5 | * F | * 18.6 | * 15.4 |
| * 10 | * 3 | * 250. | * 440. | * 0. | * 3610. | * 440. | * 0. | * 3610. | * 4750. | * 0. | * 0. | * 0. | * .76 | * 19. | * 63.1 | * F | * 17.1 | * 17.3 |
| * 11 | * 3 | * 200. | * 0. | * 0. | * 3610. | * 0. | * 0. | * 3610. | * 4750. | * 0. | * 0. | * 0. | * .76 | * 18. | * 65.1 | * F | * 17.0 | * 17.5 |
| * 12 | * 3 | * 250. | * 0. | * 1271. | * 3610. | * 0. | * 1271. | * 3610. | * 4750. | * 0. | * 0. | * 0. | * .76 | * 18. | * 67.1 | * F | * 16.9 | * 17.6 |
| * 13 | * 2 | * 50. | * 0. | * 260. | * 2339. | * 0. | * 260. | * 2730. | * 4000. | * 0. | * 0. | * -391. | * .68 | * 11. | * 128.4 | * F | * 13.3 | * 22.3 |
| * 14 | * 2 | * 50. | * 0. | * 0. | * 2079. | * 0. | * 0. | * 2470. | * 2470. | * 0. | * 0. | * 0. | * 1.00 | * 65. | * 19.0 | * E | * 19.0 | * 14.1 |
| * 15 | * 2 | * 1000. | * 260. | * 0. | * 2339. | * 260. | * 0. | * 2730. | * 4000. | * 0. | * 0. | * 0. | * .68 | * 65. | * 21.0 | * C | * 19.0 | * 14.1 |
| * 16 | * 2 | * 10. | * 0. | * 0. | * 2339. | * 0. | * 0. | * 2730. | * 4000. | * 0. | * 0. | * 0. | * .68 | * 65. | * 21.0 | * C | * 19.0 | * 14.1 |
| * 17 | * 2 | * 1500. | * 832. | * 0. | * 3171. | * 832. | * 0. | * 3562. | * 4000. | * 0. | * 0. | * 0. | * .89 | * 60. | * 29.8 | * D | * 21.5 | * 12.3 |
| * 18 | * 2 | * 1500. | * 0. | * 529. | * 3171. | * 0. | * 594. | * 3562. | * 4000. | * 0. | * 0. | * 0. | * .89 | * 60. | * 29.8 | * D | * 21.5 | * 12.3 |
| * 19 | * 2 | * 12000. | * 0. | * 0. | * 2642. | * 0. | * 0. | * 2968. | * 4000. | * 0. | * 0. | * 0. | * .74 | * 64. | * 23.1 | * C | * 19.3 | * 13.8 |

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* 20 3 500. 0. 2642. 2642. 0. 2968. 2968. 6000. 0. 0. 0. .49 65. 15.2 B 19.0 14.1 *
*
*****
* TOTAL 137309. = 26.0 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 61. 20.2 19.2 14.0 *
*
*****

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CURRENT TIME SLICE CUMULATIVE VALUES
FREEWAY TRAVEL TIME = 701. VEH-HRS 800. PASS-HRS 3647. VEH-HRS 4164. PASS-HRS
FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 701. VEH-HRS 800. PASS-HRS 3647. VEH-HRS 4164. PASS-HRS
TOTAL FRWAY TRAV DI STANCE = 42513. VEH-MI . 48599. PASS-MI . 226675. VEH-MI . 259064. PASS-MI .
AVERAGE SYSTEM SPEED = 61. MPH 62. MPH
AVERAGE DENSITY = 20. VPMP 21. VPMP
TOTAL FUEL = 2218. GALLONS 11811. GALLONS
TOTAL EMISSIONS = 593. KILOGRAMS 3154. KILOGRAMS

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***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
1 0.00 2 0.00 3 2.18 4 0.30 5 0.85
6 3.41 7 4.93 8 3.86 9 17.93 10 3.45
11 2.89 12 3.79 13 1.01 14 0.00 15 0.00
16 0.00 17 0.69 18 0.69 19 0.56 20 0.00
***** TOTAL DELAY = 46.5 VEH-HRS ***** AVERAGE DELAY = 0.85 MIN/VEH *****

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UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF NON-PRIORITY LANES
TIME SLICE 6 OF 6

```

*****
** FREEWAY TRAVEL TIME (MINUTES) **
*****

```

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | | |
|-----------------|---------------------|------|-------|-------|-------|-------|-------|-------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| 1 | 17.57 | 0.00 | 20.73 | 21.27 | 21.28 | 21.46 | 22.00 | 24.18 |
| 2 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3 | 0.00 | 0.00 | 1.15 | 1.68 | 1.69 | 1.87 | 2.41 | 4.60 |
| 4 | 0.00 | 0.00 | 0.61 | 1.15 | 1.16 | 1.34 | 1.88 | 4.07 |
| 5 | 0.00 | 0.00 | 0.09 | 0.62 | 0.63 | 0.81 | 1.36 | 3.54 |
| 6 | 0.00 | 0.00 | 0.00 | 0.12 | 0.13 | 0.31 | 0.85 | 3.04 |
| 7 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 | 0.72 | 2.90 |
| 8 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.54 | 2.72 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/ 3/2016 15: 8 PAGE 39
UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF NON-PRIORITY LANES
TIME SLICE 6 OF 6

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB NO. | SSEC | O-D DATA | ADJUSTED | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS |
|---------|------|----------|----------|------|-------|---------|---------|-------|-------|---------|-------|------|--------|
| SEC | LNS | LENGTH | ORG | DES | EFF | LENGTH | RATE | RATIO | MPH | VPMP | LEVEL | MPG | GS/VM |
| 1 | 3 | 500. | 3350. | 0. | 3350. | 3350. | 0. | 3350. | 6000. | 0. | 0. | 0. | 0. |
| 2 | 3 | 99999. | 0. | 536. | 3350. | 0. | 536. | 3350. | 6000. | 0. | 0. | 0. | 0. |
| 3 | 2 | 11000. | 0. | 0. | 2814. | 0. | 0. | 2814. | 4000. | 0. | 0. | 0. | 0. |
| 4 | 2 | 1500. | 51. | 0. | 2865. | 51. | 0. | 2865. | 4000. | 0. | 0. | 0. | 0. |
| 5 | 2 | 1400. | 0. | 0. | 2865. | 0. | 0. | 2865. | 4000. | 0. | 0. | 0. | 0. |
| 6 | 2 | 1500. | 440. | 0. | 3305. | 440. | 0. | 3305. | 4000. | 0. | 0. | 0. | 0. |
| 7 | 2 | 1300. | 0. | 0. | 3305. | 0. | 0. | 3305. | 4950. | 0. | 0. | 0. | 0. |
| 8 | 3 | 500. | 536. | 671. | 3841. | 536. | 671. | 3841. | 4950. | 0. | 0. | 0. | 0. |
| 9 | 2 | 2300. | 0. | 0. | 3170. | 0. | 0. | 3170. | 4000. | 0. | 0. | 0. | 0. |

SR-237_WB_PM_NP_MOD_2018_PL_2.txt

| | | | | | | | | | | | | | | | | | | | |
|--|---|--------|------|-------|-------|------|-------|-------|-------|----|----|----|-----|-----|------|---|------|------|---|
| *10 | 3 | 250. | 440. | 0. | 3610. | 440. | 0. | 3610. | 4750. | 0. | 0. | 0. | .76 | 65. | 18.5 | C | 19.0 | 14.1 | * |
| *11 | 3 | 200. | 0. | 0. | 3610. | 0. | 0. | 3610. | 4750. | 0. | 0. | 0. | .76 | 65. | 18.5 | C | 19.0 | 14.1 | * |
| *12 | 3 | 250. | 0. | 1271. | 3610. | 0. | 1271. | 3610. | 4750. | 0. | 0. | 0. | .76 | 65. | 18.5 | C | 19.0 | 14.1 | * |
| *13 | 2 | 50. | 0. | 260. | 2339. | 0. | 260. | 2339. | 4000. | 0. | 0. | 0. | .58 | 65. | 18.0 | B | 19.0 | 14.1 | * |
| *14 | 2 | 50. | 0. | 0. | 2079. | 0. | 0. | 2079. | 2470. | 0. | 0. | 0. | .84 | 65. | 16.0 | B | 19.0 | 14.1 | * |
| *15 | 2 | 1000. | 260. | 0. | 2339. | 260. | 0. | 2339. | 4000. | 0. | 0. | 0. | .58 | 65. | 18.0 | B | 19.0 | 14.1 | * |
| *16 | 2 | 10. | 0. | 0. | 2339. | 0. | 0. | 2339. | 4000. | 0. | 0. | 0. | .58 | 65. | 18.0 | B | 19.0 | 14.1 | * |
| *17 | 2 | 1500. | 832. | 0. | 3171. | 832. | 0. | 3171. | 4000. | 0. | 0. | 0. | .79 | 63. | 25.0 | C | 19.7 | 13.5 | * |
| *18 | 2 | 1500. | 0. | 529. | 3171. | 0. | 529. | 3171. | 4000. | 0. | 0. | 0. | .79 | 63. | 25.0 | C | 19.7 | 13.5 | * |
| *19 | 2 | 12000. | 0. | 0. | 2642. | 0. | 0. | 2642. | 4000. | 0. | 0. | 0. | .66 | 65. | 20.3 | C | 19.0 | 14.1 | * |
| *20 | 3 | 500. | 0. | 2642. | 2642. | 0. | 2642. | 2642. | 6000. | 0. | 0. | 0. | .44 | 65. | 13.5 | B | 19.0 | 14.1 | * |
| ***** | | | | | | | | | | | | | | | | | | | |
| * TOTAL 137309. = 26.0 MILES MAX(V/C) = 0.84 LOWEST LOS = D AVG = 65. 18.5 19.2 13.9 * | | | | | | | | | | | | | | | | | | | |
| ***** | | | | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | | CUMULATIVE VALUES |
|------------------------------|--------------------|-----------------|----------------------------------|
| FREEWAY TRAVEL TIME = | 648. VEH-HRS | 741. PASS-HRS | 4296. VEH-HRS 4904. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 648. VEH-HRS | 741. PASS-HRS | 4296. VEH-HRS 4904. PASS-HRS |
| TOTAL FRWAY TRAV DI STANCE = | 41861. VEH-MI. | 47846. PASS-MI. | 268536. VEH-MI. 306910. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 65. MPH | | 63. MPH |
| AVERAGE DENSITY = | 19. VPMPPL | | 21. VPMPPL |
| TOTAL FUEL = | 2185. GALLONS | | 13996. GALLONS |
| TOTAL EMISSIONS = | 583. KILOGRAMS | | 3736. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 2.18 | 4 | 0.30 | 5 | 0.28 |
| 6 | 0.55 | 7 | 0.47 | 8 | 0.00 | 9 | 0.28 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.18 | 18 | 0.18 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 4.4 VEH-HRS ***** AVERAGE DELAY = 0.09 MIN/VEH *****


```

**
** 8
** 9
** 10
** 11
** 12
** 13
** 14
** 15
** 16
** 17
** 18
** 19
** 20
**
*****
*****

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*****
**
**          FREeway TRAVEL TIME (MINUTES)
**
*****

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| * ORIGIN * DOWN | * DESTINATIONS ACROSS * | | | | | | | |
|--------------------|-------------------------|------|------|------|------|------|------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 3.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISS | | | |
|-----------|--------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|-------|----------|-----------|---------|--------|---------|---------|-------|---------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 1 | | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | | |
| * 3 | 1 | 11000. | 571. | 0. | 571. | 571. | 0. | 571. | 1500. | 0. | 0. | 0. | .38 | 62. | 9.2 | A | 21.6 | 12.8 |
| * 4 | 1 | 1500. | 0. | 0. | 571. | 0. | 0. | 571. | 1500. | 0. | 0. | 0. | .38 | 62. | 9.2 | A | 21.6 | 12.8 |
| * 5 | 1 | 1400. | 0. | 0. | 571. | 0. | 0. | 571. | 1500. | 0. | 0. | 0. | .38 | 62. | 9.2 | A | 21.6 | 12.8 |
| * 6 | 1 | 1500. | 0. | 0. | 571. | 0. | 0. | 571. | 1500. | 0. | 0. | 0. | .38 | 62. | 9.2 | A | 21.6 | 12.8 |
| * 7 | 1 | 1300. | 0. | 571. | 571. | 0. | 571. | 571. | 1500. | 0. | 0. | 0. | .38 | 62. | 9.2 | A | 21.6 | 12.8 |
| * 8 | | | | | | | | | | | | | | | | | | |
| * 9 | | | | | | | | | | | | | | | | | | |
| * 10 | | | | | | | | | | | | | | | | | | |
| * 11 | | | | | | | | | | | | | | | | | | |
| * 12 | | | | | | | | | | | | | | | | | | |
| * 13 | | | | | | | | | | | | | | | | | | |
| * 14 | | | | | | | | | | | | | | | | | | |
| * 15 | | | | | | | | | | | | | | | | | | |
| * 16 | | | | | | | | | | | | | | | | | | |
| * 17 | | | | | | | | | | | | | | | | | | |
| * 18 | | | | | | | | | | | | | | | | | | |
| * 19 | | | | | | | | | | | | | | | | | | |

* 20 *
 * *
 * ***** *
 * TOTAL 16700. = 3.2 MILES MAX(V/C) = 0.38 LOWEST LOS = A AVG = 62. 9.2 21.6 12.8 *
 * ***** *

| | | | |
|------------------------------|--------------------|----------------|-----------------------------|
| | CURRENT TIME SLICE | | CUMULATIVE VALUES |
| FREEWAY TRAVEL TIME = | 15. VEH-HRS | 29. PASS-HRS | 15. VEH-HRS 29. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 15. VEH-HRS | 29. PASS-HRS | 15. VEH-HRS 29. PASS-HRS |
| TOTAL FRWAY TRAV DI STANCE = | 903. VEH-MI. | 1807. PASS-MI. | 903. VEH-MI. 1807. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | | 62. MPH. |
| AVERAGE DENSITY = | 9. VPMP. | | 9. VPMP. |
| TOTAL FUEL = | 42. GALLONS | | 42. GALLONS |
| TOTAL EMISSIONS = | 12. KILOGRAMS | | 12. KILOGRAMS |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/ 3/2016 15:15 PAGE 6
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 1 OF 6

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| | | | | | | | | | |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
| 1 | 0.00 | 2 | 0.00 | 3 | 0.44 | 4 | 0.06 | 5 | 0.06 |
| 6 | 0.06 | 7 | 0.05 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 0.7 VEH-HRS ***** AVERAGE DELAY = 0.07 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/ 3/2016 15:15 PAGE 7
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 6

 ** FREEWAY TRAVEL TIME (MINUTES) **

| | | | | | | | | | |
|---|---------|---------------------|------|------|------|------|------|------|------|
| | ORIGINS | DESTINATIONS ACROSS | | | | | | | |
| | DOWN | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| + | * | ***** | | | | | | | |
| + | * | ***** | | | | | | | |
| + | * | 1 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * | 2 | 0.00 | 3.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * | 3 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * | 4 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * | 5 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * | 6 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * | 7 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * | 8 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * | ***** | | | | | | | |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/ 3/2016 15:15 PAGE 8
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 6

TIME SLICE FREEWAY PERFORMANCE TABLE

| | | | | | | | | | | | | | | | |
|-----------|------|----------|---------|----------|---------|------|-------|---------|---------|-------|-------|---------|-------|------|-------------|
| * SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED | VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS |
| * SEC | LNS | LENGTH | ORG | DES | SSEC | ORG | DES | LENGTH | RATE | RATIO | MPH | VPMP | LEVEL | MPG | GS/VM |
| * 1 | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | |
| * 3 | 1 | 11000. | 571. | 0. | 571. | 571. | 0. | 571. | 1500. | 0. | 0. | .38 | 62. | 9.2 | A 21.6 12.8 |
| * 4 | 1 | 1500. | 0. | 0. | 571. | 0. | 0. | 571. | 1500. | 0. | 0. | .38 | 62. | 9.2 | A 21.6 12.8 |
| * 5 | 1 | 1400. | 0. | 0. | 571. | 0. | 0. | 571. | 1500. | 0. | 0. | .38 | 62. | 9.2 | A 21.6 12.8 |
| * 6 | 1 | 1500. | 0. | 0. | 571. | 0. | 0. | 571. | 1500. | 0. | 0. | .38 | 62. | 9.2 | A 21.6 12.8 |
| * 7 | 1 | 1300. | 0. | 571. | 571. | 0. | 571. | 571. | 1500. | 0. | 0. | .38 | 62. | 9.2 | A 21.6 12.8 |
| * 8 | | | | | | | | | | | | | | | |
| * 9 | | | | | | | | | | | | | | | |

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*10
* 11
* 12
* 13
* 14
* 15
* 16
* 17
* 18
* 19
* 20
*
*****
*
* TOTAL 16700. = 3.2 MILES MAX(V/C) = 0.38 LOWEST LOS = A AVG = 62. 9.2 21.6 12.8
*
*****

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```

CURRENT TIME SLICE CUMULATIVE VALUES
FREEWAY TRAVEL TIME = 15. VEH-HRS 29. PASS-HRS 29. VEH-HRS 58. PASS-HRS
FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 15. VEH-HRS 29. PASS-HRS 29. VEH-HRS 58. PASS-HRS
TOTAL FRWAY TRAV DISTANCE = 903. VEH-MI. 1807. PASS-MI. 1807. VEH-MI. 3613. PASS-MI.
AVERAGE SYSTEM SPEED = 62. MPH. 62. MPH.
AVERAGE DENSITY = 9. VPML 9. VPML
TOTAL FUEL = 42. GALLONS 84. GALLONS
TOTAL EMISSIONS = 12. KILOGRAMS 23. KILOGRAMS

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 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 6

```

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
1 0.00 2 0.00 3 0.44 4 0.06 5 0.06
6 0.06 7 0.05 8 0.00 9 0.00 10 0.00
11 0.00 12 0.00 13 0.00 14 0.00 15 0.00
16 0.00 17 0.00 18 0.00 19 0.00 20 0.00
***** TOTAL DELAY = 0.7 VEH-HRS ***** AVERAGE DELAY = 0.07 MIN/VEH *****

```

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/ 3/2016 15:15 PAGE 10
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 3 OF 6

```

*****
**
** FREeway TRAVEL TIME (MINUTES) **
**
*****

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```

*****
* ORIGINS DESTINATIONS ACROSS *
* DOWN 1 2 3 4 5 6 7 8 *
+
* * * * *
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 2 * 0.00 3.06 0.00 0.00 0.00 0.00 0.00 0.00
+
* 3 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 4 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 5 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 8 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* *
*****

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1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/ 3/2016 15:15 PAGE 11
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 3 OF 6

```

*****
*
* TIME SLICE FREEWAY PERFORMANCE TABLE
*
*****
* SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMISS *
* SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPML LEVEL MPG GS/VM *
*****

```



```

*
* 1
* 2
* 3 1 11000. 621. 0. 621. 621. 0. 621. 1500. 0. 0. 0. .41 62. 10.0 A 21.6 12.8
* 4 1 1500. 0. 0. 621. 0. 0. 621. 1500. 0. 0. 0. .41 62. 10.0 A 21.6 12.8
* 5 1 1400. 0. 0. 621. 0. 0. 621. 1500. 0. 0. 0. .41 62. 10.0 A 21.6 12.8
* 6 1 1500. 0. 0. 621. 0. 0. 621. 1500. 0. 0. 0. .41 62. 10.0 A 21.6 12.8
* 7 1 1300. 0. 621. 621. 0. 621. 621. 1500. 0. 0. 0. .41 62. 10.0 A 21.6 12.8
* 8
* 9
* 10
* 11
* 12
* 13
* 14
* 15
* 16
* 17
* 18
* 19
* 20
*****
*
* TOTAL 16700. = 3.2 MILES MAX(V/C) = 0.41 LOWEST LOS = A AVG = 62. 10.0 21.6 12.8
*
*****

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CURRENT TIME SLICE CUMULATIVE VALUES
FREEWAY TRAVEL TIME = 16. VEH-HRS 32. PASS-HRS 45. VEH-HRS 90. PASS-HRS
FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 16. VEH-HRS 32. PASS-HRS 45. VEH-HRS 90. PASS-HRS
TOTAL FRWAY TRAV DISTANCE = 982. VEH-MI. 1964. PASS-MI. 2789. VEH-MI. 5577. PASS-MI.
AVERAGE SYSTEM SPEED = 62. MPH. 62. MPH.
AVERAGE DENSITY = 10. VPML 9. VPML
TOTAL FUEL = 46. GALLONS 129. GALLONS
TOTAL EMISSIONS = 13. KILOGRAMS 36. KILOGRAMS

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***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
1 0.00 2 0.00 3 0.48 4 0.07 5 0.06
6 0.07 7 0.06 8 0.00 9 0.00 10 0.00
11 0.00 12 0.00 13 0.00 14 0.00 15 0.00
16 0.00 17 0.00 18 0.00 19 0.00 20 0.00
***** TOTAL DELAY = 0.7 VEH-HRS ***** AVERAGE DELAY = 0.07 MIN/VEH *****

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*****
**
** FREeway TRAVEL TIME (MINUTES) **
**
*****

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*****
* ORIGINS DESTINATIONS ACROSS *
* DOWN 1 2 3 4 5 6 7 8 *
+
* * * * *
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 2 * 0.00 3.06 0.00 0.00 0.00 0.00 0.00 0.00
+
* 3 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 4 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 5 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 8 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* * * * *
*****

```

 *
 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *
 *
 *
 * SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMISS *
 * SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMP L LEVEL MPG GS/VM *
 *
 * 1 *
 * 2 *
 * 3 1 11000. 621. 0. 621. 621. 0. 621. 1500. 0. 0. 0. .41 62. 10.0 A 21.6 12.8 *
 * 4 1 1500. 0. 0. 621. 0. 0. 621. 1500. 0. 0. 0. .41 62. 10.0 A 21.6 12.8 *
 * 5 1 1400. 0. 0. 621. 0. 0. 621. 1500. 0. 0. 0. .41 62. 10.0 A 21.6 12.8 *
 * 6 1 1500. 0. 0. 621. 0. 0. 621. 1500. 0. 0. 0. .41 62. 10.0 A 21.6 12.8 *
 * 7 1 1300. 0. 621. 621. 0. 621. 621. 1500. 0. 0. 0. .41 62. 10.0 A 21.6 12.8 *
 * 8 *
 * 9 *
 * 10 *
 * 11 *
 * 12 *
 * 13 *
 * 14 *
 * 15 *
 * 16 *
 * 17 *
 * 18 *
 * 19 *
 * 20 *
 *
 *
 *
 * TOTAL 16700. = 3.2 MILES MAX(V/C) = 0.41 LOWEST LOS = A AVG = 62. 10.0 21.6 12.8 *
 *
 *

| | | |
|-----------------------------|-----------------------------|------------------------------|
| | CURRENT TIME SLICE | CUMULATIVE VALUES |
| FREEWAY TRAVEL TIME = | 16. VEH-HRS 32. PASS-HRS | 61. VEH-HRS 122. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 16. VEH-HRS 32. PASS-HRS | 61. VEH-HRS 122. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 982. VEH-MI. 1964. PASS-MI. | 3771. VEH-MI. 7541. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 62. MPH. |
| AVERAGE DENSITY = | 10. VPMP L | 10. VPMP L |
| TOTAL FUEL = | 46. GALLONS | 175. GALLONS |
| TOTAL EMISSIONS = | 13. KI LOGRAMS | 48. KI LOGRAMS |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 4 OF 6

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.48 | 4 | 0.07 | 5 | 0.06 |
| 6 | 0.07 | 7 | 0.06 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 0.7 VEH-HRS ***** AVERAGE DELAY = 0.07 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/ 3/2016 15:15 PAGE 16
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 5 OF 6

 **
 ** FREeway TRAVEL TIME (MINUTES) **
 **

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | | |
|--------------|---------------------|------|------|------|------|------|------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 3.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB | * NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISS |
|---------|--------|----------|------------|------------|--------------------|--------|---------|-----------------|-----------|----------------|-----------|-----------|---------|--------|---------|
| * SEC | * LNS | * LENGTH | * ORG | * DES SSEC | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 1 | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | |
| * 3 | 1 | 11000. | 536. | 0. 536. | 536. 0. 536. | 1500. | 0. | 0. | 0. | .36 | 62. | 8.6 | A | 21.6 | 12.8 |
| * 4 | 1 | 1500. | 0. | 0. 536. | 0. 0. 536. | 1500. | 0. | 0. | 0. | .36 | 62. | 8.6 | A | 21.6 | 12.8 |
| * 5 | 1 | 1400. | 0. | 0. 536. | 0. 0. 536. | 1500. | 0. | 0. | 0. | .36 | 62. | 8.6 | A | 21.6 | 12.8 |
| * 6 | 1 | 1500. | 0. | 0. 536. | 0. 0. 536. | 1500. | 0. | 0. | 0. | .36 | 62. | 8.6 | A | 21.6 | 12.8 |
| * 7 | 1 | 1300. | 0. | 536. 536. | 0. 536. 536. | 1500. | 0. | 0. | 0. | .36 | 62. | 8.6 | A | 21.6 | 12.8 |
| * 8 | | | | | | | | | | | | | | | |
| * 9 | | | | | | | | | | | | | | | |
| * 10 | | | | | | | | | | | | | | | |
| * 11 | | | | | | | | | | | | | | | |
| * 12 | | | | | | | | | | | | | | | |
| * 13 | | | | | | | | | | | | | | | |
| * 14 | | | | | | | | | | | | | | | |
| * 15 | | | | | | | | | | | | | | | |
| * 16 | | | | | | | | | | | | | | | |
| * 17 | | | | | | | | | | | | | | | |
| * 18 | | | | | | | | | | | | | | | |
| * 19 | | | | | | | | | | | | | | | |
| * 20 | | | | | | | | | | | | | | | |
| * TOTAL | 16700. | = | 3.2 MILES | | | | | MAX(V/C) = 0.36 | | LOWEST LOS = A | AVG = 62. | 8.6 | | 21.6 | 12.8 |

| | | |
|-----------------------------|-----------------------------|------------------------------|
| | CURRENT TIME SLICE | CUMULATIVE VALUES |
| FREEWAY TRAVEL TIME = | 14. VEH-HRS 27. PASS-HRS | 74. VEH-HRS 149. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 14. VEH-HRS 27. PASS-HRS | 74. VEH-HRS 149. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 848. VEH-MI. 1695. PASS-MI. | 4618. VEH-MI. 9237. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 62. MPH. |
| AVERAGE DENSITY = | 9. VPMP | 9. VPMP |
| TOTAL FUEL = | 39. GALLONS | 214. GALLONS |
| TOTAL EMISSIONS = | 11. KILOGRAMS | 59. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.42 | 4 | 0.06 | 5 | 0.05 |
| 6 | 0.06 | 7 | 0.05 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 0.6 VEH-HRS ***** AVERAGE DELAY = 0.07 MIN/VEH *****

 ** FREeway TRAVEL TIME (MINUTES) **

| * ORIGINS | * DESTINATIONS ACROSS * | | | | | | | |
|-----------|-------------------------|------|------|------|------|------|------|------|
| * DOWN | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 3.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

| | | | | | | | | | | | | | | | | | | |
|-------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS | | | | |
|---------|--------|----------|--------------|------------------|------|-------|---------|---------|-------|-------|---------|-------|------|--------|------|------|--|--|
| SEC | LNS | LENGTH | ORG DES SSEC | ORG DES SSEC | CAP. | EFF | LENGTH | RATE | RATIO | MPH | VP MPL | LEVEL | MPG | GS/VM | | | | |
| 1 | | | | | | | | | | | | | | | | | | |
| 2 | | | | | | | | | | | | | | | | | | |
| 3 | 1 | 11000. | 536. 0. | 536. 536. | 0. | 536. | 1500. | 0. | 0. | 0. | .36 | 62. | 8.6 | A | 21.6 | 12.8 | | |
| 4 | 1 | 1500. | 0. 0. | 536. 0. | 0. | 536. | 1500. | 0. | 0. | 0. | .36 | 62. | 8.6 | A | 21.6 | 12.8 | | |
| 5 | 1 | 1400. | 0. 0. | 536. 0. | 0. | 536. | 1500. | 0. | 0. | 0. | .36 | 62. | 8.6 | A | 21.6 | 12.8 | | |
| 6 | 1 | 1500. | 0. 0. | 536. 0. | 0. | 536. | 1500. | 0. | 0. | 0. | .36 | 62. | 8.6 | A | 21.6 | 12.8 | | |
| 7 | 1 | 1300. | 0. 536. | 536. 0. | 536. | 536. | 1500. | 0. | 0. | 0. | .36 | 62. | 8.6 | A | 21.6 | 12.8 | | |
| 8 | | | | | | | | | | | | | | | | | | |
| 9 | | | | | | | | | | | | | | | | | | |
| 10 | | | | | | | | | | | | | | | | | | |
| 11 | | | | | | | | | | | | | | | | | | |
| 12 | | | | | | | | | | | | | | | | | | |
| 13 | | | | | | | | | | | | | | | | | | |
| 14 | | | | | | | | | | | | | | | | | | |
| 15 | | | | | | | | | | | | | | | | | | |
| 16 | | | | | | | | | | | | | | | | | | |
| 17 | | | | | | | | | | | | | | | | | | |
| 18 | | | | | | | | | | | | | | | | | | |
| 19 | | | | | | | | | | | | | | | | | | |
| 20 | | | | | | | | | | | | | | | | | | |
| TOTAL | 16700. | = | 3.2 MILES | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 14. VEH-HRS | 27. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 14. VEH-HRS | 27. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 848. VEH-MI. | 1695. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH | 62. MPH |
| AVERAGE DENSITY = | 9. VP MPL | 9. VP MPL |
| TOTAL FUEL = | 39. GALLONS | 254. GALLONS |
| TOTAL EMISSIONS = | 11. KI LOGRAMS | 70. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.42 | 4 | 0.06 | 5 | 0.05 |
| 6 | 0.06 | 7 | 0.05 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 0.6 VEH-HRS ***** AVERAGE DELAY = 0.07 MIN/VEH *****

 ** FREeway TRAVEL TIME (MI MINUTES) **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN *
 * 1 2 3 4 5 6 7 8 *

Table with 8 rows of simulation data. Columns include lane ID, delay, and other performance metrics.

TIME SLICE FREEWAY PERFORMANCE TABLE

Table with 16 columns: SUB NO., SSEC, O-D DATA DEMANDS, ADJUSTED VOLUMES, SSEC, WEAVE, CONGEST STORAGE, V/C, SPEED DENSITY, LOS, FUEL, EMISSIONS.

TOTAL 137309. = 26.0 MILES MAX(V/C) = 0.92 LOWEST LOS = D AVG = 64. 19.6 19.2 13.9

Summary table comparing CURRENT TIME SLICE and CUMULATIVE VALUES for metrics like FREeway TRAVEL TIME, MERGE DELAY, etc.

Table showing MAINTENANCE DELAY (VEH-HRS) and DESIRED SPEED = 65.0. Includes columns for subsection and delay.

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|-------|-----------------------|-------|-------|-------|-------|-------|-------|---|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 17.57 | 0.00 | 20.76 | 21.31 | 21.32 | 21.50 | 22.03 | 24.22 | |
| * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| * 3 * | 0.00 | 0.00 | 1.17 | 1.72 | 1.73 | 1.92 | 2.45 | 4.63 | |
| * 4 * | 0.00 | 0.00 | 0.64 | 1.19 | 1.20 | 1.38 | 1.92 | 4.10 | |
| * 5 * | 0.00 | 0.00 | 0.09 | 0.64 | 0.65 | 0.83 | 1.36 | 3.55 | |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.12 | 0.13 | 0.31 | 0.85 | 3.03 | |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 | 0.71 | 2.89 | |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.53 | 2.72 | |

 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *
 * SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMI SS *
 * SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMP LEVEL MPG GS/VM *

| | | | | | | | | | | | | | | | | | | |
|------|---|--------|-------|-------|-------|-------|-------|-------|-------|----|----|----|-----|-----|------|---|------|------|
| * 1 | 3 | 500. | 3570. | 0. | 3570. | 3570. | 0. | 3570. | 6000. | 0. | 0. | 0. | .60 | 65. | 18.3 | C | 19.0 | 14.1 |
| * 2 | 3 | 99999. | 0. | 571. | 3570. | 0. | 571. | 3570. | 6000. | 0. | 0. | 0. | .60 | 65. | 18.3 | C | 19.0 | 14.1 |
| * 3 | 2 | 11000. | 0. | 0. | 2999. | 0. | 0. | 2999. | 4000. | 0. | 0. | 0. | .75 | 62. | 24.2 | C | 20.3 | 13.0 |
| * 4 | 2 | 1500. | 40. | 0. | 3039. | 40. | 0. | 3039. | 4000. | 0. | 0. | 0. | .76 | 62. | 24.5 | C | 20.3 | 13.0 |
| * 5 | 2 | 1400. | 0. | 0. | 3039. | 0. | 0. | 3039. | 4000. | 0. | 0. | 0. | .76 | 62. | 24.5 | C | 20.3 | 13.0 |
| * 6 | 2 | 1500. | 590. | 0. | 3629. | 590. | 0. | 3629. | 4000. | 0. | 0. | 0. | .91 | 57. | 31.6 | D | 22.1 | 11.9 |
| * 7 | 2 | 1300. | 0. | 0. | 3629. | 0. | 0. | 3629. | 4000. | 0. | 0. | 0. | .91 | 57. | 31.6 | D | 22.1 | 11.9 |
| * 8 | 3 | 500. | 571. | 750. | 4200. | 571. | 750. | 4200. | 4950. | 0. | 0. | 0. | .85 | 65. | 21.5 | C | 19.0 | 14.1 |
| * 9 | 2 | 2300. | 0. | 0. | 3450. | 0. | 0. | 3450. | 4000. | 0. | 0. | 0. | .86 | 61. | 28.3 | D | 20.9 | 12.7 |
| * 10 | 3 | 250. | 539. | 0. | 3989. | 539. | 0. | 3989. | 4750. | 0. | 0. | 0. | .84 | 65. | 20.5 | C | 19.0 | 14.1 |
| * 11 | 3 | 200. | 0. | 0. | 3989. | 0. | 0. | 3989. | 4750. | 0. | 0. | 0. | .84 | 65. | 20.5 | C | 19.0 | 14.1 |
| * 12 | 3 | 250. | 0. | 1710. | 3989. | 0. | 1710. | 3989. | 4750. | 0. | 0. | 0. | .84 | 65. | 20.5 | C | 19.0 | 14.1 |
| * 13 | 2 | 50. | 0. | 0. | 2279. | 0. | 0. | 2279. | 4000. | 0. | 0. | 0. | .57 | 65. | 17.5 | B | 19.0 | 14.1 |
| * 14 | 2 | 50. | 0. | 0. | 2279. | 0. | 0. | 2279. | 2470. | 0. | 0. | 0. | .92 | 65. | 17.5 | B | 19.0 | 14.1 |
| * 15 | 2 | 1000. | 0. | 0. | 2279. | 0. | 0. | 2279. | 4000. | 0. | 0. | 0. | .57 | 65. | 17.5 | B | 19.0 | 14.1 |
| * 16 | 2 | 10. | 0. | 0. | 2279. | 0. | 0. | 2279. | 4000. | 0. | 0. | 0. | .57 | 65. | 17.5 | B | 19.0 | 14.1 |
| * 17 | 2 | 1500. | 686. | 0. | 2965. | 686. | 0. | 2965. | 4000. | 0. | 0. | 0. | .74 | 64. | 23.1 | C | 19.3 | 13.8 |
| * 18 | 2 | 1500. | 0. | 299. | 2965. | 0. | 299. | 2965. | 4000. | 0. | 0. | 0. | .74 | 64. | 23.1 | C | 19.3 | 13.8 |
| * 19 | 2 | 12000. | 0. | 0. | 2666. | 0. | 0. | 2666. | 4000. | 0. | 0. | 0. | .67 | 65. | 20.5 | C | 19.0 | 14.1 |
| * 20 | 3 | 500. | 0. | 2666. | 2666. | 0. | 2666. | 2666. | 6000. | 0. | 0. | 0. | .44 | 65. | 13.7 | B | 19.0 | 14.1 |

 *
 * TOTAL 137309. = 26.0 MILES MAX(V/C) = 0.92 LOWEST LOS = D AVG = 64. 19.6 19.2 13.9 *
 *

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|-----------------------------|--------------------|-----------------|-------------------|------------------|
| FREWAY TRAVEL TIME = | 688. VEH-HRS | 786. PASS-HRS | 1376. VEH-HRS | 1572. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 688. VEH-HRS | 786. PASS-HRS | 1376. VEH-HRS | 1572. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 44348. VEH-MI. | 50685. PASS-MI. | 88697. VEH-MI. | 101371. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 64. MPH. | | 64. MPH. | |
| AVERAGE DENSITY = | 20. VPMP | | 20. VPMP | |
| TOTAL FUEL = | 2312. GALLONS | | 4624. GALLONS | |
| TOTAL EMISSIONS = | 616. KILOGRAMS | | 1233. KILOGRAMS | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 2.33 | 4 | 0.32 | 5 | 0.30 |
| 6 | 1.04 | 7 | 0.90 | 8 | 0.00 | 9 | 0.76 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.07 | 18 | 0.07 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 5.8 VEH-HRS ***** AVERAGE DELAY = 0.11 MIN/VEH *****

 **
 ** FREEWAY TRAVEL TIME (MINUTES)
 **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|-------|-----------------------|-------|-------|-------|-------|-------|-------|---|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 17.57 | 0.00 | 20.88 | 22.06 | 22.12 | 22.31 | 22.85 | 25.04 | |
| * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| * 3 * | 0.00 | 0.00 | 1.25 | 2.43 | 2.50 | 2.68 | 3.23 | 5.41 | |
| * 4 * | 0.00 | 0.00 | 0.71 | 1.88 | 1.95 | 2.13 | 2.68 | 4.86 | |
| * 5 * | 0.00 | 0.00 | 0.10 | 1.27 | 1.34 | 1.52 | 2.07 | 4.25 | |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.40 | 0.47 | 0.65 | 1.20 | 3.38 | |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 | 0.72 | 2.91 | |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.54 | 2.73 | |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB | * NO. | * SSEC | * O-D | * DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | |
|-------|-------|----------|-------|--------|-----------|------------|-----------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VP/MP | * LEVEL | * MPG | * GS/VM | |
| * 1 | 3 | 500. | 3881. | 0. | 3881. | 3881. | 0. | 3881. | 6000. | 0. | 0. | 0. | .65 | 65. | 19.9 | C | 19.0 | 14.1 |
| * 2 | 3 | 99999. | 0. | 621. | 3881. | 0. | 621. | 3881. | 6000. | 0. | 0. | 0. | .65 | 65. | 19.9 | C | 19.0 | 14.1 |
| * 3 | 2 | 11000. | 0. | 0. | 3260. | 0. | 0. | 3260. | 4000. | 0. | 0. | 0. | .82 | 61. | 26.9 | D | 21.0 | 12.6 |
| * 4 | 2 | 1500. | 49. | 0. | 3309. | 49. | 0. | 3309. | 4000. | 0. | 0. | 0. | .83 | 60. | 27.4 | D | 21.2 | 12.5 |
| * 5 | 2 | 1400. | 0. | 0. | 3309. | 0. | 0. | 3309. | 4000. | 0. | 0. | 0. | .83 | 60. | 27.4 | D | 21.2 | 12.5 |
| * 6 | 2 | 1500. | 660. | 0. | 3969. | 660. | 0. | 3969. | 4000. | 0. | 0. | 0. | .99 | 52. | 38.0 | E | 23.5 | 11.2 |
| * 7 | 2 | 1300. | 0. | 0. | 3969. | 0. | 0. | 3969. | 4000. | 0. | 0. | 0. | .99 | 52. | 38.0 | E | 23.5 | 11.2 |
| * 8 | 3 | 500. | 621. | 950. | 4590. | 621. | 950. | 4590. | 4950. | 0. | 0. | 0. | .93 | 58. | 26.6 | D | 22.1 | 11.9 |
| * 9 | 2 | 2300. | 0. | 0. | 3640. | 0. | 0. | 3479. | 4000. | 0. | * 2286. | 161. | .87 | 34. | 51.4 | F | 20.1 | 13.8 |
| * 10 | 3 | 250. | 561. | 0. | 4201. | 561. | 0. | 4040. | 4750. | 0. | ** 250. | 161. | .85 | 21. | 63.0 | F | 17.4 | 16.7 |
| * 11 | 3 | 200. | 0. | 0. | 4201. | 0. | 0. | 4040. | 4750. | 0. | ** 200. | 161. | .85 | 20. | 68.4 | F | 17.3 | 17.1 |
| * 12 | 3 | 250. | 0. | 1520. | 4201. | 0. | 1520. | 4040. | 4750. | 0. | ** 250. | 161. | .85 | 18. | 73.8 | F | 17.1 | 17.4 |
| * 13 | 2 | 50. | 0. | 50. | 2681. | 0. | 50. | 2520. | 4000. | 0. | ** 50. | 161. | .63 | 9. | 145.3 | F | 11.3 | 24.5 |
| * 14 | 2 | 50. | 0. | 0. | 2681. | 0. | 0. | 2470. | 2470. | 0. | 0. | 0. | 1.00 | 65. | 19.0 | E | 19.0 | 14.1 |
| * 15 | 2 | 1000. | 50. | 0. | 2681. | 50. | 0. | 2520. | 4000. | 0. | 0. | 0. | .63 | 65. | 19.4 | C | 19.0 | 14.1 |
| * 16 | 2 | 10. | 0. | 0. | 2681. | 0. | 0. | 2520. | 4000. | 0. | 0. | 0. | .63 | 65. | 19.4 | C | 19.0 | 14.1 |
| * 17 | 2 | 1500. | 748. | 0. | 3429. | 748. | 0. | 3268. | 4000. | 0. | 0. | 0. | .82 | 63. | 26.1 | D | 20.0 | 13.3 |
| * 18 | 2 | 1500. | 0. | 691. | 3429. | 0. | 659. | 3268. | 4000. | 0. | 0. | 0. | .82 | 63. | 26.1 | D | 20.0 | 13.3 |
| * 19 | 2 | 12000. | 0. | 0. | 2738. | 0. | 0. | 2609. | 4000. | 0. | 0. | 0. | .65 | 65. | 20.1 | C | 19.0 | 14.1 |
| * 20 | 3 | 500. | 0. | 2738. | 2738. | 0. | 2609. | 2609. | 6000. | 0. | 0. | 0. | .43 | 65. | 13.4 | B | 19.0 | 14.1 |

* TOTAL 137309. = 26.0 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 62. 22.0 19.3 13.9 *

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 768. VEH-HRS | 876. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 768. VEH-HRS | 876. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 47842. VEH-MI. | 54672. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 64. MPH. |
| AVERAGE DENSITY = | 22. VP/MP | 20. VP/MP |
| TOTAL FUEL = | 2484. GALLONS | 7107. GALLONS |
| TOTAL EMISSIONS = | 663. KI LOGRAMS | 1895. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 3.71 | 4 | 0.55 | 5 | 0.51 |
| 6 | 2.13 | 7 | 1.85 | 8 | 0.43 | 9 | 11.05 | 10 | 3.04 |
| 11 | 2.73 | 12 | 3.78 | 13 | 1.19 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.27 | 18 | 0.27 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 31.5 VEH-HRS ***** AVERAGE DELAY = 0.52 MIN/VEH *****

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TIME SLICE 4 OF 6

**
** FREeway TRAVEL TIME (MINUTES) **
**

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|---|-----------------------|------|-------|-------|-------|-------|-------|-------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 | * | 17.57 | 0.00 | 21.51 | 23.40 | 23.47 | 23.65 | 24.20 | 26.38 |
| * 2 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 3 | * | 0.00 | 0.00 | 1.88 | 3.77 | 3.84 | 4.02 | 4.57 | 6.75 |
| * 4 | * | 0.00 | 0.00 | 1.26 | 3.15 | 3.22 | 3.40 | 3.95 | 6.13 |
| * 5 | * | 0.00 | 0.00 | 0.27 | 2.16 | 2.23 | 2.41 | 2.96 | 5.14 |
| * 6 | * | 0.00 | 0.00 | 0.00 | 0.46 | 0.53 | 0.71 | 1.26 | 3.45 |
| * 7 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 | 0.72 | 2.91 |
| * 8 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.54 | 2.73 |

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*
* TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB | * NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISS |
|-------|-------|----------|------------|-----------|------------|-----------|---------|---------|-----------|-----------|----------|---------|-----------|-------|---------|---------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL |
| * 1 | * 3 | * 500. | * 3881. | * 0. | * 3881. | * 3881. | * 0. | * 3881. | * 6000. | * 0. | * 0. | * 0. | * .65 | * 65. | * 19.9 | * C |
| * 2 | * 3 | * 99999. | * 0. | * 621. | * 3881. | * 0. | * 621. | * 3881. | * 6000. | * 0. | * 0. | * 0. | * .65 | * 65. | * 19.9 | * C |
| * 3 | * 2 | * 11000. | * 0. | * 0. | * 3260. | * 0. | * 0. | * 3260. | * 4000. | * 0. | * 0. | * 0. | * .82 | * 61. | * 26.9 | * D |
| * 4 | * 2 | * 1500. | * 49. | * 0. | * 3309. | * 49. | * 0. | * 3309. | * 4000. | * 0. | * 0. | * 0. | * .83 | * 60. | * 27.4 | * D |
| * 5 | * 2 | * 1400. | * 0. | * 0. | * 3309. | * 0. | * 0. | * 3148. | * 4000. | * * | * 778. | * 161. | * .79 | * 47. | * 33.3 | * F |
| * 6 | * 2 | * 1500. | * 660. | * 0. | * 3969. | * 660. | * 0. | * 3808. | * 4000. | * ** | * 1500. | * 161. | * .95 | * 35. | * 54.4 | * F |
| * 7 | * 2 | * 1300. | * 0. | * 0. | * 3969. | * 0. | * 0. | * 3808. | * 4000. | * ** | * 1300. | * 161. | * .95 | * 29. | * 65.0 | * F |
| * 8 | * 3 | * 500. | * 621. | * 950. | * 4590. | * 621. | * 950. | * 4429. | * 4950. | * ** | * 500. | * 161. | * .89 | * 21. | * 69.5 | * F |
| * 9 | * 2 | * 2300. | * 0. | * 0. | * 3640. | * 0. | * 0. | * 3479. | * 4000. | * ** | * 2300. | * 161. | * .87 | * 18. | * 95.0 | * F |
| * 10 | * 3 | * 250. | * 561. | * 0. | * 4201. | * 561. | * 0. | * 4040. | * 4750. | * ** | * 250. | * 161. | * .85 | * 17. | * 78.6 | * F |
| * 11 | * 3 | * 200. | * 0. | * 0. | * 4201. | * 0. | * 0. | * 4040. | * 4750. | * ** | * 200. | * 161. | * .85 | * 17. | * 78.6 | * F |
| * 12 | * 3 | * 250. | * 0. | * 1520. | * 4201. | * 0. | * 1520. | * 4040. | * 4750. | * ** | * 250. | * 161. | * .85 | * 17. | * 78.6 | * F |
| * 13 | * 2 | * 50. | * 0. | * 50. | * 2681. | * 0. | * 50. | * 2520. | * 4000. | * ** | * 50. | * 161. | * .63 | * 9. | * 147.3 | * F |
| * 14 | * 2 | * 50. | * 0. | * 0. | * 2631. | * 0. | * 0. | * 2470. | * 2470. | * 0. | * 0. | * 0. | * 1.00 | * 65. | * 19.0 | * E |
| * 15 | * 2 | * 1000. | * 50. | * 0. | * 2681. | * 50. | * 0. | * 2520. | * 4000. | * 0. | * 0. | * 0. | * .63 | * 65. | * 19.4 | * C |
| * 16 | * 2 | * 10. | * 0. | * 0. | * 2681. | * 0. | * 0. | * 2520. | * 4000. | * 0. | * 0. | * 0. | * .63 | * 65. | * 19.4 | * C |
| * 17 | * 2 | * 1500. | * 748. | * 0. | * 3429. | * 748. | * 0. | * 3268. | * 4000. | * 0. | * 0. | * 0. | * .82 | * 63. | * 26.1 | * D |
| * 18 | * 2 | * 1500. | * 0. | * 691. | * 3429. | * 0. | * 659. | * 3268. | * 4000. | * 0. | * 0. | * 0. | * .82 | * 63. | * 26.1 | * D |
| * 19 | * 2 | * 12000. | * 0. | * 0. | * 2738. | * 0. | * 0. | * 2609. | * 4000. | * 0. | * 0. | * 0. | * .65 | * 65. | * 20.1 | * C |
| * 20 | * 3 | * 500. | * 0. | * 2738. | * 2738. | * 0. | * 2609. | * 2609. | * 6000. | * 0. | * 0. | * 0. | * .43 | * 65. | * 13.4 | * B |

* TOTAL 137309. = 26.0 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 59. 23.4 19.2 14.0 *

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 808. VEH-HRS | 921. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 2951. VEH-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 3369. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 808. VEH-HRS | 0. VEH-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 47784. VEH-MI. | 921. PASS-HRS |
| AVERAGE SYSTEM SPEED = | 59. MPH. | 2951. VEH-HRS |
| | | 184322. VEH-MI. |
| | | 62. MPH. |

AVERAGE DENSITY = 23. VP MPL
 TOTAL FUEL = 2494. GALLONS
 TOTAL EMISSIONS = 668. KI LOGRAMS

21. VP MPL
 9601. GALLONS
 2563. KI LOGRAMS

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 TIME SLICE 4 OF 6

***** MAINLINE DELAY (VEH-HRS) ***** DESI RED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 3.71 | 4 | 0.55 | 5 | 2.52 |
| 6 | 7.31 | 7 | 8.89 | 8 | 6.67 | 9 | 29.74 | 10 | 4.11 |
| 11 | 3.29 | 12 | 4.11 | 13 | 1.21 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.27 | 18 | 0.27 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 72.6 VEH-HRS ***** AVERAGE DELAY = 1.19 MIN/VEH *****

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 TIME SLICE 5 OF 6

QUEUE CLEAR SECTION 13 T2= 0.475

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 TIME SLICE 5 OF 6

 ** FREEWAY TRAVEL TIME (MI NUTES) **

| * ORI GINS | DESTI NATI ONS ACROSS | | | | | | | |
|------------|-----------------------|------|-------|-------|-------|-------|-------|-------|
| * DOWN | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 17.57 | 0.00 | 21.16 | 22.64 | 22.70 | 22.88 | 23.46 | 25.67 |
| * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 3 * | 0.00 | 0.00 | 1.57 | 3.06 | 3.11 | 3.29 | 3.87 | 6.08 |
| * 4 * | 0.00 | 0.00 | 1.01 | 2.49 | 2.55 | 2.73 | 3.31 | 5.52 |
| * 5 * | 0.00 | 0.00 | 0.21 | 1.69 | 1.75 | 1.93 | 2.51 | 4.72 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.44 | 0.49 | 0.68 | 1.25 | 3.46 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 | 0.75 | 2.96 |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.57 | 2.78 |

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 TIME SLICE 5 OF 6

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | |
|-----------|--------|------------|-----------|------------|-----------|---------|---------|-----------|-----------|-------|----------|-----------|----------|--------|-------------|---------|--------|---------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VP MPL | * LEVEL | * MPG | * GS/VM |
| * 1 | * 3 | * 500. | * 3350. | * 0. | * 3350. | * 3350. | * 0. | * 3350. | * 6000. | * 0. | * 0. | * 0. | * .56 | * 65. | * 17.2 | * B | * 19.0 | * 14.1 |
| * 2 | * 3 | * 99999. | * 0. | * 536. | * 3350. | * 0. | * 536. | * 3350. | * 6000. | * 0. | * 0. | * .56 | * 65. | * 17.2 | * B | * 19.0 | * 14.1 | * 14.1 |
| * 3 | * 2 | * 11000. | * 0. | * 0. | * 2814. | * 0. | * 0. | * 2814. | * 4000. | * 0. | * 0. | * 0. | * .70 | * 62. | * 22.7 | * C | * 20.3 | * 13.0 |
| * 4 | * 2 | * 1500. | * 50. | * 0. | * 2864. | * 50. | * 0. | * 2864. | * 4000. | * 0. | * 0. | * 0. | * .72 | * 62. | * 23.1 | * C | * 20.3 | * 13.0 |
| * 5 | * 2 | * 1400. | * 0. | * 0. | * 2864. | * 0. | * 0. | * 2864. | * 4000. | * 0. | * 0. | * 0. | * .72 | * 55. | * 25.9 | * C | * 20.1 | * 13.3 |
| * 6 | * 2 | * 1500. | * 440. | * 0. | * 3304. | * 440. | * 0. | * 3304. | * 4000. | * 0. | * 0. | * 0. | * .83 | * 43. | * 38.0 | * E | * 20.6 | * 13.1 |
| * 7 | * 2 | * 1300. | * 0. | * 0. | * 3304. | * 0. | * 0. | * 3304. | * 4000. | * 0. | * 0. | * 0. | * .83 | * 36. | * 45.5 | * F | * 20.2 | * 13.6 |
| * 8 | * 3 | * 500. | * 536. | * 671. | * 3840. | * 536. | * 671. | * 3840. | * 4950. | * 0. | * 0. | * 0. | * .78 | * 27. | * 46.6 | * F | * 18.0 | * 15.8 |
| * 9 | * 2 | * 2300. | * 0. | * 0. | * 3169. | * 0. | * 0. | * 3169. | * 4000. | * 0. | * 0. | * 0. | * .79 | * 25. | * 63.5 | * F | * 18.6 | * 15.5 |
| * 10 | * 3 | * 250. | * 429. | * 0. | * 3598. | * 429. | * 0. | * 3598. | * 4750. | * 0. | * 0. | * 0. | * .76 | * 19. | * 64.3 | * F | * 17.0 | * 17.5 |
| * 11 | * 3 | * 200. | * 0. | * 0. | * 3598. | * 0. | * 0. | * 3598. | * 4750. | * 0. | * 0. | * 0. | * .76 | * 18. | * 66.4 | * F | * 16.9 | * 17.6 |
| * 12 | * 3 | * 250. | * 0. | * 1240. | * 3598. | * 0. | * 1240. | * 3598. | * 4750. | * 0. | * 0. | * 0. | * .76 | * 18. | * 68.4 | * F | * 16.8 | * 17.8 |
| * 13 | * 2 | * 50. | * 0. | * 279. | * 2358. | * 0. | * 279. | * 2749. | * 4000. | * 0. | * 0. | * 0. | * -.391. | * .69 | * 11. | * 129.3 | * F | * 13.3 |
| * 14 | * 2 | * 50. | * 0. | * 0. | * 2079. | * 0. | * 0. | * 2470. | * 2470. | * 0. | * 0. | * 0. | * 1.00 | * 65. | * 19.0 | * E | * 19.0 | * 14.1 |
| * 15 | * 2 | * 1000. | * 280. | * 0. | * 2359. | * 280. | * 0. | * 2750. | * 4000. | * 0. | * 0. | * 0. | * .69 | * 65. | * 21.2 | * C | * 19.0 | * 14.1 |
| * 16 | * 2 | * 10. | * 0. | * 0. | * 2359. | * 0. | * 0. | * 2750. | * 4000. | * 0. | * 0. | * 0. | * .69 | * 65. | * 21.2 | * C | * 19.0 | * 14.1 |
| * 17 | * 2 | * 1500. | * 830. | * 0. | * 3189. | * 830. | * 0. | * 3580. | * 4000. | * 0. | * 0. | * 0. | * .89 | * 59. | * 30.1 | * D | * 21.5 | * 12.3 |
| * 18 | * 2 | * 1500. | * 0. | * 530. | * 3189. | * 0. | * 595. | * 3580. | * 4000. | * 0. | * 0. | * 0. | * .89 | * 59. | * 30.1 | * D | * 21.5 | * 12.3 |
| * 19 | * 2 | * 12000. | * 0. | * 0. | * 2659. | * 0. | * 0. | * 2985. | * 4000. | * 0. | * 0. | * 0. | * .75 | * 64. | * 23.2 | * C | * 19.3 | * 13.8 |

* 20 3 500. 0. 2659. 2659. 0. 2985. 2985. 6000. 0. 0. 0. .50 65. 15.3 B 19.0 14.1 *

* TOTAL 137309. = 26.0 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 61. 20.3 19.2 14.0 *

CURRENT TIME SLICE CUMULATIVE VALUES
FREQUENCY TRAVEL TIME = 703. VEH-HRS 803. PASS-HRS 3654. VEH-HRS 4172. PASS-HRS
FREQUENCY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 703. VEH-HRS 803. PASS-HRS 3654. VEH-HRS 4172. PASS-HRS
TOTAL FRWAY TRAV DISTANCE = 42543. VEH-MI. 48634. PASS-MI. 226866. VEH-MI. 259284. PASS-MI.
AVERAGE SYSTEM SPEED = 61. MPH. 62. MPH
AVERAGE DENSITY = 20. VPMP. 21. VPMP
TOTAL FUEL = 2220. GALLONS 11821. GALLONS
TOTAL EMISSIONS = 594. KILOGRAMS 3157. KILOGRAMS

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
1 0.00 2 0.00 3 2.18 4 0.30 5 1.04
6 3.68 7 5.16 8 4.01 9 18.44 10 3.55
11 2.98 12 3.90 13 1.02 14 0.00 15 0.00
16 0.00 17 0.73 18 0.73 19 0.62 20 0.00
***** TOTAL DELAY = 48.3 VEH-HRS ***** AVERAGE DELAY = 0.88 MIN/VEH *****

** FREEWAY TRAVEL TIME (MINUTES) **

* ORIGINS DESTINATIONS ACROSS *
* DOWN 1 2 3 4 5 6 7 8 *
* 1 * 17.57 0.00 20.73 21.27 21.28 21.46 22.00 24.19 *
* 2 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
* 3 * 0.00 0.00 1.15 1.68 1.69 1.87 2.41 4.60 *
* 4 * 0.00 0.00 0.61 1.15 1.16 1.34 1.88 4.07 *
* 5 * 0.00 0.00 0.09 0.62 0.63 0.81 1.36 3.54 *
* 6 * 0.00 0.00 0.00 0.12 0.13 0.31 0.86 3.04 *
* 7 * 0.00 0.00 0.00 0.00 0.00 0.17 0.72 2.90 *
* 8 * 0.00 0.00 0.00 0.00 0.00 0.00 0.54 2.72 *
* * *

TIME SLICE FREEWAY PERFORMANCE TABLE

* SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMISSIONS *
* SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMP LEVEL MPG GS/VM *
* 1 3 500. 3350. 0. 3350. 3350. 0. 3350. 6000. 0. 0. 0. .56 65. 17.2 B 19.0 14.1 *
* 2 3 99999. 0. 536. 3350. 0. 536. 3350. 6000. 0. 0. 0. .56 65. 17.2 B 19.0 14.1 *
* 3 2 11000. 0. 0. 2814. 0. 0. 2814. 4000. 0. 0. 0. .70 62. 22.7 C 20.3 13.0 *
* 4 2 1500. 50. 0. 2864. 50. 0. 2864. 4000. 0. 0. 0. .72 62. 23.1 C 20.3 13.0 *
* 5 2 1400. 0. 0. 2864. 0. 0. 2864. 4000. 0. 0. 0. .72 62. 23.1 C 20.3 13.0 *
* 6 2 1500. 440. 0. 3304. 440. 0. 3304. 4000. 0. 0. 0. .83 60. 27.3 D 21.1 12.5 *
* 7 2 1300. 0. 0. 3304. 0. 0. 3304. 4000. 0. 0. 0. .83 60. 27.3 D 21.1 12.5 *
* 8 3 500. 536. 671. 3840. 536. 671. 3840. 4950. 0. 0. 0. .78 65. 19.7 C 19.0 14.1 *
* 9 2 2300. 0. 0. 3169. 0. 0. 3169. 4000. 0. 0. 0. .79 63. 25.0 C 19.7 13.5 *

SR-237_WB_PM_P1_2018_PL_2.txt

| | | | | | | | | | | | | | | | | | | | |
|--|---|--------|------|-------|-------|------|-------|-------|-------|----|----|----|-----|-----|------|---|------|------|---|
| *10 | 3 | 250. | 429. | 0. | 3598. | 429. | 0. | 3598. | 4750. | 0. | 0. | 0. | .76 | 65. | 18.5 | C | 19.0 | 14.1 | * |
| *11 | 3 | 200. | 0. | 0. | 3598. | 0. | 0. | 3598. | 4750. | 0. | 0. | 0. | .76 | 65. | 18.5 | C | 19.0 | 14.1 | * |
| *12 | 3 | 250. | 0. | 1240. | 3598. | 0. | 1240. | 3598. | 4750. | 0. | 0. | 0. | .76 | 65. | 18.5 | C | 19.0 | 14.1 | * |
| *13 | 2 | 50. | 0. | 279. | 2358. | 0. | 279. | 2358. | 4000. | 0. | 0. | 0. | .59 | 65. | 18.1 | C | 19.0 | 14.1 | * |
| *14 | 2 | 50. | 0. | 0. | 2079. | 0. | 0. | 2079. | 2470. | 0. | 0. | 0. | .84 | 65. | 16.0 | B | 19.0 | 14.1 | * |
| *15 | 2 | 1000. | 280. | 0. | 2359. | 280. | 0. | 2359. | 4000. | 0. | 0. | 0. | .59 | 65. | 18.1 | C | 19.0 | 14.1 | * |
| *16 | 2 | 10. | 0. | 0. | 2359. | 0. | 0. | 2359. | 4000. | 0. | 0. | 0. | .59 | 65. | 18.1 | C | 19.0 | 14.1 | * |
| *17 | 2 | 1500. | 830. | 0. | 3189. | 830. | 0. | 3189. | 4000. | 0. | 0. | 0. | .80 | 63. | 25.2 | C | 19.8 | 13.5 | * |
| *18 | 2 | 1500. | 0. | 530. | 3189. | 0. | 530. | 3189. | 4000. | 0. | 0. | 0. | .80 | 63. | 25.2 | C | 19.8 | 13.5 | * |
| *19 | 2 | 12000. | 0. | 0. | 2659. | 0. | 0. | 2659. | 4000. | 0. | 0. | 0. | .66 | 65. | 20.5 | C | 19.0 | 14.1 | * |
| *20 | 3 | 500. | 0. | 2659. | 2659. | 0. | 2659. | 2659. | 6000. | 0. | 0. | 0. | .44 | 65. | 13.6 | B | 19.0 | 14.1 | * |
| ***** | | | | | | | | | | | | | | | | | | | |
| * TOTAL 137309. = 26.0 MILES MAX(V/C) = 0.84 LOWEST LOS = D AVG = 65. 18.6 19.2 13.9 * | | | | | | | | | | | | | | | | | | | |
| ***** | | | | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | | CUMULATIVE VALUES |
|------------------------------|--------------------|-----------------|----------------------------------|
| FREEWAY TRAVEL TIME = | 649. VEH-HRS | 741. PASS-HRS | 4303. VEH-HRS 4913. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 649. VEH-HRS | 741. PASS-HRS | 4303. VEH-HRS 4913. PASS-HRS |
| TOTAL FRWAY TRAV DI STANCE = | 41886. VEH-MI. | 47876. PASS-MI. | 268752. VEH-MI. 307160. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 65. MPH | | 62. MPH |
| AVERAGE DENSITY = | 19. VPMPPL | | 21. VPMPPL |
| TOTAL FUEL = | 2186. GALLONS | | 14007. GALLONS |
| TOTAL EMISSIONS = | 583. KILOGRAMS | | 3740. KILOGRAMS |

1 INSTITUTE OF TRANSPORTATION STUDIES FRE012PL REL 3.01 3/ 3/2016 15:15 PAGE 40
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF NON-PRIORITY LANES
 TIME SLICE 6 OF 6

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 2.18 | 4 | 0.30 | 5 | 0.28 |
| 6 | 0.55 | 7 | 0.47 | 8 | 0.00 | 9 | 0.28 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.20 | 18 | 0.20 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 4.5 VEH-HRS ***** AVERAGE DELAY = 0.09 MIN/VEH *****

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FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEEEE 0*A.D. MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP LLL
FFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 2222 PPP PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP PPP LLL
FFF RRR RRR EEEEEEEEE 0*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQ 1111111 222222222 PPP LLLLLLLLLL

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FREQ12PL

- 1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 3 AND 7 WILL BE SIMULATED.
- 2. SHORT TERM CONSEQUENCES ARE REQUESTED.
- 3. THERE ARE 2.0 TIME SLICES PER HOUR.
- 4. WEAVING ANALYSIS IS NOT ENGAGED.
- 5. NO ALTERNATE ROUTE IS PROVIDED.
- 6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 30
- 7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
- 8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
- 9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
- 10. NUMBER OF PRIORITY LANES = 1.
- 11. PRIORITY CUTOFF LIMIT = 2.

ON-RAMP CAPACITY LIMITS

```

1 2 3 4 5 6 7 8
6000.***** 1500. 1500.***** 2000. 1500. 1500.

```

OFF-RAMP CAPACITY LIMITS

```

1 2 3 4 5 6 7 8
***** 2000. 2000. 1500. 1500. 1500. 6000.

```

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ON-RAMP 1 IS THE MAINLINE ORIGIN
OFF-RAMP 8 IS THE MAINLINE DESTINATION

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**** ON-RAMPS 2 AND 5 ARE SYNTHETIC ORIGINS USED TO ENTER AND LEAVE THE PL LANE(S)
**** OFF-RAMPS 1 AND 2 ARE SYNTHETIC DESTINATIONS USED TO ENTER AND LEAVE THE PL LANE(S)

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INPUT HAS BEEN COMPLETED

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FREeway AND ARTERIAL DESIGN FEATURES

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| ** SUB NO. | ** SSEC | ** SSEC | ** DESIGN | ** ORG | ** TRK | ** SSEC | ** PCT | ** PCT | ** DES | ** SPECIAL | ** FF. SPD. | ** CAP. | ** ART | ** GRADE | ** SUBSECTI | ** ON |
|------------|---------|-----------|-----------|--------|--------|---------|--------|-----------|---------|-------------|-------------|---------|-------------|----------|----------------------|-------|
| ** SEC LNS | ** CAP | ** LENGTH | ** SPEED | ** DES | ** FAC | ** GRAD | ** TRK | ** TRUCKS | ** RAMP | ** ALT. RTE | ** ALT. RTE | ** TYPE | ** ALT. RTE | ** ON | ** ON | |
| ** 1 | | | | | | | | | | | | | | | | |
| ** 2 | | | | | | | | | | | | | | | | |
| ** 3 | 1 | 1500. | 11000. | 62 | 0 | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | ** |
| ** 4 | 1 | 1500. | 1500. | 62 | 0 | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence On-ramp | ** |
| ** 5 | 1 | 1500. | 1400. | 62 | | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence to Crossman | ** |
| ** 6 | 1 | 1500. | 1500. | 62 | 0 | 0.95 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Crossman On-Ramp | ** |
| ** 7 | 1 | 1500. | 1300. | 62 | D | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Crossman / Mathilda | ** |


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* 20
*
*****
* TOTAL 16700. = 3.2 MILES MAX(V/C) = 0.38 LOWEST LOS = A AVG = 62. 9.2 21.6 12.8
*
*****

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```

CURRENT TIME SLICE CUMULATIVE VALUES
FREEWAY TRAVEL TIME = 15. VEH-HRS 29. PASS-HRS 15. VEH-HRS 29. PASS-HRS
FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 15. VEH-HRS 29. PASS-HRS 15. VEH-HRS 29. PASS-HRS
TOTAL FRWAY TRAV DI STANCE = 903. VEH-MI . 1807. PASS-MI . 903. VEH-MI . 1807. PASS-MI .
AVERAGE SYSTEM SPEED = 62. MPH 62. MPH
AVERAGE DENSITY = 9. VPMP 9. VPMP
TOTAL FUEL = 42. GALLONS 42. GALLONS
TOTAL EMISSIONS = 12. KI LOGRAMS 12. KI LOGRAMS

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1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/ 3/2016 15:22 PAGE 6
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 1 OF 6

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***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
1 0.00 2 0.00 3 0.44 4 0.06 5 0.06
6 0.06 7 0.05 8 0.00 9 0.00 10 0.00
11 0.00 12 0.00 13 0.00 14 0.00 15 0.00
16 0.00 17 0.00 18 0.00 19 0.00 20 0.00
***** TOTAL DELAY = 0.7 VEH-HRS ***** AVERAGE DELAY = 0.07 MIN/VEH *****

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1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/ 3/2016 15:22 PAGE 7
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 6

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*****
** FREEWAY TRAVEL TIME (MINUTES) **
*****

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| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | | |
|-----------------|---------------------|------|------|------|------|------|------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| 1 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | 0.00 | 3.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 4 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 5 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 7 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 8 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/ 3/2016 15:22 PAGE 8
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 6

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS | | | |
|---------|------|----------|---------|----------|------|-------|---------|---------|-------|-------|---------|-------|------|--------|---|------|------|
| SEC | LNS | LENGTH | ORG DES | ORG DES | SSEC | EFF | LENGTH | RATE | RATIO | MPH | VPMP | LEVEL | MPG | GS/VM | | | |
| 1 | | | | | | | | | | | | | | | | | |
| 2 | | | | | | | | | | | | | | | | | |
| 3 | 1 | 11000. | 571. | 0. | 571. | 571. | 0. | 571. | 1500. | 0. | 0. | .38 | 62. | 9.2 | A | 21.6 | 12.8 |
| 4 | 1 | 1500. | 0. | 0. | 571. | 0. | 0. | 571. | 1500. | 0. | 0. | .38 | 62. | 9.2 | A | 21.6 | 12.8 |
| 5 | 1 | 1400. | 0. | 0. | 571. | 0. | 0. | 571. | 1500. | 0. | 0. | .38 | 62. | 9.2 | A | 21.6 | 12.8 |
| 6 | 1 | 1500. | 0. | 0. | 571. | 0. | 0. | 571. | 1500. | 0. | 0. | .38 | 62. | 9.2 | A | 21.6 | 12.8 |
| 7 | 1 | 1300. | 0. | 571. | 571. | 0. | 571. | 571. | 1500. | 0. | 0. | .38 | 62. | 9.2 | A | 21.6 | 12.8 |
| 8 | | | | | | | | | | | | | | | | | |
| 9 | | | | | | | | | | | | | | | | | |

```

*10
* 11
* 12
* 13
* 14
* 15
* 16
* 17
* 18
* 19
* 20
*****
*
* TOTAL 16700. = 3.2 MILES MAX(V/C) = 0.38 LOWEST LOS = A AVG = 62. 9.2 21.6 12.8
*
*****

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CURRENT TIME SLICE CUMULATIVE VALUES
FREEWAY TRAVEL TIME = 15. VEH-HRS 29. PASS-HRS 29. VEH-HRS 58. PASS-HRS
FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 15. VEH-HRS 29. PASS-HRS 29. VEH-HRS 58. PASS-HRS
TOTAL FRWAY TRAV DISTANCE = 903. VEH-MI. 1807. PASS-MI. 1807. VEH-MI. 3613. PASS-MI.
AVERAGE SYSTEM SPEED = 62. MPH. 62. MPH.
AVERAGE DENSITY = 9. VPML 9. VPML
TOTAL FUEL = 42. GALLONS 84. GALLONS
TOTAL EMISSIONS = 12. KILOGRAMS 23. KILOGRAMS

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1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/ 3/2016 15:22 PAGE 9
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 6

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.44 | 4 | 0.06 | 5 | 0.06 |
| 6 | 0.06 | 7 | 0.05 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 0.7 VEH-HRS ***** AVERAGE DELAY = 0.07 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/ 3/2016 15:22 PAGE 10
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 3 OF 6

 ** FREeway TRAVEL TIME (MINUTES) **

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | | |
|-----------------|---------------------|------|------|------|------|------|------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| 1 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | 0.00 | 3.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 4 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 5 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 7 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 8 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/ 3/2016 15:22 PAGE 11
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 3 OF 6

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS | |
|---------|------|----------|---------|----------|------|-------|---------|---------|------|-------|---------|------|-------|--------|-------|
| SEC | LNS | LENGTH | ORG | DES | SSEC | CAP. | EFF | LENGTH | RATE | RATIO | MPH | VPML | LEVEL | MPG | GS/VM |

```

*
* 1
* 2
* 3 1 11000. 621. 0. 621. 621. 0. 621. 1500. 0. 0. 0. .41 62. 10.0 A 21.6 12.8
* 4 1 1500. 0. 0. 621. 0. 0. 621. 1500. 0. 0. 0. .41 62. 10.0 A 21.6 12.8
* 5 1 1400. 0. 0. 621. 0. 0. 621. 1500. 0. 0. 0. .41 62. 10.0 A 21.6 12.8
* 6 1 1500. 0. 0. 621. 0. 0. 621. 1500. 0. 0. 0. .41 62. 10.0 A 21.6 12.8
* 7 1 1300. 0. 621. 621. 0. 621. 621. 1500. 0. 0. 0. .41 62. 10.0 A 21.6 12.8
* 8
* 9
* 10
* 11
* 12
* 13
* 14
* 15
* 16
* 17
* 18
* 19
* 20
*****
*
* TOTAL 16700. = 3.2 MILES MAX(V/C) = 0.41 LOWEST LOS = A AVG = 62. 10.0 21.6 12.8
*
*****

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CURRENT TIME SLICE CUMULATIVE VALUES
FREEWAY TRAVEL TIME = 16. VEH-HRS 32. PASS-HRS 45. VEH-HRS 90. PASS-HRS
FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 16. VEH-HRS 32. PASS-HRS 45. VEH-HRS 90. PASS-HRS
TOTAL FRWAY TRAV DISTANCE = 982. VEH-MI. 1964. PASS-MI. 2788. VEH-MI. 5577. PASS-MI.
AVERAGE SYSTEM SPEED = 62. MPH. 62. MPH.
AVERAGE DENSITY = 10. VPML 9. VPML
TOTAL FUEL = 46. GALLONS 129. GALLONS
TOTAL EMISSIONS = 13. KILOGRAMS 36. KILOGRAMS

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***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
1 0.00 2 0.00 3 0.48 4 0.07 5 0.06
6 0.07 7 0.06 8 0.00 9 0.00 10 0.00
11 0.00 12 0.00 13 0.00 14 0.00 15 0.00
16 0.00 17 0.00 18 0.00 19 0.00 20 0.00
***** TOTAL DELAY = 0.7 VEH-HRS ***** AVERAGE DELAY = 0.07 MIN/VEH *****

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*****
**
** FREeway TRAVEL TIME (MINUTES) **
**
*****

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*****
* ORIGINS DESTINATIONS ACROSS *
* DOWN 1 2 3 4 5 6 7 8 *
+
* * * * *
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 2 * 0.00 3.06 0.00 0.00 0.00 0.00 0.00 0.00
+
* 3 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 4 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 5 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 8 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* * * * *
*****

```


TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB * SEC | * NO. * LNS | * SSEC * LENGTH | * O-D DATA * ORG DES | * DEMANDS * SSEC | * ADJUSTED * ORG DES | * VOLUMES * SSEC | * SSEC * CAP. | * WEAVE * EFF | * CONGEST * LENGTH | * STORAGE * RATE | * V/C * RATIO | * SPEED * MPH | * DENSITY * VPMP | * LOS * LEVEL | * FUEL * MPG | * EMISSIONS * GS/VM | |
|----------------|----------------|--------------------|-------------------------|---------------------|-------------------------|---------------------|------------------|------------------|-----------------------|---------------------|------------------|------------------|---------------------|------------------|-----------------|------------------------|------|
| * 1 | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | |
| * 3 | 1 | 11000. | 536. | 0. | 536. | 536. | 0. | 536. | 1500. | 0. | 0. | .36 | 62. | 8.6 | A | 21.6 | 12.8 |
| * 4 | 1 | 1500. | 0. | 0. | 536. | 0. | 0. | 536. | 1500. | 0. | 0. | .36 | 62. | 8.6 | A | 21.6 | 12.8 |
| * 5 | 1 | 1400. | 0. | 0. | 536. | 0. | 0. | 536. | 1500. | 0. | 0. | .36 | 62. | 8.6 | A | 21.6 | 12.8 |
| * 6 | 1 | 1500. | 0. | 0. | 536. | 0. | 0. | 536. | 1500. | 0. | 0. | .36 | 62. | 8.6 | A | 21.6 | 12.8 |
| * 7 | 1 | 1300. | 0. | 536. | 536. | 0. | 536. | 536. | 1500. | 0. | 0. | .36 | 62. | 8.6 | A | 21.6 | 12.8 |
| * 8 | | | | | | | | | | | | | | | | | |
| * 9 | | | | | | | | | | | | | | | | | |
| * 10 | | | | | | | | | | | | | | | | | |
| * 11 | | | | | | | | | | | | | | | | | |
| * 12 | | | | | | | | | | | | | | | | | |
| * 13 | | | | | | | | | | | | | | | | | |
| * 14 | | | | | | | | | | | | | | | | | |
| * 15 | | | | | | | | | | | | | | | | | |
| * 16 | | | | | | | | | | | | | | | | | |
| * 17 | | | | | | | | | | | | | | | | | |
| * 18 | | | | | | | | | | | | | | | | | |
| * 19 | | | | | | | | | | | | | | | | | |
| * 20 | | | | | | | | | | | | | | | | | |
| * TOTAL | 16700. | = | 3.2 | MILES | | | | | | | | MAX(V/C) = 0.36 | LOWEST LOS = A | AVG = 62. | 8.6 | 21.6 | 12.8 |

| | | |
|-----------------------------|--------------------|-------------------|
| | CURRENT TIME SLICE | CUMULATIVE VALUES |
| FREEWAY TRAVEL TIME = | 14. VEH-HRS | 27. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 14. VEH-HRS | 27. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 848. VEH-MI. | 1696. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 62. MPH. |
| AVERAGE DENSITY = | 9. VPMP | 9. VPMP |
| TOTAL FUEL = | 39. GALLONS | 214. GALLONS |
| TOTAL EMISSIONS = | 11. KILOGRAMS | 59. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.42 | 4 | 0.06 | 5 | 0.05 |
| 6 | 0.06 | 7 | 0.05 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 0.6 VEH-HRS ***** AVERAGE DELAY = 0.07 MIN/VEH *****

 ** FREeway TRAVEL TIME (MINUTES) **

| * ORIGINS * DOWN | * DESTINATIONS ACROSS * | | | | | | | |
|---------------------|-------------------------|------|------|------|------|------|------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 3.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|-------|-----------------------|-------|-------|-------|-------|-------|-------|---|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 17.57 | 0.00 | 20.76 | 21.31 | 21.32 | 21.50 | 22.03 | 24.22 | |
| * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| * 3 * | 0.00 | 0.00 | 1.17 | 1.72 | 1.73 | 1.92 | 2.45 | 4.63 | |
| * 4 * | 0.00 | 0.00 | 0.64 | 1.19 | 1.20 | 1.38 | 1.92 | 4.10 | |
| * 5 * | 0.00 | 0.00 | 0.09 | 0.64 | 0.65 | 0.83 | 1.36 | 3.55 | |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.12 | 0.13 | 0.31 | 0.85 | 3.03 | |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 | 0.71 | 2.89 | |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.53 | 2.72 | |

 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|-----------|----------|------------|-------------|------------|-------------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|
| * SEC LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 1 3 | 500. | 3570. | 0. 3570. | 3570. | 0. 3570. | 6000. | 0. | 0. | 0. | .60 | 65. | 18.3 | C | 19.0 | 14.1 |
| * 2 3 | 99999. | 0. | 571. 3570. | 0. | 571. 3570. | 6000. | 0. | 0. | 0. | .60 | 65. | 18.3 | C | 19.0 | 14.1 |
| * 3 2 | 11000. | 0. | 0. 2999. | 0. | 0. 2999. | 4000. | 0. | 0. | 0. | .75 | 62. | 24.2 | C | 20.3 | 13.0 |
| * 4 2 | 1500. | 40. | 0. 3039. | 40. | 0. 3039. | 4000. | 0. | 0. | 0. | .76 | 62. | 24.5 | C | 20.3 | 13.0 |
| * 5 2 | 1400. | 0. | 0. 3039. | 0. | 0. 3039. | 4000. | 0. | 0. | 0. | .76 | 62. | 24.5 | C | 20.3 | 13.0 |
| * 6 2 | 1500. | 590. | 0. 3629. | 590. | 0. 3629. | 4000. | 0. | 0. | 0. | .91 | 57. | 31.6 | D | 22.1 | 11.9 |
| * 7 2 | 1300. | 0. | 0. 3629. | 0. | 0. 3629. | 4000. | 0. | 0. | 0. | .91 | 57. | 31.6 | D | 22.1 | 11.9 |
| * 8 3 | 500. | 571. | 750. 4200. | 571. | 750. 4200. | 4950. | 0. | 0. | 0. | .85 | 65. | 21.5 | C | 19.0 | 14.1 |
| * 9 2 | 2300. | 0. | 0. 3450. | 0. | 0. 3450. | 4000. | 0. | 0. | 0. | .86 | 61. | 28.3 | D | 20.9 | 12.7 |
| * 10 3 | 250. | 570. | 0. 4020. | 570. | 0. 4020. | 4750. | 0. | 0. | 0. | .85 | 65. | 20.6 | C | 19.0 | 14.1 |
| * 11 3 | 200. | 0. | 0. 4020. | 0. | 0. 4020. | 4750. | 0. | 0. | 0. | .85 | 65. | 20.6 | C | 19.0 | 14.1 |
| * 12 3 | 250. | 0. | 1709. 4020. | 0. | 1709. 4020. | 4750. | 0. | 0. | 0. | .85 | 65. | 20.6 | C | 19.0 | 14.1 |
| * 13 2 | 50. | 0. | 0. 2311. | 0. | 0. 2311. | 4000. | 0. | 0. | 0. | .58 | 65. | 17.8 | B | 19.0 | 14.1 |
| * 14 2 | 50. | 0. | 0. 2311. | 0. | 0. 2311. | 2470. | 0. | 0. | 0. | .94 | 65. | 17.8 | B | 19.0 | 14.1 |
| * 15 2 | 1000. | 0. | 0. 2311. | 0. | 0. 2311. | 4000. | 0. | 0. | 0. | .58 | 65. | 17.8 | B | 19.0 | 14.1 |
| * 16 2 | 10. | 0. | 0. 2311. | 0. | 0. 2311. | 4000. | 0. | 0. | 0. | .58 | 65. | 17.8 | B | 19.0 | 14.1 |
| * 17 2 | 1500. | 686. | 0. 2997. | 686. | 0. 2997. | 4000. | 0. | 0. | 0. | .75 | 64. | 23.3 | C | 19.3 | 13.8 |
| * 18 2 | 1500. | 0. | 301. 2997. | 0. | 301. 2997. | 4000. | 0. | 0. | 0. | .75 | 64. | 23.3 | C | 19.3 | 13.8 |
| * 19 2 | 12000. | 0. | 0. 2696. | 0. | 0. 2696. | 4000. | 0. | 0. | 0. | .67 | 65. | 20.7 | C | 19.0 | 14.1 |
| * 20 3 | 500. | 0. | 2696. 2696. | 0. | 2696. 2696. | 6000. | 0. | 0. | 0. | .45 | 65. | 13.8 | B | 19.0 | 14.1 |

 *
 * TOTAL 137309. = 26.0 MILES MAX(V/C) = 0.94 LOWEST LOS = D AVG = 64. 19.7 19.2 13.9 *
 *

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|---|
| FREWAY TRAVEL TIME = | 689. VEH-HRS | 787. PASS-HRS 1378. VEH-HRS 1573. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 689. VEH-HRS | 787. PASS-HRS 1378. VEH-HRS 1573. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 44398. VEH-MI. | 50743. PASS-MI. 88797. VEH-MI. 101487. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 64. MPH. | 64. MPH. |
| AVERAGE DENSITY = | 20. VPMP | 20. VPMP |
| TOTAL FUEL = | 2314. GALLONS | 4629. GALLONS |
| TOTAL EMISSIONS = | 617. KILOGRAMS | 1234. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 2.33 | 4 | 0.32 | 5 | 0.30 |
| 6 | 1.04 | 7 | 0.90 | 8 | 0.00 | 9 | 0.76 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.08 | 18 | 0.08 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 5.8 VEH-HRS ***** AVERAGE DELAY = 0.11 MIN/VEH *****

 **
 ** FREEWAY TRAVEL TIME (MINUTES)
 **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|-------|-----------------------|-------|-------|-------|-------|-------|-------|---|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 17.57 | 0.00 | 20.88 | 22.06 | 22.13 | 22.31 | 22.86 | 25.04 | |
| * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| * 3 * | 0.00 | 0.00 | 1.25 | 2.43 | 2.50 | 2.68 | 3.23 | 5.42 | |
| * 4 * | 0.00 | 0.00 | 0.71 | 1.89 | 1.95 | 2.14 | 2.68 | 4.87 | |
| * 5 * | 0.00 | 0.00 | 0.10 | 1.28 | 1.34 | 1.53 | 2.07 | 4.26 | |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.40 | 0.46 | 0.65 | 1.19 | 3.38 | |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 | 0.72 | 2.91 | |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.55 | 2.73 | |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB | * NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | |
|-------|-------|----------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|--------|---------|-----------|---------|--------|-------------|------|------|------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * CAP. | * EFF | * LENGTH | * RATE | * MPH | * VP/PL | * LEVEL | * MPG | * GS/VM | | | |
| * 1 | 3 | 500. | 3880. | 0. | 3880. | 3880. | 0. | 3880. | 6000. | 0. | 0. | .65 | 65. | 19.9 | C | 19.0 | 14.1 | | |
| * 2 | 3 | 99999. | 0. | 621. | 3880. | 0. | 621. | 3880. | 6000. | 0. | 0. | .65 | 65. | 19.9 | C | 19.0 | 14.1 | | |
| * 3 | 2 | 11000. | 0. | 0. | 3259. | 0. | 0. | 3259. | 4000. | 0. | 0. | .81 | 61. | 26.8 | D | 21.0 | 12.6 | | |
| * 4 | 2 | 1500. | 50. | 0. | 3309. | 50. | 0. | 3309. | 4000. | 0. | 0. | .83 | 60. | 27.4 | D | 21.2 | 12.5 | | |
| * 5 | 2 | 1400. | 0. | 0. | 3309. | 0. | 0. | 3309. | 4000. | 0. | 0. | .83 | 60. | 27.4 | D | 21.2 | 12.5 | | |
| * 6 | 2 | 1500. | 661. | 0. | 3970. | 661. | 0. | 3970. | 4000. | 0. | 0. | .99 | 52. | 38.1 | E | 23.5 | 11.2 | | |
| * 7 | 2 | 1300. | 0. | 0. | 3970. | 0. | 0. | 3970. | 4000. | 0. | 0. | .99 | 52. | 38.1 | E | 23.5 | 11.2 | | |
| * 8 | 3 | 500. | 621. | 950. | 4591. | 621. | 950. | 4591. | 4950. | 0. | 0. | .93 | 58. | 26.6 | D | 22.1 | 11.9 | | |
| * 9 | 2 | 2300. | 0. | 0. | 3641. | 0. | 0. | 3479. | 4000. | 0. | ** | 2300. | 162. | .87 | 33. | 52.1 | F | 20.1 | 13.8 |
| * 10 | 3 | 250. | 590. | 0. | 4231. | 590. | 0. | 4069. | 4750. | 0. | ** | 250. | 162. | .86 | 22. | 62.7 | F | 17.5 | 16.6 |
| * 11 | 3 | 200. | 0. | 0. | 4231. | 0. | 0. | 4069. | 4750. | 0. | ** | 200. | 162. | .86 | 20. | 67.8 | F | 17.4 | 16.9 |
| * 12 | 3 | 250. | 0. | 1519. | 4231. | 0. | 1519. | 4069. | 4750. | 0. | ** | 250. | 162. | .86 | 19. | 72.9 | F | 17.2 | 17.2 |
| * 13 | 2 | 50. | 0. | 80. | 2712. | 0. | 80. | 2550. | 4000. | 0. | ** | 50. | 162. | .64 | 9. | 143.7 | F | 11.5 | 24.2 |
| * 14 | 2 | 50. | 0. | 0. | 2632. | 0. | 0. | 2470. | 2470. | 0. | 0. | 0. | 1.00 | 65. | 19.0 | E | 19.0 | 14.1 | |
| * 15 | 2 | 1000. | 80. | 0. | 2712. | 80. | 0. | 2550. | 4000. | 0. | 0. | .64 | 65. | 19.6 | C | 19.0 | 14.1 | | |
| * 16 | 2 | 10. | 0. | 0. | 2712. | 0. | 0. | 2550. | 4000. | 0. | 0. | .64 | 65. | 19.6 | C | 19.0 | 14.1 | | |
| * 17 | 2 | 1500. | 748. | 0. | 3460. | 748. | 0. | 3298. | 4000. | 0. | 0. | .82 | 62. | 26.4 | D | 20.1 | 13.2 | | |
| * 18 | 2 | 1500. | 0. | 690. | 3460. | 0. | 658. | 3298. | 4000. | 0. | 0. | .82 | 62. | 26.4 | D | 20.1 | 13.2 | | |
| * 19 | 2 | 12000. | 0. | 0. | 2770. | 0. | 0. | 2640. | 4000. | 0. | 0. | .66 | 65. | 20.3 | C | 19.0 | 14.1 | | |
| * 20 | 3 | 500. | 0. | 2770. | 2770. | 0. | 2640. | 2640. | 6000. | 0. | 0. | .44 | 65. | 13.5 | B | 19.0 | 14.1 | | |

* TOTAL 137309. = 26.0 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 62. 22.0 19.3 13.9 *

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 768. VEH-HRS | 877. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 768. VEH-HRS | 877. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 47882. VEH-MI. | 54718. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 64. MPH. |
| AVERAGE DENSITY = | 22. VP/PL | 20. VP/PL |
| TOTAL FUEL = | 2486. GALLONS | 7114. GALLONS |
| TOTAL EMISSIONS = | 663. KI LOGRAMS | 1897. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 3.70 | 4 | 0.55 | 5 | 0.51 |
| 6 | 2.14 | 7 | 1.85 | 8 | 0.43 | 9 | 11.35 | 10 | 3.00 |
| 11 | 2.68 | 12 | 3.71 | 13 | 1.18 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.30 | 18 | 0.30 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 31.7 VEH-HRS ***** AVERAGE DELAY = 0.53 MIN/VEH *****

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 TIME SLICE 4 OF 6

 ** FREeway TRAVEL TIME (MINUTES) **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN 1 2 3 4 5 6 7 8 *

| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|-------|-------|------|-------|-------|-------|-------|-------|-------|
| * 1 * | 17.57 | 0.00 | 21.52 | 23.40 | 23.46 | 23.65 | 24.20 | 26.38 |
| * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 3 * | 0.00 | 0.00 | 1.89 | 3.77 | 3.84 | 4.02 | 4.57 | 6.75 |
| * 4 * | 0.00 | 0.00 | 1.26 | 3.15 | 3.21 | 3.40 | 3.94 | 6.13 |
| * 5 * | 0.00 | 0.00 | 0.27 | 2.15 | 2.22 | 2.40 | 2.95 | 5.13 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.45 | 0.52 | 0.70 | 1.25 | 3.44 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 | 0.72 | 2.91 |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.55 | 2.73 |

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 TIME SLICE 4 OF 6

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB | NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED | VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS | | | |
|-------|-----|--------|----------|---------|----------|---------|-------|-------|---------|---------|-------|-------|---------|-------|------|--------|------|------|------|
| * SEC | LNS | LENGTH | ORG | DES | SSEC | ORG | DES | SSEC | LENGTH | RATE | RATIO | MPH | VPMP/L | LEVEL | MPG | GS/VM | | | |
| * 1 | 3 | 500. | 3880. | 0. | 3880. | 3880. | 0. | 3880. | 6000. | 0. | 0. | .65 | 65. | 19.9 | C | 19.0 | 14.1 | | |
| * 2 | 3 | 99999. | 0. | 621. | 3880. | 0. | 621. | 3880. | 6000. | 0. | 0. | .65 | 65. | 19.9 | C | 19.0 | 14.1 | | |
| * 3 | 2 | 11000. | 0. | 0. | 3259. | 0. | 0. | 3259. | 4000. | 0. | 0. | .81 | 61. | 26.8 | D | 21.0 | 12.6 | | |
| * 4 | 2 | 1500. | 50. | 0. | 3309. | 50. | 0. | 3309. | 4000. | 0. | 0. | .83 | 60. | 27.4 | D | 21.2 | 12.5 | | |
| * 5 | 2 | 1400. | 0. | 0. | 3309. | 0. | 0. | 3147. | 4000. | 0. | * | 805. | 162. | .79 | 47. | 33.8 | F | 20.5 | 13.2 |
| * 6 | 2 | 1500. | 661. | 0. | 3970. | 661. | 0. | 3808. | 4000. | 0. | ** | 1500. | 162. | .95 | 35. | 54.8 | F | 21.7 | 12.6 |
| * 7 | 2 | 1300. | 0. | 0. | 3970. | 0. | 0. | 3808. | 4000. | 0. | ** | 1300. | 162. | .95 | 29. | 65.2 | F | 20.7 | 13.4 |
| * 8 | 3 | 500. | 621. | 950. | 4591. | 621. | 950. | 4429. | 4950. | 0. | ** | 500. | 162. | .89 | 21. | 69.8 | F | 18.5 | 15.8 |
| * 9 | 2 | 2300. | 0. | 0. | 3641. | 0. | 0. | 3479. | 4000. | 0. | ** | 2300. | 162. | .87 | 18. | 95.0 | F | 17.5 | 17.1 |
| * 10 | 3 | 250. | 590. | 0. | 4231. | 590. | 0. | 4069. | 4750. | 0. | ** | 250. | 162. | .86 | 17. | 77.5 | F | 17.1 | 17.5 |
| * 11 | 3 | 200. | 0. | 0. | 4231. | 0. | 0. | 4069. | 4750. | 0. | ** | 200. | 162. | .86 | 17. | 77.5 | F | 17.1 | 17.5 |
| * 12 | 3 | 250. | 0. | 1519. | 4231. | 0. | 1519. | 4069. | 4750. | 0. | ** | 250. | 162. | .86 | 17. | 77.5 | F | 17.1 | 17.5 |
| * 13 | 2 | 50. | 0. | 80. | 2712. | 0. | 80. | 2550. | 4000. | 0. | ** | 50. | 162. | .64 | 9. | 145.6 | F | 11.4 | 24.4 |
| * 14 | 2 | 50. | 0. | 0. | 2632. | 0. | 0. | 2470. | 2470. | 0. | 0. | 1.00 | 65. | 19.0 | E | 19.0 | 14.1 | | |
| * 15 | 2 | 1000. | 80. | 0. | 2712. | 80. | 0. | 2550. | 4000. | 0. | 0. | .64 | 65. | 19.6 | C | 19.0 | 14.1 | | |
| * 16 | 2 | 10. | 0. | 0. | 2712. | 0. | 0. | 2550. | 4000. | 0. | 0. | .64 | 65. | 19.6 | C | 19.0 | 14.1 | | |
| * 17 | 2 | 1500. | 748. | 0. | 3460. | 748. | 0. | 3298. | 4000. | 0. | 0. | .82 | 62. | 26.4 | D | 20.1 | 13.2 | | |
| * 18 | 2 | 1500. | 0. | 690. | 3460. | 0. | 658. | 3298. | 4000. | 0. | 0. | .82 | 62. | 26.4 | D | 20.1 | 13.2 | | |
| * 19 | 2 | 12000. | 0. | 0. | 2770. | 0. | 0. | 2640. | 4000. | 0. | 0. | .66 | 65. | 20.3 | C | 19.0 | 14.1 | | |
| * 20 | 3 | 500. | 0. | 2770. | 2770. | 0. | 2640. | 2640. | 6000. | 0. | 0. | .44 | 65. | 13.5 | B | 19.0 | 14.1 | | |

 * TOTAL 137309. = 26.0 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 59. 23.4 19.2 14.0 *

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 809. VEH-HRS | 922. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 809. VEH-HRS | 922. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 47823. VEH-MI. | 54654. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 59. MPH. | 62. MPH. |

AVERAGE DENSITY = 23. VPML
 TOTAL FUEL = 2496. GALLONS
 TOTAL EMISSIONS = 668. KILOGRAMS

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 21. VPML
 9610. GALLONS
 2565. KILOGRAMS

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 TIME SLICE 4 OF 6

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 3.70 | 4 | 0.55 | 5 | 2.65 |
| 6 | 7.40 | 7 | 8.95 | 8 | 6.71 | 9 | 29.74 | 10 | 4.02 |
| 11 | 3.22 | 12 | 4.02 | 13 | 1.19 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.30 | 18 | 0.30 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 72.8 VEH-HRS ***** AVERAGE DELAY = 1.20 MIN/VEH *****

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 TIME SLICE 5 OF 6

QUEUE CLEAR SECTION 13 T2= 0.476

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 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF NON-PRIORITY LANES
 TIME SLICE 5 OF 6

 ** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS | * DESTINATIONS ACROSS * | | | | | | | |
|-----------|-------------------------|------|-------|-------|-------|-------|-------|-------|
| * DOWN | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 17.57 | 0.00 | 21.16 | 22.65 | 22.70 | 22.88 | 23.46 | 25.68 |
| * 2 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 3 * | 0.00 | 0.00 | 1.58 | 3.06 | 3.11 | 3.30 | 3.88 | 6.09 |
| * 4 * | 0.00 | 0.00 | 1.01 | 2.50 | 2.55 | 2.73 | 3.31 | 5.52 |
| * 5 * | 0.00 | 0.00 | 0.21 | 1.69 | 1.74 | 1.93 | 2.51 | 4.72 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.43 | 0.48 | 0.67 | 1.25 | 3.46 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 | 0.75 | 2.97 |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.58 | 2.79 |

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 TIME SLICE 5 OF 6

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | |
|-----------|--------|------------|-----------|------------|-----------|---------|---------|-----------|-----------|-------|----------|-----------|---------|--------|-------------|---------|--------|---------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPML | * LEVEL | * MPG | * GS/VM |
| * 1 | * 3 | * 500. | * 3351. | * 0. | * 3351. | * 3351. | * 0. | * 3351. | * 6000. | * 0. | * 0. | * 0. | * .56 | * 65. | * 17.2 | * B | * 19.0 | * 14.1 |
| * 2 | * 3 | * 99999. | * 0. | * 536. | * 3351. | * 0. | * 536. | * 3351. | * 6000. | * 0. | * 0. | * 0. | * .56 | * 65. | * 17.2 | * B | * 19.0 | * 14.1 |
| * 3 | * 2 | * 11000. | * 0. | * 0. | * 2815. | * 0. | * 0. | * 2815. | * 4000. | * 0. | * 0. | * 0. | * .70 | * 62. | * 22.7 | * C | * 20.3 | * 13.0 |
| * 4 | * 2 | * 1500. | * 51. | * 0. | * 2866. | * 51. | * 0. | * 2866. | * 4000. | * 0. | * 0. | * 0. | * .72 | * 62. | * 23.1 | * C | * 20.3 | * 13.0 |
| * 5 | * 2 | * 1400. | * 0. | * 0. | * 2866. | * 0. | * 0. | * 2866. | * 4000. | * 0. | * 0. | * 0. | * .72 | * 55. | * 26.2 | * D | * 20.1 | * 13.3 |
| * 6 | * 2 | * 1500. | * 440. | * 0. | * 3306. | * 440. | * 0. | * 3306. | * 4000. | * 0. | * 0. | * 0. | * .83 | * 43. | * 38.3 | * E | * 20.6 | * 13.2 |
| * 7 | * 2 | * 1300. | * 0. | * 0. | * 3306. | * 0. | * 0. | * 3306. | * 4000. | * 0. | * 0. | * 0. | * .83 | * 36. | * 45.8 | * F | * 20.2 | * 13.6 |
| * 8 | * 3 | * 500. | * 536. | * 671. | * 3842. | * 536. | * 671. | * 3842. | * 4950. | * 0. | * 0. | * 0. | * .78 | * 27. | * 46.9 | * F | * 18.0 | * 15.8 |
| * 9 | * 2 | * 2300. | * 0. | * 0. | * 3171. | * 0. | * 0. | * 3171. | * 4000. | * 0. | * 0. | * 0. | * .79 | * 25. | * 63.8 | * F | * 18.6 | * 15.5 |
| * 10 | * 3 | * 250. | * 459. | * 0. | * 3630. | * 459. | * 0. | * 3630. | * 4750. | * 0. | * 0. | * 0. | * .76 | * 19. | * 63.8 | * F | * 17.1 | * 17.3 |
| * 11 | * 3 | * 200. | * 0. | * 0. | * 3630. | * 0. | * 0. | * 3630. | * 4750. | * 0. | * 0. | * 0. | * .76 | * 18. | * 65.8 | * F | * 17.0 | * 17.4 |
| * 12 | * 3 | * 250. | * 0. | * 1240. | * 3630. | * 0. | * 1240. | * 3630. | * 4750. | * 0. | * 0. | * 0. | * .76 | * 18. | * 67.7 | * F | * 17.0 | * 17.6 |
| * 13 | * 2 | * 50. | * 0. | * 310. | * 2390. | * 0. | * 310. | * 2780. | * 4000. | * 0. | * 0. | * 0. | * .69 | * 11. | * 128.0 | * F | * 13.4 | * 22.2 |
| * 14 | * 2 | * 50. | * 0. | * 0. | * 2080. | * 0. | * 0. | * 2470. | * 2470. | * 0. | * 0. | * 0. | * 1.00 | * 65. | * 19.0 | * E | * 19.0 | * 14.1 |
| * 15 | * 2 | * 1000. | * 310. | * 0. | * 2390. | * 310. | * 0. | * 2780. | * 4000. | * 0. | * 0. | * 0. | * .69 | * 65. | * 21.4 | * C | * 19.0 | * 14.1 |
| * 16 | * 2 | * 10. | * 0. | * 0. | * 2390. | * 0. | * 0. | * 2780. | * 4000. | * 0. | * 0. | * 0. | * .69 | * 65. | * 21.4 | * C | * 19.0 | * 14.1 |
| * 17 | * 2 | * 1500. | * 830. | * 0. | * 3220. | * 830. | * 0. | * 3610. | * 4000. | * 0. | * 0. | * 0. | * .90 | * 59. | * 30.6 | * D | * 21.6 | * 12.2 |
| * 18 | * 2 | * 1500. | * 0. | * 530. | * 3220. | * 0. | * 594. | * 3610. | * 4000. | * 0. | * 0. | * 0. | * .90 | * 59. | * 30.6 | * D | * 21.6 | * 12.2 |
| * 19 | * 2 | * 12000. | * 0. | * 0. | * 2690. | * 0. | * 0. | * 3016. | * 4000. | * 0. | * 0. | * 0. | * .75 | * 64. | * 23.5 | * C | * 19.4 | * 13.8 |

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```

* 20 3 500. 0. 2690. 2690. 0. 3016. 3016. 6000. 0. 0. 0. .50 65. 15.5 B 19.0 14.1 *
*
*****
* TOTAL 137309. = 26.0 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 61. 20.3 19.2 13.9 *
*
*****

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CURRENT TIME SLICE CUMULATIVE VALUES
FREEWAY TRAVEL TIME = 704. VEH-HRS 804. PASS-HRS 3659. VEH-HRS 4177. PASS-HRS
FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 704. VEH-HRS 804. PASS-HRS 3659. VEH-HRS 4177. PASS-HRS
TOTAL FRWAY TRAV DISTANCE = 42606. VEH-MI. 48707. PASS-MI. 227108. VEH-MI. 259565. PASS-MI.
AVERAGE SYSTEM SPEED = 61. MPH. 62. MPH
AVERAGE DENSITY = 20. VPMP 21. VPMP
TOTAL FUEL = 2222. GALLONS 11832. GALLONS
TOTAL EMISSIONS = 594. KILOGRAMS 3160. KILOGRAMS

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TIME SLICE 5 OF 6

```

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
1 0.00 2 0.00 3 2.18 4 0.30 5 1.10
6 3.75 7 5.22 8 4.05 9 18.57 10 3.50
11 2.93 12 3.83 13 1.00 14 0.00 15 0.00
16 0.00 17 0.80 18 0.80 19 0.72 20 0.00
***** TOTAL DELAY = 48.7 VEH-HRS ***** AVERAGE DELAY = 0.89 MIN/VEH *****

```

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UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF NON-PRIORITY LANES
TIME SLICE 6 OF 6

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*****
** FREEWAY TRAVEL TIME (MINUTES) **
*****

```

| * ORIGINS | | * DESTINATIONS ACROSS * | | | | | | | |
|-----------|---|-------------------------|------|-------|-------|-------|-------|-------|-------|
| * DOWN * | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| + | * | ***** | | | | | | | |
| + | * | ***** | | | | | | | |
| + | * | 17.57 | 0.00 | 20.73 | 21.27 | 21.28 | 21.46 | 22.00 | 24.19 |
| + | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * | 0.00 | 0.00 | 1.15 | 1.68 | 1.69 | 1.87 | 2.42 | 4.60 |
| + | * | 0.00 | 0.00 | 0.61 | 1.15 | 1.16 | 1.34 | 1.88 | 4.07 |
| + | * | 0.00 | 0.00 | 0.09 | 0.62 | 0.63 | 0.81 | 1.36 | 3.54 |
| + | * | 0.00 | 0.00 | 0.00 | 0.12 | 0.13 | 0.31 | 0.86 | 3.04 |
| + | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 | 0.72 | 2.90 |
| + | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.54 | 2.73 |
| + | * | ***** | | | | | | | |

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TIME SLICE 6 OF 6

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SEC LNS | * SSEC LENGTH | * O-D DATA ORG | * DEMANDS DES | * SSEC | * ADJUSTED ORG | * VOLUMES DES | * SSEC | * SSEC CAP. | * WEAVE EFF | * CONGEST LENGTH | * STORAGE RATE | * V/C RATIO | * SPEED MPH | * DENSITY VPMP | * LOS LEVEL | * FUEL MPG | * EMISSIONS GS/VM |
|-----------|-----------|---------------|----------------|---------------|---------|----------------|---------------|---------|-------------|-------------|------------------|----------------|-------------|-------------|----------------|-------------|------------|-------------------|
| * 1 | * 3 | * 500. | * 3351. | * 0. | * 3351. | * 3351. | * 0. | * 3351. | * 6000. | * 0. | * 0. | * 0. | * .56 | * 65. | * 17.2 | * B | * 19.0 | * 14.1 |
| * 2 | * 3 | * 99999. | * 0. | * 536. | * 3351. | * 0. | * 536. | * 3351. | * 6000. | * 0. | * 0. | * 0. | * .56 | * 65. | * 17.2 | * B | * 19.0 | * 14.1 |
| * 3 | * 2 | * 11000. | * 0. | * 0. | * 2815. | * 0. | * 0. | * 2815. | * 4000. | * 0. | * 0. | * 0. | * .70 | * 62. | * 22.7 | * C | * 20.3 | * 13.0 |
| * 4 | * 2 | * 1500. | * 51. | * 0. | * 2866. | * 51. | * 0. | * 2866. | * 4000. | * 0. | * 0. | * 0. | * .72 | * 62. | * 23.1 | * C | * 20.3 | * 13.0 |
| * 5 | * 2 | * 1400. | * 0. | * 0. | * 2866. | * 0. | * 0. | * 2866. | * 4000. | * 0. | * 0. | * 0. | * .72 | * 62. | * 23.1 | * C | * 20.3 | * 13.0 |
| * 6 | * 2 | * 1500. | * 440. | * 0. | * 3306. | * 440. | * 0. | * 3306. | * 4000. | * 0. | * 0. | * 0. | * .83 | * 60. | * 27.4 | * D | * 21.1 | * 12.5 |
| * 7 | * 2 | * 1300. | * 0. | * 0. | * 3306. | * 0. | * 0. | * 3306. | * 4000. | * 0. | * 0. | * 0. | * .83 | * 60. | * 27.4 | * D | * 21.1 | * 12.5 |
| * 8 | * 3 | * 500. | * 536. | * 671. | * 3842. | * 536. | * 671. | * 3842. | * 4950. | * 0. | * 0. | * 0. | * .78 | * 65. | * 19.7 | * C | * 19.0 | * 14.1 |
| * 9 | * 2 | * 2300. | * 0. | * 0. | * 3171. | * 0. | * 0. | * 3171. | * 4000. | * 0. | * 0. | * 0. | * .79 | * 63. | * 25.0 | * C | * 19.7 | * 13.5 |

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| | | | | | | | | | | | | | | | | | | | |
|-------|-------|---|---------|------|------------|-------|-----------------|-------|----------------|-------|-----------|----|------|-----|------|---|------|------|---|
| * | 10 | 3 | 250. | 459. | 0. | 3630. | 459. | 0. | 3630. | 4750. | 0. | 0. | .76 | 65. | 18.6 | C | 19.0 | 14.1 | * |
| * | 11 | 3 | 200. | 0. | 0. | 3630. | 0. | 0. | 3630. | 4750. | 0. | 0. | .76 | 65. | 18.6 | C | 19.0 | 14.1 | * |
| * | 12 | 3 | 250. | 0. | 1240. | 3630. | 0. | 1240. | 3630. | 4750. | 0. | 0. | .76 | 65. | 18.6 | C | 19.0 | 14.1 | * |
| * | 13 | 2 | 50. | 0. | 310. | 2390. | 0. | 310. | 2390. | 4000. | 0. | 0. | .60 | 65. | 18.4 | C | 19.0 | 14.1 | * |
| * | 14 | 2 | 50. | 0. | 0. | 2080. | 0. | 0. | 2080. | 2470. | 0. | 0. | .84 | 65. | 16.0 | B | 19.0 | 14.1 | * |
| * | 15 | 2 | 1000. | 310. | 0. | 2390. | 310. | 0. | 2390. | 4000. | 0. | 0. | .60 | 65. | 18.4 | C | 19.0 | 14.1 | * |
| * | 16 | 2 | 10. | 0. | 0. | 2390. | 0. | 0. | 2390. | 4000. | 0. | 0. | .60 | 65. | 18.4 | C | 19.0 | 14.1 | * |
| * | 17 | 2 | 1500. | 830. | 0. | 3220. | 830. | 0. | 3220. | 4000. | 0. | 0. | .81 | 63. | 25.6 | C | 19.9 | 13.4 | * |
| * | 18 | 2 | 1500. | 0. | 530. | 3220. | 0. | 530. | 3220. | 4000. | 0. | 0. | .81 | 63. | 25.6 | C | 19.9 | 13.4 | * |
| * | 19 | 2 | 12000. | 0. | 0. | 2690. | 0. | 0. | 2690. | 4000. | 0. | 0. | .67 | 65. | 20.7 | C | 19.0 | 14.1 | * |
| * | 20 | 3 | 500. | 0. | 2690. | 2690. | 0. | 2690. | 2690. | 6000. | 0. | 0. | .45 | 65. | 13.8 | B | 19.0 | 14.1 | * |
| ***** | | | | | | | | | | | | | | | | | | | |
| * | TOTAL | | 137309. | = | 26.0 MILES | | MAX(V/C) = 0.84 | | LOWEST LOS = D | | AVG = 65. | | 18.6 | | 19.2 | | 13.9 | | * |
| ***** | | | | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|------------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 650. VEH-HRS | 4309. VEH-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 650. VEH-HRS | 4309. VEH-HRS |
| TOTAL FRWAY TRAV DI STANCE = | 41949. VEH-MI. | 269057. VEH-MI. |
| AVERAGE SYSTEM SPEED = | 65. MPH | 62. MPH |
| AVERAGE DENSITY = | 19. VPMPPL | 21. VPMPPL |
| TOTAL FUEL = | 2189. GALLONS | 14021. GALLONS |
| TOTAL EMISSIONS = | 584. KILOGRAMS | 3743. KILOGRAMS |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF NON-PRIORITY LANES
 TIME SLICE 6 OF 6

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 2.18 | 4 | 0.30 | 5 | 0.28 |
| 6 | 0.55 | 7 | 0.47 | 8 | 0.00 | 9 | 0.28 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.22 | 18 | 0.22 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 4.5 VEH-HRS ***** AVERAGE DELAY = 0.09 MIN/VEH *****

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A.D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP EEE
FFFFFFFF RRRRRRRR EEEEE QQQ QQQ 1111 222 PPPPPPPP EEEEE
FFFFFFFF RRRRRRRR EEEEE QQQ QQQ 1111 222 PPPPPPPP EEEEE
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 2222222222 PPP EEEEEEEEE

FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 35
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREEWAY AND ARTERIAL DESIGN FEATURES

| ** SUB NO. | ** SEC LNS | ** SSEC CAP | ** SSEC LENGTH | ** DESIGN SPEED | ** ORG DES | ** TRK FAC | ** SSEC GRAD | ** PCT TRK | ** PCT DES TRUCKS | ** SPECIAL RAMP | ** FF.SPD. ALT. RTE | ** CAP. ALT. RTE | ** ART TYPE | ** GRADE ALT. RTE | ** SUBSECTION | ** LOCATION |
|------------|------------|-------------|----------------|-----------------|------------|------------|--------------|------------|-------------------|-----------------|---------------------|------------------|-------------|-------------------|--------------------------|-------------|
| ** 1 | 5 | 12500. | 500. | 65 | OD | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Seeding | ** |
| ** 2 | 3 | 8660. | 99999. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | ** |
| ** 3 | 3 | 7000. | 2830. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-87 to DLC loop-on | ** |
| ** 4 | 3 | 7000. | 930. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | DLC loop on to dia-on | ** |
| ** 5 | 3 | 7000. | 1490. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | DLC dia-on to Tomas off | ** |
| ** 6 | 3 | 7000. | 3020. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas off to on | ** |
| ** 7 | 3 | 7000. | 1030. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas on to bowers off | ** |
| ** 8 | 3 | 7000. | 1440. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers off to loop-on | ** |
| ** 9 | 3 | 7000. | 1430. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers loop-on to dia | ** |
| ** 10 | 3 | 7000. | 3480. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers dia-on to law-off | ** |
| ** 11 | 3 | 7000. | 1020. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Law off to loop-on | ** |
| ** 12 | 3 | 7000. | 980. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawr Loop to diag | ** |
| ** 13 | 3 | 7000. | 1800. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Lawrence On-ramp | ** |
| ** 14 | 3 | 7000. | 1500. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks Off-Ramp | ** |
| ** 15 | 3 | 6000. | 1300. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Fair Oaks | ** |
| ** 16 | 3 | 6000. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Fair Oaks On-Ramp | ** |
| ** 17 | 3 | 6000. | 1100. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Mathilda | ** |
| ** 18 | 3 | 6000. | 1000. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda NB Off-Ramp | ** |
| ** 19 | 3 | 6000. | 900. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | ** |
| ** 20 | 3 | 6000. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda NB On-Ramp | ** |

FREeway AND ARTERIAL DESIGN FEATURES

| SUB NO. | SEC | LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT TRUCKS | DES RAMP | SPECIAL ALT. RTE | FF. SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION | LOCATION |
|---------|-----|-----|----------|-------------|--------------|---------|---------|-----------|---------|------------|----------|------------------|-------------------|---------------|----------|----------------------|------------|----------|
| ** 21 | 3 | 3 | 6000. | 100. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | | |
| ** 22 | 3 | 3 | 6000. | 100. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda SB Off-ramp | | |
| ** 23 | 3 | 3 | 6000. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / SR-237 | | |
| ** 24 | 3 | 3 | 6000. | 1500. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 WB Off-Ramp | | |
| ** 25 | 3 | 3 | 6000. | 800. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 / SR-237 | | |
| ** 26 | 3 | 3 | 6000. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 WB On-Ramp | | |
| ** 27 | 3 | 3 | 6000. | 800. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 / Ellis | | |
| ** 28 | 3 | 3 | 6000. | 1000. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Ellis Off-ramp | | |
| ** 29 | 3 | 3 | 6000. | 8000. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | | |
| ** 30 | 5 | 5 | 10000. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | | |
| ** 31 | 5 | 5 | 6000. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Dummy Bottleneck | | |
| ** 32 | 5 | 5 | 6000. | 2640. | 65 | D | 1.00 | 0.0 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End of Network | | |

***** INPUT HAS BEEN COMPLETED *****

QUEUE COLLISION IN SECTION 18 T2 =0.582
 QUEUE COLLISION IN SECTION 16 T2 =0.631
 QUEUE COLLISION IN SECTION 15 T2 =0.468
 QUEUE COLLISION IN SECTION 14 T2 =0.491

FREeway TRAVEL TIME (MINUTES)

| ORIGINS DOWN | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
|--------------|------|-------|-------|-------|-------|-------|-------|
| * 1 * | 0.09 | 26.31 | 28.37 | 28.98 | 30.31 | 32.75 | 41.19 |
| * 2 * | 0.00 | 0.00 | 1.28 | 1.89 | 3.22 | 5.66 | 14.10 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.15 | 1.48 | 3.91 | 12.35 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.69 | 10.13 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.80 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.64 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB SEC | NO. LNS | SSEC LENGTH | O-D ORG | DATA DES | DEMANDS SSEC | ADJUSTED ORG | VOLUMES DES | SSEC SSEC | WEAVE CAP. | CONGEST EFF | STORAGE LENGTH | V/C RATIO | SPEED MPH | DENSITY VP/MPH | LOS LEVEL | FUEL MPG | EMI SS GS/VM | | |
|---------|---------|-------------|---------|----------|--------------|--------------|-------------|-----------|-----------------|----------------|----------------|-----------|-----------|----------------|-----------|----------|--------------|------|------|
| * | 1 | 5 | 500. | 8471. | 1609. | 8471. | 8471. | 1609. | 8471. | 12500. | 0. | 0. | 0. | .68 | 65. | 26.1 | D | 19.2 | 14.0 |
| * | 2 | 3 | 99999. | 0. | 0. | 6862. | 0. | 0. | 4634. | 8660. | 0. | * 742. | 2228. | .54 | 63. | 24.4 | F | 19.9 | 13.4 |
| * | 3 | 3 | 2830. | 0. | 0. | 6862. | 0. | 0. | 4634. | 7000. | 0. | ** 2830. | 2228. | .66 | 46. | 33.9 | F | 22.7 | 11.8 |
| * | 4 | 3 | 930. | 0. | 0. | 6862. | 0. | 0. | 4634. | 7000. | 0. | ** 930. | 2228. | .66 | 41. | 37.7 | F | 22.1 | 12.1 |
| * | 5 | 3 | 1490. | 0. | 0. | 6862. | 0. | 0. | 4634. | 7000. | 0. | ** 1490. | 2228. | .66 | 38. | 40.1 | F | 21.8 | 12.4 |
| * | 6 | 3 | 3020. | 0. | 0. | 6862. | 0. | 0. | 4634. | 7000. | 0. | ** 3020. | 2228. | .66 | 34. | 44.9 | F | 21.2 | 12.8 |
| * | 7 | 3 | 1030. | 0. | 0. | 6862. | 0. | 0. | 4634. | 7000. | 0. | ** 1030. | 2228. | .66 | 31. | 49.3 | F | 20.7 | 13.3 |
| * | 8 | 3 | 1440. | 0. | 0. | 6862. | 0. | 0. | 4634. | 7000. | 0. | ** 1440. | 2228. | .66 | 30. | 52.1 | F | 20.4 | 13.5 |
| * | 9 | 3 | 1430. | 0. | 0. | 6862. | 0. | 0. | 4634. | 7000. | 0. | ** 1430. | 2228. | .66 | 28. | 55.4 | F | 20.0 | 13.8 |
| * | 10 | 3 | 3480. | 0. | 0. | 6862. | 0. | 0. | 4634. | 7000. | 0. | ** 3480. | 2228. | .66 | 25. | 61.3 | F | 19.4 | 14.4 |
| * | 11 | 3 | 1020. | 0. | 0. | 6862. | 0. | 0. | 4634. | 7000. | 0. | ** 1020. | 2228. | .66 | 23. | 66.9 | F | 18.8 | 14.9 |
| * | 12 | 3 | 980. | 0. | 0. | 6862. | 0. | 0. | 4634. | 7000. | 0. | ** 980. | 2228. | .66 | 22. | 69.5 | F | 18.6 | 15.2 |
| * | 13 | 3 | 1800. | 0. | 0. | 6862. | 0. | 0. | 4634. | 7000. | 0. | ** 1800. | 2228. | .66 | 21. | 73.2 | F | 18.2 | 15.5 |
| * | 14 | 3 | 1500. | 0. | 770. | 6862. | 0. | 765. | 4634. | 6820. | 0. | ** 1500. | 2185. | .68 | 21. | 74.0 | F | 18.3 | 15.6 |
| * | 15 | 3 | 1300. | 0. | 0. | 6092. | 0. | 0. | 3869. | 6000. | 0. | ** 1300. | 2131. | .64 | 19. | 67.9 | F | 17.8 | 16.1 |
| * | 16 | 3 | 1000. | 653. | 0. | 6745. | 553. | 0. | 4422. | 5903. | 0. | ** 1000. | 1481. | .75 | 29. | 51.6 | F | 20.5 | 13.7 |
| * | 17 | 3 | 1100. | 0. | 0. | 6745. | 0. | 0. | 4422. | 6000. | 0. | ** 1100. | 1481. | .74 | 27. | 54.3 | F | 19.9 | 14.1 |
| * | 18 | 3 | 1000. | 0. | 521. | 6745. | 0. | 455. | 4422. | 5891. | 0. | ** 1000. | 1469. | .75 | 27. | 54.9 | F | 20.2 | 14.1 |
| * | 19 | 3 | 900. | 0. | 0. | 6224. | 0. | 0. | 3967. | 6000. | 0. | ** 900. | 1469. | .66 | 22. | 59.9 | F | 17.8 | 15.9 |
| * | 20 | 3 | 100. | 215. | 0. | 6439. | 215. | 0. | 4182. | 5965. | 0. | ** 100. | 1469. | .70 | 23. | 59.9 | F | 18.5 | 15.3 |
| * | 21 | 3 | 100. | 0. | 0. | 6439. | 0. | 0. | 4182. | 6000. | 0. | ** 100. | 1469. | .70 | 23. | 60.7 | F | 18.4 | 15.5 |
| * | 22 | 3 | 100. | 0. | 533. | 6439. | 0. | 468. | 4182. | 5893. | 0. | ** 100. | 1469. | .71 | 23. | 59.5 | F | 18.7 | 15.2 |
| * | 23 | 3 | 700. | 0. | 0. | 5906. | 0. | 0. | 3714. | 6000. | 0. | ** 700. | 1469. | .62 | 19. | 65.0 | F | 16.5 | 17.0 |
| * | 24 | 3 | 1500. | 0. | 833. | 5906. | 0. | 731. | 3714. | 5833. | 0. | ** 1500. | 1469. | .64 | 19. | 66.5 | F | 16.8 | 17.0 |
| * | 25 | 3 | 800. | 0. | 0. | 5073. | 0. | 0. | 2983. | 6000. | 0. | ** 800. | 1469. | .50 | 12. | 81.1 | F | 12.9 | 20.1 |
| * | 26 | 3 | 1000. | 1173. | 0. | 6246. | 1173. | 0. | 4156. | 5748. | 0. | ** 1000. | 1469. | .72 | 20. | 68.4 | F | 18.0 | 16.1 |
| * | 27 | 3 | 800. | 0. | 0. | 6246. | 0. | 0. | 4156. | 6000. | 0. | ** 800. | 1469. | .69 | 18. | 75.8 | F | 17.0 | 17.1 |
| * | 28 | 3 | 1000. | 0. | 458. | 6246. | 0. | 414. | 4156. | 5928. | 0. | ** 1000. | 1469. | .70 | 18. | 76.9 | F | 17.0 | 17.2 |
| * | 29 | 3 | 8000. | 0. | 0. | 5788. | 0. | 0. | 3742. | 6000. | 0. | ** 8000. | 1469. | .62 | 12. | 104.9 | F | 14.0 | 20.8 |
| * | 30 | 5 | 100. | 1358. | 0. | 7146. | 1358. | 0. | 5100. | 10000. | 0. | ** 100. | 1469. | .51 | 7. | 147.9 | F | 9.8 | 26.4 |
| * | 31 | 5 | 1000. | 1000. | 0. | 8146. | 900. | 0. | 6000. | 6000. | 0. | 0. | 0. | 1.00 | 65. | 18.5 | E | 19.2 | 14.0 |
| * | 32 | 5 | 2640. | 0. | 8146. | 8146. | 0. | 6000. | 6000. | 6000. | 0. | 0. | 0. | 1.00 | 65. | 18.5 | E | 20.0 | 13.7 |
| * | ***** | | | | | | | | | | | | | | | | | | |
| * | TOTAL | 144589. | = | 27.4 | MILES | | | | MAX(V/C) = 1.00 | LOWEST LOS = F | AVG = 44. | 36.3 | 19.5 | 13.9 | | | | | |
| * | ***** | | | | | | | | | | | | | | | | | | |

| CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | | | |
|----------------------------|--------------------------|-----------------------|----------------------|--------------------------------|-----------------|------------|---------|------------|----------------------|
| FREWAY TRAVEL TIME = | 3993. | VEH-HRS | 4014. | PASS-HRS | 3993. | VEH-HRS | 4014. | PASS-HRS | |
| FREWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS | |
| ON-RAMP MRG/CAP DELAY = | 100. | VEH-HRS | 110. | PASS-HRS | 100. | VEH-HRS | 110. | PASS-HRS | |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS | |
| TOTAL SYSTEM TRAVEL TIME = | 4093. | VEH-HRS | 4123. | PASS-HRS | 4093. | VEH-HRS | 4123. | PASS-HRS | |
| TOTAL TRAVEL DISTANCE = | 175909. | VEH-MI. | 176942. | PASS-MI. | 175909. | VEH-MI. | 176942. | PASS-MI. | |
| AVERAGE SYSTEM SPEED = | 43. | MPH. | | | 44. | MPH. | | | |
| AVERAGE DENSITY = | 36. | VP/MPH | | | 36. | VP/MPH | | | |
| TOTAL FUEL = | 9039. | GALLONS | | | 9039. | GALLONS | | | |
| TOTAL EMISSIONS = | 2456. | KI LOGRAMS | | | 2456. | KI LOGRAMS | | | |
| ***** | | | | | | | | | |
| ***** | MAINLINE DELAY (VEH-HRS) | ***** | DESIRED SPEED = 65.0 | ***** | | | | | |
| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
| 1 | 0.02 | 2 | 54.19 | 3 | 23.61 | 4 | 10.47 | 5 | 19.56 |
| 6 | 50.20 | 7 | 20.35 | 8 | 31.21 | 9 | 34.17 | 10 | 96.39 |
| 11 | 31.81 | 12 | 32.08 | 13 | 62.79 | 14 | 52.42 | 15 | 44.35 |
| 16 | 19.85 | 17 | 23.71 | 18 | 21.75 | 19 | 24.27 | 20 | 2.59 |
| 21 | 2.64 | 22 | 2.55 | 23 | 21.94 | 24 | 47.81 | 25 | 36.07 |
| 26 | 30.37 | 27 | 27.91 | 28 | 35.26 | 29 | 414.05 | 30 | 12.54 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |
| ***** | TOTAL DELAY = | 1286.9 | VEH-HRS | ***** | AVERAGE DELAY = | 18.76 | MIN/VEH | ***** | |
| ***** | | | | | | | | | |
| ***** | RAMP DELAYS | ***** | | | | | | | |
| ON-RAMP | 2 | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
| | | RAMP | 100. | 50.00 | 4.59 | 17.85 | 1.11 | 5.79 | 0.31 |
| | | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 50.00 | 4.59 | 17.85 | 1.11 | 5.79 | 0.31 |
| ON-RAMP | 6 | RAMP | 100. | 50.00 | 3.70 | 17.85 | 1.11 | 5.79 | 0.31 |
| | | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 50.00 | 3.70 | 17.85 | 1.11 | 5.79 | 0.31 |

**

| ORIGINS | | DESTINATIONS ACROSS | | | | | | |
|---------|--|---------------------|-------|-------|-------|-------|-------|-------|
| DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | | 0.09 | 32.25 | 34.21 | 34.88 | 36.37 | 39.09 | 47.00 |
| * 2 * | | 0.00 | 0.00 | 1.19 | 1.86 | 3.35 | 6.07 | 13.98 |
| * 3 * | | 0.00 | 0.00 | 0.00 | 0.15 | 1.64 | 4.36 | 12.27 |
| * 4 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.80 | 9.71 |
| * 5 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.79 |
| * 6 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.64 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED | VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS | | | |
|---------|--------|----------|-------------|----------|---------|-------|-------|---------|---------|-------|----------|---------|-------|------|--------|------|------|------|
| SEC LNS | LENGTH | ORG DES | SSEC | ORG DES | SSEC | CAP. | EFF | LENGTH | RATE | RATIO | MPH | VPMP | LEVEL | MPG | GS/VM | | | |
| * 1 | 5 | 500. | 7320. 1391. | 7320. | 7320. | 1391. | 7320. | 12500. | 0. | 0. | 0. | .59 | 65. | 22.5 | C | 19.2 | 14.0 | |
| * 2 | 3 | 99999. | 0. | 0. | 5929. | 0. | 0. | 5744. | 8660. | 0. | * 3022. | 185. | .66 | 60. | 32.1 | F | 19.1 | 14.1 |
| * 3 | 3 | 2830. | 0. | 0. | 5929. | 0. | 0. | 5744. | 7000. | 0. | ** 2830. | 185. | .82 | 18. | 105.8 | F | 17.6 | 17.1 |
| * 4 | 3 | 930. | 0. | 0. | 5929. | 0. | 0. | 5744. | 7000. | 0. | ** 930. | 185. | .82 | 18. | 105.8 | F | 17.6 | 17.1 |
| * 5 | 3 | 1490. | 0. | 0. | 5929. | 0. | 0. | 5744. | 7000. | 0. | ** 1490. | 185. | .82 | 18. | 105.8 | F | 17.6 | 17.1 |
| * 6 | 3 | 3020. | 0. | 0. | 5929. | 0. | 0. | 5744. | 7000. | 0. | ** 3020. | 185. | .82 | 18. | 105.8 | F | 17.6 | 17.1 |
| * 7 | 3 | 1030. | 0. | 0. | 5929. | 0. | 0. | 5744. | 7000. | 0. | ** 1030. | 185. | .82 | 18. | 105.8 | F | 17.6 | 17.1 |
| * 8 | 3 | 1440. | 0. | 0. | 5929. | 0. | 0. | 5744. | 7000. | 0. | ** 1440. | 185. | .82 | 18. | 105.8 | F | 17.6 | 17.1 |
| * 9 | 3 | 1430. | 0. | 0. | 5929. | 0. | 0. | 5744. | 7000. | 0. | ** 1430. | 185. | .82 | 18. | 105.8 | F | 17.6 | 17.1 |
| * 10 | 3 | 3480. | 0. | 0. | 5929. | 0. | 0. | 5744. | 7000. | 0. | ** 3480. | 185. | .82 | 18. | 105.8 | F | 17.6 | 17.1 |
| * 11 | 3 | 1020. | 0. | 0. | 5929. | 0. | 0. | 5744. | 7000. | 0. | ** 1020. | 185. | .82 | 18. | 105.8 | F | 17.6 | 17.1 |
| * 12 | 3 | 980. | 0. | 0. | 5929. | 0. | 0. | 5744. | 7000. | 0. | ** 980. | 185. | .82 | 18. | 105.8 | F | 17.6 | 17.1 |
| * 13 | 3 | 1800. | 0. | 0. | 5929. | 0. | 0. | 5744. | 7000. | 0. | ** 1800. | 185. | .82 | 18. | 105.8 | F | 17.6 | 17.1 |
| * 14 | 3 | 1500. | 0. | 705. | 5929. | 0. | 705. | 5744. | 6835. | 0. | ** 1500. | 185. | .84 | 19. | 99.0 | F | 18.2 | 16.4 |
| * 15 | 3 | 1300. | 0. | 0. | 5224. | 0. | 0. | 5039. | 6000. | 0. | ** 1300. | 185. | .84 | 19. | 87.1 | F | 18.2 | 16.5 |
| * 16 | 3 | 1000. | 648. | 0. | 5872. | 648. | 0. | 5687. | 5919. | 0. | ** 1000. | 185. | .96 | 30. | 63.6 | F | 21.5 | 12.8 |
| * 17 | 3 | 1100. | 0. | 0. | 5872. | 0. | 0. | 5687. | 6000. | 0. | ** 1100. | 185. | .95 | 28. | 66.9 | F | 21.1 | 13.2 |
| * 18 | 3 | 1000. | 0. | 605. | 5872. | 0. | 603. | 5687. | 5875. | 0. | ** 1000. | 185. | .97 | 31. | 61.8 | F | 21.7 | 12.6 |
| * 19 | 3 | 900. | 0. | 0. | 5267. | 0. | 0. | 5084. | 6000. | 0. | ** 900. | 185. | .85 | 20. | 85.6 | F | 18.4 | 16.2 |
| * 20 | 3 | 100. | 229. | 0. | 5496. | 229. | 0. | 5313. | 5968. | 0. | ** 100. | 185. | .89 | 23. | 77.2 | F | 19.4 | 14.9 |
| * 21 | 3 | 100. | 0. | 0. | 5496. | 0. | 0. | 5313. | 6000. | 0. | ** 100. | 185. | .89 | 23. | 78.5 | F | 19.3 | 15.1 |
| * 22 | 3 | 100. | 0. | 635. | 5496. | 0. | 633. | 5313. | 5875. | 0. | ** 100. | 185. | .90 | 24. | 73.4 | F | 19.8 | 14.5 |
| * 23 | 3 | 700. | 0. | 0. | 4861. | 0. | 0. | 4681. | 6000. | 0. | ** 700. | 185. | .78 | 16. | 98.2 | F | 16.6 | 18.3 |
| * 24 | 3 | 1500. | 0. | 927. | 4861. | 0. | 924. | 4681. | 5818. | 0. | ** 1500. | 185. | .80 | 17. | 90.8 | F | 17.2 | 17.6 |
| * 25 | 3 | 800. | 0. | 0. | 3934. | 0. | 0. | 3757. | 6000. | 0. | ** 800. | 185. | .63 | 10. | 127.0 | F | 13.0 | 23.0 |
| * 26 | 3 | 1000. | 1041. | 0. | 4975. | 1041. | 0. | 4798. | 5786. | 0. | ** 1000. | 185. | .83 | 19. | 85.9 | F | 17.8 | 16.8 |
| * 27 | 3 | 800. | 0. | 0. | 4975. | 0. | 0. | 4798. | 6000. | 0. | ** 800. | 185. | .80 | 17. | 94.6 | F | 17.1 | 17.8 |
| * 28 | 3 | 1000. | 0. | 539. | 4975. | 0. | 538. | 4798. | 5919. | 0. | ** 1000. | 185. | .81 | 18. | 91.3 | F | 17.3 | 17.4 |
| * 29 | 3 | 8000. | 0. | 0. | 4436. | 0. | 0. | 4260. | 6000. | 0. | ** 8000. | 185. | .71 | 13. | 111.3 | F | 14.7 | 20.6 |
| * 30 | 5 | 100. | 1040. | 0. | 5476. | 1040. | 0. | 5300. | 10000. | 0. | ** 100. | 185. | .53 | 7. | 144.9 | F | 10.1 | 26.0 |
| * 31 | 5 | 1000. | 700. | 0. | 6176. | 700. | 0. | 6000. | 6000. | 0. | 0. | 0. | 1.00 | 65. | 18.5 | E | 19.2 | 14.0 |
| * 32 | 5 | 2640. | 0. | 6176. | 6176. | 0. | 6000. | 6000. | 6000. | 0. | 0. | 0. | 1.00 | 65. | 18.5 | E | 20.0 | 13.7 |

| CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | | |
|----------------------------|---------|------------|---------|-------------------|---------|------------|---------|----------|
| FREWAY TRAVEL TIME = | 4283. | VEH-HRS | 4304. | PASS-HRS | 8276. | VEH-HRS | 8317. | PASS-HRS |
| FREWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 200. | VEH-HRS | 219. | PASS-HRS | 300. | VEH-HRS | 329. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 4483. | VEH-HRS | 4523. | PASS-HRS | 8576. | VEH-HRS | 8646. | PASS-HRS |
| TOTAL TRAV DISTANCE = | 157212. | VEH-MI. | 158230. | PASS-MI. | 333122. | VEH-MI. | 335172. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 35. | MPH. | | | 40. | MPH. | | |
| AVERAGE DENSITY = | 51. | VPMP | | | 44. | VPMP | | |
| TOTAL FUEL = | 8526. | GALLONS | | | 17565. | GALLONS | | |
| TOTAL EMISSIONS = | 2376. | KI LOGRAMS | | | 4832. | KI LOGRAMS | | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| US-101_NB_AM_NP_2018_PE.txt | | | | | | | | | |
|-----------------------------|--------|------------|--------|------------|--------|------------|--------|------------|--------|
| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
| 1 | 0.00 | 2 | 157.44 | 3 | 122.69 | 4 | 40.32 | 5 | 64.59 |
| 6 | 130.92 | 7 | 44.65 | 8 | 62.43 | 9 | 61.99 | 10 | 150.86 |
| 11 | 44.22 | 12 | 42.48 | 13 | 78.03 | 14 | 59.31 | 15 | 45.21 |
| 16 | 19.56 | 17 | 23.57 | 18 | 18.54 | 19 | 30.46 | 20 | 2.84 |
| 21 | 2.91 | 22 | 2.62 | 23 | 29.51 | 24 | 56.93 | 25 | 48.95 |
| 26 | 34.81 | 27 | 31.80 | 28 | 37.88 | 29 | 406.60 | 30 | 12.18 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 1864.3 VEH-HRS ***** AVERAGE DELAY = 21.78 MIN/VEH *****

***** RAMP DELAYS *****

| | | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|---------|---|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|
| ON-RAMP | 2 | RAMP | 100. | 8.02 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 8.02 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP | 6 | RAMP | 100. | 9.00 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 9.00 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |

```

FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP LLL
FFFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 1111111 222222222 PPP LLLLLLLLLL
    
```

FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 2 AND 29 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 35
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65 MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

FREeway AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC | SSEC | DESIGN | ORG | TRK | SSEC | PCT | PCT | DES | SPECIAL | FF.SPD. | CAP. | ART | GRADE | SUBSECTION | LOCATION |
|---------|------|-------|--------|-----|-----|------|-----|--------|------|---------|----------|----------|------|----------|--------------------------|----------|
| SEC | LNS | CAP | SPEED | DES | FAC | GRAD | TRK | TRUCKS | RAMP | RAMP | ALT. RTE | ALT. RTE | TYPE | ALT. RTE | | |
| 1 | | | | | | | | | | | | | | | | |
| 2 | 1 | 1650. | 99999. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | |
| 3 | 1 | 1650. | 2830. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-87 to DLC loop-on | |
| 4 | 1 | 1650. | 930. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | DLC loop on to dia-on | |
| 5 | 1 | 1650. | 1490. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | DLC dia-on to Tomas off | |
| 6 | 1 | 1650. | 3020. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas off to on | |
| 7 | 1 | 1650. | 1030. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas on to bowers off | |
| 8 | 1 | 1650. | 1440. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers off to loop-on | |
| 9 | 1 | 1650. | 1430. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers loop-on to dia | |
| 10 | 1 | 1650. | 3480. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers dia-on to law-off | |
| 11 | 1 | 1650. | 1020. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Law off to loop-on | |
| 12 | 1 | 1650. | 980. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Lawr Loop to diag | |
| 13 | 1 | 1650. | 1800. | 65 | | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Lawrence On-ramp | |
| 14 | 1 | 1650. | 1500. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks Off-Ramp | |
| 15 | 1 | 1650. | 1300. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Fair Oaks | |
| 16 | 1 | 1650. | 1000. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Fair Oaks On-Ramp | |
| 17 | 1 | 1650. | 1100. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Mathilda | |
| 18 | 1 | 1650. | 1000. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda NB Off-Ramp | |
| 19 | 1 | 1650. | 900. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | |


```

**
** 20 1 1650. 100. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Mathilda NB On-Ramp **
**
*****

```

FREEWAY AND ARTERIAL DESIGN FEATURES

```

*****
**
** SUB NO. SSEC SSEC DESIGN ORG TRK SSEC PCT PCT DES SPECIAL FF. SPD. CAP. ART GRADE SUBSECTION LOCATION **
** SEC LNS CAP LENGTH SPEED DES FAC GRAD TRK TRUCKS RAMP ALT. RTE ALT. RTE TYPE ALT. RTE **
*****
** 21 1 1650. 100. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Mathilda / Mathilda **
** 22 1 1650. 100. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Mathilda SB Off-ramp **
** 23 1 1650. 700. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Mathilda / SR-237 **
** 24 1 1650. 1500. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 SR-237 WB Off-Ramp **
** 25 1 1650. 800. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 SR-237 / SR-237 **
** 26 1 1650. 1000. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 SR-237 WB On-Ramp **
** 27 1 1650. 800. 65 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 SR-237 / Ellis **
** 28 1 1650. 1000. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Ellis Off-ramp **
** 29 1 1650. 8000. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 HOV Dummy **
** 30 **
** 31 **
** 32 **
*****

```

FREEWAY TRAVEL TIME (MINUTES)

```

*****
* ORIGINS DESTINATIONS ACROSS *
* DOWN *
+ * 1 2 3 4 5 6 7 8 *
+ * * *
+ * 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+ * 2 * 0.00 25.33 26.17 26.38 26.77 27.40 28.80 0.00 *
+ * 3 * 0.00 0.00 0.00 0.00 0.00 0.00 3.24 0.00 *
+ * 4 * 0.00 0.00 0.00 0.00 0.00 0.00 2.47 0.00 *
+ * 5 * 0.00 0.00 0.00 0.00 0.00 0.00 1.89 0.00 *
+ * 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+ * 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+ * * *
*****

```

TIME SLICE FREEWAY PERFORMANCE TABLE

```

*****
* SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMI SS *
* SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMP L LEVEL MPG GS/VM *
*****
Page 2

```


* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
* *

TIME SLICE FREEWAY PERFORMANCE TABLE

Table with 17 columns: SUB NO., SEC LNS, SSEC LENGTH, O-D DATA ORG DES, DEMANDS SSEC, ADJUSTED VOLUMES ORG DES, SSEC, WEAVE CAP, EFF, CONGEST LENGTH, STORAGE RATE, V/C RATIO, SPEED MPH, DENSITY VPMP, LOS LEVEL, FUEL MPG, EMISSIONS GS/VM. Includes a summary row for TOTAL 140349 = 26.6 MILES.

Summary statistics table comparing CURRENT TIME SLICE and CUMULATIVE VALUES for metrics like FREeway TRAVEL TIME, ON-RAMP DELAY, TOTAL SYSTEM TRAVEL TIME, etc.

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

Table showing DELAY by SUBSECTION (1-32) with columns for SUBSECTION and DELAY values.

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

```

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A.D.MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP EEE
FFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP EEEEEEEEE
    
```

FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 35
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65 MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

```

*****
**
** FREEWAY AND ARTERIAL DESIGN FEATURES
**
*****
**
** SUB NO. SSEC SSEC DESIGN ORG TRK SSEC PCT PCT DES SPECIAL FF.SPD. CAP. ART GRADE SUBSECTION LOCATION
** SEC LNS CAP LENGTH SPEED DES FAC GRAD TRK TRUCKS RAMP ALT. RTE ALT. RTE TYPE ALT. RTE
**
** 1 5 12500. 500. 65 OD 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 Seeding
**
** 2 3 8660. 99999. 65 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 Queue Capture
**
** 3 3 7000. 2830. 65 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 SR-87 to DLC loop-on
**
** 4 3 7000. 930. 65 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 DLC loop on to dia-on
**
** 5 3 7000. 1490. 65 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 DLC dia-on to Tomas off
**
** 6 3 7000. 3020. 65 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 Tomas off to on
**
** 7 3 7000. 1030. 65 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 Tomas on to bowers off
**
** 8 3 7000. 1440. 65 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 Bowers off to loop-on
**
** 9 3 7000. 1430. 65 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 Bowers loop-on to dia
**
** 10 3 7000. 3480. 65 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 Bowers dia-on to law-off
**
** 11 3 7000. 1020. 65 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 Law off to loop-on
**
** 12 3 7000. 980. 65 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 Lawr Loop to diag
**
** 13 3 7000. 1800. 65 0.96 0.0 4 0 YES 0.0 0. GOOD 0.0 Lawrence On-ramp
**
** 14 3 7000. 1500. 65 D 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 Fair Oaks Off-Ramp
**
** 15 3 6000. 1300. 65 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 Fair Oaks / Fair Oaks
**
** 16 3 6000. 1000. 65 0 0.96 0.0 4 0 YES 0.0 0. GOOD 0.0 Fair Oaks On-Ramp
**
** 17 3 6000. 1100. 65 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 Fair Oaks / Mathilda
**
** 18 4 7490. 1000. 65 D 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 Mathilda NB Off-Ramp
**
** 19 3 6000. 900. 65 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 Mathilda / Mathilda
**
** 20 3 6000. 100. 65 0 0.96 0.0 4 0 YES 0.0 0. GOOD 0.0 Mathilda NB On-Ramp
**
*****
    
```

```

*****
**
**
**          FREeway AND ARTERIAL DESIGN FEATURES          **
**
*****
** SUB NO.  SSEC  SSEC  DESIGN  ORG  TRK  SSEC  PCT  PCT  DES  SPECIAL  FF.SPD.  CAP.  ART  GRADE  SUBSECTION LOCATION
** SEC  LNS   CAP   LENGTH  SPEED  DES  FAC  GRAD  TRK  TRUCKS  RAMP   ALT. RTE  ALT. RTE  TYPE  ALT. RTE
**
** 21  3  6000.  100.  65      0.96  0.0  4   0   NO    0.0    0.  GOOD  0.0  Mathilda / Mathilda
** 22  3  6000.  100.  65      0.96  0.0  4   0   NO    0.0    0.  GOOD  0.0  Mathilda SB Off-ramp
** 23  3  6000.  700.  65      0.96  0.0  4   0   NO    0.0    0.  GOOD  0.0  Mathilda / SR-237
** 24  3  6000.  1500.  65    D  0.96  0.0  4   0   NO    0.0    0.  GOOD  0.0  SR-237 WB Off-Ramp
** 25  3  6000.  800.  65      0.96  0.0  4   0   NO    0.0    0.  GOOD  0.0  SR-237 / SR-237
** 26  3  6000.  1000.  65    0  0.96  0.0  4   0   YES   0.0    0.  GOOD  0.0  SR-237 WB On-Ramp
** 27  3  6000.  800.  65      0.96  0.0  4   0   YES   0.0    0.  GOOD  0.0  SR-237 / Ellis
** 28  3  6000.  1000.  65    D  0.96  0.0  4   0   NO    0.0    0.  GOOD  0.0  Ellis Off-ramp
** 29  3  6000.  8000.  65      0.96  0.0  4   0   NO    0.0    0.  GOOD  0.0  HOV Dummy
** 30  5  10000.  100.  65    0  0.96  0.0  4   0   NO    0.0    0.  GOOD  0.0  HOV Dummy
** 31  5  6000.  1000.  65    0  0.96  0.0  4   0   YES   0.0    0.  GOOD  0.0  Dummy Bottleneck
** 32  5  6000.  2640.  65    D  1.00  0.0  0   0   NO    0.0    0.  GOOD  0.0  End of Network
**
*****

```

***** INPUT HAS BEEN COMPLETED *****

QUEUE COLLISION IN SECTION 16 T2 =0.629
 QUEUE COLLISION IN SECTION 15 T2 =0.475
 QUEUE COLLISION IN SECTION 14 T2 =0.498

```

*****
**
**          FREeway TRAVEL TIME (MINUTES)          **
**
*****

```

```

*****
* ORIGINS DESTINATIONS ACROSS
* DOWN
* 1 2 3 4 5 6
*
* 1 * 0.09 26.40 28.66 30.87 33.42 42.05
*
* 2 * 0.00 0.00 1.47 3.68 6.23 14.86
*
* 3 * 0.00 0.00 0.00 1.62 4.17 12.80
*
* 4 * 0.00 0.00 0.00 0.00 1.76 10.38
*
* 5 * 0.00 0.00 0.00 0.00 0.00 0.80
*
* 6 * 0.00 0.00 0.00 0.00 0.00 0.64
*
*****

```

US-101_NB_AM_P1_2018_PE.txt
 TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB SEC | * NO. LNS | * SSEC LENGTH | * O-D DATA ORG | * DEMANDS DES | * SSEC | * ADJUSTED ORG | * VOLUMES DES | * SSEC SSEC | * SSEC CAP. | * WEAVE EFF | * CONGEST LENGTH | * STORAGE RATE | * V/C RATIO | * SPEED MPH | * DENSITY VPMP | * LOS LEVEL | * FUEL MPG | * EMISSIONS GS/VM |
|-----------|-----------|---------------|----------------|---------------|--------|----------------|-----------------|-------------|-------------|----------------|------------------|----------------|-------------|-------------|----------------|-------------|------------|-------------------|
| * 1 | 5 | 500. | 8470. | 1609. | 8470. | 8470. | 1609. | 8470. | 12500. | 0. | 0. | 0. | .68 | 65. | 26.1 | D | 19.2 | 14.0 |
| * 2 | 3 | 99999. | 0. | 0. | 6861. | 0. | 0. | 4536. | 8660. | 0. | ** 729. | 2325. | .52 | 63. | 23.9 | F | 19.9 | 13.4 |
| * 3 | 3 | 2830. | 0. | 0. | 6861. | 0. | 0. | 4536. | 7000. | 0. | ** 2830. | 2325. | .65 | 46. | 33.2 | F | 22.7 | 11.8 |
| * 4 | 3 | 930. | 0. | 0. | 6861. | 0. | 0. | 4536. | 7000. | 0. | ** 930. | 2325. | .65 | 41. | 37.0 | F | 22.1 | 12.1 |
| * 5 | 3 | 1490. | 0. | 0. | 6861. | 0. | 0. | 4536. | 7000. | 0. | ** 1490. | 2325. | .65 | 38. | 39.5 | F | 21.8 | 12.4 |
| * 6 | 3 | 3020. | 0. | 0. | 6861. | 0. | 0. | 4536. | 7000. | 0. | ** 3020. | 2325. | .65 | 34. | 44.2 | F | 21.2 | 12.8 |
| * 7 | 3 | 1030. | 0. | 0. | 6861. | 0. | 0. | 4536. | 7000. | 0. | ** 1030. | 2325. | .65 | 31. | 48.7 | F | 20.7 | 13.3 |
| * 8 | 3 | 1440. | 0. | 0. | 6861. | 0. | 0. | 4536. | 7000. | 0. | ** 1440. | 2325. | .65 | 29. | 51.5 | F | 20.3 | 13.5 |
| * 9 | 3 | 1430. | 0. | 0. | 6861. | 0. | 0. | 4536. | 7000. | 0. | ** 1430. | 2325. | .65 | 28. | 54.8 | F | 20.0 | 13.8 |
| * 10 | 3 | 3480. | 0. | 0. | 6861. | 0. | 0. | 4536. | 7000. | 0. | ** 3480. | 2325. | .65 | 25. | 60.7 | F | 19.3 | 14.4 |
| * 11 | 3 | 1020. | 0. | 0. | 6861. | 0. | 0. | 4536. | 7000. | 0. | ** 1020. | 2325. | .65 | 23. | 66.4 | F | 18.8 | 15.0 |
| * 12 | 3 | 980. | 0. | 0. | 6861. | 0. | 0. | 4536. | 7000. | 0. | ** 980. | 2325. | .65 | 22. | 69.0 | F | 18.5 | 15.2 |
| * 13 | 3 | 1800. | 0. | 0. | 6861. | 0. | 0. | 4536. | 7000. | 0. | ** 1800. | 2325. | .65 | 21. | 72.7 | F | 18.2 | 15.6 |
| * 14 | 3 | 1500. | 0. | 770. | 6861. | 0. | 765. | 4536. | 6820. | 0. | ** 1500. | 2284. | .67 | 21. | 73.7 | F | 18.2 | 15.6 |
| * 15 | 3 | 1300. | 0. | 0. | 6091. | 0. | 0. | 3771. | 6000. | 0. | ** 1300. | 2229. | .63 | 19. | 67.5 | F | 17.6 | 16.1 |
| * 16 | 3 | 1000. | 652. | 0. | 6743. | 552. | 0. | 4323. | 5903. | 0. | ** 1000. | 1580. | .73 | 28. | 51.9 | F | 20.3 | 13.9 |
| * 17 | 3 | 1100. | 0. | 0. | 6743. | 0. | 0. | 4323. | 6000. | 0. | ** 1100. | 1580. | .72 | 26. | 54.7 | F | 19.7 | 14.3 |
| * 18 | 4 | 1000. | 0. | 1051. | 6743. | 0. | 920. | 4323. | 7271. | 0. | ** 1000. | 1580. | .59 | 19. | 55.8 | F | 15.9 | 17.3 |
| * 19 | 3 | 900. | 0. | 0. | 5692. | 0. | 0. | 3403. | 6000. | 0. | ** 900. | 1580. | .57 | 17. | 65.6 | F | 15.2 | 17.7 |
| * 20 | 3 | 100. | 288. | 0. | 5980. | 240. | 0. | 3643. | 5948. | 0. | ** 100. | 1580. | .61 | 19. | 65.6 | F | 16.4 | 17.0 |
| * 21 | 3 | 100. | 0. | 0. | 5980. | 0. | 0. | 3643. | 6000. | 0. | ** 100. | 1580. | .61 | 18. | 66.8 | F | 16.2 | 17.2 |
| * 22 | 3 | 100. | 0. | 0. | 5980. | 0. | 0. | 3643. | 6000. | 0. | ** 100. | 1580. | .61 | 18. | 67.2 | F | 16.2 | 17.3 |
| * 23 | 3 | 700. | 0. | 0. | 5980. | 0. | 0. | 3643. | 6000. | 0. | ** 700. | 1580. | .61 | 18. | 68.7 | F | 16.0 | 17.4 |
| * 24 | 3 | 1500. | 0. | 834. | 5980. | 0. | 728. | 3643. | 5835. | 0. | ** 1500. | 1580. | .62 | 17. | 70.0 | F | 16.4 | 17.4 |
| * 25 | 3 | 800. | 0. | 0. | 5146. | 0. | 0. | 2915. | 6000. | 0. | ** 800. | 1580. | .49 | 11. | 85.1 | F | 12.6 | 20.5 |
| * 26 | 3 | 1000. | 1214. | 0. | 6360. | 1214. | 0. | 4129. | 5739. | 0. | ** 1000. | 1580. | .72 | 19. | 70.7 | F | 17.8 | 16.4 |
| * 27 | 3 | 800. | 0. | 0. | 6360. | 0. | 0. | 4129. | 6000. | 0. | ** 800. | 1580. | .69 | 18. | 78.4 | F | 16.8 | 17.3 |
| * 28 | 3 | 1000. | 0. | 459. | 6360. | 0. | 413. | 4129. | 5929. | 0. | ** 1000. | 1580. | .70 | 17. | 79.3 | F | 16.8 | 17.4 |
| * 29 | 3 | 8000. | 0. | 0. | 5901. | 0. | 0. | 3716. | 6000. | 0. | ** 8000. | 1580. | .62 | 12. | 106.6 | F | 13.8 | 21.0 |
| * 30 | 5 | 100. | 1384. | 0. | 7285. | 1384. | 0. | 5100. | 10000. | 0. | ** 100. | 1580. | .51 | 7. | 148.0 | F | 9.8 | 26.4 |
| * 31 | 5 | 1000. | 1000. | 0. | 8285. | 900. | 0. | 6000. | 6000. | 0. | 0. | 0. | 1.00 | 65. | 18.5 | E | 19.2 | 14.0 |
| * 32 | 5 | 2640. | 0. | 8285. | 8285. | 0. | 6000. | 6000. | 6000. | 0. | 0. | 0. | 1.00 | 65. | 18.5 | E | 20.0 | 13.7 |
| * TOTAL | | | 144589. | = | 27.4 | MILES | MAX(V/C) = 1.00 | | | LOWEST LOS = F | AVG = 43. | 36.1 | 19.5 | 13.9 | | | | |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 2/29/2016 15:58 PAGE 7
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 1 OF 2

| CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | | |
|----------------------------|---------|------------|---------|-------------------|---------|------------|---------|------------|
| FREWAY TRAVEL TIME = | 4042. | VEH-HRS | 4063. | PASS-HRS | 4042. | VEH-HRS | 4063. | PASS-HRS |
| FREWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 124. | VEH-HRS | 134. | PASS-HRS | 124. | VEH-HRS | 134. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 4166. | VEH-HRS | 4196. | PASS-HRS | 4166. | VEH-HRS | 4196. | PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 175558. | VEH-MI. | 176592. | PASS-MI. | 175558. | VEH-MI. | 176592. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 42. | MPH. | 43. | MPH. | 42. | MPH. | 43. | MPH. |
| AVERAGE DENSITY = | 36. | VPMP | 36. | VPMP | 36. | VPMP | 36. | VPMP |
| TOTAL FUEL = | 9065. | GALLONS | 9065. | GALLONS | 9065. | GALLONS | 9065. | GALLONS |
| TOTAL EMISSIONS = | 2462. | KI LOGRAMS | 2462. | KI LOGRAMS | 2462. | KI LOGRAMS | 2462. | KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|--------|------------|-------|
| 1 | 0.02 | 2 | 54.04 | 3 | 23.66 | 4 | 10.54 | 5 | 19.74 |
| 6 | 50.77 | 7 | 20.61 | 8 | 31.63 | 9 | 34.65 | 10 | 97.83 |
| 11 | 32.30 | 12 | 32.59 | 13 | 63.81 | 14 | 53.41 | 15 | 45.29 |
| 16 | 20.73 | 17 | 24.72 | 18 | 35.65 | 19 | 30.44 | 20 | 3.23 |
| 21 | 3.31 | 22 | 3.33 | 23 | 23.96 | 24 | 51.90 | 25 | 38.57 |
| 26 | 31.98 | 27 | 29.32 | 28 | 36.91 | 29 | 423.41 | 30 | 12.54 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 1340.9 VEH-HRS ***** AVERAGE DELAY = 19.95 MIN/VEH *****

***** RAMP DELAYS *****

| ON-RAMP | NO. | TYPE | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|---------|-----|--------|-----------------------|---------------|--------------------------------|----------|---------|---------|----------|----------------------|
| ON-RAMP | 2 | RAMP | 100. | 50.00 | 4.60 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 50.00 | 4.60 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| ON-RAMP | 3 | RAMP | 48. | 24.00 | 5.00 | 8.57 | 0.53 | 2.78 | 0.15 | 3.46 |
| | | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 48. | 24.00 | 5.00 | 8.57 | 0.53 | 2.78 | 0.15 | 3.46 |
| ON-RAMP | 6 | RAMP | 100. | 50.00 | 3.70 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 50.00 | 3.70 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 2/29/2016 15:58 PAGE 8
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 2

 ** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS | | DESTINATIONS ACROSS | | | | | |
|-----------|------|---------------------|-------|-------|-------|-------|---|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 |
| * 1 * | 0.09 | 33.22 | 35.62 | 38.12 | 40.89 | 48.89 | |
| * 2 * | 0.00 | 0.00 | 1.60 | 4.10 | 6.87 | 14.87 | |
| * 3 * | 0.00 | 0.00 | 0.00 | 1.75 | 4.51 | 12.52 | |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 1.82 | 9.82 | |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.79 | |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.64 | |

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB | * NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | |
|-------|-------|----------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|----------|---------|-----------|---------|--------|-------------|------|------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | |
| * 1 | 5 | 500. | 7321. | 1391. | 7321. | 7321. | 1391. | 7321. | 12500. | 0. | 0. | .59 | 65. | 22.5 | C | 19.2 | 14.0 | |
| * 2 | 3 | 99999. | 0. | 0. | 5930. | 0. | 0. | 5660. | 8660. | 0. | ** 3997. | .70. | .65 | 58. | 32.4 | F | 19.1 | 14.1 |
| * 3 | 3 | 2830. | 0. | 0. | 5930. | 0. | 0. | 5660. | 7000. | 0. | ** 2830. | .270. | .81 | 17. | 108.4 | F | 17.3 | 17.5 |
| * 4 | 3 | 930. | 0. | 0. | 5930. | 0. | 0. | 5660. | 7000. | 0. | ** 930. | .270. | .81 | 17. | 108.4 | F | 17.3 | 17.5 |
| * 5 | 3 | 1490. | 0. | 0. | 5930. | 0. | 0. | 5660. | 7000. | 0. | ** 1490. | .270. | .81 | 17. | 108.4 | F | 17.3 | 17.5 |
| * 6 | 3 | 3020. | 0. | 0. | 5930. | 0. | 0. | 5660. | 7000. | 0. | ** 3020. | .270. | .81 | 17. | 108.4 | F | 17.3 | 17.5 |
| * 7 | 3 | 1030. | 0. | 0. | 5930. | 0. | 0. | 5660. | 7000. | 0. | ** 1030. | .270. | .81 | 17. | 108.4 | F | 17.3 | 17.5 |
| * 8 | 3 | 1440. | 0. | 0. | 5930. | 0. | 0. | 5660. | 7000. | 0. | ** 1440. | .270. | .81 | 17. | 108.4 | F | 17.3 | 17.5 |
| * 9 | 3 | 1430. | 0. | 0. | 5930. | 0. | 0. | 5660. | 7000. | 0. | ** 1430. | .270. | .81 | 17. | 108.4 | F | 17.3 | 17.5 |
| * 10 | 3 | 3480. | 0. | 0. | 5930. | 0. | 0. | 5660. | 7000. | 0. | ** 3480. | .270. | .81 | 17. | 108.4 | F | 17.3 | 17.5 |
| * 11 | 3 | 1020. | 0. | 0. | 5930. | 0. | 0. | 5660. | 7000. | 0. | ** 1020. | .270. | .81 | 17. | 108.4 | F | 17.3 | 17.5 |
| * 12 | 3 | 980. | 0. | 0. | 5930. | 0. | 0. | 5660. | 7000. | 0. | ** 980. | .270. | .81 | 17. | 108.4 | F | 17.3 | 17.5 |
| * 13 | 3 | 1800. | 0. | 0. | 5930. | 0. | 0. | 5660. | 7000. | 0. | ** 1800. | .270. | .81 | 17. | 108.4 | F | 17.3 | 17.5 |
| * 14 | 3 | 1500. | 0. | 705. | 5930. | 0. | 705. | 5660. | 6835. | 0. | ** 1500. | .270. | .83 | 19. | 101.7 | F | 17.8 | 16.9 |
| * 15 | 3 | 1300. | 0. | 0. | 5225. | 0. | 0. | 4955. | 6000. | 0. | ** 1300. | .270. | .83 | 18. | 89.7 | F | 17.8 | 16.9 |
| * 16 | 3 | 1000. | 648. | 0. | 5873. | 648. | 0. | 5603. | 5919. | 0. | ** 1000. | .270. | .95 | 28. | 66.2 | F | 21.0 | 13.2 |
| * 17 | 3 | 1100. | 0. | 0. | 5873. | 0. | 0. | 5603. | 6000. | 0. | ** 1100. | .270. | .93 | 27. | 69.5 | F | 20.6 | 13.6 |
| * 18 | 4 | 1000. | 0. | 1236. | 5873. | 0. | 1231. | 5603. | 7236. | 0. | ** 1000. | .270. | .77 | 16. | 89.8 | F | 16.5 | 18.5 |
| * 19 | 3 | 900. | 0. | 0. | 4637. | 0. | 0. | 4372. | 6000. | 0. | ** 900. | .270. | .73 | 14. | 107.8 | F | 15.2 | 20.0 |
| * 20 | 3 | 100. | 314. | 0. | 4951. | 262. | 0. | 4634. | 5949. | 0. | ** 100. | .270. | .78 | 16. | 97.6 | F | 16.6 | 18.4 |
| * 21 | 3 | 100. | 0. | 0. | 4951. | 0. | 0. | 4634. | 6000. | 0. | ** 100. | .270. | .77 | 16. | 99.7 | F | 16.5 | 18.6 |
| * 22 | 3 | 100. | 0. | 0. | 4951. | 0. | 0. | 4634. | 6000. | 0. | ** 100. | .270. | .77 | 16. | 99.7 | F | 16.5 | 18.6 |
| * 23 | 3 | 700. | 0. | 0. | 4951. | 0. | 0. | 4634. | 6000. | 0. | ** 700. | .270. | .77 | 16. | 99.7 | F | 16.5 | 18.6 |
| * 24 | 3 | 1500. | 0. | 932. | 4951. | 0. | 916. | 4634. | 5822. | 0. | ** 1500. | .270. | .80 | 17. | 92.4 | F | 17.0 | 17.9 |
| * 25 | 3 | 800. | 0. | 0. | 4019. | 0. | 0. | 3718. | 6000. | 0. | ** 800. | .270. | .62 | 10. | 128.2 | F | 12.7 | 23.2 |
| * 26 | 3 | 1000. | 1053. | 0. | 5072. | 1053. | 0. | 4771. | 5783. | 0. | ** 1000. | .270. | .82 | 18. | 86.6 | F | 17.7 | 17.0 |
| * 27 | 3 | 800. | 0. | 0. | 5072. | 0. | 0. | 4771. | 6000. | 0. | ** 800. | .270. | .80 | 17. | 95.4 | F | 17.0 | 17.9 |
| * 28 | 3 | 1000. | 0. | 541. | 5072. | 0. | 534. | 4771. | 5921. | 0. | ** 1000. | .270. | .81 | 17. | 92.2 | F | 17.2 | 17.6 |
| * 29 | 3 | 8000. | 0. | 0. | 4531. | 0. | 0. | 4237. | 6000. | 0. | ** 8000. | .270. | .71 | 13. | 112.0 | F | 14.6 | 20.7 |
| * 30 | 5 | 100. | 1063. | 0. | 5594. | 1063. | 0. | 5300. | 10000. | 0. | ** 100. | .270. | .53 | 7. | 144.9 | F | 10.1 | 26.0 |
| * 31 | 5 | 1000. | 700. | 0. | 6294. | 700. | 0. | 6000. | 6000. | 0. | 0. | 0. | 1.00 | 65. | 18.5 | E | 19.2 | 14.0 |
| * 32 | 5 | 2640. | 0. | 6294. | 6294. | 0. | 6000. | 6000. | 6000. | 0. | 0. | 0. | 1.00 | 65. | 18.5 | E | 20.0 | 13.7 |

* TOTAL 144589. = 27.4 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 35. 52.1 18.4 15.1 *

| | CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | |
|----------------------------|--------------------|------------|---------|----------|-------------------|------------|---------|----------|
| FREWAY TRAVEL TIME = | 4417. | VEH-HRS | 4438. | PASS-HRS | 8459. | VEH-HRS | 8501. | PASS-HRS |
| FREWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 274. | VEH-HRS | 293. | PASS-HRS | 398. | VEH-HRS | 427. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 4691. | VEH-HRS | 4731. | PASS-HRS | 8857. | VEH-HRS | 8928. | PASS-HRS |
| TOTAL TRAV DISTANCE = | 156539. | VEH-MI. | 157558. | PASS-MI. | 332097. | VEH-MI. | 334150. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 33. | MPH. | | | 39. | MPH. | | |
| AVERAGE DENSITY = | 52. | VPMP | | | 44. | VPMP | | |
| TOTAL FUEL = | 8587. | GALLONS | | | 17652. | GALLONS | | |
| TOTAL EMISSIONS = | 2402. | KI LOGRAMS | | | 4864. | KI LOGRAMS | | |

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***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|--------|------------|--------|------------|--------|------------|--------|------------|--------|
| 1 | 0.00 | 2 | 200.79 | 3 | 127.58 | 4 | 41.92 | 5 | 67.17 |
| 6 | 136.14 | 7 | 46.43 | 8 | 64.92 | 9 | 64.46 | 10 | 156.88 |
| 11 | 45.98 | 12 | 44.18 | 13 | 81.14 | 14 | 61.90 | 15 | 47.46 |
| 16 | 21.29 | 17 | 25.48 | 18 | 51.70 | 19 | 43.67 | 20 | 4.19 |
| 21 | 4.31 | 22 | 4.31 | 23 | 30.18 | 24 | 58.51 | 25 | 49.59 |
| 26 | 35.29 | 27 | 32.24 | 28 | 38.48 | 29 | 410.39 | 30 | 12.18 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 2008.8 VEH-HRS ***** AVERAGE DELAY = 23.71 MIN/VEH *****

***** RAMP DELAYS *****

| | | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS | |
|---------|---|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|-------|
| ON-RAMP | 2 | RAMP | 100. | 100.00 | 8.02 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 100.00 | 8.02 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP | 3 | RAMP | 100. | 74.00 | 12.27 | 26.42 | 1.64 | 8.57 | 0.45 | 10.67 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 74.00 | 12.27 | 26.42 | 1.64 | 8.57 | 0.45 | 10.67 |
| ON-RAMP | 6 | RAMP | 100. | 100.00 | 9.00 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 100.00 | 9.00 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |


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FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP LLL
FFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 1111111 222222222 PPP LLLLLLLLLL
    
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FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 2 AND 29 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 35
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65 MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

FREeway AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC | SSEC | DESIGN | ORG | TRK | SSEC | PCT | PCT | DES | SPECIAL | FF.SPD. | CAP. | ART | GRADE | SUBSECTION | LOCATION |
|---------|------|-------|--------|-----|-----|------|-----|--------|------|---------|----------|----------|------|----------|--------------------------|----------|
| SEC | LNS | CAP | SPEED | DES | FAC | GRAD | TRK | TRUCKS | RAMP | RAMP | ALT. RTE | ALT. RTE | TYPE | ALT. RTE | | |
| 1 | | | | | | | | | | | | | | | | |
| 2 | 1 | 1650. | 99999. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | |
| 3 | 1 | 1650. | 2830. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-87 to DLC loop-on | |
| 4 | 1 | 1650. | 930. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | DLC loop on to dia-on | |
| 5 | 1 | 1650. | 1490. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | DLC dia-on to Tomas off | |
| 6 | 1 | 1650. | 3020. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas off to on | |
| 7 | 1 | 1650. | 1030. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas on to bowers off | |
| 8 | 1 | 1650. | 1440. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers off to loop-on | |
| 9 | 1 | 1650. | 1430. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers loop-on to dia | |
| 10 | 1 | 1650. | 3480. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers dia-on to law-off | |
| 11 | 1 | 1650. | 1020. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Law off to loop-on | |
| 12 | 1 | 1650. | 980. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Lawr Loop to diag | |
| 13 | 1 | 1650. | 1800. | 65 | | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Lawrence On-ramp | |
| 14 | 1 | 1650. | 1500. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks Off-Ramp | |
| 15 | 1 | 1650. | 1300. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Fair Oaks | |
| 16 | 1 | 1650. | 1000. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Fair Oaks On-Ramp | |
| 17 | 1 | 1650. | 1100. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Mathilda | |
| 18 | 1 | 1650. | 1000. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda NB Off-Ramp | |
| 19 | 1 | 1650. | 900. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | |

**
 ** 20 1 1650. 100. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Mathilda NB On-Ramp **
 **

 **
 ** FREEWAY AND ARTERIAL DESIGN FEATURES **
 **

| SUB NO. | SEC | LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT TRUCKS | DES RAMP | SPECIAL | FF. SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION | LOCATI ON | |
|---------|------|----------|----------|-------------|--------------|---------|---------|-----------|---------|------------|----------|---------|-------------------|-------------------------|-----------------------|----------------|------------|-----------|----|
| ** 21 | ** 1 | ** 1650. | ** 100. | ** 65 | ** 0.96 | ** 0.0 | ** 0 | ** 100 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Mathilda / Mathilda | ** | ** | ** | ** | |
| ** 22 | ** 1 | ** 1650. | ** 100. | ** 65 | ** 0.96 | ** 0.0 | ** 0 | ** 100 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Mathilda SB Off-ramp | ** | ** | ** | ** | |
| ** 23 | ** 1 | ** 1650. | ** 700. | ** 65 | ** 0.96 | ** 0.0 | ** 0 | ** 100 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Mathilda / SR-237 | ** | ** | ** | ** | |
| ** 24 | ** 1 | ** 1650. | ** 1500. | ** 65 | ** D | ** 0.96 | ** 0.0 | ** 0 | ** 100 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** SR-237 WB Off-Ramp | ** | ** | ** | |
| ** 25 | ** 1 | ** 1650. | ** 800. | ** 65 | ** 0.96 | ** 0.0 | ** 0 | ** 100 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** SR-237 / SR-237 | ** | ** | ** | ** | |
| ** 26 | ** 1 | ** 1650. | ** 1000. | ** 65 | ** 0 | ** 0.96 | ** 0.0 | ** 0 | ** 100 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** SR-237 WB On-Ramp | ** | ** | ** | |
| ** 27 | ** 1 | ** 1650. | ** 800. | ** 65 | ** 0.96 | ** 0.0 | ** 0 | ** 100 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** SR-237 / Ellis | ** | ** | ** | ** | |
| ** 28 | ** 1 | ** 1650. | ** 1000. | ** 65 | ** D | ** 0.96 | ** 0.0 | ** 0 | ** 100 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Ellis Off-ramp | ** | ** | ** | ** |
| ** 29 | ** 1 | ** 1650. | ** 8000. | ** 65 | ** D | ** 0.96 | ** 0.0 | ** 0 | ** 100 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** HOV Dummy | ** | ** | ** | ** |
| ** 30 | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** |
| ** 31 | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** |
| ** 32 | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** |

 **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 **

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | |
|--------------|---------------------|-------|-------|-------|-------|-------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 25.33 | 26.17 | 26.77 | 27.43 | 28.83 | 0.00 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.27 | 0.00 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.50 | 0.00 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.93 | 0.00 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

 **
 ** TIME SLICE FREEWAY PERFORMANCE TABLE **
 **

| SUB NO. | SEC | LNS | SSEC LENGTH | O-D DATA ORG DES | DEMANDS SSEC | ADJUSTED VOLUMES ORG DES | SSEC SSEC | WEAVE EFF | CONGEST LENGTH | STORAGE RATE | V/C RATIO | SPEED MPH | DENSITY VP/MPH | LOS LEVEL | FUEL MPG | EMI SS GS/VM |
|---------|-----|-----|-------------|------------------|--------------|--------------------------|-----------|-----------|----------------|--------------|-----------|-----------|----------------|-----------|----------|--------------|
|---------|-----|-----|-------------|------------------|--------------|--------------------------|-----------|-----------|----------------|--------------|-----------|-----------|----------------|-----------|----------|--------------|

* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
* *

TIME SLICE FREEWAY PERFORMANCE TABLE

Table with columns: SUB NO, SSEC, O-D DATA DEMANDS, ADJUSTED VOLUMES, SSEC, WEAVE, CONGEST, STORAGE, V/C, SPEED DENSITY, LOS, FUEL, EMISSIONS. Includes summary row: TOTAL 140349. = 26.6 MILES MAX(V/C) = 0.84 LOWEST LOS = C AVG = 65. 20.8 20.0 13.7

Summary table with columns: CURRENT TIME SLICE, CUMULATIVE VALUES. Includes rows for: FREEWAY TRAVEL TIME, FREEWAY MERGE DELAY, ON-RAMP M/RG/CAP DELAY, OFF-RAMP DELAY, TOTAL SYSTEM TRAVEL TIME, TOTAL FRWAY TRAV DISTANCE, AVERAGE SYSTEM SPEED, AVERAGE DENSITY, TOTAL FUEL, TOTAL EMISSIONS.

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

Table with columns: SUBSECTION, DELAY. Shows delay values for subsections 1 through 32.

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

```

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ    1111    222222  PPPPPPPP EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE  Q*A.D.MAY*Q  111111  222  222  PPPPPPPP EEEEEEEEE
FFF      RRR      RRR      EEE      QQQQQ  QQQQQ  1111  222  222  PPP  PPP  EEE
FFF      RRR      RRR      EEE      QQQ  QQQ  1111  222  222  PPP  PPP  EEE
FFFFFFFF RRRRRRRR EEEEEEEEE QQQ  QQQ  QQQ  1111  222  PPPPPPPP EEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE QQQ  QQQ  QQQ  1111  222  PPPPPPPP EEEEE
FFF      RRR RRR  EEE      QQQ  QQQ  QQQ  1111  2222  PPP  EEE
FFF      RRR RRR  EEE      Q*UC*  QQQQ  1111  222  PPP  EEE
FFF      RRR RRR  EEEEEEEEE Q*REGENTS*Q  1111  222  PPP  EEEEEEEEE
FFF      RRR RRR  EEEEEEEEE Q*1999*Q QQ  1111111  2222222222  PPP  EEEEEEEEE
    
```

FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 35
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65 MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

```

*****
*****
**                                     **
**                      FREeway AND ARTERIAL DESIGN FEATURES                **
**                                     **
*****
** SUB NO.  SSEC  SSEC  DESIGN  ORG  TRK  SSEC  PCT  PCT  DES  SPECIAL  FF.SPD.  CAP.  ART  GRADE  SUBSECTION LOCATION
**  SEC  LNS   CAP   LENGTH  SPEED  DES  FAC  GRAD  TRK  TRUCKS  RAMP   ALT. RTE  ALT. RTE  TYPE  ALT. RTE                                     **
*****
**  1  5  12500.   500.  65    OD  0.96  0.0  4    0    NO    0.0    0.    GOOD  0.0  Seeding
**
**  2  3  8660.    99999.  65    0.96  0.0  4    0    NO    0.0    0.    GOOD  0.0  Queue Capture
**
**  3  3  7000.     2830.  65    0.96  0.0  4    0    NO    0.0    0.    GOOD  0.0  SR-87 to DLC loop-on
**
**  4  3  7000.     930.   65    0.96  0.0  4    0    NO    0.0    0.    GOOD  0.0  DLC loop on to dia-on
**
**  5  3  7000.     1490.  65    0.96  0.0  4    0    NO    0.0    0.    GOOD  0.0  DLC dia-on to Tomas off
**
**  6  3  7000.     3020.  65    0.96  0.0  4    0    NO    0.0    0.    GOOD  0.0  Tomas off to on
**
**  7  3  7000.     1030.  65    0.96  0.0  4    0    NO    0.0    0.    GOOD  0.0  Tomas on to bowers off
**
**  8  3  7000.     1440.  65    0.96  0.0  4    0    NO    0.0    0.    GOOD  0.0  Bowers off to loop-on
**
**  9  3  7000.     1430.  65    0.96  0.0  4    0    NO    0.0    0.    GOOD  0.0  Bowers loop-on to dia
**
**  10 3  7000.     3480.  65    0.96  0.0  4    0    NO    0.0    0.    GOOD  0.0  Bowers dia-on to law-off
**
**  11 3  7000.     1020.  65    0.96  0.0  4    0    NO    0.0    0.    GOOD  0.0  Law off to loop-on
**
**  12 3  7000.     980.   65    0.96  0.0  4    0    NO    0.0    0.    GOOD  0.0  Lawr Loop to diag
**
**  13 3  7000.     1800.  65    0.96  0.0  4    0    YES   0.0    0.    GOOD  0.0  Lawrence On-ramp
**
**  14 3  7000.     1500.  65    D  0.96  0.0  4    0    NO    0.0    0.    GOOD  0.0  Fair Oaks Off-Ramp
**
**  15 3  6000.     1300.  65    0.96  0.0  4    0    NO    0.0    0.    GOOD  0.0  Fair Oaks / Fair Oaks
**
**  16 3  6000.     1000.  65    0  0.96  0.0  4    0    YES   0.0    0.    GOOD  0.0  Fair Oaks On-Ramp
**
**  17 3  6000.     1100.  65    0.96  0.0  4    0    NO    0.0    0.    GOOD  0.0  Fair Oaks / Mathilda
**
**  18 4  7490.     1000.  65    D  0.96  0.0  4    0    NO    0.0    0.    GOOD  0.0  Mathilda NB Off-Ramp
**
**  19 3  6000.     900.   65    0.96  0.0  4    0    NO    0.0    0.    GOOD  0.0  Mathilda / Mathilda
**
**  20 3  6000.     100.   65    0  0.96  0.0  4    0    YES   0.0    0.    GOOD  0.0  Mathilda NB On-Ramp
**
*****
*****
    
```

```

*****
**
**
**          FREeway AND ARTERIAL DESIGN FEATURES          **
**
*****
**
** SUB NO.  SSEC  SSEC  DESIGN  ORG  TRK  SSEC  PCT  PCT  DES  SPECIAL  FF.SPD.  CAP.  ART  GRADE  SUBSECTION LOCATION
** SEC  LNS  CAP  LENGTH  SPEED  DES  FAC  GRAD  TRK  TRUCKS  RAMP  ALT. RTE  ALT. RTE  TYPE  ALT. RTE
**
** 21  3  6000.  100.  65      0.96  0.0  4   0   NO    0.0    0.  GOOD  0.0  Mathilda / Mathilda
** 22  3  6000.  100.  65      0.96  0.0  4   0   NO    0.0    0.  GOOD  0.0  Mathilda SB Off-ramp
** 23  3  6000.  700.  65      0.96  0.0  4   0   NO    0.0    0.  GOOD  0.0  Mathilda / SR-237
** 24  3  6000.  1500.  65     D  0.96  0.0  4   0   NO    0.0    0.  GOOD  0.0  SR-237 WB Off-Ramp
** 25  3  6000.  800.  65      0.96  0.0  4   0   NO    0.0    0.  GOOD  0.0  SR-237 / SR-237
** 26  3  6000.  1000.  65     0  0.96  0.0  4   0   YES   0.0    0.  GOOD  0.0  SR-237 WB On-Ramp
** 27  3  6000.  800.  65      0.96  0.0  4   0   YES   0.0    0.  GOOD  0.0  SR-237 / Ellis
** 28  3  6000.  1000.  65     D  0.96  0.0  4   0   NO    0.0    0.  GOOD  0.0  Ellis Off-ramp
** 29  3  6000.  8000.  65      0.96  0.0  4   0   NO    0.0    0.  GOOD  0.0  HOV Dummy
** 30  5  10000.  100.  65     0  0.96  0.0  4   0   NO    0.0    0.  GOOD  0.0  HOV Dummy
** 31  5  6000.  1000.  65     0  0.96  0.0  4   0   YES   0.0    0.  GOOD  0.0  Dummy Bottleneck
** 32  5  6000.  2640.  65     D  1.00  0.0  0   0   NO    0.0    0.  GOOD  0.0  End of Network
**
*****

```

***** INPUT HAS BEEN COMPLETED *****

QUEUE COLLISION IN SECTION 16 T2 =0.631
QUEUE COLLISION IN SECTION 15 T2 =0.476
QUEUE COLLISION IN SECTION 14 T2 =0.499

```

*****
**
**          FREeway TRAVEL TIME (MINUTES)          **
**
*****

```

```

*****
* ORIGIN DESTINATIONS ACROSS
* DOWN
*   1     2     3     4     5     6
+-----+-----+-----+-----+-----+-----+
* 1 * 0.09 26.38 28.64 30.84 33.38 41.99
+-----+-----+-----+-----+-----+-----+
* 2 * 0.00 0.00 1.46 3.66 6.20 14.81
+-----+-----+-----+-----+-----+-----+
* 3 * 0.00 0.00 0.00 1.61 4.15 12.76
+-----+-----+-----+-----+-----+-----+
* 4 * 0.00 0.00 0.00 0.00 1.75 10.36
+-----+-----+-----+-----+-----+-----+
* 5 * 0.00 0.00 0.00 0.00 0.00 0.80
+-----+-----+-----+-----+-----+-----+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.64
+-----+-----+-----+-----+-----+-----+
*
*****

```

US-101_NB_AM_P2_2018_PE.txt
TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB SEC | * NO. LNS | * SSEC LENGTH | * O-D DATA ORG | * DEMANDS DES SSEC | * ADJUSTED ORG | * VOLUMES DES SSEC | * SSEC CAP. | * WEAVE EFF | * CONGEST LENGTH | * STORAGE RATE | * V/C RATIO | * SPEED MPH | * DENSITY VPMPPL | * LOS LEVEL | * FUEL MPG | * EMISSIONS GS/VM | | | |
|--|-----------|---------------|----------------|--------------------|----------------|--------------------|-------------|-------------|------------------|----------------|-------------|-------------|------------------|-------------|------------|-------------------|------|------|------|
| * 1 | 5 | 500. | 8472. | 1609. | 8472. | 8472. | 1609. | 8472. | 12500. | 0. | 0. | 0. | .68 | 65. | 26.1 | D | 19.2 | 14.0 | |
| * 2 | 3 | 99999. | 0. | 0. | 6863. | 0. | 0. | 4543. | 8660. | 0. | ** | 726. | 2320. | .52 | 63. | 23.9 | F | 19.9 | 13.4 |
| * 3 | 3 | 2830. | 0. | 0. | 6863. | 0. | 0. | 4543. | 7000. | 0. | ** | 2830. | 2320. | .65 | 46. | 33.3 | F | 22.7 | 11.8 |
| * 4 | 3 | 930. | 0. | 0. | 6863. | 0. | 0. | 4543. | 7000. | 0. | ** | 930. | 2320. | .65 | 41. | 37.0 | F | 22.1 | 12.1 |
| * 5 | 3 | 1490. | 0. | 0. | 6863. | 0. | 0. | 4543. | 7000. | 0. | ** | 1490. | 2320. | .65 | 38. | 39.5 | F | 21.8 | 12.4 |
| * 6 | 3 | 3020. | 0. | 0. | 6863. | 0. | 0. | 4543. | 7000. | 0. | ** | 3020. | 2320. | .65 | 34. | 44.3 | F | 21.2 | 12.8 |
| * 7 | 3 | 1030. | 0. | 0. | 6863. | 0. | 0. | 4543. | 7000. | 0. | ** | 1030. | 2320. | .65 | 31. | 48.7 | F | 20.7 | 13.3 |
| * 8 | 3 | 1440. | 0. | 0. | 6863. | 0. | 0. | 4543. | 7000. | 0. | ** | 1440. | 2320. | .65 | 29. | 51.5 | F | 20.4 | 13.5 |
| * 9 | 3 | 1430. | 0. | 0. | 6863. | 0. | 0. | 4543. | 7000. | 0. | ** | 1430. | 2320. | .65 | 28. | 54.8 | F | 20.0 | 13.8 |
| * 10 | 3 | 3480. | 0. | 0. | 6863. | 0. | 0. | 4543. | 7000. | 0. | ** | 3480. | 2320. | .65 | 25. | 60.7 | F | 19.4 | 14.4 |
| * 11 | 3 | 1020. | 0. | 0. | 6863. | 0. | 0. | 4543. | 7000. | 0. | ** | 1020. | 2320. | .65 | 23. | 66.4 | F | 18.8 | 15.0 |
| * 12 | 3 | 980. | 0. | 0. | 6863. | 0. | 0. | 4543. | 7000. | 0. | ** | 980. | 2320. | .65 | 22. | 69.0 | F | 18.5 | 15.2 |
| * 13 | 3 | 1800. | 0. | 0. | 6863. | 0. | 0. | 4543. | 7000. | 0. | ** | 1800. | 2320. | .65 | 21. | 72.7 | F | 18.2 | 15.6 |
| * 14 | 3 | 1500. | 0. | 770. | 6863. | 0. | 765. | 4543. | 6820. | 0. | ** | 1500. | 2277. | .67 | 21. | 73.6 | F | 18.2 | 15.6 |
| * 15 | 3 | 1300. | 0. | 0. | 6093. | 0. | 0. | 3778. | 6000. | 0. | ** | 1300. | 2222. | .63 | 19. | 67.4 | F | 17.7 | 16.1 |
| * 16 | 3 | 1000. | 653. | 0. | 6746. | 553. | 0. | 4331. | 5903. | 0. | ** | 1000. | 1572. | .73 | 28. | 51.8 | F | 20.3 | 13.8 |
| * 17 | 3 | 1100. | 0. | 0. | 6746. | 0. | 0. | 4331. | 6000. | 0. | ** | 1100. | 1572. | .72 | 26. | 54.5 | F | 19.7 | 14.3 |
| * 18 | 4 | 1000. | 0. | 1051. | 6746. | 0. | 919. | 4331. | 7271. | 0. | ** | 1000. | 1572. | .60 | 19. | 55.6 | F | 16.0 | 17.2 |
| * 19 | 3 | 900. | 0. | 0. | 5695. | 0. | 0. | 3412. | 6000. | 0. | ** | 900. | 1572. | .57 | 17. | 65.3 | F | 15.3 | 17.7 |
| * 20 | 3 | 100. | 271. | 0. | 5966. | 240. | 0. | 3652. | 5951. | 0. | ** | 100. | 1572. | .61 | 19. | 65.4 | F | 16.5 | 17.0 |
| * 21 | 3 | 100. | 0. | 0. | 5966. | 0. | 0. | 3652. | 6000. | 0. | ** | 100. | 1572. | .61 | 18. | 66.5 | F | 16.2 | 17.2 |
| * 22 | 3 | 100. | 0. | 0. | 5966. | 0. | 0. | 3652. | 6000. | 0. | ** | 100. | 1572. | .61 | 18. | 66.9 | F | 16.2 | 17.2 |
| * 23 | 3 | 700. | 0. | 0. | 5966. | 0. | 0. | 3652. | 6000. | 0. | ** | 700. | 1572. | .61 | 18. | 68.5 | F | 16.1 | 17.4 |
| * 24 | 3 | 1500. | 0. | 836. | 5966. | 0. | 732. | 3652. | 5835. | 0. | ** | 1500. | 1572. | .63 | 17. | 69.8 | F | 16.4 | 17.4 |
| * 25 | 3 | 800. | 0. | 0. | 5130. | 0. | 0. | 2920. | 6000. | 0. | ** | 800. | 1572. | .49 | 11. | 84.9 | F | 12.6 | 20.5 |
| * 26 | 3 | 1000. | 1214. | 0. | 6344. | 1214. | 0. | 4134. | 5739. | 0. | ** | 1000. | 1572. | .72 | 20. | 70.5 | F | 17.8 | 16.3 |
| * 27 | 3 | 800. | 0. | 0. | 6344. | 0. | 0. | 4134. | 6000. | 0. | ** | 800. | 1572. | .69 | 18. | 78.2 | F | 16.8 | 17.3 |
| * 28 | 3 | 1000. | 0. | 459. | 6344. | 0. | 414. | 4134. | 5929. | 0. | ** | 1000. | 1572. | .70 | 17. | 79.1 | F | 16.8 | 17.4 |
| * 29 | 3 | 8000. | 0. | 0. | 5885. | 0. | 0. | 3720. | 6000. | 0. | ** | 8000. | 1572. | .62 | 12. | 106.5 | F | 13.8 | 21.0 |
| * 30 | 5 | 100. | 1380. | 0. | 7265. | 1380. | 0. | 5100. | 10000. | 0. | ** | 100. | 1572. | .51 | 7. | 148.0 | F | 9.8 | 26.4 |
| * 31 | 5 | 1000. | 1000. | 0. | 8265. | 900. | 0. | 6000. | 6000. | 0. | 0. | 0. | 1.00 | 65. | 18.5 | E | 19.2 | 14.0 | |
| * 32 | 5 | 2640. | 0. | 8265. | 8265. | 0. | 6000. | 6000. | 6000. | 0. | 0. | 0. | 1.00 | 65. | 18.5 | E | 20.0 | 13.7 | |
| ***** | | | | | | | | | | | | | | | | | | | |
| * TOTAL 144589. = 27.4 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 43. 36.1 19.5 13.9 * | | | | | | | | | | | | | | | | | | | |
| ***** | | | | | | | | | | | | | | | | | | | |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 2/29/2016 16:40 PAGE 7
UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
TIME SLICE 1 OF 2

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 4039. VEH-HRS | 4060. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 116. VEH-HRS | 125. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 4155. VEH-HRS | 4185. PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 175631. VEH-MI. | 176663. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 42. MPH. | 43. MPH. |
| AVERAGE DENSITY = | 36. VPMPPL | 36. VPMPPL |
| TOTAL FUEL = | 9062. GALLONS | 9062. GALLONS |
| TOTAL EMISSIONS = | 2461. KILOGRAMS | 2461. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|--------|------------|-------|
| 1 | 0.02 | 2 | 54.23 | 3 | 23.65 | 4 | 10.53 | 5 | 19.71 |
| 6 | 50.68 | 7 | 20.57 | 8 | 31.57 | 9 | 34.58 | 10 | 97.62 |
| 11 | 32.23 | 12 | 32.51 | 13 | 63.66 | 14 | 53.24 | 15 | 45.13 |
| 16 | 20.57 | 17 | 24.53 | 18 | 35.41 | 19 | 30.24 | 20 | 3.21 |
| 21 | 3.29 | 22 | 3.31 | 23 | 23.81 | 24 | 51.59 | 25 | 38.42 |
| 26 | 31.84 | 27 | 29.20 | 28 | 36.77 | 29 | 422.51 | 30 | 12.54 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 1337.2 VEH-HRS ***** AVERAGE DELAY = 19.87 MIN/VEH *****

***** RAMP DELAYS *****

| ON-RAMP | RAMP | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-----------|--------|-----------------------|---------------|--------------------------------|----------|---------|---------|----------|----------------------|
| ON-RAMP 2 | RAMP | 100. | 50.00 | 4.59 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 50.00 | 4.59 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| ON-RAMP 3 | RAMP | 31. | 15.50 | 3.43 | 5.53 | 0.34 | 1.80 | 0.10 | 2.23 |
| | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 31. | 15.50 | 3.43 | 5.53 | 0.34 | 1.80 | 0.10 | 2.23 |
| ON-RAMP 6 | RAMP | 100. | 50.00 | 3.70 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 50.00 | 3.70 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 2/29/2016 16:40 PAGE 8
UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
TIME SLICE 2 OF 2

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 **
 ** FREEWAY TRAVEL TIME (MINUTES)
 **

```

*****
* ORIGIN S DESTINATIONS ACROSS *
* DOWN 1 2 3 4 5 6 *
* ***** *
* * *
* 1 * 0.09 32.90 35.27 37.76 40.51 48.50 *
* 2 * 0.00 0.00 1.57 4.06 6.82 14.80 *
* 3 * 0.00 0.00 0.00 1.75 4.50 12.48 *
* 4 * 0.00 0.00 0.00 0.00 1.82 9.80 *
* 5 * 0.00 0.00 0.00 0.00 0.00 0.79 *
* 6 * 0.00 0.00 0.00 0.00 0.00 0.64 *
* * *
*****
  
```

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 2/29/2016 16:40 PAGE 9
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 2

```

*****
* TIME SLICE FREEWAY PERFORMANCE TABLE *
* ***** *
* SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMISSIONS *
* SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMP L LEVEL MPG GS/VM *
* ***** *
* 1 5 500. 7322. 1391. 7322. 7322. 1391. 7322. 12500. 0. 0. 0. .59 65. 22.5 C 19.2 14.0 *
* 2 3 99999. 0. 0. 5931. 0. 0. 5687. 8660. 0. * 3694. 244. .66 59. 32.3 F 19.1 14.1 *
* 3 3 2830. 0. 0. 5931. 0. 0. 5687. 7000. 0. ** 2830. 244. .81 18. 107.5 F 17.4 17.4 *
* 4 3 930. 0. 0. 5931. 0. 0. 5687. 7000. 0. ** 930. 244. .81 18. 107.5 F 17.4 17.4 *
* 5 3 1490. 0. 0. 5931. 0. 0. 5687. 7000. 0. ** 1490. 244. .81 18. 107.5 F 17.4 17.4 *
* 6 3 3020. 0. 0. 5931. 0. 0. 5687. 7000. 0. ** 3020. 244. .81 18. 107.5 F 17.4 17.4 *
* 7 3 1030. 0. 0. 5931. 0. 0. 5687. 7000. 0. ** 1030. 244. .81 18. 107.5 F 17.4 17.4 *
* 8 3 1440. 0. 0. 5931. 0. 0. 5687. 7000. 0. ** 1440. 244. .81 18. 107.5 F 17.4 17.4 *
* 9 3 1430. 0. 0. 5931. 0. 0. 5687. 7000. 0. ** 1430. 244. .81 18. 107.5 F 17.4 17.4 *
* 10 3 3480. 0. 0. 5931. 0. 0. 5687. 7000. 0. ** 3480. 244. .81 18. 107.5 F 17.4 17.4 *
* 11 3 1020. 0. 0. 5931. 0. 0. 5687. 7000. 0. ** 1020. 244. .81 18. 107.5 F 17.4 17.4 *
* 12 3 980. 0. 0. 5931. 0. 0. 5687. 7000. 0. ** 980. 244. .81 18. 107.5 F 17.4 17.4 *
* 13 3 1800. 0. 0. 5931. 0. 0. 5687. 7000. 0. ** 1800. 244. .81 18. 107.5 F 17.4 17.4 *
* 14 3 1500. 0. 705. 5931. 0. 705. 5687. 6835. 0. ** 1500. 244. .83 19. 100.8 F 17.9 16.7 *
* 15 3 1300. 0. 0. 5226. 0. 0. 4982. 6000. 0. ** 1300. 244. .83 19. 88.8 F 17.9 16.8 *
* 16 3 1000. 649. 0. 5875. 649. 0. 5631. 5919. 0. ** 1000. 244. .95 29. 65.3 F 21.2 13.1 *
* 17 3 1100. 0. 0. 5875. 0. 0. 5631. 6000. 0. ** 1100. 244. .94 27. 68.6 F 20.8 13.5 *
* 18 4 1000. 0. 1236. 5875. 0. 1231. 5631. 7236. 0. ** 1000. 244. .78 16. 89.1 F 16.6 18.4 *
* 19 3 900. 0. 0. 4639. 0. 0. 4400. 6000. 0. ** 900. 244. .73 14. 106.9 F 15.3 19.9 *
* 20 3 100. 288. 0. 4927. 240. 0. 4640. 5953. 0. ** 100. 244. .78 16. 97.6 F 16.6 18.4 *
* 21 3 100. 0. 0. 4927. 0. 0. 4640. 6000. 0. ** 100. 244. .77 16. 99.5 F 16.5 18.5 *
* 22 3 100. 0. 0. 4927. 0. 0. 4640. 6000. 0. ** 100. 244. .77 16. 99.5 F 16.5 18.5 *
* 23 3 700. 0. 0. 4927. 0. 0. 4640. 6000. 0. ** 700. 244. .77 17. 99.5 F 16.5 18.5 *
* 24 3 1500. 0. 932. 4927. 0. 918. 4640. 5821. 0. ** 1500. 244. .80 17. 92.2 F 17.0 17.9 *
* 25 3 800. 0. 0. 3995. 0. 0. 3723. 6000. 0. ** 800. 244. .62 10. 128.0 F 12.7 23.2 *
* 26 3 1000. 1053. 0. 5048. 1053. 0. 4776. 5783. 0. ** 1000. 244. .83 18. 86.4 F 17.7 16.9 *
* 27 3 800. 0. 0. 5048. 0. 0. 4776. 6000. 0. ** 800. 244. .80 17. 95.3 F 17.0 17.9 *
* 28 3 1000. 0. 540. 5048. 0. 534. 4776. 5921. 0. ** 1000. 244. .81 17. 92.0 F 17.2 17.6 *
* 29 3 8000. 0. 0. 4508. 0. 0. 4242. 6000. 0. ** 8000. 244. .71 13. 111.9 F 14.6 20.7 *
* 30 5 100. 1058. 0. 5566. 1058. 0. 5300. 10000. 0. ** 100. 244. .53 7. 144.9 F 10.1 26.0 *
* 31 5 1000. 700. 0. 6266. 700. 0. 6000. 6000. 0. 0. 0. 1.00 65. 18.5 E 19.2 14.0 *
* 32 5 2640. 0. 6266. 6266. 0. 6000. 6000. 6000. 0. 0. 0. 1.00 65. 18.5 E 20.0 13.7 *
* ***** *
* * *
* TOTAL 144589. = 27.4 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 36. 51.9 18.5 15.1 *
* *****
  
```

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 2/29/2016 16:40 PAGE 10
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 2

| | CURRENT TIME SLICE | | | CUMULATIVE VALUES | | | | |
|----------------------------|--------------------|------------|---------|-------------------|---------|------------|---------|----------|
| FREWAY TRAVEL TIME = | 4390. | VEH-HRS | 4411. | PASS-HRS | 8429. | VEH-HRS | 8471. | PASS-HRS |
| FREWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 255. | VEH-HRS | 274. | PASS-HRS | 371. | VEH-HRS | 399. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 4645. | VEH-HRS | 4685. | PASS-HRS | 8799. | VEH-HRS | 8870. | PASS-HRS |
| TOTAL TRAV DISTANCE = | 156727. | VEH-MI. | 157743. | PASS-MI. | 332358. | VEH-MI. | 334407. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 34. | MPH. | | | 39. | MPH. | | |
| AVERAGE DENSITY = | 52. | VPMP | | | 44. | VPMP | | |
| TOTAL FUEL = | 8576. | GALLONS | | | 17638. | GALLONS | | |
| TOTAL EMISSIONS = | 2397. | KI LOGRAMS | | | 4858. | KI LOGRAMS | | |

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***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|--------|------------|--------|------------|--------|------------|--------|------------|--------|
| 1 | 0.00 | 2 | 186.81 | 3 | 125.99 | 4 | 41.40 | 5 | 66.33 |
| 6 | 134.45 | 7 | 45.86 | 8 | 64.11 | 9 | 63.66 | 10 | 154.93 |
| 11 | 45.41 | 12 | 43.63 | 13 | 80.14 | 14 | 61.06 | 15 | 46.73 |
| 16 | 20.71 | 17 | 24.84 | 18 | 51.12 | 19 | 43.14 | 20 | 4.19 |
| 21 | 4.30 | 22 | 4.30 | 23 | 30.09 | 24 | 58.29 | 25 | 49.52 |
| 26 | 35.19 | 27 | 32.16 | 28 | 38.38 | 29 | 409.56 | 30 | 12.18 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 1978.5 VEH-HRS ***** AVERAGE DELAY = 23.30 MIN/VEH *****

***** RAMP DELAYS *****

| | | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS | |
|---------|---|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|-------|
| ON-RAMP | 2 | RAMP | 100. | 100.00 | 8.01 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 100.00 | 8.01 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP | 3 | RAMP | 79. | 55.00 | 10.34 | 19.64 | 1.22 | 6.37 | 0.34 | 7.93 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 79. | 55.00 | 10.34 | 19.64 | 1.22 | 6.37 | 0.34 | 7.93 |
| ON-RAMP | 6 | RAMP | 100. | 100.00 | 9.00 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 100.00 | 9.00 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |

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FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP LLL
FFFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 1111111 222222222 PPP LLLLLLLLLL
    
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FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 2 AND 29 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 35
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65 MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

FREEWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC | SSEC | DESIGN | ORG | TRK | SSEC | PCT | PCT | DES | SPECIAL | FF.SPD. | CAP. | ART | GRADE | SUBSECTION | LOCATION |
|---------|------|-------|--------|-----|-----|------|-----|--------|------|---------|----------|----------|------|----------|--------------------------|----------|
| SEC | LNS | CAP | SPEED | DES | FAC | GRAD | TRK | TRUCKS | RAMP | RAMP | ALT. RTE | ALT. RTE | TYPE | ALT. RTE | | |
| 1 | | | | | | | | | | | | | | | | |
| 2 | 1 | 1650. | 99999. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | |
| 3 | 1 | 1650. | 2830. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-87 to DLC loop-on | |
| 4 | 1 | 1650. | 930. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | DLC loop on to dia-on | |
| 5 | 1 | 1650. | 1490. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | DLC dia-on to Tomas off | |
| 6 | 1 | 1650. | 3020. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas off to on | |
| 7 | 1 | 1650. | 1030. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas on to bowers off | |
| 8 | 1 | 1650. | 1440. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers off to loop-on | |
| 9 | 1 | 1650. | 1430. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers loop-on to dia | |
| 10 | 1 | 1650. | 3480. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers dia-on to law-off | |
| 11 | 1 | 1650. | 1020. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Law off to loop-on | |
| 12 | 1 | 1650. | 980. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Lawr Loop to diag | |
| 13 | 1 | 1650. | 1800. | 65 | | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Lawrence On-ramp | |
| 14 | 1 | 1650. | 1500. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks Off-Ramp | |
| 15 | 1 | 1650. | 1300. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Fair Oaks | |
| 16 | 1 | 1650. | 1000. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Fair Oaks On-Ramp | |
| 17 | 1 | 1650. | 1100. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Mathilda | |
| 18 | 1 | 1650. | 1000. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda NB Off-Ramp | |
| 19 | 1 | 1650. | 900. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | |

```

**
** 20 1 1650. 100. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Mathilda NB On-Ramp **
**
*****

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FREEWAY AND ARTERIAL DESIGN FEATURES

```

*****
**
** SUB NO. SSEC SSEC DESIGN ORG TRK SSEC PCT PCT DES SPECIAL FF. SPD. CAP. ART GRADE SUBSECTION LOCATION **
** SEC LNS CAP LENGTH SPEED DES FAC GRAD TRK TRUCKS RAMP ALT. RTE ALT. RTE TYPE ALT. RTE **
*****
** 21 1 1650. 100. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Mathilda / Mathilda **
** 22 1 1650. 100. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Mathilda SB Off-ramp **
** 23 1 1650. 700. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Mathilda / SR-237 **
** 24 1 1650. 1500. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 SR-237 WB Off-Ramp **
** 25 1 1650. 800. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 SR-237 / SR-237 **
** 26 1 1650. 1000. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 SR-237 WB On-Ramp **
** 27 1 1650. 800. 65 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 SR-237 / Ellis **
** 28 1 1650. 1000. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Ellis Off-ramp **
** 29 1 1650. 8000. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 HOV Dummy **
** 30 **
** 31 **
** 32 **
*****

```

FREEWAY TRAVEL TIME (MINUTES)

```

*****
* ORIGINS DESTINATIONS ACROSS *
* DOWN 1 2 3 4 5 6 7 *
+
* * * * *
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 2 * 0.00 25.34 26.17 26.77 27.44 28.84 0.00
+
* 3 * 0.00 0.00 0.00 0.00 0.00 3.27 0.00
+
* 4 * 0.00 0.00 0.00 0.00 0.00 2.50 0.00
+
* 5 * 0.00 0.00 0.00 0.00 0.00 1.93 0.00
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* * *
*****

```

TIME SLICE FREEWAY PERFORMANCE TABLE

```

*****
* SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMISS *
* SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMP LEVEL MPG GS/VM *
*****
Page 2

```

Table with 15 columns (ID, Lane, Volume, Delay, LOS, etc.) and 32 rows of data, followed by a summary row: TOTAL 140349. = 26.6 MILES MAX(V/C) = 0.98 LOWEST LOS = D AVG = 55. 28.7 24.1 11.4

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 16:40 PAGE 6
UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
TIME SLICE 1 OF 2

Summary table with two columns: CURRENT TIME SLICE and CUMULATIVE VALUES. Rows include: FREEWAY TRAVEL TIME, FREEWAY MERGE DELAY, ON-RAMP MRG/CAP DELAY, OFF-RAMP DELAY, TOTAL SYSTEM TRAVEL TIME, TOTAL FRWAY TRAV DISTANCE, AVERAGE SYSTEM SPEED, AVERAGE DENSITY, TOTAL FUEL, TOTAL EMISSIONS.

Table with 10 columns: SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY. Includes summary row: ***** TOTAL DELAY = 115.1 VEH-HRS ***** AVERAGE DELAY = 4.30 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 16:40 PAGE 7
UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
TIME SLICE 2 OF 2

**
** FREEWAY TRAVEL TIME (MINUTES) **
**

Table with 7 columns: ORIGINS DOWN, DESTINATIONS ACROSS. Rows 1-5 showing origin/destination delays.

US-101_NB_AM_P2_2018_PL.txt
 * 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
 * 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
 * *

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|-----------|---------|--------------------|--------------------|----------------|----------|-----------------|----------------|-----------|---------|-----------|---------|--------|-------------|
| * SEC | * LNS | * LENGTH | * ORG DES SSEC | * ORG DES SSEC | * CAP. | * LENGTH | * RATE | * RATIO | * MPH | * VPMPPL | * LEVEL | * MPG | * GS/VM |
| * 1 | | | | | | | | | | | | | |
| * 2 | 1 | 99999 | 1391. 0. 1391. | 1391. 0. 1391. | 1650. 0. | 0. | 0. | .84 | 65. | 21.4 | C | 20.0 | 13.7 |
| * 3 | 1 | 2830. | 0. 0. 1391. | 0. 0. 1391. | 1650. 0. | 0. | 0. | .84 | 65. | 21.4 | C | 20.0 | 13.7 |
| * 4 | 1 | 930. | 0. 0. 1391. | 0. 0. 1391. | 1650. 0. | 0. | 0. | .84 | 65. | 21.4 | C | 20.0 | 13.7 |
| * 5 | 1 | 1490. | 0. 0. 1391. | 0. 0. 1391. | 1650. 0. | 0. | 0. | .84 | 65. | 21.4 | C | 20.0 | 13.7 |
| * 6 | 1 | 3020. | 0. 0. 1391. | 0. 0. 1391. | 1650. 0. | 0. | 0. | .84 | 65. | 21.4 | C | 20.0 | 13.7 |
| * 7 | 1 | 1030. | 0. 0. 1391. | 0. 0. 1391. | 1650. 0. | 0. | 0. | .84 | 65. | 21.4 | C | 20.0 | 13.7 |
| * 8 | 1 | 1440. | 0. 0. 1391. | 0. 0. 1391. | 1650. 0. | 0. | 0. | .84 | 65. | 21.4 | C | 20.0 | 13.7 |
| * 9 | 1 | 1430. | 0. 0. 1391. | 0. 0. 1391. | 1650. 0. | 0. | 0. | .84 | 65. | 21.4 | C | 20.0 | 13.7 |
| * 10 | 1 | 3480. | 0. 0. 1391. | 0. 0. 1391. | 1650. 0. | 0. | 0. | .84 | 65. | 21.4 | C | 20.0 | 13.7 |
| * 11 | 1 | 1020. | 0. 0. 1391. | 0. 0. 1391. | 1650. 0. | 0. | 0. | .84 | 65. | 21.4 | C | 20.0 | 13.7 |
| * 12 | 1 | 980. | 0. 0. 1391. | 0. 0. 1391. | 1650. 0. | 0. | 0. | .84 | 65. | 21.4 | C | 20.0 | 13.7 |
| * 13 | 1 | 1800. | 0. 0. 1391. | 0. 0. 1391. | 1650. 0. | 0. | 0. | .84 | 65. | 21.4 | C | 20.0 | 13.7 |
| * 14 | 1 | 1500. | 0. 165. 1391. | 0. 165. 1391. | 1650. 0. | 0. | 0. | .84 | 65. | 21.4 | C | 20.0 | 13.7 |
| * 15 | 1 | 1300. | 0. 0. 1226. | 0. 0. 1226. | 1650. 0. | 0. | 0. | .74 | 65. | 18.9 | C | 20.0 | 13.7 |
| * 16 | 1 | 1000. | 81. 0. 1306. | 81. 0. 1306. | 1650. 0. | 0. | 0. | .79 | 65. | 20.1 | C | 20.0 | 13.7 |
| * 17 | 1 | 1100. | 0. 0. 1306. | 0. 0. 1306. | 1650. 0. | 0. | 0. | .79 | 65. | 20.1 | C | 20.0 | 13.7 |
| * 18 | 1 | 1000. | 0. 254. 1306. | 0. 254. 1306. | 1650. 0. | 0. | 0. | .79 | 65. | 20.1 | C | 20.0 | 13.7 |
| * 19 | 1 | 900. | 0. 0. 1052. | 0. 0. 1052. | 1650. 0. | 0. | 0. | .64 | 65. | 16.2 | B | 20.0 | 13.7 |
| * 20 | 1 | 100. | 47. 0. 1099. | 47. 0. 1099. | 1650. 0. | 0. | 0. | .67 | 65. | 16.9 | B | 20.0 | 13.7 |
| * 21 | 1 | 100. | 0. 0. 1099. | 0. 0. 1099. | 1650. 0. | 0. | 0. | .67 | 65. | 16.9 | B | 20.0 | 13.7 |
| * 22 | 1 | 100. | 0. 0. 1099. | 0. 0. 1099. | 1650. 0. | 0. | 0. | .67 | 65. | 16.9 | B | 20.0 | 13.7 |
| * 23 | 1 | 700. | 0. 0. 1099. | 0. 0. 1099. | 1650. 0. | 0. | 0. | .67 | 65. | 16.9 | B | 20.0 | 13.7 |
| * 24 | 1 | 1500. | 0. 179. 1099. | 0. 179. 1099. | 1650. 0. | 0. | 0. | .67 | 65. | 16.9 | B | 20.0 | 13.7 |
| * 25 | 1 | 800. | 0. 0. 920. | 0. 0. 920. | 1650. 0. | 0. | 0. | .56 | 65. | 14.2 | B | 20.0 | 13.7 |
| * 26 | 1 | 1000. | 217. 0. 1137. | 217. 0. 1137. | 1650. 0. | 0. | 0. | .69 | 65. | 17.5 | B | 20.0 | 13.7 |
| * 27 | 1 | 800. | 0. 0. 1137. | 0. 0. 1137. | 1650. 0. | 0. | 0. | .69 | 65. | 17.5 | B | 20.0 | 13.7 |
| * 28 | 1 | 1000. | 0. 79. 1137. | 0. 79. 1137. | 1650. 0. | 0. | 0. | .69 | 65. | 17.5 | B | 20.0 | 13.7 |
| * 29 | 1 | 8000. | 0. 1058. 1058. | 0. 1058. 1058. | 1650. 0. | 0. | 0. | .64 | 65. | 16.3 | B | 20.0 | 13.7 |
| * 30 | | | | | | | | | | | | | |
| * 31 | | | | | | | | | | | | | |
| * 32 | | | | | | | | | | | | | |
| * TOTAL | 140349. | = | 26.6 MILES | | | MAX(V/C) = 0.84 | LOWEST LOS = C | AVG = 65. | 20.8 | | | 20.0 | 13.7 |

| CURRENT TIME SLICE | CUMULATIVE VALUES |
|--------------------|-------------------|
| 553. VEH-HRS | 1107. PASS-HRS |
| 1315. VEH-HRS | 2630. PASS-HRS |
| 0. VEH-HRS | 0. PASS-HRS |
| 0. VEH-HRS | 0. PASS-HRS |
| 0. VEH-HRS | 0. PASS-HRS |
| 0. VEH-HRS | 0. PASS-HRS |
| 553. VEH-HRS | 1107. PASS-HRS |
| 1315. VEH-HRS | 2630. PASS-HRS |
| 35976. VEH-MI. | 71953. PASS-MI. |
| 77999. VEH-MI. | 155998. PASS-MI. |
| 65. MPH. | 59. MPH. |
| 21. VPMPPL | 25. VPMPPL |
| 1799. GALLONS | 3546. GALLONS |
| 494. KILOGRAMS | 973. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | 30 | 0.00 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

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FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP EEE
FFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP PPP EEEEEEEEE
    
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FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65 MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREEWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SEC | LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT DES TRUCKS | SPECIAL RAMP | FF. SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION | LOCATION |
|---------|-----|--------|----------|-------------|--------------|---------|---------|-----------|---------|----------------|--------------|-------------------|---------------|----------|--------------------------|------------|----------|
| 1 | 4 | 10000. | 500. | 65 | OD | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Seeding | | |
| 2 | 3 | 7000. | 99999. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | | |
| 3 | 3 | 7000. | 2830. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-87 to DLC loop-on | | |
| 4 | 3 | 7000. | 930. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | DLC loop on to dia-on | | |
| 5 | 3 | 7000. | 1490. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | DLC dia-on to Tomas off | | |
| 6 | 3 | 7000. | 3020. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas off to on | | |
| 7 | 3 | 7000. | 1030. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas on to bowers off | | |
| 8 | 3 | 7000. | 1440. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers off to loop-on | | |
| 9 | 3 | 7000. | 1430. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers loop-on to dia | | |
| 10 | 3 | 7000. | 3480. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers dia-on to law-off | | |
| 11 | 3 | 7000. | 1020. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Law off to loop-on | | |
| 12 | 3 | 7000. | 980. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawr Loop to diag | | |
| 13 | 3 | 7000. | 1800. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Lawrence On-ramp | | |
| 14 | 3 | 7000. | 1500. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks Off-Ramp | | |
| 15 | 3 | 6000. | 1300. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Fair Oaks | | |
| 16 | 3 | 6000. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Fair Oaks On-Ramp | | |
| 17 | 3 | 6000. | 1100. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Mathilda | | |
| 18 | 4 | 7020. | 1000. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda NB Off-Ramp | | |
| 19 | 3 | 6000. | 900. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | | |
| 20 | 3 | 6000. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda NB On-Ramp | | |

FREeway AND ARTERIAL DESIGN FEATURES

| SUB NO. | SEC | LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT TRUCKS | DES SPECIAL RAMP | FF.SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION | LOCATION |
|---------|-----|-------|----------|-------------|--------------|---------|---------|-----------|---------|------------|------------------|------------------|---------------|----------|----------------|----------------------|----------|
| ** 21 | 3 | 6000. | 100. | 65 | | 0.96 | 0.0 | 4 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | |
| ** 22 | 3 | 6000. | 100. | 65 | D | 0.96 | 0.0 | 4 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda SB Off-ramp | |
| ** 23 | 3 | 6000. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / SR-237 | |
| ** 24 | 3 | 6000. | 1500. | 65 | D | 0.96 | 0.0 | 4 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 WB Off-Ramp | |
| ** 25 | 3 | 6000. | 800. | 65 | | 0.96 | 0.0 | 4 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 / SR-237 | |
| ** 26 | 3 | 6000. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 WB On-Ramp | |
| ** 27 | 3 | 6000. | 800. | 65 | | 0.96 | 0.0 | 4 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 / Ellis | |
| ** 28 | 3 | 6000. | 1000. | 65 | D | 0.96 | 0.0 | 4 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Ellis Off-ramp | |
| ** 29 | 3 | 6000. | 8000. | 65 | | 0.96 | 0.0 | 4 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | |
| ** 30 | 4 | 8000. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | |
| ** 31 | 4 | 5500. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Dummy Bottleneck | |
| ** 32 | 4 | 8000. | 2640. | 65 | D | 1.00 | 0.0 | 0 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End of Network | |

***** INPUT HAS BEEN COMPLETED *****

MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 4 IN TIME SLICE 1
--- THE MAXIMUM METERING RATE WILL PREVAIL.

MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 4 IN TIME SLICE 2
--- THE MAXIMUM METERING RATE WILL PREVAIL.

FREeway TRAVEL TIME (MINUTES)

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | |
|--------------|---------------------|-------|-------|-------|-------|-------|-------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 0.09 | 21.28 | 22.06 | 22.27 | 22.65 | 23.29 | 27.79 |
| * 2 * | 0.00 | 0.00 | 0.55 | 0.76 | 1.14 | 1.79 | 6.28 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.05 | 0.44 | 1.08 | 5.58 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.50 | 5.00 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.81 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.64 |

TIME SLICE FREeway PERFORMANCE TABLE

US-101_NB_PM_NP_2018_PE.txt

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*****
* SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMI SS *
* SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMP L LEVEL MPG GS/VM *
*****
* 1 4 500. 5522. 718. 5522. 5522. 718. 5522. 10000. 0. 0. 0. .55 65. 21.2 C 19.2 14.0 *
* 2 3 99999. 0. 0. 4804. 0. 0. 4804. 7000. 0. 0. 0. .69 65. 24.7 C 19.2 13.9 *
* 3 3 2830. 0. 0. 4804. 0. 0. 4804. 7000. 0. 0. 0. .69 65. 24.7 C 19.2 13.9 *
* 4 3 930. 0. 0. 4804. 0. 0. 4804. 7000. 0. 0. 0. .69 65. 24.7 C 19.2 13.9 *
* 5 3 1490. 0. 0. 4804. 0. 0. 4804. 7000. 0. 0. 0. .69 65. 24.7 C 19.2 13.9 *
* 6 3 3020. 0. 0. 4804. 0. 0. 4804. 7000. 0. 0. 0. .69 65. 24.7 C 19.2 13.9 *
* 7 3 1030. 0. 0. 4804. 0. 0. 4804. 7000. 0. 0. 0. .69 65. 24.7 C 19.2 13.9 *
* 8 3 1440. 0. 0. 4804. 0. 0. 4804. 7000. 0. 0. 0. .69 65. 24.7 C 19.2 13.9 *
* 9 3 1430. 0. 0. 4804. 0. 0. 4804. 7000. 0. 0. 0. .69 65. 24.7 C 19.2 13.9 *
* 10 3 3480. 0. 0. 4804. 0. 0. 4804. 7000. 0. 0. 0. .69 65. 24.7 C 19.2 13.9 *
* 11 3 1020. 0. 0. 4804. 0. 0. 4804. 7000. 0. 0. 0. .69 65. 24.7 C 19.2 13.9 *
* 12 3 980. 0. 0. 4804. 0. 0. 4804. 7000. 0. 0. 0. .69 65. 24.7 C 19.2 13.9 *
* 13 3 1800. 0. 0. 4804. 0. 0. 4804. 7000. 0. 0. 0. .69 65. 24.7 C 19.2 13.9 *
* 14 3 1500. 0. 539. 4804. 0. 539. 4804. 6919. 0. 0. 0. .69 65. 24.7 C 19.3 13.9 *
* 15 3 1300. 0. 0. 4265. 0. 0. 4265. 6000. 0. 0. 0. .71 65. 21.9 C 19.2 14.0 *
* 16 3 1000. 338. 0. 4603. 240. 0. 4505. 5967. 0. 0. 0. .75 64. 23.4 C 19.6 13.7 *
* 17 3 1100. 0. 0. 4603. 0. 0. 4505. 6000. 0. 0. 0. .75 64. 23.4 C 19.5 13.7 *
* 18 4 1000. 0. 176. 4603. 0. 172. 4505. 6996. 0. 0. 0. .64 65. 17.3 B 19.2 14.0 *
* 19 3 900. 0. 0. 4427. 0. 0. 4333. 6000. 0. 0. 0. .72 65. 22.2 C 19.2 14.0 *
* 20 3 100. 210. 0. 4637. 210. 0. 4543. 5979. 0. 0. 0. .76 64. 23.7 C 19.6 13.7 *
* 21 3 100. 0. 0. 4637. 0. 0. 4543. 6000. 0. 0. 0. .76 64. 23.6 C 19.6 13.7 *
* 22 3 100. 0. 513. 4637. 0. 502. 4543. 5933. 0. 0. 0. .77 64. 23.7 C 19.7 13.6 *
* 23 3 700. 0. 0. 4124. 0. 0. 4041. 6000. 0. 0. 0. .67 65. 20.7 C 19.2 14.0 *
* 24 3 1500. 0. 629. 4124. 0. 615. 4041. 5918. 0. 0. 0. .68 65. 20.7 C 19.2 14.0 *
* 25 3 800. 0. 0. 3495. 0. 0. 3426. 6000. 0. 0. 0. .57 65. 17.6 B 19.2 14.0 *
* 26 3 1000. 1623. 0. 5118. 1273. 0. 4699. 5773. 0. 0. 0. .81 63. 25.0 C 20.2 13.2 *
* 27 3 800. 0. 0. 5118. 0. 0. 4699. 6000. 0. 0. 0. .78 64. 24.7 C 19.8 13.5 *
* 28 3 1000. 0. 296. 5118. 0. 270. 4699. 5975. 0. 0. 0. .79 63. 24.7 C 19.9 13.5 *
* 29 3 8000. 0. 0. 4822. 0. 0. 4080. 6000. 0. * 4214. 349. .68 25. 55.2 F 16.5 16.4 *
* 30 4 100. 720. 0. 5542. 720. 0. 4800. 8000. 0. ** 100. 349. .60 7. 181.4 F 9.5 26.7 *
* 31 4 1000. 800. 0. 6342. 700. 0. 5500. 5500. 0. 0. 0. 1.00 65. 21.2 E 19.2 14.0 *
* 32 4 2640. 0. 6342. 6342. 0. 5500. 5500. 8000. 0. 0. 0. .69 65. 21.2 C 20.0 13.7 *
*****
* TOTAL 144589. = 27.4 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 60. 26.2 19.1 14.1 *
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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVISION
 TIME SLICE 1 OF 3

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CURRENT TIME SLICE CUMULATIVE VALUES
FREEWAY TRAVEL TIME = 2190. VEH-HRS 2201. PASS-HRS 2190. VEH-HRS 2201. PASS-HRS
FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 274. VEH-HRS 281. PASS-HRS 274. VEH-HRS 281. PASS-HRS
OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 2464. VEH-HRS 2481. PASS-HRS 2464. VEH-HRS 2481. PASS-HRS
TOTAL TRAVEL DISTANCE = 130414. VEH-MI. 131017. PASS-MI. 130414. VEH-MI. 131017. PASS-MI.
AVERAGE SYSTEM SPEED = 53. MPH. 60. MPH.
AVERAGE DENSITY = 26. VPMP L 26. VPMP L
TOTAL FUEL = 6928. GALLONS 6928. GALLONS
TOTAL EMISSIONS = 1874. KI LOGRAMS 1874. KI LOGRAMS

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***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
1 0.00 2 3.23 3 0.09 4 0.03 5 0.05
6 0.10 7 0.03 8 0.05 9 0.05 10 0.11
11 0.03 12 0.03 13 0.06 14 0.06 15 0.00
16 0.18 17 0.19 18 0.00 19 0.00 20 0.02
21 0.02 22 0.02 23 0.00 24 0.00 25 0.00
26 0.50 27 0.25 28 0.33 29 165.55 30 12.36
31 0.00 32 0.00
***** TOTAL DELAY = 183.3 VEH-HRS ***** AVERAGE DELAY = 2.66 MIN/VEH *****

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***** RAMP DELAYS *****
OUEUE LENGTH DELAY AVERAGE METERING DELAY GAS HC CO NOX TOTAL
VEHICLES VEH-HRS MI MINUTES GALS KGMS KGMS KGMS EMISSIONS
ON-RAMP 2 RAMP 98. 49.00 8.70 17.50 1.09 5.68 0.30 7.06
FREEWAY 0. 0.00 0.00 0.00 0.00 0.00 0.00 0.00
TOTAL 98. 49.00 8.70 17.50 1.09 5.68 0.30 7.06
ON-RAMP 4 RAMP 350. 175.00 5.68 62.49 3.88 20.27 1.08 25.23
FREEWAY 0. 0.00 0.00 0.00 0.00 0.00 0.00 0.00
TOTAL 350. 175.00 5.68 62.49 3.88 20.27 1.08 25.23
ON-RAMP 6 RAMP 100. 50.00 4.31 17.85 1.11 5.79 0.31 7.21
FREEWAY 0. 0.00 0.00 0.00 0.00 0.00 0.00 0.00
TOTAL 100. 50.00 4.31 17.85 1.11 5.79 0.31 7.21

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVISION
 TIME SLICE 2 OF 3

 **

US-101_NB_PM_NP_2018_PE.txt
 ** FREEWAY TRAVEL TIME (MINUTES) **

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*****
* ORIGINS DESTINATIONS ACROSS *
* DOWN 1 2 3 4 5 6 7 *
* ***** *
* * *
+
* 1 * 0.09 21.38 22.16 22.37 22.80 25.19 40.77 *
+
* 2 * 0.00 0.00 0.55 0.76 1.19 3.58 19.16 *
+
* 3 * 0.00 0.00 0.00 0.05 0.49 2.87 18.45 *
+
* 4 * 0.00 0.00 0.00 0.00 0.00 1.93 17.50 *
+
* 5 * 0.00 0.00 0.00 0.00 0.00 0.00 0.89 *
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.64 *
* * *
*****
    
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TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB | * NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | | |
|---------|--------|----------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|---------|------------|-----------|--------------|--------|-------------|------|------|------|------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * ORG | * DES | * SSEC | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | | | |
| * 1 | 4 | 500 | 5821 | 757 | 5821 | 5821 | 757 | 5821 | 10000 | 0 | 0 | .58 | 65 | 22.4 | C | 19.2 | 14.0 | | | |
| * 2 | 3 | 99999 | 0 | 0 | 5064 | 0 | 0 | 5064 | 7000 | 0 | 0 | .72 | 65 | 26.2 | D | 19.4 | 13.8 | | | |
| * 3 | 3 | 2830 | 0 | 0 | 5064 | 0 | 0 | 5064 | 7000 | 0 | 0 | .72 | 65 | 26.2 | D | 19.4 | 13.8 | | | |
| * 4 | 3 | 930 | 0 | 0 | 5064 | 0 | 0 | 5064 | 7000 | 0 | 0 | .72 | 65 | 26.2 | D | 19.4 | 13.8 | | | |
| * 5 | 3 | 1490 | 0 | 0 | 5064 | 0 | 0 | 5064 | 7000 | 0 | 0 | .72 | 65 | 26.2 | D | 19.4 | 13.8 | | | |
| * 6 | 3 | 3020 | 0 | 0 | 5064 | 0 | 0 | 5064 | 7000 | 0 | 0 | .72 | 65 | 26.2 | D | 19.4 | 13.8 | | | |
| * 7 | 3 | 1030 | 0 | 0 | 5064 | 0 | 0 | 5064 | 7000 | 0 | 0 | .72 | 65 | 26.2 | D | 19.4 | 13.8 | | | |
| * 8 | 3 | 1440 | 0 | 0 | 5064 | 0 | 0 | 5064 | 7000 | 0 | 0 | .72 | 65 | 26.2 | D | 19.4 | 13.8 | | | |
| * 9 | 3 | 1430 | 0 | 0 | 5064 | 0 | 0 | 5064 | 7000 | 0 | 0 | .72 | 65 | 26.2 | D | 19.4 | 13.8 | | | |
| * 10 | 3 | 3480 | 0 | 0 | 5064 | 0 | 0 | 5064 | 7000 | 0 | 0 | .72 | 65 | 26.2 | D | 19.4 | 13.8 | | | |
| * 11 | 3 | 1020 | 0 | 0 | 5064 | 0 | 0 | 5064 | 7000 | 0 | 0 | .72 | 65 | 26.2 | D | 19.4 | 13.8 | | | |
| * 12 | 3 | 980 | 0 | 0 | 5064 | 0 | 0 | 5064 | 7000 | 0 | 0 | .72 | 65 | 26.2 | D | 19.4 | 13.8 | | | |
| * 13 | 3 | 1800 | 0 | 0 | 5064 | 0 | 0 | 5064 | 7000 | 0 | 0 | .72 | 65 | 26.2 | D | 19.4 | 13.8 | | | |
| * 14 | 3 | 1500 | 0 | 818 | 5064 | 0 | 818 | 5064 | 6878 | 0 | 0 | .74 | 64 | 26.2 | D | 19.4 | 13.8 | | | |
| * 15 | 3 | 1300 | 0 | 0 | 4246 | 0 | 0 | 4246 | 6000 | 0 | 0 | .71 | 65 | 21.8 | C | 19.2 | 14.0 | | | |
| * 16 | 3 | 1000 | 387 | 0 | 4633 | 385 | 0 | 4631 | 5967 | 0 | 0 | .78 | 64 | 24.2 | C | 19.8 | 13.6 | | | |
| * 17 | 3 | 1100 | 0 | 0 | 4633 | 0 | 0 | 4631 | 6000 | 0 | 0 | .77 | 64 | 24.2 | C | 19.7 | 13.6 | | | |
| * 18 | 4 | 1000 | 0 | 194 | 4633 | 0 | 194 | 4631 | 6994 | 0 | 0 | .66 | 65 | 17.8 | B | 19.2 | 14.0 | | | |
| * 19 | 3 | 900 | 0 | 0 | 4439 | 0 | 0 | 4437 | 6000 | 0 | 0 | .74 | 64 | 23.0 | C | 19.5 | 13.8 | | | |
| * 20 | 3 | 100 | 194 | 0 | 4633 | 194 | 0 | 4631 | 5983 | 0 | 0 | .77 | 64 | 24.2 | C | 19.7 | 13.6 | | | |
| * 21 | 3 | 100 | 0 | 0 | 4633 | 0 | 0 | 4631 | 6000 | 0 | 0 | .77 | 64 | 24.2 | C | 19.7 | 13.6 | | | |
| * 22 | 3 | 100 | 0 | 708 | 4633 | 0 | 704 | 4631 | 5908 | 0 | 0 | .78 | 64 | 24.3 | C | 19.8 | 13.5 | | | |
| * 23 | 3 | 700 | 0 | 0 | 3925 | 0 | 0 | 3927 | 6000 | 0 | 0 | .65 | 65 | 20.1 | C | 19.2 | 14.0 | | | |
| * 24 | 3 | 1500 | 0 | 859 | 3925 | 0 | 855 | 3114 | 5888 | 0 | ** | 690 | 813 | .53 | 55 | 18.9 | F | 18.8 | 14.2 | |
| * 25 | 3 | 800 | 0 | 0 | 3066 | 0 | 0 | 2259 | 6000 | 0 | ** | 800 | 813 | .38 | 20 | 38.1 | F | 16.7 | 15.7 | |
| * 26 | 3 | 1000 | 1610 | 0 | 4676 | 1277 | 0 | 3536 | 5777 | 0 | ** | 1000 | 813 | .61 | 22 | 53.8 | F | 15.6 | 16.9 | |
| * 27 | 3 | 800 | 0 | 0 | 4676 | 0 | 0 | 3536 | 6000 | 0 | ** | 800 | 813 | .59 | 16 | 72.2 | F | 14.3 | 18.2 | |
| * 28 | 3 | 1000 | 0 | 314 | 4676 | 0 | 288 | 3536 | 5974 | 0 | ** | 1000 | 813 | .59 | 13 | 88.3 | F | 13.3 | 19.5 | |
| * 29 | 3 | 8000 | 0 | 0 | 4362 | 0 | 0 | 3248 | 6000 | 0 | ** | 8000 | 813 | .54 | 6 | 174.9 | F | 9.4 | 26.3 | |
| * 30 | 4 | 100 | 652 | 0 | 5014 | 652 | 0 | 3900 | 8000 | 0 | ** | 100 | 813 | .49 | 5 | 214.0 | F | 8.4 | 28.7 | |
| * 31 | 4 | 1000 | 1600 | 0 | 6614 | 1600 | 0 | 5500 | 5500 | 0 | 0 | 0 | 1.00 | 65 | 21.2 | E | 19.2 | 14.0 | | |
| * 32 | 4 | 2640 | 0 | 6614 | 6614 | 0 | 5500 | 5500 | 8000 | 0 | 0 | .69 | 65 | 21.2 | C | 20.0 | 13.7 | | | |
| ***** | | | | | | | | | | | | | | | | | | | | |
| * TOTAL | 144589 | = | 27.4 | MILES | | | | | | | | MAX(V/C) = | 1.00 | LOWEST LOS = | F | AVG = | 46 | 35.1 | 18.5 | 14.4 |
| ***** | | | | | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | | | CUMULATIVE VALUES | | | | |
|----------------------------|--------------------|-----------|---------|-------------------|---------|-----------|---------|----------|
| FREWAY TRAVEL TIME = | 2953. | VEH-HRS | 2964. | PASS-HRS | 5142. | VEH-HRS | 5165. | PASS-HRS |
| FREWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 716. | VEH-HRS | 729. | PASS-HRS | 990. | VEH-HRS | 1009. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 3668. | VEH-HRS | 3693. | PASS-HRS | 6132. | VEH-HRS | 6174. | PASS-HRS |
| TOTAL TRAV DISTANCE = | 134488. | VEH-MI. | 135091. | PASS-MI. | 264902. | VEH-MI. | 266108. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 37. | MPH. | | | 52. | MPH. | | |
| AVERAGE DENSITY = | 35. | VPMP | | | 31. | VPMP | | |
| TOTAL FUEL = | 7520. | GALLONS | | | 14448. | GALLONS | | |
| TOTAL EMISSIONS = | 2039. | KILOGRAMS | | | 3912. | KILOGRAMS | | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

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| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|--------|------------|-------|
| 1 | 0.00 | 2 | 10.46 | 3 | 0.30 | 4 | 0.10 | 5 | 0.16 |
| 6 | 0.32 | 7 | 0.11 | 8 | 0.15 | 9 | 0.15 | 10 | 0.36 |
| 11 | 0.11 | 12 | 0.10 | 13 | 0.19 | 14 | 0.21 | 15 | 0.00 |
| 16 | 0.28 | 17 | 0.28 | 18 | 0.00 | 19 | 0.12 | 20 | 0.03 |
| 21 | 0.03 | 22 | 0.03 | 23 | 0.00 | 24 | 3.11 | 25 | 15.77 |
| 26 | 23.72 | 27 | 28.15 | 28 | 44.73 | 29 | 739.63 | 30 | 15.07 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 883.6 VEH-HRS ***** AVERAGE DELAY = 16.17 MIN/VEH *****

***** RAMP DELAYS *****

| | | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|---------|---|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|
| ON-RAMP | 2 | RAMP | 100. | 99.00 | 12.25 | 35.35 | 2.19 | 11.47 | 14.27 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 99.00 | 12.25 | 35.35 | 2.19 | 11.47 | 14.27 |
| ON-RAMP | 4 | RAMP | 683. | 516.50 | 14.20 | 184.43 | 11.44 | 59.84 | 74.45 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 683. | 516.50 | 14.20 | 184.43 | 11.44 | 59.84 | 74.45 |
| ON-RAMP | 6 | RAMP | 100. | 100.00 | 4.02 | 35.71 | 2.22 | 11.58 | 14.41 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 100.00 | 4.02 | 35.71 | 2.22 | 11.58 | 14.41 |

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 TIME SLICE 3 OF 3

 ** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS | * DESTINATIONS ACROSS | | | | | | |
|-----------|-----------------------|-------|-------|-------|-------|-------|-------|
| * DOWN | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 0.09 | 21.23 | 22.00 | 22.21 | 22.71 | 26.43 | 37.63 |
| * 2 * | 0.00 | 0.00 | 0.54 | 0.75 | 1.25 | 4.97 | 16.17 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.05 | 0.55 | 4.27 | 15.47 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.86 | 14.05 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.81 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.64 |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL NO DIVERSION
 TIME SLICE 3 OF 3

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISS | | | | |
|-----------|--------|------------|-----------|--------------------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|---------|------|---|------|------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * CAP. | * EFF | * RATE | * RATIO | * MPH | * VPMPL | * LEVEL | * MPG | * GS/VM | | | | |
| * 1 | 4 | 500. | 5091. | 662. | 5091. | 5091. | 662. | 5091. | 10000. | 0. | 0. | 0. | .51 | 65. | 19.6 | C | 19.2 | 14.0 |
| * 2 | 3 | 99999. | 0. | 0. | 4429. | 0. | 0. | 4429. | 7000. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 |
| * 3 | 3 | 2830. | 0. | 0. | 4429. | 0. | 0. | 4429. | 7000. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 |
| * 4 | 3 | 930. | 0. | 0. | 4429. | 0. | 0. | 4429. | 7000. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 |
| * 5 | 3 | 1490. | 0. | 0. | 4429. | 0. | 0. | 4429. | 7000. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 |
| * 6 | 3 | 3020. | 0. | 0. | 4429. | 0. | 0. | 4429. | 7000. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 |
| * 7 | 3 | 1030. | 0. | 0. | 4429. | 0. | 0. | 4429. | 7000. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 |
| * 8 | 3 | 1440. | 0. | 0. | 4429. | 0. | 0. | 4429. | 7000. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 |
| * 9 | 3 | 1430. | 0. | 0. | 4429. | 0. | 0. | 4429. | 7000. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 |
| * 10 | 3 | 3480. | 0. | 0. | 4429. | 0. | 0. | 4429. | 7000. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 |
| * 11 | 3 | 1020. | 0. | 0. | 4429. | 0. | 0. | 4429. | 7000. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 |
| * 12 | 3 | 980. | 0. | 0. | 4429. | 0. | 0. | 4429. | 7000. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 |
| * 13 | 3 | 1800. | 0. | 0. | 4429. | 0. | 0. | 4429. | 7000. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 |
| * 14 | 3 | 1500. | 0. | 644. | 4429. | 0. | 644. | 4429. | 6904. | 0. | 0. | 0. | .64 | 65. | 22.7 | C | 19.2 | 14.0 |
| * 15 | 3 | 1300. | 0. | 0. | 3785. | 0. | 0. | 3785. | 6000. | 0. | 0. | 0. | .63 | 65. | 19.4 | C | 19.2 | 14.0 |
| * 16 | 3 | 1000. | 340. | 0. | 4125. | 340. | 0. | 4125. | 5970. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 19.2 | 14.0 |
| * 17 | 3 | 1100. | 0. | 0. | 4125. | 0. | 0. | 4125. | 6000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 19.2 | 14.0 |
| * 18 | 4 | 1000. | 0. | 150. | 4125. | 0. | 150. | 4125. | 7000. | 0. | 0. | 0. | .59 | 65. | 15.9 | B | 19.2 | 14.0 |
| * 19 | 3 | 900. | 0. | 0. | 3975. | 0. | 0. | 3975. | 6000. | 0. | 0. | 0. | .66 | 65. | 20.4 | C | 19.2 | 14.0 |
| * 20 | 3 | 100. | 183. | 0. | 4158. | 183. | 0. | 4158. | 5983. | 0. | 0. | 0. | .69 | 65. | 21.3 | C | 19.2 | 14.0 |
| * 21 | 3 | 100. | 0. | 0. | 4158. | 0. | 0. | 4158. | 6000. | 0. | 0. | 0. | .69 | 65. | 21.3 | C | 19.2 | 14.0 |

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| | | | | | | | | | | | | | | | | | | | | |
|--|---|-------|-------|-------|-------|-------|-------|-------|-------|----|----|-------|-------|------|-------|-------|------|------|------|---|
| *22 | 3 | 100. | 0. | 611. | 4158. | 0. | 611. | 4158. | 5921. | 0. | 0. | .70 | 65. | 21.3 | C | 19.2 | 14.0 | * | | |
| *23 | 3 | 700. | 0. | 0. | 3547. | 0. | 0. | 3547. | 6000. | 0. | 0. | 0. | .59 | 65. | 18.2 | C | 19.2 | 14.0 | * | |
| *24 | 3 | 1500. | 0. | 735. | 3547. | 0. | 735. | 3547. | 5905. | 0. | 0. | 0. | .60 | 45. | 26.2 | D | 18.3 | 14.7 | * | |
| *25 | 3 | 800. | 0. | 0. | 2812. | 0. | 0. | 2812. | 6000. | 0. | 0. | 0. | .47 | 11. | 88.9 | F | 12.4 | 20.2 | * | |
| *26 | 3 | 1000. | 1183. | 0. | 3995. | 1333. | 0. | 4145. | 5833. | 0. | 0. | 0. | .71 | 14. | 100.5 | F | 14.7 | 20.0 | * | |
| *27 | 3 | 800. | 0. | 0. | 3995. | 0. | 0. | 4402. | 6000. | 0. | * | 218. | -257. | .73 | 10. | 142.4 | F | 13.1 | 22.5 | * |
| *28 | 3 | 1000. | 0. | 203. | 3995. | 0. | 219. | 4402. | 5982. | 0. | ** | 1000. | -257. | .74 | 10. | 148.6 | F | 13.0 | 22.9 | * |
| *29 | 3 | 8000. | 0. | 0. | 3792. | 0. | 0. | 4183. | 6000. | 0. | ** | 8000. | -257. | .70 | 9. | 159.2 | F | 11.5 | 24.3 | * |
| *30 | 4 | 100. | 567. | 0. | 4359. | 567. | 0. | 4750. | 8000. | 0. | ** | 100. | -257. | .59 | 6. | 186.2 | F | 9.3 | 27.1 | * |
| *31 | 4 | 1000. | 750. | 0. | 5109. | 750. | 0. | 5500. | 5500. | 0. | 0. | 0. | 1.00 | 65. | 21.2 | E | 19.2 | 14.0 | * | |
| *32 | 4 | 2640. | 0. | 5109. | 5109. | 0. | 5500. | 5500. | 8000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 20.0 | 13.7 | * | |
| ***** | | | | | | | | | | | | | | | | | | | | |
| * TOTAL 144589. = 27.4 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 45. 32.7 18.4 14.7 * | | | | | | | | | | | | | | | | | | | | |
| ***** | | | | | | | | | | | | | | | | | | | | |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 3 OF 3

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|---|
| FREEWAY TRAVEL TIME = | 2710. VEH-HRS | 2721. PASS-HRS 7852. VEH-HRS 7886. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 808. VEH-HRS | 821. PASS-HRS 1798. VEH-HRS 1830. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 3518. VEH-HRS | 3542. PASS-HRS 9650. VEH-HRS 9716. PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 120666. VEH-MI. | 121260. PASS-MI. 385568. VEH-MI. 387368. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 34. MPH. | 49. MPH. |
| AVERAGE DENSITY = | 33. VP/MPL | 31. VP/MPL |
| TOTAL FUEL = | 6864. GALLONS | 21312. GALLONS |
| TOTAL EMISSIONS = | 1892. KILOGRAMS | 5805. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|--------|------------|-------|
| 1 | 0.00 | 2 | 0.06 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 6.84 | 25 | 35.10 |
| 26 | 47.02 | 27 | 54.28 | 28 | 71.60 | 29 | 626.00 | 30 | 12.72 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 853.6 VEH-HRS ***** AVERAGE DELAY = 12.40 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-----------|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|
| ON-RAMP 2 | RAMP 100. | 100.00 | 13.64 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 100. | 100.00 | 13.64 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP 4 | RAMP 533. | 608.00 | 17.94 | 217.10 | 13.47 | 70.44 | 3.74 | 87.64 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 533. | 608.00 | 17.94 | 217.10 | 13.47 | 70.44 | 3.74 | 87.64 |
| ON-RAMP 6 | RAMP 100. | 100.00 | 7.97 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 100. | 100.00 | 7.97 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |

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FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP LLL
FFFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 1111111 222222222 PPP LLLLLLLLLL
    
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FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 2 AND 29 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65 MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

FREEWAY AND ARTERIAL DESIGN FEATURES

| ** SUB NO. | ** SSEC | ** SSEC | ** DESIGN | ** ORG | ** TRK | ** SSEC | ** PCT | ** PCT | ** DES | ** SPECIAL | ** FF.SPD. | ** CAP. | ** ART | ** GRADE | ** SUBSECTION | ** LOCATION | ** |
|------------|---------|---------|-----------|--------|--------|---------|--------|-----------|---------|-------------|-------------|-------------|---------|-------------|--------------------------|-------------|----|
| ** SEC | ** LNS | ** CAP | ** SPEED | ** DES | ** FAC | ** GRAD | ** TRK | ** TRUCKS | ** RAMP | ** ALT. RTE | ** ALT. RTE | ** ALT. RTE | ** TYPE | ** ALT. RTE | ** | ** | ** |
| ** 1 | | | | | | | | | | | | | | | | | ** |
| ** 2 | 1 | 1650. | 99999. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | | ** |
| ** 3 | 1 | 1650. | 2830. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-87 to DLC loop-on | | ** |
| ** 4 | 1 | 1650. | 930. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | DLC loop on to dia-on | | ** |
| ** 5 | 1 | 1650. | 1490. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | DLC dia-on to Tomas off | | ** |
| ** 6 | 1 | 1650. | 3020. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas off to on | | ** |
| ** 7 | 1 | 1650. | 1030. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas on to bowers off | | ** |
| ** 8 | 1 | 1650. | 1440. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers off to loop-on | | ** |
| ** 9 | 1 | 1650. | 1430. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers loop-on to dia | | ** |
| ** 10 | 1 | 1650. | 3480. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers dia-on to law-off | | ** |
| ** 11 | 1 | 1650. | 1020. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Law off to loop-on | | ** |
| ** 12 | 1 | 1650. | 980. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Lawr Loop to diag | | ** |
| ** 13 | 1 | 1650. | 1800. | 65 | | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Lawrence On-ramp | | ** |
| ** 14 | 1 | 1650. | 1500. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks Off-Ramp | | ** |
| ** 15 | 1 | 1650. | 1300. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Fair Oaks | | ** |
| ** 16 | 1 | 1650. | 1000. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Fair Oaks On-Ramp | | ** |
| ** 17 | 1 | 1650. | 1100. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Mathilda | | ** |
| ** 18 | 1 | 1650. | 1000. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda NB Off-Ramp | | ** |
| ** 19 | 1 | 1650. | 900. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | | ** |

** 20 1 1650. 100. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Mathilda NB On-Ramp **

FREEWAY AND ARTERIAL DESIGN FEATURES

Table with columns: SUB NO., SEC LNS, SSEC CAP, SSEC LENGTH, DESIGN SPEED, ORG DES, TRK FAC, SSEC GRAD, PCT TRK, PCT TRUCKS, SPECIAL RAMP, FF. SPD. ALT. RTE, CAP. ALT. RTE, ART TYPE, GRADE ALT. RTE, SUBSECTION, LOCATION. Rows 21-32.

FREEWAY TRAVEL TIME (MINUTES)

Table with columns: ORIGINS DOWN, DESTINATIONS ACROSS (1-8). Rows 1-7.

TIME SLICE FREEWAY PERFORMANCE TABLE

Table with columns: SUB NO., SEC LNS, SSEC LENGTH, O-D DATA ORG DES, DEMANDS SSEC, ADJUSTED VOLUMES ORG DES SSEC, SSEC CAP., WEAVE EFF, CONGEST LENGTH, STORAGE RATE, V/C RATIO, SPEED MPH, DENSITY VP/MPH, LOS LEVEL, FUEL MPG, EMISSIONS GS/VM. Row 1.

US-101_NB_PM_NP_2018_PL.txt

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*****
*
* 1
* 2 1 99999. 718. 0. 718. 718. 0. 718. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 3 1 2830. 0. 0. 718. 0. 0. 718. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 4 1 930. 0. 0. 718. 0. 0. 718. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 5 1 1490. 0. 0. 718. 0. 0. 718. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 6 1 3020. 0. 0. 718. 0. 0. 718. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 7 1 1030. 0. 0. 718. 0. 0. 718. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 8 1 1440. 0. 0. 718. 0. 0. 718. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 9 1 1430. 0. 0. 718. 0. 0. 718. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 10 1 3480. 0. 0. 718. 0. 0. 718. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 11 1 1020. 0. 0. 718. 0. 0. 718. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 12 1 980. 0. 0. 718. 0. 0. 718. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 13 1 1800. 0. 0. 718. 0. 0. 718. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 14 1 1500. 0. 81. 718. 0. 81. 718. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 15 1 1300. 0. 0. 637. 0. 0. 637. 1650. 0. 0. 0. .39 65. 9.8 A 20.0 13.7 *
* 16 1 1000. 33. 0. 670. 33. 0. 670. 1650. 0. 0. 0. .41 65. 10.3 A 20.0 13.7 *
* 17 1 1100. 0. 0. 670. 0. 0. 670. 1650. 0. 0. 0. .41 65. 10.3 A 20.0 13.7 *
* 18 1 1000. 0. 24. 670. 0. 24. 670. 1650. 0. 0. 0. .41 65. 10.3 A 20.0 13.7 *
* 19 1 900. 0. 0. 646. 0. 0. 646. 1650. 0. 0. 0. .39 65. 9.9 A 20.0 13.7 *
* 20 1 100. 21. 0. 668. 21. 0. 668. 1650. 0. 0. 0. .40 65. 10.3 A 20.0 13.7 *
* 21 1 100. 0. 0. 668. 0. 0. 668. 1650. 0. 0. 0. .40 65. 10.3 A 20.0 13.7 *
* 22 1 100. 0. 67. 668. 0. 67. 668. 1650. 0. 0. 0. .40 65. 10.3 A 20.0 13.7 *
* 23 1 700. 0. 0. 600. 0. 0. 600. 1650. 0. 0. 0. .36 65. 9.2 A 20.0 13.7 *
* 24 1 1500. 0. 82. 600. 0. 82. 600. 1650. 0. 0. 0. .36 65. 9.2 A 20.0 13.7 *
* 25 1 800. 0. 0. 518. 0. 0. 518. 1650. 0. 0. 0. .31 65. 8.0 A 20.0 13.7 *
* 26 1 1000. 227. 0. 746. 227. 0. 746. 1650. 0. 0. 0. .45 65. 11.5 B 20.0 13.7 *
* 27 1 800. 0. 0. 746. 0. 0. 746. 1650. 0. 0. 0. .45 65. 11.5 B 20.0 13.7 *
* 28 1 1000. 0. 25. 746. 0. 25. 746. 1650. 0. 0. 0. .45 65. 11.5 B 20.0 13.7 *
* 29 1 8000. 0. 720. 720. 0. 720. 720. 1650. 0. 0. 0. .44 65. 11.1 B 20.0 13.7 *
* 30
* 31
* 32
*
*****
*
* TOTAL 140349. = 26.6 MILES MAX(V/C) = 0.45 LOWEST LOS = B AVG = 65. 11.0 20.0 13.7 *
*
*****

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 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 1 OF 3

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CURRENT TIME SLICE CUMULATIVE VALUES
FREEWAY TRAVEL TIME = 292. VEH-HRS 583. PASS-HRS 292. VEH-HRS 583. PASS-HRS
FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 292. VEH-HRS 583. PASS-HRS 292. VEH-HRS 583. PASS-HRS
TOTAL FRWAY TRAV DISTANCE = 18955. VEH-MI. 37910. PASS-MI. 18955. VEH-MI. 37910. PASS-MI.
AVERAGE SYSTEM SPEED = 65. MPH. 65. MPH.
AVERAGE DENSITY = 11. VPML 11. VPML
TOTAL FUEL = 948. GALLONS 948. GALLONS
TOTAL EMISSIONS = 260. KILOGRAMS 260. KILOGRAMS

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***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | 30 | 0.00 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

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 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 3

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*****
**
** FREEWAY TRAVEL TIME (MINUTES)
**
*****

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```

*****
* ORIGINS DESTINATIONS ACROSS *
* DOWN 1 2 3 4 5 6 7 8 *
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 2 * 0.00 21.14 21.91 22.12 22.51 23.14 24.54 0.00 *
+
* 3 * 0.00 0.00 0.00 0.00 0.00 0.00 3.16 0.00 *
+
* 4 * 0.00 0.00 0.00 0.00 0.00 0.00 2.47 0.00 *
+
* 5 * 0.00 0.00 0.00 0.00 0.00 0.00 1.89 0.00 *
+

```

```
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
* *
*****
```

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED | VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS |
|---------|---------|----------|--------------|--------------|--------------|-------|-------|---------|---------|-----------------|----------------|-----------|-------|------|--------|
| SEC | LNS | LENGTH | ORG DES SSEC | ORG DES SSEC | ORG DES SSEC | CAP. | EFF | LENGTH | RATE | RATIO | MPH | VP MPL | LEVEL | MPG | GS/VM |
| * 1 | | | | | | | | | | | | | | | |
| * 2 | 1 | 99999 | 757. 0. 757. | 757. 0. 757. | 0. 757. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 3 | 1 | 2830. | 0. 0. 757. | 0. 0. 757. | 0. 0. 757. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 4 | 1 | 930. | 0. 0. 757. | 0. 0. 757. | 0. 0. 757. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 5 | 1 | 1490. | 0. 0. 757. | 0. 0. 757. | 0. 0. 757. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 6 | 1 | 3020. | 0. 0. 757. | 0. 0. 757. | 0. 0. 757. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 7 | 1 | 1030. | 0. 0. 757. | 0. 0. 757. | 0. 0. 757. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 8 | 1 | 1440. | 0. 0. 757. | 0. 0. 757. | 0. 0. 757. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 9 | 1 | 1430. | 0. 0. 757. | 0. 0. 757. | 0. 0. 757. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 10 | 1 | 3480. | 0. 0. 757. | 0. 0. 757. | 0. 0. 757. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 11 | 1 | 1020. | 0. 0. 757. | 0. 0. 757. | 0. 0. 757. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 12 | 1 | 980. | 0. 0. 757. | 0. 0. 757. | 0. 0. 757. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 13 | 1 | 1800. | 0. 0. 757. | 0. 0. 757. | 0. 0. 757. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 14 | 1 | 1500. | 0. 122. 757. | 0. 122. 757. | 0. 122. 757. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 15 | 1 | 1300. | 0. 0. 635. | 0. 0. 635. | 0. 0. 635. | 1650. | 0. | 0. | 0. | .38 | 65. | 9.8 | A | 20.0 | 13.7 |
| * 16 | 1 | 1000. | 33. 0. 667. | 33. 0. 667. | 0. 667. | 1650. | 0. | 0. | 0. | .40 | 65. | 10.3 | A | 20.0 | 13.7 |
| * 17 | 1 | 1100. | 0. 0. 667. | 0. 0. 667. | 0. 667. | 1650. | 0. | 0. | 0. | .40 | 65. | 10.3 | A | 20.0 | 13.7 |
| * 18 | 1 | 1000. | 0. 26. 667. | 0. 26. 667. | 0. 26. 667. | 1650. | 0. | 0. | 0. | .40 | 65. | 10.3 | A | 20.0 | 13.7 |
| * 19 | 1 | 900. | 0. 0. 641. | 0. 0. 641. | 0. 641. | 1650. | 0. | 0. | 0. | .39 | 65. | 9.9 | A | 20.0 | 13.7 |
| * 20 | 1 | 100. | 17. 0. 658. | 17. 0. 658. | 0. 658. | 1650. | 0. | 0. | 0. | .40 | 65. | 10.1 | A | 20.0 | 13.7 |
| * 21 | 1 | 100. | 0. 0. 658. | 0. 0. 658. | 0. 658. | 1650. | 0. | 0. | 0. | .40 | 65. | 10.1 | A | 20.0 | 13.7 |
| * 22 | 1 | 100. | 0. 92. 658. | 0. 92. 658. | 0. 92. 658. | 1650. | 0. | 0. | 0. | .40 | 65. | 10.1 | A | 20.0 | 13.7 |
| * 23 | 1 | 700. | 0. 0. 566. | 0. 0. 566. | 0. 566. | 1650. | 0. | 0. | 0. | .34 | 65. | 8.7 | A | 20.0 | 13.7 |
| * 24 | 1 | 1500. | 0. 112. 566. | 0. 112. 566. | 0. 112. 566. | 1650. | 0. | 0. | 0. | .34 | 65. | 8.7 | A | 20.0 | 13.7 |
| * 25 | 1 | 800. | 0. 0. 454. | 0. 0. 454. | 0. 454. | 1650. | 0. | 0. | 0. | .28 | 65. | 7.0 | A | 20.0 | 13.7 |
| * 26 | 1 | 1000. | 223. 0. 678. | 223. 0. 678. | 0. 678. | 1650. | 0. | 0. | 0. | .41 | 65. | 10.4 | A | 20.0 | 13.7 |
| * 27 | 1 | 800. | 0. 0. 678. | 0. 0. 678. | 0. 678. | 1650. | 0. | 0. | 0. | .41 | 65. | 10.4 | A | 20.0 | 13.7 |
| * 28 | 1 | 1000. | 0. 26. 678. | 0. 26. 678. | 0. 26. 678. | 1650. | 0. | 0. | 0. | .41 | 65. | 10.4 | A | 20.0 | 13.7 |
| * 29 | 1 | 8000. | 0. 652. 652. | 0. 652. 652. | 0. 652. 652. | 1650. | 0. | 0. | 0. | .40 | 65. | 10.0 | A | 20.0 | 13.7 |
| * 30 | | | | | | | | | | | | | | | |
| * 31 | | | | | | | | | | | | | | | |
| * 32 | | | | | | | | | | | | | | | |
| * TOTAL | 140349. | = | 26.6 MILES | | | | | | | MAX(V/C) = 0.46 | LOWEST LOS = B | AVG = 65. | 11.4 | 20.0 | 13.7 |

| CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|-----------------------------|-----------------|-------------------|--------------------------------|
| FREEWAY TRAVEL TIME = | 303. VEH-HRS | 606. PASS-HRS | 594. VEH-HRS 1189. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 303. VEH-HRS | 606. PASS-HRS | 594. VEH-HRS 1189. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 19680. VEH-MI. | 39361. PASS-MI. | 38636. VEH-MI. 77271. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 65. MPH. | | 65. MPH. |
| AVERAGE DENSITY = | 11. VP MPL | | 11. VP MPL |
| TOTAL FUEL = | 984. GALLONS | | 1932. GALLONS |
| TOTAL EMISSIONS = | 270. KI LOGRAMS | | 531. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | 30 | 0.00 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

 **

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | | |
|-----------------|---------------------|-------|-------|-------|-------|-------|-------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 21.14 | 21.91 | 22.12 | 22.51 | 23.14 | 24.54 | 0.00 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.16 | 0.00 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.47 | 0.00 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.89 | 0.00 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB SEC | NO. LNS | SSEC LENGTH | O-D DATA ORG DES | DEMANDS SSEC | ADJUSTED VOLUMES ORG DES SSEC | SSEC CAP. | WEAVE EFF | CONGEST LENGTH | STORAGE RATE | V/C RATIO | SPEED MPH | DENSITY VPMPL | LOS LEVEL | FUEL MPG | EMI SS | GS/VM |
|------------|------------|----------------|---------------------|-----------------|----------------------------------|--------------|--------------|-------------------|-----------------|--------------|--------------|------------------|--------------|-------------|-----------|-----------|
| * 1 | | | | | | | | | | | | | | | | |
| * 2 | 1 | 99999 | 662. | 0. 662. | 662. 0. | 662. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 13.7 |
| * 3 | 1 | 2830. | 0. | 0. 662. | 0. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 13.7 |
| * 4 | 1 | 930. | 0. | 0. 662. | 0. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 13.7 |
| * 5 | 1 | 1490. | 0. | 0. 662. | 0. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 13.7 |
| * 6 | 1 | 3020. | 0. | 0. 662. | 0. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 13.7 |
| * 7 | 1 | 1030. | 0. | 0. 662. | 0. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 13.7 |
| * 8 | 1 | 1440. | 0. | 0. 662. | 0. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 13.7 |
| * 9 | 1 | 1430. | 0. | 0. 662. | 0. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 13.7 |
| * 10 | 1 | 3480. | 0. | 0. 662. | 0. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 13.7 |
| * 11 | 1 | 1020. | 0. | 0. 662. | 0. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 13.7 |
| * 12 | 1 | 980. | 0. | 0. 662. | 0. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 13.7 |
| * 13 | 1 | 1800. | 0. | 0. 662. | 0. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 13.7 |
| * 14 | 1 | 1500. | 0. | 96. 662. | 0. | 96. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 13.7 |
| * 15 | 1 | 1300. | 0. | 0. 565. | 0. | 0. | 0. | 565. | 1650. | 0. | 0. | .34 | 65. | 8.7 | A | 20.0 13.7 |
| * 16 | 1 | 1000. | 30. | 0. 596. | 30. | 0. | 0. | 596. | 1650. | 0. | 0. | .36 | 65. | 9.2 | A | 20.0 13.7 |
| * 17 | 1 | 1100. | 0. | 0. 596. | 0. | 0. | 0. | 596. | 1650. | 0. | 0. | .36 | 65. | 9.2 | A | 20.0 13.7 |
| * 18 | 1 | 1000. | 0. | 20. 596. | 0. | 20. | 0. | 596. | 1650. | 0. | 0. | .36 | 65. | 9.2 | A | 20.0 13.7 |
| * 19 | 1 | 900. | 0. | 0. 575. | 0. | 0. | 0. | 575. | 1650. | 0. | 0. | .35 | 65. | 8.8 | A | 20.0 13.7 |
| * 20 | 1 | 100. | 17. | 0. 592. | 17. | 0. | 0. | 592. | 1650. | 0. | 0. | .36 | 65. | 9.1 | A | 20.0 13.7 |
| * 21 | 1 | 100. | 0. | 0. 592. | 0. | 0. | 0. | 592. | 1650. | 0. | 0. | .36 | 65. | 9.1 | A | 20.0 13.7 |
| * 22 | 1 | 100. | 0. | 79. 592. | 0. | 79. | 0. | 592. | 1650. | 0. | 0. | .36 | 65. | 9.1 | A | 20.0 13.7 |
| * 23 | 1 | 700. | 0. | 0. 513. | 0. | 0. | 0. | 513. | 1650. | 0. | 0. | .31 | 65. | 7.9 | A | 20.0 13.7 |
| * 24 | 1 | 1500. | 0. | 95. 513. | 0. | 95. | 0. | 513. | 1650. | 0. | 0. | .31 | 65. | 7.9 | A | 20.0 13.7 |
| * 25 | 1 | 800. | 0. | 0. 417. | 0. | 0. | 0. | 417. | 1650. | 0. | 0. | .25 | 65. | 6.4 | A | 20.0 13.7 |
| * 26 | 1 | 1000. | 167. | 0. 584. | 167. | 0. | 0. | 584. | 1650. | 0. | 0. | .35 | 65. | 9.0 | A | 20.0 13.7 |
| * 27 | 1 | 800. | 0. | 0. 584. | 0. | 0. | 0. | 584. | 1650. | 0. | 0. | .35 | 65. | 9.0 | A | 20.0 13.7 |
| * 28 | 1 | 1000. | 0. | 18. 584. | 0. | 18. | 0. | 584. | 1650. | 0. | 0. | .35 | 65. | 9.0 | A | 20.0 13.7 |
| * 29 | 1 | 8000. | 0. | 567. 567. | 0. | 567. 567. | 0. | 1650. | 1650. | 0. | 0. | .34 | 65. | 8.7 | A | 20.0 13.7 |
| * 30 | | | | | | | | | | | | | | | | |
| * 31 | | | | | | | | | | | | | | | | |
| * 32 | | | | | | | | | | | | | | | | |
| * TOTAL | 140349. | = | 26.6 | MILES | | | | MAX(V/C) = 0.40 | LOWEST LOS = A | AVG = 65. | 10.0 | | 20.0 | 13.7 | | |

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|-----------------------------|--------------------|-----------------|-------------------|------------------|
| FREEWAY TRAVEL TIME = | 265. VEH-HRS | 530. PASS-HRS | 859. VEH-HRS | 1719. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 265. VEH-HRS | 530. PASS-HRS | 859. VEH-HRS | 1719. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 17224. VEH-MI. | 34447. PASS-MI. | 55859. VEH-MI. | 111718. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 65. MPH. | | 65. MPH. | |
| AVERAGE DENSITY = | 10. VPMPL | | 11. VPMPL | |
| TOTAL FUEL = | 861. GALLONS | | 2793. GALLONS | |
| TOTAL EMISSIONS = | 237. KILOGRAMS | | 768. KILOGRAMS | |

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***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | 30 | 0.00 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A.D.MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP EEE
FFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP PPP EEEEEEEEE

FREQ12PEB

- 1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
- 2. THERE ARE 1.0 TIME SLICES PER HOUR.
- 3. WEAVING ANALYSIS IS NOT ENGAGED.
- 4. NO ALTERNATE ROUTE IS PROVIDED.
- 5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
- 6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
- 7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
- 8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
- 9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
- 10. THE CAPACITY BUFFER IS 0.00 (V/C).

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** FREeway AND ARTERIAL DESIGN FEATURES **  
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** SUB NO. SSEC SSEC DESIGN ORG TRK SSEC PCT PCT DES SPECIAL FF.SPD. CAP. ART GRADE SUBSECTION LOCATION **  
** SEC LNS CAP LENGTH SPEED DES FAC GRAD TRK TRUCKS RAMP ALT. RTE ALT. RTE TYPE ALT. RTE **  
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| SUB NO. | SEC | LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT TRUCKS | DES RAMP | SPECIAL | FF.SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION | LOCATION | |
|---------|------|-----------|-----------|-------------|--------------|---------|---------|-----------|---------|------------|----------|---------|------------------|-----------------------------|-------------------------|----------------|------------|----------|----|
| ** 1 | ** 4 | ** 10000. | ** 500. | ** 65 | ** OD | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Seeding | ** | ** | ** | |
| ** 2 | ** 3 | ** 7000. | ** 99999. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Queue Capture | ** | ** | ** | ** | |
| ** 3 | ** 3 | ** 7000. | ** 2830. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** SR-87 to DLC loop-on | ** | ** | ** | ** | |
| ** 4 | ** 3 | ** 7000. | ** 930. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** DLC loop on to dia-on | ** | ** | ** | ** | |
| ** 5 | ** 3 | ** 7000. | ** 1490. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** DLC dia-on to Tomas off | ** | ** | ** | ** | |
| ** 6 | ** 3 | ** 7000. | ** 3020. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Tomas off to on | ** | ** | ** | ** | |
| ** 7 | ** 3 | ** 7000. | ** 1030. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Tomas on to bowers off | ** | ** | ** | ** | |
| ** 8 | ** 3 | ** 7000. | ** 1440. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Bowers off to loop-on | ** | ** | ** | ** | |
| ** 9 | ** 3 | ** 7000. | ** 1430. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Bowers loop-on to dia | ** | ** | ** | ** | |
| ** 10 | ** 3 | ** 7000. | ** 3480. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Bowers dia-on to law-off | ** | ** | ** | ** | |
| ** 11 | ** 3 | ** 7000. | ** 1020. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Law off to loop-on | ** | ** | ** | ** | |
| ** 12 | ** 3 | ** 7000. | ** 980. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Lawr Loop to diag | ** | ** | ** | ** | |
| ** 13 | ** 3 | ** 7000. | ** 1800. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Lawrence On-ramp | ** | ** | ** | ** | |
| ** 14 | ** 3 | ** 7000. | ** 1500. | ** 65 | ** D | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Fair Oaks Off-Ramp | ** | ** | ** | ** |
| ** 15 | ** 3 | ** 6000. | ** 1300. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Fair Oaks / Fair Oaks | ** | ** | ** | ** | |
| ** 16 | ** 3 | ** 6000. | ** 1000. | ** 65 | ** 0 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Fair Oaks On-Ramp | ** | ** | ** | ** |
| ** 17 | ** 3 | ** 6000. | ** 1100. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Fair Oaks / Mathilda | ** | ** | ** | ** | |
| ** 18 | ** 4 | ** 7020. | ** 1000. | ** 65 | ** D | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Mathilda NB Off-Ramp | ** | ** | ** | ** |
| ** 19 | ** 3 | ** 6000. | ** 900. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Mathilda / Mathilda | ** | ** | ** | ** | ** |
| ** 20 | ** 3 | ** 6000. | ** 100. | ** 65 | ** 0 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Mathilda NB On-Ramp | ** | ** | ** | ** |

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FREWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SEC | LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT TRUCKS | DES RAMP | SPECIAL | FF. SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION | LOCATION | |
|---------|------|----------|----------|-------------|--------------|---------|---------|-----------|---------|------------|----------|---------|-------------------|-------------------------|-----------------------|----------------|------------|----------|-------|
| ** 21 | ** 3 | ** 6000. | ** 100. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Mathilda / Mathilda | ** ** | ** ** | ** ** | ** ** | |
| ** 22 | ** 3 | ** 6000. | ** 100. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Mathilda SB Off-ramp | ** ** | ** ** | ** ** | ** ** | |
| ** 23 | ** 3 | ** 6000. | ** 700. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Mathilda / SR-237 | ** ** | ** ** | ** ** | ** ** | |
| ** 24 | ** 3 | ** 6000. | ** 1500. | ** 65 | ** D | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** SR-237 WB Off-Ramp | ** ** | ** ** | ** ** | |
| ** 25 | ** 3 | ** 6000. | ** 800. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** SR-237 / SR-237 | ** ** | ** ** | ** ** | ** ** | |
| ** 26 | ** 3 | ** 6000. | ** 1000. | ** 65 | ** 0 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** SR-237 WB On-Ramp | ** ** | ** ** | ** ** | |
| ** 27 | ** 3 | ** 6000. | ** 800. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** SR-237 / Ellis | ** ** | ** ** | ** ** | ** ** | |
| ** 28 | ** 3 | ** 6000. | ** 1000. | ** 65 | ** D | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Ellis Off-ramp | ** ** | ** ** | ** ** | ** ** |
| ** 29 | ** 3 | ** 6000. | ** 8000. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** HOV Dummy | ** ** | ** ** | ** ** | ** ** | |
| ** 30 | ** 4 | ** 8000. | ** 100. | ** 65 | ** 0 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** HOV Dummy | ** ** | ** ** | ** ** | ** ** |
| ** 31 | ** 4 | ** 5500. | ** 1000. | ** 65 | ** 0 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Dummy Bottleneck | ** ** | ** ** | ** ** | ** ** |
| ** 32 | ** 4 | ** 8000. | ** 2640. | ** 65 | ** D | ** 1.00 | ** 0.0 | ** 0 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** End of Network | ** ** | ** ** | ** ** | ** ** |

***** INPUT HAS BEEN COMPLETED *****

MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 4 IN TIME SLICE 2
--- THE MAXIMUM METERING RATE WILL PREVAIL.

FREWAY TRAVEL TIME (MINUTES)

| ORIGINS DOWN | 1 | 2 | 3 | 4 | 5 | 6 |
|--------------|------|-------|-------|-------|-------|-------|
| * 1 * | 0.09 | 21.28 | 22.06 | 22.65 | 23.29 | 28.17 |
| * 2 * | 0.00 | 0.00 | 0.55 | 1.14 | 1.79 | 6.66 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.44 | 1.08 | 5.95 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.50 | 5.38 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.81 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.64 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB NO. | SEC | LNS | SSEC | 0-D DATA DEMANDS | ADJUSTED VOLUMES | SSEC CAP. | WEAVE EFF | CONGEST LENGTH | STORAGE RATE | V/C RATIO | SPEED MPH | DENSITY VP/MP | LOS LEVEL | FUEL MPG | EMISS GS/VM |
|---------|-----|-----|------|------------------|------------------|-----------|-----------|----------------|--------------|-----------|-----------|---------------|-----------|----------|-------------|
|---------|-----|-----|------|------------------|------------------|-----------|-----------|----------------|--------------|-----------|-----------|---------------|-----------|----------|-------------|

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| | | | | | | | | | | | | | | | | | | | | |
|---|----|---|--------|-------|------------|-------|------------|-------|-----------|---------|------|------|-----|-------|-----|------|------|------|------|---|
| * | 1 | 4 | 500. | 5520. | 718. | 5520. | 5520. | 718. | 5520. | 10000. | 0. | 0. | 0. | .55 | 65. | 21.2 | C | 19.2 | 14.0 | * |
| * | 2 | 3 | 99999. | 0. | 0.4802. | 0. | 0.4802. | 0. | 0.4802. | 7000. | 0. | 0. | 0. | .69 | 65. | 24.7 | C | 19.2 | 13.9 | * |
| * | 3 | 3 | 2830. | 0. | 0.4802. | 0. | 0.4802. | 0. | 0.4802. | 7000. | 0. | 0. | 0. | .69 | 65. | 24.7 | C | 19.2 | 13.9 | * |
| * | 4 | 3 | 930. | 0. | 0.4802. | 0. | 0.4802. | 0. | 0.4802. | 7000. | 0. | 0. | 0. | .69 | 65. | 24.7 | C | 19.2 | 13.9 | * |
| * | 5 | 3 | 1490. | 0. | 0.4802. | 0. | 0.4802. | 0. | 0.4802. | 7000. | 0. | 0. | 0. | .69 | 65. | 24.7 | C | 19.2 | 13.9 | * |
| * | 6 | 3 | 3020. | 0. | 0.4802. | 0. | 0.4802. | 0. | 0.4802. | 7000. | 0. | 0. | 0. | .69 | 65. | 24.7 | C | 19.2 | 13.9 | * |
| * | 7 | 3 | 1030. | 0. | 0.4802. | 0. | 0.4802. | 0. | 0.4802. | 7000. | 0. | 0. | 0. | .69 | 65. | 24.7 | C | 19.2 | 13.9 | * |
| * | 8 | 3 | 1440. | 0. | 0.4802. | 0. | 0.4802. | 0. | 0.4802. | 7000. | 0. | 0. | 0. | .69 | 65. | 24.7 | C | 19.2 | 13.9 | * |
| * | 9 | 3 | 1430. | 0. | 0.4802. | 0. | 0.4802. | 0. | 0.4802. | 7000. | 0. | 0. | 0. | .69 | 65. | 24.7 | C | 19.2 | 13.9 | * |
| * | 10 | 3 | 3480. | 0. | 0.4802. | 0. | 0.4802. | 0. | 0.4802. | 7000. | 0. | 0. | 0. | .69 | 65. | 24.7 | C | 19.2 | 13.9 | * |
| * | 11 | 3 | 1020. | 0. | 0.4802. | 0. | 0.4802. | 0. | 0.4802. | 7000. | 0. | 0. | 0. | .69 | 65. | 24.7 | C | 19.2 | 13.9 | * |
| * | 12 | 3 | 980. | 0. | 0.4802. | 0. | 0.4802. | 0. | 0.4802. | 7000. | 0. | 0. | 0. | .69 | 65. | 24.7 | C | 19.2 | 13.9 | * |
| * | 13 | 3 | 1800. | 0. | 0.4802. | 0. | 0.4802. | 0. | 0.4802. | 7000. | 0. | 0. | 0. | .69 | 65. | 24.7 | C | 19.2 | 13.9 | * |
| * | 14 | 3 | 1500. | 0. | 539.4802. | 0. | 539.4802. | 0. | 539.4802. | 6919. | 0. | 0. | 0. | .69 | 65. | 24.7 | C | 19.3 | 13.9 | * |
| * | 15 | 3 | 1300. | 0. | 0.4263. | 0. | 0.4263. | 0. | 0.4263. | 6000. | 0. | 0. | 0. | .71 | 65. | 21.9 | C | 19.2 | 14.0 | * |
| * | 16 | 3 | 1000. | 337. | 0.4600. | 240. | 0.4600. | 0. | 0.4503. | 5967. | 0. | 0. | 0. | .75 | 64. | 23.4 | C | 19.6 | 13.7 | * |
| * | 17 | 3 | 1100. | 0. | 0.4600. | 0. | 0.4600. | 0. | 0.4503. | 6000. | 0. | 0. | 0. | .75 | 64. | 23.4 | C | 19.5 | 13.7 | * |
| * | 18 | 4 | 1000. | 0. | 686.4600. | 0. | 670.4503. | 6926. | 0. | 0. | 0. | 0. | 0. | .65 | 65. | 17.3 | B | 19.2 | 14.0 | * |
| * | 19 | 3 | 900. | 0. | 0.3914. | 0. | 0.3833. | 6000. | 0. | 0. | 0. | 0. | 0. | .64 | 65. | 19.7 | C | 19.2 | 14.0 | * |
| * | 20 | 3 | 100. | 304. | 0.4218. | 240. | 0.4073. | 5964. | 0. | 0. | 0. | 0. | 0. | .68 | 65. | 20.9 | C | 19.2 | 14.0 | * |
| * | 21 | 3 | 100. | 0. | 0.4218. | 0. | 0.4073. | 6000. | 0. | 0. | 0. | 0. | 0. | .68 | 65. | 20.9 | C | 19.2 | 14.0 | * |
| * | 22 | 3 | 100. | 0. | 0.4218. | 0. | 0.4073. | 6000. | 0. | 0. | 0. | 0. | 0. | .68 | 65. | 20.9 | C | 19.2 | 14.0 | * |
| * | 23 | 3 | 700. | 0. | 0.4218. | 0. | 0.4073. | 6000. | 0. | 0. | 0. | 0. | 0. | .68 | 65. | 20.9 | C | 19.2 | 14.0 | * |
| * | 24 | 3 | 1500. | 0. | 630.4218. | 0. | 606.4073. | 5920. | 0. | 0. | 0. | 0. | 0. | .69 | 65. | 20.9 | C | 19.2 | 14.0 | * |
| * | 25 | 3 | 800. | 0. | 0.3588. | 0. | 0.3467. | 6000. | 0. | 0. | 0. | 0. | 0. | .58 | 65. | 17.8 | B | 19.2 | 14.0 | * |
| * | 26 | 3 | 1000. | 1587. | 0.5175. | 1277. | 0.4744. | 5777. | 0. | 0. | 0. | 0. | 0. | .82 | 63. | 25.3 | C | 20.3 | 13.2 | * |
| * | 27 | 3 | 800. | 0. | 0.5175. | 0. | 0.4744. | 6000. | 0. | 0. | 0. | 0. | 0. | .79 | 63. | 25.0 | C | 19.9 | 13.5 | * |
| * | 28 | 3 | 1000. | 0. | 296.5175. | 0. | 269.4744. | 5975. | 0. | 0. | 0. | 0. | 0. | .79 | 63. | 25.0 | C | 19.9 | 13.4 | * |
| * | 29 | 3 | 8000. | 0. | 0.4879. | 0. | 0.4071. | 6000. | 0. | * 4886. | 403. | .68 | 22. | 60.7 | F | 16.1 | 16.8 | * | | |
| * | 30 | 4 | 100. | 729. | 0.5608. | 729. | 0.4800. | 8000. | 0. | ** 100. | 403. | .60 | 7. | 181.8 | F | 9.5 | 26.7 | * | | |
| * | 31 | 4 | 1000. | 800. | 0.6408. | 700. | 0.5500. | 5500. | 0. | 0. | 0. | 1.00 | 65. | 21.2 | E | 19.2 | 14.0 | * | | |
| * | 32 | 4 | 2640. | 0. | 6408.6408. | 0. | 5500.5500. | 8000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 20.0 | 13.7 | * | | |

***** TOTAL 144589. = 27.4 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 59. 26.5 19.1 14.1 *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 2/29/2016 16: 0 PAGE 6
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 1 OF 3

| | CURRENT TIME SLICE | | CUMULATIVE VALUES |
|----------------------------|--------------------|------------------|----------------------------------|
| FREWAY TRAVEL TIME = | 2216. VEH-HRS | 2227. PASS-HRS | 2216. VEH-HRS 2227. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 286. VEH-HRS | 292. PASS-HRS | 286. VEH-HRS 292. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 2502. VEH-HRS | 2519. PASS-HRS | 2502. VEH-HRS 2519. PASS-HRS |
| TOTAL TRAV DISTANCE = | 130319. VEH-MI. | 130922. PASS-MI. | 130319. VEH-MI. 130922. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 52. MPH. | | 59. MPH. |
| AVERAGE DENSITY = | 26. VPMP/L | | 26. VPMP/L |
| TOTAL FUEL = | 6937. GALLONS | | 6937. GALLONS |
| TOTAL EMISSIONS = | 1877. KI LOGRAMS | | 1877. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|--------|------------|-------|
| 1 | 0.00 | 2 | 3.20 | 3 | 0.09 | 4 | 0.03 | 5 | 0.05 |
| 6 | 0.10 | 7 | 0.03 | 8 | 0.05 | 9 | 0.05 | 10 | 0.11 |
| 11 | 0.03 | 12 | 0.03 | 13 | 0.06 | 14 | 0.06 | 15 | 0.00 |
| 16 | 0.18 | 17 | 0.19 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.55 | 27 | 0.28 | 28 | 0.37 | 29 | 193.44 | 30 | 12.39 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 211.3 VEH-HRS ***** AVERAGE DELAY = 3.07 MIN/VEH *****

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 TIME SLICE 1 OF 3

***** RAMP DELAYS *****

| | QUEUE LENGTH | DELAY | AVERAGE | GAS | HC | CO | NOX | TOTAL |
|-----------|--------------|---------|----------------|------|-------|------|-------|-----------|
| | VEHICLES | VEH-HRS | METERING DELAY | GALS | KGMS | KGMS | KGMS | EMISSIONS |
| | | | MINUTES | | | | | KGMS |
| ON-RAMP 2 | RAMP | 97. | 48.50 | 8.64 | 17.32 | 1.07 | 5.62 | 6.99 |
| | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 97. | 48.50 | 8.64 | 17.32 | 1.07 | 5.62 | 6.99 |
| ON-RAMP 3 | RAMP | 64. | 32.00 | 6.32 | 11.43 | 0.71 | 3.71 | 4.61 |
| | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 64. | 32.00 | 6.32 | 11.43 | 0.71 | 3.71 | 4.61 |
| ON-RAMP 4 | RAMP | 310. | 155.00 | 5.14 | 55.35 | 3.43 | 17.96 | 22.34 |
| | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 310. | 155.00 | 5.14 | 55.35 | 3.43 | 17.96 | 22.34 |
| ON-RAMP 6 | RAMP | 100. | 50.00 | 4.31 | 17.85 | 1.11 | 5.79 | 7.21 |
| | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 50.00 | 4.31 | 17.85 | 1.11 | 5.79 | 7.21 |

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 ** FREeway TRAVEL TIME (MINUTES) **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | |
|-----------|--|-----------------------|-------|-------|-------|-------|-------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 |
| * 1 * | | 0.09 | 21.38 | 22.16 | 23.14 | 26.39 | 42.77 |
| * 2 * | | 0.00 | 0.00 | 0.55 | 1.53 | 4.78 | 21.16 |
| * 3 * | | 0.00 | 0.00 | 0.00 | 0.83 | 4.07 | 20.46 |
| * 4 * | | 0.00 | 0.00 | 0.00 | 0.00 | 2.46 | 18.84 |
| * 5 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.89 |
| * 6 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.64 |

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMI SS |
|-----------|----------|------------|-------------|------------|-------------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|----------|
| * SEC LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VP/PL | * LEVEL | * MPG | * GS/VM |
| * 1 4 | 500. | 5819. | 756. 5819. | 5819. | 756. 5819. | 10000. | 0. | 0. | 0. | .58 | 65. | 22.4 | C | 19.2 | 14.0 |
| * 2 3 | 99999. | 0. | 0. 5063. | 0. | 0. 5063. | 7000. | 0. | 0. | 0. | .72 | 65. | 26.1 | D | 19.4 | 13.8 |
| * 3 3 | 2830. | 0. | 0. 5063. | 0. | 0. 5063. | 7000. | 0. | 0. | 0. | .72 | 65. | 26.1 | D | 19.4 | 13.8 |
| * 4 3 | 930. | 0. | 0. 5063. | 0. | 0. 5063. | 7000. | 0. | 0. | 0. | .72 | 65. | 26.1 | D | 19.4 | 13.8 |
| * 5 3 | 1490. | 0. | 0. 5063. | 0. | 0. 5063. | 7000. | 0. | 0. | 0. | .72 | 65. | 26.1 | D | 19.4 | 13.8 |
| * 6 3 | 3020. | 0. | 0. 5063. | 0. | 0. 5063. | 7000. | 0. | 0. | 0. | .72 | 65. | 26.1 | D | 19.4 | 13.8 |
| * 7 3 | 1030. | 0. | 0. 5063. | 0. | 0. 5063. | 7000. | 0. | 0. | 0. | .72 | 65. | 26.1 | D | 19.4 | 13.8 |
| * 8 3 | 1440. | 0. | 0. 5063. | 0. | 0. 5063. | 7000. | 0. | 0. | 0. | .72 | 65. | 26.1 | D | 19.4 | 13.8 |
| * 9 3 | 1430. | 0. | 0. 5063. | 0. | 0. 5063. | 7000. | 0. | 0. | 0. | .72 | 65. | 26.1 | D | 19.4 | 13.8 |
| * 10 3 | 3480. | 0. | 0. 5063. | 0. | 0. 5063. | 7000. | 0. | 0. | 0. | .72 | 65. | 26.1 | D | 19.4 | 13.8 |
| * 11 3 | 1020. | 0. | 0. 5063. | 0. | 0. 5063. | 7000. | 0. | 0. | 0. | .72 | 65. | 26.1 | D | 19.4 | 13.8 |
| * 12 3 | 980. | 0. | 0. 5063. | 0. | 0. 5063. | 7000. | 0. | 0. | 0. | .72 | 65. | 26.1 | D | 19.4 | 13.8 |
| * 13 3 | 1800. | 0. | 0. 5063. | 0. | 0. 5063. | 7000. | 0. | 0. | 0. | .72 | 65. | 26.1 | D | 19.4 | 13.8 |
| * 14 3 | 1500. | 0. | 818. 5063. | 0. | 818. 5063. | 6878. | 0. | 0. | 0. | .74 | 64. | 26.2 | D | 19.4 | 13.8 |
| * 15 3 | 1300. | 0. | 0. 4245. | 0. | 0. 4245. | 6000. | 0. | 0. | 0. | .71 | 65. | 21.8 | C | 19.2 | 14.0 |
| * 16 3 | 1000. | 388. | 0. 4633. | 385. | 0. 4630. | 5967. | 0. | 0. | 0. | .78 | 64. | 24.2 | C | 19.8 | 13.6 |
| * 17 3 | 1100. | 0. | 0. 4633. | 0. | 0. 4630. | 6000. | 0. | 0. | 0. | .77 | 64. | 24.2 | C | 19.7 | 13.6 |
| * 18 4 | 1000. | 0. | 898. 4633. | 0. | 894. 4630. | 6898. | 0. | 0. | 0. | .67 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 19 3 | 900. | 0. | 0. 3735. | 0. | 0. 3736. | 6000. | 0. | 0. | 0. | .62 | 65. | 19.2 | C | 19.2 | 14.0 |
| * 20 3 | 100. | 277. | 0. 4012. | 241. | 0. 3977. | 5970. | 0. | 0. | 0. | .67 | 65. | 20.4 | C | 19.2 | 14.0 |
| * 21 3 | 100. | 0. | 0. 4012. | 0. | 0. 3977. | 6000. | 0. | 0. | 0. | .66 | 65. | 20.4 | C | 19.2 | 14.0 |
| * 22 3 | 100. | 0. | 0. 4012. | 0. | 0. 3977. | 6000. | 0. | 0. | 0. | .66 | 65. | 20.4 | C | 19.2 | 14.0 |
| * 23 3 | 700. | 0. | 0. 4012. | 0. | 0. 3096. | 6000. | 0. | * 507. | 881. | .52 | 54. | 19.2 | F | 18.8 | 14.2 |
| * 24 3 | 1500. | 0. | 862. 4012. | 0. | 846. 3096. | 5892. | 0. | ** 1500. | 881. | .53 | 27. | 37.8 | F | 16.7 | 15.7 |
| * 25 3 | 800. | 0. | 0. 3150. | 0. | 0. 2250. | 6000. | 0. | ** 800. | 881. | .37 | 12. | 64.8 | F | 14.8 | 17.4 |
| * 26 3 | 1000. | 1575. | 0. 4725. | 1281. | 0. 3531. | 5781. | 0. | ** 1000. | 881. | .61 | 16. | 73.1 | F | 14.4 | 18.2 |
| * 27 3 | 800. | 0. | 0. 4725. | 0. | 0. 3531. | 6000. | 0. | ** 800. | 881. | .59 | 13. | 92.3 | F | 13.1 | 19.6 |
| * 28 3 | 1000. | 0. | 315. 4725. | 0. | 290. 3531. | 5975. | 0. | ** 1000. | 881. | .59 | 11. | 107.8 | F | 12.3 | 20.9 |
| * 29 3 | 8000. | 0. | 0. 4410. | 0. | 0. 3241. | 6000. | 0. | ** 8000. | 881. | .54 | 6. | 184.2 | F | 9.1 | 27.0 |
| * 30 4 | 100. | 659. | 0. 5069. | 659. | 0. 3900. | 8000. | 0. | ** 100. | 881. | .49 | 5. | 214.0 | F | 8.4 | 28.7 |
| * 31 4 | 1000. | 1600. | 0. 6669. | 1600. | 0. 5500. | 5500. | 0. | 0. | 0. | 1.00 | 65. | 21.2 | E | 19.2 | 14.0 |
| * 32 4 | 2640. | 0. | 6669. 6669. | 0. | 5500. 5500. | 8000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 20.0 | 13.7 |

* TOTAL 144589. = 27.4 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 44. 36.3 18.4 14.5 *

| | CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | |
|----------------------------|--------------------|---------|---------|----------|-------------------|---------|---------|----------|
| FREWAY TRAVEL TIME = | 3055. | VEH-HRS | 3067. | PASS-HRS | 5271. | VEH-HRS | 5294. | PASS-HRS |
| FREWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 738. | VEH-HRS | 751. | PASS-HRS | 1023. | VEH-HRS | 1043. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 3792. | VEH-HRS | 3817. | PASS-HRS | 6294. | VEH-HRS | 6336. | PASS-HRS |
| TOTAL TRAV DISTANCE = | 134187. | VEH-MI. | 134790. | PASS-MI. | 264506. | VEH-MI. | 265712. | PASS-MI. |

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 AVERAGE SYSTEM SPEED = 35. MPH. 50. MPH.
 AVERAGE DENSITY = 36. VPMP/L 31. VPMP/L
 TOTAL FUEL = 7549. GALLONS 14487. GALLONS
 TOTAL EMISSIONS = 2046. KILOGRAMS 3923. KILOGRAMS

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|--------|------------|-------|
| 1 | 0.00 | 2 | 10.42 | 3 | 0.29 | 4 | 0.10 | 5 | 0.16 |
| 6 | 0.31 | 7 | 0.11 | 8 | 0.15 | 9 | 0.15 | 10 | 0.36 |
| 11 | 0.11 | 12 | 0.10 | 13 | 0.19 | 14 | 0.21 | 15 | 0.00 |
| 16 | 0.27 | 17 | 0.28 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 1.67 | 24 | 23.26 | 25 | 30.94 |
| 26 | 35.92 | 27 | 38.01 | 28 | 56.19 | 29 | 776.13 | 30 | 15.07 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 990.4 VEH-HRS ***** AVERAGE DELAY = 18.28 MIN/VEH *****

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 TIME SLICE 2 OF 3

***** RAMP DELAYS *****

| | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MI MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-----------|-----------------------|---------------|-----------------------------------|----------|---------|---------|----------|----------------------|
| ON-RAMP 2 | RAMP 100. | 98.50 | 12.19 | 35.17 | 2.18 | 11.41 | 0.61 | 14.20 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 100. | 98.50 | 12.19 | 35.17 | 2.18 | 11.41 | 0.61 | 14.20 |
| ON-RAMP 3 | RAMP 100. | 82.00 | 14.43 | 29.28 | 1.82 | 9.50 | 0.50 | 11.82 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 100. | 82.00 | 14.43 | 29.28 | 1.82 | 9.50 | 0.50 | 11.82 |
| ON-RAMP 4 | RAMP 604. | 457.00 | 13.03 | 163.19 | 10.12 | 52.94 | 2.81 | 65.87 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 604. | 457.00 | 13.03 | 163.19 | 10.12 | 52.94 | 2.81 | 65.87 |
| ON-RAMP 6 | RAMP 100. | 100.00 | 4.02 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 100. | 100.00 | 4.02 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 2/29/2016 16: 0 PAGE 12
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 3 OF 3

 ** FREEWAY TRAVEL TIME (MINUTES) **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN 1 2 3 4 5 6 *

| | | | | | | |
|-------|------|-------|-------|-------|-------|-------|
| * 1 * | 0.09 | 21.23 | 22.00 | 23.97 | 28.99 | 40.21 |
| * 2 * | 0.00 | 0.00 | 0.54 | 2.50 | 7.53 | 18.75 |
| * 3 * | 0.00 | 0.00 | 0.00 | 1.81 | 6.83 | 18.05 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 3.17 | 14.40 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.81 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.64 |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 3 OF 3

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | |
|-----------|--------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|---|------|------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * ORG | * DES | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP/L | * LEVEL | * MPG | * GS/VM | | | |
| * 1 | 4 | 500. | 5090. | 662. | 5090. | 5090. | 662. | 5090. | 10000. | 0. | 0. | 0. | .51 | 65. | 19.6 | C | 19.2 | 14.0 |
| * 2 | 3 | 99999. | 0. | 0. | 4428. | 0. | 0. | 4428. | 7000. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 |
| * 3 | 3 | 2830. | 0. | 0. | 4428. | 0. | 0. | 4428. | 7000. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 |

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| | | | | | | | | | | | | | | | | | | | | |
|------|---|-------|-------|-------|-------|-------|-------|-------|-------|----|----|-------|-------|-----|------|-------|------|------|------|---|
| * 4 | 3 | 930. | 0. | 0. | 4428. | 0. | 0. | 4428. | 7000. | 0. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 | * |
| * 5 | 3 | 1490. | 0. | 0. | 4428. | 0. | 0. | 4428. | 7000. | 0. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 | * |
| * 6 | 3 | 3020. | 0. | 0. | 4428. | 0. | 0. | 4428. | 7000. | 0. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 | * |
| * 7 | 3 | 1030. | 0. | 0. | 4428. | 0. | 0. | 4428. | 7000. | 0. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 | * |
| * 8 | 3 | 1440. | 0. | 0. | 4428. | 0. | 0. | 4428. | 7000. | 0. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 | * |
| * 9 | 3 | 1430. | 0. | 0. | 4428. | 0. | 0. | 4428. | 7000. | 0. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 | * |
| * 10 | 3 | 3480. | 0. | 0. | 4428. | 0. | 0. | 4428. | 7000. | 0. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 | * |
| * 11 | 3 | 1020. | 0. | 0. | 4428. | 0. | 0. | 4428. | 7000. | 0. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 | * |
| * 12 | 3 | 980. | 0. | 0. | 4428. | 0. | 0. | 4428. | 7000. | 0. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 | * |
| * 13 | 3 | 1800. | 0. | 0. | 4428. | 0. | 0. | 4428. | 7000. | 0. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 | * |
| * 14 | 3 | 1500. | 0. | 644. | 4428. | 0. | 644. | 4428. | 6904. | 0. | 0. | 0. | 0. | .64 | 65. | 22.7 | C | 19.2 | 14.0 | * |
| * 15 | 3 | 1300. | 0. | 0. | 3784. | 0. | 0. | 3784. | 6000. | 0. | 0. | 0. | 0. | .63 | 65. | 19.4 | C | 19.2 | 14.0 | * |
| * 16 | 3 | 1000. | 339. | 0. | 4123. | 339. | 0. | 4123. | 5970. | 0. | 0. | 0. | 0. | .69 | 65. | 21.1 | C | 19.2 | 14.0 | * |
| * 17 | 3 | 1100. | 0. | 0. | 4123. | 0. | 0. | 4123. | 6000. | 0. | 0. | 0. | 0. | .69 | 65. | 21.1 | C | 19.2 | 14.0 | * |
| * 18 | 4 | 1000. | 0. | 757. | 4123. | 0. | 757. | 4123. | 6917. | 0. | 0. | 0. | 0. | .60 | 65. | 15.9 | B | 19.2 | 14.0 | * |
| * 19 | 3 | 900. | 0. | 0. | 3366. | 0. | 0. | 3366. | 6000. | 0. | 0. | 0. | 0. | .56 | 65. | 17.3 | B | 19.2 | 14.0 | * |
| * 20 | 3 | 100. | 252. | 0. | 3618. | 252. | 0. | 3618. | 5972. | 0. | 0. | 0. | 0. | .61 | 65. | 18.6 | C | 19.2 | 14.0 | * |
| * 21 | 3 | 100. | 0. | 0. | 3618. | 0. | 0. | 3618. | 6000. | 0. | 0. | 0. | 0. | .60 | 65. | 18.6 | C | 19.2 | 14.0 | * |
| * 22 | 3 | 100. | 0. | 0. | 3618. | 0. | 0. | 3618. | 6000. | 0. | 0. | 0. | 0. | .60 | 65. | 18.6 | C | 19.2 | 14.0 | * |
| * 23 | 3 | 700. | 0. | 0. | 3618. | 0. | 0. | 3618. | 6000. | 0. | 0. | 0. | 0. | .60 | 37. | 32.8 | D | 17.6 | 15.2 | * |
| * 24 | 3 | 1500. | 0. | 737. | 3618. | 0. | 737. | 3618. | 5907. | 0. | 0. | 0. | 0. | .61 | 11. | 108.7 | F | 12.4 | 21.4 | * |
| * 25 | 3 | 800. | 0. | 0. | 2881. | 0. | 0. | 3061. | 6000. | 0. | * | 760. | -179. | .51 | 5. | 208.0 | F | 8.4 | 28.7 | * |
| * 26 | 3 | 1000. | 1157. | 0. | 4038. | 1337. | 0. | 4398. | 5837. | 0. | ** | 1000. | -179. | .75 | 10. | 140.5 | F | 13.4 | 22.5 | * |
| * 27 | 3 | 800. | 0. | 0. | 4038. | 0. | 0. | 4398. | 6000. | 0. | ** | 800. | -179. | .73 | 10. | 149.8 | F | 12.8 | 23.1 | * |
| * 28 | 3 | 1000. | 0. | 202. | 4038. | 0. | 221. | 4398. | 5982. | 0. | ** | 1000. | -179. | .74 | 10. | 148.8 | F | 12.9 | 23.0 | * |
| * 29 | 3 | 8000. | 0. | 0. | 3836. | 0. | 0. | 4177. | 6000. | 0. | ** | 8000. | -179. | .70 | 9. | 159.4 | F | 11.5 | 24.3 | * |
| * 30 | 4 | 100. | 573. | 0. | 4409. | 573. | 0. | 4750. | 8000. | 0. | ** | 100. | -179. | .59 | 6. | 186.2 | F | 9.3 | 27.1 | * |
| * 31 | 4 | 1000. | 750. | 0. | 5159. | 750. | 0. | 5500. | 5500. | 0. | 0. | 0. | 1.00 | 65. | 21.2 | E | 19.2 | 14.0 | * | |
| * 32 | 4 | 2640. | 0. | 5159. | 5159. | 0. | 5500. | 5500. | 8000. | 0. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 20.0 | 13.7 | * |

 * TOTAL 144589. = 27.4 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 42. 34.6 18.2 14.8 *

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 2/29/2016 16: 0 PAGE 14
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 3 OF 3

| | CURRENT TIME SLICE | | CUMULATIVE VALUES |
|----------------------------|--------------------|------------------|----------------------------------|
| FREEWAY TRAVEL TIME = | 2864. VEH-HRS | 2876. PASS-HRS | 8135. VEH-HRS 8170. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 814. VEH-HRS | 827. PASS-HRS | 1837. VEH-HRS 1870. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 3678. VEH-HRS | 3703. PASS-HRS | 9972. VEH-HRS 10039. PASS-HRS |
| TOTAL TRAV DISTANCE = | 120593. VEH-MI. | 121188. PASS-MI. | 385099. VEH-MI. 386900. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 33. MPH. | | 47. MPH. |
| AVERAGE DENSITY = | 35. VPMP/L | | 32. VPMP/L |
| TOTAL FUEL = | 6919. GALLONS | | 21405. GALLONS |
| TOTAL EMISSIONS = | 1906. KI LOGRAMS | | 5829. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|--------|------------|-------|
| 1 | 0.00 | 2 | 0.06 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 79.16 | 25 | 87.39 |
| 26 | 67.04 | 27 | 57.85 | 28 | 71.73 | 29 | 627.33 | 30 | 12.72 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 1009.0 VEH-HRS ***** AVERAGE DELAY = 14.98 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 2/29/2016 16: 0 PAGE 15
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 3 OF 3

***** RAMP DELAYS *****

| | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-----------|-----------------------|---------------|--------------------------------|----------|---------|---------|----------|----------------------|
| ON-RAMP 2 | RAMP 100. | 100.00 | 13.67 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 100. | 100.00 | 13.67 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP 3 | RAMP 100. | 100.00 | 17.05 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 100. | 100.00 | 17.05 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP 4 | RAMP 424. | 514.00 | 16.03 | 183.54 | 11.39 | 59.55 | 3.16 | 74.09 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 424. | 514.00 | 16.03 | 183.54 | 11.39 | 59.55 | 3.16 | 74.09 |
| ON-RAMP 6 | RAMP 100. | 100.00 | 7.97 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 100. | 100.00 | 7.97 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |

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FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP LLL
FFFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 1111111 222222222 PPP LLLLLLLLLL
    
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FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 2 AND 29 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65 MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

FREEWAY AND ARTERIAL DESIGN FEATURES

| ** SUB NO. | ** SSEC | ** SSEC | ** DESIGN | ** ORG | ** TRK | ** SSEC | ** PCT | ** PCT | ** DES | ** SPECIAL | ** FF.SPD. | ** CAP. | ** ART | ** GRADE | ** SUBSECTION | ** LOCATION | ** |
|------------|---------|---------|-----------|--------|--------|---------|--------|-----------|---------|-------------|-------------|-------------|---------|-------------|--------------------------|-------------|----|
| ** SEC | ** LNS | ** CAP | ** SPEED | ** DES | ** FAC | ** GRAD | ** TRK | ** TRUCKS | ** RAMP | ** ALT. RTE | ** ALT. RTE | ** ALT. RTE | ** TYPE | ** ALT. RTE | ** | ** | ** |
| ** 1 | | | | | | | | | | | | | | | | | ** |
| ** 2 | 1 | 1650. | 99999. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | | ** |
| ** 3 | 1 | 1650. | 2830. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-87 to DLC loop-on | | ** |
| ** 4 | 1 | 1650. | 930. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | DLC loop on to dia-on | | ** |
| ** 5 | 1 | 1650. | 1490. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | DLC dia-on to Tomas off | | ** |
| ** 6 | 1 | 1650. | 3020. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas off to on | | ** |
| ** 7 | 1 | 1650. | 1030. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas on to bowers off | | ** |
| ** 8 | 1 | 1650. | 1440. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers off to loop-on | | ** |
| ** 9 | 1 | 1650. | 1430. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers loop-on to dia | | ** |
| ** 10 | 1 | 1650. | 3480. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers dia-on to law-off | | ** |
| ** 11 | 1 | 1650. | 1020. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Law off to loop-on | | ** |
| ** 12 | 1 | 1650. | 980. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Lawr Loop to diag | | ** |
| ** 13 | 1 | 1650. | 1800. | 65 | | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Lawrence On-ramp | | ** |
| ** 14 | 1 | 1650. | 1500. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks Off-Ramp | | ** |
| ** 15 | 1 | 1650. | 1300. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Fair Oaks | | ** |
| ** 16 | 1 | 1650. | 1000. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Fair Oaks On-Ramp | | ** |
| ** 17 | 1 | 1650. | 1100. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Mathilda | | ** |
| ** 18 | 1 | 1650. | 1000. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda NB Off-Ramp | | ** |
| ** 19 | 1 | 1650. | 900. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | | ** |

** 20 1 1650. 100. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Mathilda NB On-Ramp **

FREEWAY AND ARTERIAL DESIGN FEATURES

Table with columns: SUB NO., SEC LNS, SSEC CAP, SSEC LENGTH, DESIGN SPEED, ORG DES, TRK FAC, SSEC GRAD, PCT TRK, PCT TRUCKS, SPECIAL RAMP, FF. SPD. ALT. RTE, CAP. ALT. RTE, ART TYPE, GRADE ALT. RTE, SUBSECTION, LOCATION. Rows 21-32.

FREEWAY TRAVEL TIME (MINUTES)

Table with columns: ORIGINS DOWN, DESTINATIONS ACROSS (1-7). Rows 1-7.

TIME SLICE FREEWAY PERFORMANCE TABLE

Table with columns: SUB NO., SEC LNS, SSEC LENGTH, O-D DATA ORG DES, DEMANDS SSEC, ADJUSTED VOLUMES ORG DES SSEC, WEAVE EFF, CONGEST LENGTH, STORAGE RATE, V/C RATIO, SPEED MPH, DENSITY VPMP, LOS LEVEL, FUEL MPG, EMISSIONS GS/VM. Row 1.

US-101_NB_PM_P1_2018_PL.txt

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*****
*
* 1
* 2 1 99999. 718. 0. 718. 718. 0. 718. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 3 1 2830. 0. 0. 718. 0. 0. 718. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 4 1 930. 0. 0. 718. 0. 0. 718. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 5 1 1490. 0. 0. 718. 0. 0. 718. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 6 1 3020. 0. 0. 718. 0. 0. 718. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 7 1 1030. 0. 0. 718. 0. 0. 718. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 8 1 1440. 0. 0. 718. 0. 0. 718. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 9 1 1430. 0. 0. 718. 0. 0. 718. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 10 1 3480. 0. 0. 718. 0. 0. 718. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 11 1 1020. 0. 0. 718. 0. 0. 718. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 12 1 980. 0. 0. 718. 0. 0. 718. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 13 1 1800. 0. 0. 718. 0. 0. 718. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 14 1 1500. 0. 81. 718. 0. 81. 718. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 15 1 1300. 0. 0. 637. 0. 0. 637. 1650. 0. 0. 0. .39 65. 9.8 A 20.0 13.7 *
* 16 1 1000. 33. 0. 670. 33. 0. 670. 1650. 0. 0. 0. .41 65. 10.3 A 20.0 13.7 *
* 17 1 1100. 0. 0. 670. 0. 0. 670. 1650. 0. 0. 0. .41 65. 10.3 A 20.0 13.7 *
* 18 1 1000. 0. 94. 670. 0. 94. 670. 1650. 0. 0. 0. .41 65. 10.3 A 20.0 13.7 *
* 19 1 900. 0. 0. 576. 0. 0. 576. 1650. 0. 0. 0. .35 65. 8.9 A 20.0 13.7 *
* 20 1 100. 36. 0. 611. 36. 0. 611. 1650. 0. 0. 0. .37 65. 9.4 A 20.0 13.7 *
* 21 1 100. 0. 0. 611. 0. 0. 611. 1650. 0. 0. 0. .37 65. 9.4 A 20.0 13.7 *
* 22 1 100. 0. 0. 611. 0. 0. 611. 1650. 0. 0. 0. .37 65. 9.4 A 20.0 13.7 *
* 23 1 700. 0. 0. 611. 0. 0. 611. 1650. 0. 0. 0. .37 65. 9.4 A 20.0 13.7 *
* 24 1 1500. 0. 80. 611. 0. 80. 611. 1650. 0. 0. 0. .37 65. 9.4 A 20.0 13.7 *
* 25 1 800. 0. 0. 532. 0. 0. 532. 1650. 0. 0. 0. .32 65. 8.2 A 20.0 13.7 *
* 26 1 1000. 223. 0. 754. 223. 0. 754. 1650. 0. 0. 0. .46 65. 11.6 B 20.0 13.7 *
* 27 1 800. 0. 0. 754. 0. 0. 754. 1650. 0. 0. 0. .46 65. 11.6 B 20.0 13.7 *
* 28 1 1000. 0. 25. 754. 0. 25. 754. 1650. 0. 0. 0. .46 65. 11.6 B 20.0 13.7 *
* 29 1 8000. 0. 729. 729. 0. 729. 729. 1650. 0. 0. 0. .44 65. 11.2 B 20.0 13.7 *
* 30
* 31
* 32
*****
*
* TOTAL 140349. = 26.6 MILES MAX(V/C) = 0.46 LOWEST LOS = B AVG = 65. 11.0 20.0 13.7 *
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 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 1 OF 3

| | | | |
|-----------------------------|--------------------|-----------------|--------------------------------|
| | CURRENT TIME SLICE | | CUMULATIVE VALUES |
| FREEWAY TRAVEL TIME = | 292. VEH-HRS | 583. PASS-HRS | 292. VEH-HRS 583. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 292. VEH-HRS | 583. PASS-HRS | 292. VEH-HRS 583. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 18961. VEH-MI. | 37922. PASS-MI. | 18961. VEH-MI. 37922. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 65. MPH. | | 65. MPH. |
| AVERAGE DENSITY = | 11. VPMP/L | | 11. VPMP/L |
| TOTAL FUEL = | 948. GALLONS | | 948. GALLONS |
| TOTAL EMISSIONS = | 261. KILOGRAMS | | 261. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | 30 | 0.00 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 16: 0 PAGE 7
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 3

 ** FREEWAY TRAVEL TIME (MINUTES) **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN 1 2 3 4 5 6 7 *

| | | | | | | | |
|-------|------|-------|-------|-------|-------|-------|------|
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 21.14 | 21.91 | 22.51 | 23.14 | 24.54 | 0.00 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.16 | 0.00 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.47 | 0.00 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.89 | 0.00 |

```
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
* *
*****
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TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMI SS |
|-----------|---------|------------|----------------|----------------|----------------|--------|---------|-----------|-----------|-----------------|----------------|-----------|---------|--------|----------|
| * SEC | * LNS | * LENGTH | * ORG DES SSEC | * ORG DES SSEC | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 1 | | | | | | | | | | | | | | | |
| * 2 | 1 | 99999 | 756. 0. 756. | 756. 0. 756. | 0. 756. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 3 | 1 | 2830. | 0. 0. 756. | 0. 0. 756. | 0. 0. 756. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 4 | 1 | 930. | 0. 0. 756. | 0. 0. 756. | 0. 0. 756. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 5 | 1 | 1490. | 0. 0. 756. | 0. 0. 756. | 0. 0. 756. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 6 | 1 | 3020. | 0. 0. 756. | 0. 0. 756. | 0. 0. 756. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 7 | 1 | 1030. | 0. 0. 756. | 0. 0. 756. | 0. 0. 756. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 8 | 1 | 1440. | 0. 0. 756. | 0. 0. 756. | 0. 0. 756. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 9 | 1 | 1430. | 0. 0. 756. | 0. 0. 756. | 0. 0. 756. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 10 | 1 | 3480. | 0. 0. 756. | 0. 0. 756. | 0. 0. 756. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 11 | 1 | 1020. | 0. 0. 756. | 0. 0. 756. | 0. 0. 756. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 12 | 1 | 980. | 0. 0. 756. | 0. 0. 756. | 0. 0. 756. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 13 | 1 | 1800. | 0. 0. 756. | 0. 0. 756. | 0. 0. 756. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 14 | 1 | 1500. | 0. 122. 756. | 0. 122. 756. | 0. 122. 756. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 15 | 1 | 1300. | 0. 0. 634. | 0. 0. 634. | 0. 0. 634. | 1650. | 0. | 0. | 0. | .38 | 65. | 9.8 | A | 20.0 | 13.7 |
| * 16 | 1 | 1000. | 33. 0. 667. | 33. 0. 667. | 0. 0. 667. | 1650. | 0. | 0. | 0. | .40 | 65. | 10.3 | A | 20.0 | 13.7 |
| * 17 | 1 | 1100. | 0. 0. 667. | 0. 0. 667. | 0. 0. 667. | 1650. | 0. | 0. | 0. | .40 | 65. | 10.3 | A | 20.0 | 13.7 |
| * 18 | 1 | 1000. | 0. 122. 667. | 0. 122. 667. | 0. 122. 667. | 1650. | 0. | 0. | 0. | .40 | 65. | 10.3 | A | 20.0 | 13.7 |
| * 19 | 1 | 900. | 0. 0. 545. | 0. 0. 545. | 0. 0. 545. | 1650. | 0. | 0. | 0. | .33 | 65. | 8.4 | A | 20.0 | 13.7 |
| * 20 | 1 | 100. | 30. 0. 574. | 30. 0. 574. | 0. 0. 574. | 1650. | 0. | 0. | 0. | .35 | 65. | 8.8 | A | 20.0 | 13.7 |
| * 21 | 1 | 100. | 0. 0. 574. | 0. 0. 574. | 0. 0. 574. | 1650. | 0. | 0. | 0. | .35 | 65. | 8.8 | A | 20.0 | 13.7 |
| * 22 | 1 | 100. | 0. 0. 574. | 0. 0. 574. | 0. 0. 574. | 1650. | 0. | 0. | 0. | .35 | 65. | 8.8 | A | 20.0 | 13.7 |
| * 23 | 1 | 700. | 0. 0. 574. | 0. 0. 574. | 0. 0. 574. | 1650. | 0. | 0. | 0. | .35 | 65. | 8.8 | A | 20.0 | 13.7 |
| * 24 | 1 | 1500. | 0. 108. 574. | 0. 108. 574. | 0. 108. 574. | 1650. | 0. | 0. | 0. | .35 | 65. | 8.8 | A | 20.0 | 13.7 |
| * 25 | 1 | 800. | 0. 0. 466. | 0. 0. 466. | 0. 0. 466. | 1650. | 0. | 0. | 0. | .28 | 65. | 7.2 | A | 20.0 | 13.7 |
| * 26 | 1 | 1000. | 219. 0. 685. | 219. 0. 685. | 0. 0. 685. | 1650. | 0. | 0. | 0. | .41 | 65. | 10.5 | A | 20.0 | 13.7 |
| * 27 | 1 | 800. | 0. 0. 685. | 0. 0. 685. | 0. 0. 685. | 1650. | 0. | 0. | 0. | .41 | 65. | 10.5 | A | 20.0 | 13.7 |
| * 28 | 1 | 1000. | 0. 25. 685. | 0. 25. 685. | 0. 25. 685. | 1650. | 0. | 0. | 0. | .41 | 65. | 10.5 | A | 20.0 | 13.7 |
| * 29 | 1 | 8000. | 0. 659. 659. | 0. 659. 659. | 0. 659. 659. | 1650. | 0. | 0. | 0. | .40 | 65. | 10.1 | A | 20.0 | 13.7 |
| * 30 | | | | | | | | | | | | | | | |
| * 31 | | | | | | | | | | | | | | | |
| * 32 | | | | | | | | | | | | | | | |
| * TOTAL | 140349. | = | 26.6 MILES | | | | | | | MAX(V/C) = 0.46 | LOWEST LOS = B | AVG = 65. | 11.4 | 20.0 | 13.7 |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 303. VEH-HRS | 605. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 303. VEH-HRS | 605. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 19673. VEH-MI. | 39347. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 65. MPH. | 65. MPH. |
| AVERAGE DENSITY = | 11. VPMP | 11. VPMP |
| TOTAL FUEL = | 984. GALLONS | 1932. GALLONS |
| TOTAL EMISSIONS = | 270. KILOGRAMS | 531. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | 30 | 0.00 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

 **

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 FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS * DOWN | * DESTINATIONS ACROSS | | | | | | |
|---------------------|-----------------------|-------|-------|-------|-------|-------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 21.14 | 21.91 | 22.51 | 23.14 | 24.54 | 0.00 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.16 | 0.00 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.47 | 0.00 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.89 | 0.00 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 3 OF 3

| * TIME SLICE FREEWAY PERFORMANCE TABLE * | | | | | | | | | | | | | | | | | |
|--|---------|----------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|---------|-----------------|----------------|-----------|--------|-------------|---------|
| * SUB | * NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | * GS/VM |
| * SEC | * LNS | * LENGTH | * ORG | * DES | * ORG | * DES | * SSEC | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * SS | * VM |
| * 1 | | | | | | | | | | | | | | | | | |
| * 2 | 1 | 99999 | 662. | 0. | 662. | 662. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 | 13.7 |
| * 3 | 1 | 2830. | 0. | 0. | 662. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 | 13.7 |
| * 4 | 1 | 930. | 0. | 0. | 662. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 | 13.7 |
| * 5 | 1 | 1490. | 0. | 0. | 662. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 | 13.7 |
| * 6 | 1 | 3020. | 0. | 0. | 662. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 | 13.7 |
| * 7 | 1 | 1030. | 0. | 0. | 662. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 | 13.7 |
| * 8 | 1 | 1440. | 0. | 0. | 662. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 | 13.7 |
| * 9 | 1 | 1430. | 0. | 0. | 662. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 | 13.7 |
| * 10 | 1 | 3480. | 0. | 0. | 662. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 | 13.7 |
| * 11 | 1 | 1020. | 0. | 0. | 662. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 | 13.7 |
| * 12 | 1 | 980. | 0. | 0. | 662. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 | 13.7 |
| * 13 | 1 | 1800. | 0. | 0. | 662. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 | 13.7 |
| * 14 | 1 | 1500. | 0. | 96. | 662. | 0. | 96. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 | 13.7 |
| * 15 | 1 | 1300. | 0. | 0. | 565. | 0. | 0. | 565. | 1650. | 0. | 0. | .34 | 65. | 8.7 | A | 20.0 | 13.7 |
| * 16 | 1 | 1000. | 30. | 0. | 595. | 30. | 0. | 595. | 1650. | 0. | 0. | .36 | 65. | 9.2 | A | 20.0 | 13.7 |
| * 17 | 1 | 1100. | 0. | 0. | 595. | 0. | 0. | 595. | 1650. | 0. | 0. | .36 | 65. | 9.2 | A | 20.0 | 13.7 |
| * 18 | 1 | 1000. | 0. | 103. | 595. | 0. | 103. | 595. | 1650. | 0. | 0. | .36 | 65. | 9.2 | A | 20.0 | 13.7 |
| * 19 | 1 | 900. | 0. | 0. | 492. | 0. | 0. | 492. | 1650. | 0. | 0. | .30 | 65. | 7.6 | A | 20.0 | 13.7 |
| * 20 | 1 | 100. | 28. | 0. | 520. | 28. | 0. | 520. | 1650. | 0. | 0. | .32 | 65. | 8.0 | A | 20.0 | 13.7 |
| * 21 | 1 | 100. | 0. | 0. | 520. | 0. | 0. | 520. | 1650. | 0. | 0. | .32 | 65. | 8.0 | A | 20.0 | 13.7 |
| * 22 | 1 | 100. | 0. | 0. | 520. | 0. | 0. | 520. | 1650. | 0. | 0. | .32 | 65. | 8.0 | A | 20.0 | 13.7 |
| * 23 | 1 | 700. | 0. | 0. | 520. | 0. | 0. | 520. | 1650. | 0. | 0. | .32 | 65. | 8.0 | A | 20.0 | 13.7 |
| * 24 | 1 | 1500. | 0. | 93. | 520. | 0. | 93. | 520. | 1650. | 0. | 0. | .32 | 65. | 8.0 | A | 20.0 | 13.7 |
| * 25 | 1 | 800. | 0. | 0. | 427. | 0. | 0. | 427. | 1650. | 0. | 0. | .26 | 65. | 6.6 | A | 20.0 | 13.7 |
| * 26 | 1 | 1000. | 163. | 0. | 591. | 163. | 0. | 591. | 1650. | 0. | 0. | .36 | 65. | 9.1 | A | 20.0 | 13.7 |
| * 27 | 1 | 800. | 0. | 0. | 591. | 0. | 0. | 591. | 1650. | 0. | 0. | .36 | 65. | 9.1 | A | 20.0 | 13.7 |
| * 28 | 1 | 1000. | 0. | 18. | 591. | 0. | 18. | 591. | 1650. | 0. | 0. | .36 | 65. | 9.1 | A | 20.0 | 13.7 |
| * 29 | 1 | 8000. | 0. | 573. | 573. | 0. | 573. | 573. | 1650. | 0. | 0. | .35 | 65. | 8.8 | A | 20.0 | 13.7 |
| * 30 | | | | | | | | | | | | | | | | | |
| * 31 | | | | | | | | | | | | | | | | | |
| * 32 | | | | | | | | | | | | | | | | | |
| * TOTAL | 140349. | = | 26.6 | MILES | | | | | | | | MAX(V/C) = 0.40 | LOWEST LOS = A | AVG = 65. | 10.0 | 20.0 | 13.7 |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 3 OF 3

| | CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | |
|-----------------------------|--------------------|------------|--------|----------|-------------------|------------|---------|----------|
| FREEWAY TRAVEL TIME = | 265. | VEH-HRS | 530. | PASS-HRS | 859. | VEH-HRS | 1719. | PASS-HRS |
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 265. | VEH-HRS | 530. | PASS-HRS | 859. | VEH-HRS | 1719. | PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 17223. | VEH-MI. | 34446. | PASS-MI. | 55858. | VEH-MI. | 111715. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 65. | MPH. | | | 65. | MPH. | | |
| AVERAGE DENSITY = | 10. | VPMP | | | 11. | VPMP | | |
| TOTAL FUEL = | 861. | GALLONS | | | 2793. | GALLONS | | |
| TOTAL EMISSIONS = | 237. | KI LOGRAMS | | | 767. | KI LOGRAMS | | |

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***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | 30 | 0.00 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

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FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP EEE
FFFFFFFF RRRRRRRR EEEEE QQQ QQQ 1111 222 PPPPPPPP EEEEE
FFFFFFFF RRRRRRRR EEEEE QQQ QQQ 1111 222 PPPPPPPP EEEEE
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP EEEEEEEEE

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FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREEWAY AND ARTERIAL DESIGN FEATURES

| ** SUB NO. | ** SEC | ** LNS | ** SSEC CAP | ** SSEC LENGTH | ** DESIGN SPEED | ** ORG DES | ** TRK FAC | ** SSEC GRAD | ** PCT TRK | ** PCT DES TRUCKS | ** SPECIAL RAMP | ** FF.SPD. ALT. RTE | ** CAP. ALT. RTE | ** ART TYPE | ** GRADE ALT. RTE | ** SUBSECTION | ** LOCATION |
|------------|--------|-----------|-------------|----------------|-----------------|------------|------------|--------------|------------|-------------------|-----------------|---------------------|------------------|-----------------------------|-------------------------|---------------|-------------|
| ** 1 | ** 4 | ** 10000. | ** 500. | ** 65 | ** OD | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Seeding | ** | ** |
| ** 2 | ** 3 | ** 7000. | ** 99999. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Queue Capture | ** | ** | |
| ** 3 | ** 3 | ** 7000. | ** 2830. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** SR-87 to DLC loop-on | ** | ** | |
| ** 4 | ** 3 | ** 7000. | ** 930. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** DLC loop on to dia-on | ** | ** | |
| ** 5 | ** 3 | ** 7000. | ** 1490. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** DLC dia-on to Tomas off | ** | ** | |
| ** 6 | ** 3 | ** 7000. | ** 3020. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Tomas off to on | ** | ** | |
| ** 7 | ** 3 | ** 7000. | ** 1030. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Tomas on to bowers off | ** | ** | |
| ** 8 | ** 3 | ** 7000. | ** 1440. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Bowers off to loop-on | ** | ** | |
| ** 9 | ** 3 | ** 7000. | ** 1430. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Bowers loop-on to dia | ** | ** | |
| ** 10 | ** 3 | ** 7000. | ** 3480. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Bowers dia-on to law-off | ** | ** | |
| ** 11 | ** 3 | ** 7000. | ** 1020. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Law off to loop-on | ** | ** | |
| ** 12 | ** 3 | ** 7000. | ** 980. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Lawr Loop to diag | ** | ** | |
| ** 13 | ** 3 | ** 7000. | ** 1800. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Lawrence On-ramp | ** | ** | |
| ** 14 | ** 3 | ** 7000. | ** 1500. | ** 65 | ** D | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Fair Oaks Off-Ramp | ** | ** |
| ** 15 | ** 3 | ** 6000. | ** 1300. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Fair Oaks / Fair Oaks | ** | ** | |
| ** 16 | ** 3 | ** 6000. | ** 1000. | ** 65 | ** 0 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Fair Oaks On-Ramp | ** | ** |
| ** 17 | ** 3 | ** 6000. | ** 1100. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Fair Oaks / Mathilda | ** | ** | |
| ** 18 | ** 4 | ** 7020. | ** 1000. | ** 65 | ** D | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Mathilda NB Off-Ramp | ** | ** |
| ** 19 | ** 3 | ** 6000. | ** 900. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Mathilda / Mathilda | ** | ** | |
| ** 20 | ** 3 | ** 6000. | ** 100. | ** 65 | ** 0 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Mathilda NB On-Ramp | ** | ** |

FREWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SEC | LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT TRUCKS | DES RAMP | SPECIAL | FF. SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION | LOCATION |
|---------|-----|-------|----------|-------------|--------------|---------|---------|-----------|---------|------------|----------|---------|-------------------|---------------|----------------------|----------------|------------|----------|
| ** 21 | 3 | 6000. | 100. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | ** | | |
| ** 22 | 3 | 6000. | 100. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda SB Off-ramp | ** | | |
| ** 23 | 3 | 6000. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / SR-237 | ** | | |
| ** 24 | 3 | 6000. | 1500. | 65 | D | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 WB Off-Ramp | ** | | |
| ** 25 | 3 | 6000. | 800. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 / SR-237 | ** | | |
| ** 26 | 3 | 6000. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 WB On-Ramp | ** | | |
| ** 27 | 3 | 6000. | 800. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 / Ellis | ** | | |
| ** 28 | 3 | 6000. | 1000. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Ellis Off-ramp | ** | | |
| ** 29 | 3 | 6000. | 8000. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | ** | | |
| ** 30 | 4 | 8000. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | ** | | |
| ** 31 | 4 | 5500. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Dummy Bottleneck | ** | | |
| ** 32 | 4 | 8000. | 2640. | 65 | D | 1.00 | 0.0 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End of Network | ** | | |

***** INPUT HAS BEEN COMPLETED *****

MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 4 IN TIME SLICE 2
--- THE MAXIMUM METERING RATE WILL PREVAIL.

FREWAY TRAVEL TIME (MINUTES)

| ORIGINS DOWN | 1 | 2 | 3 | 4 | 5 | 6 |
|--------------|------|-------|-------|-------|-------|-------|
| * 1 * | 0.09 | 21.28 | 22.05 | 22.65 | 23.29 | 28.14 |
| * 2 * | 0.00 | 0.00 | 0.55 | 1.14 | 1.79 | 6.64 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.44 | 1.08 | 5.93 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.50 | 5.36 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.81 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.64 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB NO. | SEC | LNS | SSEC | 0-D DATA DEMANDS | ADJUSTED VOLUMES | SSEC CAP. | WEAVE EFF | CONGEST LENGTH | STORAGE RATE | V/C RATIO | SPEED MPH | DENSITY VP/MP | LOS LEVEL | FUEL MPG | EMISS GS/VM |
|---------|-----|-----|------|------------------|------------------|-----------|-----------|----------------|--------------|-----------|-----------|---------------|-----------|----------|-------------|
|---------|-----|-----|------|------------------|------------------|-----------|-----------|----------------|--------------|-----------|-----------|---------------|-----------|----------|-------------|

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| | | | | | | | | | | | | | | | | | | | | |
|---|----|---|--------|-------|-------|-------|-------|-------|-------|--------|----|----|-------|------|-----|-------|---|------|------|---|
| * | 1 | 4 | 500. | 5518. | 717. | 5518. | 5518. | 717. | 5518. | 10000. | 0. | 0. | 0. | .55 | 65. | 21.2 | C | 19.2 | 14.0 | * |
| * | 2 | 3 | 99999. | 0. | 0. | 4801. | 0. | 0. | 4801. | 7000. | 0. | 0. | 0. | .69 | 65. | 24.7 | C | 19.2 | 13.9 | * |
| * | 3 | 3 | 2830. | 0. | 0. | 4801. | 0. | 0. | 4801. | 7000. | 0. | 0. | 0. | .69 | 65. | 24.7 | C | 19.2 | 13.9 | * |
| * | 4 | 3 | 930. | 0. | 0. | 4801. | 0. | 0. | 4801. | 7000. | 0. | 0. | 0. | .69 | 65. | 24.7 | C | 19.2 | 13.9 | * |
| * | 5 | 3 | 1490. | 0. | 0. | 4801. | 0. | 0. | 4801. | 7000. | 0. | 0. | 0. | .69 | 65. | 24.7 | C | 19.2 | 13.9 | * |
| * | 6 | 3 | 3020. | 0. | 0. | 4801. | 0. | 0. | 4801. | 7000. | 0. | 0. | 0. | .69 | 65. | 24.7 | C | 19.2 | 13.9 | * |
| * | 7 | 3 | 1030. | 0. | 0. | 4801. | 0. | 0. | 4801. | 7000. | 0. | 0. | 0. | .69 | 65. | 24.7 | C | 19.2 | 13.9 | * |
| * | 8 | 3 | 1440. | 0. | 0. | 4801. | 0. | 0. | 4801. | 7000. | 0. | 0. | 0. | .69 | 65. | 24.7 | C | 19.2 | 13.9 | * |
| * | 9 | 3 | 1430. | 0. | 0. | 4801. | 0. | 0. | 4801. | 7000. | 0. | 0. | 0. | .69 | 65. | 24.7 | C | 19.2 | 13.9 | * |
| * | 10 | 3 | 3480. | 0. | 0. | 4801. | 0. | 0. | 4801. | 7000. | 0. | 0. | 0. | .69 | 65. | 24.7 | C | 19.2 | 13.9 | * |
| * | 11 | 3 | 1020. | 0. | 0. | 4801. | 0. | 0. | 4801. | 7000. | 0. | 0. | 0. | .69 | 65. | 24.7 | C | 19.2 | 13.9 | * |
| * | 12 | 3 | 980. | 0. | 0. | 4801. | 0. | 0. | 4801. | 7000. | 0. | 0. | 0. | .69 | 65. | 24.7 | C | 19.2 | 13.9 | * |
| * | 13 | 3 | 1800. | 0. | 0. | 4801. | 0. | 0. | 4801. | 7000. | 0. | 0. | 0. | .69 | 65. | 24.7 | C | 19.2 | 13.9 | * |
| * | 14 | 3 | 1500. | 0. | 539. | 4801. | 0. | 539. | 4801. | 6919. | 0. | 0. | 0. | .69 | 65. | 24.7 | C | 19.3 | 13.9 | * |
| * | 15 | 3 | 1300. | 0. | 0. | 4262. | 0. | 0. | 4262. | 6000. | 0. | 0. | 0. | .71 | 65. | 21.9 | C | 19.2 | 14.0 | * |
| * | 16 | 3 | 1000. | 337. | 0. | 4599. | 240. | 0. | 4502. | 5967. | 0. | 0. | 0. | .75 | 64. | 23.4 | C | 19.6 | 13.7 | * |
| * | 17 | 3 | 1100. | 0. | 0. | 4599. | 0. | 0. | 4502. | 6000. | 0. | 0. | 0. | .75 | 64. | 23.4 | C | 19.5 | 13.7 | * |
| * | 18 | 4 | 1000. | 0. | 686. | 4599. | 0. | 670. | 4502. | 6926. | 0. | 0. | 0. | .65 | 65. | 17.3 | B | 19.2 | 14.0 | * |
| * | 19 | 3 | 900. | 0. | 0. | 3913. | 0. | 0. | 3832. | 6000. | 0. | 0. | 0. | .64 | 65. | 19.7 | C | 19.2 | 14.0 | * |
| * | 20 | 3 | 100. | 295. | 0. | 4208. | 240. | 0. | 4072. | 5965. | 0. | 0. | 0. | .68 | 65. | 20.9 | C | 19.2 | 14.0 | * |
| * | 21 | 3 | 100. | 0. | 0. | 4208. | 0. | 0. | 4072. | 6000. | 0. | 0. | 0. | .68 | 65. | 20.9 | C | 19.2 | 14.0 | * |
| * | 22 | 3 | 100. | 0. | 0. | 4208. | 0. | 0. | 4072. | 6000. | 0. | 0. | 0. | .68 | 65. | 20.9 | C | 19.2 | 14.0 | * |
| * | 23 | 3 | 700. | 0. | 0. | 4208. | 0. | 0. | 4072. | 6000. | 0. | 0. | 0. | .68 | 65. | 20.9 | C | 19.2 | 14.0 | * |
| * | 24 | 3 | 1500. | 0. | 630. | 4208. | 0. | 608. | 4072. | 5920. | 0. | 0. | 0. | .69 | 65. | 20.9 | C | 19.2 | 14.0 | * |
| * | 25 | 3 | 800. | 0. | 0. | 3578. | 0. | 0. | 3464. | 6000. | 0. | 0. | 0. | .58 | 65. | 17.8 | B | 19.2 | 14.0 | * |
| * | 26 | 3 | 1000. | 1587. | 0. | 5165. | 1277. | 0. | 4741. | 5777. | 0. | 0. | 0. | .82 | 63. | 25.3 | C | 20.3 | 13.2 | * |
| * | 27 | 3 | 800. | 0. | 0. | 5165. | 0. | 0. | 4741. | 6000. | 0. | 0. | 0. | .79 | 63. | 24.9 | C | 19.9 | 13.5 | * |
| * | 28 | 3 | 1000. | 0. | 295. | 5165. | 0. | 269. | 4741. | 5975. | 0. | 0. | 0. | .79 | 63. | 25.0 | C | 19.9 | 13.4 | * |
| * | 29 | 3 | 8000. | 0. | 0. | 4870. | 0. | 0. | 4072. | 6000. | 0. | * | 4850. | .68 | 22. | 60.4 | F | 16.1 | 16.8 | * |
| * | 30 | 4 | 100. | 728. | 0. | 5598. | 728. | 0. | 4800. | 8000. | 0. | ** | 100. | .60 | 7. | 181.8 | F | 9.5 | 26.7 | * |
| * | 31 | 4 | 1000. | 800. | 0. | 6398. | 700. | 0. | 5500. | 5500. | 0. | 0. | 0. | 1.00 | 65. | 21.2 | E | 19.2 | 14.0 | * |
| * | 32 | 4 | 2640. | 0. | 6398. | 6398. | 0. | 5500. | 5500. | 8000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 20.0 | 13.7 | * |

 * TOTAL 144589. = 27.4 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 59. 26.4 19.1 14.1 *

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 2214. VEH-HRS | 2225. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 281. VEH-HRS | 288. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 2495. VEH-HRS | 2513. PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 130293. VEH-MI. | 130896. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 52. MPH. | 59. MPH. |
| AVERAGE DENSITY = | 26. VPMP/L | 26. VPMP/L |
| TOTAL FUEL = | 6934. GALLONS | 6934. GALLONS |
| TOTAL EMISSIONS = | 1875. KILOGRAMS | 1875. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|--------|------------|-------|
| 1 | 0.00 | 2 | 3.18 | 3 | 0.09 | 4 | 0.03 | 5 | 0.05 |
| 6 | 0.10 | 7 | 0.03 | 8 | 0.05 | 9 | 0.05 | 10 | 0.11 |
| 11 | 0.03 | 12 | 0.03 | 13 | 0.06 | 14 | 0.06 | 15 | 0.00 |
| 16 | 0.18 | 17 | 0.18 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.55 | 27 | 0.28 | 28 | 0.37 | 29 | 191.91 | 30 | 12.39 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 209.7 VEH-HRS ***** AVERAGE DELAY = 3.05 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-----------|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|
| ON-RAMP 2 | RAMP 97. | 48.50 | 8.64 | 17.32 | 1.07 | 5.62 | 0.30 | 6.99 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 97. | 48.50 | 8.64 | 17.32 | 1.07 | 5.62 | 0.30 | 6.99 |
| ON-RAMP 3 | RAMP 55. | 27.50 | 5.59 | 9.82 | 0.61 | 3.19 | 0.17 | 3.96 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 55. | 27.50 | 5.59 | 9.82 | 0.61 | 3.19 | 0.17 | 3.96 |
| ON-RAMP 4 | RAMP 310. | 155.00 | 5.14 | 55.35 | 3.43 | 17.96 | 0.95 | 22.34 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 310. | 155.00 | 5.14 | 55.35 | 3.43 | 17.96 | 0.95 | 22.34 |
| ON-RAMP 6 | RAMP 100. | 50.00 | 4.31 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 100. | 50.00 | 4.31 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |

 ** FREeway TRAVEL TIME (MINUTES) **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | |
|-----------|------|-----------------------|-------|-------|-------|-------|---|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 |
| * 1 * | 0.09 | 21.38 | 22.16 | 23.12 | 26.34 | 42.69 | |
| * 2 * | 0.00 | 0.00 | 0.55 | 1.51 | 4.73 | 21.08 | |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.81 | 4.02 | 20.37 | |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 2.44 | 18.79 | |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.89 | |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.64 | |

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|-----------|----------|------------|-------------|------------|-------------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|
| * SEC LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMPL | * LEVEL | * MPG | * GS/VM |
| * 1 4 | 500. | 5820. | 756. 5820. | 5820. | 756. 5820. | 10000. | 0. | 0. | 0. | .58 | 65. | 22.4 | C | 19.2 | 14.0 |
| * 2 3 | 99999. | 0. | 0. 5064. | 0. | 0. 5064. | 7000. | 0. | 0. | 0. | .72 | 65. | 26.2 | D | 19.4 | 13.8 |
| * 3 3 | 2830. | 0. | 0. 5064. | 0. | 0. 5064. | 7000. | 0. | 0. | 0. | .72 | 65. | 26.2 | D | 19.4 | 13.8 |
| * 4 3 | 930. | 0. | 0. 5064. | 0. | 0. 5064. | 7000. | 0. | 0. | 0. | .72 | 65. | 26.2 | D | 19.4 | 13.8 |
| * 5 3 | 1490. | 0. | 0. 5064. | 0. | 0. 5064. | 7000. | 0. | 0. | 0. | .72 | 65. | 26.2 | D | 19.4 | 13.8 |
| * 6 3 | 3020. | 0. | 0. 5064. | 0. | 0. 5064. | 7000. | 0. | 0. | 0. | .72 | 65. | 26.2 | D | 19.4 | 13.8 |
| * 7 3 | 1030. | 0. | 0. 5064. | 0. | 0. 5064. | 7000. | 0. | 0. | 0. | .72 | 65. | 26.2 | D | 19.4 | 13.8 |
| * 8 3 | 1440. | 0. | 0. 5064. | 0. | 0. 5064. | 7000. | 0. | 0. | 0. | .72 | 65. | 26.2 | D | 19.4 | 13.8 |
| * 9 3 | 1430. | 0. | 0. 5064. | 0. | 0. 5064. | 7000. | 0. | 0. | 0. | .72 | 65. | 26.2 | D | 19.4 | 13.8 |
| * 10 3 | 3480. | 0. | 0. 5064. | 0. | 0. 5064. | 7000. | 0. | 0. | 0. | .72 | 65. | 26.2 | D | 19.4 | 13.8 |
| * 11 3 | 1020. | 0. | 0. 5064. | 0. | 0. 5064. | 7000. | 0. | 0. | 0. | .72 | 65. | 26.2 | D | 19.4 | 13.8 |
| * 12 3 | 980. | 0. | 0. 5064. | 0. | 0. 5064. | 7000. | 0. | 0. | 0. | .72 | 65. | 26.2 | D | 19.4 | 13.8 |
| * 13 3 | 1800. | 0. | 0. 5064. | 0. | 0. 5064. | 7000. | 0. | 0. | 0. | .72 | 65. | 26.2 | D | 19.4 | 13.8 |
| * 14 3 | 1500. | 0. | 818. 5064. | 0. | 818. 5064. | 6878. | 0. | 0. | 0. | .74 | 64. | 26.2 | D | 19.4 | 13.8 |
| * 15 3 | 1300. | 0. | 0. 4246. | 0. | 0. 4246. | 6000. | 0. | 0. | 0. | .71 | 65. | 21.8 | C | 19.8 | 14.0 |
| * 16 3 | 1000. | 388. | 0. 4634. | 385. | 0. 4631. | 5967. | 0. | 0. | 0. | .78 | 64. | 24.2 | C | 19.7 | 13.6 |
| * 17 3 | 1100. | 0. | 0. 4634. | 0. | 0. 4631. | 6000. | 0. | 0. | 0. | .77 | 64. | 24.2 | C | 19.7 | 13.6 |
| * 18 4 | 1000. | 0. | 898. 4634. | 0. | 894. 4631. | 6898. | 0. | 0. | 0. | .67 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 19 3 | 900. | 0. | 0. 3736. | 0. | 0. 3737. | 6000. | 0. | 0. | 0. | .62 | 65. | 19.2 | C | 19.2 | 14.0 |
| * 20 3 | 100. | 274. | 0. 4010. | 240. | 0. 3977. | 5971. | 0. | 0. | 0. | .67 | 65. | 20.4 | C | 19.2 | 14.0 |
| * 21 3 | 100. | 0. | 0. 4010. | 0. | 0. 3977. | 6000. | 0. | 0. | 0. | .66 | 65. | 20.4 | C | 19.2 | 14.0 |
| * 22 3 | 100. | 0. | 0. 4010. | 0. | 0. 3977. | 6000. | 0. | 0. | 0. | .66 | 65. | 20.4 | C | 19.2 | 14.0 |
| * 23 3 | 700. | 0. | 0. 4010. | 0. | 0. 3097. | 6000. | 0. | * 463. | 880. | .52 | 55. | 18.6 | F | 18.8 | 14.2 |
| * 24 3 | 1500. | 0. | 862. 4010. | 0. | 847. 3097. | 5892. | 0. | ** 1500. | 880. | .53 | 28. | 37.1 | F | 16.8 | 15.7 |
| * 25 3 | 800. | 0. | 0. 3148. | 0. | 0. 2250. | 6000. | 0. | ** 800. | 880. | .37 | 12. | 63.9 | F | 14.9 | 17.3 |
| * 26 3 | 1000. | 1575. | 0. 4723. | 1281. | 0. 3531. | 5781. | 0. | ** 1000. | 880. | .61 | 16. | 72.4 | F | 14.4 | 18.1 |
| * 27 3 | 800. | 0. | 0. 4723. | 0. | 0. 3531. | 6000. | 0. | ** 800. | 880. | .59 | 13. | 91.5 | F | 13.2 | 19.6 |
| * 28 3 | 1000. | 0. | 315. 4723. | 0. | 290. 3531. | 5975. | 0. | ** 1000. | 880. | .59 | 11. | 107.0 | F | 12.3 | 20.8 |
| * 29 3 | 8000. | 0. | 0. 4408. | 0. | 0. 3241. | 6000. | 0. | ** 8000. | 880. | .54 | 6. | 183.8 | F | 9.1 | 26.9 |
| * 30 4 | 100. | 659. | 0. 5067. | 659. | 0. 3900. | 8000. | 0. | ** 100. | 880. | .49 | 5. | 214.0 | F | 8.4 | 28.7 |
| * 31 4 | 1000. | 1600. | 0. 6667. | 1600. | 0. 5500. | 5500. | 0. | 0. | 0. | 1.00 | 65. | 21.2 | E | 19.2 | 14.0 |
| * 32 4 | 2640. | 0. | 6667. 6667. | 0. | 5500. 5500. | 8000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 20.0 | 13.7 |

* TOTAL 144589. = 27.4 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 44. 36.2 18.4 14.5 *

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|----------------------------|--------------------|------------------|-------------------|------------------|
| FREWAY TRAVEL TIME = | 3051. VEH-HRS | 3063. PASS-HRS | 5265. VEH-HRS | 5288. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 728. VEH-HRS | 741. PASS-HRS | 1009. VEH-HRS | 1028. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 3779. VEH-HRS | 3803. PASS-HRS | 6274. VEH-HRS | 6316. PASS-HRS |
| TOTAL TRAV DISTANCE = | 134217. VEH-MI. | 134820. PASS-MI. | 264510. VEH-MI. | 265716. PASS-MI. |

AVERAGE SYSTEM SPEED = 36. MPH.
 AVERAGE DENSITY = 36. VPMP/L
 TOTAL FUEL = 7545. GALLONS
 TOTAL EMISSIONS = 2045. KILOGRAMS

50. MPH.
 31. VPMP/L
 14479. GALLONS
 3920. KILOGRAMS

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|--------|------------|-------|
| 1 | 0.00 | 2 | 10.46 | 3 | 0.30 | 4 | 0.10 | 5 | 0.16 |
| 6 | 0.32 | 7 | 0.11 | 8 | 0.15 | 9 | 0.15 | 10 | 0.36 |
| 11 | 0.11 | 12 | 0.10 | 13 | 0.19 | 14 | 0.21 | 15 | 0.00 |
| 16 | 0.28 | 17 | 0.28 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 1.40 | 24 | 22.45 | 25 | 30.41 |
| 26 | 35.49 | 27 | 37.64 | 28 | 55.75 | 29 | 774.71 | 30 | 15.07 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 986.2 VEH-HRS ***** AVERAGE DELAY = 18.19 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-----------|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|
| ON-RAMP 2 | RAMP | 100. | 98.50 | 12.19 | 35.17 | 2.18 | 11.41 | 14.20 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 98.50 | 12.19 | 35.17 | 2.18 | 11.41 | 14.20 |
| ON-RAMP 3 | RAMP | 89. | 72.00 | 13.13 | 25.71 | 1.59 | 8.34 | 10.38 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 89. | 72.00 | 13.13 | 25.71 | 1.59 | 8.34 | 10.38 |
| ON-RAMP 4 | RAMP | 604. | 457.00 | 13.03 | 163.19 | 10.12 | 52.94 | 65.87 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 604. | 457.00 | 13.03 | 163.19 | 10.12 | 52.94 | 65.87 |
| ON-RAMP 6 | RAMP | 100. | 100.00 | 4.02 | 35.71 | 2.22 | 11.58 | 14.41 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 100.00 | 4.02 | 35.71 | 2.22 | 11.58 | 14.41 |

 ** FREEWAY TRAVEL TIME (MINUTES) **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN 1 2 3 4 5 6 *

| | | | | | | | |
|---|-------|------|-------|-------|-------|-------|-------|
| + | * 1 * | 0.09 | 21.23 | 22.00 | 23.83 | 28.84 | 40.06 |
| + | * 2 * | 0.00 | 0.00 | 0.54 | 2.37 | 7.38 | 18.60 |
| + | * 3 * | 0.00 | 0.00 | 0.00 | 1.67 | 6.68 | 17.90 |
| + | * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 3.17 | 14.39 |
| + | * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.81 |
| + | * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.64 |
| + | * * | | | | | | |

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB | * NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | |
|-------|-------|----------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|--------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * ORG | * DES | * SSEC | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP/L | * LEVEL | * MPG | * GS/VM | |
| * 1 | * 4 | * 500. | * 5090. | * 662. | * 5090. | * 5090. | * 662. | * 5090. | * 10000. | * 0. | * 0. | * 51 | * 65. | * 19.6 | * C | * 19.2 | * 14.0 |
| * 2 | * 3 | * 99999. | * 0. | * 0. | * 4428. | * 0. | * 0. | * 4428. | * 7000. | * 0. | * 0. | * 63 | * 65. | * 22.7 | * C | * 19.2 | * 14.0 |
| * 3 | * 3 | * 2830. | * 0. | * 0. | * 4428. | * 0. | * 0. | * 4428. | * 7000. | * 0. | * 0. | * 63 | * 65. | * 22.7 | * C | * 19.2 | * 14.0 |

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| | | | | | | | | | | | | | | | | | | | | |
|--|---|-------|-------|-------|-------|-------|-------|-------|-------|----|----|-------|-------|-----|-------|-------|------|------|------|---|
| * 4 | 3 | 930. | 0. | 0. | 4428. | 0. | 0. | 4428. | 7000. | 0. | 0. | 0. | 63 | 65. | 22.7 | C | 19.2 | 14.0 | * | |
| * 5 | 3 | 1490. | 0. | 0. | 4428. | 0. | 0. | 4428. | 7000. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 | * | |
| * 6 | 3 | 3020. | 0. | 0. | 4428. | 0. | 0. | 4428. | 7000. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 | * | |
| * 7 | 3 | 1030. | 0. | 0. | 4428. | 0. | 0. | 4428. | 7000. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 | * | |
| * 8 | 3 | 1440. | 0. | 0. | 4428. | 0. | 0. | 4428. | 7000. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 | * | |
| * 9 | 3 | 1430. | 0. | 0. | 4428. | 0. | 0. | 4428. | 7000. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 | * | |
| * 10 | 3 | 3480. | 0. | 0. | 4428. | 0. | 0. | 4428. | 7000. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 | * | |
| * 11 | 3 | 1020. | 0. | 0. | 4428. | 0. | 0. | 4428. | 7000. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 | * | |
| * 12 | 3 | 980. | 0. | 0. | 4428. | 0. | 0. | 4428. | 7000. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 | * | |
| * 13 | 3 | 1800. | 0. | 0. | 4428. | 0. | 0. | 4428. | 7000. | 0. | 0. | 0. | .63 | 65. | 22.7 | C | 19.2 | 14.0 | * | |
| * 14 | 3 | 1500. | 0. | 644. | 4428. | 0. | 644. | 4428. | 6904. | 0. | 0. | 0. | .64 | 65. | 22.7 | C | 19.2 | 14.0 | * | |
| * 15 | 3 | 1300. | 0. | 0. | 3784. | 0. | 0. | 3784. | 6000. | 0. | 0. | 0. | .63 | 65. | 19.4 | C | 19.2 | 14.0 | * | |
| * 16 | 3 | 1000. | 340. | 0. | 4124. | 340. | 0. | 4124. | 5970. | 0. | 0. | 0. | .69 | 65. | 21.1 | C | 19.2 | 14.0 | * | |
| * 17 | 3 | 1100. | 0. | 0. | 4124. | 0. | 0. | 4124. | 6000. | 0. | 0. | 0. | .69 | 65. | 21.1 | C | 19.2 | 14.0 | * | |
| * 18 | 4 | 1000. | 0. | 757. | 4124. | 0. | 757. | 4124. | 6917. | 0. | 0. | 0. | .60 | 65. | 15.9 | B | 19.2 | 14.0 | * | |
| * 19 | 3 | 900. | 0. | 0. | 3367. | 0. | 0. | 3367. | 6000. | 0. | 0. | 0. | .56 | 65. | 17.3 | B | 19.2 | 14.0 | * | |
| * 20 | 3 | 100. | 242. | 0. | 3609. | 240. | 0. | 3607. | 5973. | 0. | 0. | 0. | .60 | 65. | 18.5 | C | 19.2 | 14.0 | * | |
| * 21 | 3 | 100. | 0. | 0. | 3609. | 0. | 0. | 3607. | 6000. | 0. | 0. | 0. | .60 | 65. | 18.5 | C | 19.2 | 14.0 | * | |
| * 22 | 3 | 100. | 0. | 0. | 3609. | 0. | 0. | 3607. | 6000. | 0. | 0. | 0. | .60 | 65. | 18.5 | C | 19.2 | 14.0 | * | |
| * 23 | 3 | 700. | 0. | 0. | 3609. | 0. | 0. | 3607. | 6000. | 0. | 0. | 0. | .60 | 40. | 29.7 | D | 17.9 | 14.9 | * | |
| * 24 | 3 | 1500. | 0. | 737. | 3609. | 0. | 736. | 3607. | 5907. | 0. | 0. | 0. | .61 | 12. | 100.3 | F | 12.8 | 20.7 | * | |
| * 25 | 3 | 800. | 0. | 0. | 2872. | 0. | 0. | 3061. | 6000. | 0. | * | 621. | -191. | 51 | 5. | 206.0 | F | 8.5 | 28.5 | * |
| * 26 | 3 | 1000. | 1157. | 0. | 4029. | 1337. | 0. | 4398. | 5837. | 0. | ** | 1000. | -191. | 75 | 10. | 140.5 | F | 13.4 | 22.5 | * |
| * 27 | 3 | 800. | 0. | 0. | 4029. | 0. | 0. | 4398. | 6000. | 0. | ** | 800. | -191. | 73 | 10. | 149.8 | F | 12.9 | 23.0 | * |
| * 28 | 3 | 1000. | 0. | 202. | 4029. | 0. | 220. | 4398. | 5982. | 0. | ** | 1000. | -191. | 74 | 10. | 148.8 | F | 12.9 | 23.0 | * |
| * 29 | 3 | 8000. | 0. | 0. | 3827. | 0. | 0. | 4178. | 6000. | 0. | ** | 8000. | -191. | 70 | 9. | 159.4 | F | 11.5 | 24.3 | * |
| * 30 | 4 | 100. | 572. | 0. | 4399. | 572. | 0. | 4750. | 8000. | 0. | ** | 100. | -191. | 59 | 6. | 186.2 | F | 9.3 | 27.1 | * |
| * 31 | 4 | 1000. | 750. | 0. | 5149. | 750. | 0. | 5500. | 5500. | 0. | 0. | 0. | 1.00 | 65. | 21.2 | E | 19.2 | 14.0 | * | |
| * 32 | 4 | 2640. | 0. | 5149. | 5149. | 0. | 5500. | 5500. | 8000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 20.0 | 13.7 | * | |
| ***** | | | | | | | | | | | | | | | | | | | | |
| * TOTAL 144589. = 27.4 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 42. 34.4 18.2 14.8 * | | | | | | | | | | | | | | | | | | | | |
| ***** | | | | | | | | | | | | | | | | | | | | |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 2/29/2016 16:42 PAGE 14
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 3 OF 3

| CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | | |
|----------------------------|---------|------------|---------|-------------------|---------|------------|---------|----------|
| FREWAY TRAVEL TIME = | 2854. | VEH-HRS | 2866. | PASS-HRS | 8120. | VEH-HRS | 8154. | PASS-HRS |
| FREWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 804. | VEH-HRS | 817. | PASS-HRS | 1813. | VEH-HRS | 1845. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 3658. | VEH-HRS | 3683. | PASS-HRS | 9932. | VEH-HRS | 9999. | PASS-HRS |
| TOTAL TRAV DISTANCE = | 120589. | VEH-MI. | 121184. | PASS-MI. | 385099. | VEH-MI. | 386900. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 33. | MPH. | | | 47. | MPH. | | |
| AVERAGE DENSITY = | 34. | VPMP/L | | | 32. | VPMP/L | | |
| TOTAL FUEL = | 6911. | GALLONS | | | 21391. | GALLONS | | |
| TOTAL EMISSIONS = | 1904. | KI LOGRAMS | | | 5824. | KI LOGRAMS | | |

| ***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 ***** | | | | | | | | | |
|---|-------|------------|-------|------------|-------|------------|--------|------------|-------|
| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
| 1 | 0.00 | 2 | 0.06 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 4.48 | 24 | 71.80 | 25 | 86.42 |
| 26 | 67.02 | 27 | 57.83 | 28 | 71.71 | 29 | 627.11 | 30 | 12.72 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 999.2 VEH-HRS ***** AVERAGE DELAY = 14.81 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 2/29/2016 16:42 PAGE 15
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 3 OF 3

| ***** RAMP DELAYS ***** | | | | | | | | | |
|-------------------------|---|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|
| | | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
| ON-RAMP | 2 | RAMP | 100. | 100.00 | 13.64 | 35.71 | 2.22 | 11.58 | 14.41 |
| | | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 100.00 | 13.64 | 35.71 | 2.22 | 11.58 | 14.41 |
| ON-RAMP | 3 | RAMP | 91. | 90.00 | 16.31 | 32.14 | 1.99 | 10.43 | 12.97 |
| | | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 91. | 90.00 | 16.31 | 32.14 | 1.99 | 10.43 | 12.97 |
| ON-RAMP | 4 | RAMP | 424. | 514.00 | 16.03 | 183.54 | 11.39 | 59.55 | 74.09 |
| | | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 424. | 514.00 | 16.03 | 183.54 | 11.39 | 59.55 | 74.09 |
| ON-RAMP | 6 | RAMP | 100. | 100.00 | 7.97 | 35.71 | 2.22 | 11.58 | 14.41 |
| | | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 100.00 | 7.97 | 35.71 | 2.22 | 11.58 | 14.41 |

```

FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP LLL
FFFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 1111111 222222222 PPP LLLLLLLLLL
    
```

FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 2 AND 29 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65 MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

FREEWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC | SSEC | DESIGN | ORG | TRK | SSEC | PCT | PCT | DES | SPECIAL | FF.SPD. | CAP. | ART | GRADE | SUBSECTION | LOCATION |
|---------|------|-------|--------|-----|-----|------|-----|--------|------|---------|----------|----------|------|----------|--------------------------|----------|
| SEC | LNS | CAP | SPEED | DES | FAC | GRAD | TRK | TRUCKS | RAMP | RAMP | ALT. RTE | ALT. RTE | TYPE | ALT. RTE | | |
| 1 | | | | | | | | | | | | | | | | |
| 2 | 1 | 1650. | 99999. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | |
| 3 | 1 | 1650. | 2830. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-87 to DLC loop-on | |
| 4 | 1 | 1650. | 930. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | DLC loop on to dia-on | |
| 5 | 1 | 1650. | 1490. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | DLC dia-on to Tomas off | |
| 6 | 1 | 1650. | 3020. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas off to on | |
| 7 | 1 | 1650. | 1030. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas on to bowers off | |
| 8 | 1 | 1650. | 1440. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers off to loop-on | |
| 9 | 1 | 1650. | 1430. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers loop-on to dia | |
| 10 | 1 | 1650. | 3480. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers dia-on to law-off | |
| 11 | 1 | 1650. | 1020. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Law off to loop-on | |
| 12 | 1 | 1650. | 980. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Lawr Loop to diag | |
| 13 | 1 | 1650. | 1800. | 65 | | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Lawrence On-ramp | |
| 14 | 1 | 1650. | 1500. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks Off-Ramp | |
| 15 | 1 | 1650. | 1300. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Fair Oaks | |
| 16 | 1 | 1650. | 1000. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Fair Oaks On-Ramp | |
| 17 | 1 | 1650. | 1100. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Mathilda | |
| 18 | 1 | 1650. | 1000. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda NB Off-Ramp | |
| 19 | 1 | 1650. | 900. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | |

```

**
** 20 1 1650. 100. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Mathilda NB On-Ramp **
**
*****

```

FREEWAY AND ARTERIAL DESIGN FEATURES

```

*****
**
** SUB NO. SSEC SSEC DESIGN ORG TRK SSEC PCT PCT DES SPECIAL FF.SPD. CAP. ART GRADE SUBSECTION LOCATION **
** SEC LNS CAP LENGTH SPEED DES FAC GRAD TRK TRUCKS RAMP ALT. RTE ALT. RTE TYPE ALT. RTE **
*****
** 21 1 1650. 100. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Mathilda / Mathilda **
** 22 1 1650. 100. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Mathilda SB Off-ramp **
** 23 1 1650. 700. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Mathilda / SR-237 **
** 24 1 1650. 1500. 65 D 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 SR-237 WB Off-Ramp **
** 25 1 1650. 800. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 SR-237 / SR-237 **
** 26 1 1650. 1000. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 SR-237 WB On-Ramp **
** 27 1 1650. 800. 65 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 SR-237 / Ellis **
** 28 1 1650. 1000. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Ellis Off-ramp **
** 29 1 1650. 8000. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 HOV Dummy **
** 30 **
** 31 **
** 32 **
*****

```

FREEWAY TRAVEL TIME (MINUTES)

```

*****
* ORIGINS DESTINATIONS ACROSS *
* DOWN 1 2 3 4 5 6 7 *
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 2 * 0.00 21.14 21.91 22.51 23.14 24.54 0.00 *
+
* 3 * 0.00 0.00 0.00 0.00 0.00 3.16 0.00 *
+
* 4 * 0.00 0.00 0.00 0.00 0.00 2.47 0.00 *
+
* 5 * 0.00 0.00 0.00 0.00 0.00 1.89 0.00 *
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
* *
*****

```

TIME SLICE FREEWAY PERFORMANCE TABLE

```

*****
* SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMISS *
* SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMP LEVEL MPG GS/VM *
*****
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*****
*          *
* 1          *
* 2 1 99999. 717. 0. 717. 717. 0. 717. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 3 1 2830. 0. 0. 717. 0. 0. 717. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 4 1 930. 0. 0. 717. 0. 0. 717. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 5 1 1490. 0. 0. 717. 0. 0. 717. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 6 1 3020. 0. 0. 717. 0. 0. 717. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 7 1 1030. 0. 0. 717. 0. 0. 717. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 8 1 1440. 0. 0. 717. 0. 0. 717. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 9 1 1430. 0. 0. 717. 0. 0. 717. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 10 1 3480. 0. 0. 717. 0. 0. 717. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 11 1 1020. 0. 0. 717. 0. 0. 717. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 12 1 980. 0. 0. 717. 0. 0. 717. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 13 1 1800. 0. 0. 717. 0. 0. 717. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 14 1 1500. 0. 81. 717. 0. 81. 717. 1650. 0. 0. 0. .43 65. 11.0 B 20.0 13.7 *
* 15 1 1300. 0. 0. 637. 0. 0. 637. 1650. 0. 0. 0. .39 65. 9.8 A 20.0 13.7 *
* 16 1 1000. 33. 0. 670. 33. 0. 670. 1650. 0. 0. 0. .41 65. 10.3 A 20.0 13.7 *
* 17 1 1100. 0. 0. 670. 0. 0. 670. 1650. 0. 0. 0. .41 65. 10.3 A 20.0 13.7 *
* 18 1 1000. 0. 94. 670. 0. 94. 670. 1650. 0. 0. 0. .41 65. 10.3 A 20.0 13.7 *
* 19 1 900. 0. 0. 576. 0. 0. 576. 1650. 0. 0. 0. .35 65. 8.9 A 20.0 13.7 *
* 20 1 100. 35. 0. 610. 35. 0. 610. 1650. 0. 0. 0. .37 65. 9.4 A 20.0 13.7 *
* 21 1 100. 0. 0. 610. 0. 0. 610. 1650. 0. 0. 0. .37 65. 9.4 A 20.0 13.7 *
* 22 1 100. 0. 0. 610. 0. 0. 610. 1650. 0. 0. 0. .37 65. 9.4 A 20.0 13.7 *
* 23 1 700. 0. 0. 610. 0. 0. 610. 1650. 0. 0. 0. .37 65. 9.4 A 20.0 13.7 *
* 24 1 1500. 0. 80. 610. 0. 80. 610. 1650. 0. 0. 0. .37 65. 9.4 A 20.0 13.7 *
* 25 1 800. 0. 0. 530. 0. 0. 530. 1650. 0. 0. 0. .32 65. 8.2 A 20.0 13.7 *
* 26 1 1000. 223. 0. 753. 223. 0. 753. 1650. 0. 0. 0. .46 65. 11.6 B 20.0 13.7 *
* 27 1 800. 0. 0. 753. 0. 0. 753. 1650. 0. 0. 0. .46 65. 11.6 B 20.0 13.7 *
* 28 1 1000. 0. 25. 753. 0. 25. 753. 1650. 0. 0. 0. .46 65. 11.6 B 20.0 13.7 *
* 29 1 8000. 0. 728. 728. 0. 728. 728. 1650. 0. 0. 0. .44 65. 11.2 B 20.0 13.7 *
* 30          *
* 31          *
* 32          *
*          *
*          *
*****
* TOTAL 140349. = 26.6 MILES MAX(V/C) = 0.46 LOWEST LOS = B AVG = 65. 11.0 20.0 13.7 *
*****

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CURRENT TIME SLICE CUMULATIVE VALUES

FREEWAY TRAVEL TIME = 292. VEH-HRS 583. PASS-HRS 292. VEH-HRS 583. PASS-HRS
 FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
 ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
 OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
 TOTAL SYSTEM TRAVEL TIME = 292. VEH-HRS 583. PASS-HRS 292. VEH-HRS 583. PASS-HRS
 TOTAL FREEWAY TRAVEL DISTANCE = 18955. VEH-MI. 37909. PASS-MI. 18955. VEH-MI. 37909. PASS-MI.
 AVERAGE SYSTEM SPEED = 65. MPH. 65. MPH.
 AVERAGE DENSITY = 11. VPML 11. VPML
 TOTAL FUEL = 948. GALLONS 948. GALLONS
 TOTAL EMISSIONS = 260. KILOGRAMS 260. KILOGRAMS

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | 30 | 0.00 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

```

*****
**          **
**          **
**          **
**          **
**          **
*****
* ORIGINATIONS ACROSS DESTINATIONS ACROSS *
* DOWN          *
*          *
+          *
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+          *
* 2 * 0.00 21.14 21.91 22.51 23.14 24.54 0.00 *
+          *
* 3 * 0.00 0.00 0.00 0.00 0.00 3.16 0.00 *
+          *
* 4 * 0.00 0.00 0.00 0.00 0.00 2.47 0.00 *
+          *
* 5 * 0.00 0.00 0.00 0.00 0.00 1.89 0.00 *
+          *

```

```
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
* *
*****
```

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|-----------|---------|------------|----------------|----------------|----------------|--------|---------|-----------------|----------------|-----------|---------|-----------|---------|--------|-------------|
| * SEC | * LNS | * LENGTH | * ORG DES SSEC | * ORG DES SSEC | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 1 | | | | | | | | | | | | | | | |
| * 2 | 1 | 99999 | 756. 0. 756. | 756. 0. 756. | 0. 756. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 3 | 1 | 2830. | 0. 0. 756. | 0. 0. 756. | 0. 0. 756. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 4 | 1 | 930. | 0. 0. 756. | 0. 0. 756. | 0. 0. 756. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 5 | 1 | 1490. | 0. 0. 756. | 0. 0. 756. | 0. 0. 756. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 6 | 1 | 3020. | 0. 0. 756. | 0. 0. 756. | 0. 0. 756. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 7 | 1 | 1030. | 0. 0. 756. | 0. 0. 756. | 0. 0. 756. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 8 | 1 | 1440. | 0. 0. 756. | 0. 0. 756. | 0. 0. 756. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 9 | 1 | 1430. | 0. 0. 756. | 0. 0. 756. | 0. 0. 756. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 10 | 1 | 3480. | 0. 0. 756. | 0. 0. 756. | 0. 0. 756. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 11 | 1 | 1020. | 0. 0. 756. | 0. 0. 756. | 0. 0. 756. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 12 | 1 | 980. | 0. 0. 756. | 0. 0. 756. | 0. 0. 756. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 13 | 1 | 1800. | 0. 0. 756. | 0. 0. 756. | 0. 0. 756. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 14 | 1 | 1500. | 0. 122. 756. | 0. 122. 756. | 0. 122. 756. | 1650. | 0. | 0. | 0. | .46 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 15 | 1 | 1300. | 0. 0. 634. | 0. 0. 634. | 0. 0. 634. | 1650. | 0. | 0. | 0. | .38 | 65. | 9.8 | A | 20.0 | 13.7 |
| * 16 | 1 | 1000. | 33. 0. 667. | 33. 0. 667. | 0. 0. 667. | 1650. | 0. | 0. | 0. | .40 | 65. | 10.3 | A | 20.0 | 13.7 |
| * 17 | 1 | 1100. | 0. 0. 667. | 0. 0. 667. | 0. 0. 667. | 1650. | 0. | 0. | 0. | .40 | 65. | 10.3 | A | 20.0 | 13.7 |
| * 18 | 1 | 1000. | 0. 122. 667. | 0. 122. 667. | 0. 122. 667. | 1650. | 0. | 0. | 0. | .40 | 65. | 10.3 | A | 20.0 | 13.7 |
| * 19 | 1 | 900. | 0. 0. 545. | 0. 0. 545. | 0. 0. 545. | 1650. | 0. | 0. | 0. | .33 | 65. | 8.4 | A | 20.0 | 13.7 |
| * 20 | 1 | 100. | 29. 0. 574. | 29. 0. 574. | 0. 0. 574. | 1650. | 0. | 0. | 0. | .35 | 65. | 8.8 | A | 20.0 | 13.7 |
| * 21 | 1 | 100. | 0. 0. 574. | 0. 0. 574. | 0. 0. 574. | 1650. | 0. | 0. | 0. | .35 | 65. | 8.8 | A | 20.0 | 13.7 |
| * 22 | 1 | 100. | 0. 0. 574. | 0. 0. 574. | 0. 0. 574. | 1650. | 0. | 0. | 0. | .35 | 65. | 8.8 | A | 20.0 | 13.7 |
| * 23 | 1 | 700. | 0. 0. 574. | 0. 0. 574. | 0. 0. 574. | 1650. | 0. | 0. | 0. | .35 | 65. | 8.8 | A | 20.0 | 13.7 |
| * 24 | 1 | 1500. | 0. 108. 574. | 0. 108. 574. | 0. 108. 574. | 1650. | 0. | 0. | 0. | .35 | 65. | 8.8 | A | 20.0 | 13.7 |
| * 25 | 1 | 800. | 0. 0. 466. | 0. 0. 466. | 0. 0. 466. | 1650. | 0. | 0. | 0. | .28 | 65. | 7.2 | A | 20.0 | 13.7 |
| * 26 | 1 | 1000. | 219. 0. 684. | 219. 0. 684. | 0. 0. 684. | 1650. | 0. | 0. | 0. | .41 | 65. | 10.5 | A | 20.0 | 13.7 |
| * 27 | 1 | 800. | 0. 0. 684. | 0. 0. 684. | 0. 0. 684. | 1650. | 0. | 0. | 0. | .41 | 65. | 10.5 | A | 20.0 | 13.7 |
| * 28 | 1 | 1000. | 0. 25. 684. | 0. 25. 684. | 0. 25. 684. | 1650. | 0. | 0. | 0. | .41 | 65. | 10.5 | A | 20.0 | 13.7 |
| * 29 | 1 | 8000. | 0. 659. 659. | 0. 659. 659. | 0. 659. 659. | 1650. | 0. | 0. | 0. | .40 | 65. | 10.1 | A | 20.0 | 13.7 |
| * 30 | | | | | | | | | | | | | | | |
| * 31 | | | | | | | | | | | | | | | |
| * 32 | | | | | | | | | | | | | | | |
| * TOTAL | 140349. | = | 26.6 MILES | | | | | MAX(V/C) = 0.46 | LOWEST LOS = B | AVG = 65. | 11.4 | | | 20.0 | 13.7 |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 303. VEH-HRS | 594. VEH-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 303. VEH-HRS | 594. VEH-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 19672. VEH-MI. | 38627. VEH-MI. |
| AVERAGE SYSTEM SPEED = | 65. MPH. | 65. MPH. |
| AVERAGE DENSITY = | 11. VPMP | 11. VPMP |
| TOTAL FUEL = | 984. GALLONS | 1931. GALLONS |
| TOTAL EMISSIONS = | 270. KILOGRAMS | 531. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | 30 | 0.00 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

 **

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 FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | |
|-----------|--|-----------------------|-------|-------|-------|-------|-------|------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | | 0.00 | 21.14 | 21.91 | 22.51 | 23.14 | 24.54 | 0.00 |
| * 3 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.16 | 0.00 |
| * 4 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.47 | 0.00 |
| * 5 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.89 | 0.00 |
| * 6 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 7 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB | * NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|---------|---------|----------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * ORG | * DES | * SSEC | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 1 | | | | | | | | | | | | | | | | |
| * 2 | 1 | 99999 | 662. | 0. | 662. | 662. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 |
| * 3 | 1 | 2830. | 0. | 0. | 662. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 |
| * 4 | 1 | 930. | 0. | 0. | 662. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 |
| * 5 | 1 | 1490. | 0. | 0. | 662. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 |
| * 6 | 1 | 3020. | 0. | 0. | 662. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 |
| * 7 | 1 | 1030. | 0. | 0. | 662. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 |
| * 8 | 1 | 1440. | 0. | 0. | 662. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 |
| * 9 | 1 | 1430. | 0. | 0. | 662. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 |
| * 10 | 1 | 3480. | 0. | 0. | 662. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 |
| * 11 | 1 | 1020. | 0. | 0. | 662. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 |
| * 12 | 1 | 980. | 0. | 0. | 662. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 |
| * 13 | 1 | 1800. | 0. | 0. | 662. | 0. | 0. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 |
| * 14 | 1 | 1500. | 0. | 96. | 662. | 0. | 96. | 662. | 1650. | 0. | 0. | .40 | 65. | 10.2 | A | 20.0 |
| * 15 | 1 | 1300. | 0. | 0. | 565. | 0. | 0. | 565. | 1650. | 0. | 0. | .34 | 65. | 8.7 | A | 20.0 |
| * 16 | 1 | 1000. | 30. | 0. | 595. | 30. | 0. | 595. | 1650. | 0. | 0. | .36 | 65. | 9.2 | A | 20.0 |
| * 17 | 1 | 1100. | 0. | 0. | 595. | 0. | 0. | 595. | 1650. | 0. | 0. | .36 | 65. | 9.2 | A | 20.0 |
| * 18 | 1 | 1000. | 0. | 103. | 595. | 0. | 103. | 595. | 1650. | 0. | 0. | .36 | 65. | 9.2 | A | 20.0 |
| * 19 | 1 | 900. | 0. | 0. | 492. | 0. | 0. | 492. | 1650. | 0. | 0. | .30 | 65. | 7.6 | A | 20.0 |
| * 20 | 1 | 100. | 27. | 0. | 519. | 27. | 0. | 519. | 1650. | 0. | 0. | .31 | 65. | 8.0 | A | 20.0 |
| * 21 | 1 | 100. | 0. | 0. | 519. | 0. | 0. | 519. | 1650. | 0. | 0. | .31 | 65. | 8.0 | A | 20.0 |
| * 22 | 1 | 100. | 0. | 0. | 519. | 0. | 0. | 519. | 1650. | 0. | 0. | .31 | 65. | 8.0 | A | 20.0 |
| * 23 | 1 | 700. | 0. | 0. | 519. | 0. | 0. | 519. | 1650. | 0. | 0. | .31 | 65. | 8.0 | A | 20.0 |
| * 24 | 1 | 1500. | 0. | 93. | 519. | 0. | 93. | 519. | 1650. | 0. | 0. | .31 | 65. | 8.0 | A | 20.0 |
| * 25 | 1 | 800. | 0. | 0. | 426. | 0. | 0. | 426. | 1650. | 0. | 0. | .26 | 65. | 6.6 | A | 20.0 |
| * 26 | 1 | 1000. | 163. | 0. | 589. | 163. | 0. | 589. | 1650. | 0. | 0. | .36 | 65. | 9.1 | A | 20.0 |
| * 27 | 1 | 800. | 0. | 0. | 589. | 0. | 0. | 589. | 1650. | 0. | 0. | .36 | 65. | 9.1 | A | 20.0 |
| * 28 | 1 | 1000. | 0. | 18. | 589. | 0. | 18. | 589. | 1650. | 0. | 0. | .36 | 65. | 9.1 | A | 20.0 |
| * 29 | 1 | 8000. | 0. | 572. | 572. | 0. | 572. | 572. | 1650. | 0. | 0. | .35 | 65. | 8.8 | A | 20.0 |
| * 30 | | | | | | | | | | | | | | | | |
| * 31 | | | | | | | | | | | | | | | | |
| * 32 | | | | | | | | | | | | | | | | |
| * TOTAL | 140349. | = | 26.6 | MILES | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | |
|-----------------------------|--------------------|------------|--------|----------|-------------------|------------|---------|----------|
| FREEWAY TRAVEL TIME = | 265. | VEH-HRS | 530. | PASS-HRS | 859. | VEH-HRS | 1718. | PASS-HRS |
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 265. | VEH-HRS | 530. | PASS-HRS | 859. | VEH-HRS | 1718. | PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 17220. | VEH-MI. | 34439. | PASS-MI. | 55846. | VEH-MI. | 111693. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 65. | MPH. | | | 65. | MPH. | | |
| AVERAGE DENSITY = | 10. | VPMP | | | 11. | VPMP | | |
| TOTAL FUEL = | 861. | GALLONS | | | 2792. | GALLONS | | |
| TOTAL EMISSIONS = | 237. | KI LOGRAMS | | | 767. | KI LOGRAMS | | |

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***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | 30 | 0.00 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

```

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q* A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP EEE
FFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQ 1111111 222222222 PPP PPP EEEEEEEEE

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FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

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*****
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**
**                      FREeway AND ARTERIAL DESIGN FEATURES
**
*****
**
** SUB NO.   SSEC  SSEC  DESIGN  ORG  TRK  SSEC  PCT  PCT  DES  SPECIAL  FF. SPD.  CAP.  ART  GRADE  SUBSECTION LOCATION
** SEC  LNS   CAP   LENGTH SPEED  DES  FAC  GRAD  TRK  TRUCKS RAMP   ALT. RTE  ALT. RTE  TYPE ALT. RTE
**
**  1   5  10000.  1370.  65   OD  0.96  0.0  4    0    NO   0.0     0.   GOOD  0.0  Seeding
**
**  2   3   6226.  99999. 65   0.96  0.0  4    0    NO   0.0     0.   GOOD  0.0  Queue Capture
**
**  3   3   6000.  2740.  65   0.96  0.0  4    0    NO   0.0     0.   GOOD  0.0  SR-85 Off to Shore On
**
**  4   3   6000.   600.  65   0.96  0.0  4    0    NO   0.0     0.   GOOD  0.0  Shore. On to Moffet Off
**
**  5   3   6000.   700.  65   0.96  0.0  4    0    NO   0.0     0.   GOOD  0.0  Moffett Off to On
**
**  6   3   6000.  2630.  65   0.96  0.0  4    0    NO   0.0     0.   GOOD  0.0  Moffett On to Ellis Off
**
**  7   3   6000.  2530.  65   0.96  0.0  4    0    NO   0.0     0.   GOOD  0.0  Ellis Off to On-ramp
**
**  8   4   6240.  1500.  65   0  0.96  0.0  4    0    YES  0.0     0.   GOOD  0.0  Ellis On-ramp
**
**  9   4   6240.   700.  65   0.96  0.0  4    0    YES  0.0     0.   GOOD  0.0  Ellis / US 237
**
** 10   4   6240.  1500.  65   D  0.96  0.0  4    0    NO   0.0     0.   GOOD  0.0  SR-237 EB Off-Ramp
**
** 11   3   6000.   750.  65   0.96  0.0  4    0    NO   0.0     0.   GOOD  0.0  SR-237 / SR-237
**
** 12   4   6410.   350.  65   0  0.96  0.0  4    0    YES  0.0     0.   GOOD  0.0  SR-237 EB On-Ramp
**
** 13   4   6410.   350.  65   0.96  0.0  4    0    YES  0.0     0.   GOOD  0.0  US 237 / Mathilda
**
** 14   4   6410.   350.  65   D  0.96  0.0  4    0    NO   0.0     0.   GOOD  0.0  Mathilda Off-Ramp
**
** 15   3   6000.   700.  65   0.96  0.0  4    0    NO   0.0     0.   GOOD  0.0  Mathilda / Mathilda
**
** 16   3   6000.   900.  65   0  0.96  0.0  4    0    YES  0.0     0.   GOOD  0.0  Mathilda SB On-Ramp
**
** 17   3   6000.  1400.  65   0  0.96  0.0  4    0    YES  0.0     0.   GOOD  0.0  Mathilda NB On-Ramp
**
** 18   3   6000.   200.  65   0.96  0.0  4    0    NO   0.0     0.   GOOD  0.0  Mathilda / Fair Oaks
**
** 19   3   6000.  1400.  65   D  0.96  0.0  4    0    NO   0.0     0.   GOOD  0.0  Fair Oaks SB Off-Ramp
**
** 20   3   6000.   900.  65   0.96  0.0  4    0    NO   0.0     0.   GOOD  0.0  Fair Oaks SB/ Fair Oaks
**
*****
*****

```

FREWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC | SSEC | DESIGN | ORG | TRK | SSEC | PCT | PCT | DES | SPECIAL | FF. SPD. | CAP. | ART | GRADE | SUBSECTION | LOCATION |
|---------|------|--------|--------|-----|-----|------|-----|--------|------|---------|----------|----------|------|----------|------------------|-----------|
| SEC | LNS | CAP | LENGTH | DES | FAC | GRAD | TRK | TRUCKS | RAMP | RAMP | ALT. RTE | ALT. RTE | TYPE | ALT. RTE | | |
| ** 21 | 4 | 6130. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Fair Oaks SB | On-Ramp |
| ** 22 | 4 | 6130. | 100. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks NB | Off-Ramp |
| ** 23 | 3 | 6000. | 600. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks NB/ | Fair Oaks |
| ** 24 | 3 | 6000. | 1500. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Oaks On-Ramp | to Mid |
| ** 25 | 3 | 6000. | 1500. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mid to Lawrence | Off-ramp |
| ** 26 | 3 | 6000. | 8000. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | |
| ** 27 | 5 | 10000. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | |
| ** 28 | 5 | 7750. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Dummy Bottleneck | |
| ** 29 | 5 | 9685. | 1000. | 65 | 0D | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | End of Network | |

***** INPUT HAS BEEN COMPLETED *****

FREWAY TRAVEL TIME (MINUTES)

| ORIGINS | DESTINATIONS ACROSS | | | | | |
|---------|---------------------|-------|-------|-------|-------|-------|
| DOWN | 1 | 2 | 3 | 4 | 5 | 6 |
| * 1 * | 0.24 | 20.28 | 20.59 | 21.40 | 21.59 | 24.02 |
| * 2 * | 0.00 | 0.65 | 0.96 | 1.77 | 1.96 | 4.38 |
| * 3 * | 0.00 | 0.00 | 0.18 | 0.99 | 1.18 | 3.61 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.68 | 0.87 | 3.30 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.52 | 0.72 | 3.14 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.03 | 2.46 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.32 |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.37 |
| * 9 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.35 |
| * 10 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED | VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMISS | | | |
|---------|------|----------|---------|----------|---------|-------|-------|---------|---------|-------|-------|---------|-------|------|-------|---|------|------|
| SEC | LNS | LENGTH | ORG | DES | SSEC | CAP. | EFF | LENGTH | RATE | RATIO | MPH | VPML | LEVEL | MPG | GS/VM | | | |
| * 1 | 5 | 1370. | 5690. | 967. | 5690. | 5690. | 967. | 5690. | 10000. | 0. | 0. | 0. | .57 | 65. | 17.5 | B | 19.2 | 14.0 |

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| | | | | | | | | | | | | | | | | | | | | |
|---|--|---|--------|------|-------|-------|------|-------|-------|--------|----|----|----|-----|-----|------|---|------|------|---|
| * | 2 | 3 | 99999. | 0. | 0. | 4723. | 0. | 0. | 4723. | 6226. | 0. | 0. | 0. | .76 | 64. | 24.6 | C | 19.6 | 13.7 | * |
| * | 3 | 3 | 2740. | 0. | 0. | 4723. | 0. | 0. | 4723. | 6000. | 0. | 0. | 0. | .79 | 63. | 24.8 | C | 19.9 | 13.5 | * |
| * | 4 | 3 | 600. | 0. | 0. | 4723. | 0. | 0. | 4723. | 6000. | 0. | 0. | 0. | .79 | 63. | 24.8 | C | 19.9 | 13.5 | * |
| * | 5 | 3 | 700. | 0. | 0. | 4723. | 0. | 0. | 4723. | 6000. | 0. | 0. | 0. | .79 | 63. | 24.8 | C | 19.9 | 13.5 | * |
| * | 6 | 3 | 2630. | 0. | 0. | 4723. | 0. | 0. | 4723. | 6000. | 0. | 0. | 0. | .79 | 63. | 24.8 | C | 19.9 | 13.5 | * |
| * | 7 | 3 | 2530. | 0. | 0. | 4723. | 0. | 0. | 4723. | 6000. | 0. | 0. | 0. | .79 | 63. | 24.8 | C | 19.9 | 13.5 | * |
| * | 8 | 4 | 1500. | 171. | 0. | 4894. | 171. | 0. | 4894. | 6220. | 0. | 0. | 0. | .79 | 65. | 18.8 | C | 19.2 | 14.0 | * |
| * | 9 | 4 | 700. | 0. | 0. | 4894. | 0. | 0. | 4894. | 6240. | 0. | 0. | 0. | .78 | 65. | 18.8 | C | 19.2 | 14.0 | * |
| * | 10 | 4 | 1500. | 0. | 1395. | 4894. | 0. | 1395. | 4894. | 5965. | 0. | 0. | 0. | .82 | 65. | 18.8 | C | 19.2 | 14.0 | * |
| * | 11 | 3 | 750. | 0. | 0. | 3499. | 0. | 0. | 3499. | 6000. | 0. | 0. | 0. | .58 | 65. | 17.9 | B | 19.2 | 14.0 | * |
| * | 12 | 4 | 350. | 767. | 0. | 4266. | 767. | 0. | 4266. | 6277. | 0. | 0. | 0. | .68 | 65. | 16.4 | B | 19.2 | 14.0 | * |
| * | 13 | 4 | 350. | 0. | 0. | 4266. | 0. | 0. | 4266. | 6410. | 0. | 0. | 0. | .67 | 65. | 16.4 | B | 19.2 | 14.0 | * |
| * | 14 | 4 | 350. | 0. | 277. | 4266. | 0. | 277. | 4266. | 6367. | 0. | 0. | 0. | .67 | 65. | 16.4 | B | 19.2 | 14.0 | * |
| * | 15 | 3 | 700. | 0. | 0. | 3989. | 0. | 0. | 3989. | 6000. | 0. | 0. | 0. | .66 | 65. | 20.5 | C | 19.2 | 14.0 | * |
| * | 16 | 3 | 900. | 94. | 0. | 4083. | 94. | 0. | 4083. | 5983. | 0. | 0. | 0. | .68 | 65. | 20.9 | C | 19.2 | 14.0 | * |
| * | 17 | 3 | 1400. | 236. | 0. | 4319. | 236. | 0. | 4319. | 5956. | 0. | 0. | 0. | .73 | 65. | 22.1 | C | 19.2 | 14.0 | * |
| * | 18 | 3 | 200. | 0. | 0. | 4319. | 0. | 0. | 4319. | 6000. | 0. | 0. | 0. | .72 | 65. | 22.1 | C | 19.2 | 14.0 | * |
| * | 19 | 3 | 1400. | 0. | 272. | 4319. | 0. | 272. | 4319. | 5961. | 0. | 0. | 0. | .72 | 65. | 22.1 | C | 19.2 | 14.0 | * |
| * | 20 | 3 | 900. | 0. | 0. | 4047. | 0. | 0. | 4047. | 6000. | 0. | 0. | 0. | .67 | 65. | 20.8 | C | 19.2 | 14.0 | * |
| * | 21 | 4 | 100. | 158. | 0. | 4205. | 158. | 0. | 4205. | 6098. | 0. | 0. | 0. | .69 | 65. | 16.2 | B | 19.2 | 14.0 | * |
| * | 22 | 4 | 100. | 0. | 71. | 4205. | 0. | 71. | 4205. | 6120. | 0. | 0. | 0. | .69 | 65. | 16.2 | B | 19.2 | 14.0 | * |
| * | 23 | 3 | 600. | 0. | 0. | 4134. | 0. | 0. | 4134. | 6000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 19.2 | 14.0 | * |
| * | 24 | 3 | 1500. | 423. | 0. | 4557. | 423. | 0. | 4557. | 5913. | 0. | 0. | 0. | .77 | 64. | 23.8 | C | 19.7 | 13.6 | * |
| * | 25 | 3 | 1500. | 0. | 0. | 4557. | 0. | 0. | 4557. | 6000. | 0. | 0. | 0. | .76 | 64. | 23.7 | C | 19.6 | 13.7 | * |
| * | 26 | 3 | 8000. | 0. | 0. | 4557. | 0. | 0. | 4557. | 6000. | 0. | 0. | 0. | .76 | 64. | 23.7 | C | 19.6 | 13.7 | * |
| * | 27 | 5 | 100. | 933. | 0. | 5490. | 933. | 0. | 5490. | 10000. | 0. | 0. | 0. | .55 | 65. | 16.9 | B | 19.2 | 14.0 | * |
| * | 28 | 5 | 1000. | 0. | 0. | 5490. | 0. | 0. | 5490. | 7750. | 0. | 0. | 0. | .71 | 65. | 16.9 | B | 19.2 | 14.0 | * |
| * | 29 | 5 | 1000. | 0. | 5490. | 5490. | 0. | 5490. | 5490. | 9685. | 0. | 0. | 0. | .57 | 65. | 16.9 | B | 19.2 | 14.0 | * |
| * | ***** | | | | | | | | | | | | | | | | | | | |
| * | * TOTAL 135469. = 25.7 MILES MAX(V/C) = 0.82 LOWEST LOS = C AVG = 64. 23.9 19.6 13.7 * | | | | | | | | | | | | | | | | | | | |
| * | ***** | | | | | | | | | | | | | | | | | | | |

| CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | | |
|----------------------------|---------|-----------|---------|-------------------|---------|-----------|---------|----------|
| FREEWAY TRAVEL TIME = | 1882. | VEH-HRS | 1891. | PASS-HRS | 1882. | VEH-HRS | 1891. | PASS-HRS |
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1882. | VEH-HRS | 1891. | PASS-HRS | 1882. | VEH-HRS | 1891. | PASS-HRS |
| TOTAL TRAV DISTANCE = | 120606. | VEH-MI. | 121251. | PASS-MI. | 120606. | VEH-MI. | 121251. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 64. | MPH. | | | 64. | MPH. | | |
| AVERAGE DENSITY = | 24. | VPMP | | | 24. | VPMP | | |
| TOTAL FUEL = | 6163. | GALLONS | | | 6163. | GALLONS | | |
| TOTAL EMISSIONS = | 1652. | KILOGRAMS | | | 1652. | KILOGRAMS | | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 20.65 | 3 | 0.92 | 4 | 0.20 | 5 | 0.24 |
| 6 | 0.88 | 7 | 0.85 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.37 | 25 | 0.30 |
| 26 | 1.62 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 26.0 VEH-HRS ***** AVERAGE DELAY = 0.33 MIN/VEH *****

 ** FREEWAY TRAVEL TIME (MINUTES) **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN *
 * 1 2 3 4 5 6 *

 * * *
 * * *
 * 1 * 0.24 21.74 22.05 22.92 23.12 25.84 *
 * 2 * 0.00 0.65 0.96 1.83 2.03 4.75 *
 * 3 * 0.00 0.00 0.18 1.05 1.25 3.97 *
 * 4 * 0.00 0.00 0.00 0.74 0.94 3.66 *
 * 5 * 0.00 0.00 0.00 0.58 0.78 3.50 *
 * 6 * 0.00 0.00 0.00 0.00 0.03 2.76 *
 * 7 * 0.00 0.00 0.00 0.00 0.00 2.61 *
 * 8 * 0.00 0.00 0.00 0.00 0.00 0.37 *

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* 9 * 0.00 0.00 0.00 0.00 0.00 0.35 *
 * 10 * 0.00 0.00 0.00 0.00 0.00 0.17 *
 * * * * *

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | |
|-----------|--------|------------|----------------|----------------|----------------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|------|------|
| * SEC | * LNS | * LENGTH | * ORG DES SSEC | * ORG DES SSEC | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP/L | * LEVEL | * MPG | * GS/VM | | |
| * 1 | 5 | 1370. | 6681. | 1136. | 6681. | 6681. | 1136. | 6681. | 10000. | 0. | 0. | .67 | 65. | 20.6 | C | 19.2 | 14.0 |
| * 2 | 3 | 99999. | 0. | 0. | 5545. | 0. | 0. | 5545. | 6226. | 0. | 0. | .89 | 60. | 31.0 | D | 21.7 | 12.3 |
| * 3 | 3 | 2740. | 0. | 0. | 5545. | 0. | 0. | 5545. | 6000. | 0. | 0. | .92 | 58. | 32.0 | D | 22.3 | 11.9 |
| * 4 | 3 | 600. | 0. | 0. | 5545. | 0. | 0. | 5545. | 6000. | 0. | 0. | .92 | 58. | 32.0 | D | 22.3 | 11.9 |
| * 5 | 3 | 700. | 0. | 0. | 5545. | 0. | 0. | 5545. | 6000. | 0. | 0. | .92 | 58. | 32.0 | D | 22.3 | 11.9 |
| * 6 | 3 | 2630. | 0. | 0. | 5545. | 0. | 0. | 5545. | 6000. | 0. | 0. | .92 | 58. | 32.0 | D | 22.3 | 11.9 |
| * 7 | 3 | 2530. | 0. | 0. | 5545. | 0. | 0. | 5545. | 6000. | 0. | 0. | .92 | 58. | 32.0 | D | 22.3 | 11.9 |
| * 8 | 4 | 1500. | 212. | 0. | 5757. | 212. | 0. | 5757. | 6213. | 0. | 0. | .93 | 65. | 22.1 | C | 19.2 | 14.0 |
| * 9 | 4 | 700. | 0. | 0. | 5757. | 0. | 0. | 5757. | 6240. | 0. | 0. | .92 | 65. | 22.1 | C | 19.2 | 14.0 |
| * 10 | 4 | 1500. | 0. | 1597. | 5757. | 0. | 1597. | 5757. | 5927. | 0. | 0. | .97 | 65. | 22.1 | C | 19.2 | 14.0 |
| * 11 | 3 | 750. | 0. | 0. | 4160. | 0. | 0. | 4160. | 6000. | 0. | 0. | .69 | 65. | 21.3 | C | 19.2 | 14.0 |
| * 12 | 4 | 350. | 1079. | 0. | 5239. | 1079. | 0. | 5239. | 6219. | 0. | 0. | .84 | 65. | 20.1 | C | 19.2 | 14.0 |
| * 13 | 4 | 350. | 0. | 0. | 5239. | 0. | 0. | 5239. | 6410. | 0. | 0. | .82 | 65. | 20.1 | C | 19.2 | 14.0 |
| * 14 | 4 | 350. | 0. | 356. | 5239. | 0. | 356. | 5239. | 6356. | 0. | 0. | .82 | 65. | 20.1 | C | 19.2 | 14.0 |
| * 15 | 3 | 700. | 0. | 0. | 4883. | 0. | 0. | 4883. | 6000. | 0. | 0. | .81 | 63. | 25.9 | C | 20.2 | 13.2 |
| * 16 | 3 | 900. | 106. | 0. | 4989. | 106. | 0. | 4989. | 5980. | 0. | 0. | .83 | 62. | 26.8 | D | 20.5 | 13.0 |
| * 17 | 3 | 1400. | 362. | 0. | 5351. | 362. | 0. | 5351. | 5930. | 0. | 0. | .90 | 59. | 30.2 | D | 21.9 | 12.1 |
| * 18 | 3 | 200. | 0. | 0. | 5351. | 0. | 0. | 5351. | 6000. | 0. | 0. | .89 | 60. | 29.9 | D | 21.7 | 12.2 |
| * 19 | 3 | 1400. | 0. | 202. | 5351. | 0. | 202. | 5351. | 5972. | 0. | 0. | .90 | 59. | 30.0 | D | 21.8 | 12.2 |
| * 20 | 3 | 900. | 0. | 0. | 5149. | 0. | 0. | 5149. | 6000. | 0. | 0. | .86 | 61. | 28.1 | D | 21.0 | 12.7 |
| * 21 | 4 | 100. | 208. | 0. | 5357. | 208. | 0. | 5357. | 6088. | 0. | 0. | .88 | 65. | 20.6 | C | 19.2 | 14.0 |
| * 22 | 4 | 100. | 0. | 113. | 5357. | 0. | 113. | 5357. | 6115. | 0. | 0. | .88 | 65. | 20.6 | C | 19.2 | 14.0 |
| * 23 | 3 | 600. | 0. | 0. | 5244. | 0. | 0. | 5244. | 6000. | 0. | 0. | .87 | 60. | 28.9 | D | 21.4 | 12.5 |
| * 24 | 3 | 1500. | 473. | 0. | 5717. | 473. | 0. | 5717. | 5903. | 0. | 0. | .97 | 55. | 34.8 | D | 23.2 | 11.4 |
| * 25 | 3 | 1500. | 0. | 0. | 5717. | 0. | 0. | 5717. | 6000. | 0. | 0. | .95 | 56. | 34.1 | D | 22.9 | 11.5 |
| * 26 | 3 | 8000. | 0. | 0. | 5717. | 0. | 0. | 5717. | 6000. | 0. | 0. | .95 | 56. | 34.1 | D | 22.9 | 11.5 |
| * 27 | 5 | 100. | 1171. | 0. | 6888. | 1171. | 0. | 6888. | 10000. | 0. | 0. | .69 | 65. | 21.2 | C | 19.2 | 14.0 |
| * 28 | 5 | 1000. | 0. | 0. | 6888. | 0. | 0. | 6888. | 7750. | 0. | 0. | .89 | 65. | 21.2 | C | 19.2 | 14.0 |
| * 29 | 5 | 1000. | 0. | 6888. | 6888. | 0. | 6888. | 6888. | 9685. | 0. | 0. | .71 | 65. | 21.2 | C | 19.2 | 14.0 |

 * TOTAL 135469. = 25.7 MILES MAX(V/C) = 0.97 LOWEST LOS = D AVG = 60. 30.6 21.6 12.3 *

| CURRENT TIME SLICE | | | CUMULATIVE VALUES | | |
|----------------------------|------------------|------------------|-------------------|------------------|--|
| FREWAY TRAVEL TIME = | 2399. VEH-HRS | 2412. PASS-HRS | 4281. VEH-HRS | 4303. PASS-HRS | |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | |
| TOTAL SYSTEM TRAVEL TIME = | 2399. VEH-HRS | 2412. PASS-HRS | 4281. VEH-HRS | 4303. PASS-HRS | |
| TOTAL TRAV DISTANCE = | 142945. VEH-MI. | 143733. PASS-MI. | 263550. VEH-MI. | 264984. PASS-MI. | |
| AVERAGE SYSTEM SPEED = | 60. MPH. | | 62. MPH. | | |
| AVERAGE DENSITY = | 31. VPMP/L | | 27. VPMP/L | | |
| TOTAL FUEL = | 6611. GALLONS | | 12773. GALLONS | | |
| TOTAL EMISSIONS = | 1760. KI LOGRAMS | | 3412. KI LOGRAMS | | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|--------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 144.31 | 3 | 5.51 | 4 | 1.21 | 5 | 1.41 |
| 6 | 5.29 | 7 | 5.09 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.36 |
| 16 | 0.62 | 17 | 2.20 | 18 | 0.28 | 19 | 2.06 | 20 | 0.85 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.69 | 24 | 4.66 | 25 | 4.06 |
| 26 | 21.64 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 200.2 VEH-HRS ***** AVERAGE DELAY = 2.16 MIN/VEH *****

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FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP LLL
FFFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 1111111 222222222 PPP LLLLLLLLLL
    
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FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 2 AND 26 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65 MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

FREeway AND ARTERIAL DESIGN FEATURES

| ** SUB NO. | ** SSEC | ** SSEC | ** DESIGN | ** ORG | ** TRK | ** SSEC | ** PCT | ** PCT | ** DES | ** SPECIAL | ** FF.SPD. | ** CAP. | ** ART | ** GRADE | ** SUBSECTION | ** LOCATION | ** |
|------------|---------|---------|-----------|--------|--------|---------|--------|-----------|---------|-------------|-------------|-------------|---------|-------------|-------------------------|-------------|----|
| ** SEC | ** LNS | ** CAP | ** LENGTH | ** DES | ** FAC | ** GRAD | ** TRK | ** TRUCKS | ** RAMP | ** ALT. RTE | ** ALT. RTE | ** ALT. RTE | ** TYPE | ** ALT. RTE | ** | ** | ** |
| ** 1 | | | | | | | | | | | | | | | | | ** |
| ** 2 | 1 | 1650. | 99999. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | | ** |
| ** 3 | 1 | 1650. | 2740. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-85 Off to Shore On | | ** |
| ** 4 | 1 | 1650. | 600. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Shore. On to Moffet Off | | ** |
| ** 5 | 1 | 1650. | 700. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Moffett Off to On | | ** |
| ** 6 | 1 | 1650. | 2630. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Moffett On to Ellis Off | | ** |
| ** 7 | 1 | 1650. | 2530. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Ellis Off to On-ramp | | ** |
| ** 8 | 1 | 1650. | 1500. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Ellis On-ramp | | ** |
| ** 9 | 1 | 1650. | 700. | 65 | | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Ellis / US 237 | | ** |
| ** 10 | 1 | 1650. | 1500. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 EB Off-Ramp | | ** |
| ** 11 | 1 | 1650. | 750. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 / SR-237 | | ** |
| ** 12 | 1 | 1650. | 350. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 EB On-Ramp | | ** |
| ** 13 | 1 | 1650. | 350. | 65 | | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | US 237 / Mathilda | | ** |
| ** 14 | 1 | 1650. | 350. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-Ramp | | ** |
| ** 15 | 1 | 1650. | 700. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | | ** |
| ** 16 | 1 | 1650. | 900. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda SB On-Ramp | | ** |
| ** 17 | 1 | 1650. | 1400. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda NB On-Ramp | | ** |
| ** 18 | 1 | 1650. | 200. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Fair Oaks | | ** |
| ** 19 | 1 | 1650. | 1400. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks SB Off-Ramp | | ** |

** 20 1 1650. 900. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks SB/ Fair Oaks **

FREEWAY AND ARTERIAL DESIGN FEATURES

Table with columns: SUB NO., SEC LNS, SSEC CAP, SSEC LENGTH, DESIGN SPEED, ORG DES, TRK FAC, SSEC GRAD, PCT TRK, PCT TRUCKS, SPECIAL RAMP, FF. SPD. ALT. RTE, CAP. ALT. RTE, ART TYPE, GRADE ALT. RTE, SUBSECTION, LOCATION. Rows 21-29.

FREEWAY TRAVEL TIME (MINUTES)

Table with columns: ORIGINS DOWN, DESTINATIONS ACROSS (1-7). Rows 1-11.

TIME SLICE FREEWAY PERFORMANCE TABLE

| US-101_SB_AM_NP_2018_PL.txt | | | | | | | | | | | | | | | | | |
|---------------------------------|------------------|-------|------|-------|-------|---------|---------|-----------------|----------------|-----------|-------|------|--------|-------|-----|-------|------|
| * SUB NO. SSEC O-D DATA DEMANDS | ADJUSTED VOLUMES | | | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS | * | | | |
| * SEC LNS LENGTH | ORG | DES | SSEC | ORG | DES | SSEC | CAP. | EFF | LENGTH | RATE | RATIO | MPH | VPMP | LEVEL | MPG | GS/VM | * |
| * 1 | | | | | | | | | | | | | | | | | |
| * 2 | 1 | 99999 | 967. | 0. | 967. | 967. | 0. | 967. | 1650. | 0. | 0. | .59 | 65. | 14.9 | B | 20.0 | 13.7 |
| * 3 | 1 | 2740. | 0. | 0. | 967. | 0. | 0. | 967. | 1650. | 0. | 0. | .59 | 65. | 14.9 | B | 20.0 | 13.7 |
| * 4 | 1 | 600. | 0. | 0. | 967. | 0. | 0. | 967. | 1650. | 0. | 0. | .59 | 65. | 14.9 | B | 20.0 | 13.7 |
| * 5 | 1 | 700. | 0. | 0. | 967. | 0. | 0. | 967. | 1650. | 0. | 0. | .59 | 65. | 14.9 | B | 20.0 | 13.7 |
| * 6 | 1 | 2630. | 0. | 0. | 967. | 0. | 0. | 967. | 1650. | 0. | 0. | .59 | 65. | 14.9 | B | 20.0 | 13.7 |
| * 7 | 1 | 2530. | 0. | 0. | 967. | 0. | 0. | 967. | 1650. | 0. | 0. | .59 | 65. | 14.9 | B | 20.0 | 13.7 |
| * 8 | 1 | 1500. | 20. | 0. | 988. | 20. | 0. | 988. | 1650. | 0. | 0. | .60 | 65. | 15.2 | B | 20.0 | 13.7 |
| * 9 | 1 | 700. | 0. | 0. | 988. | 0. | 0. | 988. | 1650. | 0. | 0. | .60 | 65. | 15.2 | B | 20.0 | 13.7 |
| * 10 | 1 | 1500. | 0. | 275. | 988. | 0. | 275. | 988. | 1650. | 0. | 0. | .60 | 65. | 15.2 | B | 20.0 | 13.7 |
| * 11 | 1 | 750. | 0. | 0. | 713. | 0. | 0. | 713. | 1650. | 0. | 0. | .43 | 65. | 11.0 | A | 20.0 | 13.7 |
| * 12 | 1 | 350. | 133. | 0. | 846. | 133. | 0. | 846. | 1650. | 0. | 0. | .51 | 65. | 13.0 | B | 20.0 | 13.7 |
| * 13 | 1 | 350. | 0. | 0. | 846. | 0. | 0. | 846. | 1650. | 0. | 0. | .51 | 65. | 13.0 | B | 20.0 | 13.7 |
| * 14 | 1 | 350. | 0. | 43. | 846. | 0. | 43. | 846. | 1650. | 0. | 0. | .51 | 65. | 13.0 | B | 20.0 | 13.7 |
| * 15 | 1 | 700. | 0. | 0. | 803. | 0. | 0. | 803. | 1650. | 0. | 0. | .49 | 65. | 12.3 | B | 20.0 | 13.7 |
| * 16 | 1 | 900. | 17. | 0. | 820. | 17. | 0. | 820. | 1650. | 0. | 0. | .50 | 65. | 12.6 | B | 20.0 | 13.7 |
| * 17 | 1 | 1400. | 44. | 0. | 864. | 44. | 0. | 864. | 1650. | 0. | 0. | .52 | 65. | 13.3 | B | 20.0 | 13.7 |
| * 18 | 1 | 200. | 0. | 0. | 864. | 0. | 0. | 864. | 1650. | 0. | 0. | .52 | 65. | 13.3 | B | 20.0 | 13.7 |
| * 19 | 1 | 1400. | 0. | 39. | 864. | 0. | 39. | 864. | 1650. | 0. | 0. | .52 | 65. | 13.3 | B | 20.0 | 13.7 |
| * 20 | 1 | 900. | 0. | 0. | 825. | 0. | 0. | 825. | 1650. | 0. | 0. | .50 | 65. | 12.7 | B | 20.0 | 13.7 |
| * 21 | 1 | 100. | 32. | 0. | 857. | 32. | 0. | 857. | 1650. | 0. | 0. | .52 | 65. | 13.2 | B | 20.0 | 13.7 |
| * 22 | 1 | 100. | 0. | 10. | 857. | 0. | 10. | 857. | 1650. | 0. | 0. | .52 | 65. | 13.2 | B | 20.0 | 13.7 |
| * 23 | 1 | 600. | 0. | 0. | 847. | 0. | 0. | 847. | 1650. | 0. | 0. | .51 | 65. | 13.0 | B | 20.0 | 13.7 |
| * 24 | 1 | 1500. | 87. | 0. | 933. | 87. | 0. | 933. | 1650. | 0. | 0. | .57 | 65. | 14.4 | B | 20.0 | 13.7 |
| * 25 | 1 | 1500. | 0. | 0. | 933. | 0. | 0. | 933. | 1650. | 0. | 0. | .57 | 65. | 14.4 | B | 20.0 | 13.7 |
| * 26 | 1 | 8000. | 0. | 933. | 933. | 0. | 933. | 933. | 1650. | 0. | 0. | .57 | 65. | 14.4 | B | 20.0 | 13.7 |
| * 27 | | | | | | | | | | | | | | | | | |
| * 28 | | | | | | | | | | | | | | | | | |
| * 29 | | | | | | | | | | | | | | | | | |
| ***** | | | | | | | | | | | | | | | | | |
| * TOTAL | 131999. | = | 25.0 | MILES | | | | MAX(V/C) = 0.60 | LOWEST LOS = B | AVG = 65. | 14.7 | 20.0 | 13.7 | | | | |
| ***** | | | | | | | | | | | | | | | | | |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 13:22 PAGE 6
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 1 OF 2

| | CURRENT TIME SLICE | | | CUMULATIVE VALUES | | | | |
|-----------------------------|--------------------|------------|--------|-------------------|--------|------------|--------|----------|
| FREWAY TRAVEL TIME = | 368. | VEH-HRS | 736. | PASS-HRS | 368. | VEH-HRS | 736. | PASS-HRS |
| FREWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 368. | VEH-HRS | 736. | PASS-HRS | 368. | VEH-HRS | 736. | PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 23922. | VEH-MI. | 47843. | PASS-MI. | 23922. | VEH-MI. | 47843. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 65. | MPH. | | | 65. | MPH. | | |
| AVERAGE DENSITY = | 15. | VPMP | | | 15. | VPMP | | |
| TOTAL FUEL = | 1196. | GALLONS | | | 1196. | GALLONS | | |
| TOTAL EMISSIONS = | 329. | KI LOGRAMS | | | 329. | KI LOGRAMS | | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 13:22 PAGE 7
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 2

 ** FREWAY TRAVEL TIME (MI MINUTES) **

| * ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | |
|----------------|---------------------|-------|-------|-------|-------|-------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 19.74 | 20.05 | 20.86 | 21.05 | 23.08 | 0.00 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 1.96 | 3.99 | 0.00 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.21 | 0.00 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.90 | 0.00 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.74 | 0.00 |

| | | | | | | | | | | | | | | | | | | | | |
|---|----|---|------|------|------|------|------|------|------|------|--|--|--|--|--|--|--|--|--|---|
| * | 7 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.06 | 0.00 | | | | | | | | | | * |
| * | 8 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.92 | 0.00 | | | | | | | | | | * |
| * | 9 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | | | | | | | | | * |
| * | 10 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | | | | | | | | | * |
| * | 11 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | | | | | | | | | * |
| * | * | * | | | | | | | | | | | | | | | | | | * |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | | |
|-----------|--------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|-----------------|----------------|-----------|---------|--------|-------------|---------|-------|---------|--|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | |
| * 1 | | | | | | | | | | | | | | | | | | | |
| * 2 | 1 | 99999 | 1136 | 0 | 1136 | 1136 | 0 | 1136 | 1650 | 0 | 0 | 0 | .69 | 65 | 17.5 | B | 20.0 | 13.7 | |
| * 3 | 1 | 2740 | 0 | 0 | 1136 | 0 | 0 | 1136 | 1650 | 0 | 0 | 0 | .69 | 65 | 17.5 | B | 20.0 | 13.7 | |
| * 4 | 1 | 600 | 0 | 0 | 1136 | 0 | 0 | 1136 | 1650 | 0 | 0 | 0 | .69 | 65 | 17.5 | B | 20.0 | 13.7 | |
| * 5 | 1 | 700 | 0 | 0 | 1136 | 0 | 0 | 1136 | 1650 | 0 | 0 | 0 | .69 | 65 | 17.5 | B | 20.0 | 13.7 | |
| * 6 | 1 | 2630 | 0 | 0 | 1136 | 0 | 0 | 1136 | 1650 | 0 | 0 | 0 | .69 | 65 | 17.5 | B | 20.0 | 13.7 | |
| * 7 | 1 | 2530 | 0 | 0 | 1136 | 0 | 0 | 1136 | 1650 | 0 | 0 | 0 | .69 | 65 | 17.5 | B | 20.0 | 13.7 | |
| * 8 | 1 | 1500 | 27 | 0 | 1162 | 27 | 0 | 1162 | 1650 | 0 | 0 | 0 | .70 | 65 | 17.9 | B | 20.0 | 13.7 | |
| * 9 | 1 | 700 | 0 | 0 | 1162 | 0 | 0 | 1162 | 1650 | 0 | 0 | 0 | .70 | 65 | 17.9 | B | 20.0 | 13.7 | |
| * 10 | 1 | 1500 | 0 | 313 | 1162 | 0 | 313 | 1162 | 1650 | 0 | 0 | 0 | .70 | 65 | 17.9 | B | 20.0 | 13.7 | |
| * 11 | 1 | 750 | 0 | 0 | 849 | 0 | 0 | 849 | 1650 | 0 | 0 | 0 | .51 | 65 | 13.1 | B | 20.0 | 13.7 | |
| * 12 | 1 | 350 | 191 | 0 | 1040 | 191 | 0 | 1040 | 1650 | 0 | 0 | 0 | .63 | 65 | 16.0 | B | 20.0 | 13.7 | |
| * 13 | 1 | 350 | 0 | 0 | 1040 | 0 | 0 | 1040 | 1650 | 0 | 0 | 0 | .63 | 65 | 16.0 | B | 20.0 | 13.7 | |
| * 14 | 1 | 350 | 0 | 54 | 1040 | 0 | 54 | 1040 | 1650 | 0 | 0 | 0 | .63 | 65 | 16.0 | B | 20.0 | 13.7 | |
| * 15 | 1 | 700 | 0 | 0 | 986 | 0 | 0 | 986 | 1650 | 0 | 0 | 0 | .60 | 65 | 15.2 | B | 20.0 | 13.7 | |
| * 16 | 1 | 900 | 20 | 0 | 1006 | 20 | 0 | 1006 | 1650 | 0 | 0 | 0 | .61 | 65 | 15.5 | B | 20.0 | 13.7 | |
| * 17 | 1 | 1400 | 70 | 0 | 1076 | 70 | 0 | 1076 | 1650 | 0 | 0 | 0 | .65 | 65 | 16.5 | B | 20.0 | 13.7 | |
| * 18 | 1 | 200 | 0 | 0 | 1076 | 0 | 0 | 1076 | 1650 | 0 | 0 | 0 | .65 | 65 | 16.5 | B | 20.0 | 13.7 | |
| * 19 | 1 | 1400 | 0 | 28 | 1076 | 0 | 28 | 1076 | 1650 | 0 | 0 | 0 | .65 | 65 | 16.5 | B | 20.0 | 13.7 | |
| * 20 | 1 | 900 | 0 | 0 | 1048 | 0 | 0 | 1048 | 1650 | 0 | 0 | 0 | .64 | 65 | 16.1 | B | 20.0 | 13.7 | |
| * 21 | 1 | 100 | 42 | 0 | 1090 | 42 | 0 | 1090 | 1650 | 0 | 0 | 0 | .66 | 65 | 16.8 | B | 20.0 | 13.7 | |
| * 22 | 1 | 100 | 0 | 15 | 1090 | 0 | 15 | 1090 | 1650 | 0 | 0 | 0 | .66 | 65 | 16.8 | B | 20.0 | 13.7 | |
| * 23 | 1 | 600 | 0 | 0 | 1074 | 0 | 0 | 1074 | 1650 | 0 | 0 | 0 | .65 | 65 | 16.5 | B | 20.0 | 13.7 | |
| * 24 | 1 | 1500 | 97 | 0 | 1171 | 97 | 0 | 1171 | 1650 | 0 | 0 | 0 | .71 | 65 | 18.0 | C | 20.0 | 13.7 | |
| * 25 | 1 | 1500 | 0 | 0 | 1171 | 0 | 0 | 1171 | 1650 | 0 | 0 | 0 | .71 | 65 | 18.0 | C | 20.0 | 13.7 | |
| * 26 | 1 | 8000 | 0 | 1171 | 1171 | 0 | 1171 | 1171 | 1650 | 0 | 0 | 0 | .71 | 65 | 18.0 | C | 20.0 | 13.7 | |
| * 27 | | | | | | | | | | | | | | | | | | | |
| * 28 | | | | | | | | | | | | | | | | | | | |
| * 29 | | | | | | | | | | | | | | | | | | | |
| * TOTAL | 131999 | = | 25.0 | MILES | | | | | | MAX(V/C) = 0.71 | LOWEST LOS = C | AVG = 65 | 17.4 | 20.0 | 13.7 | | | | |

| FREQUENCY | | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|------------------|-------------------------|--------------------|------------|-------------------|------------|
| FREQUENCY | TRAVEL TIME = | 436 | VEH-HRS | 872 | PASS-HRS |
| FREQUENCY | MERGE DELAY = | 0 | VEH-HRS | 0 | PASS-HRS |
| FREQUENCY | ON-RAMP MRG/CAP DELAY = | 0 | VEH-HRS | 0 | PASS-HRS |
| FREQUENCY | OFF-RAMP DELAY = | 0 | VEH-HRS | 0 | PASS-HRS |
| TOTAL SYSTEM | TRAVEL TIME = | 436 | VEH-HRS | 872 | PASS-HRS |
| TOTAL FRWAY TRAV | DI STANCE = | 28327 | VEH-MI | 56653 | PASS-MI |
| AVERAGE SYSTEM | SPEED = | 65 | MPH | 65 | MPH |
| AVERAGE DENSITY | = | 17 | VPMP | 16 | VPMP |
| TOTAL FUEL | = | 1416 | GALLONS | 2612 | GALLONS |
| TOTAL EMISSIONS | = | 389 | KI LOGRAMS | 718 | KI LOGRAMS |

| ***** MAINLINE DELAY (VEH-HRS) ***** | | ***** DESIRED SPEED = 65.0 ***** | | | | | | | |
|--------------------------------------|-------|----------------------------------|-----------------------|------------|---------|------------|-------|------------|-------|
| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |
| ***** TOTAL DELAY = | 0.0 | VEH-HRS | ***** AVERAGE DELAY = | 0.00 | MIN/VEH | ***** | | | |

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP EEE
FFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 2222222222 PPP PPP EEEEEEEEE

FREQ12PEB

- 1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
- 2. THERE ARE 1.0 TIME SLICES PER HOUR.
- 3. WEAVING ANALYSIS IS NOT ENGAGED.
- 4. NO ALTERNATE ROUTE IS PROVIDED.
- 5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
- 6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
- 7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
- 8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
- 9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
- 10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREEWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SEC | LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT DES TRUCKS | SPECIAL RAMP | FF. SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION | LOCATION |
|---------|-----|--------|----------|-------------|--------------|---------|---------|-----------|---------|----------------|--------------|-------------------|---------------|----------|-------------------------|------------|----------|
| 1 | 5 | 10000. | 1370. | 65 | OD | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Seeding | | |
| 2 | 3 | 6226. | 99999. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | | |
| 3 | 3 | 6000. | 2740. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-85 Off to Shore On | | |
| 4 | 3 | 6000. | 600. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Shore. On to Moffet Off | | |
| 5 | 3 | 6000. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Moffett Off to On | | |
| 6 | 3 | 6000. | 2630. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Moffett On to Ellis Off | | |
| 7 | 3 | 6000. | 2530. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Ellis Off to On-ramp | | |
| 8 | 4 | 6240. | 1500. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Ellis On-ramp | | |
| 9 | 4 | 6240. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Ellis / US 237 | | |
| 10 | 4 | 6240. | 1500. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 EB Off-Ramp | | |
| 11 | 3 | 6000. | 750. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 / SR-237 | | |
| 12 | 4 | 6690. | 350. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 EB On-Ramp | | |
| 13 | 4 | 6690. | 350. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US 237 / Mathilda | | |
| 14 | 4 | 6690. | 350. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-Ramp | | |
| 15 | 3 | 6000. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | | |
| 16 | 3 | 6000. | 900. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda SB On-Ramp | | |
| 17 | 3 | 6000. | 1400. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda NB On-Ramp | | |
| 18 | 3 | 6000. | 200. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Fair Oaks | | |
| 19 | 3 | 6000. | 1400. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks SB Off-Ramp | | |
| 20 | 3 | 6000. | 900. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks SB/ Fair Oaks | | |

FREeway AND ARTERIAL DESIGN FEATURES

| SUB NO. SEC LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT TRUCKS | DES RAMP | SPECIAL | FF. SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION | LOCATION |
|-----------------|----------|-------------|--------------|---------|---------|-----------|---------|------------|----------|---------|-------------------|---------------|----------|----------------|------------------|-----------|
| ** 21 | 4 | 6130. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Fair Oaks SB | On-Ramp |
| ** 22 | 4 | 6130. | 100. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks NB | Off-Ramp |
| ** 23 | 3 | 6000. | 600. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks NB/ | Fair Oaks |
| ** 24 | 3 | 6000. | 1500. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Oaks On-Ramp to | Mid |
| ** 25 | 3 | 6000. | 1500. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mid to Lawrence | Off-ramp |
| ** 26 | 3 | 6000. | 8000. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | |
| ** 27 | 5 | 10000. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | |
| ** 28 | 5 | 7750. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Dummy Bottleneck | |
| ** 29 | 5 | 9685. | 1000. | 65 | 0D | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | End of Network | |

***** INPUT HAS BEEN COMPLETED *****

FREeway TRAVEL TIME (MINUTES)

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | |
|--------------|---------------------|-------|-------|-------|-------|-------|
| | 1 | 2 | 3 | 4 | 5 | 6 |
| * 1 * | 0.24 | 20.28 | 20.59 | 21.40 | 21.60 | 24.03 |
| * 2 * | 0.00 | 0.65 | 0.96 | 1.77 | 1.96 | 4.40 |
| * 3 * | 0.00 | 0.00 | 0.18 | 0.99 | 1.19 | 3.62 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.69 | 0.88 | 3.31 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.53 | 0.72 | 3.15 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.03 | 2.47 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.33 |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.37 |
| * 9 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.35 |
| * 10 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 |

TIME SLICE FREeway PERFORMANCE TABLE

| SUB NO. SEC LNS | SSEC LENGTH | O-D DATA ORG DES | DEMANDS SSEC | ADJUSTED VOLUMES ORG DES SSEC | SSEC CAP. | WEAVE EFF | CONGEST LENGTH | STORAGE RATE | V/C RATIO | SPEED MPH | DENSITY VPMPL | LOS LEVEL | FUEL MPG | EMI SS GS/VM |
|-----------------|-------------|------------------|--------------|-------------------------------|-----------|------------|----------------|--------------|-----------|-----------|---------------|-----------|----------|--------------|
| * 1 | 5 | 1370. | 5690. | 967. 5690. | 5690. | 967. 5690. | 10000. | 0. | 0. | 0. | .57 | 65. | 17.5 | B 19.2 14.0 |

US-101_SB_AM_P1_2018_PE.txt

| | | | | | | | | | | | | | | | | | | | | |
|-------|-------|---|--------|---------|-------|-------|-------|-------|-------|--------|----|----|----|-----|-----|------|---|------|------|---|
| * | 2 | 3 | 99999. | 0. | 0. | 4723. | 0. | 0. | 4723. | 6226. | 0. | 0. | 0. | .76 | 64. | 24.6 | C | 19.6 | 13.7 | * |
| * | 3 | 3 | 2740. | 0. | 0. | 4723. | 0. | 0. | 4723. | 6000. | 0. | 0. | 0. | .79 | 63. | 24.8 | C | 19.9 | 13.5 | * |
| * | 4 | 3 | 600. | 0. | 0. | 4723. | 0. | 0. | 4723. | 6000. | 0. | 0. | 0. | .79 | 63. | 24.8 | C | 19.9 | 13.5 | * |
| * | 5 | 3 | 700. | 0. | 0. | 4723. | 0. | 0. | 4723. | 6000. | 0. | 0. | 0. | .79 | 63. | 24.8 | C | 19.9 | 13.5 | * |
| * | 6 | 3 | 2630. | 0. | 0. | 4723. | 0. | 0. | 4723. | 6000. | 0. | 0. | 0. | .79 | 63. | 24.8 | C | 19.9 | 13.5 | * |
| * | 7 | 3 | 2530. | 0. | 0. | 4723. | 0. | 0. | 4723. | 6000. | 0. | 0. | 0. | .79 | 63. | 24.8 | C | 19.9 | 13.5 | * |
| * | 8 | 4 | 1500. | 171. | 0. | 4894. | 171. | 0. | 4894. | 6219. | 0. | 0. | 0. | .79 | 65. | 18.8 | C | 19.2 | 14.0 | * |
| * | 9 | 4 | 700. | 0. | 0. | 4894. | 0. | 0. | 4894. | 6240. | 0. | 0. | 0. | .78 | 65. | 18.8 | C | 19.2 | 14.0 | * |
| * | 10 | 4 | 1500. | 0. | 1229. | 4894. | 0. | 1229. | 4894. | 5998. | 0. | 0. | 0. | .82 | 65. | 18.8 | C | 19.2 | 14.0 | * |
| * | 11 | 3 | 750. | 0. | 0. | 3665. | 0. | 0. | 3665. | 6000. | 0. | 0. | 0. | .61 | 65. | 18.8 | C | 19.2 | 14.0 | * |
| * | 12 | 4 | 350. | 772. | 0. | 4437. | 772. | 0. | 4437. | 6562. | 0. | 0. | 0. | .68 | 65. | 17.1 | B | 19.2 | 14.0 | * |
| * | 13 | 4 | 350. | 0. | 0. | 4437. | 0. | 0. | 4437. | 6690. | 0. | 0. | 0. | .66 | 65. | 17.1 | B | 19.2 | 14.0 | * |
| * | 14 | 4 | 350. | 0. | 449. | 4437. | 0. | 449. | 4437. | 6619. | 0. | 0. | 0. | .67 | 65. | 17.1 | B | 19.2 | 14.0 | * |
| * | 15 | 3 | 700. | 0. | 0. | 3988. | 0. | 0. | 3988. | 6000. | 0. | 0. | 0. | .66 | 65. | 20.5 | C | 19.2 | 14.0 | * |
| * | 16 | 3 | 900. | 93. | 0. | 4081. | 93. | 0. | 4081. | 5983. | 0. | 0. | 0. | .68 | 65. | 20.9 | C | 19.2 | 14.0 | * |
| * | 17 | 3 | 1400. | 312. | 0. | 4393. | 312. | 0. | 4393. | 5942. | 0. | 0. | 0. | .74 | 64. | 22.8 | C | 19.5 | 13.8 | * |
| * | 18 | 3 | 200. | 0. | 0. | 4393. | 0. | 0. | 4393. | 6000. | 0. | 0. | 0. | .73 | 64. | 22.7 | C | 19.4 | 13.8 | * |
| * | 19 | 3 | 1400. | 0. | 272. | 4393. | 0. | 272. | 4393. | 5962. | 0. | 0. | 0. | .74 | 64. | 22.7 | C | 19.4 | 13.8 | * |
| * | 20 | 3 | 900. | 0. | 0. | 4121. | 0. | 0. | 4121. | 6000. | 0. | 0. | 0. | .69 | 65. | 21.1 | C | 19.2 | 14.0 | * |
| * | 21 | 4 | 100. | 158. | 0. | 4279. | 158. | 0. | 4279. | 6098. | 0. | 0. | 0. | .70 | 65. | 16.5 | B | 19.2 | 14.0 | * |
| * | 22 | 4 | 100. | 0. | 70. | 4279. | 0. | 70. | 4279. | 6120. | 0. | 0. | 0. | .70 | 65. | 16.5 | B | 19.2 | 14.0 | * |
| * | 23 | 3 | 600. | 0. | 0. | 4209. | 0. | 0. | 4209. | 6000. | 0. | 0. | 0. | .70 | 65. | 21.6 | C | 19.2 | 14.0 | * |
| * | 24 | 3 | 1500. | 423. | 0. | 4632. | 423. | 0. | 4632. | 5913. | 0. | 0. | 0. | .78 | 64. | 24.3 | C | 19.8 | 13.5 | * |
| * | 25 | 3 | 1500. | 0. | 0. | 4632. | 0. | 0. | 4632. | 6000. | 0. | 0. | 0. | .77 | 64. | 24.2 | C | 19.7 | 13.6 | * |
| * | 26 | 3 | 8000. | 0. | 0. | 4632. | 0. | 0. | 4632. | 6000. | 0. | 0. | 0. | .77 | 64. | 24.2 | C | 19.7 | 13.6 | * |
| * | 27 | 5 | 100. | 949. | 0. | 5581. | 949. | 0. | 5581. | 10000. | 0. | 0. | 0. | .56 | 65. | 17.2 | B | 19.2 | 14.0 | * |
| * | 28 | 5 | 1000. | 0. | 0. | 5581. | 0. | 0. | 5581. | 7750. | 0. | 0. | 0. | .72 | 65. | 17.2 | B | 19.2 | 14.0 | * |
| * | 29 | 5 | 1000. | 0. | 5581. | 5581. | 0. | 5581. | 5581. | 9685. | 0. | 0. | 0. | .58 | 65. | 17.2 | B | 19.2 | 14.0 | * |
| ***** | | | | | | | | | | | | | | | | | | | | |
| * | TOTAL | | | 135469. | = | 25.7 | MILES | | | | | | | | | | | | | * |
| * | | | | | | | | | | | | | | | | | | | | * |
| * | | | | | | | | | | | | | | | | | | | | * |
| ***** | | | | | | | | | | | | | | | | | | | | |
| * | | | | | | | | | | | | | | | | | | | | * |
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| ***** | | | | | | | | | | | | | | | | | | | | |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 2/29/2016 16: 3 PAGE 6
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 1 OF 2

| CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | | |
|----------------------------|---------|-----------|---------|-------------------|---------|-----------|---------|----------|
| FREEWAY TRAVEL TIME = | 1887. | VEH-HRS | 1897. | PASS-HRS | 1887. | VEH-HRS | 1897. | PASS-HRS |
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1887. | VEH-HRS | 1897. | PASS-HRS | 1887. | VEH-HRS | 1897. | PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 120921. | VEH-MI. | 121574. | PASS-MI. | 120921. | VEH-MI. | 121574. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 64. | MPH. | | | 64. | MPH. | | |
| AVERAGE DENSITY = | 24. | VPMP/L | | | 24. | VPMP/L | | |
| TOTAL FUEL = | 6174. | GALLONS | | | 6174. | GALLONS | | |
| TOTAL EMISSIONS = | 1655. | KILOGRAMS | | | 1655. | KILOGRAMS | | |

| ***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 ***** | | | | | | | | | |
|---|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
| 1 | 0.00 | 2 | 20.65 | 3 | 0.92 | 4 | 0.20 | 5 | 0.24 |
| 6 | 0.88 | 7 | 0.85 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.18 | 18 | 0.02 | 19 | 0.17 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.47 | 25 | 0.00 |
| 26 | 2.06 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

| ***** TOTAL DELAY = 27.0 VEH-HRS ***** AVERAGE DELAY = 0.34 MIN/VEH ***** | | | | | | | | | |
|---|--|--|--|--|--|--|--|--|--|
|---|--|--|--|--|--|--|--|--|--|

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 2/29/2016 16: 3 PAGE 7
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 2

 ** FREEWAY TRAVEL TIME (MINUTES) **

| ***** ORIGINATIONS ACROSS ***** | | | | | | |
|---------------------------------|------|-------|-------|-------|-------|-------|
| * DOWN | 1 | 2 | 3 | 4 | 5 | 6 |
| * 1 * | 0.24 | 21.74 | 22.05 | 22.93 | 23.14 | 25.92 |
| * 2 * | 0.00 | 0.65 | 0.96 | 1.84 | 2.05 | 4.83 |
| * 3 * | 0.00 | 0.00 | 0.18 | 1.06 | 1.27 | 4.05 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.75 | 0.96 | 3.74 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.59 | 0.79 | 3.58 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.03 | 2.82 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.67 |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.37 |

Page 3

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+
+
+
* 9 * 0.00 0.00 0.00 0.00 0.00 0.35
* 10 * 0.00 0.00 0.00 0.00 0.00 0.17
*
*****

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TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | |
|--|----------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|---|------|------|
| * SEC LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | | |
| * 1 | 5 | 1370. | 6679. | 1135. | 6679. | 6679. | 1135. | 6679. | 10000. | 0. | 0. | 0. | .67 | 65. | 20.6 | C | 19.2 | 14.0 |
| * 2 | 3 | 99999. | 0. | 0. | 5544. | 0. | 0. | 5544. | 6226. | 0. | 0. | 0. | .89 | 60. | 31.0 | D | 21.7 | 12.3 |
| * 3 | 3 | 2740. | 0. | 0. | 5544. | 0. | 0. | 5544. | 6000. | 0. | 0. | 0. | .92 | 58. | 32.0 | D | 22.3 | 11.9 |
| * 4 | 3 | 600. | 0. | 0. | 5544. | 0. | 0. | 5544. | 6000. | 0. | 0. | 0. | .92 | 58. | 32.0 | D | 22.3 | 11.9 |
| * 5 | 3 | 700. | 0. | 0. | 5544. | 0. | 0. | 5544. | 6000. | 0. | 0. | 0. | .92 | 58. | 32.0 | D | 22.3 | 11.9 |
| * 6 | 3 | 2630. | 0. | 0. | 5544. | 0. | 0. | 5544. | 6000. | 0. | 0. | 0. | .92 | 58. | 32.0 | D | 22.3 | 11.9 |
| * 7 | 3 | 2530. | 0. | 0. | 5544. | 0. | 0. | 5544. | 6000. | 0. | 0. | 0. | .92 | 58. | 32.0 | D | 22.3 | 11.9 |
| * 8 | 4 | 1500. | 213. | 0. | 5757. | 213. | 0. | 5757. | 6213. | 0. | 0. | 0. | .93 | 65. | 22.1 | C | 19.2 | 14.0 |
| * 9 | 4 | 700. | 0. | 0. | 5757. | 0. | 0. | 5757. | 6240. | 0. | 0. | 0. | .92 | 65. | 22.1 | C | 19.2 | 14.0 |
| * 10 | 4 | 1500. | 0. | 1363. | 5757. | 0. | 1363. | 5757. | 5973. | 0. | 0. | 0. | .96 | 65. | 22.1 | C | 19.2 | 14.0 |
| * 11 | 3 | 750. | 0. | 0. | 4394. | 0. | 0. | 4394. | 6000. | 0. | 0. | 0. | .73 | 64. | 22.7 | C | 19.4 | 13.8 |
| * 12 | 4 | 350. | 1088. | 0. | 5482. | 1088. | 0. | 5482. | 6507. | 0. | 0. | 0. | .84 | 65. | 21.1 | C | 19.2 | 14.0 |
| * 13 | 4 | 350. | 0. | 0. | 5482. | 0. | 0. | 5482. | 6690. | 0. | 0. | 0. | .82 | 65. | 21.1 | C | 19.2 | 14.0 |
| * 14 | 4 | 350. | 0. | 599. | 5482. | 0. | 599. | 5482. | 6599. | 0. | 0. | 0. | .83 | 65. | 21.1 | C | 19.2 | 14.0 |
| * 15 | 3 | 700. | 0. | 0. | 4883. | 0. | 0. | 4883. | 6000. | 0. | 0. | 0. | .81 | 63. | 25.9 | C | 20.2 | 13.2 |
| * 16 | 3 | 900. | 113. | 0. | 4996. | 113. | 0. | 4996. | 5979. | 0. | 0. | 0. | .84 | 62. | 26.8 | D | 20.6 | 13.0 |
| * 17 | 3 | 1400. | 476. | 0. | 5472. | 476. | 0. | 5472. | 5909. | 0. | 0. | 0. | .93 | 58. | 31.6 | D | 22.3 | 11.9 |
| * 18 | 3 | 200. | 0. | 0. | 5472. | 0. | 0. | 5472. | 6000. | 0. | 0. | 0. | .91 | 59. | 31.2 | D | 22.1 | 12.0 |
| * 19 | 3 | 1400. | 0. | 204. | 5472. | 0. | 204. | 5472. | 5973. | 0. | 0. | 0. | .92 | 58. | 31.3 | D | 22.1 | 12.0 |
| * 20 | 3 | 900. | 0. | 0. | 5268. | 0. | 0. | 5268. | 6000. | 0. | 0. | 0. | .88 | 60. | 29.1 | D | 21.5 | 12.4 |
| * 21 | 4 | 100. | 208. | 0. | 5476. | 208. | 0. | 5476. | 6088. | 0. | 0. | 0. | .90 | 65. | 21.1 | C | 19.2 | 14.0 |
| * 22 | 4 | 100. | 0. | 115. | 5476. | 0. | 115. | 5476. | 6115. | 0. | 0. | 0. | .90 | 65. | 21.1 | C | 19.2 | 14.0 |
| * 23 | 3 | 600. | 0. | 0. | 5361. | 0. | 0. | 5361. | 6000. | 0. | 0. | 0. | .89 | 60. | 30.0 | D | 21.8 | 12.2 |
| * 24 | 3 | 1500. | 473. | 0. | 5834. | 473. | 0. | 5834. | 5903. | 0. | 0. | 0. | .99 | 53. | 36.5 | E | 23.6 | 11.2 |
| * 25 | 3 | 1500. | 0. | 0. | 5834. | 0. | 0. | 5834. | 6000. | 0. | 0. | 0. | .97 | 54. | 35.7 | E | 23.3 | 11.3 |
| * 26 | 3 | 8000. | 0. | 0. | 5834. | 0. | 0. | 5834. | 6000. | 0. | 0. | 0. | .97 | 54. | 35.7 | E | 23.3 | 11.3 |
| * 27 | 5 | 100. | 1195. | 0. | 7029. | 1195. | 0. | 7029. | 10000. | 0. | 0. | 0. | .70 | 65. | 21.6 | C | 19.2 | 14.0 |
| * 28 | 5 | 1000. | 0. | 0. | 7029. | 0. | 0. | 7029. | 7750. | 0. | 0. | 0. | .91 | 65. | 21.6 | C | 19.2 | 14.0 |
| * 29 | 5 | 1000. | 0. | 7029. | 7029. | 0. | 7029. | 7029. | 9685. | 0. | 0. | 0. | .73 | 65. | 21.6 | C | 19.2 | 14.0 |
| ***** | | | | | | | | | | | | | | | | | | |
| TOTAL 135469. = 25.7 MILES MAX(V/C) = 0.99 LOWEST LOS = E AVG = 59. 30.7 21.7 12.3 | | | | | | | | | | | | | | | | | | |
| ***** | | | | | | | | | | | | | | | | | | |

| CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | | |
|----------------------------|---------|------------|---------|-------------------|---------|------------|---------|----------|
| FREEWAY TRAVEL TIME = | 2414. | VEH-HRS | 2427. | PASS-HRS | 4302. | VEH-HRS | 4324. | PASS-HRS |
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 2414. | VEH-HRS | 2427. | PASS-HRS | 4302. | VEH-HRS | 4324. | PASS-HRS |
| TOTAL TRAV DISTANCE = | 143413. | VEH-MI. | 144213. | PASS-MI. | 264334. | VEH-MI. | 265788. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 59. | MPH. | | | 61. | MPH. | | |
| AVERAGE DENSITY = | 31. | VPMP | | | 27. | VPMP | | |
| TOTAL FUEL = | 6620. | GALLONS | | | 12794. | GALLONS | | |
| TOTAL EMISSIONS = | 1762. | KI LOGRAMS | | | 3417. | KI LOGRAMS | | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|--------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 144.04 | 3 | 5.50 | 4 | 1.21 | 5 | 1.41 |
| 6 | 5.28 | 7 | 5.08 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.08 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.36 |
| 16 | 0.63 | 17 | 2.83 | 18 | 0.35 | 19 | 2.57 | 20 | 1.08 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.86 | 24 | 5.65 | 25 | 4.92 |
| 26 | 26.24 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 208.1 VEH-HRS ***** AVERAGE DELAY = 2.24 MIN/VEH *****

```

FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP LLL
FFFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 1111111 222222222 PPP LLLLLLLLLL
    
```

FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 2 AND 26 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

FREWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT TRUCKS | DES RAMP | SPECIAL | FF.SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION | LOCATION |
|---------|----------|----------|-------------|--------------|---------|---------|-----------|---------|------------|----------|---------|------------------|---------------|----------|----------------|-------------------------|----------|
| 1 | | | | | | | | | | | | | | | | | |
| 2 | 1 | 1650. | 99999. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | NO | | 0.0 | 0. | GOOD | 0.0 | Queue Capture | |
| 3 | 1 | 1650. | 2740. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | | 0.0 | 0. | GOOD | 0.0 | SR-85 Off to Shore On | |
| 4 | 1 | 1650. | 600. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | | 0.0 | 0. | GOOD | 0.0 | Shore. On to Moffet Off | |
| 5 | 1 | 1650. | 700. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | | 0.0 | 0. | GOOD | 0.0 | Moffett Off to On | |
| 6 | 1 | 1650. | 2630. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | | 0.0 | 0. | GOOD | 0.0 | Moffett On to Ellis Off | |
| 7 | 1 | 1650. | 2530. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | | 0.0 | 0. | GOOD | 0.0 | Ellis Off to On-ramp | |
| 8 | 1 | 1650. | 1500. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | | 0.0 | 0. | GOOD | 0.0 | Ellis On-ramp | |
| 9 | 1 | 1650. | 700. | 65 | | 0.96 | 0.0 | 0 | 100 | YES | | 0.0 | 0. | GOOD | 0.0 | Ellis / US 237 | |
| 10 | 1 | 1650. | 1500. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | | 0.0 | 0. | GOOD | 0.0 | SR-237 EB Off-Ramp | |
| 11 | 1 | 1650. | 750. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | | 0.0 | 0. | GOOD | 0.0 | SR-237 / SR-237 | |
| 12 | 1 | 1650. | 350. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | | 0.0 | 0. | GOOD | 0.0 | SR-237 EB On-Ramp | |
| 13 | 1 | 1650. | 350. | 65 | | 0.96 | 0.0 | 0 | 100 | YES | | 0.0 | 0. | GOOD | 0.0 | US 237 / Mathilda | |
| 14 | 1 | 1650. | 350. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-Ramp | |
| 15 | 1 | 1650. | 700. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | |
| 16 | 1 | 1650. | 900. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | | 0.0 | 0. | GOOD | 0.0 | Mathilda SB On-Ramp | |
| 17 | 1 | 1650. | 1400. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | | 0.0 | 0. | GOOD | 0.0 | Mathilda NB On-Ramp | |
| 18 | 1 | 1650. | 200. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | | 0.0 | 0. | GOOD | 0.0 | Mathilda / Fair Oaks | |
| 19 | 1 | 1650. | 1400. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | | 0.0 | 0. | GOOD | 0.0 | Fair Oaks SB Off-Ramp | |

** 20 1 1650. 900. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks SB/ Fair Oaks **

FREEWAY AND ARTERIAL DESIGN FEATURES

Table with columns: SUB NO., SEC LNS, SSEC CAP, SSEC LENGTH, DESIGN SPEED, ORG DES, TRK FAC, SSEC GRAD, PCT TRK, PCT DES TRUCKS, SPECIAL RAMP, FF. SPD. ALT. RTE, CAP. ALT. RTE, ART TYPE, GRADE ALT. RTE, SUBSECTION, LOCATION. Rows 21-29.

FREEWAY TRAVEL TIME (MINUTES)

Table with columns: ORIGINS DOWN, DESTINATIONS ACROSS (1-7). Rows 1-11.

TIME SLICE FREEWAY PERFORMANCE TABLE

US-101_SB_AM_P1_2018_PL.txt

| * SUB SEC | NO. LNS | SSEC LENGTH | O-D ORG | DATA DES | DEMANDS SSEC | ADJUSTED ORG | VOLUMES DES | SSEC SSEC | WEAVE CAP. | CONGEST EFF | STORAGE LENGTH | V/C RATE | SPEED MPH | DENSITY VPMP | LOS LEVEL | FUEL MPG | EMI SS GS/VM |
|--|---------|-------------|---------|----------|--------------|--------------|-------------|-----------|------------|-------------|----------------|----------|-----------|--------------|-----------|----------|--------------|
| * 1 | | | | | | | | | | | | | | | | | |
| * 2 | 1 | 99999 | 967 | 0 | 967 | 967 | 0 | 967 | 1650 | 0 | 0 | .59 | 65 | 14.9 | B | 20.0 | 13.7 |
| * 3 | 1 | 2740 | 0 | 0 | 967 | 0 | 0 | 967 | 1650 | 0 | 0 | .59 | 65 | 14.9 | B | 20.0 | 13.7 |
| * 4 | 1 | 600 | 0 | 0 | 967 | 0 | 0 | 967 | 1650 | 0 | 0 | .59 | 65 | 14.9 | B | 20.0 | 13.7 |
| * 5 | 1 | 700 | 0 | 0 | 967 | 0 | 0 | 967 | 1650 | 0 | 0 | .59 | 65 | 14.9 | B | 20.0 | 13.7 |
| * 6 | 1 | 2630 | 0 | 0 | 967 | 0 | 0 | 967 | 1650 | 0 | 0 | .59 | 65 | 14.9 | B | 20.0 | 13.7 |
| * 7 | 1 | 2530 | 0 | 0 | 967 | 0 | 0 | 967 | 1650 | 0 | 0 | .59 | 65 | 14.9 | B | 20.0 | 13.7 |
| * 8 | 1 | 1500 | 21 | 0 | 988 | 21 | 0 | 988 | 1650 | 0 | 0 | .60 | 65 | 15.2 | B | 20.0 | 13.7 |
| * 9 | 1 | 700 | 0 | 0 | 988 | 0 | 0 | 988 | 1650 | 0 | 0 | .60 | 65 | 15.2 | B | 20.0 | 13.7 |
| * 10 | 1 | 1500 | 0 | 242 | 988 | 0 | 242 | 988 | 1650 | 0 | 0 | .60 | 65 | 15.2 | B | 20.0 | 13.7 |
| * 11 | 1 | 750 | 0 | 0 | 746 | 0 | 0 | 746 | 1650 | 0 | 0 | .45 | 65 | 11.5 | B | 20.0 | 13.7 |
| * 12 | 1 | 350 | 128 | 0 | 874 | 128 | 0 | 874 | 1650 | 0 | 0 | .53 | 65 | 13.4 | B | 20.0 | 13.7 |
| * 13 | 1 | 350 | 0 | 0 | 874 | 0 | 0 | 874 | 1650 | 0 | 0 | .53 | 65 | 13.4 | B | 20.0 | 13.7 |
| * 14 | 1 | 350 | 0 | 71 | 874 | 0 | 71 | 874 | 1650 | 0 | 0 | .53 | 65 | 13.4 | B | 20.0 | 13.7 |
| * 15 | 1 | 700 | 0 | 0 | 803 | 0 | 0 | 803 | 1650 | 0 | 0 | .49 | 65 | 12.3 | B | 20.0 | 13.7 |
| * 16 | 1 | 900 | 17 | 0 | 820 | 17 | 0 | 820 | 1650 | 0 | 0 | .50 | 65 | 12.6 | B | 20.0 | 13.7 |
| * 17 | 1 | 1400 | 58 | 0 | 878 | 58 | 0 | 878 | 1650 | 0 | 0 | .53 | 65 | 13.5 | B | 20.0 | 13.7 |
| * 18 | 1 | 200 | 0 | 0 | 878 | 0 | 0 | 878 | 1650 | 0 | 0 | .53 | 65 | 13.5 | B | 20.0 | 13.7 |
| * 19 | 1 | 1400 | 0 | 38 | 878 | 0 | 38 | 878 | 1650 | 0 | 0 | .53 | 65 | 13.5 | B | 20.0 | 13.7 |
| * 20 | 1 | 900 | 0 | 0 | 840 | 0 | 0 | 840 | 1650 | 0 | 0 | .51 | 65 | 12.9 | B | 20.0 | 13.7 |
| * 21 | 1 | 100 | 32 | 0 | 872 | 32 | 0 | 872 | 1650 | 0 | 0 | .53 | 65 | 13.4 | B | 20.0 | 13.7 |
| * 22 | 1 | 100 | 0 | 10 | 872 | 0 | 10 | 872 | 1650 | 0 | 0 | .53 | 65 | 13.4 | B | 20.0 | 13.7 |
| * 23 | 1 | 600 | 0 | 0 | 862 | 0 | 0 | 862 | 1650 | 0 | 0 | .52 | 65 | 13.3 | B | 20.0 | 13.7 |
| * 24 | 1 | 1500 | 87 | 0 | 949 | 87 | 0 | 949 | 1650 | 0 | 0 | .57 | 65 | 14.6 | B | 20.0 | 13.7 |
| * 25 | 1 | 1500 | 0 | 0 | 949 | 0 | 0 | 949 | 1650 | 0 | 0 | .57 | 65 | 14.6 | B | 20.0 | 13.7 |
| * 26 | 1 | 8000 | 0 | 949 | 949 | 0 | 949 | 949 | 1650 | 0 | 0 | .57 | 65 | 14.6 | B | 20.0 | 13.7 |
| * 27 | | | | | | | | | | | | | | | | | |
| * 28 | | | | | | | | | | | | | | | | | |
| * 29 | | | | | | | | | | | | | | | | | |
| ***** | | | | | | | | | | | | | | | | | |
| * TOTAL 131999. = 25.0 MILES MAX(V/C) = 0.60 LOWEST LOS = B AVG = 65. 14.8 20.0 13.7 * | | | | | | | | | | | | | | | | | |
| ***** | | | | | | | | | | | | | | | | | |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 1 OF 2

| | CURRENT TIME SLICE | | | CUMULATIVE VALUES | | |
|-----------------------------|--------------------|-----------------|----------------|-------------------|--|--|
| FREWAY TRAVEL TIME = | 369. VEH-HRS | 738. PASS-HRS | 369. VEH-HRS | 738. PASS-HRS | | |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | | |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | | |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | | |
| TOTAL SYSTEM TRAVEL TIME = | 369. VEH-HRS | 738. PASS-HRS | 369. VEH-HRS | 738. PASS-HRS | | |
| TOTAL FRWAY TRAV DISTANCE = | 23973. VEH-MI. | 47946. PASS-MI. | 23973. VEH-MI. | 47946. PASS-MI. | | |
| AVERAGE SYSTEM SPEED = | 65. MPH. | | 65. MPH. | | | |
| AVERAGE DENSITY = | 15. VPMP | | 15. VPMP | | | |
| TOTAL FUEL = | 1199. GALLONS | | 1199. GALLONS | | | |
| TOTAL EMISSIONS = | 329. KILOGRAMS | | 329. KILOGRAMS | | | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 16: 3 PAGE 7
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 2

 ** FREWAY TRAVEL TIME (MI MINUTES) **

| * ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | |
|----------------|---------------------|-------|-------|-------|-------|-------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 19.74 | 20.05 | 20.86 | 21.05 | 23.08 | 0.00 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 1.96 | 3.99 | 0.00 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.21 | 0.00 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.90 | 0.00 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.74 | 0.00 |


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FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 Pppppppp EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q* A. D. MAY*Q 111111 222 222 Pppppppp EEEEEEEEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 Ppp Ppp EEE
FFF RRR RRR EEE QQQ QQQ 1111 222 Ppp Ppp EEE
FFFFFFFF RRRRRRRR EEEEE QQQ QQQ 1111 222 Pppppppp EEEEE
FFFFFFFF RRRRRRRR EEEEE QQQ QQQ 1111 2222 Pppppppp EEEEE
FFF RRR RRR EEE QQQ QQQ 1111 2222 Ppp EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 Ppp EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 Ppp EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q Q 1111111 222222222 Ppp EEEEEEEEE

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FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

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*****
*****
**
** FREWAY AND ARTERIAL DESIGN FEATURES
**
*****
**
** SUB NO. SSEC SSEC DESIGN ORG TRK SSEC PCT PCT DES SPECIAL FF. SPD. CAP. ART GRADE SUBSECTION LOCATION
** SEC LNS CAP LENGTH SPEED DES FAC GRAD TRK TRUCKS RAMP ALT. RTE ALT. RTE TYPE ALT. RTE
**
** 1 5 10000. 1370. 65 OD 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 Seeding
**
** 2 3 6226. 99999. 65 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 Queue Capture
**
** 3 3 6000. 2740. 65 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 SR-85 Off to Shore On
**
** 4 3 6000. 600. 65 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 Shore. On to Moffett Off
**
** 5 3 6000. 700. 65 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 Moffett Off to On
**
** 6 3 6000. 2630. 65 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 Moffett On to Ellis Off
**
** 7 3 6000. 2530. 65 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 Ellis Off to On-ramp
**
** 8 4 6240. 1500. 65 0 0.96 0.0 4 0 YES 0.0 0. GOOD 0.0 Ellis On-ramp
**
** 9 4 6240. 700. 65 0.96 0.0 4 0 YES 0.0 0. GOOD 0.0 Ellis / US 237
**
** 10 4 6240. 1500. 65 D 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 SR-237 EB Off-Ramp
**
** 11 3 6000. 750. 65 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 SR-237 / SR-237
**
** 12 4 6690. 350. 65 0 0.96 0.0 4 0 YES 0.0 0. GOOD 0.0 SR-237 EB On-Ramp
**
** 13 4 6690. 350. 65 0.96 0.0 4 0 YES 0.0 0. GOOD 0.0 US 237 / Mathilda
**
** 14 4 6690. 350. 65 D 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 Mathilda Off-Ramp
**
** 15 3 6000. 700. 65 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 Mathilda / Mathilda
**
** 16 3 6000. 900. 65 0 0.96 0.0 4 0 YES 0.0 0. GOOD 0.0 Mathilda SB On-Ramp
**
** 17 3 6000. 1400. 65 0 0.96 0.0 4 0 YES 0.0 0. GOOD 0.0 Mathilda NB On-Ramp
**
** 18 3 6000. 200. 65 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 Mathilda / Fair Oaks
**
** 19 3 6000. 1400. 65 D 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 Fair Oaks SB Off-Ramp
**
** 20 3 6000. 900. 65 0.96 0.0 4 0 NO 0.0 0. GOOD 0.0 Fair Oaks SB/ Fair Oaks
**
*****
*****

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FREEWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. SEC LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT DES TRUCKS | SPECIAL RAMP | FF.SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION | LOCATION |
|--------------------|-------------|----------------|-----------------|------------|------------|--------------|------------|----------------------|-----------------|---------------------|------------------|-------------|-------------------|------------|--------------------------|
| 21 | 4 | 6130. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Fair Oaks SB On-Ramp |
| 22 | 4 | 6130. | 100. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks NB Off-Ramp |
| 23 | 3 | 6000. | 600. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks NB/ Fair Oaks |
| 24 | 3 | 6000. | 1500. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Oaks On-Ramp to Mid |
| 25 | 3 | 6000. | 1500. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mid to Lawrence Off-ramp |
| 26 | 3 | 6000. | 8000. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| 27 | 5 | 10000. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| 28 | 5 | 7750. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Dummy Bottleneck |
| 29 | 5 | 9685. | 1000. | 65 | 0D | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | End of Network |

***** INPUT HAS BEEN COMPLETED *****

FREEWAY TRAVEL TIME (MINUTES)

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | |
|-----------------|---------------------|-------|-------|-------|-------|-------|
| | 1 | 2 | 3 | 4 | 5 | 6 |
| 1 | 0.24 | 20.28 | 20.59 | 21.40 | 21.59 | 24.03 |
| 2 | 0.00 | 0.65 | 0.96 | 1.77 | 1.96 | 4.39 |
| 3 | 0.00 | 0.00 | 0.18 | 0.99 | 1.19 | 3.62 |
| 4 | 0.00 | 0.00 | 0.00 | 0.69 | 0.88 | 3.31 |
| 5 | 0.00 | 0.00 | 0.00 | 0.53 | 0.72 | 3.15 |
| 6 | 0.00 | 0.00 | 0.00 | 0.00 | 0.03 | 2.47 |
| 7 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.33 |
| 8 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.37 |
| 9 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.35 |
| 10 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB NO. SEC LNS | SSEC LENGTH | O-D DATA ORG DES | DEMANDS SSEC | ADJUSTED VOLUMES ORG DES SSEC | SSEC CAP. | WEAVE EFF | CONGEST LENGTH | STORAGE RATE | V/C RATIO | SPEED MPH | DENSITY VPMPL | LOS LEVEL | FUEL MPG | EMISS GS/VM |
|--------------------|----------------|---------------------|-----------------|----------------------------------|--------------|--------------|-------------------|-----------------|--------------|--------------|------------------|--------------|-------------|----------------|
| 1 | 5 | 1370. | 5689. | 967. 5689. | 5689. | 967. 5689. | 10000. | 0. | 0. | 0. | .57 | 65. | 17.5 | B 19.2 14.0 |

US-101_SB_AM_P2_2018_PE.txt

| | | | | | | | | | | | | | | | | | | | | |
|---|----|---|--------|------|-------|-------|------|-------|-------|--------|----|----|----|-----|-----|------|---|------|------|---|
| * | 2 | 3 | 99999. | 0. | 0. | 4722. | 0. | 0. | 4722. | 6226. | 0. | 0. | 0. | .76 | 64. | 24.6 | C | 19.6 | 13.7 | * |
| * | 3 | 3 | 2740. | 0. | 0. | 4722. | 0. | 0. | 4722. | 6000. | 0. | 0. | 0. | .79 | 63. | 24.8 | C | 19.9 | 13.5 | * |
| * | 4 | 3 | 600. | 0. | 0. | 4722. | 0. | 0. | 4722. | 6000. | 0. | 0. | 0. | .79 | 63. | 24.8 | C | 19.9 | 13.5 | * |
| * | 5 | 3 | 700. | 0. | 0. | 4722. | 0. | 0. | 4722. | 6000. | 0. | 0. | 0. | .79 | 63. | 24.8 | C | 19.9 | 13.5 | * |
| * | 6 | 3 | 2630. | 0. | 0. | 4722. | 0. | 0. | 4722. | 6000. | 0. | 0. | 0. | .79 | 63. | 24.8 | C | 19.9 | 13.5 | * |
| * | 7 | 3 | 2530. | 0. | 0. | 4722. | 0. | 0. | 4722. | 6000. | 0. | 0. | 0. | .79 | 63. | 24.8 | C | 19.9 | 13.5 | * |
| * | 8 | 4 | 1500. | 171. | 0. | 4893. | 171. | 0. | 4893. | 6219. | 0. | 0. | 0. | .79 | 65. | 18.8 | C | 19.2 | 14.0 | * |
| * | 9 | 4 | 700. | 0. | 0. | 4893. | 0. | 0. | 4893. | 6240. | 0. | 0. | 0. | .78 | 65. | 18.8 | C | 19.2 | 14.0 | * |
| * | 10 | 4 | 1500. | 0. | 1229. | 4893. | 0. | 1229. | 4893. | 5998. | 0. | 0. | 0. | .82 | 65. | 18.8 | C | 19.2 | 14.0 | * |
| * | 11 | 3 | 750. | 0. | 0. | 3664. | 0. | 0. | 3664. | 6000. | 0. | 0. | 0. | .61 | 65. | 18.8 | C | 19.2 | 14.0 | * |
| * | 12 | 4 | 350. | 772. | 0. | 4436. | 772. | 0. | 4436. | 6562. | 0. | 0. | 0. | .68 | 65. | 17.1 | B | 19.2 | 14.0 | * |
| * | 13 | 4 | 350. | 0. | 0. | 4436. | 0. | 0. | 4436. | 6690. | 0. | 0. | 0. | .66 | 65. | 17.1 | B | 19.2 | 14.0 | * |
| * | 14 | 4 | 350. | 0. | 449. | 4436. | 0. | 449. | 4436. | 6619. | 0. | 0. | 0. | .67 | 65. | 17.1 | B | 19.2 | 14.0 | * |
| * | 15 | 3 | 700. | 0. | 0. | 3987. | 0. | 0. | 3987. | 6000. | 0. | 0. | 0. | .66 | 65. | 20.4 | C | 19.2 | 14.0 | * |
| * | 16 | 3 | 900. | 93. | 0. | 4080. | 93. | 0. | 4080. | 5983. | 0. | 0. | 0. | .68 | 65. | 20.9 | C | 19.2 | 14.0 | * |
| * | 17 | 3 | 1400. | 303. | 0. | 4383. | 303. | 0. | 4383. | 5943. | 0. | 0. | 0. | .74 | 64. | 22.7 | C | 19.5 | 13.8 | * |
| * | 18 | 3 | 200. | 0. | 0. | 4383. | 0. | 0. | 4383. | 6000. | 0. | 0. | 0. | .73 | 64. | 22.7 | C | 19.4 | 13.8 | * |
| * | 19 | 3 | 1400. | 0. | 271. | 4383. | 0. | 271. | 4383. | 5961. | 0. | 0. | 0. | .74 | 64. | 22.7 | C | 19.4 | 13.8 | * |
| * | 20 | 3 | 900. | 0. | 0. | 4112. | 0. | 0. | 4112. | 6000. | 0. | 0. | 0. | .69 | 65. | 21.1 | C | 19.2 | 14.0 | * |
| * | 21 | 4 | 100. | 158. | 0. | 4270. | 158. | 0. | 4270. | 6098. | 0. | 0. | 0. | .70 | 65. | 16.4 | B | 19.2 | 14.0 | * |
| * | 22 | 4 | 100. | 0. | 70. | 4270. | 0. | 70. | 4270. | 6120. | 0. | 0. | 0. | .70 | 65. | 16.4 | B | 19.2 | 14.0 | * |
| * | 23 | 3 | 600. | 0. | 0. | 4200. | 0. | 0. | 4200. | 6000. | 0. | 0. | 0. | .70 | 65. | 21.5 | C | 19.2 | 14.0 | * |
| * | 24 | 3 | 1500. | 423. | 0. | 4623. | 423. | 0. | 4623. | 5913. | 0. | 0. | 0. | .78 | 64. | 24.2 | C | 19.8 | 13.5 | * |
| * | 25 | 3 | 1500. | 0. | 0. | 4623. | 0. | 0. | 4623. | 6000. | 0. | 0. | 0. | .77 | 64. | 24.1 | C | 19.7 | 13.6 | * |
| * | 26 | 3 | 8000. | 0. | 0. | 4623. | 0. | 0. | 4623. | 6000. | 0. | 0. | 0. | .77 | 64. | 24.1 | C | 19.7 | 13.6 | * |
| * | 27 | 5 | 100. | 947. | 0. | 5570. | 947. | 0. | 5570. | 10000. | 0. | 0. | 0. | .56 | 65. | 17.1 | B | 19.2 | 14.0 | * |
| * | 28 | 5 | 1000. | 0. | 0. | 5570. | 0. | 0. | 5570. | 7750. | 0. | 0. | 0. | .72 | 65. | 17.1 | B | 19.2 | 14.0 | * |
| * | 29 | 5 | 1000. | 0. | 5570. | 5570. | 0. | 5570. | 5570. | 9685. | 0. | 0. | 0. | .58 | 65. | 17.1 | B | 19.2 | 14.0 | * |

 * TOTAL 135469. = 25.7 MILES MAX(V/C) = 0.82 LOWEST LOS = C AVG = 64. 24.0 19.6 13.7 *

| | CURRENT TIME SLICE | | | CUMULATIVE VALUES | | | | |
|----------------------------|--------------------|-----------|---------|-------------------|---------|-----------|---------|----------|
| FREEWAY TRAVEL TIME = | 1886. | VEH-HRS | 1896. | PASS-HRS | 1886. | VEH-HRS | 1896. | PASS-HRS |
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1886. | VEH-HRS | 1896. | PASS-HRS | 1886. | VEH-HRS | 1896. | PASS-HRS |
| TOTAL TRAV DISTANCE = | 120867. | VEH-MI. | 121520. | PASS-MI. | 120867. | VEH-MI. | 121520. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 64. | MPH. | | | 64. | MPH. | | |
| AVERAGE DENSITY = | 24. | VPMP/L | | | 24. | VPMP/L | | |
| TOTAL FUEL = | 6172. | GALLONS | | | 6172. | GALLONS | | |
| TOTAL EMISSIONS = | 1654. | KILOGRAMS | | | 1654. | KILOGRAMS | | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 20.59 | 3 | 0.92 | 4 | 0.20 | 5 | 0.23 |
| 6 | 0.88 | 7 | 0.85 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.18 | 18 | 0.02 | 19 | 0.17 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.45 | 25 | 0.00 |
| 26 | 2.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 26.9 VEH-HRS ***** AVERAGE DELAY = 0.34 MIN/VEH *****

 ** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS | * DESTINATIONS ACROSS * | | | | | |
|-----------|-------------------------|-------|-------|-------|-------|-------|
| * DOWN | 1 | 2 | 3 | 4 | 5 | 6 |
| * 1 * | 0.24 | 21.74 | 22.05 | 22.93 | 23.13 | 25.90 |
| * 2 * | 0.00 | 0.65 | 0.96 | 1.84 | 2.04 | 4.81 |
| * 3 * | 0.00 | 0.00 | 0.18 | 1.06 | 1.26 | 4.03 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.75 | 0.95 | 3.72 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.58 | 0.79 | 3.56 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.03 | 2.80 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.65 |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.37 |

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+
+
+
* 9 * 0.00 0.00 0.00 0.00 0.00 0.35
* 10 * 0.00 0.00 0.00 0.00 0.00 0.17
*
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TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | |
|-----------|----------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|---|------|------|
| * SEC LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | | |
| * 1 | 5 | 1370. | 6679. | 1135. | 6679. | 6679. | 1135. | 6679. | 10000. | 0. | 0. | 0. | .67 | 65. | 20.6 | C | 19.2 | 14.0 |
| * 2 | 3 | 99999. | 0. | 0. | 5544. | 0. | 0. | 5544. | 6226. | 0. | 0. | 0. | .89 | 60. | 31.0 | D | 21.7 | 12.3 |
| * 3 | 3 | 2740. | 0. | 0. | 5544. | 0. | 0. | 5544. | 6000. | 0. | 0. | 0. | .92 | 58. | 32.0 | D | 22.3 | 11.9 |
| * 4 | 3 | 600. | 0. | 0. | 5544. | 0. | 0. | 5544. | 6000. | 0. | 0. | 0. | .92 | 58. | 32.0 | D | 22.3 | 11.9 |
| * 5 | 3 | 700. | 0. | 0. | 5544. | 0. | 0. | 5544. | 6000. | 0. | 0. | 0. | .92 | 58. | 32.0 | D | 22.3 | 11.9 |
| * 6 | 3 | 2630. | 0. | 0. | 5544. | 0. | 0. | 5544. | 6000. | 0. | 0. | 0. | .92 | 58. | 32.0 | D | 22.3 | 11.9 |
| * 7 | 3 | 2530. | 0. | 0. | 5544. | 0. | 0. | 5544. | 6000. | 0. | 0. | 0. | .92 | 58. | 32.0 | D | 22.3 | 11.9 |
| * 8 | 4 | 1500. | 213. | 0. | 5757. | 213. | 0. | 5757. | 6213. | 0. | 0. | 0. | .93 | 65. | 22.1 | C | 19.2 | 14.0 |
| * 9 | 4 | 700. | 0. | 0. | 5757. | 0. | 0. | 5757. | 6240. | 0. | 0. | 0. | .92 | 65. | 22.1 | C | 19.2 | 14.0 |
| * 10 | 4 | 1500. | 0. | 1363. | 5757. | 0. | 1363. | 5757. | 5973. | 0. | 0. | 0. | .96 | 65. | 22.1 | C | 19.2 | 14.0 |
| * 11 | 3 | 750. | 0. | 0. | 4394. | 0. | 0. | 4394. | 6000. | 0. | 0. | 0. | .73 | 64. | 22.7 | C | 19.4 | 13.8 |
| * 12 | 4 | 350. | 1088. | 0. | 5482. | 1088. | 0. | 5482. | 6507. | 0. | 0. | 0. | .84 | 65. | 21.1 | C | 19.2 | 14.0 |
| * 13 | 4 | 350. | 0. | 0. | 5482. | 0. | 0. | 5482. | 6690. | 0. | 0. | 0. | .82 | 65. | 21.1 | C | 19.2 | 14.0 |
| * 14 | 4 | 350. | 0. | 599. | 5482. | 0. | 599. | 5482. | 6599. | 0. | 0. | 0. | .83 | 65. | 21.1 | C | 19.2 | 14.0 |
| * 15 | 3 | 700. | 0. | 0. | 4883. | 0. | 0. | 4883. | 6000. | 0. | 0. | 0. | .81 | 63. | 25.9 | C | 20.2 | 13.2 |
| * 16 | 3 | 900. | 103. | 0. | 4986. | 103. | 0. | 4986. | 5980. | 0. | 0. | 0. | .83 | 62. | 26.8 | D | 20.5 | 13.0 |
| * 17 | 3 | 1400. | 456. | 0. | 5442. | 456. | 0. | 5442. | 5912. | 0. | 0. | 0. | .92 | 58. | 31.3 | D | 22.2 | 11.9 |
| * 18 | 3 | 200. | 0. | 0. | 5442. | 0. | 0. | 5442. | 6000. | 0. | 0. | 0. | .91 | 59. | 30.9 | D | 22.0 | 12.1 |
| * 19 | 3 | 1400. | 0. | 203. | 5442. | 0. | 203. | 5442. | 5973. | 0. | 0. | 0. | .91 | 59. | 31.0 | D | 22.0 | 12.1 |
| * 20 | 3 | 900. | 0. | 0. | 5239. | 0. | 0. | 5239. | 6000. | 0. | 0. | 0. | .87 | 61. | 28.9 | D | 21.3 | 12.5 |
| * 21 | 4 | 100. | 208. | 0. | 5447. | 208. | 0. | 5447. | 6088. | 0. | 0. | 0. | .89 | 65. | 21.0 | C | 19.2 | 14.0 |
| * 22 | 4 | 100. | 0. | 113. | 5447. | 0. | 113. | 5447. | 6115. | 0. | 0. | 0. | .89 | 65. | 21.0 | C | 19.2 | 14.0 |
| * 23 | 3 | 600. | 0. | 0. | 5334. | 0. | 0. | 5334. | 6000. | 0. | 0. | 0. | .89 | 60. | 29.8 | D | 21.7 | 12.3 |
| * 24 | 3 | 1500. | 473. | 0. | 5807. | 473. | 0. | 5807. | 5903. | 0. | 0. | 0. | .98 | 54. | 36.1 | E | 23.5 | 11.2 |
| * 25 | 3 | 1500. | 0. | 0. | 5807. | 0. | 0. | 5807. | 6000. | 0. | 0. | 0. | .97 | 55. | 35.3 | E | 23.2 | 11.4 |
| * 26 | 3 | 8000. | 0. | 0. | 5807. | 0. | 0. | 5807. | 6000. | 0. | 0. | 0. | .97 | 55. | 35.3 | E | 23.2 | 11.4 |
| * 27 | 5 | 100. | 1190. | 0. | 6997. | 1190. | 0. | 6997. | 10000. | 0. | 0. | 0. | .70 | 65. | 21.5 | C | 19.2 | 14.0 |
| * 28 | 5 | 1000. | 0. | 0. | 6997. | 0. | 0. | 6997. | 7750. | 0. | 0. | 0. | .90 | 65. | 21.5 | C | 19.2 | 14.0 |
| * 29 | 5 | 1000. | 0. | 6997. | 6997. | 0. | 6997. | 6997. | 9685. | 0. | 0. | 0. | .72 | 65. | 21.5 | C | 19.2 | 14.0 |

TOTAL 135469. = 25.7 MILES MAX(V/C) = 0.98 LOWEST LOS = E AVG = 59. 30.7 21.7 12.3

| CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | | |
|----------------------------|---------|------------|---------|-------------------|---------|------------|---------|----------|
| FREEWAY TRAVEL TIME = | 2411. | VEH-HRS | 2423. | PASS-HRS | 4297. | VEH-HRS | 4320. | PASS-HRS |
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 2411. | VEH-HRS | 2423. | PASS-HRS | 4297. | VEH-HRS | 4320. | PASS-HRS |
| TOTAL TRAV DISTANCE = | 143316. | VEH-MI. | 144114. | PASS-MI. | 264183. | VEH-MI. | 265634. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 59. | MPH. | | | 61. | MPH. | | |
| AVERAGE DENSITY = | 31. | VPMP | | | 27. | VPMP | | |
| TOTAL FUEL = | 6618. | GALLONS | | | 12790. | GALLONS | | |
| TOTAL EMISSIONS = | 1761. | KI LOGRAMS | | | 3416. | KI LOGRAMS | | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|--------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 144.04 | 3 | 5.50 | 4 | 1.21 | 5 | 1.41 |
| 6 | 5.28 | 7 | 5.08 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.08 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.36 |
| 16 | 0.61 | 17 | 2.67 | 18 | 0.33 | 19 | 2.44 | 20 | 1.02 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.82 | 24 | 5.41 | 25 | 4.71 |
| 26 | 25.11 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 206.1 VEH-HRS ***** AVERAGE DELAY = 2.22 MIN/VEH *****

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FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP LLL
FFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 1111111 222222222 PPP LLLLLLLLLL
    
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FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 2 AND 26 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65 MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

** FREeway AND ARTERIAL DESIGN FEATURES **

| ** SUB NO. | ** SSEC | ** SSEC | ** DESIGN | ** ORG | ** TRK | ** SSEC | ** PCT | ** PCT | ** DES | ** SPECIAL | ** FF.SPD. | ** CAP. | ** ART | ** GRADE | ** SUBSECTION | ** LOCATION | ** |
|------------|---------|---------|-----------|--------|--------|---------|--------|-----------|---------|-------------|-------------|-------------|---------|-------------|-------------------------|-------------|----|
| ** SEC | ** LNS | ** CAP | ** SPEED | ** DES | ** FAC | ** GRAD | ** TRK | ** TRUCKS | ** RAMP | ** ALT. RTE | ** ALT. RTE | ** ALT. RTE | ** TYPE | ** ALT. RTE | ** | ** | ** |
| ** 1 | | | | | | | | | | | | | | | | | ** |
| ** 2 | 1 | 1650. | 99999. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | | ** |
| ** 3 | 1 | 1650. | 2740. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-85 Off to Shore On | | ** |
| ** 4 | 1 | 1650. | 600. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Shore. On to Moffet Off | | ** |
| ** 5 | 1 | 1650. | 700. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Moffett Off to On | | ** |
| ** 6 | 1 | 1650. | 2630. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Moffett On to Ellis Off | | ** |
| ** 7 | 1 | 1650. | 2530. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Ellis Off to On-ramp | | ** |
| ** 8 | 1 | 1650. | 1500. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Ellis On-ramp | | ** |
| ** 9 | 1 | 1650. | 700. | 65 | | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Ellis / US 237 | | ** |
| ** 10 | 1 | 1650. | 1500. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 EB Off-Ramp | | ** |
| ** 11 | 1 | 1650. | 750. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 / SR-237 | | ** |
| ** 12 | 1 | 1650. | 350. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 EB On-Ramp | | ** |
| ** 13 | 1 | 1650. | 350. | 65 | | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | US 237 / Mathilda | | ** |
| ** 14 | 1 | 1650. | 350. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-Ramp | | ** |
| ** 15 | 1 | 1650. | 700. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | | ** |
| ** 16 | 1 | 1650. | 900. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda SB On-Ramp | | ** |
| ** 17 | 1 | 1650. | 1400. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda NB On-Ramp | | ** |
| ** 18 | 1 | 1650. | 200. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Fair Oaks | | ** |
| ** 19 | 1 | 1650. | 1400. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks SB Off-Ramp | | ** |

** 20 1 1650. 900. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks SB/ Fair Oaks **

FREEWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SEC | LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT DES TRUCKS | SPECIAL RAMP | FF. SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION | LOCATION |
|---------|-----|-------|----------|-------------|--------------|---------|---------|-----------|---------|----------------|--------------|-------------------|---------------|----------|----------------|----------------------|----------|
| 21 | 1 | 1650. | 100. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Fair Oaks | SB On-Ramp | |
| 22 | 1 | 1650. | 100. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks | NB Off-Ramp | |
| 23 | 1 | 1650. | 600. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks | NB/ Fair Oaks | |
| 24 | 1 | 1650. | 1500. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Oaks | On-Ramp to Mid | |
| 25 | 1 | 1650. | 1500. | 65 | | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Mid | to Lawrence Off-ramp | |
| 26 | 1 | 1650. | 8000. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | HOV | Dummy | |
| 27 | | | | | | | | | | | | | | | | | |
| 28 | | | | | | | | | | | | | | | | | |
| 29 | | | | | | | | | | | | | | | | | |

FREEWAY TRAVEL TIME (MINUTES)

| ORIGINS DOWN | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
|--------------|------|-------|-------|-------|-------|-------|------|
| 1 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | 0.00 | 19.74 | 20.05 | 20.86 | 21.05 | 23.08 | 0.00 |
| 3 | 0.00 | 0.00 | 0.00 | 0.00 | 1.96 | 3.99 | 0.00 |
| 4 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.21 | 0.00 |
| 5 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.90 | 0.00 |
| 6 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.74 | 0.00 |
| 7 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.06 | 0.00 |
| 8 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.92 | 0.00 |
| 9 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 10 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 11 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

TIME SLICE FREEWAY PERFORMANCE TABLE

US-101_SB_AM_P2_2018_PL.txt

| * SUB SEC | NO. LNS | SSEC LENGTH | O-D ORG | DATA DES | DEMANDS SSEC | ADJUSTED ORG | VOLUMES DES | SSEC SSEC | WEAVE EFF | CONGEST LENGTH | STORAGE RATE | V/C RATIO | SPEED MPH | DENSITY VPMP | LOS LEVEL | FUEL MPG | EMI SS GS/VM | |
|-----------|---------|-------------|---------|----------|--------------|--------------|-------------|-----------|-----------------|----------------|--------------|-----------|-----------|--------------|-----------|----------|--------------|------|
| * | 1 | | | | | | | | | | | | | | | | | |
| * | 2 | 1 | 99999 | 967 | 0 | 967 | 967 | 0 | 967 | 1650 | 0 | 0 | .59 | 65 | 14.9 | B | 20.0 | 13.7 |
| * | 3 | 1 | 2740 | 0 | 0 | 967 | 0 | 0 | 967 | 1650 | 0 | 0 | .59 | 65 | 14.9 | B | 20.0 | 13.7 |
| * | 4 | 1 | 600 | 0 | 0 | 967 | 0 | 0 | 967 | 1650 | 0 | 0 | .59 | 65 | 14.9 | B | 20.0 | 13.7 |
| * | 5 | 1 | 700 | 0 | 0 | 967 | 0 | 0 | 967 | 1650 | 0 | 0 | .59 | 65 | 14.9 | B | 20.0 | 13.7 |
| * | 6 | 1 | 2630 | 0 | 0 | 967 | 0 | 0 | 967 | 1650 | 0 | 0 | .59 | 65 | 14.9 | B | 20.0 | 13.7 |
| * | 7 | 1 | 2530 | 0 | 0 | 967 | 0 | 0 | 967 | 1650 | 0 | 0 | .59 | 65 | 14.9 | B | 20.0 | 13.7 |
| * | 8 | 1 | 1500 | 21 | 0 | 988 | 21 | 0 | 988 | 1650 | 0 | 0 | .60 | 65 | 15.2 | B | 20.0 | 13.7 |
| * | 9 | 1 | 700 | 0 | 0 | 988 | 0 | 0 | 988 | 1650 | 0 | 0 | .60 | 65 | 15.2 | B | 20.0 | 13.7 |
| * | 10 | 1 | 1500 | 0 | 242 | 988 | 0 | 242 | 988 | 1650 | 0 | 0 | .60 | 65 | 15.2 | B | 20.0 | 13.7 |
| * | 11 | 1 | 750 | 0 | 0 | 746 | 0 | 0 | 746 | 1650 | 0 | 0 | .45 | 65 | 11.5 | B | 20.0 | 13.7 |
| * | 12 | 1 | 350 | 128 | 0 | 874 | 128 | 0 | 874 | 1650 | 0 | 0 | .53 | 65 | 13.4 | B | 20.0 | 13.7 |
| * | 13 | 1 | 350 | 0 | 0 | 874 | 0 | 0 | 874 | 1650 | 0 | 0 | .53 | 65 | 13.4 | B | 20.0 | 13.7 |
| * | 14 | 1 | 350 | 0 | 71 | 874 | 0 | 71 | 874 | 1650 | 0 | 0 | .53 | 65 | 13.4 | B | 20.0 | 13.7 |
| * | 15 | 1 | 700 | 0 | 0 | 803 | 0 | 0 | 803 | 1650 | 0 | 0 | .49 | 65 | 12.3 | B | 20.0 | 13.7 |
| * | 16 | 1 | 900 | 17 | 0 | 820 | 17 | 0 | 820 | 1650 | 0 | 0 | .50 | 65 | 12.6 | B | 20.0 | 13.7 |
| * | 17 | 1 | 1400 | 57 | 0 | 877 | 57 | 0 | 877 | 1650 | 0 | 0 | .53 | 65 | 13.5 | B | 20.0 | 13.7 |
| * | 18 | 1 | 200 | 0 | 0 | 877 | 0 | 0 | 877 | 1650 | 0 | 0 | .53 | 65 | 13.5 | B | 20.0 | 13.7 |
| * | 19 | 1 | 1400 | 0 | 39 | 877 | 0 | 39 | 877 | 1650 | 0 | 0 | .53 | 65 | 13.5 | B | 20.0 | 13.7 |
| * | 20 | 1 | 900 | 0 | 0 | 838 | 0 | 0 | 838 | 1650 | 0 | 0 | .51 | 65 | 12.9 | B | 20.0 | 13.7 |
| * | 21 | 1 | 100 | 32 | 0 | 870 | 32 | 0 | 870 | 1650 | 0 | 0 | .53 | 65 | 13.4 | B | 20.0 | 13.7 |
| * | 22 | 1 | 100 | 0 | 10 | 870 | 0 | 10 | 870 | 1650 | 0 | 0 | .53 | 65 | 13.4 | B | 20.0 | 13.7 |
| * | 23 | 1 | 600 | 0 | 0 | 860 | 0 | 0 | 860 | 1650 | 0 | 0 | .52 | 65 | 13.2 | B | 20.0 | 13.7 |
| * | 24 | 1 | 1500 | 87 | 0 | 947 | 87 | 0 | 947 | 1650 | 0 | 0 | .57 | 65 | 14.6 | B | 20.0 | 13.7 |
| * | 25 | 1 | 1500 | 0 | 0 | 947 | 0 | 0 | 947 | 1650 | 0 | 0 | .57 | 65 | 14.6 | B | 20.0 | 13.7 |
| * | 26 | 1 | 8000 | 0 | 947 | 947 | 0 | 947 | 947 | 1650 | 0 | 0 | .57 | 65 | 14.6 | B | 20.0 | 13.7 |
| * | 27 | | | | | | | | | | | | | | | | | |
| * | 28 | | | | | | | | | | | | | | | | | |
| * | 29 | | | | | | | | | | | | | | | | | |
| * | TOTAL | 131999 | = | 25.0 | MILES | | | | MAX(V/C) = 0.60 | LOWEST LOS = B | AVG = 65 | 14.7 | 20.0 | 13.7 | | | | |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 16:45 PAGE 6
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 1 OF 2

| | CURRENT TIME SLICE | | CUMULATIVE VALUES |
|-----------------------------|--------------------|-----------------|--------------------------------|
| FREWAY TRAVEL TIME = | 369. VEH-HRS | 737. PASS-HRS | 369. VEH-HRS 737. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 369. VEH-HRS | 737. PASS-HRS | 369. VEH-HRS 737. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 23968. VEH-MI. | 47936. PASS-MI. | 23968. VEH-MI. 47936. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 65. MPH. | | 65. MPH. |
| AVERAGE DENSITY = | 15. VPMP | | 15. VPMP |
| TOTAL FUEL = | 1198. GALLONS | | 1198. GALLONS |
| TOTAL EMISSIONS = | 329. KILOGRAMS | | 329. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 16:45 PAGE 7
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 2

 ** FREWAY TRAVEL TIME (MI MINUTES) **

| * ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | |
|----------------|---------------------|-------|-------|-------|-------|-------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 19.74 | 20.05 | 20.86 | 21.05 | 23.08 | 0.00 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 1.96 | 3.99 | 0.00 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.21 | 0.00 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.90 | 0.00 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.74 | 0.00 |


```

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP EEE
FFFFFFFF RRRRRRRR EEEEE QQQ QQQ 1111 222 PPPPPPPP EEEEE
FFFFFFFF RRRRRRRR EEEEE QQQ QQQ 1111 222 PPPPPPPP EEEEE
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP EEEEEEEEE
    
```

FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREEWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SEC | LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT DES TRUCKS | SPECIAL RAMP | FF. SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION | LOCATION |
|---------|------|-----------|-----------|-------------|--------------|---------|---------|-----------|---------|----------------|--------------|-------------------|---------------|-----------------------------|--------------------------|------------|----------|
| ** 1 | ** 5 | ** 10000. | ** 1370. | ** 65 | ** OD | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Seeding | ** | ** |
| ** 2 | ** 3 | ** 7360. | ** 99999. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Queue Capture | ** | ** | |
| ** 3 | ** 3 | ** 6000. | ** 2740. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** SR-85 Off to Shore On | ** | ** | |
| ** 4 | ** 3 | ** 6000. | ** 600. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Shore. On to Moffett Off | ** | ** | |
| ** 5 | ** 3 | ** 6000. | ** 700. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Moffett Off to On | ** | ** | |
| ** 6 | ** 3 | ** 6000. | ** 2630. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Moffett On to Ellis Off | ** | ** | |
| ** 7 | ** 3 | ** 6000. | ** 2530. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Ellis Off to On-ramp | ** | ** | |
| ** 8 | ** 4 | ** 6440. | ** 1500. | ** 65 | ** 0 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Ellis On-ramp | ** | ** |
| ** 9 | ** 4 | ** 6440. | ** 700. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Ellis / US 237 | ** | ** | |
| ** 10 | ** 4 | ** 6440. | ** 1500. | ** 65 | ** D | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** SR-237 EB Off-Ramp | ** | ** |
| ** 11 | ** 3 | ** 6000. | ** 750. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** SR-237 / SR-237 | ** | ** | |
| ** 12 | ** 4 | ** 6550. | ** 350. | ** 65 | ** 0 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** SR-237 EB On-Ramp | ** | ** |
| ** 13 | ** 4 | ** 6550. | ** 350. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** US 237 / Mathilda | ** | ** | |
| ** 14 | ** 4 | ** 6550. | ** 350. | ** 65 | ** D | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Mathilda Off-Ramp | ** | ** |
| ** 15 | ** 3 | ** 6000. | ** 700. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Mathilda / Mathilda | ** | ** | |
| ** 16 | ** 3 | ** 6000. | ** 900. | ** 65 | ** 0 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Mathilda SB On-Ramp | ** | ** |
| ** 17 | ** 3 | ** 6000. | ** 1400. | ** 65 | ** 0 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Mathilda NB On-Ramp | ** | ** |
| ** 18 | ** 3 | ** 6000. | ** 200. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Mathilda / Fair Oaks | ** | ** | |
| ** 19 | ** 3 | ** 6000. | ** 1400. | ** 65 | ** D | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Fair Oaks SB Off-Ramp | ** | ** |
| ** 20 | ** 3 | ** 6000. | ** 900. | ** 65 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Fair Oaks SB/ Fair Oaks | ** | ** | |

FREeway AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC | SSEC | DESIGN | ORG | TRK | SSEC | PCT | PCT | DES | SPECIAL | FF.SPD. | CAP. | ART | GRADE | SUBSECTION | LOCATION |
|---------|------|--------|--------|-----|-----|------|-----|--------|------|---------|----------|----------|------|----------|--------------------------|----------|
| SEC | LNS | CAP | SPEED | DES | FAC | GRAD | TRK | TRUCKS | RAMP | RAMP | ALT. RTE | ALT. RTE | TYPE | ALT. RTE | | |
| ** 21 | 4 | 6230. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Fair Oaks SB On-Ramp | ** |
| ** 22 | 4 | 6230. | 100. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks NB Off-Ramp | ** |
| ** 23 | 3 | 6000. | 600. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks NB/ Fair Oaks | ** |
| ** 24 | 3 | 6000. | 1500. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Oaks On-Ramp to Mid | ** |
| ** 25 | 3 | 6000. | 1500. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mid to Lawrence Off-ramp | ** |
| ** 26 | 3 | 6000. | 8000. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | ** |
| ** 27 | 5 | 10000. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | ** |
| ** 28 | 5 | 7750. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Dummy Bottleneck | ** |
| ** 29 | 5 | 7750. | 1000. | 65 | 0D | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | End of Network | ** |

***** INPUT HAS BEEN COMPLETED *****

QUEUE COLLISION IN SECTION 28 T2 =0.044
QUEUE COLLISION IN SECTION 10 T2 =0.848

FREeway TRAVEL TIME (MINUTES)

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | |
|--------------|---------------------|-------|-------|-------|-------|-------|
| | 1 | 2 | 3 | 4 | 5 | 6 |
| * 1 * | 0.24 | 22.63 | 23.71 | 26.94 | 28.01 | 45.82 |
| * 2 * | 0.00 | 1.43 | 2.51 | 5.74 | 6.82 | 24.62 |
| * 3 * | 0.00 | 0.00 | 0.65 | 3.89 | 4.96 | 22.76 |
| * 4 * | 0.00 | 0.00 | 0.00 | 2.71 | 3.78 | 21.59 |
| * 5 * | 0.00 | 0.00 | 0.00 | 2.13 | 3.21 | 21.01 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.19 | 18.00 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 17.19 |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.39 |
| * 9 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.14 |
| * 10 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.22 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB SEC | * NO. LNS | * SSEC LENGTH | * O-D ORG | * DATA DES | * DEMANDS SSEC | * ADJUSTED ORG | * VOLUMES DES | * SSEC SSEC | * WEAVE CAP | * CONGEST EFF | * STORAGE LENGTH | * V/C RATIO | * SPEED MPH | * DENSITY VP/MPH | * LOS LEVEL | * FUEL MPG | * EMISSIONS GS/VM |
|-----------|-----------|---------------|-----------|------------|----------------|----------------|---------------|-------------|-------------|-----------------|------------------|-------------|-------------|------------------|-------------|------------|-------------------|
| * 1 | 5 | 1370. | 7621. | 1524. | 7621. | 7621. | 1524. | 7621. | 10000. | 0. | 0. | .76 | 64. | 23.8 | C | 19.6 | 13.7 |
| * 2 | 3 | 99999. | 0. | 0. | 6097. | 0. | 0. | 6000. | 7360. | 0. | * 1368. | .82 | 61. | 33.0 | F | 20.4 | 13.1 |
| * 3 | 3 | 2740. | 0. | 0. | 6097. | 0. | 0. | 6000. | 6000. | 0. | 0. | 1.00 | 52. | 38.3 | E | 23.8 | 11.1 |
| * 4 | 3 | 600. | 0. | 0. | 6097. | 0. | 0. | 6000. | 6000. | 0. | 0. | 1.00 | 52. | 38.3 | E | 23.8 | 11.1 |
| * 5 | 3 | 700. | 0. | 0. | 6097. | 0. | 0. | 6000. | 6000. | 0. | 0. | 1.00 | 52. | 38.3 | E | 23.8 | 11.1 |
| * 6 | 3 | 2630. | 0. | 0. | 6097. | 0. | 0. | 3386. | 6000. | 0. | * 1086. | .56 | 50. | 22.4 | F | 23.6 | 11.2 |
| * 7 | 3 | 2530. | 0. | 0. | 6097. | 0. | 0. | 3386. | 6000. | 0. | ** 2530. | .56 | 38. | 29.6 | F | 22.1 | 11.9 |
| * 8 | 4 | 1500. | 336. | 0. | 6433. | 286. | 0. | 3672. | 6386. | 0. | ** 1500. | .57 | 31. | 29.7 | F | 20.5 | 12.8 |
| * 9 | 4 | 700. | 0. | 0. | 6433. | 0. | 0. | 3672. | 6440. | 0. | ** 700. | .57 | 27. | 33.4 | F | 19.6 | 13.2 |
| * 10 | 4 | 1500. | 0. | 1304. | 6433. | 0. | 1194. | 3672. | 6134. | 0. | ** 1500. | .60 | 29. | 31.8 | F | 20.2 | 12.9 |
| * 11 | 3 | 750. | 0. | 0. | 5129. | 0. | 0. | 2430. | 6000. | 0. | ** 750. | .40 | 20. | 40.6 | F | 17.2 | 15.1 |
| * 12 | 4 | 350. | 480. | 0. | 5609. | 430. | 0. | 2860. | 6453. | 0. | ** 350. | .44 | 19. | 36.8 | F | 16.1 | 16.2 |
| * 13 | 4 | 350. | 0. | 0. | 5609. | 0. | 0. | 2860. | 6550. | 0. | ** 350. | .44 | 18. | 39.6 | F | 15.9 | 16.4 |
| * 14 | 4 | 350. | 0. | 421. | 5609. | 0. | 399. | 2860. | 6461. | 0. | ** 350. | .44 | 17. | 41.1 | F | 15.7 | 16.6 |
| * 15 | 3 | 700. | 0. | 0. | 5188. | 0. | 0. | 2461. | 6000. | 0. | ** 700. | .41 | 15. | 53.6 | F | 16.1 | 16.0 |
| * 16 | 3 | 900. | 761. | 0. | 5949. | 661. | 0. | 3122. | 5831. | 0. | ** 900. | .54 | 18. | 58.8 | F | 16.7 | 15.3 |
| * 17 | 3 | 1400. | 327. | 0. | 6276. | 240. | 0. | 3362. | 5927. | 0. | ** 1400. | .57 | 17. | 66.0 | F | 16.4 | 15.6 |
| * 18 | 3 | 200. | 0. | 0. | 6276. | 0. | 0. | 3362. | 6000. | 0. | ** 200. | .56 | 16. | 71.0 | F | 15.8 | 16.1 |
| * 19 | 3 | 1400. | 0. | 479. | 6276. | 0. | 442. | 3362. | 5919. | 0. | ** 1400. | .57 | 15. | 74.1 | F | 15.6 | 16.4 |
| * 20 | 3 | 900. | 0. | 0. | 5797. | 0. | 0. | 2920. | 6000. | 0. | ** 900. | .49 | 12. | 83.5 | F | 14.2 | 17.8 |
| * 21 | 4 | 100. | 225. | 0. | 6022. | 225. | 0. | 3145. | 6175. | 0. | ** 100. | .51 | 12. | 66.6 | F | 13.1 | 19.4 |
| * 22 | 4 | 100. | 0. | 128. | 6022. | 0. | 119. | 3145. | 6208. | 0. | ** 100. | .51 | 12. | 67.7 | F | 13.0 | 19.4 |
| * 23 | 3 | 600. | 0. | 0. | 5894. | 0. | 0. | 3026. | 6000. | 0. | ** 600. | .50 | 11. | 90.4 | F | 13.7 | 18.3 |
| * 24 | 3 | 1500. | 184. | 0. | 6078. | 184. | 0. | 3210. | 5954. | 0. | ** 1500. | .54 | 11. | 95.7 | F | 13.5 | 18.7 |
| * 25 | 3 | 1500. | 0. | 0. | 6078. | 0. | 0. | 3210. | 6000. | 0. | ** 1500. | .53 | 10. | 107.6 | F | 12.7 | 19.7 |
| * 26 | 3 | 8000. | 0. | 0. | 6078. | 0. | 0. | 3210. | 6000. | 0. | ** 8000. | .53 | 7. | 147.9 | F | 10.5 | 23.4 |
| * 27 | 5 | 100. | 1520. | 0. | 7598. | 1520. | 0. | 4730. | 10000. | 0. | ** 100. | .47 | 5. | 208.1 | F | 8.7 | 28.0 |
| * 28 | 5 | 1000. | 1560. | 0. | 9158. | 1460. | 0. | 6190. | 7750. | 0. | ** 1000. | .80 | 12. | 100.6 | F | 14.4 | 20.9 |
| * 29 | 5 | 1000. | 1560. | 10718. | 10718. | 1560. | 7750. | 7750. | 7750. | 0. | 0. | 1.00 | 52. | 29.7 | E | 23.8 | 11.1 |
| ***** | | | | | | | | | | | | | | | | | |
| * TOTAL | 135469. | = | 25.7 | MILES | | | | | | MAX(V/C) = 1.00 | LOWEST LOS = F | AVG = 38. | 43.5 | | | 19.4 | 13.7 |
| ***** | | | | | | | | | | | | | | | | | |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 2/29/2016 13:30 PAGE 7
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL NO DIVERSION
 TIME SLICE 1 OF 3

| CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | |
|----------------------------|---------|------------|---------|-------------------|---------|------------|---------|
| FREEWAY TRAVEL TIME = | 3885. | VEH-HRS | 3923. | PASS-HRS | 3885. | VEH-HRS | 3923. |
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. |
| ON-RAMP MRG/CAP DELAY = | 194. | VEH-HRS | 204. | PASS-HRS | 194. | VEH-HRS | 204. |
| OFF-RAMP DELAY = | 24. | VEH-HRS | 24. | PASS-HRS | 24. | VEH-HRS | 24. |
| TOTAL SYSTEM TRAVEL TIME = | 4103. | VEH-HRS | 4151. | PASS-HRS | 4103. | VEH-HRS | 4151. |
| TOTAL TRAVEL DISTANCE = | 149534. | VEH-MI. | 150536. | PASS-MI. | 149534. | VEH-MI. | 150536. |
| AVERAGE SYSTEM SPEED = | 36. | MPH. | | | 38. | MPH. | |
| AVERAGE DENSITY = | 43. | VP/MPH | | | 43. | VP/MPH | |
| TOTAL FUEL = | 7800. | GALLONS | | | 7800. | GALLONS | |
| TOTAL EMISSIONS = | 2079. | KI LOGRAMS | | | 2079. | KI LOGRAMS | |

| ***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 ***** | | | | | | | | | |
|---|--------|------------|--------|------------|-------|------------|-------|------------|--------|
| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
| 1 | 0.49 | 2 | 126.42 | 3 | 11.72 | 4 | 2.57 | 5 | 2.99 |
| 6 | 13.17 | 7 | 30.14 | 8 | 28.46 | 9 | 16.15 | 10 | 31.23 |
| 11 | 21.43 | 12 | 11.29 | 13 | 12.38 | 14 | 12.91 | 15 | 27.57 |
| 16 | 33.20 | 17 | 56.26 | 18 | 8.74 | 19 | 63.74 | 20 | 50.25 |
| 21 | 5.72 | 22 | 5.82 | 23 | 35.35 | 24 | 89.98 | 25 | 100.02 |
| 26 | 684.72 | 27 | 18.63 | 28 | 77.66 | 29 | 5.53 | | |

***** TOTAL DELAY = 1584.5 VEH-HRS ***** AVERAGE DELAY = 27.69 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 2/29/2016 13:30 PAGE 8
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL NO DIVERSION
 TIME SLICE 1 OF 3

| ***** RAMP DELAYS ***** | | | | | | | | | |
|-------------------------|--------------|---------|----------------|------|-------|------|------|-----------|------|
| | QUEUE LENGTH | DELAY | AVERAGE | GAS | HC | CO | NOX | TOTAL | |
| | VEHICLES | VEH-HRS | METERING DELAY | GALS | KGMS | KGMS | KGMS | EMISSIONS | |
| | | | MINUTES | | | | | KGMS | |
| ON-RAMP 2 | RAMP | 50. | 25.00 | 4.46 | 8.93 | 0.55 | 2.90 | 0.15 | 3.60 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 50. | 25.00 | 4.46 | 8.93 | 0.55 | 2.90 | 0.15 | 3.60 |
| ON-RAMP 3 | RAMP | 50. | 25.00 | 3.13 | 8.93 | 0.55 | 2.90 | 0.15 | 3.60 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 50. | 25.00 | 3.13 | 8.93 | 0.55 | 2.90 | 0.15 | 3.60 |
| ON-RAMP 4 | RAMP | 100. | 50.00 | 3.94 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 50.00 | 3.94 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| ON-RAMP 5 | RAMP | 87. | 43.50 | 7.98 | 15.53 | 0.96 | 5.04 | 0.27 | 6.27 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 87. | 43.50 | 7.98 | 15.53 | 0.96 | 5.04 | 0.27 | 6.27 |

 * TOTAL 135469. = 25.7 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 38. 46.5 19.0 14.6 *

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 2/29/2016 13:30 PAGE 12
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 3

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|----------------------------|--------------------|------------------|-------------------|------------------|
| FREEWAY TRAVEL TIME = | 3786. VEH-HRS | 3818. PASS-HRS | 7671. VEH-HRS | 7741. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 395. VEH-HRS | 415. PASS-HRS | 588. VEH-HRS | 618. PASS-HRS |
| OFF-RAMP DELAY = | 109. VEH-HRS | 109. PASS-HRS | 133. VEH-HRS | 133. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 4289. VEH-HRS | 4342. PASS-HRS | 8391. VEH-HRS | 8493. PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 144749. VEH-MI. | 145774. PASS-MI. | 294284. VEH-MI. | 296309. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 34. MPH. | | 38. MPH. | |
| AVERAGE DENSITY = | 46. VPMPPL | | 45. VPMPPL | |
| TOTAL FUEL = | 7793. GALLONS | | 15594. GALLONS | |
| TOTAL EMISSIONS = | 2179. KI LOGRAMS | | 4258. KI LOGRAMS | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|--------|------------|--------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 98.36 | 3 | 62.81 | 4 | 18.63 | 5 | 23.95 |
| 6 | 108.40 | 7 | 109.86 | 8 | 67.85 | 9 | 32.95 | 10 | 56.02 |
| 11 | 52.03 | 12 | 24.45 | 13 | 25.55 | 14 | 24.48 | 15 | 47.57 |
| 16 | 35.99 | 17 | 46.56 | 18 | 7.15 | 19 | 45.47 | 20 | 47.45 |
| 21 | 5.16 | 22 | 5.25 | 23 | 30.85 | 24 | 68.10 | 25 | 70.14 |
| 26 | 374.09 | 27 | 13.77 | 28 | 50.52 | 29 | 5.53 | | |

***** TOTAL DELAY = 1558.9 VEH-HRS ***** AVERAGE DELAY = 17.32 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 2/29/2016 13:30 PAGE 13
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 3

***** RAMP DELAYS *****

| | | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS | |
|----------|---|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|-------|
| ON-RAMP | 2 | RAMP | 50. | 50.00 | 6.94 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 50. | 50.00 | 6.94 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| ON-RAMP | 3 | RAMP | 50. | 50.00 | 5.34 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 50. | 50.00 | 5.34 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| ON-RAMP | 4 | RAMP | 100. | 100.00 | 6.59 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 100.00 | 6.59 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP | 5 | RAMP | 100. | 93.50 | 12.38 | 33.39 | 2.07 | 10.83 | 0.57 | 13.48 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 93.50 | 12.38 | 33.39 | 2.07 | 10.83 | 0.57 | 13.48 |
| ON-RAMP | 6 | RAMP | 2. | 1.00 | 0.25 | 0.36 | 0.02 | 0.12 | 0.01 | 0.14 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 2. | 1.00 | 0.25 | 0.36 | 0.02 | 0.12 | 0.01 | 0.14 |
| ON-RAMP | 9 | RAMP | 100. | 100.00 | 11.63 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 100.00 | 11.63 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| OFF-RAMP | 2 | OUTPUT POINT | 169. | 108.55 | | 38.76 | 2.40 | 12.58 | 0.67 | 15.65 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 2/29/2016 13:30 PAGE 14
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 3 OF 3

 ** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS | DESTINATIONS ACROSS | | | | | |
|-----------|---------------------|-------|-------|-------|-------|-------|
| * DOWN | 1 | 2 | 3 | 4 | 5 | 6 |
| * 1 * | 0.24 | 30.68 | 32.92 | 36.60 | 37.66 | 48.68 |
| * 2 * | 0.00 | 3.01 | 5.25 | 8.94 | 10.00 | 21.02 |
| * 3 * | 0.00 | 0.00 | 1.25 | 4.94 | 6.00 | 17.02 |

***** RAMP DELAYS *****

| | | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|----------|---|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|
| ON-RAMP | 2 | RAMP | 50. | 50.00 | 9.15 | 17.85 | 1.11 | 5.79 | 7.21 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 50. | 50.00 | 9.15 | 17.85 | 1.11 | 5.79 | 7.21 |
| ON-RAMP | 3 | RAMP | 50. | 50.00 | 5.11 | 17.85 | 1.11 | 5.79 | 7.21 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 50. | 50.00 | 5.11 | 17.85 | 1.11 | 5.79 | 7.21 |
| ON-RAMP | 4 | RAMP | 100. | 100.00 | 8.08 | 35.71 | 2.22 | 11.58 | 14.41 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 100.00 | 8.08 | 35.71 | 2.22 | 11.58 | 14.41 |
| ON-RAMP | 5 | RAMP | 100. | 100.00 | 13.99 | 35.71 | 2.22 | 11.58 | 14.41 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 100.00 | 13.99 | 35.71 | 2.22 | 11.58 | 14.41 |
| ON-RAMP | 6 | RAMP | 0. | 1.00 | 0.04 | 0.36 | 0.02 | 0.12 | 0.14 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 0. | 1.00 | 0.04 | 0.36 | 0.02 | 0.12 | 0.14 |
| ON-RAMP | 9 | RAMP | 100. | 100.00 | 8.57 | 35.71 | 2.22 | 11.58 | 14.41 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 100.00 | 8.57 | 35.71 | 2.22 | 11.58 | 14.41 |
| OFF-RAMP | 2 | OUTPUT POINT | 109. | 139.06 | | 49.66 | 3.08 | 16.11 | 20.04 |


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FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP LLL
FFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 1111111 222222222 PPP LLLLLLLLLL
    
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FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 2 AND 26 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65 MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

FREWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC | SSEC | DESIGN | ORG | TRK | SSEC | PCT | PCT | DES | SPECIAL | FF.SPD. | CAP. | ART | GRADE | SUBSECTION | LOCATION |
|---------|------|-------|--------|-----|-----|------|-----|--------|------|---------|----------|----------|------|----------|-------------------------|----------|
| SEC | LNS | CAP | LENGTH | DES | FAC | GRAD | TRK | TRUCKS | RAMP | RAMP | ALT. RTE | ALT. RTE | TYPE | ALT. RTE | | |
| 1 | | | | | | | | | | | | | | | | |
| 2 | 1 | 1650. | 99999. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | |
| 3 | 1 | 1650. | 2740. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-85 Off to Shore On | |
| 4 | 1 | 1650. | 600. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Shore. On to Moffet Off | |
| 5 | 1 | 1650. | 700. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Moffett Off to On | |
| 6 | 1 | 1650. | 2630. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Moffett On to Ellis Off | |
| 7 | 1 | 1650. | 2530. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Ellis Off to On-ramp | |
| 8 | 1 | 1650. | 1500. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Ellis On-ramp | |
| 9 | 1 | 1650. | 700. | 65 | | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Ellis / US 237 | |
| 10 | 1 | 1650. | 1500. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 EB Off-Ramp | |
| 11 | 1 | 1650. | 750. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 / SR-237 | |
| 12 | 1 | 1650. | 350. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 EB On-Ramp | |
| 13 | 1 | 1650. | 350. | 65 | | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | US 237 / Mathilda | |
| 14 | 1 | 1650. | 350. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-Ramp | |
| 15 | 1 | 1650. | 700. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | |
| 16 | 1 | 1650. | 900. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda SB On-Ramp | |
| 17 | 1 | 1650. | 1400. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda NB On-Ramp | |
| 18 | 1 | 1650. | 200. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Fair Oaks | |
| 19 | 1 | 1650. | 1400. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks SB Off-Ramp | |

** 20 1 1650. 900. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks SB/ Fair Oaks **

FREEWAY AND ARTERIAL DESIGN FEATURES

Table with columns: SUB NO., SEC LNS, SSEC CAP, SSEC LENGTH, DESIGN SPEED, ORG DES, TRK FAC, SSEC GRAD, PCT TRK, PCT TRUCKS, SPECIAL RAMP, FF. SPD. ALT. RTE, CAP. ALT. RTE, ART TYPE, GRADE ALT. RTE, SUBSECTION, LOCATION. Rows 21-29.

FREEWAY TRAVEL TIME (MINUTES)

Table with columns: ORIGINS DOWN, DESTINATIONS ACROSS (1-7). Rows 1-11.

TIME SLICE FREEWAY PERFORMANCE TABLE

US-101_SB_PM_NP_2018_MOD_PL.txt

| * SUB SEC | NO. LNS | SSEC LENGTH | O-D ORG | DATA DES | DEMANDS SSEC | ADJUSTED ORG | VOLUMES DES | SSEC SSEC | WEAVE CAP. | CONGEST EFF | STORAGE LENGTH | V/C RATIO | SPEED MPH | DENSITY VPMP | LOS LEVEL | FUEL MPG | EMI SS GS/VM |
|-----------|---------|-------------|---------|----------|--------------|--------------|-------------|-----------|------------|-------------|----------------|-----------------|----------------|--------------|-----------|----------|--------------|
| * 1 | | | | | | | | | | | | | | | | | |
| * 2 | 1 | 99999 | 1524 | 0 | 1524 | 1524 | 0 | 1524 | 1650 | 0 | 0 | .92 | 58 | 26.4 | D | 23.4 | 11.7 |
| * 3 | 1 | 2740 | 0 | 0 | 1524 | 0 | 0 | 1524 | 1650 | 0 | 0 | .92 | 58 | 26.4 | D | 23.4 | 11.7 |
| * 4 | 1 | 600 | 0 | 0 | 1524 | 0 | 0 | 1524 | 1650 | 0 | 0 | .92 | 58 | 26.4 | D | 23.4 | 11.7 |
| * 5 | 1 | 700 | 0 | 0 | 1524 | 0 | 0 | 1524 | 1650 | 0 | 0 | .92 | 58 | 26.4 | D | 23.4 | 11.7 |
| * 6 | 1 | 2630 | 0 | 0 | 1524 | 0 | 0 | 1524 | 1650 | 0 | 0 | .92 | 58 | 26.4 | D | 23.4 | 11.7 |
| * 7 | 1 | 2530 | 0 | 0 | 1524 | 0 | 0 | 1524 | 1650 | 0 | 0 | .92 | 58 | 26.4 | D | 23.4 | 11.7 |
| * 8 | 1 | 1500 | 54 | 0 | 1578 | 54 | 0 | 1578 | 1650 | 0 | 0 | .96 | 56 | 28.3 | D | 24.2 | 11.3 |
| * 9 | 1 | 700 | 0 | 0 | 1578 | 0 | 0 | 1578 | 1650 | 0 | 0 | .96 | 56 | 28.3 | D | 24.2 | 11.3 |
| * 10 | 1 | 1500 | 0 | 306 | 1578 | 0 | 285 | 1578 | 1650 | 0 | 0 | .96 | 56 | 28.3 | D | 24.2 | 11.3 |
| * 11 | 1 | 750 | 0 | 0 | 1271 | 0 | 0 | 1271 | 1650 | 0 | 0 | .77 | 65 | 19.6 | C | 20.0 | 13.7 |
| * 12 | 1 | 350 | 97 | 0 | 1369 | 97 | 0 | 1369 | 1650 | 0 | 0 | .83 | 65 | 21.1 | C | 20.0 | 13.7 |
| * 13 | 1 | 350 | 0 | 0 | 1369 | 0 | 0 | 1369 | 1650 | 0 | 0 | .83 | 65 | 21.1 | C | 20.0 | 13.7 |
| * 14 | 1 | 350 | 0 | 89 | 1369 | 0 | 89 | 1369 | 1650 | 0 | 0 | .83 | 65 | 21.1 | C | 20.0 | 13.7 |
| * 15 | 1 | 700 | 0 | 0 | 1280 | 0 | 0 | 1280 | 1650 | 0 | 0 | .78 | 65 | 19.7 | C | 20.0 | 13.7 |
| * 16 | 1 | 900 | 169 | 0 | 1449 | 169 | 0 | 1449 | 1650 | 0 | 0 | .88 | 65 | 22.3 | C | 20.0 | 13.7 |
| * 17 | 1 | 1400 | 73 | 0 | 1522 | 73 | 0 | 1522 | 1650 | 0 | 0 | .92 | 58 | 26.3 | D | 23.4 | 11.7 |
| * 18 | 1 | 200 | 0 | 0 | 1522 | 0 | 0 | 1522 | 1650 | 0 | 0 | .92 | 58 | 26.3 | D | 23.4 | 11.7 |
| * 19 | 1 | 1400 | 0 | 81 | 1522 | 0 | 81 | 1522 | 1650 | 0 | 0 | .92 | 58 | 26.3 | D | 23.4 | 11.7 |
| * 20 | 1 | 900 | 0 | 0 | 1441 | 0 | 0 | 1441 | 1650 | 0 | 0 | .87 | 65 | 22.2 | C | 20.0 | 13.7 |
| * 21 | 1 | 100 | 55 | 0 | 1496 | 55 | 0 | 1496 | 1650 | 0 | 0 | .91 | 59 | 25.4 | C | 23.1 | 11.9 |
| * 22 | 1 | 100 | 0 | 22 | 1496 | 0 | 22 | 1496 | 1650 | 0 | 0 | .91 | 59 | 25.4 | C | 23.1 | 11.9 |
| * 23 | 1 | 600 | 0 | 0 | 1474 | 0 | 0 | 1474 | 1650 | 0 | 0 | .89 | 60 | 24.7 | C | 22.9 | 12.0 |
| * 24 | 1 | 1500 | 46 | 0 | 1520 | 46 | 0 | 1520 | 1650 | 0 | 0 | .92 | 58 | 26.2 | D | 23.4 | 11.8 |
| * 25 | 1 | 1500 | 0 | 0 | 1520 | 0 | 0 | 1520 | 1650 | 0 | 0 | .92 | 58 | 26.2 | D | 23.4 | 11.8 |
| * 26 | 1 | 8000 | 0 | 1520 | 1520 | 0 | 1520 | 1520 | 1650 | 0 | 0 | .92 | 58 | 26.2 | D | 23.4 | 11.8 |
| * 27 | | | | | | | | | | | | | | | | | |
| * 28 | | | | | | | | | | | | | | | | | |
| * 29 | | | | | | | | | | | | | | | | | |
| ***** | | | | | | | | | | | | | | | | | |
| * TOTAL | 131999 | = | 25.0 | MILES | | | | | | | | MAX(V/C) = 0.96 | LOWEST LOS = D | AVG = 58. | 26.2 | 23.3 | 11.8 |
| ***** | | | | | | | | | | | | | | | | | |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 13:30 PAGE 6
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 1 OF 3

| | CURRENT TIME SLICE | | CUMULATIVE VALUES |
|-----------------------------|--------------------|-----------------|--------------------------------|
| FREWAY TRAVEL TIME = | 655. VEH-HRS | 1311. PASS-HRS | 655. VEH-HRS 1311. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 10. VEH-HRS | 21. PASS-HRS | 10. VEH-HRS 21. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 666. VEH-HRS | 1332. PASS-HRS | 666. VEH-HRS 1332. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 37998. VEH-MI. | 75996. PASS-MI. | 37998. VEH-MI. 75996. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 57. MPH. | | 58. MPH. |
| AVERAGE DENSITY = | 26. VPMP | | 26. VPMP |
| TOTAL FUEL = | 1633. GALLONS | | 1633. GALLONS |
| TOTAL EMISSIONS = | 449. KILOGRAMS | | 449. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 55.10 | 3 | 1.51 | 4 | 0.33 | 5 | 0.39 |
| 6 | 1.45 | 7 | 1.39 | 8 | 1.15 | 9 | 0.54 | 10 | 1.15 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.76 | 18 | 0.11 | 19 | 0.76 | 20 | 0.00 |
| 21 | 0.05 | 22 | 0.05 | 23 | 0.24 | 24 | 0.80 | 25 | 0.80 |
| 26 | 4.28 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 70.9 VEH-HRS ***** AVERAGE DELAY = 2.79 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-------------------------|-----------------------|---------------|----------|---------|---------|----------|----------------------|
| OFF-RAMP 2 OUTPUT POINT | 21. | 10.47 | 3.59 | 0.23 | 1.18 | 0.06 | 1.47 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 13:30 PAGE 7
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 3

 ** FREWAY TRAVEL TIME (MINUTES) **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN 1 2 3 4 5 6 7 *

| | | | | | | | |
|-------|------|-------|-------|-------|-------|-------|------|
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 19.80 | 20.11 | 20.91 | 21.11 | 23.14 | 0.00 |

| | | | | | | | | | | | | | | | | | | | | |
|---|---|----|---|------|------|------|------|------|------|------|------|--|--|--|--|--|--|--|--|---|
| + | * | 3 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.02 | 4.04 | 0.00 | | | | | | | | | * |
| + | * | 4 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.21 | 0.00 | | | | | | | | | * |
| + | * | 5 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.90 | 0.00 | | | | | | | | | * |
| + | * | 6 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.74 | 0.00 | | | | | | | | | * |
| + | * | 7 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.06 | 0.00 | | | | | | | | | * |
| + | * | 8 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.92 | 0.00 | | | | | | | | | * |
| + | * | 9 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | | | | | | | | * |
| + | * | 10 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | | | | | | | | * |
| + | * | 11 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | | | | | | | | * |
| + | * | * | * | | | | | | | | | | | | | | | | | * |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB | * NO. | * SSEC | * O-D | * DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | |
|---------|---------|----------|-------|--------|-----------|------------|-----------|--------|---------|-----------------|----------------|-----------|---------|-----------|--------|---------|-------------|---------|--|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | |
| * 1 | | | | | | | | | | | | | | | | | | | |
| * 2 | 1 | 99999. | 1414. | 0. | 1414. | 1414. | 0. | 1414. | 1650. | 0. | 0. | 0. | .86 | 65. | 21.8 | C | 20.0 | 13.7 | |
| * 3 | 1 | 2740. | 0. | 0. | 1414. | 0. | 0. | 1414. | 1650. | 0. | 0. | 0. | .86 | 65. | 21.8 | C | 20.0 | 13.7 | |
| * 4 | 1 | 600. | 0. | 0. | 1414. | 0. | 0. | 1414. | 1650. | 0. | 0. | 0. | .86 | 65. | 21.8 | C | 20.0 | 13.7 | |
| * 5 | 1 | 700. | 0. | 0. | 1414. | 0. | 0. | 1414. | 1650. | 0. | 0. | 0. | .86 | 65. | 21.8 | C | 20.0 | 13.7 | |
| * 6 | 1 | 2630. | 0. | 0. | 1414. | 0. | 0. | 1414. | 1650. | 0. | 0. | 0. | .86 | 65. | 21.8 | C | 20.0 | 13.7 | |
| * 7 | 1 | 2530. | 0. | 0. | 1414. | 0. | 0. | 1414. | 1650. | 0. | 0. | 0. | .86 | 65. | 21.8 | C | 20.0 | 13.7 | |
| * 8 | 1 | 1500. | 57. | 0. | 1471. | 57. | 0. | 1471. | 1650. | 0. | 0. | 0. | .89 | 60. | 24.7 | C | 22.8 | 12.1 | |
| * 9 | 1 | 700. | 0. | 0. | 1471. | 0. | 0. | 1471. | 1650. | 0. | 0. | 0. | .89 | 60. | 24.7 | C | 22.8 | 12.1 | |
| * 10 | 1 | 1500. | 0. | 301. | 1471. | 0. | 282. | 1471. | 1650. | 0. | 0. | 0. | .89 | 60. | 24.7 | C | 22.8 | 12.1 | |
| * 11 | 1 | 750. | 0. | 0. | 1170. | 0. | 0. | 1170. | 1650. | 0. | 0. | 0. | .71 | 65. | 18.0 | B | 20.0 | 13.7 | |
| * 12 | 1 | 350. | 97. | 0. | 1267. | 97. | 0. | 1267. | 1650. | 0. | 0. | 0. | .77 | 65. | 19.5 | C | 20.0 | 13.7 | |
| * 13 | 1 | 350. | 0. | 0. | 1267. | 0. | 0. | 1267. | 1650. | 0. | 0. | 0. | .77 | 65. | 19.5 | C | 20.0 | 13.7 | |
| * 14 | 1 | 350. | 0. | 94. | 1267. | 0. | 94. | 1267. | 1650. | 0. | 0. | 0. | .77 | 65. | 19.5 | C | 20.0 | 13.7 | |
| * 15 | 1 | 700. | 0. | 0. | 1173. | 0. | 0. | 1173. | 1650. | 0. | 0. | 0. | .71 | 65. | 18.0 | C | 20.0 | 13.7 | |
| * 16 | 1 | 900. | 171. | 0. | 1344. | 171. | 0. | 1344. | 1650. | 0. | 0. | 0. | .81 | 65. | 20.7 | C | 20.0 | 13.7 | |
| * 17 | 1 | 1400. | 77. | 0. | 1422. | 77. | 0. | 1422. | 1650. | 0. | 0. | 0. | .86 | 65. | 21.9 | C | 20.0 | 13.7 | |
| * 18 | 1 | 200. | 0. | 0. | 1422. | 0. | 0. | 1422. | 1650. | 0. | 0. | 0. | .86 | 65. | 21.9 | C | 20.0 | 13.7 | |
| * 19 | 1 | 1400. | 0. | 101. | 1422. | 0. | 101. | 1422. | 1650. | 0. | 0. | 0. | .86 | 65. | 21.9 | C | 20.0 | 13.7 | |
| * 20 | 1 | 900. | 0. | 0. | 1321. | 0. | 0. | 1321. | 1650. | 0. | 0. | 0. | .80 | 65. | 20.3 | C | 20.0 | 13.7 | |
| * 21 | 1 | 100. | 58. | 0. | 1379. | 58. | 0. | 1379. | 1650. | 0. | 0. | 0. | .84 | 65. | 21.2 | C | 20.0 | 13.7 | |
| * 22 | 1 | 100. | 0. | 32. | 1379. | 0. | 32. | 1379. | 1650. | 0. | 0. | 0. | .84 | 65. | 21.2 | C | 20.0 | 13.7 | |
| * 23 | 1 | 600. | 0. | 0. | 1347. | 0. | 0. | 1347. | 1650. | 0. | 0. | 0. | .82 | 65. | 20.7 | C | 20.0 | 13.7 | |
| * 24 | 1 | 1500. | 42. | 0. | 1389. | 42. | 0. | 1389. | 1650. | 0. | 0. | 0. | .84 | 65. | 21.4 | C | 20.0 | 13.7 | |
| * 25 | 1 | 1500. | 0. | 0. | 1389. | 0. | 0. | 1389. | 1650. | 0. | 0. | 0. | .84 | 65. | 21.4 | C | 20.0 | 13.7 | |
| * 26 | 1 | 8000. | 0. | 1389. | 1389. | 0. | 1389. | 1389. | 1650. | 0. | 0. | 0. | .84 | 65. | 21.4 | C | 20.0 | 13.7 | |
| * 27 | | | | | | | | | | | | | | | | | | | |
| * 28 | | | | | | | | | | | | | | | | | | | |
| * 29 | | | | | | | | | | | | | | | | | | | |
| * TOTAL | 131999. | = | 25.0 | MILES | | | | | | MAX(V/C) = 0.89 | LOWEST LOS = C | AVG = 65. | 21.7 | | | 20.1 | 13.7 | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 543. VEH-HRS | 1086. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 30. VEH-HRS | 61. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 573. VEH-HRS | 1147. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 35209. VEH-MI. | 70418. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 61. MPH. | 61. MPH. |
| AVERAGE DENSITY = | 22. VPMP | 24. VPMP |
| TOTAL FUEL = | 1764. GALLONS | 3398. GALLONS |
| TOTAL EMISSIONS = | 486. KILOGRAMS | 935. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.58 | 9 | 0.27 | 10 | 0.58 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|-----------------------------|--------------------|-----------------|-------------------|------------------|
| FREEWAY TRAVEL TIME = | 499. VEH-HRS | 997. PASS-HRS | 1697. VEH-HRS | 3395. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 34. VEH-HRS | 68. PASS-HRS | 75. VEH-HRS | 150. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 533. VEH-HRS | 1066. PASS-HRS | 1772. VEH-HRS | 3544. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 32418. VEH-MI. | 64837. PASS-MI. | 105626. VEH-MI. | 211251. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 61. MPH | | 62. MPH | |
| AVERAGE DENSITY = | 20. VPMP | | 23. VPMP | |
| TOTAL FUEL = | 1633. GALLONS | | 5030. GALLONS | |
| TOTAL EMISSIONS = | 450. KILOGRAMS | | 1385. KILOGRAMS | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH | DELAY | GAS | HC | CO | NOX | TOTAL |
|-------------------------|--------------|---------|-------|------|------|------|-----------|
| | VEHICLES | VEH-HRS | GALS | KGMS | KGMS | KGMS | EMISSIONS |
| OFF-RAMP 2 OUTPUT POINT | 28. | 34.04 | 11.68 | 0.74 | 3.84 | 0.20 | 4.78 |

**
**
** FREeway AND ARTERIAL DESIGN FEATURES **
**

| ** SUB NO. | ** SEC LNS | ** SSEC CAP | ** SSEC LENGTH | ** DESIGN SPEED | ** ORG DES | ** TRK FAC | ** SSEC GRAD | ** PCT TRK | ** PCT DES TRUCKS | ** SPECIAL RAMP | ** FF.SPD. ALT. RTE | ** CAP. ALT. RTE | ** ART TYPE | ** GRADE ALT. RTE | ** SUBSECTION | ** LOCATION |
|------------|------------|-------------|----------------|-----------------|------------|------------|--------------|------------|-------------------|-----------------|---------------------|------------------|-------------|-------------------|-----------------------------|-------------|
| ** 21 | ** 4 | ** 6230. | ** 100. | ** 65 | ** 0 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Fair Oaks SB On-Ramp | ** |
| ** 22 | ** 4 | ** 6230. | ** 100. | ** 65 | ** D | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Fair Oaks NB Off-Ramp | ** |
| ** 23 | ** 3 | ** 6000. | ** 600. | ** 65 | ** 0 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Fair Oaks NB/ Fair Oaks | ** |
| ** 24 | ** 3 | ** 6000. | ** 1500. | ** 65 | ** 0 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Oaks On-Ramp to Mid | ** |
| ** 25 | ** 3 | ** 6000. | ** 1500. | ** 65 | ** 0 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Mid to Lawrence Off-ramp | ** |
| ** 26 | ** 3 | ** 6000. | ** 8000. | ** 65 | ** 0 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** HOV Dummy | ** |
| ** 27 | ** 5 | ** 10000. | ** 100. | ** 65 | ** 0 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** HOV Dummy | ** |
| ** 28 | ** 5 | ** 7750. | ** 1000. | ** 65 | ** 0 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Dummy Bottleneck | ** |
| ** 29 | ** 5 | ** 7750. | ** 1000. | ** 65 | ** OD | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** End of Network | ** |

***** INPUT HAS BEEN COMPLETED *****

QUEUE COLLISION IN SECTION 28 T2 =0.044
QUEUE COLLISION IN SECTION 10 T2 =0.838

**
** FREeway TRAVEL TIME (MINUTES) **
**

| ** ORIGINS DOWN | ** DESTINATIONS ACROSS | | | | | |
|-----------------|------------------------|----------|----------|----------|----------|----------|
| ** | ** 1 | ** 2 | ** 3 | ** 4 | ** 5 | ** 6 |
| ** 1 * | ** 0.24 | ** 22.66 | ** 23.76 | ** 27.05 | ** 28.14 | ** 46.05 |
| ** 2 * | ** 0.00 | ** 1.46 | ** 2.56 | ** 5.86 | ** 6.94 | ** 24.85 |
| ** 3 * | ** 0.00 | ** 0.00 | ** 0.67 | ** 3.96 | ** 5.05 | ** 22.96 |
| ** 4 * | ** 0.00 | ** 0.00 | ** 0.00 | ** 2.76 | ** 3.85 | ** 21.76 |
| ** 5 * | ** 0.00 | ** 0.00 | ** 0.00 | ** 2.16 | ** 3.25 | ** 21.16 |
| ** 6 * | ** 0.00 | ** 0.00 | ** 0.00 | ** 0.00 | ** 0.20 | ** 18.10 |
| ** 7 * | ** 0.00 | ** 0.00 | ** 0.00 | ** 0.00 | ** 0.00 | ** 17.29 |
| ** 8 * | ** 0.00 | ** 0.00 | ** 0.00 | ** 0.00 | ** 0.00 | ** 1.39 |
| ** 9 * | ** 0.00 | ** 0.00 | ** 0.00 | ** 0.00 | ** 0.00 | ** 1.14 |
| ** 10 * | ** 0.00 | ** 0.00 | ** 0.00 | ** 0.00 | ** 0.00 | ** 0.22 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB SEC | NO. LNS | SSEC LENGTH | O-D ORG | DATA DES | DEMANDS SSEC | ADJUSTED ORG | VOLUMES DES | SSEC SSEC | WEAVE CAP. | CONGEST EFF | STORAGE LENGTH | V/C RATIO | SPEED MPH | DENSITY VPMP | LOS LEVEL | FUEL MPG | EMI SS GS/VM | | |
|---------|---------|-------------|---------|----------|--------------|--------------|-------------|-----------|------------|-------------|-----------------|----------------|-----------|--------------|-----------|----------|--------------|------|------|
| * | 1 | 5 | 1370. | 7619. | 1524. | 7619. | 7619. | 1524. | 7619. | 10000. | 0. | 0. | 0. | .76 | 64. | 23.8 | C | 19.6 | 13.7 |
| * | 2 | 3 | 99999. | 0. | 0. | 6095. | 0. | 0. | 6000. | 7360. | 0. | * 1340. | 95. | .82 | 61. | 32.9 | F | 20.4 | 13.1 |
| * | 3 | 3 | 2740. | 0. | 0. | 6095. | 0. | 0. | 6000. | 6000. | 0. | 0. | 0. | 1.00 | 52. | 38.3 | E | 23.8 | 11.1 |
| * | 4 | 3 | 600. | 0. | 0. | 6095. | 0. | 0. | 6000. | 6000. | 0. | 0. | 0. | 1.00 | 52. | 38.3 | E | 23.8 | 11.1 |
| * | 5 | 3 | 700. | 0. | 0. | 6095. | 0. | 0. | 6000. | 6000. | 0. | 0. | 0. | 1.00 | 52. | 38.3 | E | 23.8 | 11.1 |
| * | 6 | 3 | 2630. | 0. | 0. | 6095. | 0. | 0. | 3373. | 6000. | 0. | * 1190. | 2627. | .56 | 50. | 22.4 | F | 23.6 | 11.2 |
| * | 7 | 3 | 2530. | 0. | 0. | 6095. | 0. | 0. | 3373. | 6000. | 0. | ** 2530. | 2627. | .56 | 38. | 29.9 | F | 22.0 | 11.9 |
| * | 8 | 4 | 1500. | 336. | 0. | 6431. | 286. | 0. | 3659. | 6386. | 0. | ** 1500. | 2627. | .57 | 31. | 30.0 | F | 20.4 | 12.8 |
| * | 9 | 4 | 700. | 0. | 0. | 6431. | 0. | 0. | 3659. | 6440. | 0. | ** 700. | 2627. | .57 | 27. | 33.7 | F | 19.6 | 13.3 |
| * | 10 | 4 | 1500. | 0. | 1231. | 6431. | 0. | 1176. | 3659. | 6151. | 0. | ** 1500. | 2492. | .59 | 28. | 32.6 | F | 20.1 | 13.1 |
| * | 11 | 3 | 750. | 0. | 0. | 5200. | 0. | 0. | 2483. | 6000. | 0. | ** 750. | 2492. | .41 | 20. | 42.0 | F | 17.2 | 15.1 |
| * | 12 | 4 | 350. | 481. | 0. | 5681. | 431. | 0. | 2914. | 6544. | 0. | ** 350. | 2492. | .45 | 19. | 38.4 | F | 16.0 | 16.3 |
| * | 13 | 4 | 350. | 0. | 0. | 5681. | 0. | 0. | 2914. | 6640. | 0. | ** 350. | 2492. | .44 | 18. | 41.2 | F | 15.8 | 16.5 |
| * | 14 | 4 | 350. | 0. | 495. | 5681. | 0. | 470. | 2914. | 6535. | 0. | ** 350. | 2492. | .45 | 17. | 42.6 | F | 15.6 | 16.7 |
| * | 15 | 3 | 700. | 0. | 0. | 5186. | 0. | 0. | 2444. | 6000. | 0. | ** 700. | 2492. | .41 | 15. | 54.6 | F | 16.1 | 16.1 |
| * | 16 | 3 | 900. | 720. | 0. | 5906. | 620. | 0. | 3064. | 5840. | 0. | ** 900. | 2492. | .52 | 17. | 59.8 | F | 16.5 | 15.5 |
| * | 17 | 3 | 1400. | 393. | 0. | 6299. | 293. | 0. | 3357. | 5913. | 0. | ** 1400. | 2492. | .57 | 17. | 66.9 | F | 16.4 | 15.7 |
| * | 18 | 3 | 200. | 0. | 0. | 6299. | 0. | 0. | 3357. | 6000. | 0. | ** 200. | 2492. | .56 | 16. | 72.0 | F | 15.8 | 16.2 |
| * | 19 | 3 | 1400. | 0. | 479. | 6299. | 0. | 442. | 3357. | 5919. | 0. | ** 1400. | 2492. | .57 | 15. | 75.1 | F | 15.5 | 16.5 |
| * | 20 | 3 | 900. | 0. | 0. | 5820. | 0. | 0. | 2915. | 6000. | 0. | ** 900. | 2492. | .49 | 12. | 84.5 | F | 14.1 | 17.8 |
| * | 21 | 4 | 100. | 225. | 0. | 6045. | 225. | 0. | 3140. | 6175. | 0. | ** 100. | 2492. | .51 | 12. | 67.3 | F | 13.0 | 19.4 |
| * | 22 | 4 | 100. | 0. | 128. | 6045. | 0. | 119. | 3140. | 6208. | 0. | ** 100. | 2492. | .51 | 11. | 68.4 | F | 13.0 | 19.5 |
| * | 23 | 3 | 600. | 0. | 0. | 5917. | 0. | 0. | 3021. | 6000. | 0. | ** 600. | 2492. | .50 | 11. | 91.3 | F | 13.6 | 18.4 |
| * | 24 | 3 | 1500. | 184. | 0. | 6101. | 184. | 0. | 3205. | 5954. | 0. | ** 1500. | 2492. | .54 | 11. | 96.6 | F | 13.4 | 18.7 |
| * | 25 | 3 | 1500. | 0. | 0. | 6101. | 0. | 0. | 3205. | 6000. | 0. | ** 1500. | 2492. | .53 | 10. | 108.4 | F | 12.6 | 19.8 |
| * | 26 | 3 | 8000. | 0. | 0. | 6101. | 0. | 0. | 3205. | 6000. | 0. | ** 8000. | 2492. | .53 | 7. | 148.4 | F | 10.5 | 23.4 |
| * | 27 | 5 | 100. | 1525. | 0. | 7626. | 1525. | 0. | 4730. | 10000. | 0. | ** 100. | 2492. | .47 | 5. | 208.2 | F | 8.7 | 28.0 |
| * | 28 | 5 | 1000. | 1560. | 0. | 9186. | 1460. | 0. | 6190. | 7750. | 0. | ** 1000. | 1560. | .80 | 12. | 100.6 | F | 14.4 | 20.9 |
| * | 29 | 5 | 1000. | 1560. | 10746. | 10746. | 1560. | 7750. | 7750. | 7750. | 0. | 0. | 0. | 1.00 | 52. | 29.7 | E | 23.8 | 11.1 |
| * | TOTAL | 135469. | = | 25.7 | MILES | | | | | | MAX(V/C) = 1.00 | LOWEST LOS = F | AVG = 38. | 43.6 | | 19.3 | 13.7 | | |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL NO DIVERSION
 TIME SLICE 1 OF 3

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 3899. VEH-HRS | 3937. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 200. VEH-HRS | 210. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 4099. VEH-HRS | 4147. PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 149472. VEH-MI. | 150473. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 36. MPH. | 38. MPH. |
| AVERAGE DENSITY = | 44. VPMP | 44. VPMP |
| TOTAL FUEL = | 7797. GALLONS | 7797. GALLONS |
| TOTAL EMISSIONS = | 2077. KI LOGRAMS | 2077. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|--------|------------|--------|------------|-------|------------|-------|------------|--------|
| 1 | 0.49 | 2 | 125.12 | 3 | 11.72 | 4 | 2.57 | 5 | 2.99 |
| 6 | 13.55 | 7 | 31.04 | 8 | 29.04 | 9 | 16.43 | 10 | 32.79 |
| 11 | 22.07 | 12 | 11.79 | 13 | 12.90 | 14 | 13.37 | 15 | 28.39 |
| 16 | 34.42 | 17 | 57.31 | 18 | 8.90 | 19 | 64.85 | 20 | 50.98 |
| 21 | 5.79 | 22 | 5.90 | 23 | 35.79 | 24 | 90.98 | 25 | 100.92 |
| 26 | 687.70 | 27 | 18.64 | 28 | 77.66 | 29 | 5.53 | | |

***** TOTAL DELAY = 1599.6 VEH-HRS ***** AVERAGE DELAY = 28.02 MIN/VEH *****

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL NO DIVERSION
 TIME SLICE 1 OF 3

***** RAMP DELAYS *****

| | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-----------|-----------------------|---------------|--------------------------------|----------|---------|---------|----------|----------------------|
| ON-RAMP 2 | RAMP 50. | 25.00 | 4.46 | 8.93 | 0.55 | 2.90 | 0.15 | 3.60 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 50. | 25.00 | 4.46 | 8.93 | 0.55 | 2.90 | 0.15 | 3.60 |
| ON-RAMP 3 | RAMP 50. | 25.00 | 3.12 | 8.93 | 0.55 | 2.90 | 0.15 | 3.60 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 50. | 25.00 | 3.12 | 8.93 | 0.55 | 2.90 | 0.15 | 3.60 |
| ON-RAMP 4 | RAMP 100. | 50.00 | 4.17 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 100. | 50.00 | 4.17 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| ON-RAMP 5 | RAMP 100. | 50.00 | 7.63 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 100. | 50.00 | 7.63 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |

| | | | | | | | | | | |
|---------|---|--------|------|-------|------|-------|------|------|------|------|
| ON-RAMP | 9 | RAMP | 100. | 50.00 | 2.40 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 50.00 | 2.40 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |

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1 INSTITUTE OF TRANSPORTATION STUDIES
 UNIVERSITY OF CALIFORNIA, BERKELEY
 FREQ12PE REL 3.01
 SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 3
 2/29/2016 16: 6 PAGE 9
 QUEUE COLLISION IN SECTION 3 T2 =0.535

1 INSTITUTE OF TRANSPORTATION STUDIES
 UNIVERSITY OF CALIFORNIA, BERKELEY
 FREQ12PE REL 3.01
 SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 3
 2/29/2016 16: 6 PAGE 10

 **
 ** FREeway TRAVEL TIME (MINUTES) **
 **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | |
|-----------|--|-----------------------|-------|-------|-------|-------|-------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 |
| * 1 * | | 0.24 | 27.14 | 29.08 | 32.04 | 32.92 | 42.12 |
| * 2 * | | 0.00 | 2.41 | 4.35 | 7.31 | 8.19 | 17.39 |
| * 3 * | | 0.00 | 0.00 | 1.10 | 4.06 | 4.94 | 14.13 |
| * 4 * | | 0.00 | 0.00 | 0.00 | 2.19 | 3.06 | 12.26 |
| * 5 * | | 0.00 | 0.00 | 0.00 | 1.58 | 2.46 | 11.66 |
| * 6 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.15 | 9.35 |
| * 7 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 8.73 |
| * 8 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.95 |
| * 9 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.81 |
| * 10 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.22 |

1 INSTITUTE OF TRANSPORTATION STUDIES
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 FREQ12PE REL 3.01
 SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 3
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TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|-----------|--------|------------|-------------------|--------------------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|
| * SEC | * LNS | * LENGTH | * ORG DES SSEC | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 1 | 5 | 1370. | 7070. 1414. 7070. | 7070. 1414. 7070. | 10000. | 0. | 0. | 0. | .71 | 65. | 21.8 | C | 19.2 | 14.0 |
| * 2 | 3 | 99999. | 0. 0. 5656. | 0. 0. 5337. | 7360. | 0. * | 2242. | 319. | .73 | 60. | 29.5 | F | 19.6 | 13.7 |
| * 3 | 3 | 2740. | 0. 0. 5656. | 0. 0. 5337. | 6000. | 0. ** | 2740. | 431. | .89 | 23. | 76.7 | F | 19.0 | 15.3 |
| * 4 | 3 | 600. | 0. 0. 5656. | 0. 0. 5337. | 6000. | 0. ** | 600. | 431. | .89 | 20. | 89.5 | F | 18.1 | 16.4 |
| * 5 | 3 | 700. | 0. 0. 5656. | 0. 0. 5337. | 6000. | 0. ** | 700. | 431. | .89 | 19. | 94.6 | F | 17.7 | 16.9 |
| * 6 | 3 | 2630. | 0. 0. 5656. | 0. 0. 5337. | 6000. | 0. ** | 2630. | 431. | .89 | 17. | 105.7 | F | 17.0 | 17.8 |
| * 7 | 3 | 2530. | 0. 0. 5656. | 0. 0. 5337. | 6000. | 0. ** | 2530. | 431. | .89 | 16. | 108.9 | F | 16.8 | 18.1 |
| * 8 | 4 | 1500. | 382. 0. 6038. | 382. 0. 5719. | 6383. | 0. ** | 1500. | 431. | .90 | 17. | 85.5 | F | 17.0 | 17.9 |
| * 9 | 4 | 700. | 0. 0. 6038. | 0. 0. 5719. | 6440. | 0. ** | 700. | 431. | .89 | 16. | 88.0 | F | 16.8 | 18.1 |
| * 10 | 4 | 1500. | 0. 1226. 6038. | 0. 1216. 5719. | 6156. | 0. ** | 1500. | 431. | .93 | 19. | 75.9 | F | 18.0 | 16.7 |
| * 11 | 3 | 750. | 0. 0. 4812. | 0. 0. 4471. | 6000. | 0. ** | 750. | 431. | .75 | 10. | 146.6 | F | 13.2 | 22.7 |
| * 12 | 4 | 350. | 562. 0. 5374. | 562. 0. 5033. | 6535. | 0. ** | 350. | 431. | .77 | 11. | 114.4 | F | 13.7 | 22.0 |
| * 13 | 4 | 350. | 0. 0. 5374. | 0. 0. 5033. | 6640. | 0. ** | 350. | 431. | .76 | 11. | 118.9 | F | 13.5 | 22.3 |
| * 14 | 4 | 350. | 0. 532. 5374. | 0. 540. 5033. | 6532. | 0. ** | 350. | 431. | .77 | 11. | 114.3 | F | 13.7 | 22.0 |
| * 15 | 3 | 700. | 0. 0. 4842. | 0. 0. 4493. | 6000. | 0. ** | 700. | 431. | .75 | 10. | 145.7 | F | 13.3 | 22.6 |
| * 16 | 3 | 900. | 763. 0. 5605. | 763. 0. 5256. | 5838. | 0. ** | 900. | 431. | .90 | 17. | 103.2 | F | 17.1 | 17.7 |
| * 17 | 3 | 1400. | 438. 0. 6043. | 438. 0. 5694. | 5907. | 0. ** | 1400. | 213. | .96 | 22. | 88.0 | F | 19.0 | 15.5 |
| * 18 | 3 | 200. | 0. 0. 6043. | 0. 0. 5694. | 6000. | 0. ** | 200. | 213. | .95 | 20. | 93.3 | F | 18.6 | 15.9 |
| * 19 | 3 | 1400. | 0. 630. 6043. | 0. 608. 5694. | 5900. | 0. ** | 1400. | 206. | .97 | 22. | 87.6 | F | 19.0 | 15.4 |
| * 20 | 3 | 900. | 0. 0. 5413. | 0. 0. 5086. | 6000. | 0. ** | 900. | 206. | .85 | 14. | 119.8 | F | 15.7 | 19.5 |
| * 21 | 4 | 100. | 242. 0. 5655. | 240. 0. 5326. | 6172. | 0. ** | 100. | 206. | .86 | 15. | 89.4 | F | 16.2 | 18.9 |
| * 22 | 4 | 100. | 0. 198. 5655. | 0. 190. 5326. | 6198. | 0. ** | 100. | 206. | .86 | 15. | 90.5 | F | 16.1 | 19.1 |
| * 23 | 3 | 600. | 0. 0. 5457. | 0. 0. 5136. | 6000. | 0. ** | 600. | 206. | .86 | 15. | 117.6 | F | 15.9 | 19.2 |
| * 24 | 3 | 1500. | 168. 0. 5625. | 168. 0. 5304. | 5958. | 0. ** | 1500. | 206. | .89 | 16. | 107.9 | F | 16.8 | 18.1 |
| * 25 | 3 | 1500. | 0. 0. 5625. | 0. 0. 5304. | 6000. | 0. ** | 1500. | 206. | .88 | 16. | 110.3 | F | 16.7 | 18.3 |
| * 26 | 3 | 8000. | 0. 0. 5625. | 0. 0. 5304. | 6000. | 0. ** | 8000. | 206. | .88 | 16. | 110.3 | F | 16.7 | 18.3 |
| * 27 | 5 | 100. | 1406. 0. 7031. | 1406. 0. 6710. | 10000. | 0. ** | 100. | 206. | .67 | 8. | 166.0 | F | 10.8 | 25.1 |
| * 28 | 5 | 1000. | 520. 0. 7551. | 520. 0. 7230. | 7750. | 0. ** | 1000. | 206. | .93 | 19. | 75.6 | F | 18.1 | 16.6 |
| * 29 | 5 | 1000. | 520. 8071. 8071. | 520. 7750. 7750. | 7750. | 0. | 0. | 0. | 1.00 | 52. | 29.7 | E | 23.8 | 11.1 |

* TOTAL 135469. = 25.7 MILES US-101_SB_PM_P1_2018_PE.txt
 * MAX(V/C) = 1.00 LOWEST LOS = F AVG = 37. 47.1 18.9 14.7 *

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 2/29/2016 16: 6 PAGE 12
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 3

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|----------------------------|--------------------|------------------|-------------------|------------------|
| FREEWAY TRAVEL TIME = | 3876. VEH-HRS | 3908. PASS-HRS | 7775. VEH-HRS | 7845. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 401. VEH-HRS | 421. PASS-HRS | 601. VEH-HRS | 631. PASS-HRS |
| OFF-RAMP DELAY = | 16. VEH-HRS | 16. PASS-HRS | 16. VEH-HRS | 16. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 4293. VEH-HRS | 4345. PASS-HRS | 8392. VEH-HRS | 8493. PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 144381. VEH-MI. | 145405. PASS-MI. | 293853. VEH-MI. | 295878. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 34. MPH | | 38. MPH | |
| AVERAGE DENSITY = | 47. VPMPPL | | 45. VPMPPL | |
| TOTAL FUEL = | 7785. GALLONS | | 15582. GALLONS | |
| TOTAL EMISSIONS = | 2176. KILOGRAMS | | 4253. KILOGRAMS | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|--------|------------|--------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 128.51 | 3 | 79.22 | 4 | 21.59 | 5 | 27.12 |
| 6 | 117.45 | 7 | 117.21 | 8 | 72.21 | 9 | 34.99 | 10 | 61.20 |
| 11 | 52.72 | 12 | 25.21 | 13 | 26.40 | 14 | 25.18 | 15 | 48.77 |
| 16 | 38.99 | 17 | 46.81 | 18 | 7.29 | 19 | 46.49 | 20 | 47.93 |
| 21 | 5.22 | 22 | 5.30 | 23 | 31.13 | 24 | 68.81 | 25 | 70.85 |
| 26 | 377.85 | 27 | 13.77 | 28 | 50.52 | 29 | 5.53 | | |

***** TOTAL DELAY = 1654.3 VEH-HRS ***** AVERAGE DELAY = 18.55 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 2/29/2016 16: 6 PAGE 13
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 3

***** RAMP DELAYS *****

| | QUEUE LENGTH | DELAY | AVERAGE | GAS | HC | CO | NOX | TOTAL | |
|------------|--------------|---------|----------------|-------|-------|------|-------|-----------|-------|
| | VEHICLES | VEH-HRS | METERING DELAY | GALS | KGMS | KGMS | KGMS | EMISSIONS | |
| | | | MINUTES | | | | | KGMS | |
| ON-RAMP 2 | RAMP | 50. | 50.00 | 6.94 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 50. | 50.00 | 6.94 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| ON-RAMP 3 | RAMP | 50. | 50.00 | 4.90 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 50. | 50.00 | 4.90 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| ON-RAMP 4 | RAMP | 100. | 100.00 | 6.95 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 100.00 | 6.95 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP 5 | RAMP | 100. | 100.00 | 11.15 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 100.00 | 11.15 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP 6 | RAMP | 2. | 1.00 | 0.25 | 0.36 | 0.02 | 0.12 | 0.01 | 0.14 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 2. | 1.00 | 0.25 | 0.36 | 0.02 | 0.12 | 0.01 | 0.14 |
| ON-RAMP 9 | RAMP | 100. | 100.00 | 11.63 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 100.00 | 11.63 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| OFF-RAMP 2 | OUTPUT POINT | 32. | 16.04 | | 5.73 | 0.36 | 1.86 | 0.10 | 2.31 |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 3 OF 3

 ** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS | DESTINATIONS ACROSS | | | | | |
|-----------|---------------------|-------|-------|-------|-------|-------|
| * DOWN | 1 | 2 | 3 | 4 | 5 | 6 |
| * 1 * | 0.24 | 31.85 | 34.08 | 37.80 | 38.86 | 49.88 |
| * 2 * | 0.00 | 3.02 | 5.25 | 8.97 | 10.03 | 21.05 |
| * 3 * | 0.00 | 0.00 | 1.28 | 5.00 | 6.06 | 17.08 |
| * 4 * | 0.00 | 0.00 | 0.00 | 2.85 | 3.91 | 14.93 |

***** RAMP DELAYS *****

| | | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|------------|--------------|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|
| ON-RAMP 2 | RAMP | 50. | 50.00 | 9.15 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 50. | 50.00 | 9.15 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| ON-RAMP 3 | RAMP | 50. | 50.00 | 5.42 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 50. | 50.00 | 5.42 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| ON-RAMP 4 | RAMP | 100. | 100.00 | 8.45 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 100.00 | 8.45 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP 5 | RAMP | 100. | 100.00 | 12.10 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 100.00 | 12.10 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP 6 | RAMP | 0. | 1.00 | 0.04 | 0.36 | 0.02 | 0.12 | 0.01 | 0.14 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 0. | 1.00 | 0.04 | 0.36 | 0.02 | 0.12 | 0.01 | 0.14 |
| ON-RAMP 9 | RAMP | 100. | 100.00 | 8.57 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 100.00 | 8.57 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| OFF-RAMP 2 | OUTPUT POINT | 0. | 16.04 | | 5.73 | 0.36 | 1.86 | 0.10 | 2.31 |

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FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP LLL
FFFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 1111111 222222222 PPP LLLLLLLLLL
    
```

FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 2 AND 26 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

FREWAY AND ARTERIAL DESIGN FEATURES

| ** SUB NO. | ** SSEC | ** SSEC | ** DESIGN | ** ORG | ** TRK | ** SSEC | ** PCT | ** PCT | ** DES | ** SPECIAL | ** FF.SPD. | ** CAP. | ** ART | ** GRADE | ** SUBSECTION | ** LOCATION |
|------------|---------|---------|-----------|--------|--------|---------|--------|-----------|---------|-------------|-------------|-------------|---------|-------------|-------------------------|-------------|
| ** SEC | ** LNS | ** CAP | ** LENGTH | ** DES | ** FAC | ** GRAD | ** TRK | ** TRUCKS | ** RAMP | ** ALT. RTE | ** ALT. RTE | ** ALT. RTE | ** TYPE | ** ALT. RTE | ** LOCATION | ** LOCATION |
| ** 1 | | | | | | | | | | | | | | | | |
| ** 2 | 1 | 1650. | 99999. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | |
| ** 3 | 1 | 1650. | 2740. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-85 Off to Shore On | |
| ** 4 | 1 | 1650. | 600. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Shore. On to Moffet Off | |
| ** 5 | 1 | 1650. | 700. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Moffett Off to On | |
| ** 6 | 1 | 1650. | 2630. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Moffett On to Ellis Off | |
| ** 7 | 1 | 1650. | 2530. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Ellis Off to On-ramp | |
| ** 8 | 1 | 1650. | 1500. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Ellis On-ramp | |
| ** 9 | 1 | 1650. | 700. | 65 | | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Ellis / US 237 | |
| ** 10 | 1 | 1650. | 1500. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 EB Off-Ramp | |
| ** 11 | 1 | 1650. | 750. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 / SR-237 | |
| ** 12 | 1 | 1650. | 350. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 EB On-Ramp | |
| ** 13 | 1 | 1650. | 350. | 65 | | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | US 237 / Mathilda | |
| ** 14 | 1 | 1650. | 350. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-Ramp | |
| ** 15 | 1 | 1650. | 700. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | |
| ** 16 | 1 | 1650. | 900. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda SB On-Ramp | |
| ** 17 | 1 | 1650. | 1400. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda NB On-Ramp | |
| ** 18 | 1 | 1650. | 200. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Fair Oaks | |
| ** 19 | 1 | 1650. | 1400. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks SB Off-Ramp | |

```

**
** 20 1 1650. 900. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks SB/ Fair Oaks **
**
*****

```

FREEWAY AND ARTERIAL DESIGN FEATURES

```

*****
**
** SUB NO. SSEC SSEC DESIGN ORG TRK SSEC PCT PCT DES SPECIAL FF. SPD. CAP. ART GRADE SUBSECTION LOCATION **
** SEC LNS CAP LENGTH SPEED DES FAC GRAD TRK TRUCKS RAMP ALT. RTE ALT. RTE TYPE ALT. RTE **
*****
** 21 1 1650. 100. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Fair Oaks SB On-Ramp **
** 22 1 1650. 100. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks NB Off-Ramp **
** 23 1 1650. 600. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks NB/ Fair Oaks **
** 24 1 1650. 1500. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Oaks On-Ramp to Mid **
** 25 1 1650. 1500. 65 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Mid to Lawrence Off-ramp **
** 26 1 1650. 8000. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 HOV Dummy **
** 27 **
** 28 **
** 29 **
*****

```

FREEWAY TRAVEL TIME (MINUTES)

```

*****
* ORIGINS DESTINATIONS ACROSS *
* DOWN *
* 1 2 3 4 5 6 7 *
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 2 * 0.00 22.21 22.52 23.39 23.59 25.87 0.00 *
+
* 3 * 0.00 0.00 0.00 0.00 2.14 4.41 0.00 *
+
* 4 * 0.00 0.00 0.00 0.00 0.00 3.53 0.00 *
+
* 5 * 0.00 0.00 0.00 0.00 0.00 3.22 0.00 *
+
* 6 * 0.00 0.00 0.00 0.00 0.00 3.06 0.00 *
+
* 7 * 0.00 0.00 0.00 0.00 0.00 2.32 0.00 *
+
* 8 * 0.00 0.00 0.00 0.00 0.00 2.16 0.00 *
+
* 9 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 10 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 11 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
* *
*****

```

TIME SLICE FREEWAY PERFORMANCE TABLE

US-101_SB_PM_P1_2018_PL.txt

| * SUB SEC | NO. LNS | SSEC LENGTH | O-D ORG | DATA DES | DEMANDS SSEC | ADJUSTED ORG | VOLUMES DES | SSEC CAP. | WEAVE EFF | CONGEST LENGTH | STORAGE RATE | V/C RATIO | SPEED MPH | DENSITY VPMP | LOS LEVEL | FUEL MPG | EMI SS GS/VM |
|--|---------|-------------|---------|----------|--------------|--------------|-------------|-----------|-----------|----------------|--------------|-----------|-----------|--------------|-----------|----------|--------------|
| * 1 | | | | | | | | | | | | | | | | | |
| * 2 | 1 | 99999 | 1524 | 0 | 1524 | 1524 | 0 | 1524 | 1650 | 0 | 0 | .92 | 58 | 26.3 | D | 23.4 | 11.7 |
| * 3 | 1 | 2740 | 0 | 0 | 1524 | 0 | 0 | 1524 | 1650 | 0 | 0 | .92 | 58 | 26.3 | D | 23.4 | 11.7 |
| * 4 | 1 | 600 | 0 | 0 | 1524 | 0 | 0 | 1524 | 1650 | 0 | 0 | .92 | 58 | 26.3 | D | 23.4 | 11.7 |
| * 5 | 1 | 700 | 0 | 0 | 1524 | 0 | 0 | 1524 | 1650 | 0 | 0 | .92 | 58 | 26.3 | D | 23.4 | 11.7 |
| * 6 | 1 | 2630 | 0 | 0 | 1524 | 0 | 0 | 1524 | 1650 | 0 | 0 | .92 | 58 | 26.3 | D | 23.4 | 11.7 |
| * 7 | 1 | 2530 | 0 | 0 | 1524 | 0 | 0 | 1524 | 1650 | 0 | 0 | .92 | 58 | 26.3 | D | 23.4 | 11.7 |
| * 8 | 1 | 1500 | 54 | 0 | 1577 | 54 | 0 | 1577 | 1650 | 0 | 0 | .96 | 56 | 28.3 | D | 24.1 | 11.3 |
| * 9 | 1 | 700 | 0 | 0 | 1577 | 0 | 0 | 1577 | 1650 | 0 | 0 | .96 | 56 | 28.3 | D | 24.1 | 11.3 |
| * 10 | 1 | 1500 | 0 | 289 | 1577 | 0 | 285 | 1577 | 1650 | 0 | 0 | .96 | 56 | 28.3 | D | 24.1 | 11.3 |
| * 11 | 1 | 750 | 0 | 0 | 1288 | 0 | 0 | 1288 | 1650 | 0 | 0 | .78 | 65 | 19.8 | C | 20.0 | 13.7 |
| * 12 | 1 | 350 | 96 | 0 | 1384 | 96 | 0 | 1384 | 1650 | 0 | 0 | .84 | 65 | 21.3 | C | 20.0 | 13.7 |
| * 13 | 1 | 350 | 0 | 0 | 1384 | 0 | 0 | 1384 | 1650 | 0 | 0 | .84 | 65 | 21.3 | C | 20.0 | 13.7 |
| * 14 | 1 | 350 | 0 | 105 | 1384 | 0 | 105 | 1384 | 1650 | 0 | 0 | .84 | 65 | 21.3 | C | 20.0 | 13.7 |
| * 15 | 1 | 700 | 0 | 0 | 1279 | 0 | 0 | 1279 | 1650 | 0 | 0 | .78 | 65 | 19.7 | C | 20.0 | 13.7 |
| * 16 | 1 | 900 | 160 | 0 | 1440 | 160 | 0 | 1440 | 1650 | 0 | 0 | .97 | 65 | 22.1 | C | 20.0 | 13.7 |
| * 17 | 1 | 1400 | 87 | 0 | 1527 | 87 | 0 | 1527 | 1650 | 0 | 0 | .93 | 58 | 26.5 | D | 23.5 | 11.7 |
| * 18 | 1 | 200 | 0 | 0 | 1527 | 0 | 0 | 1527 | 1650 | 0 | 0 | .93 | 58 | 26.5 | D | 23.5 | 11.7 |
| * 19 | 1 | 1400 | 0 | 81 | 1527 | 0 | 81 | 1527 | 1650 | 0 | 0 | .93 | 58 | 26.5 | D | 23.5 | 11.7 |
| * 20 | 1 | 900 | 0 | 0 | 1446 | 0 | 0 | 1446 | 1650 | 0 | 0 | .88 | 65 | 22.2 | C | 20.0 | 13.7 |
| * 21 | 1 | 100 | 55 | 0 | 1501 | 55 | 0 | 1501 | 1650 | 0 | 0 | .91 | 59 | 25.6 | C | 23.2 | 11.9 |
| * 22 | 1 | 100 | 0 | 22 | 1501 | 0 | 22 | 1501 | 1650 | 0 | 0 | .91 | 59 | 25.6 | C | 23.2 | 11.9 |
| * 23 | 1 | 600 | 0 | 0 | 1479 | 0 | 0 | 1479 | 1650 | 0 | 0 | .90 | 59 | 24.9 | C | 22.9 | 12.0 |
| * 24 | 1 | 1500 | 46 | 0 | 1525 | 46 | 0 | 1525 | 1650 | 0 | 0 | .92 | 58 | 26.4 | D | 23.4 | 11.7 |
| * 25 | 1 | 1500 | 0 | 0 | 1525 | 0 | 0 | 1525 | 1650 | 0 | 0 | .92 | 58 | 26.4 | D | 23.4 | 11.7 |
| * 26 | 1 | 8000 | 0 | 1525 | 1525 | 0 | 1525 | 1525 | 1650 | 0 | 0 | .92 | 58 | 26.4 | D | 23.4 | 11.7 |
| * 27 | | | | | | | | | | | | | | | | | |
| * 28 | | | | | | | | | | | | | | | | | |
| * 29 | | | | | | | | | | | | | | | | | |
| ***** | | | | | | | | | | | | | | | | | |
| * TOTAL 131999. = 25.0 MILES MAX(V/C) = 0.96 LOWEST LOS = D AVG = 58. 26.2 23.3 11.8 * | | | | | | | | | | | | | | | | | |
| ***** | | | | | | | | | | | | | | | | | |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 16: 6 PAGE 6
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE TIME SLICE 1 OF 3

| | CURRENT TIME SLICE | | CUMULATIVE VALUES |
|-----------------------------|--------------------|-----------------|--------------------------------|
| FREEWAY TRAVEL TIME = | 656. VEH-HRS | 1311. PASS-HRS | 656. VEH-HRS 1311. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 2. VEH-HRS | 4. PASS-HRS | 2. VEH-HRS 4. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 658. VEH-HRS | 1315. PASS-HRS | 658. VEH-HRS 1315. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 38010. VEH-MI. | 76020. PASS-MI. | 38010. VEH-MI. 76020. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 58. MPH. | | 58. MPH. |
| AVERAGE DENSITY = | 26. VPMP | | 26. VPMP |
| TOTAL FUEL = | 1631. GALLONS | | 1631. GALLONS |
| TOTAL EMISSIONS = | 448. KILOGRAMS | | 448. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 54.96 | 3 | 1.51 | 4 | 0.33 | 5 | 0.38 |
| 6 | 1.45 | 7 | 1.39 | 8 | 1.15 | 9 | 0.54 | 10 | 1.15 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.79 | 18 | 0.11 | 19 | 0.79 | 20 | 0.00 |
| 21 | 0.05 | 22 | 0.05 | 23 | 0.25 | 24 | 0.83 | 25 | 0.83 |
| 26 | 4.44 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 71.0 VEH-HRS ***** AVERAGE DELAY = 2.79 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-------------------------|-----------------------|---------------|----------|---------|---------|----------|----------------------|
| OFF-RAMP 2 OUTPUT POINT | 4. | 1.90 | 0.65 | 0.04 | 0.21 | 0.01 | 0.27 |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE TIME SLICE 2 OF 3

 ** FREeway TRAVEL TIME (MINUTES) **

| * ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | |
|----------------|---------------------|-------|-------|-------|-------|-------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 19.80 | 20.11 | 20.91 | 21.11 | 23.14 | 0.00 |

| | | | | | | | | |
|--------|------|------|------|------|------|------|------|------|
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.02 | 4.04 | 0.00 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.21 | 0.00 | |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.90 | 0.00 | |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.74 | 0.00 | |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.06 | 0.00 | |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.92 | 0.00 | |
| * 9 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| * 10 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| * 11 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | |
|-----------|----------|------------|-----------|--------------------|--------|-----------------|-----------|----------------|---------|-----------|-----------|---------|--------|-------------|------|
| * SEC LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | |
| * 1 | | | | | | | | | | | | | | | |
| * 2 | 1 | 99999. | 1414. | 0. 1414. | 1414. | 0. 1414. | 1650. | 0. | 0. | .86 | 65. | 21.8 | C | 20.0 | 13.7 |
| * 3 | 1 | 2740. | 0. | 0. 1414. | 0. | 0. 1414. | 1650. | 0. | 0. | .86 | 65. | 21.8 | C | 20.0 | 13.7 |
| * 4 | 1 | 600. | 0. | 0. 1414. | 0. | 0. 1414. | 1650. | 0. | 0. | .86 | 65. | 21.8 | C | 20.0 | 13.7 |
| * 5 | 1 | 700. | 0. | 0. 1414. | 0. | 0. 1414. | 1650. | 0. | 0. | .86 | 65. | 21.8 | C | 20.0 | 13.7 |
| * 6 | 1 | 2630. | 0. | 0. 1414. | 0. | 0. 1414. | 1650. | 0. | 0. | .86 | 65. | 21.8 | C | 20.0 | 13.7 |
| * 7 | 1 | 2530. | 0. | 0. 1414. | 0. | 0. 1414. | 1650. | 0. | 0. | .86 | 65. | 21.8 | C | 20.0 | 13.7 |
| * 8 | 1 | 1500. | 57. | 0. 1471. | 57. | 0. 1471. | 1650. | 0. | 0. | .89 | 60. | 24.7 | C | 22.8 | 12.0 |
| * 9 | 1 | 700. | 0. | 0. 1471. | 0. | 0. 1471. | 1650. | 0. | 0. | .89 | 60. | 24.7 | C | 22.8 | 12.0 |
| * 10 | 1 | 1500. | 0. | 284. 1471. | 0. | 283. 1471. | 1650. | 0. | 0. | .89 | 60. | 24.7 | C | 22.8 | 12.0 |
| * 11 | 1 | 750. | 0. | 0. 1187. | 0. | 0. 1187. | 1650. | 0. | 0. | .72 | 65. | 18.3 | C | 20.0 | 13.7 |
| * 12 | 1 | 350. | 105. | 0. 1292. | 105. | 0. 1292. | 1650. | 0. | 0. | .78 | 65. | 19.9 | C | 20.0 | 13.7 |
| * 13 | 1 | 350. | 0. | 0. 1292. | 0. | 0. 1292. | 1650. | 0. | 0. | .78 | 65. | 19.9 | C | 20.0 | 13.7 |
| * 14 | 1 | 350. | 0. | 108. 1292. | 0. | 108. 1292. | 1650. | 0. | 0. | .78 | 65. | 19.9 | C | 20.0 | 13.7 |
| * 15 | 1 | 700. | 0. | 0. 1184. | 0. | 0. 1184. | 1650. | 0. | 0. | .72 | 65. | 18.2 | C | 20.0 | 13.7 |
| * 16 | 1 | 900. | 162. | 0. 1345. | 162. | 0. 1345. | 1650. | 0. | 0. | .82 | 65. | 20.7 | C | 20.0 | 13.7 |
| * 17 | 1 | 1400. | 93. | 0. 1438. | 93. | 0. 1438. | 1650. | 0. | 0. | .87 | 65. | 22.1 | C | 20.0 | 13.7 |
| * 18 | 1 | 200. | 0. | 0. 1438. | 0. | 0. 1438. | 1650. | 0. | 0. | .87 | 65. | 22.1 | C | 20.0 | 13.7 |
| * 19 | 1 | 1400. | 0. | 100. 1438. | 0. | 100. 1438. | 1650. | 0. | 0. | .87 | 65. | 22.1 | C | 20.0 | 13.7 |
| * 20 | 1 | 900. | 0. | 0. 1338. | 0. | 0. 1338. | 1650. | 0. | 0. | .81 | 65. | 20.6 | C | 20.0 | 13.7 |
| * 21 | 1 | 100. | 58. | 0. 1396. | 58. | 0. 1396. | 1650. | 0. | 0. | .85 | 65. | 21.5 | C | 20.0 | 13.7 |
| * 22 | 1 | 100. | 0. | 32. 1396. | 0. | 32. 1396. | 1650. | 0. | 0. | .85 | 65. | 21.5 | C | 20.0 | 13.7 |
| * 23 | 1 | 600. | 0. | 0. 1364. | 0. | 0. 1364. | 1650. | 0. | 0. | .83 | 65. | 21.0 | C | 20.0 | 13.7 |
| * 24 | 1 | 1500. | 42. | 0. 1406. | 42. | 0. 1406. | 1650. | 0. | 0. | .85 | 65. | 21.6 | C | 20.0 | 13.7 |
| * 25 | 1 | 1500. | 0. | 0. 1406. | 0. | 0. 1406. | 1650. | 0. | 0. | .85 | 65. | 21.6 | C | 20.0 | 13.7 |
| * 26 | 1 | 8000. | 0. | 1406. 1406. | 0. | 1406. 1406. | 1650. | 0. | 0. | .85 | 65. | 21.6 | C | 20.0 | 13.7 |
| * 27 | | | | | | | | | | | | | | | |
| * 28 | | | | | | | | | | | | | | | |
| * 29 | | | | | | | | | | | | | | | |
| * TOTAL | 131999. | = | 25.0 | MI LES | | MAX(V/C) = 0.89 | | LOWEST LOS = C | | AVG = 65. | 21.8 | | 20.1 | 13.7 | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 544. VEH-HRS | 1088. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 5. VEH-HRS | 9. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 549. VEH-HRS | 1098. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 35269. VEH-MI. | 70539. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 64. MPH. | 61. MPH. |
| AVERAGE DENSITY = | 22. VPMP | 24. VPMP |
| TOTAL FUEL = | 1759. GALLONS | 3389. GALLONS |
| TOTAL EMISSIONS = | 484. KI LOGRAMS | 931. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.58 | 9 | 0.27 | 10 | 0.58 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 1.4 VEH-HRS ***** AVERAGE DELAY = 0.06 MIN/VEH *****
 US-101_SB_PM_P1_2018_PL.txt

***** RAMP DELAYS *****

| OFF-RAMP | 2 | OUTPUT POINT | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|----------|---|--------------|--------------------------|------------------|-------------|------------|------------|-------------|----------------------------|
| | | | 6. | 4.75 | 1.63 | 0.10 | 0.54 | 0.03 | 0.67 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 16: 6 PAGE 10
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 3 OF 3

 **
 ** FREeway TRAVEL TIME (MINUTES) **
 **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | |
|-----------|--|-----------------------|-------|-------|-------|-------|-------|------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | | 0.00 | 19.74 | 20.05 | 20.86 | 21.05 | 23.08 | 0.00 |
| * 3 * | | 0.00 | 0.00 | 0.00 | 0.00 | 1.96 | 3.99 | 0.00 |
| * 4 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.21 | 0.00 |
| * 5 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.90 | 0.00 |
| * 6 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.74 | 0.00 |
| * 7 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.06 | 0.00 |
| * 8 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.92 | 0.00 |
| * 9 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 10 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 11 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 3 OF 3

 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *

| * SUB | * NO. | * SSEC | * O-D DATA | | * DEMANDS | * ADJUSTED VOLUMES | | | * SSEC | * WAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|---------|-------|----------|------------|-------|-----------|--------------------|-------|----------------|-----------|--------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * SSEC | * CAP | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 1 | | | | | | | | | | | | | | | | | | |
| * 2 | 1 | 99999. | 1302. | 0. | 1302. | 1302. | 0. | 1302. | 1650. | 0. | 0. | 0. | .79 | 65. | 20.0 | C | 20.0 | 13.7 |
| * 3 | 1 | 2740. | 0. | 0. | 1302. | 0. | 0. | 1302. | 1650. | 0. | 0. | 0. | .79 | 65. | 20.0 | C | 20.0 | 13.7 |
| * 4 | 1 | 600. | 0. | 0. | 1302. | 0. | 0. | 1302. | 1650. | 0. | 0. | 0. | .79 | 65. | 20.0 | C | 20.0 | 13.7 |
| * 5 | 1 | 700. | 0. | 0. | 1302. | 0. | 0. | 1302. | 1650. | 0. | 0. | 0. | .79 | 65. | 20.0 | C | 20.0 | 13.7 |
| * 6 | 1 | 2630. | 0. | 0. | 1302. | 0. | 0. | 1302. | 1650. | 0. | 0. | 0. | .79 | 65. | 20.0 | C | 20.0 | 13.7 |
| * 7 | 1 | 2530. | 0. | 0. | 1302. | 0. | 0. | 1302. | 1650. | 0. | 0. | 0. | .79 | 65. | 20.0 | C | 20.0 | 13.7 |
| * 8 | 1 | 1500. | 42. | 0. | 1344. | 42. | 0. | 1344. | 1650. | 0. | 0. | 0. | .81 | 65. | 20.7 | C | 20.0 | 13.7 |
| * 9 | 1 | 700. | 0. | 0. | 1344. | 0. | 0. | 1344. | 1650. | 0. | 0. | 0. | .81 | 65. | 20.7 | C | 20.0 | 13.7 |
| * 10 | 1 | 1500. | 0. | 261. | 1344. | 0. | 261. | 1344. | 1650. | 0. | 0. | 0. | .81 | 65. | 20.7 | C | 20.0 | 13.7 |
| * 11 | 1 | 750. | 0. | 0. | 1083. | 0. | 0. | 1083. | 1650. | 0. | 0. | 0. | .66 | 65. | 16.7 | B | 20.0 | 13.7 |
| * 12 | 1 | 350. | 96. | 0. | 1179. | 96. | 0. | 1179. | 1650. | 0. | 0. | 0. | .71 | 65. | 18.1 | C | 20.0 | 13.7 |
| * 13 | 1 | 350. | 0. | 0. | 1179. | 0. | 0. | 1179. | 1650. | 0. | 0. | 0. | .71 | 65. | 18.1 | C | 20.0 | 13.7 |
| * 14 | 1 | 350. | 0. | 94. | 1179. | 0. | 94. | 1179. | 1650. | 0. | 0. | 0. | .71 | 65. | 18.1 | C | 20.0 | 13.7 |
| * 15 | 1 | 700. | 0. | 0. | 1085. | 0. | 0. | 1085. | 1650. | 0. | 0. | 0. | .66 | 65. | 16.7 | B | 20.0 | 13.7 |
| * 16 | 1 | 900. | 130. | 0. | 1215. | 130. | 0. | 1215. | 1650. | 0. | 0. | 0. | .74 | 65. | 18.7 | C | 20.0 | 13.7 |
| * 17 | 1 | 1400. | 85. | 0. | 1300. | 85. | 0. | 1300. | 1650. | 0. | 0. | 0. | .79 | 65. | 20.0 | C | 20.0 | 13.7 |
| * 18 | 1 | 200. | 0. | 0. | 1300. | 0. | 0. | 1300. | 1650. | 0. | 0. | 0. | .79 | 65. | 20.0 | C | 20.0 | 13.7 |
| * 19 | 1 | 1400. | 0. | 86. | 1300. | 0. | 86. | 1300. | 1650. | 0. | 0. | 0. | .79 | 65. | 20.0 | C | 20.0 | 13.7 |
| * 20 | 1 | 900. | 0. | 0. | 1214. | 0. | 0. | 1214. | 1650. | 0. | 0. | 0. | .74 | 65. | 18.7 | C | 20.0 | 13.7 |
| * 21 | 1 | 100. | 46. | 0. | 1260. | 46. | 0. | 1260. | 1650. | 0. | 0. | 0. | .76 | 65. | 19.4 | C | 20.0 | 13.7 |
| * 22 | 1 | 100. | 0. | 28. | 1260. | 0. | 28. | 1260. | 1650. | 0. | 0. | 0. | .76 | 65. | 19.4 | C | 20.0 | 13.7 |
| * 23 | 1 | 600. | 0. | 0. | 1232. | 0. | 0. | 1232. | 1650. | 0. | 0. | 0. | .75 | 65. | 19.0 | C | 20.0 | 13.7 |
| * 24 | 1 | 1500. | 50. | 0. | 1282. | 50. | 0. | 1282. | 1650. | 0. | 0. | 0. | .78 | 65. | 19.7 | C | 20.0 | 13.7 |
| * 25 | 1 | 1500. | 0. | 0. | 1282. | 0. | 0. | 1282. | 1650. | 0. | 0. | 0. | .78 | 65. | 19.7 | C | 20.0 | 13.7 |
| * 26 | 1 | 8000. | 0. | 1282. | 1282. | 0. | 1282. | 1282. | 1650. | 0. | 0. | 0. | .78 | 65. | 19.7 | C | 20.0 | 13.7 |
| * 27 | | | | | | | | | | | | | | | | | | |
| * 28 | | | | | | | | | | | | | | | | | | |
| * 29 | | | | | | | | | | | | | | | | | | |
| * TOTAL | | 131999. | = | 25.0 | MILES | MAX(V/C) = 0.81 | | LOWEST LOS = C | AVG = 65. | 19.9 | 20.0 | 13.7 | | | | | | |

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|-----------------------------|--------------------|-----------------|-------------------|------------------|
| FREEWAY TRAVEL TIME = | 499. VEH-HRS | 997. PASS-HRS | 1698. VEH-HRS | 3397. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 3. VEH-HRS | 6. PASS-HRS | 9. VEH-HRS | 19. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 502. VEH-HRS | 1003. PASS-HRS | 1708. VEH-HRS | 3416. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 32413. VEH-MI. | 64826. PASS-MI. | 105692. VEH-MI. | 211385. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 65. MPH | | 62. MPH | |
| AVERAGE DENSITY = | 20. VPMP | | 23. VPMP | |
| TOTAL FUEL = | 1622. GALLONS | | 5011. GALLONS | |
| TOTAL EMISSIONS = | 446. KILOGRAMS | | 1377. KILOGRAMS | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-------------------------|--------------------------|------------------|-------------|------------|------------|-------------|----------------------------|
| OFF-RAMP 2 OUTPUT POINT | 0. | 2.84 | 0.98 | 0.06 | 0.32 | 0.02 | 0.40 |

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FFFFFFFFF RRRRRRRR EEEEEEEEEE QQQQQQQ    1111    222222    PPPPPPPP    EEEEEEEEEE
FFFFFFFFF RRRRRRRRRR EEEEEEEEEE Q*A. D. MAY*Q 111111    222    222    PPPPPPPP    EEEEEEEEEE
FFF       RRR       RRR EEE         QQQQQQ  QQQQQ    1111    222    222    PPP    PPP    EEE
FFF       RRR       RRR EEE         QQQQ   QQQQ    1111    222    222    PPP    PPP    EEE
FFFFFFFFF RRRRRRRRRR EEEEEEEEEE QQQQ   QQQQ    1111    222    222    PPPPPPPP    EEEEEEEEEE
FFFFFFFFF RRRRRRRRRR EEEEEEEEEE QQQQ   QQQQ    1111    2222    PPPPPPPP    EEEEEEEEEE
FFF       RRR       RRR EEE         QQQQ   QQQQ    1111    2222    PPP    PPP    EEE
FFF       RRR       RRR EEE         Q*UC*   QQQQQ    1111    222    222    PPP    PPP    EEE
FFF       RRR       RRR EEEEEEEEEE Q*REGENTS*Q 1111    222    222    PPP    PPP    EEEEEEEEEE
FFF       RRR       RRR EEEEEEEEEE Q*1999*Q  QQQ 11111111    2222222222    PPP    PPP    EEEEEEEEEE

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FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

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**                                     FREEWAY AND ARTERIAL DESIGN FEATURES                                     **
**                                                                                                                                                       **
**                                                                                                                                                       **
** SUB NO.    SSEC    SSEC    DESIGN    ORG    TRK    SSEC    PCT    PCT    DES    SPECIAL    FF.SPD.    CAP.    ART    GRADE    SUBSECTION  LOCATION **
** SEC   LNS    CAP    LENGTH    SPEED    DES    FAC    GRAD    TRK    TRUCKS    RAMP    ALT. RTE    ALT. RTE    TYPE    ALT. RTE                **
**                                                                                                                                                       **
** 1   5  10000.  1370.  65     OD  0.96  0.0  4     0     NO     0.0     0.    GOOD  0.0  Seeding              **
** 2   3   7360.  99999.  65     0.96  0.0  4     0     NO     0.0     0.    GOOD  0.0  Queue Capture        **
** 3   3   6000.  2740.  65     0.96  0.0  4     0     NO     0.0     0.    GOOD  0.0  SR-85 Off to Shore On **
** 4   3   6000.    600.  65     0.96  0.0  4     0     NO     0.0     0.    GOOD  0.0  Shore. On to Moffet Off **
** 5   3   6000.    700.  65     0.96  0.0  4     0     NO     0.0     0.    GOOD  0.0  Moffett Off to On      **
** 6   3   6000.  2630.  65     0.96  0.0  4     0     NO     0.0     0.    GOOD  0.0  Moffett On to Ellis Off **
** 7   3   6000.  2530.  65     0.96  0.0  4     0     NO     0.0     0.    GOOD  0.0  Ellis Off to On-ramp   **
** 8   4   6440.  1500.  65     0  0.96  0.0  4     0     YES    0.0     0.    GOOD  0.0  Ellis On-ramp         **
** 9   4   6440.    700.  65     0.96  0.0  4     0     YES    0.0     0.    GOOD  0.0  Ellis / US 237        **
** 10  4   6440.  1500.  65     D  0.96  0.0  4     0     NO     0.0     0.    GOOD  0.0  SR-237 EB Off-Ramp    **
** 11  3   6000.    750.  65     0.96  0.0  4     0     NO     0.0     0.    GOOD  0.0  SR-237 / SR-237      **
** 12  4   6640.    350.  65     0  0.96  0.0  4     0     YES    0.0     0.    GOOD  0.0  SR-237 EB On-Ramp     **
** 13  4   6640.    350.  65     0.96  0.0  4     0     YES    0.0     0.    GOOD  0.0  US 237 / Mathilda    **
** 14  4   6640.    350.  65     D  0.96  0.0  4     0     NO     0.0     0.    GOOD  0.0  Mathilda Off-Ramp     **
** 15  3   6000.    700.  65     0.96  0.0  4     0     NO     0.0     0.    GOOD  0.0  Mathilda / Mathilda   **
** 16  3   6000.    900.  65     0  0.96  0.0  4     0     YES    0.0     0.    GOOD  0.0  Mathilda SB On-Ramp   **
** 17  3   6000.  1400.  65     0  0.96  0.0  4     0     YES    0.0     0.    GOOD  0.0  Mathilda NB On-Ramp   **
** 18  3   6000.    200.  65     0.96  0.0  4     0     NO     0.0     0.    GOOD  0.0  Mathilda / Fair Oaks  **
** 19  3   6000.  1400.  65     D  0.96  0.0  4     0     NO     0.0     0.    GOOD  0.0  Fair Oaks SB Off-Ramp **
** 20  3   6000.    900.  65     0.96  0.0  4     0     NO     0.0     0.    GOOD  0.0  Fair Oaks SB/ Fair Oaks **
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FREeway AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC | SSEC | DESIGN | ORG | TRK | SSEC | PCT | PCT | DES | SPECIAL | FF.SPD. | CAP. | ART | GRADE | SUBSECTION | LOCATION |
|---------|------|--------|--------|-----|-----|------|-----|--------|------|---------|----------|----------|------|----------|--------------------------|----------|
| SEC | LNS | CAP | SPEED | DES | FAC | GRAD | TRK | TRUCKS | RAMP | RAMP | ALT. RTE | ALT. RTE | TYPE | ALT. RTE | | |
| ** 21 | 4 | 6230. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Fair Oaks SB On-Ramp | ** |
| ** 22 | 4 | 6230. | 100. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks NB Off-Ramp | ** |
| ** 23 | 3 | 6000. | 600. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks NB/ Fair Oaks | ** |
| ** 24 | 3 | 6000. | 1500. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Oaks On-Ramp to Mid | ** |
| ** 25 | 3 | 6000. | 1500. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mid to Lawrence Off-ramp | ** |
| ** 26 | 3 | 6000. | 8000. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | ** |
| ** 27 | 5 | 10000. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | ** |
| ** 28 | 5 | 7750. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Dummy Bottleneck | ** |
| ** 29 | 5 | 7750. | 1000. | 65 | 0D | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | End of Network | ** |

***** INPUT HAS BEEN COMPLETED *****

QUEUE COLLISION IN SECTION 28 T2 =0.044
QUEUE COLLISION IN SECTION 10 T2 =0.830

FREeway TRAVEL TIME (MINUTES)

| ORIGINS | DESTINATIONS ACROSS | | | | | |
|---------|---------------------|-------|-------|-------|-------|-------|
| DOWN | 1 | 2 | 3 | 4 | 5 | 6 |
| * 1 * | 0.24 | 22.73 | 23.87 | 27.22 | 28.32 | 46.33 |
| * 2 * | 0.00 | 1.50 | 2.64 | 5.99 | 7.09 | 25.10 |
| * 3 * | 0.00 | 0.00 | 0.69 | 4.04 | 5.14 | 23.15 |
| * 4 * | 0.00 | 0.00 | 0.00 | 2.80 | 3.90 | 21.92 |
| * 5 * | 0.00 | 0.00 | 0.00 | 2.20 | 3.29 | 21.31 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.20 | 18.21 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 17.39 |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.39 |
| * 9 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.14 |
| * 10 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.22 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB SEC | * NO. LNS | * SSEC LENGTH | * O-D ORG | * DATA DES | * DEMANDS SSEC | * ADJUSTED ORG | * VOLUMES DES | * SSEC SSEC | * WEAVE CAP. | * CONGEST EFF | * STORAGE LENGTH | * V/C RATIO | * SPEED MPH | * DENSITY VP/MPH | * LOS LEVEL | * FUEL MPG | * EMISSIONS GS/VM | |
|-----------|-----------|---------------|-----------|------------|----------------|----------------|---------------|-------------|--------------|-----------------|------------------|-------------|-------------|------------------|-------------|------------|-------------------|------|
| * 1 | 5 | 1370. | 7619. | 1524. | 7619. | 7619. | 1524. | 7619. | 10000. | 0. | 0. | .76 | 64. | 23.8 | C | 19.6 | 13.7 | |
| * 2 | 3 | 99999. | 0. | 0. | 6095. | 0. | 0. | 6000. | 7360. | 0. | * 1340. | .95 | .82 | 61. | 32.9 | F | 20.4 | 13.1 |
| * 3 | 3 | 2740. | 0. | 0. | 6095. | 0. | 0. | 6000. | 6000. | 0. | 0. | 1.00 | 52. | 38.3 | E | 23.8 | 11.1 | |
| * 4 | 3 | 600. | 0. | 0. | 6095. | 0. | 0. | 6000. | 6000. | 0. | 0. | 1.00 | 52. | 38.3 | E | 23.8 | 11.1 | |
| * 5 | 3 | 700. | 0. | 0. | 6095. | 0. | 0. | 6000. | 6000. | 0. | 0. | 1.00 | 52. | 38.3 | E | 23.8 | 11.1 | |
| * 6 | 3 | 2630. | 0. | 0. | 6095. | 0. | 0. | 3344. | 6000. | 0. | * 1445. | 2656. | .56 | 49. | 22.7 | F | 23.5 | 11.3 |
| * 7 | 3 | 2530. | 0. | 0. | 6095. | 0. | 0. | 3344. | 6000. | 0. | ** 2530. | 2656. | .56 | 36. | 30.6 | F | 21.8 | 12.0 |
| * 8 | 4 | 1500. | 336. | 0. | 6431. | 286. | 0. | 3630. | 6386. | 0. | ** 1500. | 2656. | .57 | 30. | 30.6 | F | 20.2 | 12.9 |
| * 9 | 4 | 700. | 0. | 0. | 6431. | 0. | 0. | 3630. | 6440. | 0. | ** 700. | 2656. | .56 | 26. | 34.3 | F | 19.4 | 13.4 |
| * 10 | 4 | 1500. | 0. | 1231. | 6431. | 0. | 1176. | 3630. | 6151. | 0. | ** 1500. | 2521. | .59 | 27. | 33.3 | F | 19.9 | 13.2 |
| * 11 | 3 | 750. | 0. | 0. | 5200. | 0. | 0. | 2454. | 6000. | 0. | ** 750. | 2521. | .41 | 19. | 42.9 | F | 17.2 | 15.2 |
| * 12 | 4 | 350. | 482. | 0. | 5682. | 432. | 0. | 2886. | 6544. | 0. | ** 350. | 2521. | .44 | 18. | 39.3 | F | 15.9 | 16.4 |
| * 13 | 4 | 350. | 0. | 0. | 5682. | 0. | 0. | 2886. | 6640. | 0. | ** 350. | 2521. | .43 | 17. | 42.1 | F | 15.7 | 16.6 |
| * 14 | 4 | 350. | 0. | 495. | 5682. | 0. | 470. | 2886. | 6535. | 0. | ** 350. | 2521. | .44 | 17. | 43.5 | F | 15.5 | 16.7 |
| * 15 | 3 | 700. | 0. | 0. | 5187. | 0. | 0. | 2416. | 6000. | 0. | ** 700. | 2521. | .40 | 14. | 55.6 | F | 16.0 | 16.1 |
| * 16 | 3 | 900. | 744. | 0. | 5931. | 644. | 0. | 3060. | 5834. | 0. | ** 900. | 2521. | .52 | 17. | 60.7 | F | 16.4 | 15.5 |
| * 17 | 3 | 1400. | 393. | 0. | 6324. | 293. | 0. | 3353. | 5913. | 0. | ** 1400. | 2521. | .57 | 16. | 67.8 | F | 16.3 | 15.7 |
| * 18 | 3 | 200. | 0. | 0. | 6324. | 0. | 0. | 3353. | 6000. | 0. | ** 200. | 2521. | .56 | 15. | 73.0 | F | 15.7 | 16.2 |
| * 19 | 3 | 1400. | 0. | 480. | 6324. | 0. | 443. | 3353. | 5919. | 0. | ** 1400. | 2521. | .57 | 15. | 76.0 | F | 15.5 | 16.5 |
| * 20 | 3 | 900. | 0. | 0. | 5844. | 0. | 0. | 2910. | 6000. | 0. | ** 900. | 2521. | .48 | 11. | 85.4 | F | 14.1 | 17.9 |
| * 21 | 4 | 100. | 225. | 0. | 6069. | 225. | 0. | 3135. | 6175. | 0. | ** 100. | 2521. | .51 | 12. | 67.9 | F | 13.0 | 19.5 |
| * 22 | 4 | 100. | 0. | 129. | 6069. | 0. | 120. | 3135. | 6208. | 0. | ** 100. | 2521. | .50 | 11. | 69.0 | F | 12.9 | 19.6 |
| * 23 | 3 | 600. | 0. | 0. | 5940. | 0. | 0. | 3015. | 6000. | 0. | ** 600. | 2521. | .50 | 11. | 92.1 | F | 13.6 | 18.4 |
| * 24 | 3 | 1500. | 184. | 0. | 6124. | 184. | 0. | 3199. | 5954. | 0. | ** 1500. | 2521. | .54 | 11. | 97.4 | F | 13.4 | 18.7 |
| * 25 | 3 | 1500. | 0. | 0. | 6124. | 0. | 0. | 3199. | 6000. | 0. | ** 1500. | 2521. | .53 | 10. | 109.1 | F | 12.6 | 19.8 |
| * 26 | 3 | 8000. | 0. | 0. | 6124. | 0. | 0. | 3199. | 6000. | 0. | ** 8000. | 2521. | .53 | 7. | 148.9 | F | 10.5 | 23.5 |
| * 27 | 5 | 100. | 1531. | 0. | 7655. | 1531. | 0. | 4730. | 10000. | 0. | ** 100. | 2521. | .47 | 5. | 208.2 | F | 8.7 | 28.0 |
| * 28 | 5 | 1000. | 1560. | 0. | 9215. | 1460. | 0. | 6190. | 7750. | 0. | ** 1000. | 1560. | .80 | 12. | 100.6 | F | 14.4 | 20.9 |
| * 29 | 5 | 1000. | 1560. | 10775. | 10775. | 1560. | 7750. | 7750. | 7750. | 0. | 0. | 1.00 | 52. | 29.7 | E | 23.8 | 11.1 | |
| ***** | | | | | | | | | | | | | | | | | | |
| * TOTAL | 135469. | = | 25.7 | MILES | | | | | | MAX(V/C) = 1.00 | LOWEST LOS = F | AVG = 38. | 43.7 | | | 19.3 | 13.7 | |
| ***** | | | | | | | | | | | | | | | | | | |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL NO DIVERSION
 TIME SLICE 1 OF 3

| CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | |
|----------------------------|---------------|----------------|---------------|-------------------|-------------------------|------------------|------------------|
| FREEWAY TRAVEL TIME = | 3918. VEH-HRS | 3956. PASS-HRS | 3918. VEH-HRS | 3956. PASS-HRS | FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 200. VEH-HRS | 210. PASS-HRS | 200. VEH-HRS | 210. PASS-HRS | OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 4118. VEH-HRS | 4166. PASS-HRS | 4118. VEH-HRS | 4166. PASS-HRS | TOTAL TRAVEL DISTANCE = | 149405. VEH-MI. | 150405. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 36. MPH. | | 38. MPH. | | AVERAGE DENSITY = | 44. VP/MPH | 44. VP/MPH |
| TOTAL FUEL = | 7799. GALLONS | | 7799. GALLONS | | TOTAL EMISSIONS = | 2077. KI LOGRAMS | 2077. KI LOGRAMS |

| ***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 ***** | | | | | | | | | |
|---|--------|------------|--------|------------|-------|------------|-------|------------|--------|
| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
| 1 | 0.49 | 2 | 125.12 | 3 | 11.72 | 4 | 2.57 | 5 | 2.99 |
| 6 | 14.67 | 7 | 33.26 | 8 | 30.47 | 9 | 17.12 | 10 | 34.26 |
| 11 | 23.02 | 12 | 12.25 | 13 | 13.37 | 14 | 13.83 | 15 | 29.28 |
| 16 | 35.18 | 17 | 58.45 | 18 | 9.06 | 19 | 65.90 | 20 | 51.67 |
| 21 | 5.87 | 22 | 5.97 | 23 | 36.23 | 24 | 91.96 | 25 | 101.80 |
| 26 | 690.76 | 27 | 18.65 | 28 | 77.66 | 29 | 5.53 | | |

***** TOTAL DELAY = 1619.1 VEH-HRS ***** AVERAGE DELAY = 28.46 MIN/VEH *****

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL NO DIVERSION
 TIME SLICE 1 OF 3

| ***** RAMP DELAYS ***** | | | | | | | | | |
|-------------------------|--------------|---------|----------------|-------|------|------|------|-----------|--|
| | QUEUE LENGTH | DELAY | AVERAGE | GAS | HC | CO | NOX | TOTAL | |
| ON-RAMP | VEHICLES | VEH-HRS | METERING DELAY | GALS | KGMS | KGMS | KGMS | EMISSIONS | |
| 2 | RAMP | 50. | 4.46 | 8.93 | 0.55 | 2.90 | 0.15 | 3.60 | |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| | TOTAL | 50. | 4.46 | 8.93 | 0.55 | 2.90 | 0.15 | 3.60 | |
| 3 | RAMP | 50. | 3.11 | 8.93 | 0.55 | 2.90 | 0.15 | 3.60 | |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| | TOTAL | 50. | 3.11 | 8.93 | 0.55 | 2.90 | 0.15 | 3.60 | |
| 4 | RAMP | 100. | 4.03 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 | |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| | TOTAL | 100. | 4.03 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 | |
| 5 | RAMP | 100. | 7.63 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 | |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| | TOTAL | 100. | 7.63 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 | |

| | | | | | | | | | | |
|---------|---|--------|------|-------|------|-------|------|------|------|------|
| ON-RAMP | 9 | RAMP | 100. | 50.00 | 2.40 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 50.00 | 2.40 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |

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1 INSTITUTE OF TRANSPORTATION STUDIES
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 TIME SLICE 2 OF 3
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 QUEUE COLLISION IN SECTION 3 T2 =0.481

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 SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 3
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 **
 ** FREeway TRAVEL TIME (MINUTES) **
 **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | |
|-----------|--|-----------------------|-------|-------|-------|-------|-------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 |
| * 1 * | | 0.24 | 27.59 | 29.56 | 32.55 | 33.43 | 42.66 |
| * 2 * | | 0.00 | 2.46 | 4.43 | 7.42 | 8.30 | 17.53 |
| * 3 * | | 0.00 | 0.00 | 1.12 | 4.10 | 4.98 | 14.21 |
| * 4 * | | 0.00 | 0.00 | 0.00 | 2.20 | 3.08 | 12.31 |
| * 5 * | | 0.00 | 0.00 | 0.00 | 1.59 | 2.47 | 11.70 |
| * 6 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.15 | 9.39 |
| * 7 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 8.76 |
| * 8 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.95 |
| * 9 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.81 |
| * 10 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.22 |

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 TIME SLICE 2 OF 3
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TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISS |
|-----------|--------|------------|-------------------|--------------------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|---------|
| * SEC | * LNS | * LENGTH | * ORG DES SSEC | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 1 | 5 | 1370. | 7071. 1414. 7071. | 7071. 1414. 7071. | 10000. | 0. | 0. | 0. | .71 | 65. | 21.8 | C | 19.2 | 14.0 |
| * 2 | 3 | 99999. | 0. 0. 5657. | 0. 0. 5302. | 7360. | 0. * | 2699. | 355. | .72 | 60. | 29.6 | F | 19.6 | 13.7 |
| * 3 | 3 | 2740. | 0. 0. 5657. | 0. 0. 5302. | 6000. | 0. ** | 2740. | 467. | .88 | 22. | 81.0 | F | 18.6 | 15.7 |
| * 4 | 3 | 600. | 0. 0. 5657. | 0. 0. 5302. | 6000. | 0. ** | 600. | 467. | .88 | 19. | 93.5 | F | 17.7 | 16.8 |
| * 5 | 3 | 700. | 0. 0. 5657. | 0. 0. 5302. | 6000. | 0. ** | 700. | 467. | .88 | 18. | 98.5 | F | 17.4 | 17.2 |
| * 6 | 3 | 2630. | 0. 0. 5657. | 0. 0. 5302. | 6000. | 0. ** | 2630. | 467. | .88 | 16. | 108.3 | F | 16.8 | 18.1 |
| * 7 | 3 | 2530. | 0. 0. 5657. | 0. 0. 5302. | 6000. | 0. ** | 2530. | 467. | .88 | 16. | 110.4 | F | 16.7 | 18.3 |
| * 8 | 4 | 1500. | 382. 0. 6039. | 382. 0. 5684. | 6383. | 0. ** | 1500. | 467. | .89 | 16. | 86.7 | F | 16.9 | 18.1 |
| * 9 | 4 | 700. | 0. 0. 6039. | 0. 0. 5684. | 6440. | 0. ** | 700. | 467. | .88 | 16. | 89.1 | F | 16.7 | 18.3 |
| * 10 | 4 | 1500. | 0. 1226. 6039. | 0. 1216. 5684. | 6156. | 0. ** | 1500. | 467. | .92 | 18. | 77.0 | F | 17.8 | 16.9 |
| * 11 | 3 | 750. | 0. 0. 4813. | 0. 0. 4436. | 6000. | 0. ** | 750. | 467. | .74 | 10. | 148.1 | F | 13.1 | 22.8 |
| * 12 | 4 | 350. | 563. 0. 5376. | 563. 0. 4999. | 6535. | 0. ** | 350. | 467. | .77 | 11. | 115.5 | F | 13.6 | 22.2 |
| * 13 | 4 | 350. | 0. 0. 5376. | 0. 0. 4999. | 6640. | 0. ** | 350. | 467. | .75 | 10. | 120.0 | F | 13.4 | 22.5 |
| * 14 | 4 | 350. | 0. 532. 5376. | 0. 540. 4999. | 6532. | 0. ** | 350. | 467. | .77 | 11. | 115.4 | F | 13.6 | 22.1 |
| * 15 | 3 | 700. | 0. 0. 4844. | 0. 0. 4460. | 6000. | 0. ** | 700. | 467. | .74 | 10. | 147.1 | F | 13.2 | 22.7 |
| * 16 | 3 | 900. | 789. 0. 5633. | 789. 0. 5249. | 5833. | 0. ** | 900. | 467. | .90 | 17. | 103.2 | F | 17.1 | 17.8 |
| * 17 | 3 | 1400. | 437. 0. 6070. | 437. 0. 5686. | 5907. | 0. ** | 1400. | 221. | .96 | 21. | 88.4 | F | 19.0 | 15.5 |
| * 18 | 3 | 200. | 0. 0. 6070. | 0. 0. 5686. | 6000. | 0. ** | 200. | 221. | .95 | 20. | 93.7 | F | 18.6 | 16.0 |
| * 19 | 3 | 1400. | 0. 631. 6070. | 0. 606. 5686. | 5901. | 0. ** | 1400. | 215. | .96 | 22. | 88.1 | F | 19.0 | 15.5 |
| * 20 | 3 | 900. | 0. 0. 5439. | 0. 0. 5080. | 6000. | 0. ** | 900. | 215. | .85 | 14. | 120.1 | F | 15.6 | 19.6 |
| * 21 | 4 | 100. | 242. 0. 5681. | 240. 0. 5320. | 6172. | 0. ** | 100. | 215. | .86 | 15. | 89.6 | F | 16.2 | 19.0 |
| * 22 | 4 | 100. | 0. 199. 5681. | 0. 191. 5320. | 6198. | 0. ** | 100. | 215. | .86 | 15. | 90.7 | F | 16.0 | 19.1 |
| * 23 | 3 | 600. | 0. 0. 5482. | 0. 0. 5129. | 6000. | 0. ** | 600. | 215. | .85 | 14. | 118.0 | F | 15.9 | 19.2 |
| * 24 | 3 | 1500. | 168. 0. 5650. | 168. 0. 5297. | 5958. | 0. ** | 1500. | 215. | .89 | 16. | 108.2 | F | 16.8 | 18.1 |
| * 25 | 3 | 1500. | 0. 0. 5650. | 0. 0. 5297. | 6000. | 0. ** | 1500. | 215. | .88 | 16. | 110.6 | F | 16.7 | 18.3 |
| * 26 | 3 | 8000. | 0. 0. 5650. | 0. 0. 5297. | 6000. | 0. ** | 8000. | 215. | .88 | 16. | 110.6 | F | 16.7 | 18.3 |
| * 27 | 5 | 100. | 1413. 0. 7063. | 1413. 0. 6710. | 10000. | 0. ** | 100. | 215. | .67 | 8. | 166.0 | F | 10.8 | 25.1 |
| * 28 | 5 | 1000. | 520. 0. 7583. | 520. 0. 7230. | 7750. | 0. ** | 1000. | 215. | .93 | 19. | 75.6 | F | 18.1 | 16.6 |
| * 29 | 5 | 1000. | 520. 8103. 8103. | 520. 7750. 7750. | 7750. | 0. | 0. | 0. | 1.00 | 52. | 29.7 | E | 23.8 | 11.1 |

* TOTAL 135469. = 25.7 MILES US-101_SB_PM_P2_2018_MOD_PE.txt
 * MAX(V/C) = 1.00 LOWEST LOS = F AVG = 37. 47.5 18.9 14.7 *

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 3

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|----------------------------|--------------------|------------------|-------------------|------------------|
| FREEWAY TRAVEL TIME = | 3917. VEH-HRS | 3949. PASS-HRS | 7834. VEH-HRS | 7905. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 401. VEH-HRS | 421. PASS-HRS | 601. VEH-HRS | 631. PASS-HRS |
| OFF-RAMP DELAY = | 16. VEH-HRS | 16. PASS-HRS | 16. VEH-HRS | 16. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 4334. VEH-HRS | 4386. PASS-HRS | 8451. VEH-HRS | 8552. PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 144249. VEH-MI. | 145273. PASS-MI. | 293654. VEH-MI. | 295679. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 33. MPH | | 37. MPH | |
| AVERAGE DENSITY = | 48. VPMP | | 46. VPMP | |
| TOTAL FUEL = | 7796. GALLONS | | 15595. GALLONS | |
| TOTAL EMISSIONS = | 2180. KILOGRAMS | | 4257. KILOGRAMS | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|--------|------------|--------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 146.13 | 3 | 86.42 | 4 | 23.01 | 5 | 28.71 |
| 6 | 121.47 | 7 | 119.61 | 8 | 73.63 | 9 | 35.65 | 10 | 62.62 |
| 11 | 53.43 | 12 | 25.54 | 13 | 26.72 | 14 | 25.50 | 15 | 49.42 |
| 16 | 39.03 | 17 | 47.13 | 18 | 7.33 | 19 | 46.86 | 20 | 48.10 |
| 21 | 5.24 | 22 | 5.32 | 23 | 31.24 | 24 | 69.10 | 25 | 71.14 |
| 26 | 379.40 | 27 | 13.77 | 28 | 50.52 | 29 | 5.53 | | |

***** TOTAL DELAY = 1697.6 VEH-HRS ***** AVERAGE DELAY = 19.12 MIN/VEH *****

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 3

***** RAMP DELAYS *****

| | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|------------|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|
| ON-RAMP 2 | RAMP 50. | 50.00 | 6.94 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 50. | 50.00 | 6.94 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| ON-RAMP 3 | RAMP 50. | 50.00 | 4.89 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 50. | 50.00 | 4.89 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| ON-RAMP 4 | RAMP 100. | 100.00 | 6.75 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 100. | 100.00 | 6.75 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP 5 | RAMP 100. | 100.00 | 11.17 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 100. | 100.00 | 11.17 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP 6 | RAMP 2. | 1.00 | 0.25 | 0.36 | 0.02 | 0.12 | 0.01 | 0.14 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 2. | 1.00 | 0.25 | 0.36 | 0.02 | 0.12 | 0.01 | 0.14 |
| ON-RAMP 9 | RAMP 100. | 100.00 | 11.63 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 100. | 100.00 | 11.63 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| OFF-RAMP 2 | OUTPUT POINT 32. | 16.04 | | 5.73 | 0.36 | 1.86 | 0.10 | 2.31 |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 3 OF 3

 ** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS | * DESTINATIONS ACROSS * | | | | | |
|-----------|-------------------------|-------|-------|-------|-------|-------|
| * DOWN | 1 | 2 | 3 | 4 | 5 | 6 |
| * 1 * | 0.24 | 32.62 | 34.87 | 38.60 | 39.67 | 50.71 |
| * 2 * | 0.00 | 3.05 | 5.31 | 9.04 | 10.10 | 21.14 |
| * 3 * | 0.00 | 0.00 | 1.29 | 5.02 | 6.08 | 17.12 |
| * 4 * | 0.00 | 0.00 | 0.00 | 2.85 | 3.91 | 14.95 |

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| | | | | | | | | | |
|---|----|---|------|------|------|------|------|-------|---|
| * | 5 | * | 0.00 | 0.00 | 0.00 | 2.09 | 3.15 | 14.19 | * |
| * | 6 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.19 | 11.23 | * |
| * | 7 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 10.47 | * |
| * | 8 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.04 | * |
| * | 9 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.88 | * |
| * | 10 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.22 | * |
| * | * | * | * | * | * | * | * | * | * |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB | * NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMI SS | | | |
|-------|-------|----------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|----------|------|------|------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * ORG | * DES | * SSEC | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VP/PL | * LEVEL | * MPG | * GS/VM | | | |
| * 1 | 5 | 1370. | 6510. | 1302. | 6510. | 6510. | 1302. | 6510. | 10000. | 0. | 0. | .65 | 65. | 20.0 | C | 19.2 | 14.0 | | |
| * 2 | 3 | 99999. | 0. | 0. | 5208. | 0. | 0. | 5027. | 7360. | 0. | * | 4540. | 181. | .68 | 52. | 32.0 | F | 18.8 | 14.3 |
| * 3 | 3 | 2740. | 0. | 0. | 5208. | 0. | 0. | 5027. | 6000. | 0. | ** | 2740. | 181. | .84 | 14. | 122.4 | F | 15.3 | 19.9 |
| * 4 | 3 | 600. | 0. | 0. | 5208. | 0. | 0. | 5027. | 6000. | 0. | ** | 600. | 181. | .84 | 14. | 122.4 | F | 15.3 | 19.9 |
| * 5 | 3 | 700. | 0. | 0. | 5208. | 0. | 0. | 5027. | 6000. | 0. | ** | 700. | 181. | .84 | 14. | 122.4 | F | 15.3 | 19.9 |
| * 6 | 3 | 2630. | 0. | 0. | 5208. | 0. | 0. | 5027. | 6000. | 0. | ** | 2630. | 181. | .84 | 14. | 122.4 | F | 15.3 | 19.9 |
| * 7 | 3 | 2530. | 0. | 0. | 5208. | 0. | 0. | 5027. | 6000. | 0. | ** | 2530. | 181. | .84 | 14. | 122.4 | F | 15.3 | 19.9 |
| * 8 | 4 | 1500. | 278. | 0. | 5486. | 278. | 0. | 5305. | 6398. | 0. | ** | 1500. | 181. | .83 | 13. | 99.7 | F | 15.1 | 20.2 |
| * 9 | 4 | 700. | 0. | 0. | 5486. | 0. | 0. | 5305. | 6440. | 0. | ** | 700. | 181. | .82 | 13. | 101.5 | F | 14.9 | 20.4 |
| * 10 | 4 | 1500. | 0. | 1109. | 5486. | 0. | 1109. | 5305. | 6179. | 0. | ** | 1500. | 181. | .86 | 15. | 90.3 | F | 16.0 | 19.1 |
| * 11 | 3 | 750. | 0. | 0. | 4377. | 0. | 0. | 4196. | 6000. | 0. | ** | 750. | 181. | .70 | 9. | 158.6 | F | 11.6 | 24.2 |
| * 12 | 4 | 350. | 504. | 0. | 4881. | 504. | 0. | 4700. | 6544. | 0. | ** | 350. | 181. | .72 | 9. | 125.7 | F | 12.3 | 23.6 |
| * 13 | 4 | 350. | 0. | 0. | 4881. | 0. | 0. | 4700. | 6640. | 0. | ** | 350. | 181. | .71 | 9. | 129.8 | F | 11.9 | 23.9 |
| * 14 | 4 | 350. | 0. | 455. | 4881. | 0. | 455. | 4700. | 6546. | 0. | ** | 350. | 181. | .72 | 9. | 125.8 | F | 12.3 | 23.6 |
| * 15 | 3 | 700. | 0. | 0. | 4426. | 0. | 0. | 4245. | 6000. | 0. | ** | 700. | 181. | .71 | 9. | 156.5 | F | 11.9 | 23.9 |
| * 16 | 3 | 900. | 627. | 0. | 5053. | 627. | 0. | 4872. | 5866. | 0. | ** | 900. | 181. | .83 | 13. | 121.5 | F | 15.1 | 20.1 |
| * 17 | 3 | 1400. | 395. | 0. | 5448. | 395. | 0. | 5267. | 5915. | 0. | ** | 1400. | 181. | .89 | 16. | 107.1 | F | 16.9 | 18.1 |
| * 18 | 3 | 200. | 0. | 0. | 5448. | 0. | 0. | 5267. | 6000. | 0. | ** | 200. | 181. | .88 | 16. | 112.0 | F | 16.6 | 18.5 |
| * 19 | 3 | 1400. | 0. | 524. | 5448. | 0. | 525. | 5267. | 5914. | 0. | ** | 1400. | 181. | .89 | 16. | 107.1 | F | 16.9 | 18.1 |
| * 20 | 3 | 900. | 0. | 0. | 4924. | 0. | 0. | 4742. | 6000. | 0. | ** | 900. | 181. | .79 | 12. | 134.8 | F | 14.1 | 21.4 |
| * 21 | 4 | 100. | 194. | 0. | 5118. | 196. | 0. | 4938. | 6184. | 0. | ** | 100. | 181. | .80 | 12. | 102.6 | F | 14.3 | 21.2 |
| * 22 | 4 | 100. | 0. | 174. | 5118. | 0. | 174. | 4938. | 6202. | 0. | ** | 100. | 181. | .80 | 12. | 103.3 | F | 14.2 | 21.3 |
| * 23 | 3 | 600. | 0. | 0. | 4944. | 0. | 0. | 4764. | 6000. | 0. | ** | 600. | 181. | .79 | 12. | 133.9 | F | 14.2 | 21.3 |
| * 24 | 3 | 1500. | 200. | 0. | 5144. | 200. | 0. | 4964. | 5950. | 0. | ** | 1500. | 181. | .83 | 14. | 122.3 | F | 15.2 | 20.0 |
| * 25 | 3 | 1500. | 0. | 0. | 5144. | 0. | 0. | 4964. | 6000. | 0. | ** | 1500. | 181. | .83 | 13. | 125.1 | F | 15.0 | 20.2 |
| * 26 | 3 | 8000. | 0. | 0. | 5144. | 0. | 0. | 4964. | 6000. | 0. | ** | 8000. | 181. | .83 | 13. | 125.1 | F | 15.0 | 20.2 |
| * 27 | 5 | 100. | 1286. | 0. | 6430. | 1286. | 0. | 6250. | 10000. | 0. | ** | 100. | 181. | .63 | 7. | 178.0 | F | 9.9 | 26.3 |
| * 28 | 5 | 1000. | 750. | 0. | 7180. | 750. | 0. | 7000. | 7750. | 0. | ** | 1000. | 181. | .90 | 17. | 81.6 | F | 17.2 | 17.6 |
| * 29 | 5 | 1000. | 750. | 7930. | 7930. | 750. | 7750. | 7750. | 7750. | 0. | * | 0. | 0. | 1.00 | 52. | 29.7 | E | 23.8 | 11.1 |

TOTAL 135469. = 25.7 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 31. 53.3 17.8 15.6

| | CURRENT TIME SLICE | | CUMULATIVE VALUES |
|----------------------------|--------------------|----------|-------------------|
| FREWAY TRAVEL TIME = | 4324. VEH-HRS | PASS-HRS | 12158. VEH-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | PASS-HRS | 0. VEH-HRS |
| ON-RAMP MRG/CAP DELAY = | 401. VEH-HRS | PASS-HRS | 1002. VEH-HRS |
| OFF-RAMP DELAY = | 16. VEH-HRS | PASS-HRS | 32. VEH-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 4741. VEH-HRS | PASS-HRS | 13193. VEH-HRS |
| TOTAL TRAV DISTANCE = | 133384. VEH-MI. | PASS-MI. | 427038. VEH-MI. |
| AVERAGE SYSTEM SPEED = | 28. MPH. | | 35. MPH. |
| AVERAGE DENSITY = | 53. VP/PL | | 48. VP/PL |
| TOTAL FUEL = | 7639. GALLONS | | 23234. GALLONS |
| TOTAL EMISSIONS = | 2143. KI LOGRAMS | | 6400. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|--------|------------|--------|------------|--------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 364.65 | 3 | 150.41 | 4 | 32.94 | 5 | 38.43 |
| 6 | 144.37 | 7 | 138.88 | 8 | 90.11 | 9 | 43.00 | 10 | 79.48 |
| 11 | 58.42 | 12 | 28.54 | 13 | 29.62 | 14 | 28.56 | 15 | 53.58 |
| 16 | 49.38 | 17 | 63.72 | 18 | 9.65 | 19 | 63.68 | 20 | 56.51 |
| 21 | 6.33 | 22 | 6.39 | 23 | 37.30 | 24 | 82.53 | 25 | 84.96 |
| 26 | 453.11 | 27 | 15.04 | 28 | 56.88 | 29 | 5.53 | | |

***** TOTAL DELAY = 2272.0 VEH-HRS ***** AVERAGE DELAY = 27.17 MIN/VEH *****

***** RAMP DELAYS *****

| | | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS | |
|----------|---|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|-------|
| ON-RAMP | 2 | RAMP | 50. | 50.00 | 9.15 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 50. | 50.00 | 9.15 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| ON-RAMP | 3 | RAMP | 50. | 50.00 | 5.42 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 50. | 50.00 | 5.42 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| ON-RAMP | 4 | RAMP | 100. | 100.00 | 8.25 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 100.00 | 8.25 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP | 5 | RAMP | 100. | 100.00 | 12.12 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 100.00 | 12.12 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP | 6 | RAMP | 0. | 1.00 | 0.04 | 0.36 | 0.02 | 0.12 | 0.01 | 0.14 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 0. | 1.00 | 0.04 | 0.36 | 0.02 | 0.12 | 0.01 | 0.14 |
| ON-RAMP | 9 | RAMP | 100. | 100.00 | 8.57 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 100.00 | 8.57 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| OFF-RAMP | 2 | OUTPUT POINT | 0. | 16.04 | | 5.73 | 0.36 | 1.86 | 0.10 | 2.31 |

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FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP PPP LLL
FFFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEE QQQ QQQ 1111 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQ QQQ 1111 222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 1111111 222222222 PPP LLLLLLLLLL
    
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FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 2 AND 26 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65 MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

FREeway AND ARTERIAL DESIGN FEATURES

| ** SUB NO. | ** SSEC | ** SSEC | ** DESIGN | ** ORG | ** TRK | ** SSEC | ** PCT | ** PCT | ** DES | ** SPECIAL | ** FF.SPD. | ** CAP. | ** ART | ** GRADE | ** SUBSECTION | ** LOCATION | ** |
|------------|---------|---------|-----------|--------|--------|---------|--------|-----------|---------|-------------|-------------|-------------|---------|-------------|-------------------------|-------------|----|
| ** SEC | ** LNS | ** CAP | ** LENGTH | ** DES | ** FAC | ** GRAD | ** TRK | ** TRUCKS | ** RAMP | ** ALT. RTE | ** ALT. RTE | ** ALT. RTE | ** TYPE | ** ALT. RTE | ** | ** | ** |
| ** 1 | | | | | | | | | | | | | | | | | ** |
| ** 2 | 1 | 1650. | 99999. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | | ** |
| ** 3 | 1 | 1650. | 2740. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-85 Off to Shore On | | ** |
| ** 4 | 1 | 1650. | 600. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Shore. On to Moffet Off | | ** |
| ** 5 | 1 | 1650. | 700. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Moffett Off to On | | ** |
| ** 6 | 1 | 1650. | 2630. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Moffett On to Ellis Off | | ** |
| ** 7 | 1 | 1650. | 2530. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Ellis Off to On-ramp | | ** |
| ** 8 | 1 | 1650. | 1500. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Ellis On-ramp | | ** |
| ** 9 | 1 | 1650. | 700. | 65 | | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Ellis / US 237 | | ** |
| ** 10 | 1 | 1650. | 1500. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 EB Off-Ramp | | ** |
| ** 11 | 1 | 1650. | 750. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 / SR-237 | | ** |
| ** 12 | 1 | 1650. | 350. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 EB On-Ramp | | ** |
| ** 13 | 1 | 1650. | 350. | 65 | | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | US 237 / Mathilda | | ** |
| ** 14 | 1 | 1650. | 350. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-Ramp | | ** |
| ** 15 | 1 | 1650. | 700. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | | ** |
| ** 16 | 1 | 1650. | 900. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda SB On-Ramp | | ** |
| ** 17 | 1 | 1650. | 1400. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda NB On-Ramp | | ** |
| ** 18 | 1 | 1650. | 200. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Fair Oaks | | ** |
| ** 19 | 1 | 1650. | 1400. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks SB Off-Ramp | | ** |

** 20 1 1650. 900. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks SB/ Fair Oaks **

FREEWAY AND ARTERIAL DESIGN FEATURES

Table with columns: SUB NO., SEC LNS, SSEC CAP, SSEC LENGTH, DESIGN SPEED, ORG DES, TRK FAC, SSEC GRAD, PCT TRK, PCT DES TRUCKS, SPECIAL RAMP, FF. SPD. ALT. RTE, CAP. ALT. RTE, ART TYPE, GRADE ALT. RTE, SUBSECTION, LOCATION. Rows 21-29.

FREEWAY TRAVEL TIME (MINUTES)

Table with columns: ORIGINS DOWN, DESTINATIONS ACROSS (1-7). Rows 1-11.

TIME SLICE FREEWAY PERFORMANCE TABLE

US-101_SB_PM_P2_2018_MOD_PL.txt

Table with columns: SUB SEC, NO. LNS, SSEC LENGTH, O-D ORG, DATA DES, DEMANDS SSEC, ADJUSTED ORG, VOLUMES DES, SSEC, WEAVE EFF, CONGEST LENGTH, STORAGE RATE, V/C RATIO, SPEED MPH, DENSITY VPML, LOS LEVEL, FUEL MPG, EMISSIONS GS/VM. Includes a summary row for TOTAL.

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 16:47 PAGE 6
UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
TIME SLICE 1 OF 3

Summary table comparing CURRENT TIME SLICE and CUMULATIVE VALUES for metrics like FREEWAY TRAVEL TIME, MERGE DELAY, RAMP DELAY, SYSTEM TRAVEL TIME, etc.

Mainline delay summary table with columns: SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY. Includes total and average delay values.

***** TOTAL DELAY = 71.7 VEH-HRS ***** AVERAGE DELAY = 2.82 MIN/VEH *****

***** RAMP DELAYS *****

Ramp delay summary table with columns: OFF-RAMP, OUTPUT POINT, QUEUE LENGTH, DELAY, GAS, HC, CO, NOX, TOTAL EMISSIONS.

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 2/29/2016 16:47 PAGE 7
UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
TIME SLICE 2 OF 3

**
** FREeway TRAVEL TIME (MINUTES) **
**

* ORIGINS DESTINATIONS ACROSS *
* DOWN 1 2 3 4 5 6 7 *

Origin-Destination matrix table showing travel times between various origin and destination points.

| | | | | | | | | | | |
|---|--------|------|------|------|------|------|------|------|------|---|
| + | * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.02 | 4.04 | 0.00 | * |
| + | * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.21 | 0.00 | | * |
| + | * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.90 | 0.00 | | * |
| + | * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.74 | 0.00 | | * |
| + | * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.06 | 0.00 | | * |
| + | * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.92 | 0.00 | | * |
| + | * 9 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | * |
| + | * 10 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | * |
| + | * 11 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | * |
| + | * * | | | | | | | | | * |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | |
|-----------|----------|------------|-----------|------------|-----------|--------|---------|-----------------|----------------|-----------|---------|-----------|---------|--------|-------------|------|------|
| * SEC LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | |
| * 1 | | | | | | | | | | | | | | | | | |
| * 2 | 1 | 99999. | 1414. | 0. | 1414. | 1414. | 0. | 1414. | 1650. | 0. | 0. | .86 | 65. | 21.8 | C | 20.0 | 13.7 |
| * 3 | 1 | 2740. | 0. | 0. | 1414. | 0. | 0. | 1414. | 1650. | 0. | 0. | .86 | 65. | 21.8 | C | 20.0 | 13.7 |
| * 4 | 1 | 600. | 0. | 0. | 1414. | 0. | 0. | 1414. | 1650. | 0. | 0. | .86 | 65. | 21.8 | C | 20.0 | 13.7 |
| * 5 | 1 | 700. | 0. | 0. | 1414. | 0. | 0. | 1414. | 1650. | 0. | 0. | .86 | 65. | 21.8 | C | 20.0 | 13.7 |
| * 6 | 1 | 2630. | 0. | 0. | 1414. | 0. | 0. | 1414. | 1650. | 0. | 0. | .86 | 65. | 21.8 | C | 20.0 | 13.7 |
| * 7 | 1 | 2530. | 0. | 0. | 1414. | 0. | 0. | 1414. | 1650. | 0. | 0. | .86 | 65. | 21.8 | C | 20.0 | 13.7 |
| * 8 | 1 | 1500. | 57. | 0. | 1471. | 57. | 0. | 1471. | 1650. | 0. | 0. | .89 | 60. | 24.7 | C | 22.8 | 12.0 |
| * 9 | 1 | 700. | 0. | 0. | 1471. | 0. | 0. | 1471. | 1650. | 0. | 0. | .89 | 60. | 24.7 | C | 22.8 | 12.0 |
| * 10 | 1 | 1500. | 0. | 284. | 1471. | 0. | 283. | 1471. | 1650. | 0. | 0. | .89 | 60. | 24.7 | C | 22.8 | 12.0 |
| * 11 | 1 | 750. | 0. | 0. | 1187. | 0. | 0. | 1187. | 1650. | 0. | 0. | .72 | 65. | 18.3 | C | 20.0 | 13.7 |
| * 12 | 1 | 350. | 105. | 0. | 1292. | 105. | 0. | 1292. | 1650. | 0. | 0. | .78 | 65. | 19.9 | C | 20.0 | 13.7 |
| * 13 | 1 | 350. | 0. | 0. | 1292. | 0. | 0. | 1292. | 1650. | 0. | 0. | .78 | 65. | 19.9 | C | 20.0 | 13.7 |
| * 14 | 1 | 350. | 0. | 108. | 1292. | 0. | 108. | 1292. | 1650. | 0. | 0. | .78 | 65. | 19.9 | C | 20.0 | 13.7 |
| * 15 | 1 | 700. | 0. | 0. | 1184. | 0. | 0. | 1184. | 1650. | 0. | 0. | .72 | 65. | 18.2 | C | 20.0 | 13.7 |
| * 16 | 1 | 900. | 167. | 0. | 1351. | 167. | 0. | 1351. | 1650. | 0. | 0. | .82 | 65. | 20.8 | C | 20.0 | 13.7 |
| * 17 | 1 | 1400. | 93. | 0. | 1444. | 93. | 0. | 1444. | 1650. | 0. | 0. | .87 | 65. | 22.2 | C | 20.0 | 13.7 |
| * 18 | 1 | 200. | 0. | 0. | 1444. | 0. | 0. | 1444. | 1650. | 0. | 0. | .87 | 65. | 22.2 | C | 20.0 | 13.7 |
| * 19 | 1 | 1400. | 0. | 99. | 1444. | 0. | 99. | 1444. | 1650. | 0. | 0. | .87 | 65. | 22.2 | C | 20.0 | 13.7 |
| * 20 | 1 | 900. | 0. | 0. | 1344. | 0. | 0. | 1344. | 1650. | 0. | 0. | .81 | 65. | 20.7 | C | 20.0 | 13.7 |
| * 21 | 1 | 100. | 58. | 0. | 1402. | 58. | 0. | 1402. | 1650. | 0. | 0. | .85 | 65. | 21.6 | C | 20.0 | 13.7 |
| * 22 | 1 | 100. | 0. | 32. | 1402. | 0. | 32. | 1402. | 1650. | 0. | 0. | .85 | 65. | 21.6 | C | 20.0 | 13.7 |
| * 23 | 1 | 600. | 0. | 0. | 1371. | 0. | 0. | 1371. | 1650. | 0. | 0. | .83 | 65. | 21.1 | C | 20.0 | 13.7 |
| * 24 | 1 | 1500. | 42. | 0. | 1413. | 42. | 0. | 1413. | 1650. | 0. | 0. | .86 | 65. | 21.7 | C | 20.0 | 13.7 |
| * 25 | 1 | 1500. | 0. | 0. | 1413. | 0. | 0. | 1413. | 1650. | 0. | 0. | .86 | 65. | 21.7 | C | 20.0 | 13.7 |
| * 26 | 1 | 8000. | 0. | 1413. | 1413. | 0. | 1413. | 1413. | 1650. | 0. | 0. | .86 | 65. | 21.7 | C | 20.0 | 13.7 |
| * 27 | | | | | | | | | | | | | | | | | |
| * 28 | | | | | | | | | | | | | | | | | |
| * 29 | | | | | | | | | | | | | | | | | |
| * TOTAL | 131999. | = | 25.0 | MILES | | | | MAX(V/C) = 0.89 | LOWEST LOS = C | AVG = 65. | 21.8 | | | 20.1 | 13.7 | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|-----------------------------------|------------------------------------|
| FREEWAY TRAVEL TIME = | 544. VEH-HRS 1089. PASS-HRS | 1201. VEH-HRS 2402. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 5. VEH-HRS 9. PASS-HRS | 7. VEH-HRS 13. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 549. VEH-HRS 1098. PASS-HRS | 1208. VEH-HRS 2416. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 35289. VEH-MI. 70578. PASS-MI. | 73322. VEH-MI. 146644. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 64. MPH. | 61. MPH. |
| AVERAGE DENSITY = | 22. VPMP | 24. VPMP |
| TOTAL FUEL = | 1760. GALLONS | 3389. GALLONS |
| TOTAL EMISSIONS = | 484. KILOGRAMS | 931. KILOGRAMS |

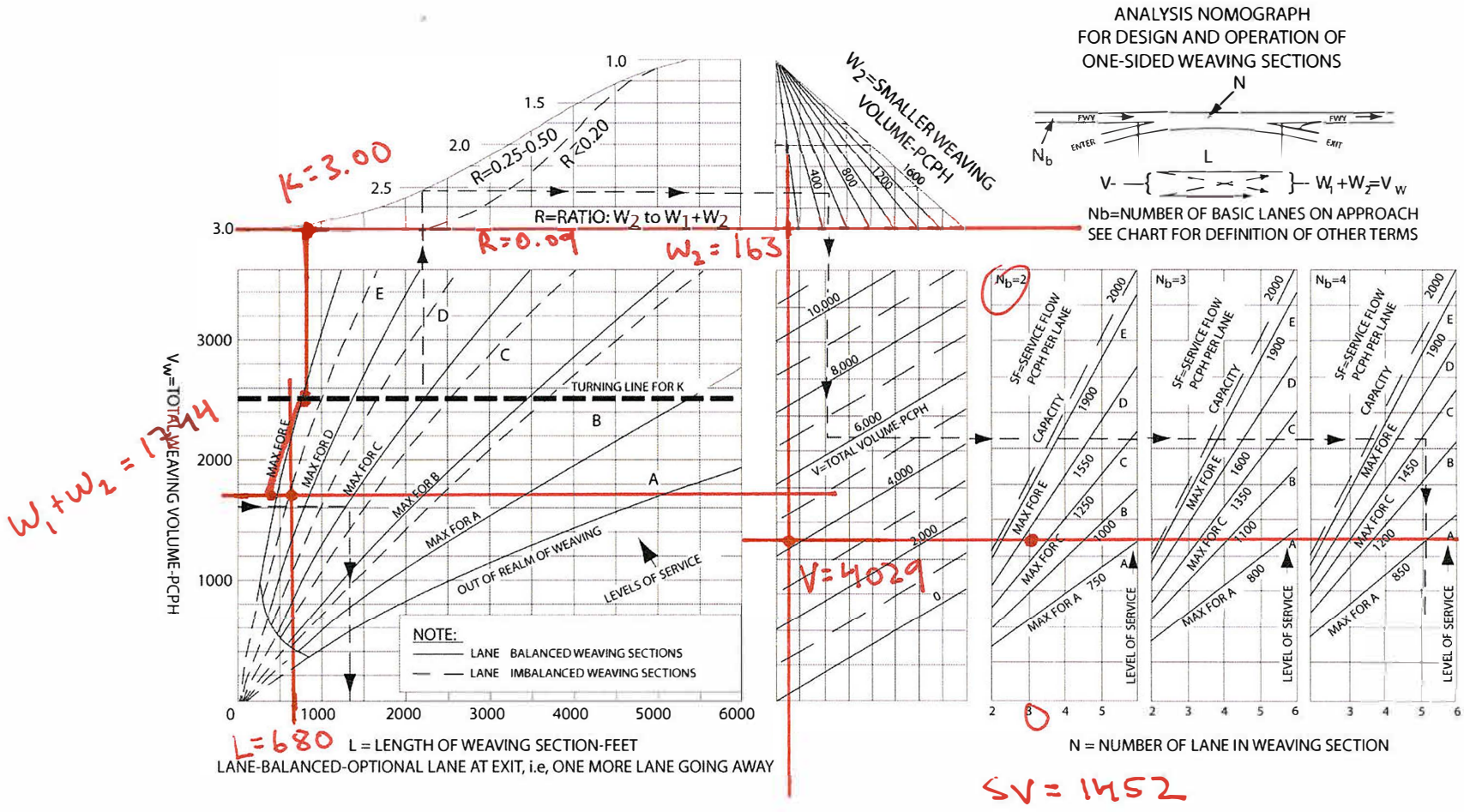
***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.58 | 9 | 0.27 | 10 | 0.58 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

APPENDIX N – YEAR 2018 LEISCH WEAVING ANALYSIS SHEETS



LOSS



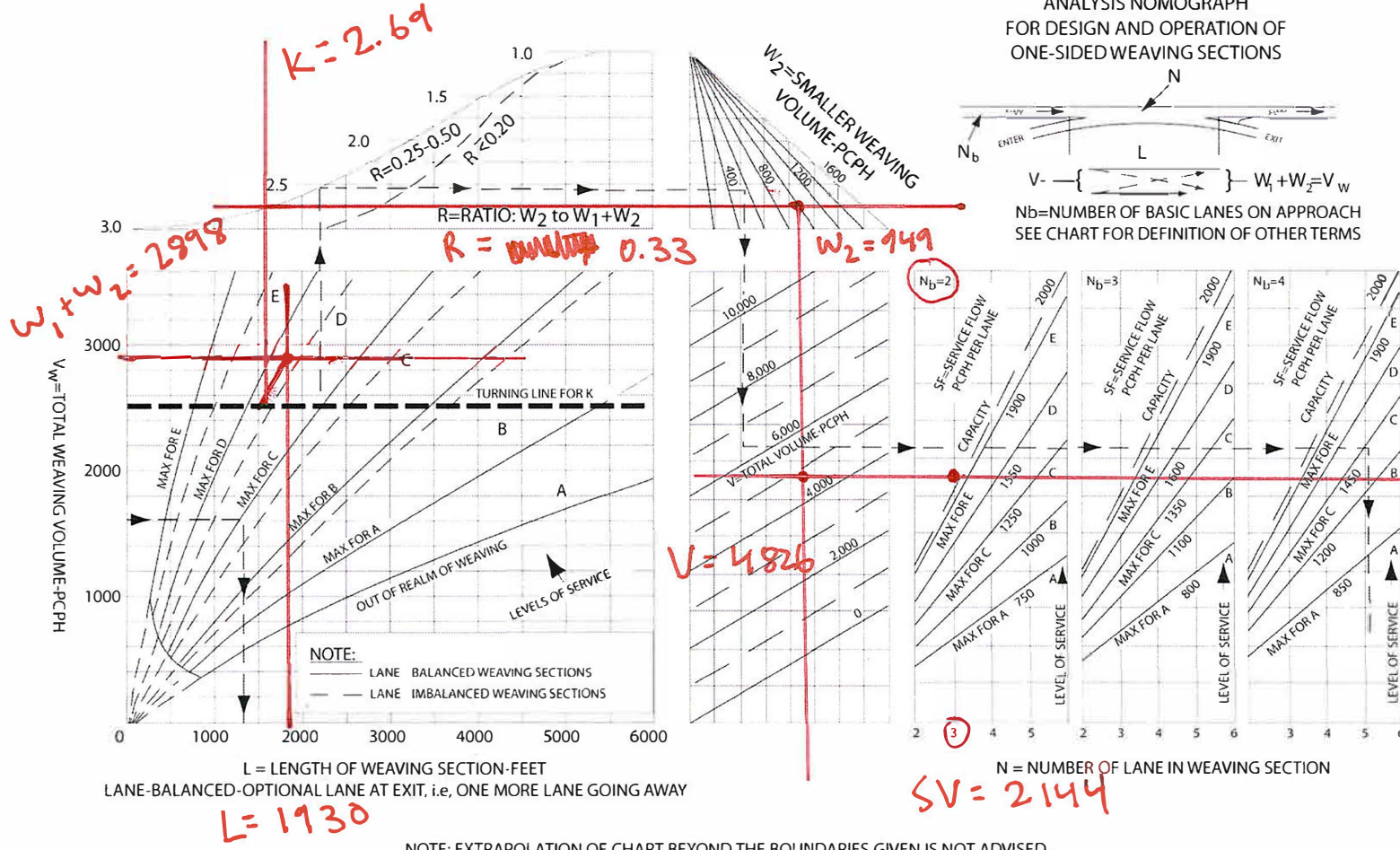
Design Curve for Freeway and Collector Weaving

Figure 504.7A

NOTE: EXTRAPOLATION OF CHART BEYOND THE BOUNDARIES GIVEN IS NOT ADVISED.

Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, W_1+W_2 (or W_w) followed by projection to the right, intersecting the desired weaving LOS: a vertical drop from this point provides weaving distance $L = 1300$ ft. Returning to first intersection point of W_w with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K:" from here the solution line is extended vertically to intersect the K values curve, from which a horizontal extension meets the desired W_2 volume. Then a downward turn to total volume, V , from which the line is horizontally projected to the right, intersection (in this case) the desired LOS = C curve having an SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields a N of 5.2: this would be rounded to $N = 5$ lanes.

LOS F



Design Curve for Freeway and Collector Weaving
Figure 504.7A

SV = 2144

L = 1930

Nb = 2

N = 3

V = 4826

W₁+W₂ = 2998

K = 2.69

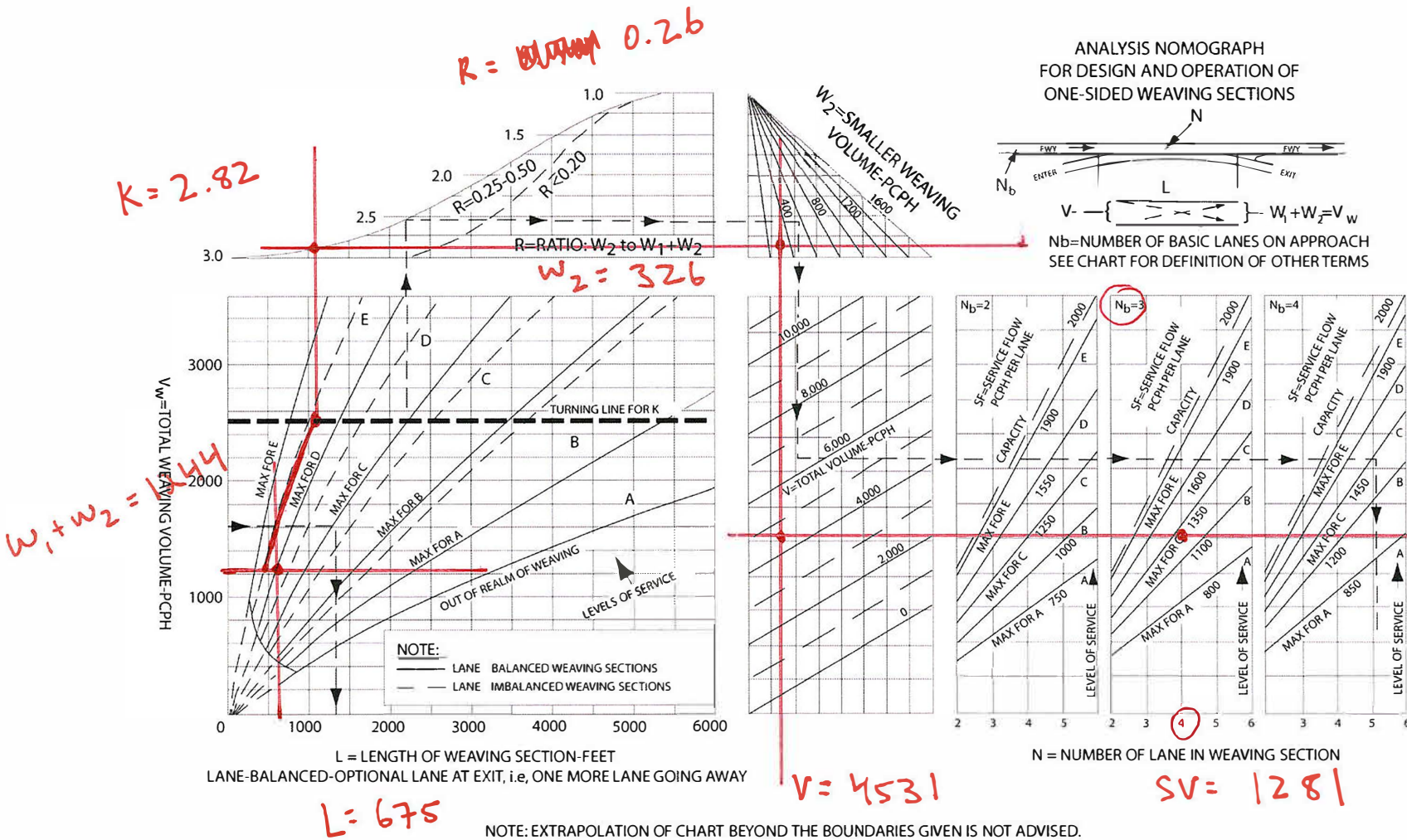
R = 0.33

W₂ = 949

LOS C

Design Curve for Freeway and Collector Weaving

Figure 504.7A



LOS E

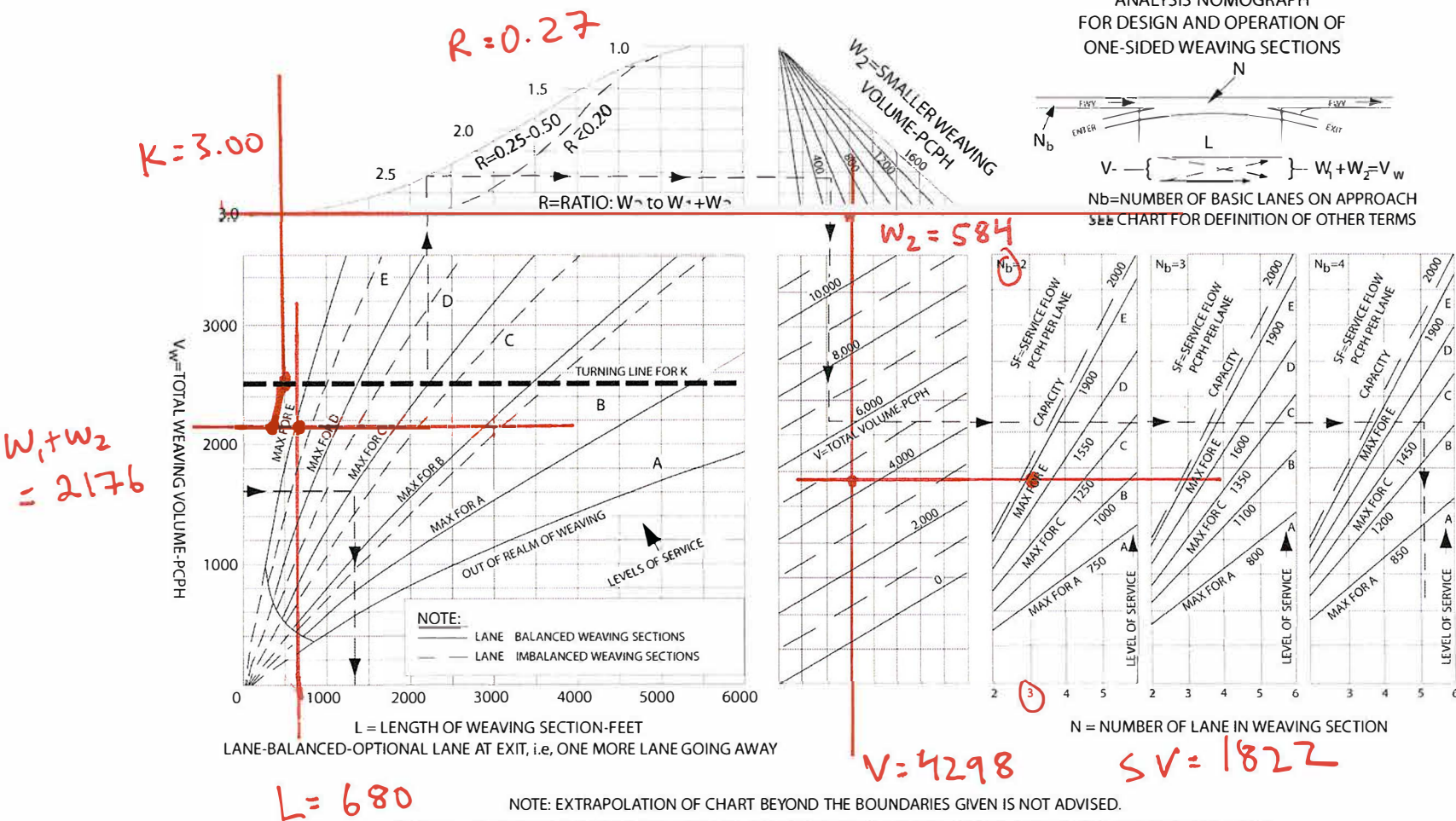
4

500-40
May 7, 2012

HIGHWAY DESIGN MANUAL

Design Curve for Freeway and Collector Weaving

Figure 504.7A



$W_1 + W_2 = 2176$

$R = 0.27$

$K = 3.00$

$W_2 = 584$

$V = 4298$

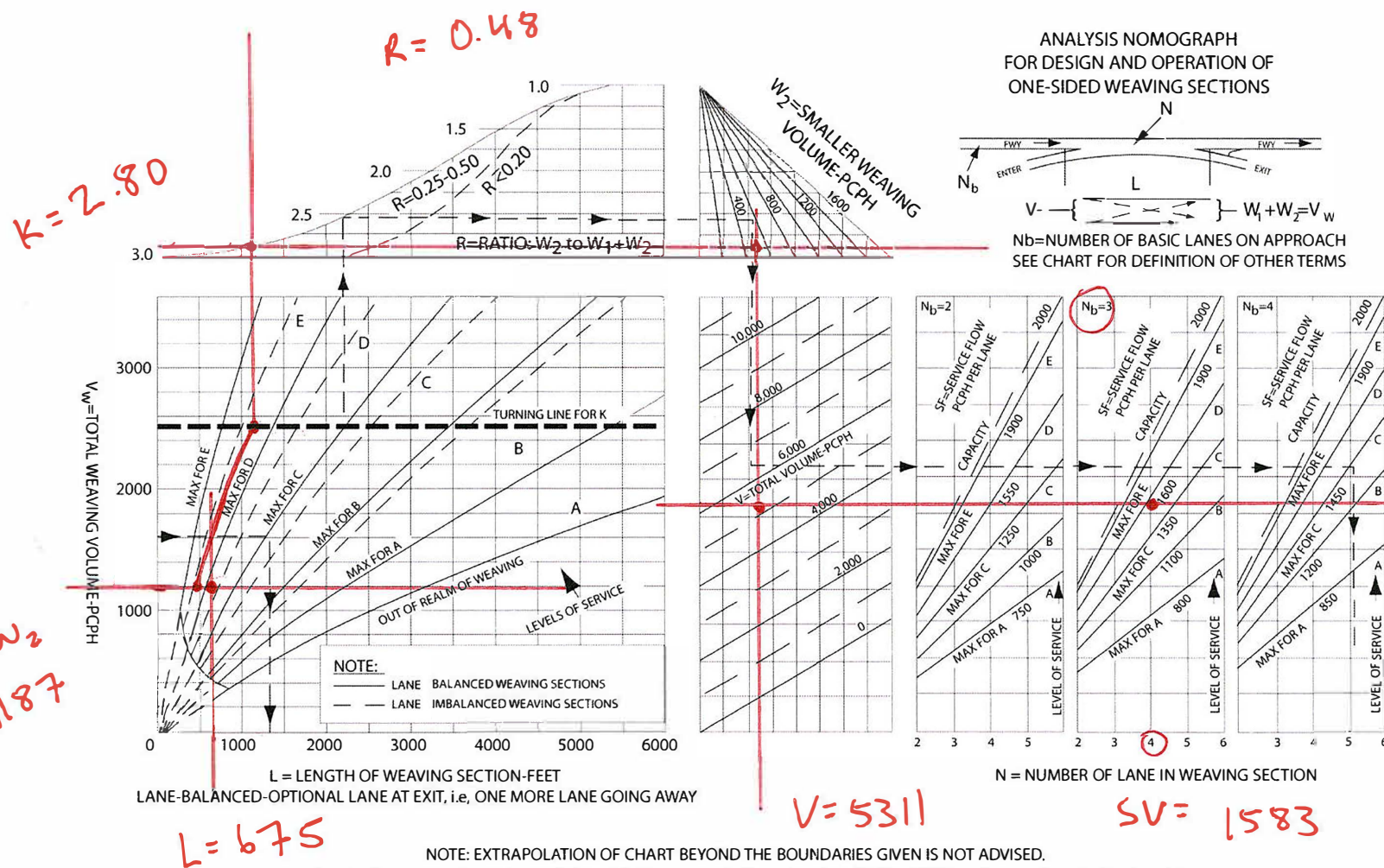
$SF = 1450$

$L = 680$

LOS D

Design Curve for Freeway and Collector Weaving

Figure 504.7A



$W_1+W_2 = 1187$

$L = 675$

$V = 5311$

$SV = 1583$

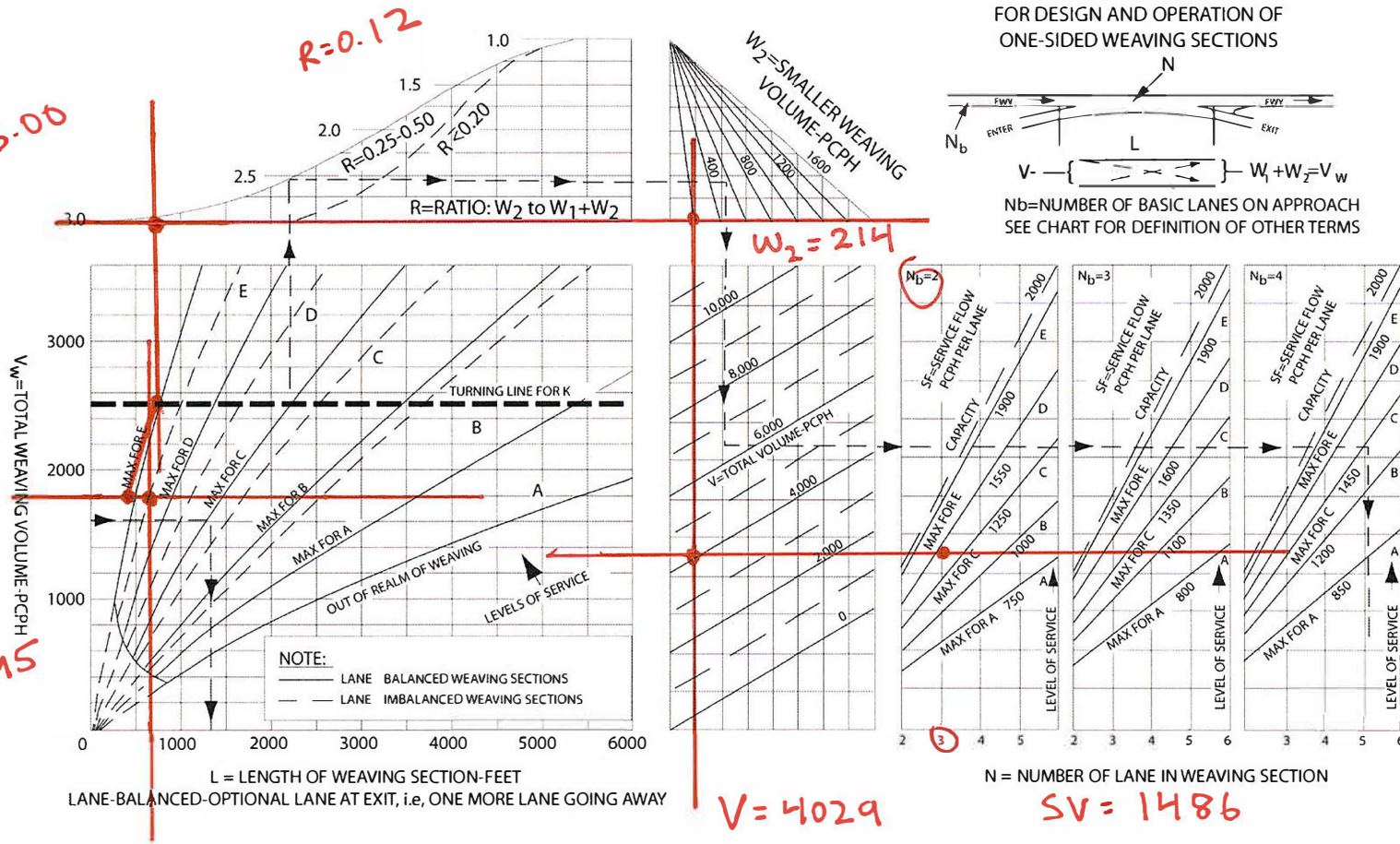
Design Curve for Freeway and Collector Weaving

Figure 504.7A

ANALYSIS NOMOGRAPH FOR DESIGN AND OPERATION OF ONE-SIDED WEAVING SECTIONS



Nb=NUMBER OF BASIC LANES ON APPROACH
SEE CHART FOR DEFINITION OF OTHER TERMS



NOTE: EXTRAPOLATION OF CHART BEYOND THE BOUNDARIES GIVEN IS NOT ADVISED.

Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, W_1+W_2 (or V_w) followed by projection to the right, intersecting the desired weaving LOS: a vertical drop from this point provides weaving distance $L = 1300$ ft. Returning to first intersection point of V_w with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K." from here the solution line is extended vertically to intersect the K values curve, from which a horizontal extension meets the desired W_2 volume. Then a downward turn to total volume, V , from which the line is horizontally projected to the right, intersection (in this case) the desired LOS = C curve having an SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields a N of 5.2: this would be rounded to $N = 5$ lanes.

K=3.00

R=0.12

W2=214

V=4029

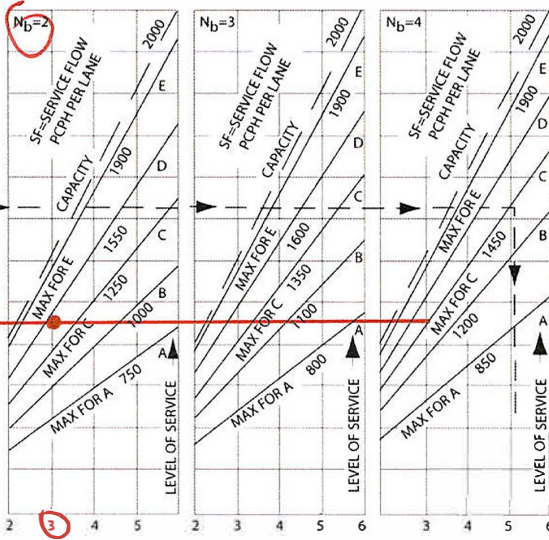
SV=1486

L=680

W1+W2=1795

NOTE:
— LANE BALANCED WEAVING SECTIONS
- - LANE IMBALANCED WEAVING SECTIONS

L = LENGTH OF WEAVING SECTION- FEET
LANE-BALANCED-OPTIONAL LANE AT EXIT, i.e., ONE MORE LANE GOING AWAY



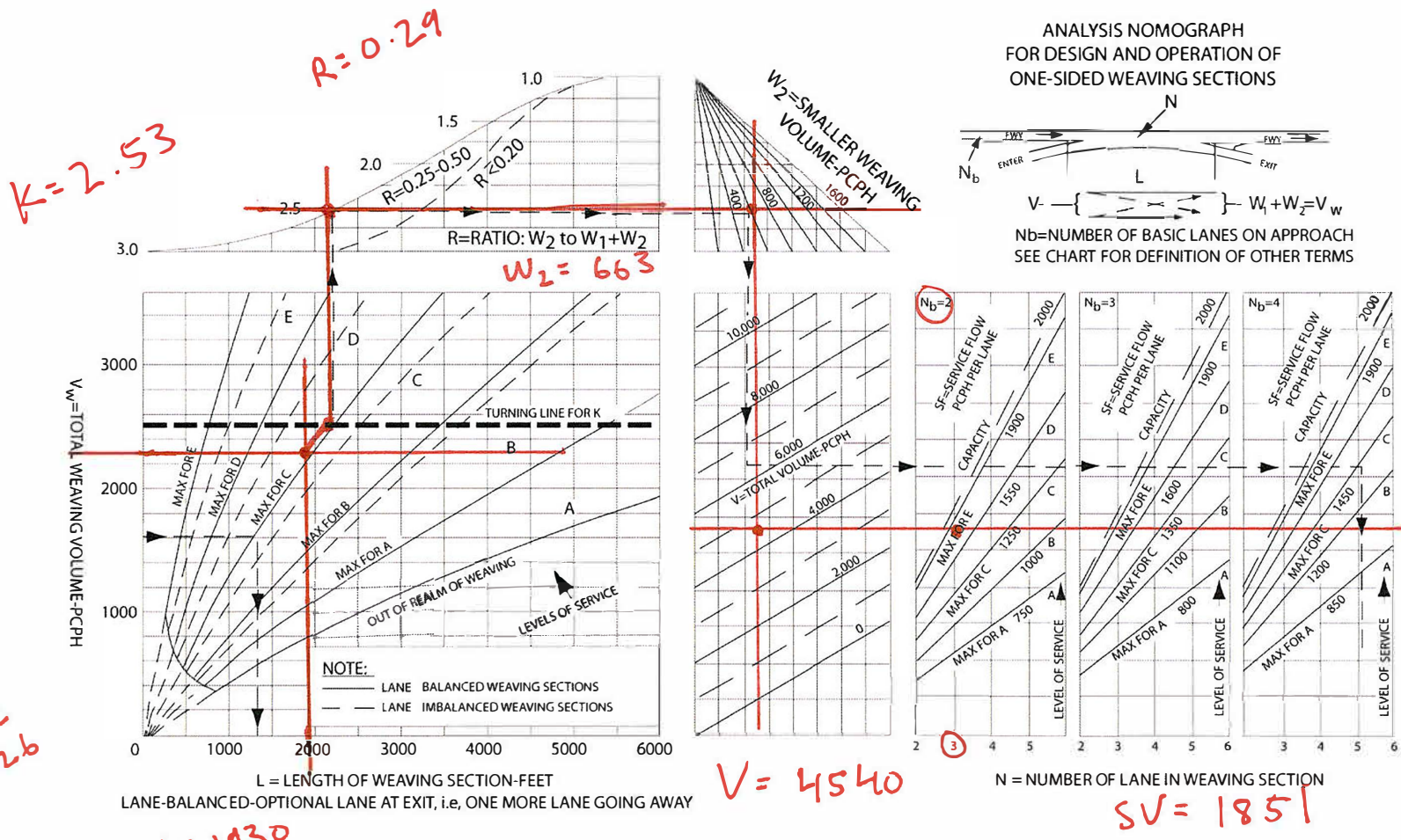
Design Curve for Freeway and Collector Weaving

Figure 504.7A

ANALYSIS NOMOGRAPH FOR DESIGN AND OPERATION OF ONE-SIDED WEAVING SECTIONS



$V = \{ \dots \} W_1 + W_2 = V_w$
 Nb = NUMBER OF BASIC LANES ON APPROACH
 SEE CHART FOR DEFINITION OF OTHER TERMS



NOTE: EXTRAPOLATION OF CHART BEYOND THE BOUNDARIES GIVEN IS NOT ADVISED.

Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, $W_1 + W_2$ (or V_w) followed by projection to the right, intersecting the desired weaving LOS: a vertical drop from this point provides weaving distance $L = 1300$ ft. Returning to first intersection point of V_w with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K." from here the solution line is extended vertically to intersect the K values curve, from which a horizontal extension meets the desired W_2 volume. Then a downward turn to total volume, V , from which the line is horizontally projected to the right, intersection (in this case) the desired LOS = C curve having a SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields a N of 5.2: this would be rounded to $N = 5$ lanes.

$W_1 + W_2 = 2326$

$R = 0.29$

$K = 2.53$

$W_2 = 663$

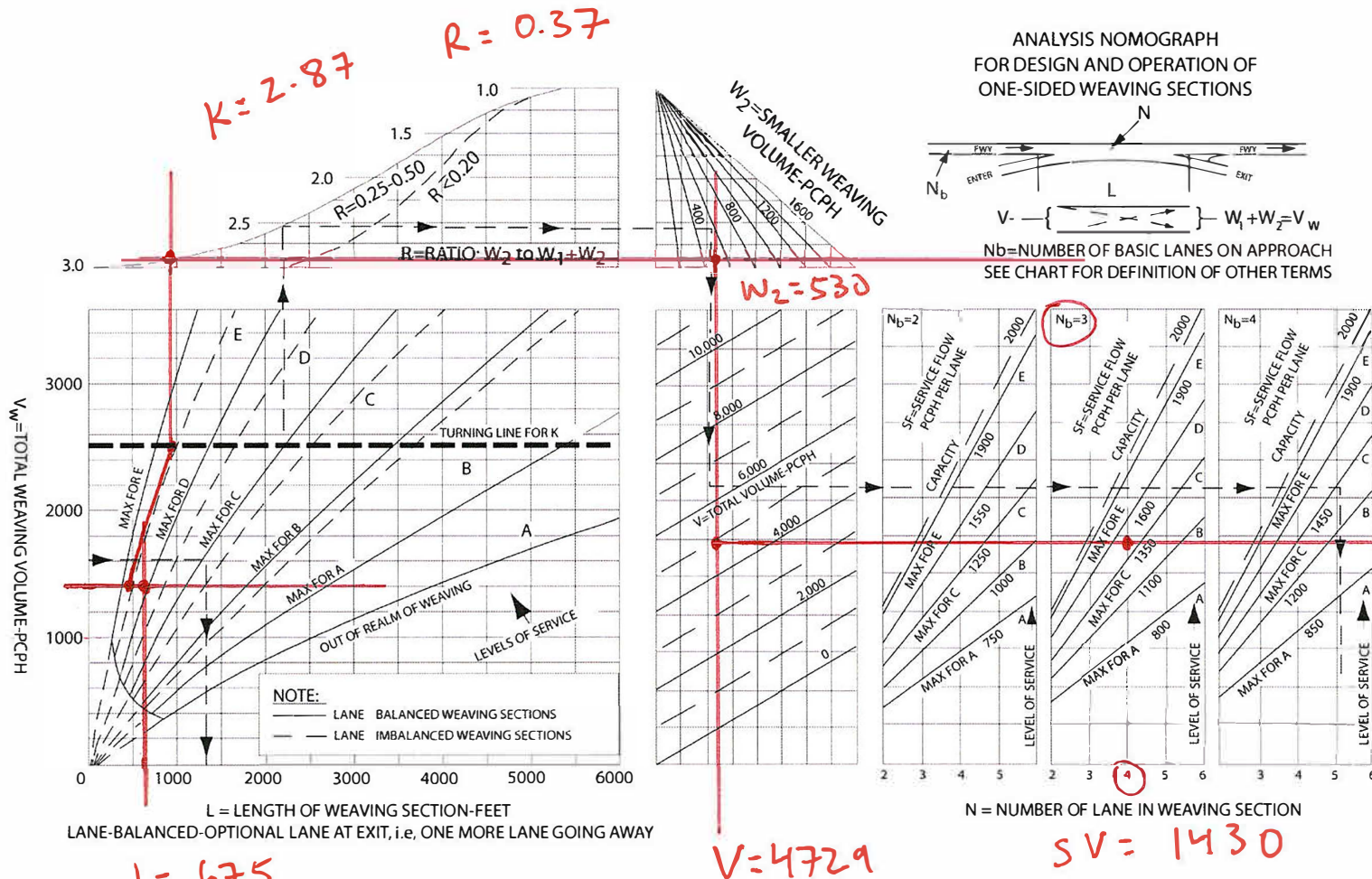
$L = 1930$

$V = 4540$

$SV = 1851$

Design Curve for Freeway and Collector Weaving

Figure 504.7A



$W_1 + W_2 = 1448$

$L = 675$

$V = 4729$

$SF = 1430$

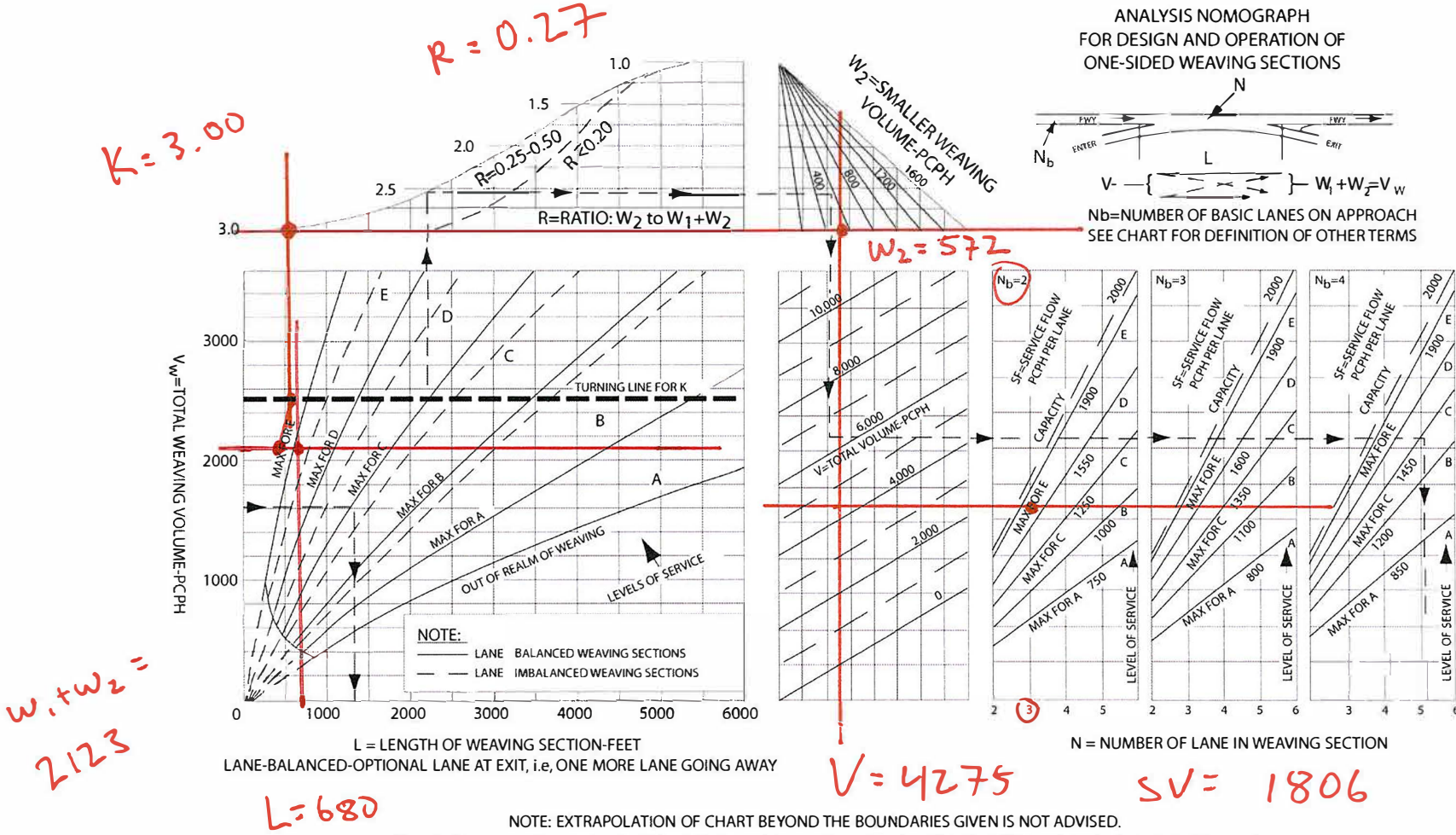
NOTE: EXTRAPOLATION OF CHART BEYOND THE BOUNDARIES GIVEN IS NOT ADVISED.

Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, $W_1 + W_2$ (or V_w) followed by projection to the right, intersecting the desired weaving LOS: a vertical drop from this point provides weaving distance $L = 1300$ ft. Returning to first intersection point of V_w with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K:" from here the solution line is extended vertically to intersect the K values curve, from which a horizontal extension meets the desired W_1 volume. Then a downward turn to total volume, V , from which the line is horizontally projected to the right, intersection (in this case) the desired LOS = C curve having an SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields a N of 5.2: this would be rounded to $N = 5$ lanes.

LOS E

Design Curve for Freeway and Collector Weaving

Figure 504.7A



NOTE: EXTRAPOLATION OF CHART BEYOND THE BOUNDARIES GIVEN IS NOT ADVISED.

Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, W_1+W_2 (or V_w) followed by projection to the right, intersecting the desired weaving LOS; a vertical drop from this point provides weaving distance $L = 1300$ ft. Returning to first intersection point of V_w with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K;" from here the solution line is extended vertically to intersect the K values curve, from which a horizontal extension meets the desired W_2 volume. Then a downward turn to total volume, V , from which the line is horizontally projected to the right, intersection (in this case) the desired LOS = C curve having an SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields a N of 5.2; this would be rounded to $N = 5$ lanes.

$W_1+W_2 = 2123$

$L = 680$

$V = 4275$

$SV = 1806$

LOS D

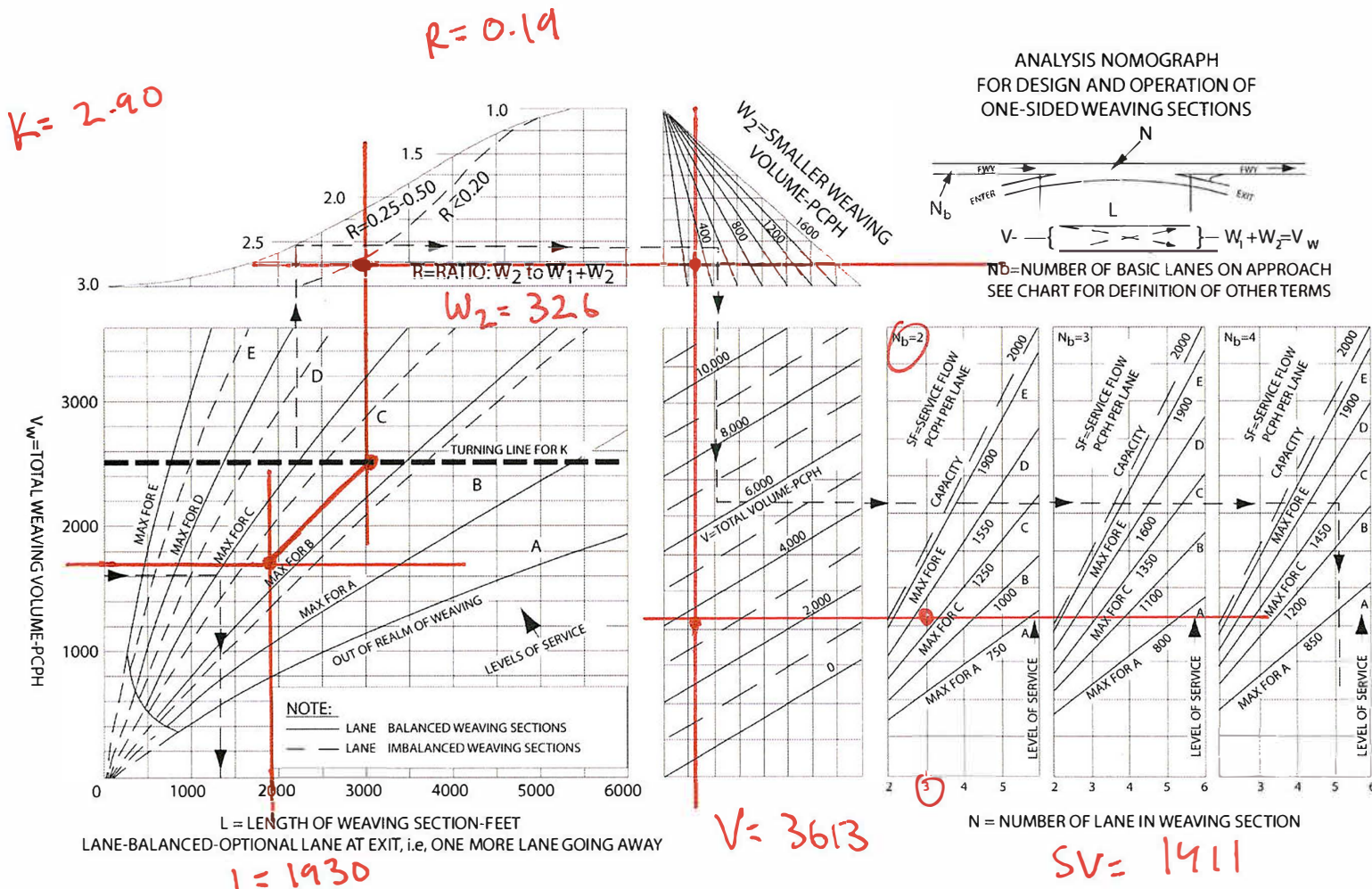
11

500-40
May 7, 2012

HIGHWAY DESIGN MANUAL

Design Curve for Freeway and Collector Weaving

Figure 504.7A

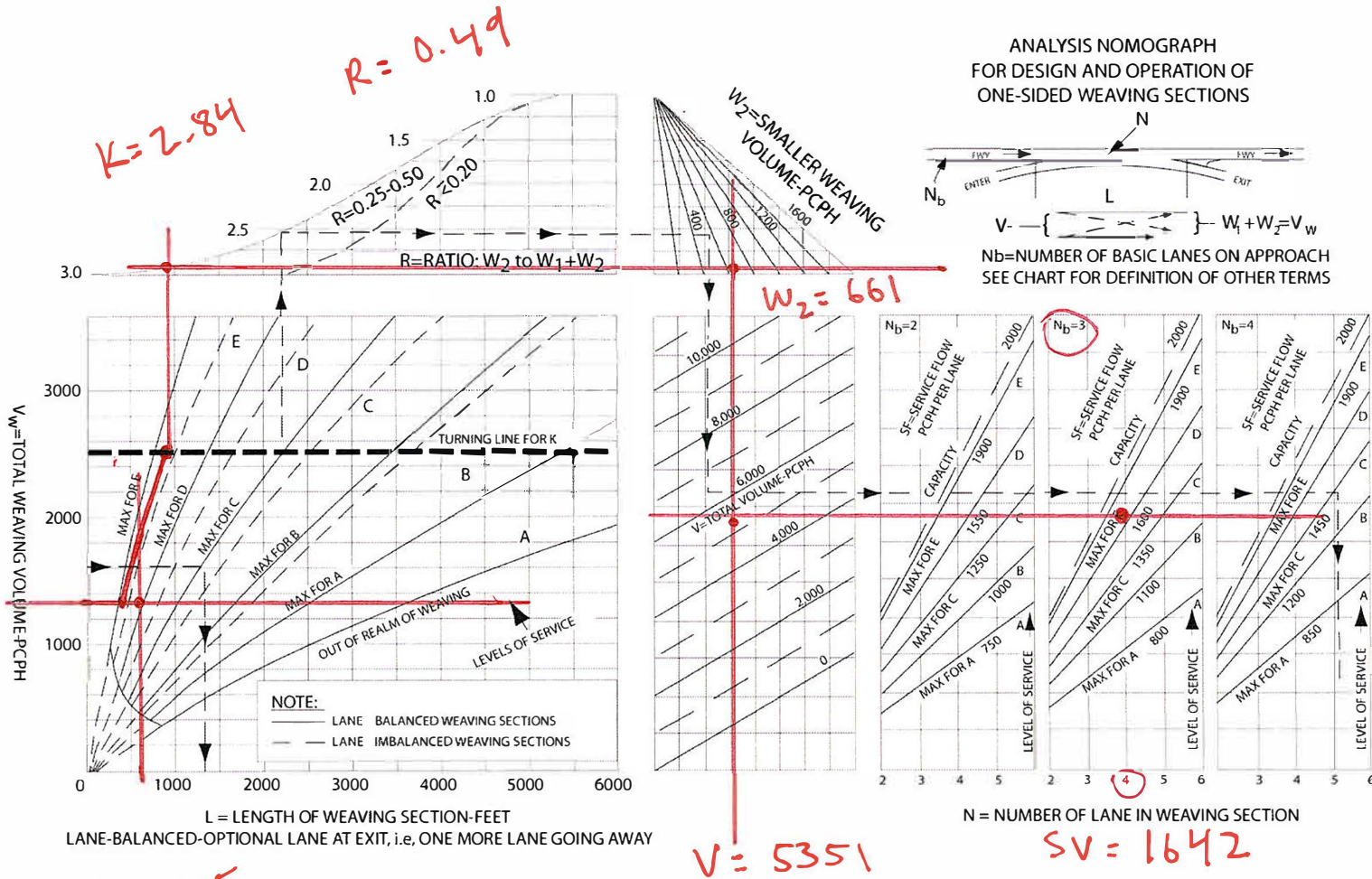


Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, W_1+W_2 (or V_w) followed by projection to the right, intersecting the desired weaving LOS; a vertical drop from this point provides weaving distance $L = 1300$ ft. Returning to first intersection point of V_w with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K;" from here the solution line is extended vertically to intersect the K values curve, from which a horizontal extension meets the desired W_2 volume. Then a downward turn to total volume, V , from which the line is horizontally projected to the right, intersection (in this case) the desired LOS = C curve having an SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields a N of 5.2; this would be rounded to $N = 5$ lanes.

$W_1 + W_2 = 1720$

Design Curve for Freeway and Collector Weaving

Figure 504.7A



$W_1 + W_2 = 1341$

$R = 0.49$

$K = 2.84$

$W_2 = 661$

$V = 5351$

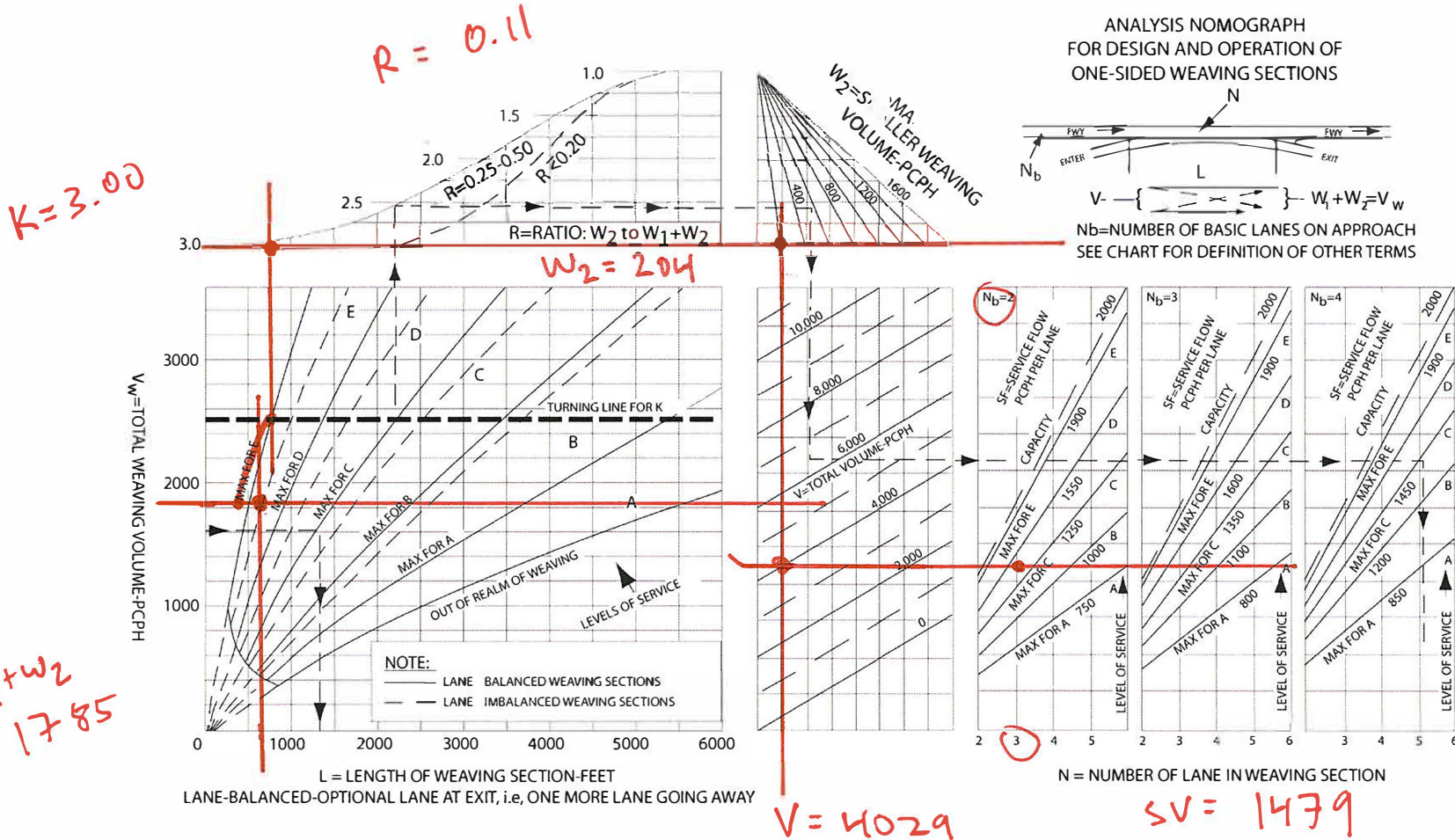
$S_v = 1642$

$L = 675$

LOS D

Design Curve for Freeway and Collector Weaving

Figure 504.7A



NOTE: EXTRAPOLATION OF CHART BEYOND THE BOUNDARIES GIVEN IS NOT ADVISED.

Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, $W_1 + W_2$ (or V_w) followed by projection to the right, intersecting the desired weaving LOS: a vertical drop from this point provides weaving distance $L = 1300$ ft. Returning to first intersection point of V_w with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K." from here the solution line is extended vertically to intersect the K values curve, from which a horizontal extension meets the desired W_2 volume. Then a downward turn to total volume, V , from which the line is horizontally projected to the right, intersection (in this case) the desired LOS = C curve having an SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields a N of 5.2: this would be rounded to N = 5 lanes.

$W_1 + W_2 = 5871$

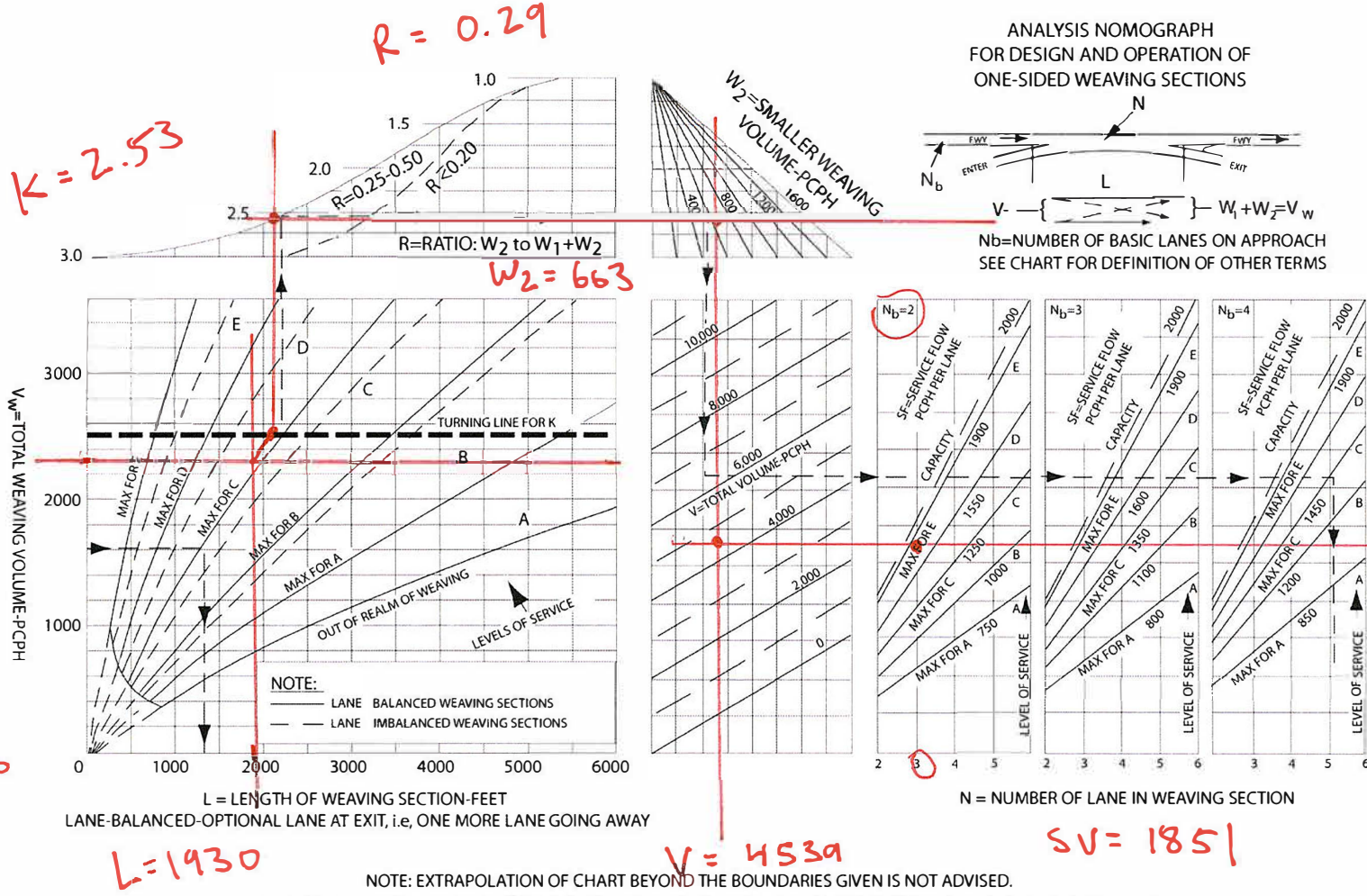
$L = 680$

LOS E

14

Design Curve for Freeway and Collector Weaving

Figure 504.7A



$W_1 + W_2 = 2326$

$L = 1930$

$V = 4539$

$SV = 1851$

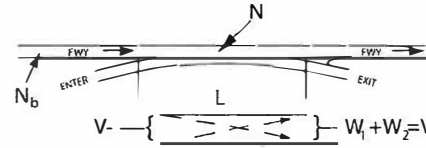
Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, $W_1 + W_2$ (or V_w) followed by projection to the right, intersecting the desired weaving LOS: a vertical drop from this point provides weaving distance $L = 1300$ ft. Returning to first intersection point of V_w with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K": from here the solution line is extended vertically to intersect the K values curve, from which a horizontal extension meets the desired W_2 volume. Then a downward turn to total volume, V , from which the line is horizontally projected to the right, intersection (in this case) the desired LOS = C curve having an SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields a N of 5.2: this would be rounded to N = 5 lanes.

LOSS

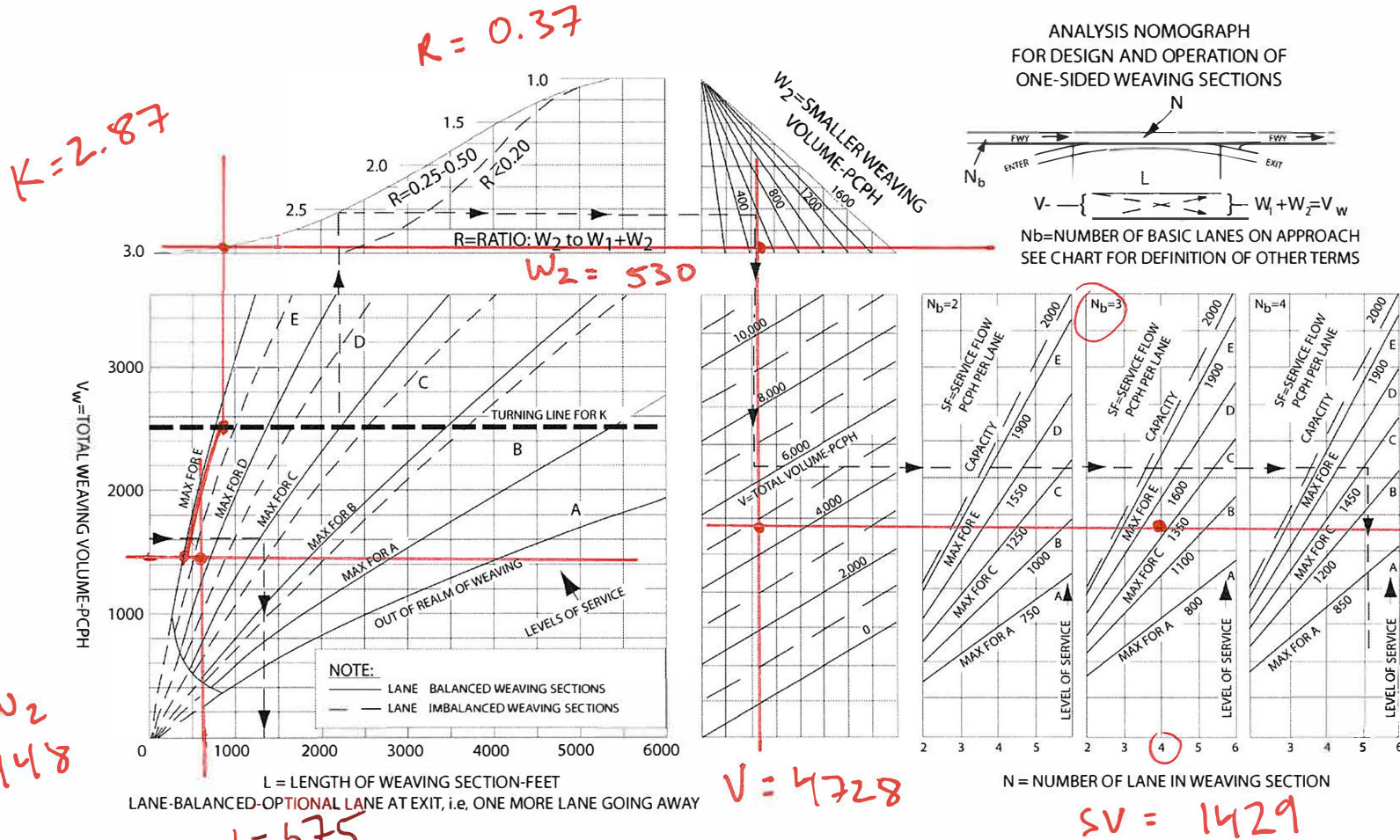
Design Curve for Freeway and Collector Weaving

Figure 504.7A

ANALYSIS NOMOGRAPH FOR DESIGN AND OPERATION OF ONE-SIDED WEAVING SECTIONS



Nb=NUMBER OF BASIC LANES ON APPROACH
SEE CHART FOR DEFINITION OF OTHER TERMS



$W_1 + W_2 = 1448$

$L = 675$

$V = 4728$

$SV = 1429$

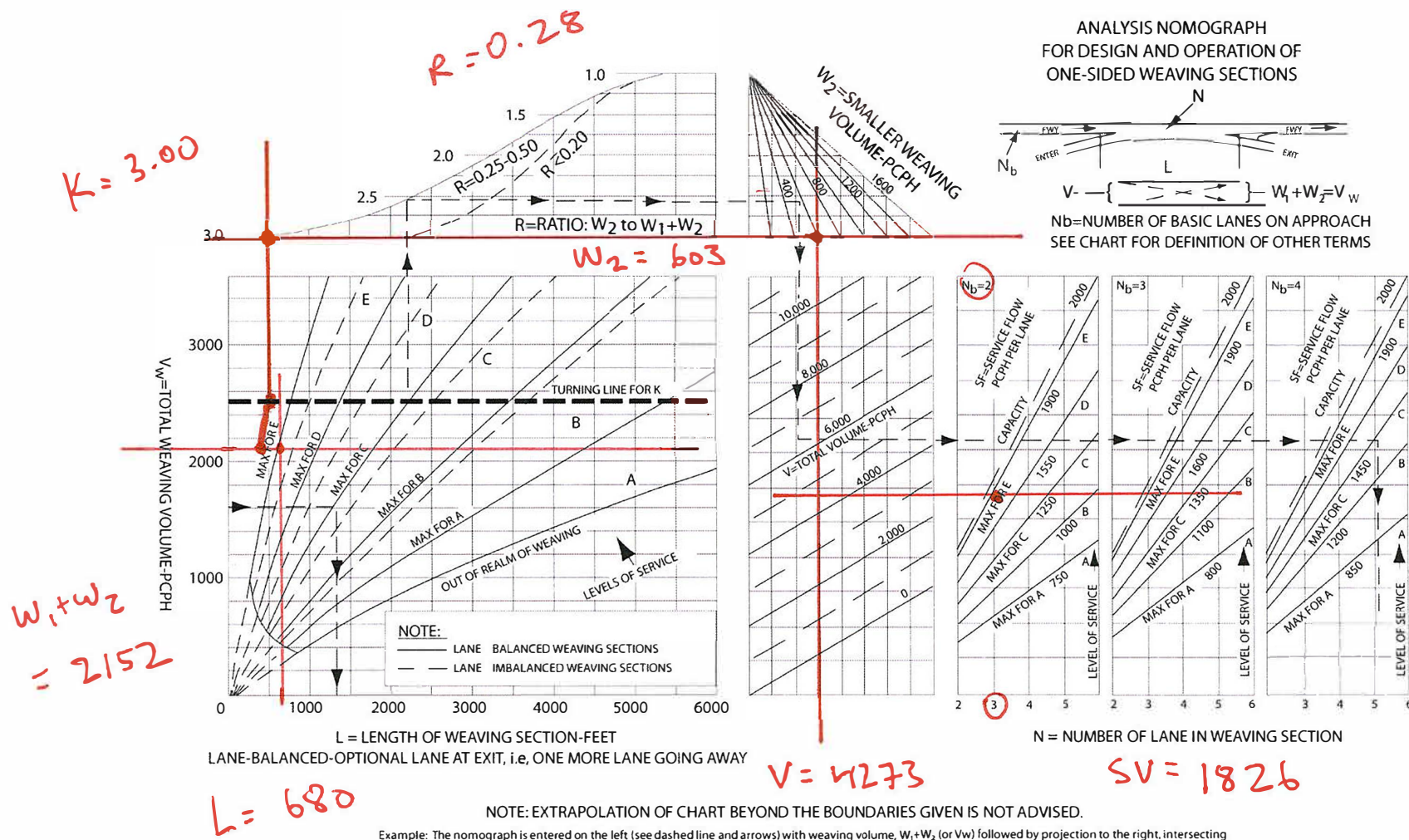
NOTE: EXTRAPOLATION OF CHART BEYOND THE BOUNDARIES GIVEN IS NOT ADVISED.

Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, $W_1 + W_2$ (or V_w) followed by projection to the right, intersecting the desired weaving LOS: a vertical drop from this point provides weaving distance $L = 1300$ ft. Returning to first intersection point of V_w with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K." from here the solution line is extended vertically to intersect the K values curve, from which a horizontal extension meets the desired W_2 volume. Then a downward turn to total volume, V , from which the line is horizontally projected to the right, intersection (in this case) the desired LOS = C curve having an SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields a N of 5.2: this would be rounded to $N = 5$ lanes.

LOSE

Design Curve for Freeway and Collector Weaving

Figure 504.7A



K = 3.00

R = 0.28

W₂ = 603

W₁+W₂ = 2152

L = 680

V = 4273

Sv = 1826

LOS D

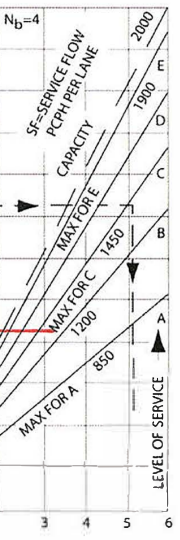
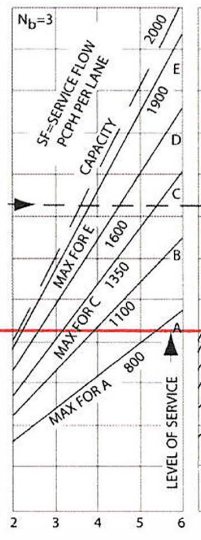
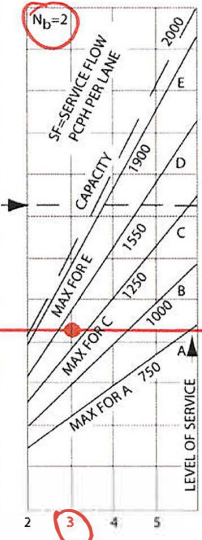
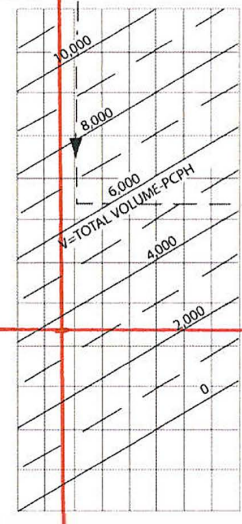
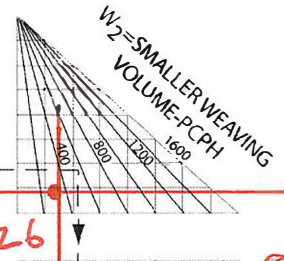
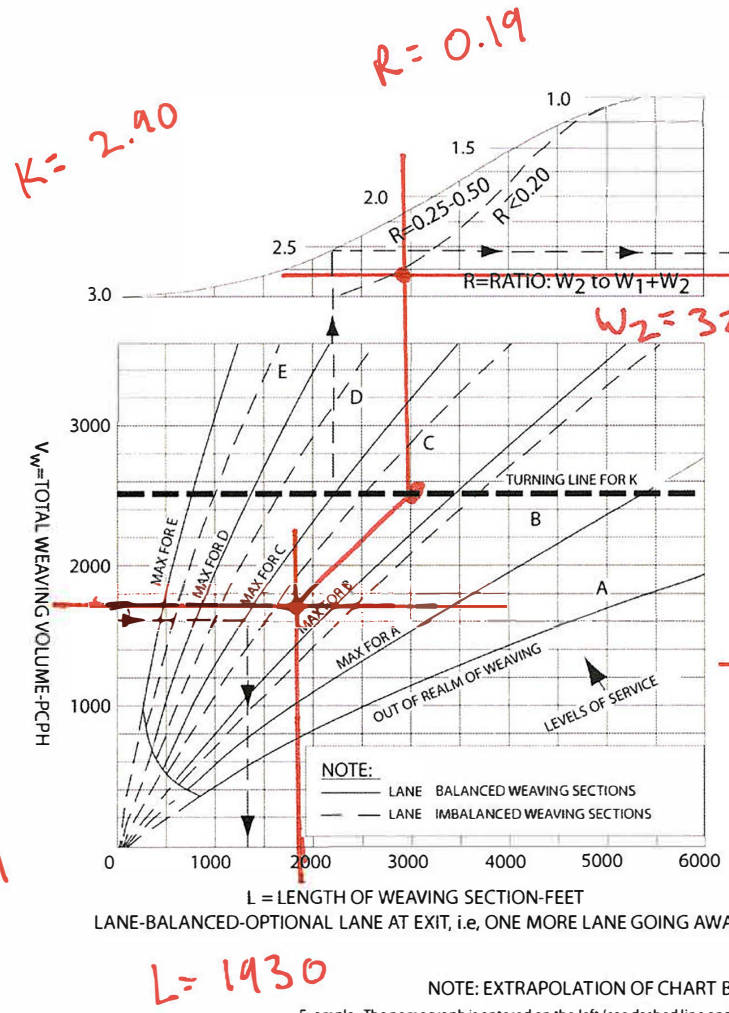
Design Curve for Freeway and Collector Weaving

Figure 504.7A

ANALYSIS NOMOGRAPH FOR DESIGN AND OPERATION OF ONE-SIDED WEAVING SECTIONS



N_b = NUMBER OF BASIC LANES ON APPROACH
SEE CHART FOR DEFINITION OF OTHER TERMS



N = NUMBER OF LANE IN WEAVING SECTION

SV = 1409

NOTE: EXTRAPOLATION OF CHART BEYOND THE BOUNDARIES GIVEN IS NOT ADVISED.

Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, W₁+W₂ (or V_w) followed by projection to the right, intersecting the desired weaving LOS; a vertical drop from this point provides weaving distance L = 1300 ft. Returning to first intersection point of V_w with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K" from here the solution line is extended vertically to intersect the K values curve, from which a horizontal extension meets the desired W₂ volume. Then a downward turn to total volume, V, from which the line is horizontally projected to the right, intersection (in this case) the desired LOS = C curve having an SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields a N of 5.2: this would be rounded to N = 5 lanes.

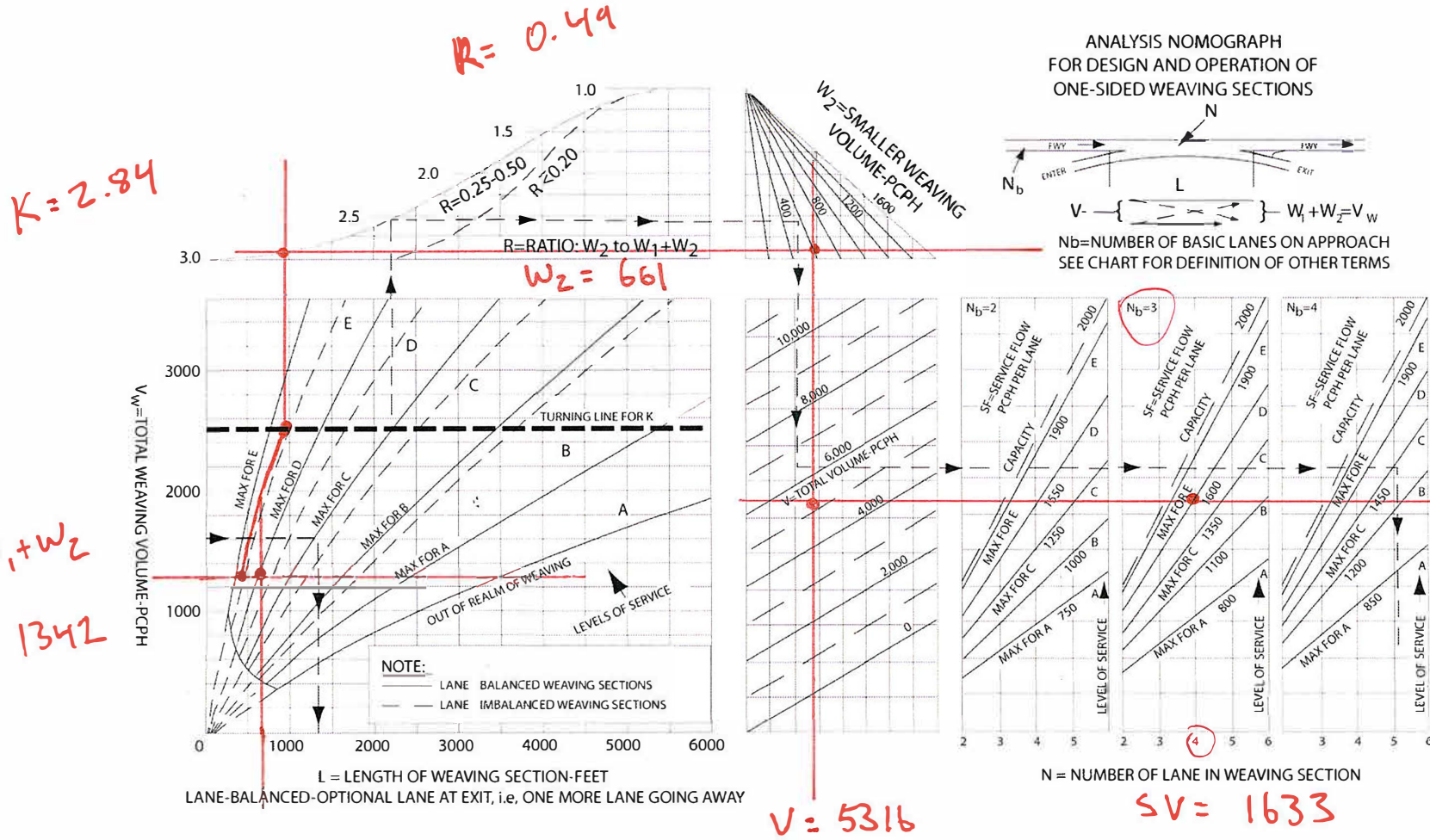
W₁+W₂ = 1721

L = 1930

LOSE

Design Curve for Freeway and Collector Weaving

Figure 504.7A



K = 2.84

R = 0.49

W₂ = 661

W₁ + W₂ = 1342

L = 675

V = 5316

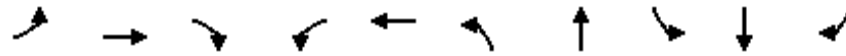
Sv = 1633

APPENDIX O – YEAR 2040 INTERSECTION CALCULATION SHEETS



Lanes, Volumes, Timings
1: Mathilda Ave & 5th Ave

3/4/2016

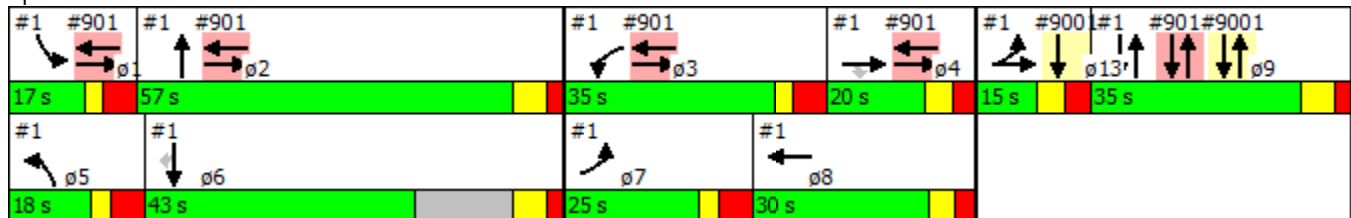


| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT | SBR | ø2 | ø7 |
|----------------------|------|------|--------|-------|-------|-------|-----|------|-----|--------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 30 | 30 | 90 | 60 | 30 | 200 | 840 | 40 | 520 | 110 | | |
| Turn Type | Prot | NA | custom | Prot | NA | Prot | NA | Prot | NA | custom | | |
| Protected Phases | 7 13 | 4 13 | | 3 | 8 | 5 | 2 9 | 1 | 6 9 | | 2 | 7 |
| Permitted Phases | | | 4 | | | | | | | 6 | | |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 5 | 2 | 1 | 6 | 6 | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 13.0 | 12.0 | 8.0 | 11.0 | | 10.0 | | 12.0 | 12.0 | 12.0 |
| Minimum Split (s) | | | 20.0 | 19.0 | 29.5 | 18.0 | | 17.0 | | 41.0 | 35.0 | 19.0 |
| Total Split (s) | | | 20.0 | 35.0 | 30.0 | 18.0 | | 17.0 | | 43.0 | 57.0 | 25.0 |
| Total Split (%) | | | 11.2% | 19.6% | 16.8% | 10.1% | | 9.5% | | 24.0% | 32% | 14% |
| Yellow Time (s) | | | 3.6 | 2.5 | 3.6 | 2.5 | | 2.5 | | 4.7 | 4.7 | 2.5 |
| All-Red Time (s) | | | 3.4 | 4.5 | 2.9 | 4.5 | | 4.5 | | 2.3 | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | | 0.0 | | |
| Total Lost Time (s) | | | 7.0 | 7.0 | 6.5 | 7.0 | | 7.0 | | 7.0 | | |
| Lead/Lag | | | Lag | Lead | Lag | Lead | | Lead | | Lag | Lag | Lead |
| Lead-Lag Optimize? | | | Yes | Yes | Yes | Yes | | Yes | | Yes | Yes | Yes |
| Recall Mode | | | None | None | None | None | | None | | Min | Min | None |

Intersection Summary

Cycle Length: 179
 Actuated Cycle Length: 105.1
 Natural Cycle: 160
 Control Type: Actuated-Uncoordinated

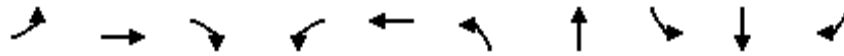
Splits and Phases: 1: Mathilda Ave & 5th Ave



| Lane Group | ø9 | ø13 |
|----------------------|------|------|
| Lane Configurations | | |
| Volume (vph) | | |
| Turn Type | | |
| Protected Phases | 9 | 13 |
| Permitted Phases | | |
| Detector Phase | | |
| Switch Phase | | |
| Minimum Initial (s) | 28.0 | 8.0 |
| Minimum Split (s) | 35.0 | 15.0 |
| Total Split (s) | 35.0 | 15.0 |
| Total Split (%) | 20% | 8% |
| Yellow Time (s) | 4.7 | 3.6 |
| All-Red Time (s) | 2.3 | 3.4 |
| Lost Time Adjust (s) | | |
| Total Lost Time (s) | | |
| Lead/Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes |
| Recall Mode | None | None |
| Intersection Summary | | |

Lanes, Volumes, Timings
2: Mathilda Ave & Innovation Way

3/4/2016

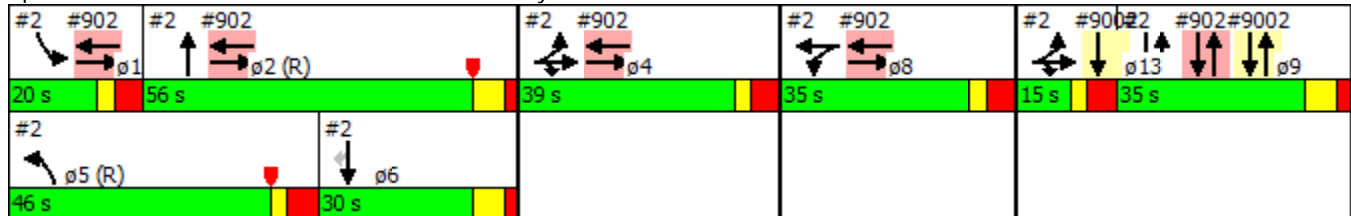


| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT | SBR | ø2 | ø4 |
|----------------------|-------|------|------|-------|-------|-------|------|-------|-----|--------|-------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 40 | 20 | 110 | 100 | 40 | 1070 | 1060 | 20 | 420 | 230 | | |
| Turn Type | Split | NA | Prot | Split | NA | Prot | NA | Prot | NA | custom | | |
| Protected Phases | 4 13 | 4 13 | 4 13 | 8 | 8 | 5 | 2 9 | 1 | 6 9 | | 2 | 4 |
| Permitted Phases | | | | | | | | | | | | 6 |
| Detector Phase | 4 | 4 | 4 | 8 | 8 | 5 | 2 | 1 | 6 | 6 | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | | 10.0 | 10.0 | 13.0 | | 10.0 | | 12.0 | 12.0 | 14.0 |
| Minimum Split (s) | | | | 35.0 | 35.0 | 20.0 | | 16.8 | | 30.0 | 19.0 | 39.0 |
| Total Split (s) | | | | 35.0 | 35.0 | 46.0 | | 20.0 | | 30.0 | 56.0 | 39.0 |
| Total Split (%) | | | | 17.5% | 17.5% | 23.0% | | 10.0% | | 15.0% | 28% | 20% |
| Yellow Time (s) | | | | 2.5 | 2.5 | 2.5 | | 2.5 | | 4.7 | 4.7 | 2.5 |
| All-Red Time (s) | | | | 4.5 | 4.5 | 4.5 | | 4.3 | | 2.3 | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | | 0.0 | 0.0 | 0.0 | | 0.0 | | 0.0 | | |
| Total Lost Time (s) | | | | 7.0 | 7.0 | 7.0 | | 6.8 | | 7.0 | | |
| Lead/Lag | | | | | | Lead | | Lead | | Lag | Lag | |
| Lead-Lag Optimize? | | | | | | Yes | | Yes | | Yes | Yes | |
| Recall Mode | | | | None | None | C-Max | | None | | Min | C-Min | None |

Intersection Summary

Cycle Length: 200
 Actuated Cycle Length: 200
 Offset: 39 (20%), Referenced to phase 2:NBT and 5:NBL, Start of Yellow
 Natural Cycle: 175
 Control Type: Actuated-Coordinated

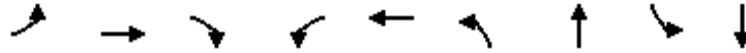
Splits and Phases: 2: Mathilda Ave & Innovation Way



| Lane Group | ø9 | ø13 |
|----------------------|------|------|
| Lane Configurations | | |
| Volume (vph) | | |
| Turn Type | | |
| Protected Phases | 9 | 13 |
| Permitted Phases | | |
| Detector Phase | | |
| Switch Phase | | |
| Minimum Initial (s) | 28.0 | 8.0 |
| Minimum Split (s) | 35.0 | 15.0 |
| Total Split (s) | 35.0 | 15.0 |
| Total Split (%) | 18% | 8% |
| Yellow Time (s) | 4.7 | 2.5 |
| All-Red Time (s) | 2.3 | 4.5 |
| Lost Time Adjust (s) | | |
| Total Lost Time (s) | | |
| Lead/Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes |
| Recall Mode | None | None |
| Intersection Summary | | |

Lanes, Volumes, Timings
 3: Mathilda Ave & Moffett Park Dr

3/4/2016

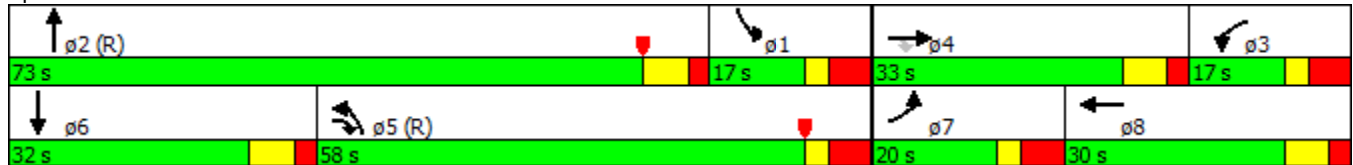


| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↶ | ↷ | ↷ | ↶↷ | ↷ | ↶↷ | ↑↑↷ | ↷ | ↑↑↑ |
| Volume (vph) | 50 | 70 | 90 | 120 | 280 | 920 | 2380 | 30 | 420 |
| Turn Type | Prot | NA | pm+ov | Prot | NA | Prot | NA | Prot | NA |
| Protected Phases | 7 | 4 | 5 | 3 | 8 | 5 | 2 | 1 | 6 |
| Permitted Phases | | | 4 | | | | | | |
| Detector Phase | 7 | 4 | 5 | 3 | 8 | 5 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | | |
| Minimum Initial (s) | 8.0 | 8.0 | 4.0 | 8.0 | 8.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | 15.0 | 15.0 | 11.0 | 15.0 | 30.0 | 11.0 | 32.9 | 11.0 | 10.9 |
| Total Split (s) | 20.0 | 33.0 | 58.0 | 17.0 | 30.0 | 58.0 | 73.0 | 17.0 | 32.0 |
| Total Split (%) | 14.3% | 23.6% | 41.4% | 12.1% | 21.4% | 41.4% | 52.1% | 12.1% | 22.9% |
| Yellow Time (s) | 2.5 | 4.7 | 2.5 | 2.5 | 4.5 | 2.5 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 4.5 | 2.3 | 4.5 | 4.5 | 2.5 | 4.5 | 2.2 | 4.5 | 2.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.9 | 7.0 | 6.9 |
| Lead/Lag | Lead | Lead | Lag | Lag | Lag | Lag | Lead | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | C-Max | None | None | C-Max | C-Max | None | None |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 120 (86%), Referenced to phase 2:NBT and 5:NBL, Start of Yellow
 Natural Cycle: 150
 Control Type: Actuated-Coordinated

Splits and Phases: 3: Mathilda Ave & Moffett Park Dr



Lanes, Volumes, Timings

4: Mathilda Ave & SR 237 Off/On Ramp/SR 237 EB On-Ramp

3/4/2016

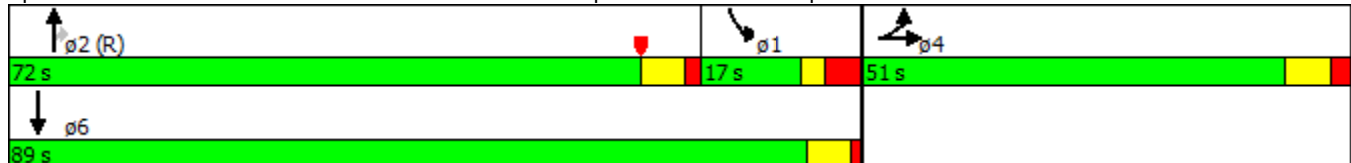


| Lane Group | EBL | EBT | NBT | NBR | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | |
| Volume (vph) | 1110 | 0 | 2610 | 920 | 80 | 1030 |
| Turn Type | Split | NA | NA | Perm | Prot | NA |
| Protected Phases | 4 | 4 | 2 | | 1 | 6 |
| Permitted Phases | | | | 2 | | |
| Detector Phase | 4 | 4 | 2 | 2 | 1 | 6 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | 12.0 | 12.0 | 20.2 | 20.2 | 10.4 | 9.9 |
| Total Split (s) | 51.0 | 51.0 | 72.0 | 72.0 | 17.0 | 89.0 |
| Total Split (%) | 36.4% | 36.4% | 51.4% | 51.4% | 12.1% | 63.6% |
| Yellow Time (s) | 4.8 | 4.8 | 4.7 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 2.2 | 2.2 | 1.5 | 1.5 | 3.9 | 1.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 6.2 | 6.2 | 6.4 | 5.9 |
| Lead/Lag | | | Lead | Lead | Lag | |
| Lead-Lag Optimize? | | | Yes | Yes | Yes | |
| Recall Mode | None | None | C-Max | C-Max | None | None |

Intersection Summary

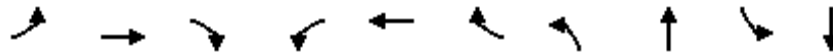
Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 134 (96%), Referenced to phase 2:NBT, Start of Yellow
 Natural Cycle: 70
 Control Type: Actuated-Coordinated

Splits and Phases: 4: Mathilda Ave & SR 237 Off/On Ramp/SR 237 EB On-Ramp



Lanes, Volumes, Timings
5: Mathilda Ave & Ross Dr

3/4/2016



| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↖ | ↑ | ↗ | ↖ | ↑ | ↗ | ↖ | ↑↑↑↑ | ↖ | ↑↑↑ |
| Volume (vph) | 90 | 70 | 40 | 130 | 40 | 300 | 70 | 3140 | 70 | 980 |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | Prot | NA | Prot | NA |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | 1 | 6 |
| Permitted Phases | 4 | | 4 | 8 | | 8 | | | | |
| Detector Phase | 4 | 4 | 4 | 8 | 8 | 8 | 5 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 4.0 | 5.0 | 4.0 | 5.0 |
| Minimum Split (s) | 41.0 | 41.0 | 41.0 | 13.0 | 13.0 | 13.0 | 11.0 | 31.4 | 11.0 | 11.6 |
| Total Split (s) | 43.0 | 43.0 | 43.0 | 43.0 | 43.0 | 43.0 | 20.0 | 80.0 | 17.0 | 77.0 |
| Total Split (%) | 30.7% | 30.7% | 30.7% | 30.7% | 30.7% | 30.7% | 14.3% | 57.1% | 12.1% | 55.0% |
| Yellow Time (s) | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 2.5 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 3.4 | 3.4 | 3.4 | 3.4 | 3.4 | 3.4 | 4.5 | 1.7 | 4.5 | 1.9 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.4 | 7.0 | 6.6 |
| Lead/Lag | | | | | | | Lead | Lead | Lag | Lag |
| Lead-Lag Optimize? | | | | | | | Yes | Yes | Yes | Yes |
| Recall Mode | Max | Max | Max | None | None | None | None | C-Max | Max | None |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 0 (0%), Referenced to phase 2:NBT, Start of Yellow, Master Intersection
 Natural Cycle: 105
 Control Type: Actuated-Coordinated

Splits and Phases: 5: Mathilda Ave & Ross Dr



Lanes, Volumes, Timings
 8: Mathilda Ave & Almanor Ave/Ahwanee Ave

3/4/2016

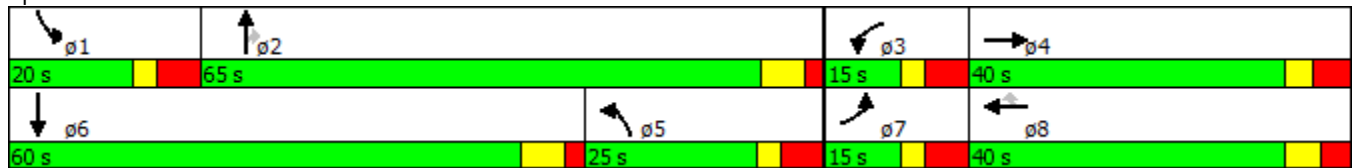


| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | | |
| Volume (vph) | 130 | 30 | 90 | 50 | 260 | 140 | 3430 | 70 | 160 | 1760 |
| Turn Type | Prot | NA | Prot | NA | Perm | Prot | NA | Perm | Prot | NA |
| Protected Phases | 7 | 4 | 3 | 8 | | 5 | 2 | | 1 | 6 |
| Permitted Phases | | | | | 8 | | | 2 | | |
| Detector Phase | 7 | 4 | 3 | 8 | 8 | 5 | 2 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 12.0 | 12.0 | 8.0 | 12.0 |
| Minimum Split (s) | 15.0 | 40.0 | 15.0 | 15.0 | 15.0 | 15.0 | 33.7 | 33.7 | 15.0 | 18.7 |
| Total Split (s) | 15.0 | 40.0 | 15.0 | 40.0 | 40.0 | 25.0 | 65.0 | 65.0 | 20.0 | 60.0 |
| Total Split (%) | 10.7% | 28.6% | 10.7% | 28.6% | 28.6% | 17.9% | 46.4% | 46.4% | 14.3% | 42.9% |
| Yellow Time (s) | 2.5 | 2.8 | 2.5 | 3.6 | 3.6 | 2.5 | 4.7 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 4.5 | 4.2 | 4.5 | 3.4 | 3.4 | 4.5 | 2.0 | 2.0 | 4.5 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.7 | 6.7 | 7.0 | 6.7 |
| Lead/Lag | Lead | Lag | Lead | Lag | Lag | Lag | Lag | Lag | Lead | Lead |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | None | Min | Min | None | Min |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 119.3
 Natural Cycle: 145
 Control Type: Actuated-Uncoordinated

Splits and Phases: 8: Mathilda Ave & Almanor Ave/Ahwanee Ave



Lanes, Volumes, Timings
 9: US 101 On-Ramp & Moffett Park Dr

3/4/2016

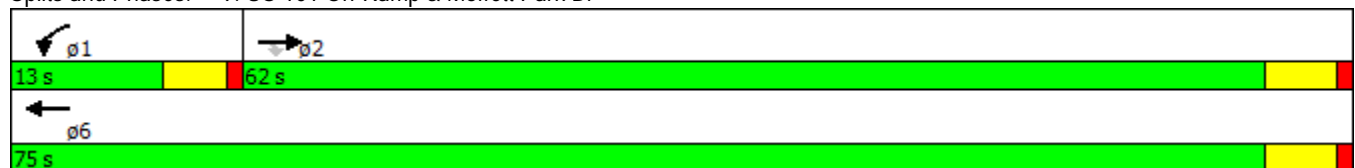


| Lane Group | EBT | EBR | WBL | WBT |
|----------------------|-------|-------|-------|--------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ |
| Volume (vph) | 230 | 20 | 40 | 1010 |
| Turn Type | NA | Perm | Prot | NA |
| Protected Phases | 2 | | 1 | 6 |
| Permitted Phases | | 2 | | |
| Detector Phase | 2 | 2 | 1 | 6 |
| Switch Phase | | | | |
| Minimum Initial (s) | 15.0 | 15.0 | 6.0 | 15.0 |
| Minimum Split (s) | 20.0 | 20.0 | 10.5 | 20.0 |
| Total Split (s) | 62.0 | 62.0 | 13.0 | 75.0 |
| Total Split (%) | 82.7% | 82.7% | 17.3% | 100.0% |
| Yellow Time (s) | 4.0 | 4.0 | 3.5 | 4.0 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.0 | 5.0 | 4.5 | 5.0 |
| Lead/Lag | Lag | Lag | Lead | |
| Lead-Lag Optimize? | | | | |
| Recall Mode | Min | Min | None | Min |

Intersection Summary

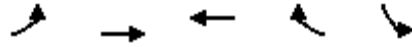
Cycle Length: 75
 Actuated Cycle Length: 42.4
 Natural Cycle: 40
 Control Type: Semi Act-Uncoord

Splits and Phases: 9: US 101 On-Ramp & Moffett Park Dr



Lanes, Volumes, Timings
 10: Moffett Park Dr & Innovation Way

3/4/2016

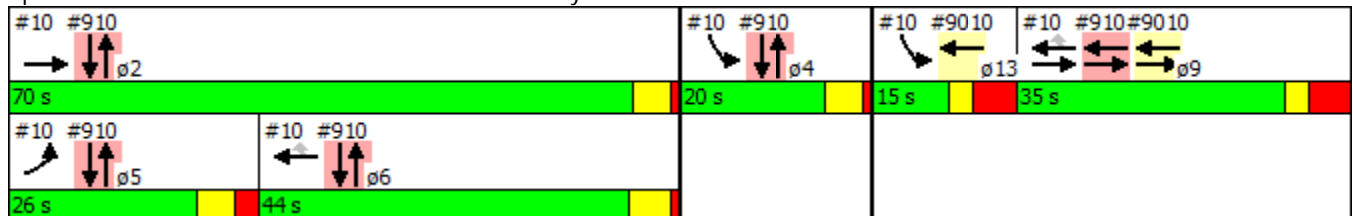


| Lane Group | EBL | EBT | WBT | WBR | SBL | ø2 | ø4 | ø6 | ø9 | ø13 |
|----------------------|-------|-----|-----|------|------|------|------|------|------|------|
| Lane Configurations | ↖ | ↑↑ | ↑↑ | ↗ | ↘↘ | | | | | |
| Volume (vph) | 70 | 160 | 920 | 460 | 70 | | | | | |
| Turn Type | Prot | NA | NA | Perm | Prot | | | | | |
| Protected Phases | 5 | 2 9 | 6 9 | | 4 13 | 2 | 4 | 6 | 9 | 13 |
| Permitted Phases | | | | 6 9 | | | | | | |
| Detector Phase | 5 | 2 | 6 | 6 9 | 4 | | | | | |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 8.0 | | | | | 10.0 | 10.0 | 10.0 | 28.0 | 8.0 |
| Minimum Split (s) | 14.5 | | | | | 14.9 | 15.0 | 15.5 | 35.0 | 15.0 |
| Total Split (s) | 26.0 | | | | | 70.0 | 20.0 | 44.0 | 35.0 | 15.0 |
| Total Split (%) | 18.6% | | | | | 50% | 14% | 31% | 25% | 11% |
| Yellow Time (s) | 4.0 | | | | | 3.9 | 4.0 | 4.5 | 2.5 | 2.5 |
| All-Red Time (s) | 2.5 | | | | | 1.0 | 1.0 | 1.0 | 4.5 | 4.5 |
| Lost Time Adjust (s) | 0.0 | | | | | | | | | |
| Total Lost Time (s) | 6.5 | | | | | | | | | |
| Lead/Lag | Lead | | | | | | | Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | | | | | | | Yes | Yes | Yes |
| Recall Mode | None | | | | | Min | None | Min | None | None |

Intersection Summary



















Cycle Length: 140
 Actuated Cycle Length: 97.6
 Natural Cycle: 95
 Control Type: Actuated-Uncoordinated

Splits and Phases: 10: Moffett Park Dr & Innovation Way



Lanes, Volumes, Timings
 11: Innovation Way & 11th Ave

3/4/2016

| |  |  |  |  |  |  |  |  |
|---------------------|---|---|---|---|---|---|---|---|
| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBT |
| Lane Configurations |  |  |  |  |  |  |   |   |
| Volume (vph) | 50 | 0 | 80 | 20 | 0 | 220 | 30 | 100 |
| Sign Control | | Stop | | | Stop | | Stop | Stop |

Intersection Summary

Control Type: Unsignalized

Lanes, Volumes, Timings
 12: Innovation Way & Juniper Driveway

3/4/2016















| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
|---------------------|------|-----|-----|------|------|-----|
| Lane Configurations | | | | | | |
| Volume (vph) | 100 | 60 | 30 | 70 | 500 | 840 |
| Sign Control | Stop | | | Stop | Stop | |

Intersection Summary

Control Type: Unsignalized

Lanes, Volumes, Timings
 13: Bordeaux Dr & Innovation Way/Driveway

3/4/2016

| |  |  |  |  |  |  |
|---------------------|---|---|---|---|---|---|
| Lane Group | EBT | EBR | WBT | NBL | NBT | SBT |
| Lane Configurations |  |  |  |  |  |  |
| Volume (vph) | 50 | 120 | 20 | 50 | 130 | 60 |
| Sign Control | Stop | | Stop | | Stop | Stop |

Intersection Summary

Control Type: Unsignalized

Lanes, Volumes, Timings

33: Mathilda Ave & SR 237 WB On-Ramp/SR 237 WB Off-Ramp

3/4/2016

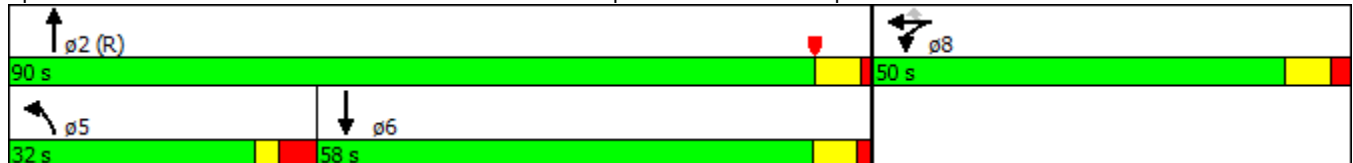


| Lane Group | WBL | WBT | WBR | NBL | NBT | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↶ | ↷ | ↷ | ↶ | ↑↑↑ | ↑↑↑ |
| Volume (vph) | 670 | 0 | 620 | 180 | 3540 | 440 |
| Turn Type | Split | NA | Perm | Prot | NA | NA |
| Protected Phases | 8 | 8 | | 5 | 2 | 6 |
| Permitted Phases | | | 8 | | | |
| Detector Phase | 8 | 8 | 8 | 5 | 2 | 6 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | 11.0 | 11.0 | 11.0 | 10.3 | 20.0 | 10.3 |
| Total Split (s) | 50.0 | 50.0 | 50.0 | 32.0 | 90.0 | 58.0 |
| Total Split (%) | 35.7% | 35.7% | 35.7% | 22.9% | 64.3% | 41.4% |
| Yellow Time (s) | 4.8 | 4.8 | 4.8 | 2.5 | 4.7 | 4.7 |
| All-Red Time (s) | 2.2 | 2.2 | 2.2 | 3.8 | 1.3 | 1.6 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 6.3 | 6.0 | 6.3 |
| Lead/Lag | | | | Lead | | Lag |
| Lead-Lag Optimize? | | | | Yes | | Yes |
| Recall Mode | Max | Max | Max | None | C-Max | None |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 120 (86%), Referenced to phase 2:NBT, Start of Yellow
 Natural Cycle: 100
 Control Type: Actuated-Coordinated

Splits and Phases: 33: Mathilda Ave & SR 237 WB On-Ramp/SR 237 WB Off-Ramp



**SimTraffic Post-Processor
Average Results from 10 Runs
Network Performance**

**Mathilda Avenue Improvements
2040 No Build
AM Peak Hour**

| Performance Measure | Average | Std. Dev. | Minimum | Maximum |
|---------------------------------|---------|-----------|---------|---------|
| Average Delay (seconds) | 866.0 | 22.1 | 825.0 | 904.7 |
| Total Delay (hours) | 2,989 | 57 | 2,916 | 3,120 |
| Average Stopped Delay (seconds) | 813.6 | 23.0 | 771.4 | 845.3 |
| Total Stopped Delay (hours) | 2808 | 60 | 2734 | 2931 |
| Total Stops | 35,663 | 2,093 | 31,843 | 38,176 |
| Average Stops | 2.87 | 0.10 | 2.69 | 2.99 |
| Total Distance Traveled (miles) | 33,391 | 1,015 | 31,144 | 34,703 |
| Average Speed (mph) | 8.9 | 0.3 | 8.0 | 9.0 |
| Total Travel Time (hours) | 4,284.4 | 96.8 | 4,121.2 | 4,434.4 |
| Vehicles Entered | 9,942 | 269 | 9,381 | 10,261 |
| Vehicles Exited | 7,948 | 355 | 7,292 | 8,377 |
| Percent Demand Served | 79.9% | 2.0% | 77.4% | 82.7% |
| Fuel Used (gallons) | 1,574 | 25 | 1,542 | 1,610 |
| HC Emissions (grams) | 13,652 | 721 | 12,564 | 14,607 |
| CO Emissions (grams) | 406,064 | 13,253 | 388,754 | 423,729 |
| NOx Emissions (grams) | 44,452 | 1,844 | 41,285 | 46,461 |

Intersection 1 Mathilda Avenue/5th Avenue Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 200 | 121 | 60.5% | 45.2 | 6.9 | D |
| | Through | 840 | 518 | 61.7% | 18.7 | 2.3 | B |
| | Right Turn | 80 | 49 | 60.8% | 15.0 | 2.1 | B |
| | Subtotal | 1,120 | 688 | 61.4% | 23.1 | 2.8 | C |
| SB | Left Turn | 40 | 41 | 103.3% | 61.6 | 14.0 | E |
| | Through | 520 | 509 | 97.9% | 46.4 | 54.2 | D |
| | Right Turn | 110 | 102 | 92.4% | 40.5 | 83.8 | D |
| | Subtotal | 670 | 652 | 97.3% | 45.9 | 54.4 | D |
| EB | Left Turn | 30 | 26 | 88.0% | 40.4 | 16.5 | D |
| | Through | 30 | 32 | 107.3% | 39.3 | 14.5 | D |
| | Right Turn | 90 | 87 | 97.0% | 15.1 | 15.9 | B |
| | Subtotal | 150 | 146 | 97.3% | 25.0 | 15.8 | C |
| WB | Left Turn | 60 | 55 | 91.0% | 58.8 | 36.9 | E |
| | Through | 30 | 34 | 112.7% | 51.7 | 34.8 | D |
| | Right Turn | 20 | 20 | 98.5% | 32.0 | 51.0 | C |
| | Subtotal | 110 | 108 | 98.3% | 51.8 | 38.4 | D |
| Total | | 2,050 | 1,593 | 77.7% | 33.5 | 23.9 | C |

Intersection 2 Mathilda Avenue/Innovation Way Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 1,070 | 629 | 58.7% | 63.7 | 14.0 | E |
| | Through | 1,060 | 643 | 60.7% | 26.8 | 4.2 | C |
| | Right Turn | 360 | 216 | 60.0% | 25.4 | 5.3 | C |
| | Subtotal | 2,490 | 1,488 | 59.8% | 42.2 | 8.3 | D |
| SB | Left Turn | 20 | 20 | 101.0% | 263.3 | 189.8 | F |
| | Through | 420 | 354 | 84.3% | 286.8 | 201.9 | F |
| | Right Turn | 230 | 214 | 93.2% | 170.1 | 163.4 | F |
| | Subtotal | 670 | 588 | 87.8% | 244.5 | 189.9 | F |
| EB | Left Turn | 40 | 33 | 82.5% | 291.4 | 120.3 | F |
| | Through | 20 | 18 | 89.0% | 283.9 | 121.1 | F |
| | Right Turn | 110 | 85 | 77.0% | 323.0 | 136.2 | F |
| | Subtotal | 170 | 136 | 79.7% | 310.2 | 130.2 | F |
| WB | Left Turn | 100 | 78 | 77.7% | 289.6 | 198.8 | F |
| | Through | 40 | 36 | 89.8% | 265.8 | 199.1 | F |
| | Right Turn | 20 | 18 | 91.5% | 249.7 | 249.8 | F |
| | Subtotal | 160 | 132 | 82.4% | 278.8 | 202.8 | F |
| Total | | 3,490 | 2,344 | 67.2% | 116.9 | 53.7 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2040 No Build
AM Peak Hour

Intersection 3

Mathilda Avenue/Moffett Park Drive/SR 237 WB Ramps

Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-------------------------|--------------------------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn (Moffett Park) | 920 | 551 | 59.9% | 34.5 | 3.5 | C |
| | Left Turn (SR 237 WB On-Ramp) | 180 | 97 | 53.8% | 68.7 | 9.0 | E |
| | Through | 3,540 | 2,112 | 59.7% | 36.9 | 3.3 | D |
| | Right Turn (Moffett Park) | 860 | 517 | 60.1% | 33.3 | 3.4 | C |
| | Subtotal | 5,500 | 3,277 | 59.6% | 36.8 | 2.9 | D |
| SB | Left Turn (Moffett Park) | 30 | 24 | 80.7% | 259.8 | 54.5 | F |
| | Through | 420 | 336 | 80.0% | 487.2 | 72.1 | F |
| | Right Turn (Moffett Park) | 180 | 126 | 70.1% | 806.9 | 83.3 | F |
| | Right Turn (SR 237 WB On-Ramp) | 190 | 151 | 79.2% | 480.7 | 72.7 | F |
| | Subtotal | 820 | 637 | 77.9% | 540.4 | 67.9 | F |
| EB (Moffett Park) | Left Turn | 50 | 47 | 94.8% | 64.4 | 4.5 | E |
| | Through | 70 | 72 | 103.0% | 61.6 | 5.3 | E |
| | Right Turn | 90 | 88 | 97.6% | 24.6 | 2.1 | C |
| | Subtotal | 210 | 207 | 98.8% | 46.6 | 2.6 | D |
| WB (Moffett Park) | Left Turn | 120 | 107 | 89.3% | 366.3 | 132.3 | F |
| | Through | 280 | 252 | 90.0% | 467.8 | 133.2 | F |
| | Right Turn | 60 | 53 | 87.7% | 457.5 | 134.8 | F |
| | Subtotal | 460 | 412 | 89.5% | 440.1 | 134.7 | F |
| WB (SR 237 WB Off-Ramp) | Left Turn | 670 | 367 | 54.8% | 1469.8 | 129.1 | F |
| | Through | | | | | | F |
| | Right Turn | 620 | 343 | 55.3% | 1609.9 | 139.9 | F |
| | Subtotal | 1,290 | 710 | 55.0% | 1537.5 | 135.6 | F |
| Total | | 8,280 | 5,243 | 63.3% | 885.2 | 50.5 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2040 No Build
AM Peak Hour

Intersection 4 Mathilda Avenue/SR 237 EB Off-Ramp-SR 237 EB On-Ramp Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | 2,610 | 1,286 | 49.3% | 74.3 | 15.2 | E |
| | Right Turn | 920 | 461 | 50.1% | 3.2 | 0.4 | A |
| | Subtotal | 3,530 | 1,747 | 49.5% | 55.5 | 10.8 | E |
| SB | Left Turn | 80 | 66 | 82.8% | 66.7 | 15.2 | E |
| | Through | 1,030 | 669 | 64.9% | 15.1 | 2.2 | B |
| | Right Turn | | | | | | |
| | Subtotal | 1,110 | 735 | 66.2% | 19.7 | 2.7 | B |
| EB | Left Turn | 1,110 | 933 | 84.1% | 805.4 | 209.3 | F |
| | Through | | | | | | |
| | Right Turn | 80 | 67 | 84.1% | 768.8 | 199.2 | F |
| | Subtotal | 1,190 | 1,000 | 84.1% | 803.1 | 208.8 | F |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 5,830 | 3,482 | 59.7% | 257.7 | 43.7 | F |

Intersection 5 Mathilda Avenue/Ross Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 70 | 31 | 43.6% | 65.8 | 9.2 | E |
| | Through | 3,140 | 1,405 | 44.7% | 602.9 | 209.9 | F |
| | Right Turn | 120 | 56 | 46.8% | 96.2 | 13.7 | F |
| | Subtotal | 3,330 | 1,491 | 44.8% | 572.7 | 196.9 | F |
| SB | Left Turn | 70 | 47 | 67.1% | 67.8 | 10.6 | E |
| | Through | 980 | 652 | 66.5% | 19.6 | 3.7 | B |
| | Right Turn | 60 | 37 | 60.8% | 16.4 | 3.0 | B |
| | Subtotal | 1,110 | 735 | 66.2% | 22.5 | 3.9 | C |
| EB | Left Turn | 90 | 93 | 102.9% | 319.2 | 207.5 | F |
| | Through | 70 | 66 | 93.7% | 270.7 | 193.2 | F |
| | Right Turn | 40 | 39 | 98.0% | 226.7 | 179.6 | F |
| | Subtotal | 200 | 197 | 98.7% | 284.4 | 196.0 | F |
| WB | Left Turn | 130 | 109 | 83.9% | 547.4 | 176.4 | F |
| | Through | 40 | 36 | 89.0% | 559.2 | 196.9 | F |
| | Right Turn | 300 | 256 | 85.3% | 550.2 | 187.7 | F |
| | Subtotal | 470 | 401 | 85.2% | 551.0 | 184.5 | F |
| Total | | 5,110 | 2,825 | 55.3% | 393.7 | 98.6 | F |

Intersection 8 **Mathilda Avenue/Almanor Avenue-Ahwanee Avenue** **Signal**

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|--------------|------------|---------------------|---------------------|--------------|-----------------------|-------------|----------|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 140 | 66 | 46.8% | 1381.0 | 168.5 | F |
| | Through | 3,430 | 1,506 | 43.9% | 1458.0 | 197.4 | F |
| | Right Turn | 70 | 31 | 44.6% | 1574.5 | 253.4 | F |
| | Subtotal | 3,640 | 1,603 | 44.0% | 1457.0 | 196.7 | F |
| SB | Left Turn | 160 | 136 | 84.7% | 114.9 | 24.6 | F |
| | Through | 1,760 | 1,511 | 85.9% | 41.4 | 2.1 | D |
| | Right Turn | 340 | 292 | 85.9% | 31.0 | 2.3 | C |
| | Subtotal | 2,260 | 1,939 | 85.8% | 45.1 | 3.0 | D |
| EB | Left Turn | 130 | 99 | 76.4% | 558.9 | 361.3 | F |
| | Through | 30 | 24 | 79.0% | 369.1 | 294.8 | F |
| | Right Turn | 40 | 34 | 83.8% | 333.1 | 286.8 | F |
| | Subtotal | 200 | 157 | 78.3% | 476.9 | 331.5 | F |
| WB | Left Turn | 90 | 75 | 83.0% | 194.9 | 46.8 | F |
| | Through | 50 | 45 | 89.2% | 190.6 | 73.5 | F |
| | Right Turn | 260 | 231 | 89.0% | 213.5 | 97.3 | F |
| | Subtotal | 400 | 351 | 87.7% | 207.7 | 81.5 | F |
| Total | | 6,500 | 4,048 | 62.3% | 619.7 | 30.4 | F |

Intersection 9 **US 101 On-Ramp/Moffett Park Drive** **Signal**

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|--------------|------------|---------------------|---------------------|--------------|-----------------------|------------|----------|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| EB | Left Turn | | | | | | |
| | Through | 230 | 227 | 98.7% | 2.8 | 0.4 | A |
| | Right Turn | 20 | 19 | 96.0% | 1.8 | 0.4 | A |
| | Subtotal | 250 | 246 | 98.5% | 2.7 | 0.3 | A |
| WB | Left Turn | 40 | 24 | 60.3% | 8.4 | 0.6 | A |
| | Through | 1,010 | 707 | 70.0% | 3.4 | 0.3 | A |
| | Right Turn | | | | | | |
| | Subtotal | 1,050 | 731 | 69.6% | 3.6 | 0.3 | A |
| Total | | 1,300 | 977 | 75.2% | 3.4 | 0.3 | A |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2040 No Build
AM Peak Hour

Intersection 10 Innovation Way/Moffett Park Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | 70 | 61 | 87.7% | 37.5 | 4.4 | D |
| | Through | | | | | | |
| | Right Turn | 130 | 110 | 84.6% | 32.7 | 4.0 | C |
| | Subtotal | 200 | 171 | 85.7% | 34.4 | 4.0 | C |
| EB | Left Turn | 70 | 61 | 87.6% | 37.3 | 4.7 | D |
| | Through | 160 | 166 | 103.6% | 4.6 | 1.0 | A |
| | Right Turn | | | | | | |
| | Subtotal | 230 | 227 | 98.7% | 13.3 | 1.3 | B |
| WB | Left Turn | | | | | | |
| | Through | 920 | 623 | 67.8% | 11.3 | 0.9 | B |
| | Right Turn | 460 | 310 | 67.3% | 9.5 | 1.3 | A |
| | Subtotal | 1,380 | 933 | 67.6% | 10.7 | 0.8 | B |
| Total | | 1,810 | 1,332 | 73.6% | 14.2 | 0.7 | B |

Intersection 11 Innovation Way/11th Avenue All-way Stop

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 220 | 153 | 69.5% | 12.7 | 1.0 | B |
| | Through | 30 | 24 | 80.3% | 15.2 | 1.5 | C |
| | Right Turn | 180 | 128 | 71.1% | 9.9 | 1.1 | A |
| | Subtotal | 430 | 305 | 70.9% | 11.7 | 1.1 | B |
| SB | Left Turn | 60 | 41 | 67.5% | 7.0 | 0.3 | A |
| | Through | 100 | 70 | 70.4% | 12.7 | 1.1 | B |
| | Right Turn | 400 | 289 | 72.1% | 9.7 | 0.7 | A |
| | Subtotal | 560 | 399 | 71.3% | 9.9 | 0.6 | A |
| EB | Left Turn | 50 | 50 | 99.6% | 12.4 | 2.6 | B |
| | Through | | | | | | |
| | Right Turn | 80 | 81 | 100.8% | 9.8 | 1.2 | A |
| | Subtotal | 130 | 130 | 100.3% | 10.8 | 1.2 | B |
| WB | Left Turn | 20 | 21 | 107.0% | 5.1 | 0.6 | A |
| | Through | | | | | | |
| | Right Turn | 20 | 21 | 105.0% | 3.3 | 0.2 | A |
| | Subtotal | 40 | 42 | 106.0% | 4.2 | 0.2 | A |
| Total | | 1,160 | 877 | 75.6% | 10.4 | 0.4 | B |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2040 No Build
AM Peak Hour

Intersection 12

Innovation Way/Juniper Driveway

All-way Stop

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 30 | 26 | 87.7% | 20.8 | 25.9 | C |
| | Through | 70 | 66 | 94.1% | 88.0 | 94.0 | F |
| | Right Turn | | | | | | |
| | Subtotal | 100 | 92 | 92.2% | 67.5 | 70.9 | F |
| SB | Left Turn | | | | | | |
| | Through | 500 | 340 | 67.9% | 24.5 | 5.4 | C |
| | Right Turn | 840 | 542 | 64.5% | 18.8 | 4.1 | C |
| | Subtotal | 1,340 | 882 | 65.8% | 21.0 | 4.6 | C |
| EB | Left Turn | 100 | 82 | 82.4% | 177.2 | 172.8 | F |
| | Through | | | | | | |
| | Right Turn | 60 | 59 | 98.2% | 9.5 | 2.4 | A |
| | Subtotal | 160 | 141 | 88.3% | 100.6 | 90.2 | F |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 1,600 | 1,115 | 69.7% | 34.2 | 17.3 | D |

Intersection 13

Bordeaux Drive/Innovation Way

All-way Stop

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 50 | 37 | 73.4% | 5.5 | 1.5 | A |
| | Through | 130 | 234 | 179.9% | 2.6 | 0.2 | A |
| | Right Turn | | | | | | |
| | Subtotal | 180 | 271 | 150.3% | 3.0 | 0.3 | A |
| SB | Left Turn | | | | | | |
| | Through | 60 | 59 | 97.8% | 8.4 | 0.8 | A |
| | Right Turn | 30 | 31 | 101.7% | 7.2 | 2.8 | A |
| | Subtotal | 90 | 89 | 99.1% | 7.9 | 1.2 | A |
| EB | Left Turn | 70 | 39 | 55.3% | 6.4 | 0.5 | A |
| | Through | 50 | 35 | 70.8% | 6.9 | 0.5 | A |
| | Right Turn | 120 | 77 | 64.3% | 4.9 | 0.4 | A |
| | Subtotal | 240 | 151 | 63.0% | 5.7 | 0.4 | A |
| WB | Left Turn | | | | | | |
| | Through | 20 | 22 | 108.0% | 5.4 | 0.5 | A |
| | Right Turn | | | | | | |
| | Subtotal | 20 | 22 | 108.0% | 5.4 | 0.5 | A |
| Total | | 530 | 533 | 100.5% | 4.7 | 0.4 | A |

Intersection 1

Mathilda Avenue/5th Avenue

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 625 | 25 | 8 | 50 | 15 | 75 | 14 | 0% | 0% |
| | Through | 625 | 25 | 6 | 50 | 7 | 75 | 17 | 0% | 0% |
| | Right Turn | 625 | 50 | 19 | 100 | 35 | 125 | 34 | 0% | 0% |
| NB | Left Turn | 425 | 75 | 10 | 125 | 23 | 150 | 30 | 0% | 0% |
| | Through | 1,125 | 100 | 11 | 175 | 22 | 225 | 38 | 0% | 0% |
| | Through/Right | 1,125 | 125 | 12 | 225 | 23 | 250 | 35 | 0% | 0% |
| SB | Left Turn | 250 | 50 | 6 | 100 | 20 | 125 | 60 | 0% | 0% |
| | Through | 1,325 | 175 | 170 | 375 | 404 | 475 | 394 | 8% | 0% |
| | Right Turn | 250 | 25 | 23 | 100 | 80 | 175 | 107 | 0% | 0% |
| WB | Left Turn | 925 | 75 | 27 | 125 | 75 | 175 | 117 | 19% | 0% |
| | Through/Right | 75 | 50 | 6 | 100 | 8 | 100 | 1 | 11% | 0% |

Intersection 2

Mathilda Avenue/Innovation Way

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 200 | 50 | 14 | 100 | 23 | 125 | 26 | 0% | 18% |
| | Through/Right | 225 | 25 | 2 | 50 | 4 | 50 | 16 | 0% | 70% |
| | Right Turn | 225 | 175 | 29 | 250 | 34 | 250 | 30 | 0% | 33% |
| NB | Left Turn | 400 | 275 | 51 | 425 | 73 | 450 | 61 | 3% | 0% |
| | Through | 975 | 150 | 62 | 425 | 202 | 700 | 349 | 0% | 0% |
| | Through/Right | 975 | 200 | 36 | 375 | 81 | 475 | 191 | 0% | 0% |
| SB | Left Turn | 75 | 50 | 10 | 125 | 18 | 150 | 1 | 5% | 0% |
| | Through | 975 | 475 | 274 | 875 | 352 | 950 | 332 | 71% | 8% |
| | Right Turn | 225 | 200 | 24 | 350 | 45 | 275 | 0 | 10% | 0% |
| WB | Left Turn | 425 | 200 | 116 | 425 | 160 | 500 | 110 | 11% | 1% |
| | Shared | 225 | 150 | 41 | 250 | 39 | 225 | 3 | 26% | 0% |

SimTraffic Post-Processor
Average Results from 10 Runs
Queue Length

Mathilda Avenue Improvements
2040 No Build
AM Peak Hour

Intersection 3

Mathilda Avenue/Moffett Park Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-------------------------|-----------------------------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB (Moffett Park) | Left Turn | 525 | 50 | 2 | 75 | 7 | 100 | 14 | 0% | 0% |
| | Through/Right | 1,125 | 75 | 10 | 150 | 20 | 150 | 14 | 0% | 6% |
| | Right Turn | 1,125 | 75 | 2 | 100 | 6 | 125 | 18 | 0% | 0% |
| NB | Left Turn (Moffett Park) | 125 | 50 | 3 | 50 | 6 | 50 | 11 | 0% | 19% |
| | Through | 300 | 275 | 13 | 325 | 20 | 350 | 21 | 0% | 64% |
| | Through/Right (Moffett Park) | 300 | 300 | 12 | 350 | 20 | 350 | 25 | 0% | 81% |
| | Left Turn (SR 237 WB On-Ramp) | 175 | 100 | 21 | 175 | 25 | 200 | 10 | 0% | 5% |
| SB | Left Turn (Moffett Park) | 175 | 25 | 6 | 75 | 12 | 100 | 20 | 0% | 0% |
| | Through | 1,100 | 1,050 | 64 | 1,200 | 83 | 1,125 | 70 | 7% | 49% |
| | Through/Right (Moffett Park) | 975 | 1,050 | 23 | 1,125 | 28 | 1,125 | 22 | 0% | 60% |
| WB (Moffett Park) | Through/Right (SR 237 WB On-Ramp) | 1,100 | 1,050 | 65 | 1,225 | 84 | 1,175 | 72 | 7% | 49% |
| | Left Turn | 300 | 1,025 | 194 | 1,500 | 152 | 1,375 | 102 | 0% | 0% |
| WB (Moffett Park) | Through/Right | 675 | 625 | 44 | 700 | 49 | 675 | 3 | 83% | 51% |
| | Left Turn | 1,075 | 1,175 | 1 | 1,200 | 6 | 1,200 | 6 | 0% | 71% |
| WB (SR 237 WB Off-Ramp) | Left/Through | 325 | 450 | 1 | 450 | 3 | 450 | 0 | 6% | 0% |
| | Right Turn | 325 | 13,150 | 569 | 17,875 | 500 | 15,425 | 57 | 85% | 0% |

Intersection 4

Mathilda Avenue/SR 237 EB Off-Ramp-SR 237 EB On-Ramp

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,025 | 6,425 | 1,982 | 9,700 | 2,356 | 9,275 | 2,221 | 84% | 5% |
| | Shared | 1,025 | 550 | 5 | 575 | 40 | 575 | 0 | 47% | 0% |
| NB | Through | 275 | 275 | 16 | 325 | 23 | 325 | 37 | 0% | 62% |
| | Right Turn | 275 | 75 | 29 | 250 | 64 | 300 | 24 | 0% | 5% |
| SB | Left Turn | 175 | 75 | 7 | 150 | 13 | 175 | 18 | 0% | 1% |
| | Through | 175 | 100 | 14 | 175 | 16 | 200 | 18 | 0% | 1% |
| | | | | | | | | | | |

Intersection 5

Mathilda Avenue/Ross Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 250 | 500 | 324 | 1,000 | 522 | 1,025 | 481 | 79% | 1% |
| | Through | 1,575 | 75 | 7 | 125 | 5 | 100 | 0 | 34% | 0% |
| | Right Turn | 50 | 50 | 6 | 75 | 6 | 75 | 3 | 3% | 0% |
| NB | Left Turn | 150 | 50 | 6 | 100 | 10 | 125 | 19 | 0% | 0% |
| | Through | 2,800 | 1,100 | 72 | 1,100 | 94 | 1,100 | 48 | 1% | 63% |
| | Through/Right | 450 | 525 | 14 | 575 | 60 | 575 | 0 | 0% | 85% |
| SB | Left Turn | 225 | 50 | 13 | 100 | 35 | 125 | 55 | 3% | 0% |
| | Through | 225 | 100 | 22 | 225 | 33 | 250 | 39 | 6% | 1% |
| | Through/Right | 225 | 125 | 24 | 250 | 35 | 250 | 28 | 0% | 2% |
| WB | Left Turn | 100 | 2,325 | 915 | 3,600 | 1,364 | 3,425 | 1,254 | 35% | 0% |
| | Through | 225 | 100 | 4 | 125 | 13 | 100 | 0 | 12% | 0% |
| | Right Turn | 100 | 75 | 2 | 100 | 8 | 100 | 0 | 63% | 0% |

Intersection 8

Mathilda Avenue/Almanor Avenue-Ahwanee Avenue

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,025 | 250 | 48 | 475 | 62 | 400 | 15 | 63% | 40% |
| | Through/Right | 125 | 100 | 11 | 225 | 16 | 225 | 0 | 1% | 0% |
| NB | Left Turn | 425 | 125 | 29 | 325 | 65 | 375 | 1 | 0% | 0% |
| | Through | 750 | 10,150 | 31 | 15,025 | 56 | 12,875 | 12 | 79% | 0% |
| | Right Turn | 75 | 25 | 9 | 100 | 21 | 100 | 0 | 0% | 0% |
| SB | Left Turn | 125 | 150 | 8 | 200 | 5 | 175 | 0 | 44% | 0% |
| | Through | 2,225 | 500 | 26 | 550 | 47 | 600 | 81 | 15% | 0% |
| | Through/Right | 2,225 | 325 | 20 | 475 | 23 | 525 | 20 | 0% | 0% |
| WB | Left Turn | 250 | 150 | 42 | 375 | 55 | 350 | 0 | 1% | 0% |
| | Through | 1,025 | 550 | 174 | 1,175 | 276 | 1,025 | 84 | 6% | 0% |
| | Right Turn | 75 | 125 | 3 | 150 | 4 | 125 | 0 | 69% | 0% |

Intersection 9

US 101 On-Ramp/Moffett Park Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Through | 850 | 25 | 5 | 75 | 15 | 100 | 19 | 0% | 0% |
| | Right Turn | 150 | 25 | 1 | 25 | 7 | 25 | 16 | 0% | 0% |
| WB | Left Turn | 850 | 25 | 3 | 50 | 4 | 75 | 8 | 0% | 0% |
| | Through | 850 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | | | | | | | | | | |
| | | | | | | | | | | |

Intersection 10

Innovation Way/Moffett Park Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 225 | 50 | 6 | 100 | 9 | 125 | 22 | 0% | 0% |
| | Through | 850 | 25 | 5 | 75 | 11 | 100 | 19 | 0% | 0% |
| SB | Left Turn | 575 | 50 | 3 | 50 | 7 | 75 | 15 | 0% | 0% |
| | Shared | 575 | 100 | 5 | 175 | 10 | 200 | 14 | 0% | 0% |
| WB | Through | 1,150 | 125 | 13 | 200 | 22 | 250 | 59 | 0% | 0% |
| | Right Turn | 1,150 | 75 | 18 | 200 | 26 | 225 | 20 | 0% | 0% |
| | | | | | | | | | | |

Intersection 11

Innovation Way/11th Avenue

All-way Stop

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 125 | 50 | 4 | 75 | 7 | 75 | 12 | 0% | 0% |
| | Through/Right | 325 | 25 | 4 | 50 | 4 | 50 | 16 | 0% | 0% |
| | Right Turn | 325 | 50 | 4 | 75 | 6 | 100 | 17 | 0% | 0% |
| NB | Left Turn | 125 | 25 | 3 | 50 | 4 | 75 | 7 | 0% | 0% |
| | Left/Through | 575 | 50 | 3 | 75 | 6 | 75 | 8 | 0% | 0% |
| | Through/Right | 575 | 50 | 4 | 75 | 10 | 75 | 15 | 0% | 0% |
| SB | Left/Through | 1,000 | 25 | 2 | 50 | 4 | 50 | 17 | 0% | 0% |
| | Through/Right | 1,000 | 75 | 4 | 125 | 13 | 150 | 35 | 0% | 0% |
| WB | Left Turn | 325 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | Through/Right | 325 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |

Intersection 12

Innovation Way/Juniper Driveway

All-way Stop

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 200 | 150 | 120 | 375 | 297 | 450 | 262 | 0% | 0% |
| | Right Turn | 200 | 50 | 3 | 75 | 5 | 75 | 11 | 0% | 0% |
| NB | Left Turn | 125 | 25 | 9 | 75 | 33 | 100 | 56 | 0% | 0% |
| | Through | 1,000 | 100 | 29 | 175 | 78 | 200 | 76 | 11% | 0% |
| SB | Through/Right | 300 | 225 | 22 | 275 | 26 | 325 | 26 | 0% | 7% |
| | Right Turn | 300 | 250 | 16 | 300 | 19 | 300 | 18 | 0% | 4% |
| | | | | | | | | | | |

Intersection 13

Bordeaux Drive/Innovation Way

All-way Stop

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left/Through | 375 | 50 | 4 | 75 | 5 | 75 | 13 | 0% | 0% |
| | Right Turn | 125 | 50 | 3 | 75 | 8 | 75 | 23 | 0% | 0% |
| NB | Left Turn | 325 | 25 | 3 | 50 | 4 | 75 | 12 | 0% | 0% |
| | Through/Right | 2,025 | 50 | 4 | 75 | 6 | 75 | 9 | 0% | 0% |
| SB | Left Turn | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | Through/Right | 725 | 50 | 3 | 75 | 8 | 75 | 18 | 0% | 0% |
| WB | Left/Through | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | Right Turn | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |

Arterial Level of Service

No Build 2040 AM

2/25/2016

Arterial Level of Service: NB Mathilda Ave

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|----------------------|------|---------------|-----------------|------------|----------------|
| Ahwanee Ave | 8 | 161.8 | 172.4 | 0.1 | 3 |
| US 101 SB Diag. On-R | 702 | 49.7 | 56.3 | 0.1 | 5 |
| US 101 SB Loop On-Ra | 701 | 122.9 | 130.7 | 0.1 | 3 |
| US 101 NB Loop On-Ra | 602 | 101.6 | 107.3 | 0.1 | 2 |
| US 101 NB Diag.Off-R | 601 | 138.8 | 145.6 | 0.1 | 2 |
| Ross Dr | 5 | 144.7 | 152.0 | 0.1 | 2 |
| SR 237 EB On-Ramp | 4 | 69.1 | 74.4 | 0.1 | 3 |
| SR 237 WB Off-Ramp | 33 | 25.2 | 29.0 | 0.0 | 6 |
| Moffett Park Dr | 3 | 4.1 | 6.8 | 0.0 | 22 |
| Innovation Way | 2 | 27.5 | 44.2 | 0.2 | 17 |
| 5th Ave | 1 | 18.9 | 38.1 | 0.2 | 22 |
| | 107 | 4.4 | 26.5 | 0.3 | 37 |
| Total | | 868.8 | 983.3 | 1.5 | 5 |

Arterial Level of Service: SB Mathilda Ave

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|----------------------|------|---------------|-----------------|------------|----------------|
| 5th Ave | 1 | 33.2 | 55.4 | 0.3 | 18 |
| Innovation Way | 2 | 277.6 | 294.7 | 0.2 | 3 |
| Moffett Park Dr | 3 | 447.2 | 461.5 | 0.2 | 2 |
| SR 237 WB On-Ramp | 33 | 5.5 | 8.5 | 0.0 | 18 |
| SR 237 Off/On Ramp | 4 | 14.2 | 18.3 | 0.0 | 9 |
| Ross Dr | 5 | 20.6 | 25.6 | 0.1 | 9 |
| US 101 NB Diag.Off-R | 601 | 5.0 | 13.3 | 0.1 | 25 |
| US 101 NB Loop Off-R | 602 | 2.2 | 7.9 | 0.1 | 41 |
| US 101 SB Loop On-Ra | 701 | 1.1 | 7.2 | 0.1 | 33 |
| US 101 SB Off-Ramp | 702 | 1.6 | 8.3 | 0.1 | 45 |
| Almanor Ave | 8 | 30.0 | 38.1 | 0.1 | 8 |
| San Aleso Ave | 201 | 4.1 | 15.5 | 0.1 | 33 |
| Total | | 842.5 | 954.3 | 1.5 | 5 |

Arterial Level of Service

No Build 2040 AM

2/25/2016

Arterial Level of Service: NB Innovation Way

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|------------------|------|---------------|-----------------|------------|----------------|
| | 910 | 6.5 | 8.4 | 0.0 | 10 |
| | 38 | 1.4 | 6.5 | 0.0 | 23 |
| | 11 | 8.3 | 15.5 | 0.1 | 17 |
| | 200 | 9.1 | 25.5 | 0.2 | 22 |
| Juniper Driveway | 12 | 85.6 | 91.3 | 0.1 | 2 |
| Driveway | 217 | 62.9 | 65.7 | 0.0 | 2 |
| | 902 | 179.7 | 182.4 | 0.0 | 0 |
| Mathilda Ave | 2 | 26.3 | 27.8 | 0.0 | 3 |
| | 53 | 1.4 | 14.2 | 0.1 | 25 |
| Bordeaux Dr | 13 | 5.4 | 16.5 | 0.1 | 17 |
| Total | | 386.6 | 453.8 | 0.6 | 5 |

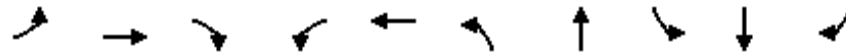
Arterial Level of Service: SB Innovation Way

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|------------------|------|---------------|-----------------|------------|----------------|
| | 53 | 51.5 | 62.5 | 0.1 | 5 |
| Mathilda Ave | 2 | 214.8 | 225.6 | 0.1 | 2 |
| | 902 | 7.6 | 12.2 | 0.0 | 7 |
| Driveway | 217 | 2.7 | 4.6 | 0.0 | 17 |
| Juniper Driveway | 12 | 19.4 | 23.3 | 0.0 | 6 |
| | 200 | 3.0 | 9.5 | 0.1 | 21 |
| 11th Ave | 11 | 10.1 | 25.7 | 0.2 | 22 |
| | 38 | 3.3 | 11.1 | 0.1 | 23 |
| | 910 | 20.0 | 24.4 | 0.0 | 6 |
| Moffett Park Dr | 10 | 15.3 | 18.6 | 0.0 | 4 |
| Total | | 347.5 | 417.5 | 0.6 | 5 |

Lanes, Volumes, Timings

1: Mathilda Ave & 5th Ave

3/4/2016

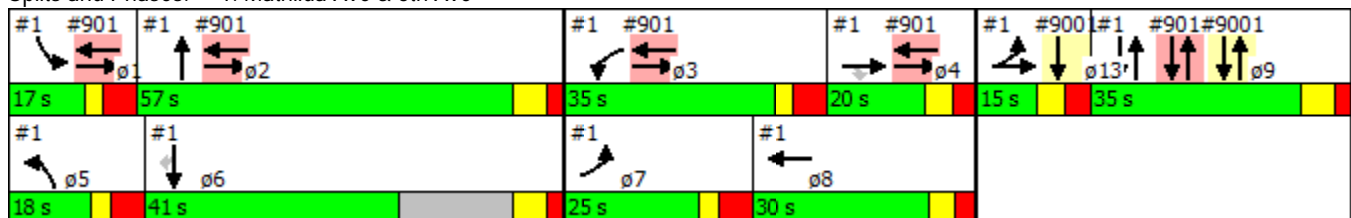


| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT | SBR | ø2 | ø7 |
|----------------------|------|------|--------|-------|-------|-------|-----|------|------|--------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 180 | 40 | 170 | 290 | 20 | 140 | 620 | 20 | 1120 | 30 | | |
| Turn Type | Prot | NA | custom | Prot | NA | Prot | NA | Prot | NA | custom | | |
| Protected Phases | 7 13 | 4 13 | | 3 | 8 | 5 | 2 9 | 1 | 6 9 | | 2 | 7 |
| Permitted Phases | | | 4 | | | | | | | 6 | | |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 5 | 2 | 1 | 6 | 6 | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 13.0 | 12.0 | 8.0 | 11.0 | | 10.0 | | 12.0 | 12.0 | 12.0 |
| Minimum Split (s) | | | 20.0 | 19.0 | 29.5 | 18.0 | | 17.0 | | 41.0 | 35.0 | 19.0 |
| Total Split (s) | | | 20.0 | 35.0 | 30.0 | 18.0 | | 17.0 | | 41.0 | 57.0 | 25.0 |
| Total Split (%) | | | 11.2% | 19.6% | 16.8% | 10.1% | | 9.5% | | 22.9% | 32% | 14% |
| Yellow Time (s) | | | 3.6 | 2.5 | 3.6 | 2.5 | | 2.5 | | 4.7 | 4.7 | 2.5 |
| All-Red Time (s) | | | 3.4 | 4.5 | 2.9 | 4.5 | | 4.5 | | 2.3 | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | | 0.0 | | |
| Total Lost Time (s) | | | 7.0 | 7.0 | 6.5 | 7.0 | | 7.0 | | 7.0 | | |
| Lead/Lag | | | Lag | Lead | Lag | Lead | | Lead | | Lag | Lag | Lead |
| Lead-Lag Optimize? | | | Yes | Yes | Yes | Yes | | Yes | | Yes | Yes | Yes |
| Recall Mode | | | None | None | None | None | | None | | Min | Min | None |

Intersection Summary

Cycle Length: 179
 Actuated Cycle Length: 119.2
 Natural Cycle: 160
 Control Type: Actuated-Uncoordinated

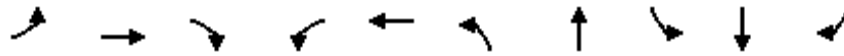
Splits and Phases: 1: Mathilda Ave & 5th Ave



| Lane Group | ø9 | ø13 |
|----------------------|------|------|
| Lane Configurations | | |
| Volume (vph) | | |
| Turn Type | | |
| Protected Phases | 9 | 13 |
| Permitted Phases | | |
| Detector Phase | | |
| Switch Phase | | |
| Minimum Initial (s) | 28.0 | 8.0 |
| Minimum Split (s) | 35.0 | 15.0 |
| Total Split (s) | 35.0 | 15.0 |
| Total Split (%) | 20% | 8% |
| Yellow Time (s) | 4.7 | 3.6 |
| All-Red Time (s) | 2.3 | 3.4 |
| Lost Time Adjust (s) | | |
| Total Lost Time (s) | | |
| Lead/Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes |
| Recall Mode | None | None |
| Intersection Summary | | |

Lanes, Volumes, Timings
 2: Mathilda Ave & Innovation Way

3/4/2016



| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT | SBR | ø2 | ø4 |
|----------------------|-------|------|------|-------|-------|-------|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 330 | 50 | 910 | 180 | 20 | 190 | 470 | 20 | 1490 | 70 | | |
| Turn Type | Split | NA | Prot | Split | NA | Prot | NA | Prot | NA | Perm | | |
| Protected Phases | 4 13 | 4 13 | 4 13 | 8 | 8 | 5 | 2 9 | 1 | 6 9 | | 2 | 4 |
| Permitted Phases | | | | | | | | | | | | 6 9 |
| Detector Phase | 4 | 4 | 4 | 8 | 8 | 5 | 2 | 1 | 6 | 6 | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | | 10.0 | 10.0 | 13.0 | | 10.0 | | | 12.0 | 14.0 |
| Minimum Split (s) | | | | 35.0 | 35.0 | 20.0 | | 16.8 | | | 19.0 | 39.0 |
| Total Split (s) | | | | 35.0 | 35.0 | 20.0 | | 19.2 | | | 37.8 | 58.0 |
| Total Split (%) | | | | 17.5% | 17.5% | 10.0% | | 9.6% | | | 19% | 29% |
| Yellow Time (s) | | | | 2.5 | 2.5 | 2.5 | | 2.5 | | | 4.7 | 2.5 |
| All-Red Time (s) | | | | 4.5 | 4.5 | 4.5 | | 4.3 | | | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | | 0.0 | 0.0 | 0.0 | | 0.0 | | | | |
| Total Lost Time (s) | | | | 7.0 | 7.0 | 7.0 | | 6.8 | | | | |
| Lead/Lag | | | | | | | Lead | Lead | | | | Lag |
| Lead-Lag Optimize? | | | | | | | Yes | Yes | | | | Yes |
| Recall Mode | | | | None | None | None | | None | | | Min | Max |

Intersection Summary

Cycle Length: 200
 Actuated Cycle Length: 177
 Natural Cycle: 175
 Control Type: Actuated-Uncoordinated

Splits and Phases: 2: Mathilda Ave & Innovation Way



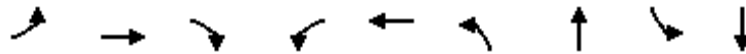
Lanes, Volumes, Timings
 2: Mathilda Ave & Innovation Way

3/4/2016

| Lane Group | ø6 | ø9 | ø13 |
|----------------------|------|------|------|
| Lane Configurations | | | |
| Volume (vph) | | | |
| Turn Type | | | |
| Protected Phases | 6 | 9 | 13 |
| Permitted Phases | | | |
| Detector Phase | | | |
| Switch Phase | | | |
| Minimum Initial (s) | 12.0 | 28.0 | 8.0 |
| Minimum Split (s) | 30.0 | 35.0 | 15.0 |
| Total Split (s) | 37.0 | 35.0 | 15.0 |
| Total Split (%) | 19% | 18% | 8% |
| Yellow Time (s) | 4.7 | 4.7 | 2.5 |
| All-Red Time (s) | 2.3 | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | |
| Total Lost Time (s) | | | |
| Lead/Lag | Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes | Yes |
| Recall Mode | Min | None | None |
| Intersection Summary | | | |

Lanes, Volumes, Timings
3: Mathilda Ave & Moffett Park Dr

3/4/2016

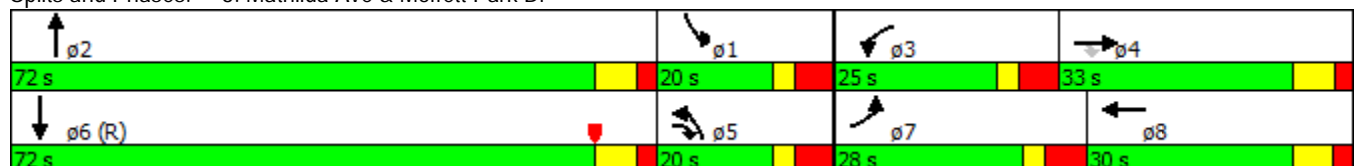


| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↶ | ↷ | ↷ | ↶↷ | ↷ | ↶↷ | ↶↷↷ | ↶ | ↶↶↶ |
| Volume (vph) | 180 | 270 | 640 | 390 | 330 | 180 | 620 | 60 | 2290 |
| Turn Type | Prot | NA | pm+ov | Prot | NA | Prot | NA | Prot | NA |
| Protected Phases | 7 | 4 | 5 | 3 | 8 | 5 | 2 | 1 | 6 |
| Permitted Phases | | | 4 | | | | | | |
| Detector Phase | 7 | 4 | 5 | 3 | 8 | 5 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | | |
| Minimum Initial (s) | 8.0 | 8.0 | 4.0 | 8.0 | 8.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | 15.0 | 15.0 | 11.0 | 15.0 | 30.0 | 11.0 | 34.9 | 11.0 | 10.9 |
| Total Split (s) | 28.0 | 33.0 | 20.0 | 25.0 | 30.0 | 20.0 | 72.0 | 20.0 | 72.0 |
| Total Split (%) | 18.7% | 22.0% | 13.3% | 16.7% | 20.0% | 13.3% | 48.0% | 13.3% | 48.0% |
| Yellow Time (s) | 2.5 | 4.7 | 2.5 | 2.5 | 4.5 | 2.5 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 4.5 | 2.3 | 4.5 | 4.5 | 2.5 | 4.5 | 2.2 | 4.5 | 2.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.9 | 7.0 | 6.9 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | Max | Max | Max | None | Max | Max | None | C-Max |

Intersection Summary

Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 0 (0%), Referenced to phase 6:SBT, Start of Yellow, Master Intersection
 Natural Cycle: 135
 Control Type: Actuated-Coordinated

Splits and Phases: 3: Mathilda Ave & Moffett Park Dr



Lanes, Volumes, Timings

4: Mathilda Ave & SR 237 Off/On Ramp/SR 237 EB On-Ramp

3/4/2016



| Lane Group | EBL | EBT | NBT | NBR | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | |
| Volume (vph) | 280 | 0 | 600 | 860 | 460 | 3120 |
| Turn Type | Split | NA | NA | Perm | Prot | NA |
| Protected Phases | 4 | 4 | 2 | | 1 | 6 |
| Permitted Phases | | | | 2 | | |
| Detector Phase | 4 | 4 | 2 | 2 | 1 | 6 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 5.0 | 5.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | 12.0 | 12.0 | 20.2 | 20.2 | 10.4 | 10.9 |
| Total Split (s) | 40.6 | 40.6 | 61.0 | 61.0 | 48.4 | 109.4 |
| Total Split (%) | 27.1% | 27.1% | 40.7% | 40.7% | 32.3% | 72.9% |
| Yellow Time (s) | 4.8 | 4.8 | 4.7 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 2.2 | 2.2 | 1.5 | 1.5 | 3.9 | 2.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 6.2 | 6.2 | 6.4 | 6.9 |
| Lead/Lag | | | Lag | Lag | Lead | |
| Lead-Lag Optimize? | | | Yes | Yes | Yes | |
| Recall Mode | Max | Max | None | None | Max | C-Max |

Intersection Summary

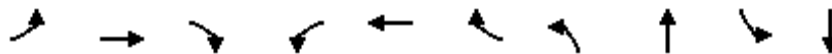
Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 49 (33%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 90
 Control Type: Actuated-Coordinated

Splits and Phases: 4: Mathilda Ave & SR 237 Off/On Ramp/SR 237 EB On-Ramp



Lanes, Volumes, Timings
5: Mathilda Ave & Ross Dr

3/4/2016

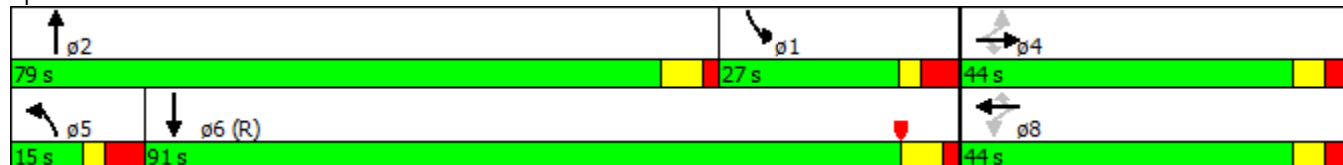


| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↖ | ↑ | ↗ | ↖ | ↑ | ↗ | ↖ | ↑↑↑↑ | ↖ | ↑↑↑ |
| Volume (vph) | 60 | 200 | 60 | 290 | 70 | 130 | 120 | 1270 | 180 | 3040 |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | Prot | NA | Prot | NA |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | 1 | 6 |
| Permitted Phases | 4 | | 4 | 8 | | 8 | | | | |
| Detector Phase | 4 | 4 | 4 | 8 | 8 | 8 | 5 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 4.0 | 5.0 | 4.0 | 5.0 |
| Minimum Split (s) | 41.0 | 41.0 | 41.0 | 13.0 | 13.0 | 13.0 | 11.0 | 31.4 | 11.0 | 11.6 |
| Total Split (s) | 44.0 | 44.0 | 44.0 | 44.0 | 44.0 | 44.0 | 15.0 | 79.0 | 27.0 | 91.0 |
| Total Split (%) | 29.3% | 29.3% | 29.3% | 29.3% | 29.3% | 29.3% | 10.0% | 52.7% | 18.0% | 60.7% |
| Yellow Time (s) | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 2.5 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 3.4 | 3.4 | 3.4 | 3.4 | 3.4 | 3.4 | 4.5 | 1.7 | 4.5 | 1.9 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.4 | 7.0 | 6.6 |
| Lead/Lag | | | | | | | Lead | Lead | Lag | Lag |
| Lead-Lag Optimize? | | | | | | | Yes | Yes | Yes | Yes |
| Recall Mode | Max | Max | Max | Max | Max | Max | Max | Max | None | C-Max |

Intersection Summary

Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 35 (23%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 145
 Control Type: Actuated-Coordinated

Splits and Phases: 5: Mathilda Ave & Ross Dr



Lanes, Volumes, Timings
 8: Mathilda Ave & Almanor Ave/Ahwanee Ave

3/4/2016

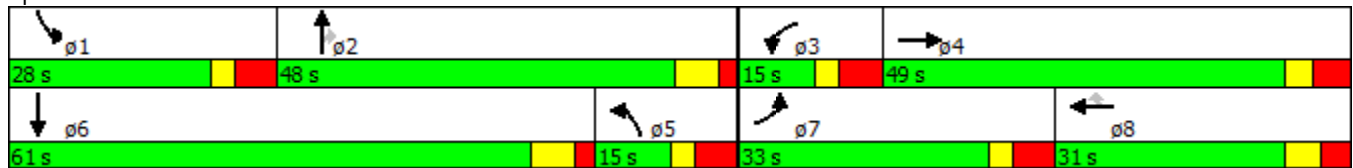


| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | | |
| Volume (vph) | 430 | 40 | 60 | 30 | 260 | 80 | 1790 | 60 | 260 | 2990 |
| Turn Type | Prot | NA | Prot | NA | Perm | Prot | NA | Perm | Prot | NA |
| Protected Phases | 7 | 4 | 3 | 8 | | 5 | 2 | | 1 | 6 |
| Permitted Phases | | | | | 8 | | | 2 | | |
| Detector Phase | 7 | 4 | 3 | 8 | 8 | 5 | 2 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 12.0 | 12.0 | 8.0 | 12.0 |
| Minimum Split (s) | 15.0 | 49.0 | 15.0 | 15.0 | 15.0 | 15.0 | 36.7 | 36.7 | 15.0 | 27.7 |
| Total Split (s) | 33.0 | 49.0 | 15.0 | 31.0 | 31.0 | 15.0 | 48.0 | 48.0 | 28.0 | 61.0 |
| Total Split (%) | 23.6% | 35.0% | 10.7% | 22.1% | 22.1% | 10.7% | 34.3% | 34.3% | 20.0% | 43.6% |
| Yellow Time (s) | 2.5 | 2.8 | 2.5 | 3.6 | 3.6 | 2.5 | 4.7 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 4.5 | 4.2 | 4.5 | 3.4 | 3.4 | 4.5 | 2.0 | 2.0 | 4.5 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.7 | 6.7 | 7.0 | 6.7 |
| Lead/Lag | Lead | Lag | Lead | Lag | Lag | Lag | Lag | Lag | Lead | Lead |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | None | Max | Max | None | Max |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 120
 Natural Cycle: 150
 Control Type: Actuated-Uncoordinated

Splits and Phases: 8: Mathilda Ave & Almanor Ave/Ahwanee Ave



Lanes, Volumes, Timings
 9: US 101 On Ramp & Moffett Park Dr

3/4/2016

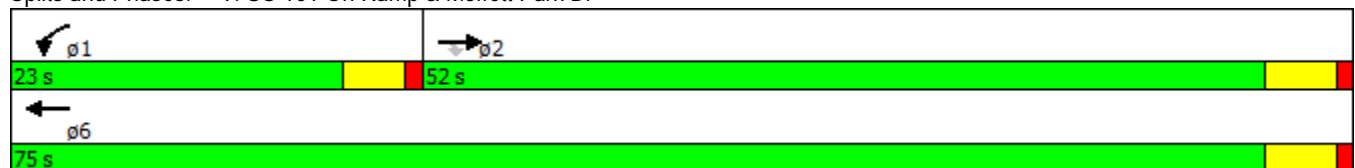


| Lane Group | EBT | EBR | WBL | WBT |
|----------------------|-------|-------|-------|--------|
| Lane Configurations | ↑ | ↗ | ↖ | ↑ |
| Volume (vph) | 1010 | 150 | 350 | 450 |
| Turn Type | NA | Perm | Prot | NA |
| Protected Phases | 2 | | 1 | 6 |
| Permitted Phases | | 2 | | |
| Detector Phase | 2 | 2 | 1 | 6 |
| Switch Phase | | | | |
| Minimum Initial (s) | 15.0 | 15.0 | 6.0 | 15.0 |
| Minimum Split (s) | 20.0 | 20.0 | 10.5 | 20.0 |
| Total Split (s) | 52.0 | 52.0 | 23.0 | 75.0 |
| Total Split (%) | 69.3% | 69.3% | 30.7% | 100.0% |
| Yellow Time (s) | 4.0 | 4.0 | 3.5 | 4.0 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.0 | 5.0 | 4.5 | 5.0 |
| Lead/Lag | Lag | Lag | Lead | |
| Lead-Lag Optimize? | | | | |
| Recall Mode | Min | Min | Max | Min |

Intersection Summary

Cycle Length: 75
 Actuated Cycle Length: 70.6
 Natural Cycle: 70
 Control Type: Semi Act-Uncoord

Splits and Phases: 9: US 101 On Ramp & Moffett Park Dr



Lanes, Volumes, Timings
 10: Moffett Park Dr & Innovation Way

3/4/2016

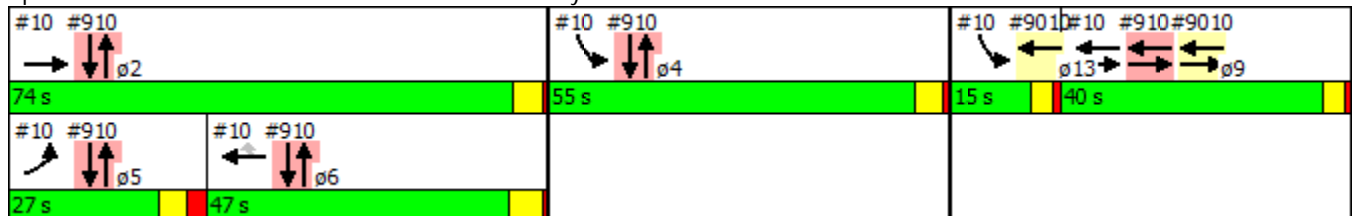


| Lane Group | EBL | EBT | WBT | WBR | SBL | ø2 | ø4 | ø9 | ø13 |
|----------------------|-------|-----|-----|--------|------|------|------|------|------|
| Lane Configurations | ↶ | ↕↕ | ↕↕ | ↶ | ↶↶ | | | | |
| Volume (vph) | 60 | 950 | 610 | 130 | 370 | | | | |
| Turn Type | Prot | NA | NA | custom | Prot | | | | |
| Protected Phases | 5 | 2 9 | 6 9 | | 4 13 | 2 | 4 | 9 | 13 |
| Permitted Phases | | | | 6 | | | | | |
| Detector Phase | 5 | 2 | 6 | 6 | 4 | | | | |
| Switch Phase | | | | | | | | | |
| Minimum Initial (s) | 8.0 | | | 10.0 | | 10.0 | 10.0 | 46.0 | 10.0 |
| Minimum Split (s) | 14.5 | | | 15.5 | | 14.9 | 15.0 | 50.0 | 14.0 |
| Total Split (s) | 27.0 | | | 47.0 | | 74.0 | 55.0 | 40.0 | 15.0 |
| Total Split (%) | 14.7% | | | 25.5% | | 40% | 30% | 22% | 8% |
| Yellow Time (s) | 4.0 | | | 4.5 | | 3.9 | 4.0 | 3.0 | 3.0 |
| All-Red Time (s) | 2.5 | | | 1.0 | | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | | | 0.0 | | | | | |
| Total Lost Time (s) | 6.5 | | | 5.5 | | | | | |
| Lead/Lag | Lead | | | Lag | | | | Lag | Lead |
| Lead-Lag Optimize? | Yes | | | Yes | | | | Yes | Yes |
| Recall Mode | None | | | Min | | Min | None | None | None |

Intersection Summary

















Cycle Length: 184
 Actuated Cycle Length: 90.2
 Natural Cycle: 110
 Control Type: Actuated-Uncoordinated

Splits and Phases: 10: Moffett Park Dr & Innovation Way



Lanes, Volumes, Timings
 11: Innovation Way & 11th Ave

3/4/2016

| |  |  |  |  |  |  |  |  |
|---------------------|---|---|---|---|---|---|---|---|
| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBT |
| Lane Configurations |  |  |  |  |  |  |  |  |
| Volume (vph) | 500 | 0 | 340 | 40 | 0 | 40 | 90 | 110 |
| Sign Control | | Stop | | | Stop | | Stop | Stop |

Intersection Summary

Control Type: Unsignalized

Lanes, Volumes, Timings
 12: Innovation Way & Juniper Driveway

3/4/2016



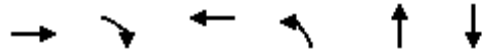
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
|---------------------|------|-----|-----|------|------|-----|
| Lane Configurations | | | | | | |
| Volume (vph) | 700 | 80 | 20 | 590 | 110 | 170 |
| Sign Control | Stop | | | Stop | Stop | |

Intersection Summary

Control Type: Unsignalized

Lanes, Volumes, Timings
 13: Bordeaux Dr & Innovation Way/Driveway

3/4/2016



| Lane Group | EBT | EBR | WBT | NBL | NBT | SBT |
|---------------------|------|-----|------|-----|------|------|
| Lane Configurations | | | | | | |
| Volume (vph) | 30 | 70 | 30 | 60 | 50 | 180 |
| Sign Control | Stop | | Stop | | Stop | Stop |

Intersection Summary

Control Type: Unsignalized

Lanes, Volumes, Timings

33: Mathilda Ave & SR 237 WB On-Ramp/SR 237 WB Off-Ramp

3/4/2016

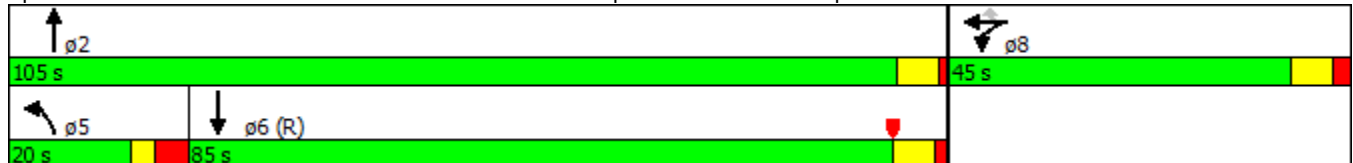


| Lane Group | WBL | WBT | WBR | NBL | NBT | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | |
| Volume (vph) | 820 | 0 | 240 | 110 | 770 | 2760 |
| Turn Type | Split | NA | Perm | Prot | NA | NA |
| Protected Phases | 8 | 8 | | 5 | 2 | 6 |
| Permitted Phases | | | 8 | | | |
| Detector Phase | 8 | 8 | 8 | 5 | 2 | 6 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | 11.0 | 11.0 | 11.0 | 10.3 | 19.0 | 10.3 |
| Total Split (s) | 45.0 | 45.0 | 45.0 | 20.0 | 105.0 | 85.0 |
| Total Split (%) | 30.0% | 30.0% | 30.0% | 13.3% | 70.0% | 56.7% |
| Yellow Time (s) | 4.8 | 4.8 | 4.8 | 2.5 | 4.7 | 4.7 |
| All-Red Time (s) | 2.2 | 2.2 | 2.2 | 3.8 | 1.3 | 1.6 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 6.3 | 6.0 | 6.3 |
| Lead/Lag | | | | Lead | | Lag |
| Lead-Lag Optimize? | | | | Yes | | Yes |
| Recall Mode | Max | Max | Max | Max | Max | C-Max |

Intersection Summary

Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 33 (22%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 130
 Control Type: Actuated-Coordinated

Splits and Phases: 33: Mathilda Ave & SR 237 WB On-Ramp/SR 237 WB Off-Ramp



**SimTraffic Post-Processor
Average Results from 10 Runs
Network Performance**

**Mathilda Avenue Improvements
2040 No Build
PM Peak Hour**

| Performance Measure | Average | Std. Dev. | Minimum | Maximum |
|---------------------------------|---------|-----------|---------|---------|
| Average Delay (seconds) | 893.8 | 7.3 | 883.2 | 908.2 |
| Total Delay (hours) | 3,830 | 44 | 3,765 | 3,887 |
| Average Stopped Delay (seconds) | 858.3 | 8.8 | 845.5 | 876.9 |
| Total Stopped Delay (hours) | 3678 | 48 | 3605 | 3733 |
| Total Stops | 49,049 | 1,966 | 44,634 | 51,312 |
| Average Stops | 3.18 | 0.12 | 2.92 | 3.34 |
| Total Distance Traveled (miles) | 40,044 | 611 | 38,552 | 40,712 |
| Average Speed (mph) | 8.0 | 0.0 | 8.0 | 8.0 |
| Total Travel Time (hours) | 5,004.3 | 49.4 | 4,927.3 | 5,092.3 |
| Vehicles Entered | 12,488 | 110 | 12,347 | 12,691 |
| Vehicles Exited | 8,820 | 150 | 8,506 | 9,050 |
| Percent Demand Served | 70.6% | 1.1% | 68.7% | 71.9% |
| Fuel Used (gallons) | 1,872 | 14 | 1,853 | 1,896 |
| HC Emissions (grams) | 17,012 | 694 | 16,284 | 18,632 |
| CO Emissions (grams) | 487,345 | 12,394 | 471,828 | 514,562 |
| NOx Emissions (grams) | 57,274 | 1,721 | 55,265 | 61,414 |

**SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement**

**Mathilda Avenue Improvements
2040 No Build
PM Peak Hour**

Intersection 1 Mathilda Avenue/5th Avenue Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|--------------|------------|------------------------|---------------------|--------------|-----------------------|-------------|----------|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 140 | 84 | 60.1% | 56.8 | 5.2 | E |
| | Through | 620 | 381 | 61.5% | 22.5 | 3.0 | C |
| | Right Turn | 60 | 40 | 66.2% | 13.9 | 3.3 | B |
| | Subtotal | 820 | 505 | 61.6% | 27.6 | 3.0 | C |
| SB | Left Turn | 20 | 12 | 60.0% | 881.2 | 152.6 | F |
| | Through | 1,120 | 662 | 59.1% | 1028.6 | 183.0 | F |
| | Right Turn | 30 | 16 | 53.3% | 1028.4 | 223.0 | F |
| | Subtotal | 1,170 | 690 | 59.0% | 1025.6 | 182.1 | F |
| EB | Left Turn | 180 | 170 | 94.6% | 50.4 | 10.2 | D |
| | Through | 40 | 38 | 94.8% | 74.1 | 11.7 | E |
| | Right Turn | 170 | 167 | 98.0% | 50.1 | 11.5 | D |
| | Subtotal | 390 | 375 | 96.1% | 52.6 | 10.8 | D |
| WB | Left Turn | 290 | 140 | 48.4% | 1463.1 | 454.6 | F |
| | Through | 20 | 7 | 34.0% | 1462.2 | 512.1 | F |
| | Right Turn | 110 | 55 | 49.5% | 1444.6 | 462.4 | F |
| | Subtotal | 420 | 202 | 48.0% | 1458.1 | 457.8 | F |
| Total | | 2,800 | 1,771 | 63.3% | 565.6 | 60.4 | F |

Intersection 2 Mathilda Avenue/Innovation Way Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|--------------|------------|------------------------|---------------------|--------------|-----------------------|-------------|----------|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 190 | 141 | 74.3% | 80.0 | 4.2 | E |
| | Through | 470 | 340 | 72.4% | 37.2 | 4.9 | D |
| | Right Turn | 180 | 131 | 72.5% | 29.0 | 5.5 | C |
| | Subtotal | 840 | 612 | 72.8% | 45.4 | 3.6 | D |
| SB | Left Turn | 20 | 14 | 68.0% | 376.8 | 46.6 | F |
| | Through | 1,490 | 911 | 61.2% | 417.0 | 41.8 | F |
| | Right Turn | 70 | 41 | 58.7% | 424.6 | 62.9 | F |
| | Subtotal | 1,580 | 966 | 61.1% | 416.6 | 42.0 | F |
| EB | Left Turn | 330 | 146 | 44.2% | 103.9 | 13.9 | F |
| | Through | 50 | 23 | 46.2% | 102.4 | 13.6 | F |
| | Right Turn | 910 | 390 | 42.8% | 109.0 | 16.4 | F |
| | Subtotal | 1,290 | 558 | 43.3% | 107.4 | 15.6 | F |
| WB | Left Turn | 180 | 149 | 82.7% | 146.1 | 50.0 | F |
| | Through | 20 | 17 | 85.5% | 170.2 | 77.8 | F |
| | Right Turn | 20 | 18 | 88.0% | 166.3 | 78.2 | F |
| | Subtotal | 220 | 184 | 83.5% | 150.0 | 52.3 | F |
| Total | | 3,930 | 2,320 | 59.0% | 222.0 | 14.5 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2040 No Build
PM Peak Hour

Intersection 3 Mathilda Avenue/Moffett Park Drive/SR 237 WB Ramps Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-------------------------|--------------------------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn (Moffett Park) | 180 | 133 | 74.1% | 65.9 | 19.0 | E |
| | Left Turn (SR 237 WB On-Ramp) | 110 | 70 | 63.7% | 80.5 | 4.2 | F |
| | Through | 770 | 598 | 77.6% | 50.9 | 14.5 | D |
| | Right Turn (Moffett Park) | 210 | 168 | 79.8% | 36.8 | 13.2 | D |
| | Subtotal | 1,270 | 969 | 76.5% | 52.7 | 13.6 | D |
| SB | Left Turn (Moffett Park) | 60 | 33 | 54.8% | 166.0 | 39.1 | F |
| | Through | 2,290 | 1,266 | 55.3% | 227.9 | 26.6 | F |
| | Right Turn (Moffett Park) | 230 | 146 | 63.3% | 280.9 | 25.0 | F |
| | Right Turn (SR 237 WB On-Ramp) | 560 | 306 | 54.6% | 221.3 | 27.1 | F |
| | Subtotal | 3,140 | 1,750 | 55.8% | 230.0 | 25.0 | F |
| EB (Moffett Park) | Left Turn | 180 | 100 | 55.4% | 338.8 | 55.0 | F |
| | Through | 270 | 161 | 59.6% | 346.0 | 64.9 | F |
| | Right Turn | 640 | 364 | 56.8% | 345.9 | 49.6 | F |
| | Subtotal | 1,090 | 624 | 57.3% | 344.8 | 53.5 | F |
| WB (Moffett Park) | Left Turn | 390 | 291 | 74.5% | 962.2 | 104.5 | F |
| | Through | 330 | 254 | 76.8% | 676.7 | 88.7 | F |
| | Right Turn | 40 | 30 | 75.3% | 662.6 | 92.1 | F |
| | Subtotal | 760 | 574 | 75.6% | 820.5 | 95.2 | F |
| WB (SR 237 WB Off-Ramp) | Left Turn | 820 | 654 | 79.7% | 692.7 | 119.2 | F |
| | Through | | | | | | F |
| | Right Turn | 240 | 187 | 77.7% | 702.7 | 136.8 | F |
| | Subtotal | 1,060 | 840 | 79.3% | 694.9 | 120.6 | F |
| Total | | 7,320 | 4,757 | 65.0% | 454.3 | 34.4 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2040 No Build
PM Peak Hour

Intersection 4 Mathilda Avenue/SR 237 EB Off-Ramp-SR 237 EB On-Ramp Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | 600 | 401 | 66.9% | 39.8 | 7.2 | D |
| | Right Turn | 860 | 587 | 68.2% | 10.0 | 0.9 | A |
| | Subtotal | 1,460 | 988 | 67.7% | 22.0 | 2.6 | C |
| SB | Left Turn | 460 | 275 | 59.8% | 34.0 | 3.1 | C |
| | Through | 3,120 | 1,995 | 63.9% | 15.2 | 0.6 | B |
| | Right Turn | | | | | | |
| | Subtotal | 3,580 | 2,270 | 63.4% | 17.5 | 0.8 | B |
| EB | Left Turn | 280 | 269 | 96.1% | 71.9 | 18.2 | E |
| | Through | | | | | | |
| | Right Turn | 220 | 220 | 100.0% | 58.7 | 38.6 | E |
| | Subtotal | 500 | 489 | 97.8% | 65.8 | 26.9 | E |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 5,540 | 3,748 | 67.6% | 25.0 | 3.7 | C |

Intersection 5 Mathilda Avenue/Ross Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 120 | 77 | 64.2% | 109.3 | 38.0 | F |
| | Through | 1,270 | 872 | 68.7% | 457.4 | 37.1 | F |
| | Right Turn | 350 | 236 | 67.3% | 90.5 | 3.8 | F |
| | Subtotal | 1,740 | 1,185 | 68.1% | 361.9 | 26.1 | F |
| SB | Left Turn | 180 | 121 | 67.3% | 43.3 | 3.1 | D |
| | Through | 3,040 | 2,023 | 66.5% | 12.9 | 1.9 | B |
| | Right Turn | 120 | 75 | 62.3% | 9.8 | 2.8 | A |
| | Subtotal | 3,340 | 2,219 | 66.4% | 14.5 | 1.7 | B |
| EB | Left Turn | 60 | 62 | 104.0% | 56.3 | 7.5 | E |
| | Through | 200 | 196 | 98.2% | 53.7 | 3.6 | D |
| | Right Turn | 60 | 65 | 108.0% | 40.0 | 5.0 | D |
| | Subtotal | 320 | 324 | 101.1% | 51.5 | 3.9 | D |
| WB | Left Turn | 290 | 134 | 46.2% | 1412.8 | 95.3 | F |
| | Through | 70 | 33 | 46.9% | 1391.3 | 156.5 | F |
| | Right Turn | 130 | 59 | 45.5% | 1347.2 | 142.8 | F |
| | Subtotal | 490 | 226 | 46.1% | 1392.3 | 108.2 | F |
| Total | | 5,890 | 3,953 | 67.1% | 200.0 | 9.3 | F |

Intersection 8 **Mathilda Avenue/Almanor Avenue-Ahwanee Avenue** **Signal**

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 80 | 46 | 57.1% | 1156.4 | 90.2 | F |
| | Through | 1,790 | 923 | 51.6% | 1272.9 | 93.0 | F |
| | Right Turn | 60 | 28 | 47.2% | 1489.1 | 94.2 | F |
| | Subtotal | 1,930 | 997 | 51.7% | 1273.6 | 92.7 | F |
| SB | Left Turn | 260 | 198 | 76.2% | 122.4 | 11.2 | F |
| | Through | 2,990 | 2,241 | 74.9% | 115.0 | 16.4 | F |
| | Right Turn | 100 | 76 | 76.2% | 36.9 | 8.8 | D |
| | Subtotal | 3,350 | 2,515 | 75.1% | 113.2 | 15.3 | F |
| EB | Left Turn | 430 | 269 | 62.5% | 1089.2 | 329.9 | F |
| | Through | 40 | 27 | 67.3% | 1045.0 | 324.7 | F |
| | Right Turn | 90 | 55 | 61.1% | 1034.3 | 332.0 | F |
| | Subtotal | 560 | 351 | 62.6% | 1077.0 | 330.0 | F |
| WB | Left Turn | 60 | 54 | 90.5% | 162.2 | 65.6 | F |
| | Through | 30 | 28 | 94.0% | 216.4 | 75.4 | F |
| | Right Turn | 260 | 260 | 99.9% | 216.8 | 89.1 | F |
| | Subtotal | 350 | 342 | 97.8% | 208.3 | 83.9 | F |
| Total | | 6,190 | 4,205 | 67.9% | 471.8 | 29.7 | F |

Intersection 9 **US 101 On-Ramp/Moffett Park Drive** **Signal**

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| EB | Left Turn | | | | | | |
| | Through | 1,010 | 557 | 55.1% | 116.9 | 26.1 | F |
| | Right Turn | 150 | 88 | 58.3% | 60.6 | 15.8 | E |
| | Subtotal | 1,160 | 645 | 55.6% | 109.3 | 24.9 | F |
| WB | Left Turn | 350 | 245 | 70.1% | 28.5 | 2.2 | C |
| | Through | 450 | 314 | 69.7% | 2.2 | 0.2 | A |
| | Right Turn | | | | | | |
| | Subtotal | 800 | 559 | 69.9% | 13.8 | 1.0 | B |
| Total | | 1,960 | 1,204 | 61.4% | 64.3 | 11.2 | E |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2040 No Build
PM Peak Hour

Intersection 10 Innovation Way/Moffett Park Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | 370 | 241 | 65.0% | 375.7 | 51.4 | F |
| | Through | | | | | | |
| | Right Turn | 190 | 121 | 63.7% | 363.0 | 50.2 | F |
| | Subtotal | 560 | 362 | 64.6% | 371.4 | 51.1 | F |
| EB | Left Turn | 60 | 28 | 47.0% | 415.8 | 270.6 | F |
| | Through | 950 | 493 | 51.9% | 371.8 | 54.3 | F |
| | Right Turn | | | | | | |
| | Subtotal | 1,010 | 521 | 51.6% | 370.0 | 53.1 | F |
| WB | Left Turn | | | | | | |
| | Through | 610 | 439 | 72.0% | 29.1 | 15.6 | C |
| | Right Turn | 130 | 83 | 64.0% | 157.9 | 321.0 | F |
| | Subtotal | 740 | 523 | 70.6% | 39.4 | 42.9 | D |
| Total | | 2,310 | 1,406 | 60.8% | 245.4 | 34.3 | F |

Intersection 11 Innovation Way/11th Avenue All-way Stop

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 40 | 20 | 49.8% | 556.7 | 1049.0 | F |
| | Through | 90 | 49 | 54.7% | 704.8 | 1380.9 | F |
| | Right Turn | 20 | 11 | 56.0% | 615.3 | 1243.9 | F |
| | Subtotal | 150 | 80 | 53.5% | 605.1 | 1158.3 | F |
| SB | Left Turn | 30 | 24 | 80.3% | 75.9 | 44.3 | F |
| | Through | 110 | 86 | 78.1% | 144.2 | 80.5 | F |
| | Right Turn | 50 | 39 | 77.6% | 173.7 | 104.7 | F |
| | Subtotal | 190 | 149 | 78.3% | 139.6 | 78.4 | F |
| EB | Left Turn | 500 | 262 | 52.4% | 832.3 | 311.2 | F |
| | Through | | | | | | |
| | Right Turn | 340 | 185 | 54.4% | 824.1 | 344.7 | F |
| | Subtotal | 840 | 447 | 53.2% | 825.8 | 317.3 | F |
| WB | Left Turn | 40 | 39 | 98.3% | 261.0 | 84.6 | F |
| | Through | | | | | | |
| | Right Turn | 20 | 19 | 93.5% | 32.4 | 15.2 | D |
| | Subtotal | 60 | 58 | 96.7% | 185.3 | 52.8 | F |
| Total | | 1,240 | 734 | 59.2% | 545.1 | 173.2 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2040 No Build
PM Peak Hour

Intersection 12

Innovation Way/Juniper Driveway

All-way Stop

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 20 | 11 | 56.0% | 354.8 | 186.6 | F |
| | Through | 590 | 330 | 55.8% | 445.4 | 219.5 | F |
| | Right Turn | | | | | | |
| | Subtotal | 610 | 341 | 55.9% | 442.3 | 217.7 | F |
| SB | Left Turn | | | | | | |
| | Through | 110 | 85 | 76.9% | 86.1 | 24.2 | F |
| | Right Turn | 170 | 115 | 67.7% | 54.1 | 20.5 | F |
| | Subtotal | 280 | 200 | 71.3% | 67.5 | 21.1 | F |
| EB | Left Turn | 700 | 229 | 32.6% | 1585.0 | 102.2 | F |
| | Through | | | | | | |
| | Right Turn | 80 | 71 | 89.3% | 361.9 | 159.4 | F |
| | Subtotal | 780 | 300 | 38.4% | 1295.5 | 90.6 | F |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 1,670 | 840 | 50.3% | 658.8 | 97.2 | F |

Intersection 13

Bordeaux Drive/Innovation Way

All-way Stop

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 60 | 42 | 69.3% | 5.3 | 0.6 | A |
| | Through | 50 | 50 | 100.6% | 4.7 | 0.4 | A |
| | Right Turn | | | | | | |
| | Subtotal | 110 | 92 | 83.5% | 5.0 | 0.3 | A |
| SB | Left Turn | | | | | | |
| | Through | 180 | 91 | 50.7% | 10.9 | 1.4 | B |
| | Right Turn | 40 | 21 | 53.3% | 7.2 | 1.0 | A |
| | Subtotal | 220 | 113 | 51.1% | 10.2 | 1.2 | B |
| EB | Left Turn | 50 | 32 | 64.4% | 6.8 | 0.6 | A |
| | Through | 30 | 19 | 62.3% | 8.2 | 0.4 | A |
| | Right Turn | 70 | 49 | 69.3% | 5.4 | 0.4 | A |
| | Subtotal | 150 | 99 | 66.3% | 6.4 | 0.3 | A |
| WB | Left Turn | | | | | | |
| | Through | 30 | 28 | 92.7% | 5.2 | 0.5 | A |
| | Right Turn | | | | | | |
| | Subtotal | 30 | 28 | 92.7% | 5.2 | 0.5 | A |
| Total | | 510 | 332 | 65.0% | 7.1 | 0.5 | A |

Intersection 1

Mathilda Avenue/5th Avenue

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 625 | 125 | 17 | 225 | 26 | 250 | 34 | 26% | 0% |
| | Through | 625 | 25 | 5 | 75 | 7 | 100 | 16 | 0% | 0% |
| | Right Turn | 625 | 125 | 32 | 275 | 46 | 350 | 58 | 0% | 0% |
| NB | Left Turn | 425 | 75 | 7 | 125 | 16 | 125 | 29 | 0% | 0% |
| | Through | 1,125 | 75 | 10 | 150 | 17 | 200 | 42 | 0% | 0% |
| | Through/Right | 1,125 | 75 | 9 | 175 | 21 | 200 | 33 | 0% | 0% |
| SB | Left Turn | 250 | 75 | 26 | 250 | 55 | 300 | 1 | 0% | 0% |
| | Through | 1,325 | 2,500 | 333 | 4,225 | 469 | 4,600 | 465 | 94% | 0% |
| | Right Turn | 250 | 75 | 17 | 275 | 31 | 300 | 0 | 0% | 0% |
| WB | Left Turn | 925 | 3,700 | 488 | 6,050 | 564 | 5,125 | 316 | 90% | 37% |
| | Through/Right | 75 | 50 | 10 | 100 | 12 | 100 | 0 | 9% | 0% |

Intersection 2

Mathilda Avenue/Innovation Way

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 200 | 75 | 14 | 175 | 14 | 175 | 18 | 0% | 36% |
| | Through/Right | 225 | 25 | 3 | 50 | 8 | 75 | 19 | 0% | 46% |
| | Right Turn | 225 | 250 | 14 | 325 | 14 | 325 | 22 | 0% | 55% |
| NB | Left Turn | 400 | 75 | 11 | 150 | 19 | 175 | 34 | 0% | 0% |
| | Through | 975 | 100 | 10 | 175 | 22 | 225 | 33 | 0% | 0% |
| | Through/Right | 975 | 150 | 21 | 275 | 40 | 300 | 47 | 0% | 0% |
| SB | Left Turn | 225 | 25 | 7 | 100 | 16 | 150 | 0 | 0% | 0% |
| | Through | 75 | 1,200 | 2 | 1,200 | 6 | 1,225 | 15 | 90% | 66% |
| | Right Turn | 975 | 150 | 22 | 350 | 21 | 275 | 0 | 0% | 0% |
| WB | Left Turn | 425 | 200 | 50 | 450 | 71 | 575 | 41 | 8% | 0% |
| | Shared | 225 | 125 | 27 | 225 | 28 | 225 | 0 | 14% | 0% |

Intersection 3

Mathilda Avenue/Moffett Park Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-------------------------|-----------------------------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB (Moffett Park) | Left Turn | 525 | 225 | 56 | 400 | 60 | 375 | 2 | 1% | 0% |
| | Through/Right | 1,125 | 1,150 | 21 | 1,175 | 17 | 1,175 | 16 | 0% | 55% |
| | Right Turn | 1,125 | 1,150 | 4 | 1,150 | 9 | 1,175 | 13 | 0% | 53% |
| NB | Left Turn (Moffett Park) | 125 | 25 | 4 | 50 | 6 | 75 | 9 | 0% | 12% |
| | Through | 300 | 150 | 21 | 275 | 48 | 300 | 86 | 0% | 36% |
| | Through/Right (Moffett Park) | 300 | 150 | 17 | 275 | 39 | 300 | 78 | 0% | 36% |
| | Left Turn (SR 237 WB On-Ramp) | 175 | 75 | 9 | 150 | 20 | 175 | 27 | 0% | 1% |
| SB | Left Turn (Moffett Park) | 175 | 50 | 7 | 100 | 20 | 150 | 56 | 0% | 0% |
| | Through | 1,100 | 1,125 | 64 | 1,250 | 64 | 1,200 | 23 | 66% | 53% |
| | Through/Right (Moffett Park) | 975 | 1,075 | 4 | 1,100 | 13 | 1,125 | 11 | 0% | 49% |
| WB (Moffett Park) | Through/Right (SR 237 WB On-Ramp) | 1,100 | 1,125 | 60 | 1,225 | 59 | 1,200 | 23 | 66% | 57% |
| | Left Turn | 300 | 3,800 | 214 | 5,825 | 255 | 5,950 | 252 | 96% | 0% |
| WB (SR 237 WB Off-Ramp) | Through/Right | 675 | 650 | 1 | 650 | 2 | 650 | 2 | 24% | 54% |
| | Left Turn | 1,075 | 5,425 | 1,272 | 8,525 | 1,393 | 8,550 | 1,278 | 63% | 0% |
| | Left/Through | 325 | 450 | 1 | 450 | 4 | 450 | 0 | 62% | 0% |
| | Right Turn | 325 | 350 | 26 | 475 | 20 | 375 | 0 | 17% | 0% |

Intersection 4

Mathilda Avenue/SR 237 EB Off-Ramp-SR 237 EB On-Ramp

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,025 | 175 | 77 | 375 | 253 | 625 | 308 | 0% | 0% |
| | Shared | 1,025 | 200 | 39 | 400 | 89 | 450 | 95 | 5% | 0% |
| NB | Through | 275 | 50 | 10 | 100 | 24 | 150 | 62 | 0% | 0% |
| | Right Turn | 275 | 75 | 18 | 200 | 34 | 275 | 32 | 0% | 1% |
| SB | Left Turn | 175 | 100 | 12 | 175 | 15 | 200 | 12 | 0% | 5% |
| | Through | 175 | 200 | 8 | 225 | 13 | 225 | 10 | 0% | 18% |
| | | | | | | | | | | |

Intersection 5

Mathilda Avenue/Ross Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 250 | 250 | 28 | 400 | 40 | 450 | 44 | 36% | 0% |
| | Through | 1,575 | 100 | 2 | 125 | 6 | 100 | 0 | 63% | 0% |
| | Right Turn | 50 | 50 | 3 | 75 | 4 | 75 | 4 | 12% | 0% |
| NB | Left Turn | 150 | 100 | 23 | 200 | 40 | 225 | 24 | 14% | 0% |
| | Through | 2,200 | 1,025 | 50 | 1,100 | 101 | 1,100 | 137 | 0% | 51% |
| | Through/Right | 450 | 525 | 2 | 550 | 7 | 575 | 6 | 0% | 82% |
| SB | Left Turn | 225 | 100 | 9 | 175 | 16 | 200 | 29 | 10% | 0% |
| | Through | 225 | 150 | 14 | 250 | 23 | 275 | 19 | 5% | 1% |
| | Through/Right | 225 | 150 | 15 | 250 | 23 | 300 | 1 | 0% | 5% |
| WB | Left Turn | 100 | 6,300 | 587 | 9,575 | 904 | 9,725 | 819 | 87% | 0% |
| | Through | 225 | 75 | 5 | 150 | 3 | 100 | 0 | 5% | 0% |
| | Right Turn | 100 | 50 | 8 | 100 | 9 | 75 | 1 | 4% | 0% |

Intersection 8

Mathilda Avenue/Almanor Avenue-Ahwanee Avenue

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,025 | 350 | 31 | 350 | 28 | 350 | 13 | 89% | 79% |
| | Through/Right | 125 | 125 | 23 | 300 | 15 | 225 | 0 | 7% | 0% |
| NB | Left Turn | 425 | 100 | 26 | 275 | 67 | 375 | 3 | 0% | 0% |
| | Through | 750 | 4,725 | 35 | 7,725 | 57 | 7,675 | 17 | 86% | 0% |
| | Right Turn | 75 | 25 | 9 | 100 | 18 | 100 | 0 | 0% | 0% |
| SB | Left Turn | 125 | 175 | 5 | 200 | 6 | 175 | 0 | 58% | 0% |
| | Through | 2,225 | 1,400 | 46 | 1,775 | 54 | 1,900 | 27 | 36% | 0% |
| | Through/Right | 2,225 | 375 | 51 | 525 | 59 | 525 | 34 | 0% | 0% |
| WB | Left Turn | 250 | 175 | 42 | 400 | 69 | 375 | 0 | 1% | 0% |
| | Through | 1,025 | 600 | 214 | 1,025 | 249 | 975 | 147 | 8% | 0% |
| | Right Turn | 75 | 125 | 3 | 125 | 7 | 125 | 0 | 82% | 0% |

Intersection 9

US 101 On-Ramp/Moffett Park Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Through | 850 | 700 | 64 | 1,125 | 33 | 900 | 2 | 63% | 15% |
| | Right Turn | 150 | 200 | 38 | 475 | 36 | 375 | 0 | 0% | 0% |
| WB | Left Turn | 850 | 150 | 8 | 250 | 28 | 300 | 40 | 0% | 0% |
| | Through | 850 | 25 | 1 | 25 | 12 | 25 | 34 | 0% | 0% |
| | | | | | | | | | | |
| | | | | | | | | | | |

Intersection 10

Innovation Way/Moffett Park Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 225 | 175 | 33 | 425 | 36 | 350 | 0 | 7% | 0% |
| | Through | 850 | 850 | 52 | 1,050 | 77 | 925 | 9 | 87% | 31% |
| SB | Left Turn | 575 | 500 | 13 | 575 | 17 | 550 | 19 | 0% | 61% |
| | Shared | 575 | 525 | 7 | 575 | 10 | 550 | 10 | 0% | 66% |
| WB | Through | 1,150 | 200 | 153 | 400 | 372 | 400 | 314 | 1% | 5% |
| | Right Turn | 1,150 | 50 | 48 | 125 | 93 | 200 | 68 | 11% | 0% |
| | | | | | | | | | | |

Intersection 11

Innovation Way/11th Avenue

All-way Stop

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 125 | 125 | 10 | 200 | 8 | 150 | 0 | 58% | 0% |
| | Through/Right | 325 | 3,075 | 1,111 | 5,850 | 1,571 | 5,850 | 1,285 | 45% | 0% |
| | Right Turn | 325 | 2,650 | 1,026 | 5,250 | 1,409 | 5,400 | 888 | 0% | 0% |
| NB | Left Turn | 125 | 25 | 2 | 25 | 15 | 75 | 44 | 0% | 0% |
| | Left/Through | 575 | 150 | 103 | 300 | 148 | 325 | 99 | 18% | 12% |
| | Through/Right | 575 | 125 | 98 | 225 | 143 | 250 | 107 | 0% | 7% |
| SB | Left/Through | 1,000 | 100 | 47 | 250 | 126 | 375 | 184 | 0% | 0% |
| | Through/Right | 1,000 | 150 | 65 | 350 | 137 | 425 | 178 | 0% | 0% |
| WB | Left Turn | 325 | 125 | 29 | 225 | 48 | 250 | 42 | 0% | 0% |
| | Through/Right | 325 | 25 | 4 | 50 | 7 | 75 | 10 | 0% | 0% |

Intersection 12

Innovation Way/Juniper Driveway

All-way Stop

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 200 | 9,425 | 707 | 14,950 | 1,052 | 15,225 | 1,081 | 0% | 0% |
| | Right Turn | 200 | 1,825 | 907 | 4,550 | 3,992 | 7,225 | 7,034 | 0% | 0% |
| NB | Left Turn | 125 | 50 | 19 | 175 | 38 | 175 | 0 | 0% | 0% |
| | Through | 1,000 | 650 | 215 | 1,100 | 242 | 1,100 | 204 | 89% | 77% |
| SB | Through/Right | 300 | 200 | 26 | 225 | 54 | 250 | 81 | 0% | 4% |
| | Right Turn | 300 | 200 | 40 | 250 | 55 | 250 | 28 | 0% | 1% |
| | | | | | | | | | | |

Intersection 13

Bordeaux Drive/Innovation Way

All-way Stop

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left/Through | 375 | 50 | 3 | 75 | 5 | 75 | 16 | 0% | 0% |
| | Right Turn | 125 | 25 | 3 | 75 | 5 | 75 | 20 | 0% | 0% |
| NB | Left Turn | 325 | 25 | 3 | 50 | 3 | 75 | 17 | 0% | 0% |
| | Through/Right | 2,025 | 25 | 2 | 50 | 4 | 75 | 11 | 0% | 0% |
| SB | Left Turn | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | Through/Right | 725 | 50 | 7 | 75 | 9 | 100 | 12 | 0% | 0% |
| WB | Left/Through | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | Right Turn | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |

Arterial Level of Service: NB Mathilda Ave

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|----------------------|------|---------------|-----------------|------------|----------------|
| Ahwanee Ave | 8 | 236.6 | 247.0 | 0.1 | 2 |
| US 101 SB Diag. On-R | 702 | 27.2 | 33.7 | 0.1 | 9 |
| US 101 SB Loop On-Ra | 701 | 124.8 | 132.3 | 0.1 | 3 |
| US 101 NB Loop On-Ra | 602 | 92.5 | 98.1 | 0.1 | 2 |
| US 101 NB Diag.Off-R | 601 | 129.2 | 136.0 | 0.1 | 2 |
| Ross Dr | 5 | 75.7 | 83.4 | 0.1 | 4 |
| SR 237 EB On-Ramp | 4 | 36.9 | 42.1 | 0.1 | 6 |
| SR 237 WB Off-Ramp | 33 | 18.8 | 22.6 | 0.0 | 8 |
| Moffett Park Dr | 3 | 30.7 | 33.5 | 0.0 | 4 |
| Innovation Way | 2 | 38.1 | 55.0 | 0.2 | 14 |
| 5th Ave | 1 | 23.5 | 42.5 | 0.2 | 20 |
| | 107 | 4.2 | 26.4 | 0.3 | 37 |
| Total | | 838.3 | 952.6 | 1.5 | 5 |

Arterial Level of Service: SB Mathilda Ave

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|----------------------|------|---------------|-----------------|------------|----------------|
| 5th Ave | 1 | 629.0 | 647.8 | 0.3 | 2 |
| Innovation Way | 2 | 381.9 | 397.5 | 0.2 | 2 |
| Moffett Park Dr | 3 | 202.2 | 218.2 | 0.2 | 4 |
| SR 237 WB On-Ramp | 33 | 3.1 | 6.1 | 0.0 | 24 |
| SR 237 Off/On Ramp | 4 | 4.1 | 8.3 | 0.0 | 21 |
| Ross Dr | 5 | 10.9 | 15.9 | 0.1 | 15 |
| US 101 NB Diag.Off-R | 601 | 29.2 | 37.4 | 0.1 | 9 |
| US 101 NB Loop Off-R | 602 | 18.3 | 24.0 | 0.1 | 14 |
| US 101 SB Loop On-Ra | 701 | 6.2 | 12.3 | 0.1 | 19 |
| US 101 SB Off-Ramp | 702 | 7.8 | 14.4 | 0.1 | 26 |
| Almanor Ave | 8 | 51.2 | 59.3 | 0.1 | 5 |
| San Aleso Ave | 201 | 6.0 | 17.3 | 0.1 | 29 |
| Total | | 1350.0 | 1458.5 | 1.5 | 4 |

Arterial Level of Service: NB Innovation Way

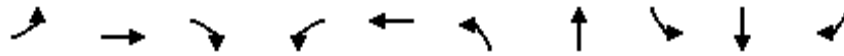
| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|------------------|------|---------------|-----------------|-----------|----------------|
| | 910 | 24.3 | 26.2 | 0.0 | 3 |
| | 38 | 44.3 | 50.4 | 0.0 | 3 |
| | 11 | 244.1 | 253.7 | 0.1 | 1 |
| | 200 | 132.9 | 148.0 | 0.2 | 4 |
| Juniper Driveway | 12 | 200.9 | 208.5 | 0.1 | 1 |
| Driveway | 217 | 37.0 | 41.1 | 0.0 | 3 |
| | 902 | 56.3 | 60.0 | 0.0 | 1 |
| Mathilda Ave | 2 | 7.9 | 10.1 | 0.0 | 9 |
| | 53 | 1.5 | 14.5 | 0.1 | 24 |
| Bordeaux Dr | 13 | 6.5 | 15.9 | 0.1 | 18 |
| Total | | 755.7 | 828.4 | 0.6 | 3 |

Arterial Level of Service: SB Innovation Way

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|------------------|------|---------------|-----------------|-----------|----------------|
| | 53 | 15.5 | 27.1 | 0.1 | 10 |
| Mathilda Ave | 2 | 139.6 | 149.7 | 0.1 | 2 |
| | 902 | 8.0 | 12.3 | 0.0 | 8 |
| Driveway | 217 | 1.8 | 4.3 | 0.0 | 17 |
| Juniper Driveway | 12 | 82.0 | 87.5 | 0.0 | 2 |
| | 200 | 1.9 | 11.0 | 0.1 | 19 |
| 11th Ave | 11 | 145.4 | 167.1 | 0.2 | 3 |
| | 38 | 201.4 | 209.0 | 0.1 | 1 |
| | 910 | 115.7 | 120.7 | 0.0 | 1 |
| Moffett Park Dr | 10 | 19.6 | 22.8 | 0.0 | 4 |
| Total | | 730.8 | 811.5 | 0.6 | 3 |

Lanes, Volumes, Timings
1: Mathilda Ave & 5th Ave

3/4/2016

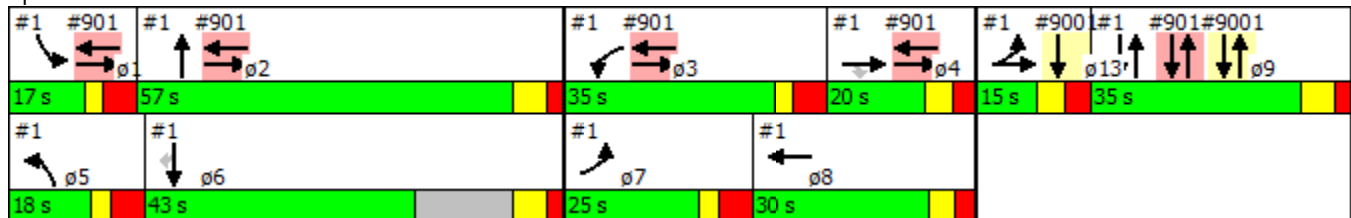


| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT | SBR | ø2 | ø7 |
|----------------------|------|------|--------|-------|-------|-------|-----|------|-----|--------|------|------|
| Lane Configurations | ↔↔ | ↑ | ↗ | ↔↔ | ↖ | ↔↔ | ↕↕↖ | ↗ | ↕↕↕ | ↗ | | |
| Volume (vph) | 30 | 30 | 90 | 60 | 30 | 200 | 860 | 40 | 520 | 110 | | |
| Turn Type | Prot | NA | custom | Prot | NA | Prot | NA | Prot | NA | custom | | |
| Protected Phases | 7 13 | 4 13 | | 3 | 8 | 5 | 2 9 | 1 | 6 9 | | 2 | 7 |
| Permitted Phases | | | 4 | | | | | | | 6 | | |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 5 | 2 | 1 | 6 | 6 | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 13.0 | 12.0 | 8.0 | 11.0 | | 10.0 | | 12.0 | 12.0 | 12.0 |
| Minimum Split (s) | | | 20.0 | 19.0 | 29.5 | 18.0 | | 17.0 | | 41.0 | 37.0 | 19.0 |
| Total Split (s) | | | 20.0 | 35.0 | 30.0 | 18.0 | | 17.0 | | 43.0 | 57.0 | 25.0 |
| Total Split (%) | | | 11.2% | 19.6% | 16.8% | 10.1% | | 9.5% | | 24.0% | 32% | 14% |
| Yellow Time (s) | | | 3.6 | 2.5 | 3.6 | 2.5 | | 2.5 | | 4.7 | 4.7 | 2.5 |
| All-Red Time (s) | | | 3.4 | 4.5 | 2.9 | 4.5 | | 4.5 | | 2.3 | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | | 0.0 | | |
| Total Lost Time (s) | | | 7.0 | 7.0 | 6.5 | 7.0 | | 7.0 | | 7.0 | | |
| Lead/Lag | | | Lag | Lead | Lag | Lead | | Lead | | Lag | Lag | Lead |
| Lead-Lag Optimize? | | | Yes | Yes | Yes | Yes | | Yes | | Yes | Yes | Yes |
| Recall Mode | | | None | None | None | None | | None | | None | Min | None |

Intersection Summary

Cycle Length: 179
 Actuated Cycle Length: 105.4
 Natural Cycle: 160
 Control Type: Actuated-Uncoordinated

Splits and Phases: 1: Mathilda Ave & 5th Ave



| Lane Group | ø9 | ø13 |
|----------------------|------|------|
| Lane Configurations | | |
| Volume (vph) | | |
| Turn Type | | |
| Protected Phases | 9 | 13 |
| Permitted Phases | | |
| Detector Phase | | |
| Switch Phase | | |
| Minimum Initial (s) | 28.0 | 8.0 |
| Minimum Split (s) | 35.0 | 15.0 |
| Total Split (s) | 35.0 | 15.0 |
| Total Split (%) | 20% | 8% |
| Yellow Time (s) | 4.7 | 3.6 |
| All-Red Time (s) | 2.3 | 3.4 |
| Lost Time Adjust (s) | | |
| Total Lost Time (s) | | |
| Lead/Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes |
| Recall Mode | None | None |
| Intersection Summary | | |

Lanes, Volumes, Timings
 2: Mathilda Ave & Innovation Way

3/4/2016

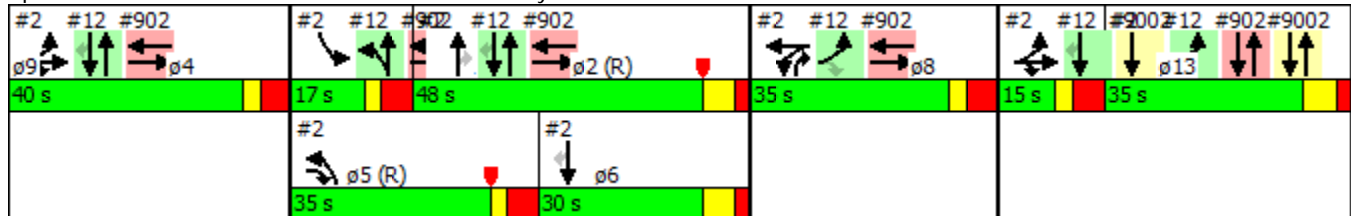


| Lane Group | EBT | EBR | WBL | WBT | NBL | NBT | NBR | SBL | SBT | SBR | ø2 | ø4 |
|----------------------|------|--------|-------|-------|-------|------|-------|------|-----|------|-------|------|
| Lane Configurations | ↕ | ↕↕ | ↕ | ↕↕ | ↕↕ | ↕↕ | ↕ | ↕ | ↕↕↕ | ↕ | | |
| Volume (vph) | 90 | 110 | 360 | 180 | 760 | 1020 | 1240 | 50 | 390 | 230 | | |
| Turn Type | NA | pt+ov | Split | NA | Prot | NA | pm+ov | Prot | NA | Perm | | |
| Protected Phases | 4 13 | 4 13 5 | 8 | 8 | 5 | 2 9 | 8 | 1 | 6 9 | | 2 | 4 |
| Permitted Phases | | | | | | | 2 9 | | | 6 9 | | |
| Detector Phase | 4 | 4 | 8 | 8 | 5 | 2 | 2 | 1 | 6 | 6 | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 10.0 | 10.0 | 13.0 | | 10.0 | 10.0 | | | 12.0 | 14.0 |
| Minimum Split (s) | | | 35.0 | 35.0 | 20.0 | | 35.0 | 16.8 | | | 19.0 | 39.0 |
| Total Split (s) | | | 35.0 | 35.0 | 35.0 | | 35.0 | 17.0 | | | 48.0 | 40.0 |
| Total Split (%) | | | 18.4% | 18.4% | 18.4% | | 18.4% | 8.9% | | | 25% | 21% |
| Yellow Time (s) | | | 2.5 | 2.5 | 2.5 | | 2.5 | 2.5 | | | 4.7 | 2.5 |
| All-Red Time (s) | | | 4.5 | 4.5 | 4.5 | | 4.5 | 4.3 | | | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | | | | |
| Total Lost Time (s) | | | 7.0 | 7.0 | 7.0 | | 7.0 | 6.8 | | | | |
| Lead/Lag | | | | | Lead | | | Lead | | | Lag | |
| Lead-Lag Optimize? | | | | | Yes | | | Yes | | | Yes | |
| Recall Mode | | | None | None | C-Max | | None | None | | | C-Max | None |

Intersection Summary

Cycle Length: 190
 Actuated Cycle Length: 190
 Offset: 133 (70%), Referenced to phase 2:NBT and 5:NBL, Start of Yellow
 Natural Cycle: 175
 Control Type: Actuated-Coordinated

Splits and Phases: 2: Mathilda Ave & Innovation Way



Lanes, Volumes, Timings
 2: Mathilda Ave & Innovation Way

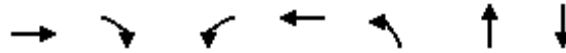
3/4/2016

| Lane Group | ø6 | ø9 | ø13 |
|----------------------|------|------|------|
| Lane Configurations | | | |
| Volume (vph) | | | |
| Turn Type | | | |
| Protected Phases | 6 | 9 | 13 |
| Permitted Phases | | | |
| Detector Phase | | | |
| Switch Phase | | | |
| Minimum Initial (s) | 12.0 | 28.0 | 8.0 |
| Minimum Split (s) | 30.0 | 35.0 | 15.0 |
| Total Split (s) | 30.0 | 35.0 | 15.0 |
| Total Split (%) | 16% | 18% | 8% |
| Yellow Time (s) | 4.7 | 4.7 | 2.5 |
| All-Red Time (s) | 2.3 | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | |
| Total Lost Time (s) | | | |
| Lead/Lag | Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes | Yes |
| Recall Mode | Min | None | None |
| Intersection Summary | | | |

Lanes, Volumes, Timings

3: Mathilda Ave & Moffett Park Dr/SR 237 WB Off-Ramp

3/4/2016

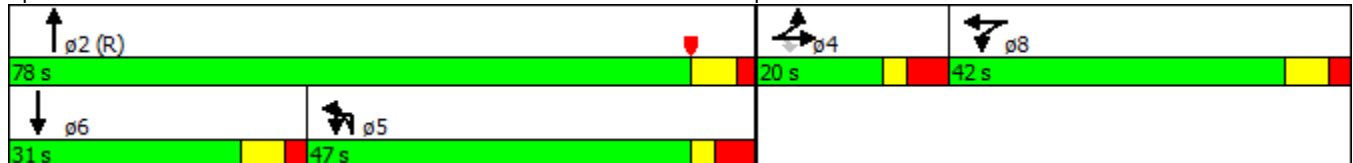


| Lane Group | EBT | EBR | WBL | WBT | NBL | NBT | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | |
| Volume (vph) | 0 | 110 | 670 | 300 | 920 | 2660 | 540 |
| Turn Type | NA | Perm | Split | NA | Prot | NA | NA |
| Protected Phases | 4 | | 8 | 8 | 5 | 2 | 6 |
| Permitted Phases | | 4 | | | | | |
| Detector Phase | 4 | 4 | 8 | 8 | 5 | 2 | 6 |
| Switch Phase | | | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 8.0 | 8.0 |
| Minimum Split (s) | 11.0 | 11.0 | 40.0 | 40.0 | 11.0 | 26.9 | 14.9 |
| Total Split (s) | 20.0 | 20.0 | 42.0 | 42.0 | 47.0 | 78.0 | 31.0 |
| Total Split (%) | 14.3% | 14.3% | 30.0% | 30.0% | 33.6% | 55.7% | 22.1% |
| Yellow Time (s) | 2.5 | 2.5 | 4.5 | 4.5 | 2.5 | 4.7 | 4.7 |
| All-Red Time (s) | 4.5 | 4.5 | 2.5 | 2.5 | 4.5 | 2.2 | 2.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.9 | 6.9 |
| Lead/Lag | | | | | Lag | | Lead |
| Lead-Lag Optimize? | | | | | Yes | | Yes |
| Recall Mode | Max | Max | Max | Max | None | C-Max | None |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 130 (93%), Referenced to phase 2:NBT, Start of Yellow
 Natural Cycle: 130
 Control Type: Actuated-Coordinated

Splits and Phases: 3: Mathilda Ave & Moffett Park Dr/SR 237 WB Off-Ramp



Lanes, Volumes, Timings
 4: Mathilda Ave & SR 237 EB Ramps

3/4/2016

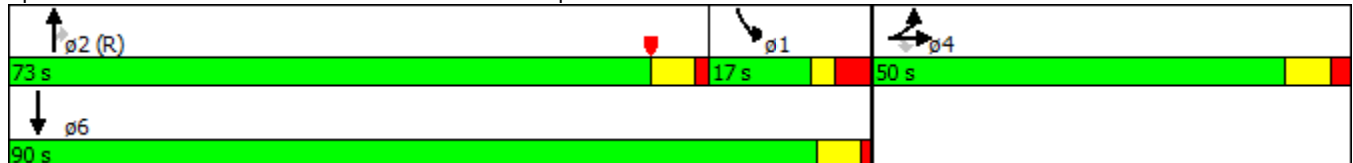


| Lane Group | EBL | EBT | EBR | NBT | NBR | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↶ | ↷ | ↷ | ↑↑↑↑ | ↷↷ | ↶ | ↑↑↑ |
| Volume (vph) | 780 | 0 | 70 | 2980 | 920 | 80 | 1050 |
| Turn Type | Split | NA | Perm | NA | Perm | Prot | NA |
| Protected Phases | 4 | 4 | | 2 | | 1 | 6 |
| Permitted Phases | | | 4 | | 2 | | |
| Detector Phase | 4 | 4 | 4 | 2 | 2 | 1 | 6 |
| Switch Phase | | | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 4.0 | 8.0 | 8.0 | 4.0 | 8.0 |
| Minimum Split (s) | 11.0 | 11.0 | 11.0 | 18.2 | 18.2 | 10.4 | 13.9 |
| Total Split (s) | 50.0 | 50.0 | 50.0 | 73.0 | 73.0 | 17.0 | 90.0 |
| Total Split (%) | 35.7% | 35.7% | 35.7% | 52.1% | 52.1% | 12.1% | 64.3% |
| Yellow Time (s) | 4.8 | 4.8 | 4.8 | 4.7 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 2.2 | 2.2 | 2.2 | 1.5 | 1.5 | 3.9 | 1.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 6.2 | 6.2 | 6.4 | 5.9 |
| Lead/Lag | | | | Lead | Lead | Lag | |
| Lead-Lag Optimize? | | | | Yes | Yes | Yes | |
| Recall Mode | Max | Max | Max | C-Max | C-Max | None | Max |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 135 (96%), Referenced to phase 2:NBT, Start of Yellow
 Natural Cycle: 90
 Control Type: Actuated-Coordinated

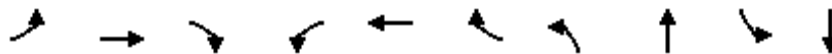
Splits and Phases: 4: Mathilda Ave & SR 237 EB Ramps



Lanes, Volumes, Timings

5: Mathilda Ave & Ross Dr

3/4/2016

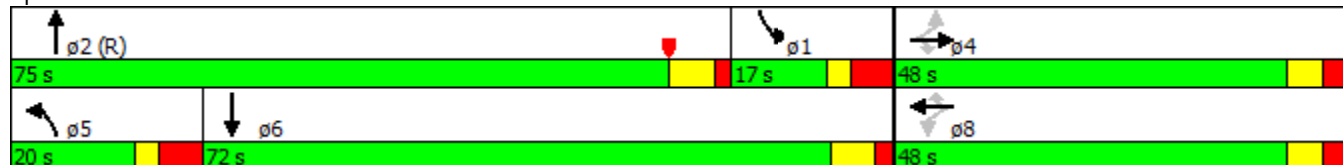


| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | | |
| Volume (vph) | 90 | 70 | 40 | 130 | 40 | 300 | 80 | 3510 | 70 | 1000 |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | Prot | NA | Prot | NA |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | 1 | 6 |
| Permitted Phases | 4 | | 4 | 8 | | 8 | | | | |
| Detector Phase | 4 | 4 | 4 | 8 | 8 | 8 | 5 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 4.0 | 5.0 | 4.0 | 5.0 |
| Minimum Split (s) | 48.0 | 48.0 | 48.0 | 19.0 | 19.0 | 19.0 | 11.0 | 31.4 | 11.0 | 11.6 |
| Total Split (s) | 48.0 | 48.0 | 48.0 | 48.0 | 48.0 | 48.0 | 20.0 | 75.0 | 17.0 | 72.0 |
| Total Split (%) | 34.3% | 34.3% | 34.3% | 34.3% | 34.3% | 34.3% | 14.3% | 53.6% | 12.1% | 51.4% |
| Yellow Time (s) | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 2.5 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 3.4 | 3.4 | 3.4 | 3.4 | 3.4 | 3.4 | 4.5 | 1.7 | 4.5 | 1.9 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.4 | 7.0 | 6.6 |
| Lead/Lag | | | | | | | Lead | Lead | Lag | Lag |
| Lead-Lag Optimize? | | | | | | | Yes | Yes | Yes | Yes |
| Recall Mode | Max | Max | Max | None | None | None | None | C-Max | Max | None |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 0 (0%), Referenced to phase 2:NBT, Start of Yellow, Master Intersection
 Natural Cycle: 125
 Control Type: Actuated-Coordinated

Splits and Phases: 5: Mathilda Ave & Ross Dr



Lanes, Volumes, Timings
 6: Mathilda Ave & US 101 NB Ramps

3/4/2016



| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↖↗ | ↖↗ | ↑↑↑ | ↗ | ↖ | ↑↑↑ |
| Volume (vph) | 770 | 780 | 2930 | 570 | 20 | 1150 |
| Turn Type | Prot | pm+ov | NA | Perm | Prot | NA |
| Protected Phases | 8 | 1 | 2 | | 1 | 6 |
| Permitted Phases | | 8 | | 2 | | |
| Detector Phase | 8 | 1 | 2 | 2 | 1 | 6 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 8.0 | 4.0 | 8.0 | 8.0 | 4.0 | 4.0 |
| Minimum Split (s) | 14.9 | 9.7 | 39.9 | 39.9 | 9.7 | 10.9 |
| Total Split (s) | 44.0 | 16.0 | 80.0 | 80.0 | 16.0 | 96.0 |
| Total Split (%) | 31.4% | 11.4% | 57.1% | 57.1% | 11.4% | 68.6% |
| Yellow Time (s) | 4.7 | 3.5 | 4.7 | 4.7 | 3.5 | 4.7 |
| All-Red Time (s) | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.9 | 5.7 | 6.9 | 6.9 | 5.7 | 6.9 |
| Lead/Lag | | Lead | Lag | Lag | Lead | |
| Lead-Lag Optimize? | | Yes | Yes | Yes | Yes | |
| Recall Mode | None | None | C-Max | C-Max | None | None |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 118 (84%), Referenced to phase 2:NBT, Start of Yellow
 Natural Cycle: 150
 Control Type: Actuated-Coordinated

Splits and Phases: 6: Mathilda Ave & US 101 NB Ramps



Lanes, Volumes, Timings
 7: Mathilda Ave & US 101 SB Ramps

3/4/2016



| Lane Group | EBL | EBR | NBT | NBR | SBT |
|----------------------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | |
| Volume (vph) | 380 | 520 | 3120 | 700 | 1730 |
| Turn Type | Prot | Prot | NA | Perm | NA |
| Protected Phases | 7 | 7 | 2 | | 6 |
| Permitted Phases | | | | 2 | |
| Detector Phase | 7 | 7 | 2 | 2 | 6 |
| Switch Phase | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 8.0 | 8.0 | 8.0 |
| Minimum Split (s) | 10.9 | 10.9 | 14.9 | 14.9 | 14.9 |
| Total Split (s) | 40.0 | 40.0 | 100.0 | 100.0 | 100.0 |
| Total Split (%) | 28.6% | 28.6% | 71.4% | 71.4% | 71.4% |
| Yellow Time (s) | 4.7 | 4.7 | 4.7 | 4.7 | 4.7 |
| All-Red Time (s) | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.9 | 6.9 | 6.9 | 6.9 | 6.9 |
| Lead/Lag | | | | | |
| Lead-Lag Optimize? | | | | | |
| Recall Mode | None | None | C-Max | C-Max | None |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 117 (84%), Referenced to phase 2:NBT, Start of Yellow
 Natural Cycle: 90
 Control Type: Actuated-Coordinated

Splits and Phases: 7: Mathilda Ave & US 101 SB Ramps



Lanes, Volumes, Timings
 8: Mathilda Ave & Almanor Ave/Ahwanee Ave

3/4/2016

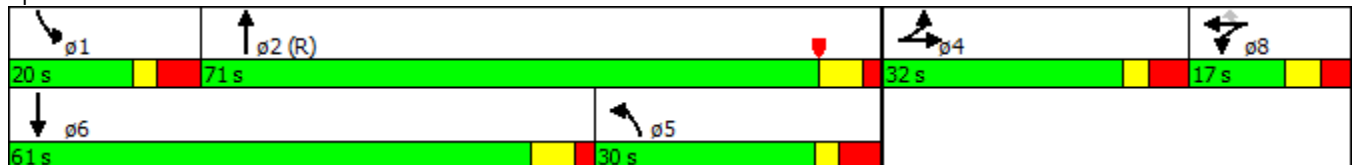


| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | |
| Volume (vph) | 130 | 30 | 90 | 50 | 260 | 140 | 3430 | 160 | 1760 |
| Turn Type | Split | NA | Split | NA | Perm | Prot | NA | Prot | NA |
| Protected Phases | 4 | 4 | 8 | 8 | | 5 | 2 | 1 | 6 |
| Permitted Phases | | | | | 8 | | | | |
| Detector Phase | 4 | 4 | 8 | 8 | 8 | 5 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | | |
| Minimum Initial (s) | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 12.0 | 8.0 | 12.0 |
| Minimum Split (s) | 32.0 | 32.0 | 15.0 | 15.0 | 15.0 | 15.0 | 36.7 | 15.0 | 18.7 |
| Total Split (s) | 32.0 | 32.0 | 17.0 | 17.0 | 17.0 | 30.0 | 71.0 | 20.0 | 61.0 |
| Total Split (%) | 22.9% | 22.9% | 12.1% | 12.1% | 12.1% | 21.4% | 50.7% | 14.3% | 43.6% |
| Yellow Time (s) | 2.8 | 2.8 | 3.6 | 3.6 | 3.6 | 2.5 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 4.2 | 4.2 | 3.4 | 3.4 | 3.4 | 4.5 | 2.0 | 4.5 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.7 | 7.0 | 6.7 |
| Lead/Lag | | | | | | Lag | Lag | Lead | Lead |
| Lead-Lag Optimize? | | | | | | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | None | C-Max | None | None |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 103 (74%), Referenced to phase 2:NBT, Start of Yellow
 Natural Cycle: 150
 Control Type: Actuated-Coordinated

Splits and Phases: 8: Mathilda Ave & Almanor Ave/Ahwanee Ave



Lanes, Volumes, Timings
 9: US 101 On-Ramp & Moffett Park Dr

3/4/2016

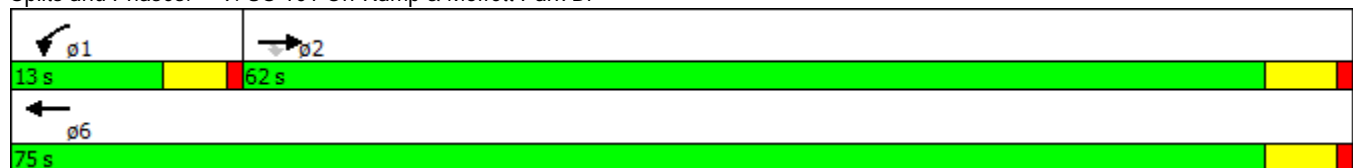


| Lane Group | EBT | EBR | WBL | WBT |
|----------------------|-------|-------|-------|--------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ |
| Volume (vph) | 230 | 20 | 40 | 990 |
| Turn Type | NA | Perm | Prot | NA |
| Protected Phases | 2 | | 1 | 6 |
| Permitted Phases | | 2 | | |
| Detector Phase | 2 | 2 | 1 | 6 |
| Switch Phase | | | | |
| Minimum Initial (s) | 15.0 | 15.0 | 6.0 | 15.0 |
| Minimum Split (s) | 20.0 | 20.0 | 10.5 | 20.0 |
| Total Split (s) | 62.0 | 62.0 | 13.0 | 75.0 |
| Total Split (%) | 82.7% | 82.7% | 17.3% | 100.0% |
| Yellow Time (s) | 4.0 | 4.0 | 3.5 | 4.0 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.0 | 5.0 | 4.5 | 5.0 |
| Lead/Lag | Lag | Lag | Lead | |
| Lead-Lag Optimize? | | | | |
| Recall Mode | Min | Min | None | Min |

Intersection Summary

Cycle Length: 75
 Actuated Cycle Length: 41.3
 Natural Cycle: 40
 Control Type: Semi Act-Uncoord

Splits and Phases: 9: US 101 On-Ramp & Moffett Park Dr



Lanes, Volumes, Timings
 10: Moffett Park Dr & Innovation Way

3/4/2016

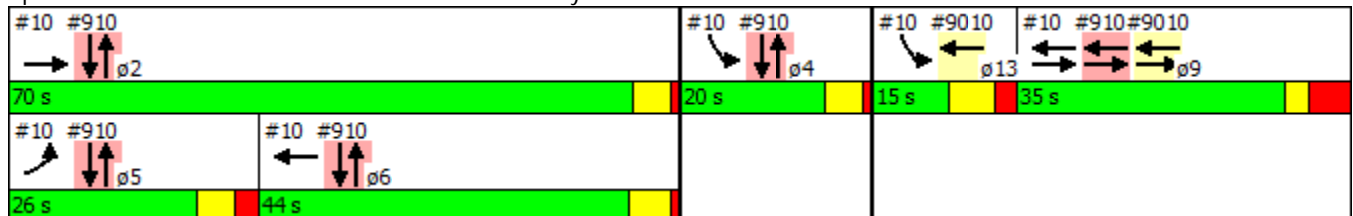


| Lane Group | EBL | EBT | WBT | SBL | ø2 | ø4 | ø6 | ø9 | ø13 |
|----------------------|-------|-----|-----|------|------|------|------|------|------|
| Lane Configurations | ↖ | ↑↑ | ↑↑ | ↖↗ | | | | | |
| Volume (vph) | 140 | 90 | 900 | 70 | | | | | |
| Turn Type | Prot | NA | NA | Prot | | | | | |
| Protected Phases | 5 | 2 9 | 6 9 | 4 13 | 2 | 4 | 6 | 9 | 13 |
| Permitted Phases | | | | | | | | | |
| Detector Phase | 5 | 2 | 6 | 4 | | | | | |
| Switch Phase | | | | | | | | | |
| Minimum Initial (s) | 8.0 | | | | 10.0 | 10.0 | 10.0 | 28.0 | 8.0 |
| Minimum Split (s) | 14.5 | | | | 14.9 | 15.0 | 27.5 | 35.0 | 15.0 |
| Total Split (s) | 26.0 | | | | 70.0 | 20.0 | 44.0 | 35.0 | 15.0 |
| Total Split (%) | 18.6% | | | | 50% | 14% | 31% | 25% | 11% |
| Yellow Time (s) | 4.0 | | | | 3.9 | 4.0 | 4.5 | 2.5 | 4.7 |
| All-Red Time (s) | 2.5 | | | | 1.0 | 1.0 | 1.0 | 4.5 | 2.3 |
| Lost Time Adjust (s) | 0.0 | | | | | | | | |
| Total Lost Time (s) | 6.5 | | | | | | | | |
| Lead/Lag | Lead | | | | | | Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | | | | | | Yes | Yes | Yes |
| Recall Mode | None | | | | Min | None | Min | None | None |

Intersection Summary

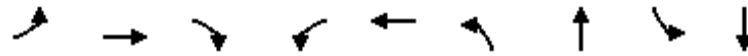
Cycle Length: 140
 Actuated Cycle Length: 107.7
 Natural Cycle: 110
 Control Type: Actuated-Uncoordinated

Splits and Phases: 10: Moffett Park Dr & Innovation Way



Lanes, Volumes, Timings
 11: Innovation Way & 11th Ave

3/4/2016



| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT |
|---------------------|-----|------|-----|-----|------|-----|------|-----|------|
| Lane Configurations | | | | | | | | | |
| Volume (vph) | 50 | 0 | 80 | 20 | 0 | 270 | 180 | 130 | 110 |
| Sign Control | | Stop | | | Stop | | Stop | | Stop |

Intersection Summary

Control Type: Unsignalized

Lanes, Volumes, Timings
 12: Innovation Way & Juniper Driveway

3/4/2016

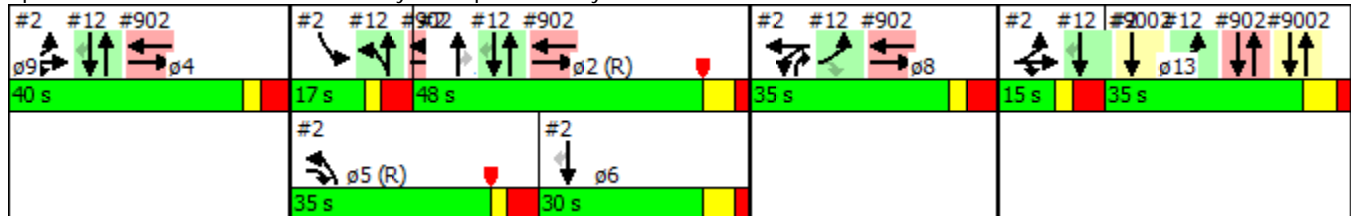


| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR | ø2 | ø4 | ø5 | ø6 | ø8 | ø9 |
|----------------------|------|------|------|-------|--------|--------|-------|------|-------|------|------|------|
| Lane Configurations | ↖ | ↗ | ↖ | ↑↑ | ↑ | ↗ | | | | | | |
| Volume (vph) | 100 | 60 | 110 | 140 | 420 | 750 | | | | | | |
| Turn Type | Prot | Perm | Prot | NA | NA | Perm | | | | | | |
| Protected Phases | 8 9 | | 1 | 1 2 4 | 2 4 13 | | 2 | 4 | 5 | 6 | 8 | 9 |
| Permitted Phases | | 8 9 | | | | 2 4 13 | | | | | | |
| Detector Phase | 8 | 8 | 1 | 1 2 4 | 2 4 | 2 4 | | | | | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 10.0 | | | | 12.0 | 14.0 | 13.0 | 12.0 | 10.0 | 28.0 |
| Minimum Split (s) | | | 16.8 | | | | 19.0 | 39.0 | 20.0 | 30.0 | 35.0 | 35.0 |
| Total Split (s) | | | 17.0 | | | | 48.0 | 40.0 | 35.0 | 30.0 | 35.0 | 35.0 |
| Total Split (%) | | | 8.9% | | | | 25% | 21% | 18% | 16% | 18% | 18% |
| Yellow Time (s) | | | 2.5 | | | | 4.7 | 2.5 | 2.5 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | | | 4.3 | | | | 2.3 | 4.5 | 4.5 | 2.3 | 4.5 | 2.3 |
| Lost Time Adjust (s) | | | 0.0 | | | | | | | | | |
| Total Lost Time (s) | | | 6.8 | | | | | | | | | |
| Lead/Lag | | | Lead | | | | Lag | Lead | Lag | Lag | Lag | Lag |
| Lead-Lag Optimize? | | | Yes | | | | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | | | None | | | | C-Max | None | C-Max | Min | None | None |

Intersection Summary

Cycle Length: 190
 Actuated Cycle Length: 190
 Offset: 133 (70%), Referenced to phase 2:NBT and 5:NBL, Start of Yellow
 Natural Cycle: 175
 Control Type: Actuated-Coordinated

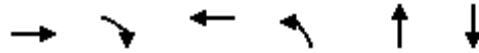
Splits and Phases: 12: Innovation Way & Juniper Driveway



| | |
|----------------------|------|
| Lane Group | ø13 |
| Lane Configurations | |
| Volume (vph) | |
| Turn Type | |
| Protected Phases | 13 |
| Permitted Phases | |
| Detector Phase | |
| Switch Phase | |
| Minimum Initial (s) | 8.0 |
| Minimum Split (s) | 15.0 |
| Total Split (s) | 15.0 |
| Total Split (%) | 8% |
| Yellow Time (s) | 2.5 |
| All-Red Time (s) | 4.5 |
| Lost Time Adjust (s) | |
| Total Lost Time (s) | |
| Lead/Lag | Lead |
| Lead-Lag Optimize? | Yes |
| Recall Mode | None |
| Intersection Summary | |

Lanes, Volumes, Timings
 13: Bordeaux Dr & Innovation Way

3/4/2016

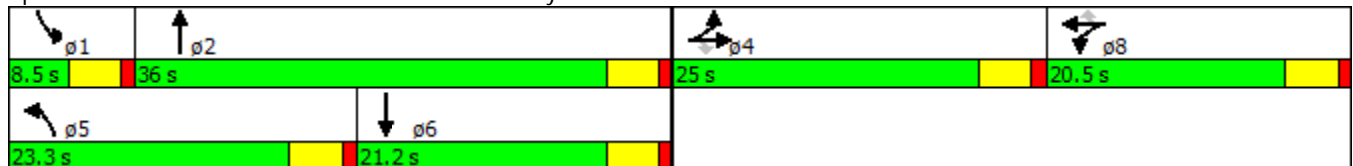


| Lane Group | EBT | EBR | WBT | NBL | NBT | SBT | ø1 |
|----------------------|-------|-------|-------|-------|-------|-------|------|
| Lane Configurations | ↕ | ↗ | ↕ | ↖ | ↗ | ↗ | |
| Volume (vph) | 50 | 690 | 20 | 390 | 130 | 60 | |
| Turn Type | NA | Perm | NA | Prot | NA | NA | |
| Protected Phases | 4 | | 8 | 5 | 2 | 6 | 1 |
| Permitted Phases | | 4 | | | | | |
| Detector Phase | 4 | 4 | 8 | 5 | 2 | 6 | |
| Switch Phase | | | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | 20.5 | 20.5 | 20.5 | 8.5 | 20.5 | 20.5 | 8.5 |
| Total Split (s) | 25.0 | 25.0 | 20.5 | 23.3 | 36.0 | 21.2 | 8.5 |
| Total Split (%) | 27.8% | 27.8% | 22.8% | 25.9% | 40.0% | 23.6% | 9% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | |
| Lead/Lag | | | | Lead | Lag | Lag | Lead |
| Lead-Lag Optimize? | | | | Yes | Yes | Yes | Yes |
| Recall Mode | Max | Max | None | None | None | None | None |

Intersection Summary

Cycle Length: 90
 Actuated Cycle Length: 67.3
 Natural Cycle: 90
 Control Type: Semi Act-Uncoord

Splits and Phases: 13: Bordeaux Dr & Innovation Way



**SimTraffic Post-Processor
Average Results from 10 Runs
Network Performance**

**Mathilda Avenue Improvements
Alternative 1 Year 2040
AM Peak Hour**

| Performance Measure | Average | Std. Dev. | Minimum | Maximum |
|---------------------------------|---------|-----------|---------|---------|
| Average Delay (seconds) | 519.3 | 24.4 | 476.5 | 543.2 |
| Total Delay (hours) | 1,948 | 100 | 1,747 | 2,050 |
| Average Stopped Delay (seconds) | 439.3 | 23.7 | 400.0 | 466.4 |
| Total Stopped Delay (hours) | 1648 | 94 | 1467 | 1749 |
| Total Stops | 49,230 | 1,277 | 46,781 | 50,679 |
| Average Stops | 3.65 | 0.07 | 3.54 | 3.74 |
| Total Distance Traveled (miles) | 49,422 | 625 | 47,925 | 50,059 |
| Average Speed (mph) | 15.6 | 0.7 | 15.0 | 17.0 |
| Total Travel Time (hours) | 3,345.2 | 119.7 | 3,135.1 | 3,519.4 |
| Vehicles Entered | 11,102 | 173 | 10,843 | 11,316 |
| Vehicles Exited | 9,802 | 128 | 9,529 | 9,937 |
| Percent Demand Served | 88.3% | 1.6% | 86.0% | 91.1% |
| Fuel Used (gallons) | 1,693 | 23 | 1,648 | 1,734 |
| HC Emissions (grams) | 20,805 | 1,310 | 18,497 | 22,916 |
| CO Emissions (grams) | 574,255 | 24,401 | 532,903 | 615,264 |
| NOx Emissions (grams) | 75,937 | 3,128 | 70,998 | 81,613 |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Alternative 1 Year 2040
AM Peak Hour

Intersection 1 Mathilda Avenue/5th Avenue Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | 200 | 148 | 73.8% | 45.2 | 5.4 | D |
| | Through | 860 | 641 | 74.5% | 17.7 | 1.9 | B |
| | Right Turn | 80 | 60 | 74.9% | 12.7 | 3.0 | B |
| | Subtotal | 1,140 | 849 | 74.4% | 22.1 | 1.9 | C |
| SB | Left Turn | 40 | 36 | 90.0% | 59.0 | 8.1 | E |
| | Through | 520 | 502 | 96.5% | 28.7 | 0.9 | C |
| | Right Turn | 110 | 105 | 95.4% | 12.2 | 1.2 | B |
| | Subtotal | 670 | 643 | 95.9% | 27.7 | 0.8 | C |
| EB | Left Turn | 30 | 29 | 96.7% | 36.1 | 3.6 | D |
| | Through | 30 | 35 | 115.7% | 34.9 | 3.6 | C |
| | Right Turn | 90 | 90 | 99.6% | 11.2 | 2.1 | B |
| | Subtotal | 150 | 153 | 102.2% | 21.1 | 2.9 | C |
| WB | Left Turn | 60 | 60 | 100.2% | 48.3 | 5.3 | D |
| | Through | 30 | 31 | 102.0% | 42.2 | 11.2 | D |
| | Right Turn | 20 | 22 | 110.0% | 18.1 | 6.0 | B |
| | Subtotal | 110 | 113 | 102.5% | 40.7 | 5.9 | D |
| Total | | 2,070 | 1,757 | 84.9% | 25.3 | 1.3 | C |

Intersection 2 Mathilda Avenue/Innovation Way-Driveway Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | 760 | 590 | 77.6% | 84.9 | 10.3 | F |
| | Through | 1,020 | 768 | 75.3% | 37.6 | 1.6 | D |
| | Right Turn | 1,240 | 941 | 75.9% | 95.7 | 10.3 | F |
| | Subtotal | 3,020 | 2,299 | 76.1% | 73.5 | 5.5 | E |
| SB | Left Turn | 50 | 48 | 96.6% | 108.3 | 12.8 | F |
| | Through | 390 | 372 | 95.4% | 54.2 | 5.2 | D |
| | Right Turn | 230 | 234 | 101.6% | 39.5 | 7.3 | D |
| | Subtotal | 670 | 654 | 97.6% | 53.0 | 3.4 | D |
| EB | Left Turn | 40 | 33 | 82.0% | 59.4 | 19.7 | E |
| | Through | 90 | 86 | 95.0% | 59.5 | 18.0 | E |
| | Right Turn | 110 | 103 | 93.6% | 52.8 | 18.1 | D |
| | Subtotal | 240 | 221 | 92.2% | 56.3 | 18.2 | E |
| WB | Left Turn | 360 | 248 | 68.9% | 228.6 | 7.0 | F |
| | Through | 180 | 129 | 71.7% | 264.0 | 12.1 | F |
| | Right Turn | 80 | 55 | 68.5% | 247.8 | 14.9 | F |
| | Subtotal | 620 | 432 | 69.6% | 241.6 | 8.4 | F |
| Total | | 4,550 | 3,606 | 79.2% | 88.9 | 3.7 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Alternative 1 Year 2040
AM Peak Hour

Intersection 3 Mathilda Avenue/Moffett Park Drive-SR 237 WB Off-Ramp Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | 1,100 | 830 | 75.5% | 65.9 | 8.8 | E |
| | Through | 2,660 | 1,921 | 72.2% | 60.3 | 4.0 | E |
| | Right Turn | | | | | | |
| | Subtotal | 3,760 | 2,751 | 73.2% | 61.9 | 4.3 | E |
| SB | Left Turn | | | | | | |
| | Through | 540 | 442 | 81.9% | 91.5 | 21.3 | F |
| | Right Turn | 320 | 253 | 79.0% | 179.5 | 89.4 | F |
| | Subtotal | 860 | 695 | 80.8% | 122.8 | 44.2 | F |
| EB | Left Turn | 50 | 44 | 87.8% | 69.7 | 16.3 | E |
| | Through | | | | | | |
| | Right Turn | 110 | 99 | 90.4% | 8.4 | 6.7 | A |
| | Subtotal | 160 | 143 | 89.6% | 26.9 | 7.4 | C |
| WB | Left Turn | 670 | 648 | 96.7% | 93.0 | 33.0 | F |
| | Through | 300 | 292 | 97.5% | 115.0 | 41.5 | F |
| | Right Turn | 310 | 301 | 97.0% | 129.0 | 54.1 | F |
| | Subtotal | 1,280 | 1,241 | 97.0% | 107.0 | 40.1 | F |
| Total | | 6,060 | 4,830 | 79.7% | 81.4 | 9.9 | F |

Intersection 4 Mathilda Avenue/SR 237 EB Ramps Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | | | | | | |
| | Through | 2,980 | 2,309 | 77.5% | 43.4 | 5.3 | D |
| | Right Turn | 920 | 723 | 78.5% | 2.6 | 0.2 | A |
| | Subtotal | 3,900 | 3,031 | 77.7% | 33.6 | 4.0 | C |
| SB | Left Turn | 80 | 72 | 90.1% | 145.6 | 40.3 | F |
| | Through | 1,050 | 927 | 88.3% | 39.1 | 11.7 | D |
| | Right Turn | | | | | | |
| | Subtotal | 1,130 | 999 | 88.4% | 46.7 | 10.6 | D |
| EB | Left Turn | 780 | 448 | 57.5% | 1158.6 | 527.5 | F |
| | Through | | | | | | |
| | Right Turn | 70 | 41 | 59.0% | 877.6 | 451.8 | F |
| | Subtotal | 850 | 490 | 57.6% | 1134.3 | 521.0 | F |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 5,880 | 4,520 | 76.9% | 142.3 | 24.8 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Alternative 1 Year 2040
AM Peak Hour

Intersection 5 Mathilda Avenue/Ross Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | 80 | 56 | 70.5% | 108.8 | 12.5 | F |
| | Through | 3,510 | 2,670 | 76.1% | 73.5 | 13.0 | E |
| | Right Turn | 120 | 94 | 78.3% | 56.3 | 8.0 | E |
| | Subtotal | 3,710 | 2,820 | 76.0% | 73.6 | 12.8 | E |
| SB | Left Turn | 70 | 57 | 81.3% | 53.4 | 2.6 | D |
| | Through | 1,000 | 882 | 88.2% | 29.4 | 8.4 | C |
| | Right Turn | 50 | 46 | 91.4% | 21.2 | 7.3 | C |
| | Subtotal | 1,120 | 985 | 87.9% | 30.4 | 7.7 | C |
| EB | Left Turn | 90 | 88 | 97.2% | 76.3 | 15.0 | E |
| | Through | 70 | 71 | 102.0% | 40.3 | 6.3 | D |
| | Right Turn | 40 | 41 | 101.5% | 14.5 | 4.2 | B |
| | Subtotal | 200 | 200 | 99.8% | 50.6 | 8.2 | D |
| WB | Left Turn | 130 | 115 | 88.5% | 213.9 | 192.4 | F |
| | Through | 40 | 38 | 95.5% | 199.5 | 169.6 | F |
| | Right Turn | 300 | 277 | 92.2% | 216.8 | 184.7 | F |
| | Subtotal | 470 | 430 | 91.5% | 214.4 | 185.3 | F |
| Total | | 5,500 | 4,434 | 80.6% | 76.0 | 18.8 | E |

Intersection 6 Mathilda Avenue/US 101 NB Ramps Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | | | | | | |
| | Through | 2,930 | 2,085 | 71.1% | 72.7 | 15.1 | E |
| | Right Turn | 570 | 389 | 68.3% | 12.0 | 1.8 | B |
| | Subtotal | 3,500 | 2,474 | 70.7% | 63.2 | 12.9 | E |
| SB | Left Turn | 20 | 17 | 85.0% | 58.5 | 4.6 | E |
| | Through | 1,150 | 1,033 | 89.9% | 26.1 | 2.5 | C |
| | Right Turn | | | | | | |
| | Subtotal | 1,170 | 1,050 | 89.8% | 26.6 | 2.5 | C |
| EB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| WB | Left Turn | 770 | 764 | 99.2% | 177.8 | 80.1 | F |
| | Through | | | | | | |
| | Right Turn | 780 | 754 | 96.7% | 162.9 | 78.9 | F |
| | Subtotal | 1,550 | 1,518 | 97.9% | 170.4 | 79.5 | F |
| Total | | 6,220 | 5,043 | 81.1% | 87.9 | 26.8 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Alternative 1 Year 2040
AM Peak Hour

Intersection 7 Mathilda Avenue/US 101 SB Ramps Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | | | | | | |
| | Through | 3,120 | 2,134 | 68.4% | 62.4 | 16.8 | E |
| | Right Turn | 700 | 484 | 69.1% | 24.2 | 5.0 | C |
| | Subtotal | 3,820 | 2,617 | 68.5% | 55.4 | 14.6 | E |
| SB | Left Turn | | | | | | |
| | Through | 1,730 | 1,619 | 93.6% | 15.1 | 1.2 | B |
| | Right Turn | 190 | 169 | 88.9% | 12.9 | 1.0 | B |
| | Subtotal | 1,920 | 1,788 | 93.1% | 14.9 | 1.1 | B |
| EB | Left Turn | 380 | 374 | 98.4% | 88.0 | 11.3 | F |
| | Through | | | | | | |
| | Right Turn | 520 | 507 | 97.5% | 36.3 | 5.2 | D |
| | Subtotal | 900 | 881 | 97.9% | 58.2 | 7.3 | E |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 6,640 | 5,286 | 79.6% | 42.0 | 8.0 | D |

Intersection 8 Mathilda Avenue/Almanor Avenue-Ahwanee Avenue Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | 140 | 90 | 64.1% | 927.5 | 89.7 | F |
| | Through | 3,430 | 2,237 | 65.2% | 945.3 | 96.6 | F |
| | Right Turn | 70 | 48 | 68.6% | 946.9 | 97.8 | F |
| | Subtotal | 3,640 | 2,375 | 65.3% | 944.7 | 96.3 | F |
| SB | Left Turn | 160 | 151 | 94.1% | 155.1 | 36.8 | F |
| | Through | 1,760 | 1,670 | 94.9% | 42.4 | 3.9 | D |
| | Right Turn | 330 | 302 | 91.4% | 48.6 | 5.0 | D |
| | Subtotal | 2,250 | 2,122 | 94.3% | 51.3 | 5.4 | D |
| EB | Left Turn | 130 | 126 | 97.2% | 75.7 | 5.8 | E |
| | Through | 30 | 29 | 96.7% | 74.6 | 7.9 | E |
| | Right Turn | 40 | 43 | 106.8% | 45.1 | 6.2 | D |
| | Subtotal | 200 | 198 | 99.0% | 68.7 | 3.8 | E |
| WB | Left Turn | 90 | 88 | 98.2% | 70.8 | 8.1 | E |
| | Through | 50 | 51 | 101.4% | 73.5 | 12.9 | E |
| | Right Turn | 260 | 265 | 101.8% | 35.4 | 10.9 | D |
| | Subtotal | 400 | 404 | 100.9% | 47.9 | 9.6 | D |
| Total | | 6,490 | 5,099 | 78.6% | 466.2 | 32.9 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Alternative 1 Year 2040
AM Peak Hour

Intersection 9 US 101 NB Slip Ramp/Moffett Park Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| EB | Left Turn | | | | | | |
| | Through | 230 | 224 | 97.5% | 2.1 | 0.4 | A |
| | Right Turn | 20 | 19 | 95.5% | 1.4 | 0.3 | A |
| | Subtotal | 250 | 243 | 97.3% | 2.0 | 0.4 | A |
| WB | Left Turn | 40 | 30 | 75.0% | 10.1 | 0.8 | B |
| | Through | 990 | 821 | 82.9% | 5.6 | 0.6 | A |
| | Right Turn | | | | | | |
| | Subtotal | 1,030 | 851 | 82.6% | 5.7 | 0.6 | A |
| Total | | 1,280 | 1,094 | 85.5% | 4.9 | 0.5 | A |

Intersection 10 Innovation Way/Moffett Park Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | 70 | 59 | 84.6% | 46.4 | 4.4 | D |
| | Through | | | | | | |
| | Right Turn | 130 | 120 | 92.5% | 38.9 | 4.0 | D |
| | Subtotal | 200 | 179 | 89.7% | 41.3 | 3.8 | D |
| EB | Left Turn | 140 | 138 | 98.5% | 43.8 | 8.2 | D |
| | Through | 90 | 86 | 95.9% | 4.6 | 1.2 | A |
| | Right Turn | | | | | | |
| | Subtotal | 230 | 224 | 97.5% | 28.6 | 5.0 | C |
| WB | Left Turn | | | | | | |
| | Through | 900 | 733 | 81.4% | 19.6 | 1.6 | B |
| | Right Turn | 640 | 511 | 79.8% | 24.8 | 2.7 | C |
| | Subtotal | 1,540 | 1,244 | 80.8% | 21.7 | 1.9 | C |
| Total | | 1,970 | 1,647 | 83.6% | 24.8 | 1.9 | C |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Alternative 1 Year 2040
AM Peak Hour

Intersection 11 Innovation Way/11th Avenue All-way Stop

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 270 | 228 | 84.6% | 12.3 | 0.9 | B |
| | Through | 180 | 149 | 83.0% | 12.5 | 0.7 | B |
| | Right Turn | 240 | 198 | 82.7% | 8.3 | 0.6 | A |
| | Subtotal | 690 | 576 | 83.5% | 11.0 | 0.7 | B |
| SB | Left Turn | 130 | 108 | 83.2% | 7.8 | 0.6 | A |
| | Through | 110 | 91 | 82.9% | 13.5 | 1.2 | B |
| | Right Turn | 240 | 198 | 82.4% | 10.8 | 0.9 | B |
| | Subtotal | 480 | 397 | 82.7% | 10.7 | 0.7 | B |
| EB | Left Turn | 50 | 50 | 100.2% | 15.5 | 2.6 | C |
| | Through | | | | | | |
| | Right Turn | 80 | 80 | 99.4% | 11.9 | 2.1 | B |
| | Subtotal | 130 | 130 | 99.7% | 13.3 | 1.5 | B |
| WB | Left Turn | 20 | 19 | 94.0% | 5.0 | 0.5 | A |
| | Through | | | | | | |
| | Right Turn | 20 | 19 | 95.0% | 3.4 | 0.2 | A |
| | Subtotal | 40 | 38 | 94.5% | 4.2 | 0.2 | A |
| Total | | 1,340 | 1,141 | 85.1% | 10.9 | 0.5 | B |

Intersection 12 Innovation Way/Juniper Networks Driveway All-way Stop

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 110 | 96 | 87.5% | 198.9 | 84.5 | F |
| | Through | 140 | 122 | 87.4% | 43.3 | 33.9 | E |
| | Right Turn | | | | | | |
| | Subtotal | 250 | 219 | 87.4% | 113.2 | 59.5 | F |
| SB | Left Turn | | | | | | |
| | Through | 420 | 337 | 80.2% | 9.2 | 0.8 | A |
| | Right Turn | 750 | 619 | 82.5% | 9.0 | 0.6 | A |
| | Subtotal | 1,170 | 956 | 81.7% | 9.1 | 0.5 | A |
| EB | Left Turn | 100 | 100 | 100.1% | 74.2 | 33.0 | F |
| | Through | | | | | | |
| | Right Turn | 60 | 61 | 101.2% | 13.2 | 2.2 | B |
| | Subtotal | 160 | 161 | 100.5% | 50.7 | 18.6 | F |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 1,580 | 1,335 | 84.5% | 31.4 | 12.2 | D |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Alternative 1 Year 2040
AM Peak Hour

Intersection 13

Bordeaux Drive/Innovation Way

Side-street Stop

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 390 | 233 | 59.6% | 489.7 | 124.0 | F |
| | Through | 130 | 76 | 58.2% | 320.9 | 112.9 | F |
| | Right Turn | | | | | | |
| | Subtotal | 520 | 308 | 59.3% | 448.3 | 122.1 | F |
| SB | Left Turn | | | | | | |
| | Through | 60 | 63 | 105.7% | 96.1 | 58.6 | F |
| | Right Turn | 150 | 149 | 99.3% | 94.8 | 55.1 | F |
| | Subtotal | 210 | 212 | 101.1% | 95.1 | 55.9 | F |
| EB | Left Turn | 370 | 291 | 78.7% | 38.7 | 2.5 | E |
| | Through | 50 | 37 | 73.6% | 38.5 | 6.1 | E |
| | Right Turn | 690 | 537 | 77.8% | 22.7 | 1.5 | C |
| | Subtotal | 1,110 | 865 | 77.9% | 28.8 | 1.9 | D |
| WB | Left Turn | | | | | | |
| | Through | 20 | 20 | 98.5% | 63.3 | 18.0 | F |
| | Right Turn | | | | | | |
| | Subtotal | 20 | 20 | 98.5% | 63.3 | 18.0 | F |
| Total | | 1,860 | 1,405 | 75.5% | 130.2 | 28.4 | F |

Intersection 1

Mathilda Avenue/5th Avenue

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 625 | 25 | 5 | 50 | 6 | 75 | 16 | 0% | 0% |
| | Through | 625 | 25 | 5 | 50 | 8 | 75 | 13 | 0% | 0% |
| | Right Turn | 625 | 50 | 7 | 75 | 15 | 125 | 21 | 0% | 0% |
| NB | Left Turn | 425 | 75 | 6 | 125 | 13 | 175 | 31 | 0% | 0% |
| | Through | 1,125 | 100 | 12 | 200 | 20 | 225 | 21 | 0% | 0% |
| | Through/Right | 1,125 | 125 | 14 | 225 | 25 | 275 | 22 | 0% | 0% |
| SB | Left Turn | 250 | 50 | 5 | 75 | 11 | 100 | 26 | 0% | 0% |
| | Through | 1,325 | 100 | 7 | 175 | 15 | 225 | 32 | 0% | 0% |
| | Right Turn | 250 | 25 | 5 | 50 | 15 | 100 | 23 | 0% | 0% |
| WB | Left Turn | 925 | 75 | 10 | 125 | 20 | 150 | 23 | 15% | 0% |
| | Through/Right | 75 | 50 | 7 | 100 | 8 | 100 | 0 | 11% | 0% |

Intersection 2

Mathilda Avenue/Innovation Way-Driveway

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|--------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left/Through | 225 | 150 | 24 | 225 | 31 | 250 | 31 | 0% | 6% |
| | Right Turn | 225 | 25 | 4 | 50 | 6 | 75 | 15 | 0% | 8% |
| NB | Left Turn | 725 | 400 | 44 | 700 | 111 | 750 | 227 | 2% | 0% |
| | Through | 975 | 900 | 162 | 1,350 | 76 | 1,100 | 13 | 1% | 5% |
| | Right Turn | 975 | 975 | 53 | 1,200 | 68 | 1,075 | 12 | 0% | 8% |
| SB | Left Turn | 75 | 75 | 8 | 125 | 11 | 150 | 4 | 15% | 0% |
| | Through | 975 | 125 | 16 | 250 | 38 | 325 | 64 | 20% | 0% |
| | Right Turn | 225 | 150 | 17 | 250 | 28 | 275 | 21 | 4% | 0% |
| WB | Left Turn | 425 | 775 | 4 | 800 | 7 | 800 | 13 | 36% | 44% |
| | Shared | 225 | 250 | 1 | 250 | 3 | 250 | 2 | 77% | 0% |

Intersection 3

Mathilda Avenue/Moffett Park Drive-SR 237 WB Off-Ramp

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|----------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Shared | 1,125 | 50 | 8 | 125 | 15 | 175 | 46 | 0% | 0% |
| | Right Turn | 1,125 | 25 | 10 | 75 | 33 | 100 | 61 | 0% | 0% |
| NB | Left Turn | 350 | 325 | 46 | 475 | 45 | 475 | 32 | 0% | 11% |
| | Through | 350 | 425 | 16 | 500 | 25 | 500 | 22 | 0% | 33% |
| | Right Diagonal | 350 | 175 | 11 | 225 | 9 | 200 | 14 | 0% | 50% |
| SB | Through | 975 | 400 | 159 | 700 | 268 | 725 | 246 | 0% | 0% |
| | Through/Right | 975 | 500 | 141 | 750 | 208 | 775 | 202 | 0% | 1% |
| WB | Left Turn | 525 | 425 | 84 | 550 | 82 | 575 | 64 | 8% | 0% |
| | Left/Through | 1,225 | 525 | 183 | 750 | 296 | 825 | 292 | 13% | 1% |
| | Through/Right | 1,225 | 575 | 168 | 775 | 226 | 850 | 242 | 0% | 0% |

Intersection 4

Mathilda Avenue/SR 237 EB Ramps

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|--------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,025 | 5,275 | 2,490 | 9,625 | 3,258 | 9,825 | 3,084 | 0% | 0% |
| | Left/Through | 1,025 | 1,025 | 55 | 1,175 | 85 | 1,100 | 8 | 84% | 38% |
| | Right Turn | 450 | 225 | 63 | 675 | 78 | 575 | 0 | 0% | 0% |
| NB | Through | 275 | 225 | 28 | 275 | 45 | 275 | 38 | 0% | 16% |
| | Right Turn | 275 | 25 | 7 | 50 | 25 | 50 | 35 | 0% | 0% |
| SB | Left Turn | 325 | 200 | 25 | 325 | 56 | 350 | 51 | 2% | 0% |
| | Through | 350 | 300 | 32 | 400 | 39 | 450 | 40 | 0% | 5% |
| | | | | | | | | | | |

SimTraffic Post-Processor
Average Results from 10 Runs
Queue Length
Intersection 5

Mathilda Avenue Improvements
Alternative 1 Year 2040
AM Peak Hour
Signal

Mathilda Avenue/Ross Drive

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 250 | 75 | 7 | 125 | 5 | 125 | 1 | 26% | 0% |
| | Through | 1,575 | 100 | 22 | 225 | 52 | 325 | 90 | 35% | 0% |
| | Right Turn | 50 | 50 | 6 | 100 | 10 | 100 | 3 | 5% | 0% |
| NB | Left Turn | 250 | 150 | 30 | 350 | 45 | 300 | 1 | 0% | 0% |
| | Through | 700 | 650 | 53 | 825 | 35 | 750 | 20 | 56% | 8% |
| | Through/Right | 225 | 275 | 4 | 275 | 16 | 275 | 0 | 39% | 0% |
| SB | Left Turn | 225 | 75 | 9 | 125 | 12 | 150 | 15 | 0% | 0% |
| | Through | 225 | 125 | 29 | 275 | 39 | 250 | 6 | 0% | 17% |
| | Through/Right | 225 | 150 | 29 | 300 | 38 | 275 | 18 | 0% | 20% |
| WB | Left Turn | 100 | 75 | 9 | 125 | 6 | 100 | 0 | 11% | 0% |
| | Through | 225 | 900 | 737 | 1,575 | 1,047 | 1,725 | 845 | 2% | 0% |
| | Right Turn | 100 | 100 | 1 | 125 | 2 | 125 | 0 | 70% | 0% |

Intersection 6

Mathilda Avenue/US 101 NB Ramps

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NB | Through | 575 | 600 | 64 | 725 | 40 | 675 | 24 | 0% | 27% |
| | Right Turn | 575 | 350 | 100 | 750 | 89 | 650 | 48 | 0% | 0% |
| SB | Left Turn | 375 | 25 | 7 | 75 | 32 | 175 | 134 | 0% | 0% |
| | Through | 700 | 200 | 26 | 400 | 49 | 450 | 87 | 1% | 0% |
| WB | Left Turn | 1,025 | 525 | 260 | 1,375 | 422 | 1,975 | 484 | 0% | 0% |
| | Right Turn | 1,025 | 150 | 7 | 175 | 15 | 175 | 18 | 0% | 53% |
| 0 | | | | | | | | | | |

Mathilda Avenue/US 101 SB Ramps

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,050 | 200 | 34 | 325 | 60 | 400 | 75 | 12% | 0% |
| | Right Turn | 1,050 | 25 | 1 | 25 | 13 | 25 | 37 | 0% | 0% |
| NB | Through | 750 | 625 | 95 | 925 | 96 | 800 | 15 | 0% | 7% |
| | Right Turn | 750 | 525 | 108 | 1,025 | 122 | 800 | 179 | 0% | 7% |
| SB | Through | 575 | 150 | 16 | 300 | 32 | 350 | 103 | 0% | 0% |
| | Through/Right | 575 | 175 | 20 | 325 | 27 | 350 | 15 | 0% | 0% |
| | | | | | | | | | | |

Intersection 8

Mathilda Avenue/Almanor Avenue-Ahwanee Avenue

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,025 | 75 | 5 | 150 | 13 | 200 | 41 | 4% | 0% |
| | Through/Right | 125 | 75 | 6 | 125 | 17 | 200 | 38 | 2% | 0% |
| NB | Left Turn | 425 | 200 | 23 | 500 | 31 | 425 | 0 | 0% | 0% |
| | Through | 750 | 9,275 | 588 | 13,875 | 532 | 12,300 | 49 | 75% | 33% |
| | Through/Right | 750 | 325 | 1 | 325 | 3 | 325 | 0 | 49% | 0% |
| SB | Left Turn | 275 | 225 | 34 | 350 | 44 | 350 | 1 | 20% | 0% |
| | Through | 750 | 300 | 30 | 550 | 72 | 725 | 129 | 10% | 1% |
| | Through/Right | 750 | 325 | 20 | 575 | 51 | 700 | 76 | 0% | 0% |
| WB | Left Turn | 250 | 100 | 14 | 200 | 46 | 250 | 87 | 0% | 0% |
| | Through | 1,025 | 175 | 39 | 350 | 113 | 475 | 242 | 24% | 0% |
| | Right Turn | 75 | 100 | 6 | 150 | 3 | 125 | 0 | 51% | 0% |

US 101 NB Slip Ramp/Moffett Park Drive

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Through | 850 | 25 | 5 | 75 | 11 | 100 | 13 | 0% | 0% |
| | Right Turn | 150 | 25 | 2 | 25 | 11 | 25 | 19 | 0% | 0% |
| WB | Left Turn | 850 | 25 | 4 | 75 | 6 | 75 | 15 | 0% | 0% |
| | Through | 850 | 25 | 5 | 25 | 51 | 50 | 149 | 0% | 0% |
| | | | | | | | | | | |
| | | | | | | | | | | |

Intersection 10

Innovation Way/Moffett Park Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 225 | 100 | 11 | 175 | 23 | 200 | 32 | 0% | 0% |
| | Through | 850 | 25 | 8 | 75 | 33 | 125 | 70 | 0% | 0% |
| SB | Left Turn | 575 | 50 | 4 | 75 | 7 | 100 | 15 | 0% | 0% |
| | Shared | 575 | 125 | 8 | 200 | 12 | 250 | 14 | 0% | 0% |
| WB | Through | 1,150 | 200 | 28 | 350 | 124 | 625 | 428 | 0% | 0% |
| | Through/Right | 1,150 | 275 | 28 | 475 | 116 | 700 | 355 | 0% | 0% |
| | | | | | | | | | | |

SimTraffic Post-Processor
Average Results from 10 Runs
Queue Length
Intersection 11

Mathilda Avenue Improvements
Alternative 1 Year 2040
AM Peak Hour
All-way Stop

Innovation Way/11th Avenue

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 125 | 50 | 3 | 75 | 5 | 75 | 18 | 0% | 0% |
| | Left/Through | 325 | 25 | 3 | 50 | 6 | 50 | 14 | 0% | 0% |
| | Right Turn | 325 | 50 | 5 | 75 | 11 | 100 | 15 | 0% | 0% |
| NB | Left Turn | 125 | 75 | 7 | 100 | 14 | 125 | 24 | 1% | 0% |
| | Through | 575 | 100 | 4 | 200 | 6 | 250 | 10 | 0% | 0% |
| | Through/Right | 575 | 50 | 4 | 100 | 10 | 125 | 31 | 0% | 0% |
| SB | Left Turn | 175 | 50 | 3 | 75 | 9 | 100 | 18 | 0% | 0% |
| | Through | 1,000 | 25 | 3 | 50 | 5 | 50 | 14 | 0% | 0% |
| | Through/Right | 1,000 | 100 | 10 | 175 | 22 | 200 | 35 | 0% | 0% |
| WB | Left Turn | 325 | 25 | 2 | 50 | 2 | 50 | 9 | 0% | 0% |
| | Through/Right | 325 | 25 | 5 | 50 | 6 | 50 | 10 | 0% | 0% |

Intersection 12

Innovation Way/Juniper Networks Driveway

All-way Stop

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 200 | 100 | 29 | 200 | 60 | 250 | 89 | 0% | 0% |
| | Right Turn | 200 | 50 | 5 | 75 | 8 | 75 | 16 | 0% | 0% |
| NB | Left Turn | 125 | 150 | 25 | 175 | 6 | 175 | 3 | 61% | 0% |
| | Through | 1,000 | 225 | 104 | 375 | 142 | 400 | 106 | 0% | 0% |
| SB | Through | 300 | 175 | 17 | 250 | 30 | 275 | 45 | 0% | 0% |
| | Right Turn | 300 | 125 | 10 | 225 | 24 | 275 | 35 | 0% | 3% |
| | | | | | | | | | | |

SimTraffic Post-Processor
 Average Results from 10 Runs
 Queue Length
 Intersection 13

Bordeaux Drive/Innovation Way

Mathilda Avenue Improvements
 Alternative 1 Year 2040
 AM Peak Hour
 Side-street Stop

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left/Through | 375 | 325 | 12 | 450 | 18 | 375 | 2 | 35% | 10% |
| | Right Turn | 125 | 125 | 2 | 150 | 11 | 150 | 0 | 19% | 0% |
| NB | Left Turn | 325 | 325 | 1 | 350 | 2 | 350 | 0 | 90% | 0% |
| | Through/Right | 2,025 | 800 | 6 | 825 | 26 | 800 | 2 | 1% | 62% |
| SB | Left Turn | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | Through/Right | 725 | 225 | 93 | 400 | 182 | 450 | 122 | 50% | 1% |
| WB | Left/Through | 525 | 25 | 6 | 75 | 10 | 100 | 19 | 0% | 0% |
| | Right Turn | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |

Arterial Level of Service: NB Mathilda Ave

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|--------------------|------|---------------|-----------------|------------|----------------|
| Ahwanee Ave | 8 | 99.4 | 110.4 | 0.1 | 5 |
| | 7 | 59.8 | 72.5 | 0.2 | 8 |
| US 101 NB Ramps | 6 | 70.5 | 80.4 | 0.1 | 6 |
| Ross Dr | 5 | 70.7 | 82.3 | 0.1 | 6 |
| SR 237 EB Ramps | 4 | 41.4 | 46.7 | 0.1 | 5 |
| SR 237 WB On-Ramp | 33 | 21.8 | 25.3 | 0.0 | 7 |
| SR 237 WB Off-Ramp | 3 | 36.4 | 39.5 | 0.0 | 3 |
| Innovation Way | 2 | 39.7 | 56.4 | 0.2 | 14 |
| 5th Ave | 1 | 18.0 | 37.2 | 0.2 | 23 |
| | 107 | 4.5 | 26.6 | 0.3 | 37 |
| Total | | 462.3 | 577.3 | 1.4 | 9 |

Arterial Level of Service: SB Mathilda Ave

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|-------------------|------|---------------|-----------------|------------|----------------|
| 5th Ave | 1 | 20.3 | 42.5 | 0.3 | 23 |
| Innovation Way | 2 | 55.3 | 73.4 | 0.2 | 12 |
| Moffett Park Dr | 3 | 88.4 | 105.3 | 0.2 | 7 |
| SR 237 WB On-Ramp | 33 | 11.0 | 14.1 | 0.0 | 10 |
| SR 237 EB Ramps | 4 | 32.5 | 36.3 | 0.0 | 5 |
| Ross Dr | 5 | 28.7 | 33.5 | 0.1 | 7 |
| US 101 NB Ramps | 6 | 29.4 | 40.9 | 0.1 | 13 |
| US 101 SB Ramps | 7 | 14.1 | 24.8 | 0.1 | 19 |
| Almanor Ave | 8 | 39.0 | 51.4 | 0.2 | 11 |
| San Aleso Ave | 201 | 4.1 | 15.4 | 0.1 | 33 |
| Total | | 322.7 | 437.7 | 1.4 | 12 |

Arterial Level of Service: NB Innovation Way

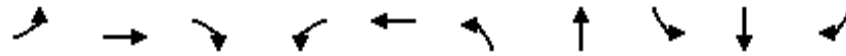
| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|------------------|------|---------------|-----------------|------------|----------------|
| | 910 | 2.9 | 6.9 | 0.0 | 12 |
| | 43 | 1.4 | 6.4 | 0.0 | 23 |
| | 11 | 8.5 | 16.0 | 0.1 | 16 |
| | 200 | 18.8 | 35.4 | 0.2 | 16 |
| Juniper Driveway | 12 | 26.0 | 31.7 | 0.1 | 6 |
| Driveway | 217 | 6.4 | 9.7 | 0.0 | 14 |
| | 902 | 35.3 | 37.6 | 0.0 | 2 |
| Mathilda Ave | 2 | 17.1 | 19.5 | 0.0 | 5 |
| | 52 | 10.6 | 24.1 | 0.1 | 14 |
| Bordeaux Dr | 13 | 38.4 | 49.6 | 0.1 | 6 |
| Total | | 165.4 | 236.9 | 0.6 | 9 |

Arterial Level of Service: SB Innovation Way

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|------------------|------|---------------|-----------------|-----------|----------------|
| | 52 | 43.1 | 49.8 | 0.1 | 6 |
| Mathilda Ave | 2 | 175.6 | 187.4 | 0.1 | 2 |
| | 902 | 7.8 | 12.8 | 0.0 | 7 |
| Driveway | 217 | 0.9 | 3.1 | 0.0 | 24 |
| Juniper Driveway | 12 | 5.7 | 9.7 | 0.0 | 14 |
| | 200 | 1.4 | 7.8 | 0.1 | 26 |
| 11th Ave | 11 | 12.4 | 28.1 | 0.2 | 20 |
| | 43 | 3.4 | 10.9 | 0.1 | 24 |
| | 910 | 24.3 | 28.7 | 0.0 | 5 |
| Moffett Park Dr | 10 | 19.4 | 22.9 | 0.0 | 4 |
| Total | | 293.9 | 361.3 | 0.6 | 6 |

Lanes, Volumes, Timings
1: Mathilda Ave & 5th Ave

3/4/2016

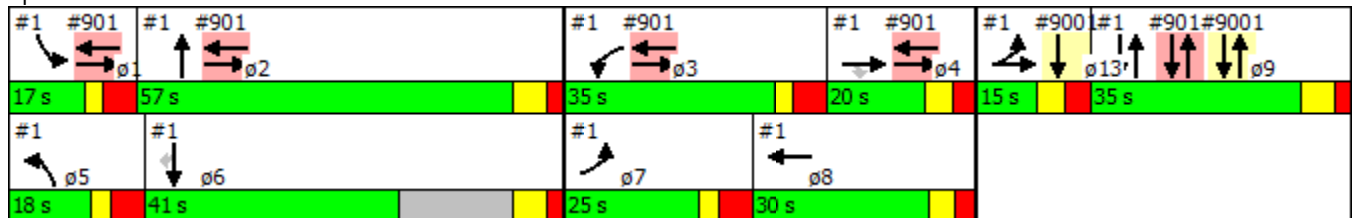


| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT | SBR | ø2 | ø7 |
|----------------------|------|------|--------|-------|-------|-------|-----|------|------|--------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 180 | 40 | 170 | 290 | 20 | 140 | 660 | 20 | 1120 | 30 | | |
| Turn Type | Prot | NA | custom | Prot | NA | Prot | NA | Prot | NA | custom | | |
| Protected Phases | 7 13 | 4 13 | | 3 | 8 | 5 | 2 9 | 1 | 6 9 | | 2 | 7 |
| Permitted Phases | | | 4 | | | | | | | 6 | | |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 5 | 2 | 1 | 6 | 6 | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 13.0 | 12.0 | 8.0 | 11.0 | | 10.0 | | 12.0 | 12.0 | 12.0 |
| Minimum Split (s) | | | 20.0 | 19.0 | 29.5 | 18.0 | | 17.0 | | 41.0 | 35.0 | 19.0 |
| Total Split (s) | | | 20.0 | 35.0 | 30.0 | 18.0 | | 17.0 | | 41.0 | 57.0 | 25.0 |
| Total Split (%) | | | 11.2% | 19.6% | 16.8% | 10.1% | | 9.5% | | 22.9% | 32% | 14% |
| Yellow Time (s) | | | 3.6 | 2.5 | 3.6 | 2.5 | | 2.5 | | 4.7 | 4.7 | 2.5 |
| All-Red Time (s) | | | 3.4 | 4.5 | 2.9 | 4.5 | | 4.5 | | 2.3 | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | | 0.0 | | |
| Total Lost Time (s) | | | 7.0 | 7.0 | 6.5 | 7.0 | | 7.0 | | 7.0 | | |
| Lead/Lag | | | Lag | Lead | Lag | Lead | | Lead | | Lag | Lag | Lead |
| Lead-Lag Optimize? | | | Yes | Yes | Yes | Yes | | Yes | | Yes | Yes | Yes |
| Recall Mode | | | None | None | None | None | | None | | None | Min | None |

Intersection Summary

Cycle Length: 179
 Actuated Cycle Length: 119.2
 Natural Cycle: 160
 Control Type: Actuated-Uncoordinated

Splits and Phases: 1: Mathilda Ave & 5th Ave



| Lane Group | ø9 | ø13 |
|----------------------|------|------|
| Lane Configurations | | |
| Volume (vph) | | |
| Turn Type | | |
| Protected Phases | 9 | 13 |
| Permitted Phases | | |
| Detector Phase | | |
| Switch Phase | | |
| Minimum Initial (s) | 28.0 | 8.0 |
| Minimum Split (s) | 35.0 | 15.0 |
| Total Split (s) | 35.0 | 15.0 |
| Total Split (%) | 20% | 8% |
| Yellow Time (s) | 4.7 | 3.6 |
| All-Red Time (s) | 2.3 | 3.4 |
| Lost Time Adjust (s) | | |
| Total Lost Time (s) | | |
| Lead/Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes |
| Recall Mode | None | None |
| Intersection Summary | | |

Lanes, Volumes, Timings
 2: Mathilda Ave & Innovation Way

3/4/2016

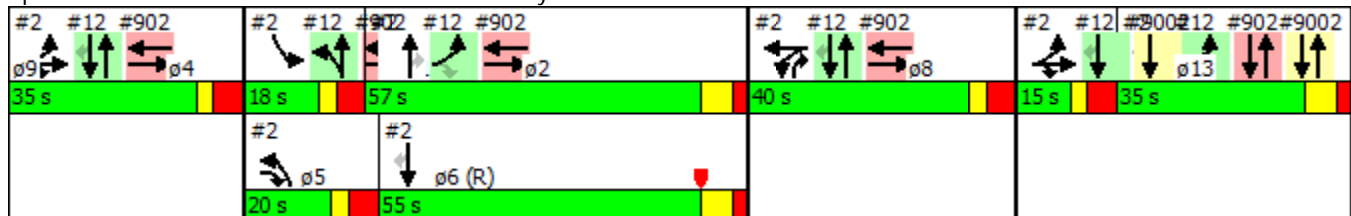


| Lane Group | EBT | EBR | WBL | WBT | NBL | NBT | NBR | SBL | SBT | SBR | ø2 | ø4 |
|----------------------|------|--------|-------|-------|-------|-----|-------|------|------|------|------|------|
| Lane Configurations | ↕ | ↕↕ | ↕ | ↕↕ | ↕↕ | ↕↕ | ↕ | ↕ | ↕↕↕ | ↕ | | |
| Volume (vph) | 320 | 910 | 735 | 190 | 70 | 470 | 390 | 80 | 1430 | 70 | | |
| Turn Type | NA | pt+ov | Split | NA | Prot | NA | pm+ov | Prot | NA | Perm | | |
| Protected Phases | 4 13 | 4 13 5 | 8 | 8 | 5 | 2 9 | 8 | 1 | 6 9 | | 2 | 4 |
| Permitted Phases | | | | | | | 2 9 | | | | | 6 9 |
| Detector Phase | 4 | 4 | 8 | 8 | 5 | 2 | 2 | 1 | 6 | 6 | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 10.0 | 10.0 | 13.0 | | 10.0 | 10.0 | | | 12.0 | 14.0 |
| Minimum Split (s) | | | 35.0 | 35.0 | 20.0 | | 35.0 | 16.8 | | | 19.0 | 39.0 |
| Total Split (s) | | | 40.0 | 40.0 | 20.0 | | 40.0 | 18.0 | | | 57.0 | 35.0 |
| Total Split (%) | | | 20.0% | 20.0% | 10.0% | | 20.0% | 9.0% | | | 29% | 18% |
| Yellow Time (s) | | | 2.5 | 2.5 | 2.5 | | 2.5 | 2.5 | | | 4.7 | 2.5 |
| All-Red Time (s) | | | 4.5 | 4.5 | 4.5 | | 4.5 | 4.3 | | | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | | | | |
| Total Lost Time (s) | | | 7.0 | 7.0 | 7.0 | | 7.0 | 6.8 | | | | |
| Lead/Lag | | | | | Lead | | | Lead | | | Lag | |
| Lead-Lag Optimize? | | | | | Yes | | | Yes | | | Yes | |
| Recall Mode | | | None | None | None | | None | None | | | Max | None |

Intersection Summary

Cycle Length: 200
 Actuated Cycle Length: 200
 Offset: 0 (0%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 175
 Control Type: Actuated-Coordinated

Splits and Phases: 2: Mathilda Ave & Innovation Way



Lanes, Volumes, Timings
 2: Mathilda Ave & Innovation Way

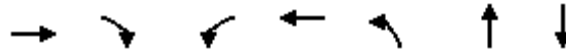
3/4/2016

| Lane Group | ø6 | ø9 | ø13 |
|----------------------|-------|------|------|
| Lane Configurations | | | |
| Volume (vph) | | | |
| Turn Type | | | |
| Protected Phases | 6 | 9 | 13 |
| Permitted Phases | | | |
| Detector Phase | | | |
| Switch Phase | | | |
| Minimum Initial (s) | 12.0 | 28.0 | 8.0 |
| Minimum Split (s) | 30.0 | 35.0 | 15.0 |
| Total Split (s) | 55.0 | 35.0 | 15.0 |
| Total Split (%) | 28% | 18% | 8% |
| Yellow Time (s) | 4.7 | 4.7 | 2.5 |
| All-Red Time (s) | 2.3 | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | |
| Total Lost Time (s) | | | |
| Lead/Lag | Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes | Yes |
| Recall Mode | C-Min | None | None |
| Intersection Summary | | | |

Lanes, Volumes, Timings

3: Mathilda Ave & Moffett Park Dr/SR 237 WB Off-Ramp

3/4/2016

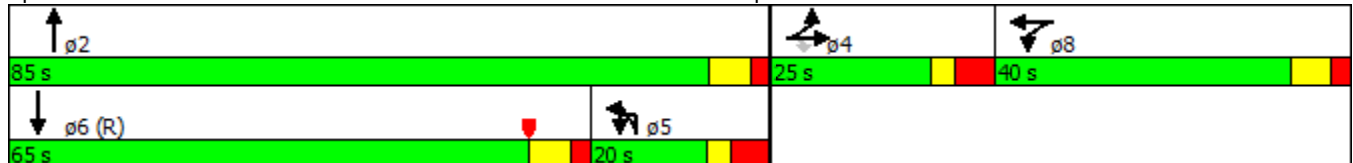


| Lane Group | EBT | EBR | WBL | WBT | NBL | NBT | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | |
| Volume (vph) | 0 | 870 | 820 | 120 | 180 | 630 | 2680 |
| Turn Type | NA | Perm | Split | NA | Prot | NA | NA |
| Protected Phases | 4 | | 8 | 8 | 5 | 2 | 6 |
| Permitted Phases | | 4 | | | | | |
| Detector Phase | 4 | 4 | 8 | 8 | 5 | 2 | 6 |
| Switch Phase | | | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 8.0 | 8.0 |
| Minimum Split (s) | 11.0 | 11.0 | 40.0 | 40.0 | 11.0 | 26.9 | 14.9 |
| Total Split (s) | 25.0 | 25.0 | 40.0 | 40.0 | 20.0 | 85.0 | 65.0 |
| Total Split (%) | 16.7% | 16.7% | 26.7% | 26.7% | 13.3% | 56.7% | 43.3% |
| Yellow Time (s) | 2.5 | 2.5 | 4.5 | 4.5 | 2.5 | 4.7 | 4.7 |
| All-Red Time (s) | 4.5 | 4.5 | 2.5 | 2.5 | 4.5 | 2.2 | 2.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.9 | 6.9 |
| Lead/Lag | | | | | Lag | | Lead |
| Lead-Lag Optimize? | | | | | Yes | | Yes |
| Recall Mode | None | None | None | None | Max | None | C-Max |

Intersection Summary

Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 0 (0%), Referenced to phase 6:SBT, Start of Yellow, Master Intersection
 Natural Cycle: 150
 Control Type: Actuated-Coordinated

Splits and Phases: 3: Mathilda Ave & Moffett Park Dr/SR 237 WB Off-Ramp



Lanes, Volumes, Timings
 4: Mathilda Ave & SR 237 EB Ramps

3/4/2016

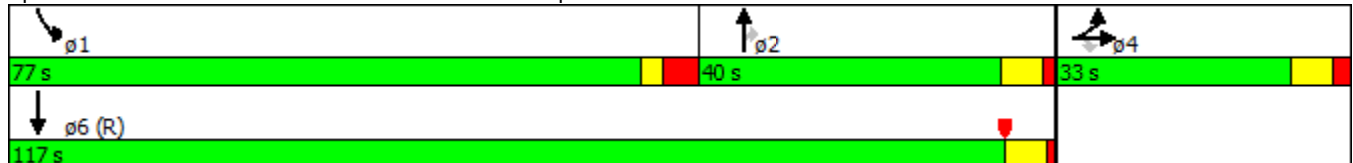


| Lane Group | EBL | EBT | EBR | NBT | NBR | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | |
| Volume (vph) | 220 | 0 | 210 | 700 | 860 | 460 | 3160 |
| Turn Type | Split | NA | Perm | NA | Perm | Prot | NA |
| Protected Phases | 4 | 4 | | 2 | | 1 | 6 |
| Permitted Phases | | | 4 | | 2 | | |
| Detector Phase | 4 | 4 | 4 | 2 | 2 | 1 | 6 |
| Switch Phase | | | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 4.0 | 8.0 | 8.0 | 4.0 | 8.0 |
| Minimum Split (s) | 11.0 | 11.0 | 11.0 | 18.2 | 18.2 | 10.4 | 13.9 |
| Total Split (s) | 33.0 | 33.0 | 33.0 | 40.0 | 40.0 | 77.0 | 117.0 |
| Total Split (%) | 22.0% | 22.0% | 22.0% | 26.7% | 26.7% | 51.3% | 78.0% |
| Yellow Time (s) | 4.8 | 4.8 | 4.8 | 4.7 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 2.2 | 2.2 | 2.2 | 1.5 | 1.5 | 3.9 | 1.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 6.2 | 6.2 | 6.4 | 5.9 |
| Lead/Lag | | | | Lag | Lag | Lead | |
| Lead-Lag Optimize? | | | | Yes | Yes | Yes | |
| Recall Mode | None | None | None | None | None | None | C-Max |

Intersection Summary

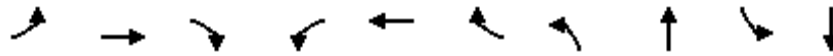
Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 10 (7%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 60
 Control Type: Actuated-Coordinated

Splits and Phases: 4: Mathilda Ave & SR 237 EB Ramps



Lanes, Volumes, Timings
5: Mathilda Ave & Ross Dr

3/4/2016

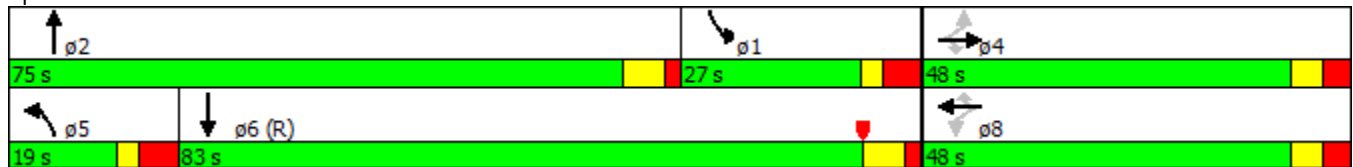


| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↖ | ↑ | ↗ | ↖ | ↑ | ↗ | ↖ | ↑↑↑↑ | ↖ | ↑↑↑ |
| Volume (vph) | 60 | 200 | 60 | 290 | 70 | 130 | 160 | 1370 | 180 | 3110 |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | Prot | NA | Prot | NA |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | 1 | 6 |
| Permitted Phases | 4 | | 4 | 8 | | 8 | | | | |
| Detector Phase | 4 | 4 | 4 | 8 | 8 | 8 | 5 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 4.0 | 5.0 | 4.0 | 5.0 |
| Minimum Split (s) | 48.0 | 48.0 | 48.0 | 19.0 | 19.0 | 19.0 | 11.0 | 31.4 | 11.0 | 11.6 |
| Total Split (s) | 48.0 | 48.0 | 48.0 | 48.0 | 48.0 | 48.0 | 19.0 | 75.0 | 27.0 | 83.0 |
| Total Split (%) | 32.0% | 32.0% | 32.0% | 32.0% | 32.0% | 32.0% | 12.7% | 50.0% | 18.0% | 55.3% |
| Yellow Time (s) | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 2.5 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 3.4 | 3.4 | 3.4 | 3.4 | 3.4 | 3.4 | 4.5 | 1.7 | 4.5 | 1.9 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.4 | 7.0 | 6.6 |
| Lead/Lag | | | | | | | Lead | Lead | Lag | Lag |
| Lead-Lag Optimize? | | | | | | | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | Max | Max | Max | Max | None | None | C-Max |

Intersection Summary

Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 20 (13%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 145
 Control Type: Actuated-Coordinated

Splits and Phases: 5: Mathilda Ave & Ross Dr



Lanes, Volumes, Timings
 6: Mathilda Ave & US 101 NB Ramps

3/4/2016



| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↖↗ | ↖↗ | ↑↑↑ | ↖ | ↖ | ↑↑↑ |
| Volume (vph) | 850 | 280 | 1600 | 340 | 40 | 3420 |
| Turn Type | Prot | pm+ov | NA | Perm | Prot | NA |
| Protected Phases | 8 | 1 | 2 | | 1 | 6 |
| Permitted Phases | | 8 | | 2 | | |
| Detector Phase | 8 | 1 | 2 | 2 | 1 | 6 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 8.0 | 4.0 | 8.0 | 8.0 | 4.0 | 4.0 |
| Minimum Split (s) | 14.9 | 9.7 | 39.9 | 39.9 | 9.7 | 10.9 |
| Total Split (s) | 48.0 | 18.0 | 84.0 | 84.0 | 18.0 | 102.0 |
| Total Split (%) | 32.0% | 12.0% | 56.0% | 56.0% | 12.0% | 68.0% |
| Yellow Time (s) | 4.7 | 3.5 | 4.7 | 4.7 | 3.5 | 4.7 |
| All-Red Time (s) | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.9 | 5.7 | 6.9 | 6.9 | 5.7 | 6.9 |
| Lead/Lag | | Lead | Lag | Lag | Lead | |
| Lead-Lag Optimize? | | Yes | Yes | Yes | Yes | |
| Recall Mode | None | None | None | None | None | C-Max |

Intersection Summary

Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 27 (18%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 140
 Control Type: Actuated-Coordinated

Splits and Phases: 6: Mathilda Ave & US 101 NB Ramps



Lanes, Volumes, Timings
 7: Mathilda Ave & US 101 SB Ramps

3/4/2016



| Lane Group | EBL | EBR | NBT | NBR | SBT |
|----------------------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | |
| Volume (vph) | 140 | 550 | 1800 | 680 | 2810 |
| Turn Type | Prot | Prot | NA | Perm | NA |
| Protected Phases | 7 | 7 | 2 | | 6 |
| Permitted Phases | | | | 2 | |
| Detector Phase | 7 | 7 | 2 | 2 | 6 |
| Switch Phase | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 8.0 | 8.0 | 8.0 |
| Minimum Split (s) | 10.9 | 10.9 | 14.9 | 14.9 | 14.9 |
| Total Split (s) | 35.0 | 35.0 | 115.0 | 115.0 | 115.0 |
| Total Split (%) | 23.3% | 23.3% | 76.7% | 76.7% | 76.7% |
| Yellow Time (s) | 4.7 | 4.7 | 4.7 | 4.7 | 4.7 |
| All-Red Time (s) | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.9 | 6.9 | 6.9 | 6.9 | 6.9 |
| Lead/Lag | | | | | |
| Lead-Lag Optimize? | | | | | |
| Recall Mode | None | None | None | None | C-Max |

Intersection Summary

Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 27 (18%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 150
 Control Type: Actuated-Coordinated

Splits and Phases: 7: Mathilda Ave & US 101 SB Ramps



Lanes, Volumes, Timings
 8: Mathilda Ave & Almanor Ave/Ahwanee Ave

3/4/2016

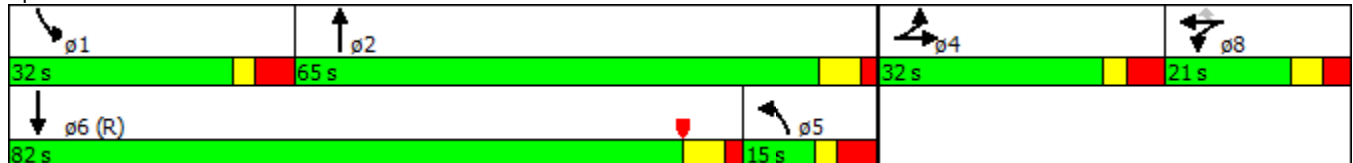


| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↖↗ | ↖ | ↖ | ↖ | ↖ | ↖ | ↑↑↑ | ↖ | ↑↑↑ |
| Volume (vph) | 430 | 40 | 60 | 30 | 260 | 80 | 1790 | 260 | 3000 |
| Turn Type | Split | NA | Split | NA | Perm | Prot | NA | Prot | NA |
| Protected Phases | 4 | 4 | 8 | 8 | | 5 | 2 | 1 | 6 |
| Permitted Phases | | | | | 8 | | | | |
| Detector Phase | 4 | 4 | 8 | 8 | 8 | 5 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | | |
| Minimum Initial (s) | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 12.0 | 8.0 | 12.0 |
| Minimum Split (s) | 32.0 | 32.0 | 15.0 | 15.0 | 15.0 | 15.0 | 36.7 | 15.0 | 18.7 |
| Total Split (s) | 32.0 | 32.0 | 21.0 | 21.0 | 21.0 | 15.0 | 65.0 | 32.0 | 82.0 |
| Total Split (%) | 21.3% | 21.3% | 14.0% | 14.0% | 14.0% | 10.0% | 43.3% | 21.3% | 54.7% |
| Yellow Time (s) | 2.8 | 2.8 | 3.6 | 3.6 | 3.6 | 2.5 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 4.2 | 4.2 | 3.4 | 3.4 | 3.4 | 4.5 | 2.0 | 4.5 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.7 | 7.0 | 6.7 |
| Lead/Lag | | | | | | Lag | Lag | Lead | Lead |
| Lead-Lag Optimize? | | | | | | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | None | None | None | C-Max |

Intersection Summary

Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 3 (2%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 130
 Control Type: Actuated-Coordinated

Splits and Phases: 8: Mathilda Ave & Almanor Ave/Ahwanee Ave



Lanes, Volumes, Timings
 9: US 101 On-Ramp & Moffett Park Dr

3/4/2016



| Lane Group | EBT | EBR | WBL | WBT |
|----------------------|-------|-------|-------|--------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ |
| Volume (vph) | 1010 | 150 | 350 | 315 |
| Turn Type | NA | Perm | Prot | NA |
| Protected Phases | 2 | | 1 | 6 |
| Permitted Phases | | 2 | | |
| Detector Phase | 2 | 2 | 1 | 6 |
| Switch Phase | | | | |
| Minimum Initial (s) | 15.0 | 15.0 | 6.0 | 15.0 |
| Minimum Split (s) | 20.0 | 20.0 | 10.5 | 20.0 |
| Total Split (s) | 52.0 | 52.0 | 23.0 | 75.0 |
| Total Split (%) | 69.3% | 69.3% | 30.7% | 100.0% |
| Yellow Time (s) | 4.0 | 4.0 | 3.5 | 4.0 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.0 | 5.0 | 4.5 | 5.0 |
| Lead/Lag | Lag | Lag | Lead | |
| Lead-Lag Optimize? | | | | |
| Recall Mode | Min | Min | None | Min |

Intersection Summary

Cycle Length: 75
 Actuated Cycle Length: 67.6
 Natural Cycle: 70
 Control Type: Actuated-Uncoordinated

Splits and Phases: 9: US 101 On-Ramp & Moffett Park Dr



Lanes, Volumes, Timings
 10: Moffett Park Dr & Innovation Way

3/4/2016

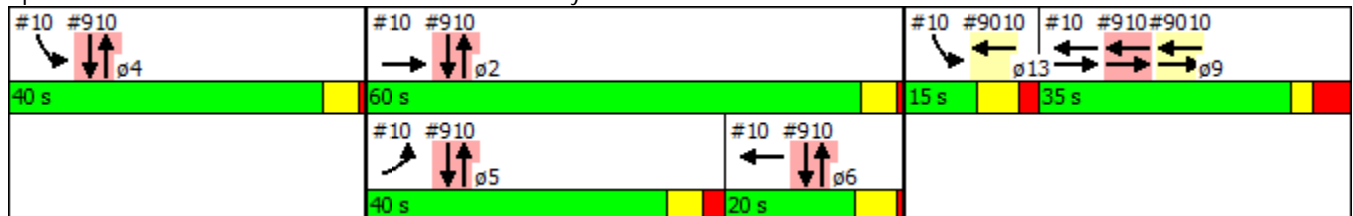


| Lane Group | EBL | EBT | WBT | SBL | ø2 | ø4 | ø6 | ø9 | ø13 |
|----------------------|-------|-----|-----|------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | |
| Volume (vph) | 330 | 680 | 475 | 370 | | | | | |
| Turn Type | Prot | NA | NA | Prot | | | | | |
| Protected Phases | 5 | 2 9 | 6 9 | 4 13 | 2 | 4 | 6 | 9 | 13 |
| Permitted Phases | | | | | | | | | |
| Detector Phase | 5 | 2 | 6 | 4 | | | | | |
| Switch Phase | | | | | | | | | |
| Minimum Initial (s) | 8.0 | | | | 10.0 | 10.0 | 10.0 | 28.0 | 8.0 |
| Minimum Split (s) | 14.5 | | | | 14.9 | 15.0 | 27.5 | 35.0 | 15.0 |
| Total Split (s) | 40.0 | | | | 60.0 | 40.0 | 20.0 | 35.0 | 15.0 |
| Total Split (%) | 26.7% | | | | 40% | 27% | 13% | 23% | 10% |
| Yellow Time (s) | 4.0 | | | | 3.9 | 4.0 | 4.5 | 2.5 | 4.7 |
| All-Red Time (s) | 2.5 | | | | 1.0 | 1.0 | 1.0 | 4.5 | 2.3 |
| Lost Time Adjust (s) | 0.0 | | | | | | | | |
| Total Lost Time (s) | 6.5 | | | | | | | | |
| Lead/Lag | Lead | | | | | | Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | | | | | | Yes | Yes | Yes |
| Recall Mode | Max | | | | Min | None | Min | None | None |

Intersection Summary

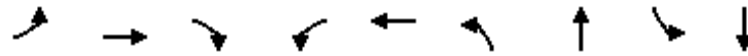
Cycle Length: 150
 Actuated Cycle Length: 110.9
 Natural Cycle: 120
 Control Type: Semi Act-Uncoord

Splits and Phases: 10: Moffett Park Dr & Innovation Way



Lanes, Volumes, Timings
 11: Innovation Way & 11th Ave

3/4/2016



| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT |
|---------------------|-----|------|-----|-----|------|-----|------|-----|------|
| Lane Configurations | | | | | | | | | |
| Volume (vph) | 500 | 0 | 340 | 40 | 0 | 80 | 400 | 110 | 110 |
| Sign Control | | Stop | | | Stop | | Stop | | Stop |

Intersection Summary

Control Type: Unsignalized

Lanes, Volumes, Timings
 12: Innovation Way & Juniper Driveway

3/4/2016

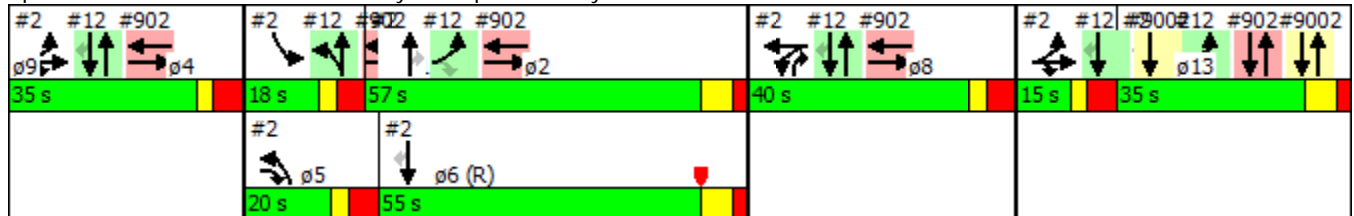


| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR | ø2 | ø4 | ø5 | ø6 | ø8 | ø9 |
|----------------------|------|------|------|-------|--------|--------|------|------|------|-------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 700 | 80 | 60 | 860 | 160 | 170 | | | | | | |
| Turn Type | Prot | Perm | Prot | NA | NA | Perm | | | | | | |
| Protected Phases | 2 9 | | 1 | 1 4 8 | 4 8 13 | | 2 | 4 | 5 | 6 | 8 | 9 |
| Permitted Phases | | 2 9 | | | | 4 8 13 | | | | | | |
| Detector Phase | 2 | 2 | 1 | 1 4 8 | 4 8 | 4 8 | | | | | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 10.0 | | | | 12.0 | 14.0 | 13.0 | 12.0 | 10.0 | 28.0 |
| Minimum Split (s) | | | 16.8 | | | | 19.0 | 39.0 | 20.0 | 30.0 | 35.0 | 35.0 |
| Total Split (s) | | | 18.0 | | | | 57.0 | 35.0 | 20.0 | 55.0 | 40.0 | 35.0 |
| Total Split (%) | | | 9.0% | | | | 29% | 18% | 10% | 28% | 20% | 18% |
| Yellow Time (s) | | | 2.5 | | | | 4.7 | 2.5 | 2.5 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | | | 4.3 | | | | 2.3 | 4.5 | 4.5 | 2.3 | 4.5 | 2.3 |
| Lost Time Adjust (s) | | | 0.0 | | | | | | | | | |
| Total Lost Time (s) | | | 6.8 | | | | | | | | | |
| Lead/Lag | | | Lead | | | | Lag | Lead | Lag | Lag | Lag | Lag |
| Lead-Lag Optimize? | | | Yes | | | | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | | | None | | | | Max | None | None | C-Min | None | None |

Intersection Summary

Cycle Length: 200
 Actuated Cycle Length: 200
 Offset: 0 (0%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 175
 Control Type: Actuated-Coordinated

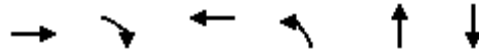
Splits and Phases: 12: Innovation Way & Juniper Driveway



| | |
|-----------------------------|------|
| Lane Group | ø13 |
| Lane Configurations | |
| Volume (vph) | |
| Turn Type | |
| Protected Phases | 13 |
| Permitted Phases | |
| Detector Phase | |
| Switch Phase | |
| Minimum Initial (s) | 8.0 |
| Minimum Split (s) | 15.0 |
| Total Split (s) | 15.0 |
| Total Split (%) | 8% |
| Yellow Time (s) | 2.5 |
| All-Red Time (s) | 4.5 |
| Lost Time Adjust (s) | |
| Total Lost Time (s) | |
| Lead/Lag | Lead |
| Lead-Lag Optimize? | Yes |
| Recall Mode | None |
| Intersection Summary | |

Lanes, Volumes, Timings
 13: Bordeaux Dr & Innovation Way

3/4/2016

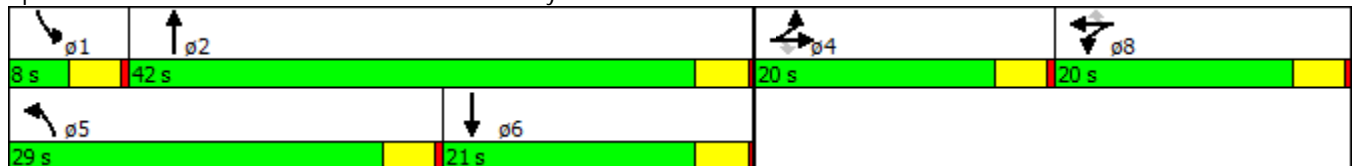


| Lane Group | EBT | EBR | WBT | NBL | NBT | SBT | ø1 |
|----------------------|-------|-------|-------|-------|-------|-------|------|
| Lane Configurations | ↕ | ↗ | ↕ | ↖ | ↗ | ↗ | |
| Volume (vph) | 30 | 230 | 30 | 630 | 50 | 180 | |
| Turn Type | NA | Perm | NA | Prot | NA | NA | |
| Protected Phases | 4 | | 8 | 5 | 2 | 6 | 1 |
| Permitted Phases | | 4 | | | | | |
| Detector Phase | 4 | 4 | 8 | 5 | 2 | 6 | |
| Switch Phase | | | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | 20.0 | 20.0 | 20.0 | 8.0 | 20.0 | 20.0 | 8.0 |
| Total Split (s) | 20.0 | 20.0 | 20.0 | 29.0 | 42.0 | 21.0 | 8.0 |
| Total Split (%) | 22.2% | 22.2% | 22.2% | 32.2% | 46.7% | 23.3% | 9% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Lead/Lag | | | | Lead | Lag | Lag | Lead |
| Lead-Lag Optimize? | | | | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | None | None |

Intersection Summary

Cycle Length: 90
 Actuated Cycle Length: 69.3
 Natural Cycle: 100
 Control Type: Actuated-Uncoordinated

Splits and Phases: 13: Bordeaux Dr & Innovation Way



**SimTraffic Post-Processor
Average Results from 10 Runs
Network Performance**

**Mathilda Avenue Improvements
Alternative 1 Year 2040
PM Peak Hour**

| Performance Measure | Average | Std. Dev. | Minimum | Maximum |
|---------------------------------|---------|-----------|---------|---------|
| Average Delay (seconds) | 750.0 | 36.6 | 673.0 | 802.8 |
| Total Delay (hours) | 3,131 | 158 | 2,773 | 3,353 |
| Average Stopped Delay (seconds) | 700.8 | 36.5 | 626.6 | 752.8 |
| Total Stopped Delay (hours) | 2926 | 157 | 2582 | 3144 |
| Total Stops | 46,461 | 3,369 | 41,051 | 50,025 |
| Average Stops | 3.09 | 0.22 | 2.76 | 3.36 |
| Total Distance Traveled (miles) | 43,213 | 1,003 | 41,139 | 44,360 |
| Average Speed (mph) | 10.1 | 0.6 | 9.0 | 11.0 |
| Total Travel Time (hours) | 4,588.3 | 141.1 | 4,286.9 | 4,725.2 |
| Vehicles Entered | 12,144 | 112 | 12,010 | 12,335 |
| Vehicles Exited | 9,447 | 291 | 8,945 | 9,873 |
| Percent Demand Served | 77.8% | 2.1% | 74.1% | 81.7% |
| Fuel Used (gallons) | 1,866 | 25 | 1,823 | 1,903 |
| HC Emissions (grams) | 18,989 | 1,324 | 17,237 | 21,171 |
| CO Emissions (grams) | 531,324 | 23,124 | 499,096 | 566,150 |
| NOx Emissions (grams) | 67,226 | 3,127 | 62,534 | 71,857 |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Alternative 1 Year 2040
PM Peak Hour

Intersection 1 Mathilda Avenue/5th Avenue Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 140 | 94 | 67.2% | 56.3 | 6.5 | E |
| | Through | 660 | 440 | 66.7% | 17.0 | 1.4 | B |
| | Right Turn | 60 | 38 | 63.2% | 12.0 | 3.4 | B |
| | Subtotal | 860 | 572 | 66.6% | 23.1 | 2.1 | C |
| SB | Left Turn | 20 | 14 | 70.0% | 620.3 | 182.0 | F |
| | Through | 1,120 | 765 | 68.3% | 699.3 | 185.5 | F |
| | Right Turn | 30 | 20 | 65.3% | 645.9 | 180.2 | F |
| | Subtotal | 1,170 | 799 | 68.3% | 696.7 | 184.8 | F |
| EB | Left Turn | 180 | 177 | 98.4% | 67.5 | 39.9 | E |
| | Through | 40 | 39 | 97.5% | 89.6 | 42.9 | F |
| | Right Turn | 170 | 169 | 99.1% | 65.5 | 40.7 | E |
| | Subtotal | 390 | 385 | 98.6% | 68.8 | 40.4 | E |
| WB | Left Turn | 290 | 100 | 34.6% | 79.3 | 28.5 | E |
| | Through | 20 | 6 | 28.5% | 89.6 | 44.1 | F |
| | Right Turn | 110 | 37 | 33.8% | 39.8 | 23.4 | D |
| | Subtotal | 420 | 143 | 34.1% | 69.3 | 26.3 | E |
| Total | | 2,840 | 1,899 | 66.9% | 315.9 | 70.8 | F |

Intersection 2 Mathilda Avenue/Innovation Way-Driveway Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 70 | 57 | 81.6% | 94.4 | 13.4 | F |
| | Through | 470 | 372 | 79.2% | 43.2 | 4.1 | D |
| | Right Turn | 390 | 309 | 79.3% | 17.8 | 4.4 | B |
| | Subtotal | 930 | 739 | 79.5% | 36.5 | 3.2 | D |
| SB | Left Turn | 80 | 53 | 66.5% | 436.7 | 39.9 | F |
| | Through | 1,430 | 911 | 63.7% | 408.2 | 23.5 | F |
| | Right Turn | 70 | 43 | 61.9% | 360.7 | 44.8 | F |
| | Subtotal | 1,580 | 1,008 | 63.8% | 407.6 | 23.9 | F |
| EB | Left Turn | 330 | 173 | 52.3% | 87.3 | 13.9 | F |
| | Through | 320 | 169 | 52.7% | 89.0 | 13.9 | F |
| | Right Turn | 910 | 452 | 49.7% | 91.6 | 14.5 | F |
| | Subtotal | 1,560 | 794 | 50.9% | 90.1 | 14.2 | F |
| WB | Left Turn | 735 | 251 | 34.1% | 374.3 | 24.7 | F |
| | Through | 190 | 61 | 32.1% | 402.4 | 33.5 | F |
| | Right Turn | 60 | 22 | 36.2% | 393.2 | 36.8 | F |
| | Subtotal | 985 | 333 | 33.8% | 380.9 | 26.0 | F |
| Total | | 5,055 | 2,873 | 56.8% | 220.9 | 8.3 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Alternative 1 Year 2040
PM Peak Hour

Intersection 3 Mathilda Avenue/Moffett Park Drive-SR 237 WB Off-Ramp Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | 290 | 224 | 77.2% | 160.9 | 94.5 | F |
| | Through | 630 | 546 | 86.7% | 32.6 | 16.9 | C |
| | Right Turn | | | | | | |
| | Subtotal | 920 | 770 | 83.7% | 67.7 | 33.2 | E |
| SB | Left Turn | | | | | | |
| | Through | 2,680 | 1,389 | 51.8% | 200.7 | 13.9 | F |
| | Right Turn | 395 | 215 | 54.4% | 246.5 | 22.2 | F |
| | Subtotal | 3,075 | 1,603 | 52.1% | 206.8 | 13.8 | F |
| EB | Left Turn | 180 | 97 | 54.1% | 613.5 | 177.7 | F |
| | Through | | | | | | |
| | Right Turn | 870 | 511 | 58.7% | 398.0 | 29.4 | F |
| | Subtotal | 1,050 | 609 | 58.0% | 430.2 | 38.0 | F |
| WB | Left Turn | 820 | 642 | 78.2% | 296.9 | 57.3 | F |
| | Through | 120 | 98 | 81.9% | 75.8 | 18.5 | E |
| | Right Turn | 120 | 95 | 79.4% | 59.5 | 26.6 | E |
| | Subtotal | 1,060 | 835 | 78.8% | 243.9 | 49.1 | F |
| Total | | 6,105 | 3,817 | 62.5% | 221.4 | 22.4 | F |

Intersection 4 Mathilda Avenue/SR 237 EB Ramps Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | | | | | | |
| | Through | 700 | 577 | 82.4% | 38.0 | 22.3 | D |
| | Right Turn | 860 | 723 | 84.1% | 57.2 | 9.6 | E |
| | Subtotal | 1,560 | 1,300 | 83.3% | 48.6 | 9.8 | D |
| SB | Left Turn | 460 | 256 | 55.7% | 105.9 | 28.4 | F |
| | Through | 3,160 | 1,877 | 59.4% | 27.9 | 4.4 | C |
| | Right Turn | | | | | | |
| | Subtotal | 3,620 | 2,133 | 58.9% | 37.2 | 5.2 | D |
| EB | Left Turn | 220 | 201 | 91.1% | 111.5 | 65.5 | F |
| | Through | | | | | | |
| | Right Turn | 210 | 201 | 95.9% | 68.2 | 27.8 | E |
| | Subtotal | 430 | 402 | 93.5% | 88.4 | 35.6 | F |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 5,610 | 3,835 | 68.4% | 46.5 | 9.4 | D |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Alternative 1 Year 2040
PM Peak Hour

Intersection 5 Mathilda Avenue/Ross Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | 160 | 134 | 83.7% | 219.4 | 39.5 | F |
| | Through | 1,370 | 1,169 | 85.4% | 147.0 | 29.6 | F |
| | Right Turn | 350 | 295 | 84.4% | 204.0 | 52.4 | F |
| | Subtotal | 1,880 | 1,599 | 85.0% | 163.7 | 31.2 | F |
| SB | Left Turn | 180 | 106 | 58.8% | 57.0 | 7.5 | E |
| | Through | 3,110 | 1,930 | 62.1% | 29.5 | 3.7 | C |
| | Right Turn | 80 | 52 | 64.9% | 21.8 | 4.1 | C |
| | Subtotal | 3,370 | 2,088 | 62.0% | 30.7 | 3.5 | C |
| EB | Left Turn | 60 | 55 | 92.2% | 56.6 | 12.7 | E |
| | Through | 200 | 204 | 102.1% | 52.5 | 11.5 | D |
| | Right Turn | 60 | 63 | 105.3% | 35.4 | 8.6 | D |
| | Subtotal | 320 | 323 | 100.8% | 49.7 | 10.0 | D |
| WB | Left Turn | 290 | 179 | 61.8% | 989.8 | 167.2 | F |
| | Through | 70 | 46 | 66.3% | 986.4 | 169.5 | F |
| | Right Turn | 130 | 82 | 63.4% | 979.8 | 191.0 | F |
| | Subtotal | 490 | 308 | 62.8% | 986.0 | 172.7 | F |
| Total | | 6,060 | 4,317 | 71.2% | 148.3 | 17.8 | F |

Intersection 6 Mathilda Avenue/US 101 NB Ramps Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | | | | | | |
| | Through | 1,600 | 1,407 | 87.9% | 95.0 | 35.7 | F |
| | Right Turn | 340 | 307 | 90.4% | 8.9 | 2.5 | A |
| | Subtotal | 1,940 | 1,714 | 88.4% | 79.7 | 30.1 | E |
| SB | Left Turn | 40 | 24 | 59.8% | 88.2 | 11.3 | F |
| | Through | 3,420 | 2,160 | 63.2% | 48.7 | 6.0 | D |
| | Right Turn | | | | | | |
| | Subtotal | 3,460 | 2,184 | 63.1% | 49.1 | 5.8 | D |
| EB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| WB | Left Turn | 850 | 711 | 83.6% | 335.1 | 199.0 | F |
| | Through | | | | | | |
| | Right Turn | 280 | 232 | 82.7% | 325.8 | 198.2 | F |
| | Subtotal | 1,130 | 942 | 83.4% | 332.9 | 198.7 | F |
| Total | | 6,530 | 4,840 | 74.1% | 112.6 | 41.2 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Alternative 1 Year 2040
PM Peak Hour

Intersection 7 Mathilda Avenue/US 101 SB Ramps Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | | | | | | |
| | Through | 1,800 | 1,630 | 90.6% | 53.6 | 32.8 | D |
| | Right Turn | 680 | 638 | 93.9% | 17.6 | 4.7 | B |
| | Subtotal | 2,480 | 2,269 | 91.5% | 43.5 | 25.0 | D |
| SB | Left Turn | | | | | | |
| | Through | 2,810 | 1,960 | 69.7% | 9.6 | 1.9 | A |
| | Right Turn | 1,460 | 916 | 62.7% | 18.9 | 3.3 | B |
| | Subtotal | 4,270 | 2,875 | 67.3% | 12.5 | 2.2 | B |
| EB | Left Turn | 140 | 127 | 90.7% | 133.2 | 49.3 | F |
| | Through | | | | | | |
| | Right Turn | 550 | 557 | 101.3% | 34.8 | 10.9 | C |
| | Subtotal | 690 | 684 | 99.1% | 52.8 | 17.3 | D |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 7,440 | 5,828 | 78.3% | 29.0 | 11.7 | C |

Intersection 8 Mathilda Avenue/Almanor Avenue-Ahwanee Avenue Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | LOS |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | |
| NB | Left Turn | 80 | 73 | 91.5% | 176.4 | 95.5 | F |
| | Through | 1,790 | 1,653 | 92.3% | 133.3 | 115.1 | F |
| | Right Turn | 60 | 56 | 93.2% | 126.2 | 119.9 | F |
| | Subtotal | 1,930 | 1,782 | 92.3% | 134.9 | 114.3 | F |
| SB | Left Turn | 260 | 197 | 75.7% | 95.3 | 11.1 | F |
| | Through | 3,000 | 2,242 | 74.7% | 23.9 | 1.3 | C |
| | Right Turn | 100 | 77 | 77.2% | 18.8 | 3.0 | B |
| | Subtotal | 3,360 | 2,516 | 74.9% | 29.4 | 2.0 | C |
| EB | Left Turn | 430 | 423 | 98.3% | 104.7 | 9.5 | F |
| | Through | 40 | 39 | 97.5% | 107.2 | 11.4 | F |
| | Right Turn | 90 | 93 | 102.8% | 74.8 | 7.2 | E |
| | Subtotal | 560 | 554 | 99.0% | 99.9 | 9.0 | F |
| WB | Left Turn | 60 | 64 | 106.0% | 64.3 | 12.1 | E |
| | Through | 30 | 31 | 103.3% | 64.0 | 7.1 | E |
| | Right Turn | 260 | 254 | 97.8% | 21.8 | 6.4 | C |
| | Subtotal | 350 | 349 | 99.7% | 33.2 | 6.4 | C |
| Total | | 6,200 | 5,201 | 83.9% | 71.5 | 34.1 | E |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Alternative 1 Year 2040
PM Peak Hour

Intersection 9 US 101 NB Slip Ramp/Moffett Park Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| EB | Left Turn | | | | | | |
| | Through | 1,010 | 615 | 60.9% | 134.4 | 34.5 | F |
| | Right Turn | 150 | 92 | 61.0% | 74.0 | 20.6 | E |
| | Subtotal | 1,160 | 707 | 60.9% | 126.5 | 32.2 | F |
| WB | Left Turn | 350 | 211 | 60.3% | 27.9 | 2.5 | C |
| | Through | 315 | 197 | 62.5% | 3.6 | 0.4 | A |
| | Right Turn | | | | | | |
| | Subtotal | 665 | 408 | 61.3% | 16.2 | 1.4 | B |
| Total | | 1,825 | 1,115 | 61.1% | 85.4 | 17.9 | F |

Intersection 10 Innovation Way/Moffett Park Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | 370 | 195 | 52.6% | 520.4 | 150.1 | F |
| | Through | | | | | | |
| | Right Turn | 190 | 97 | 50.8% | 497.7 | 141.7 | F |
| | Subtotal | 560 | 291 | 52.0% | 513.0 | 147.6 | F |
| EB | Left Turn | 330 | 195 | 59.0% | 246.5 | 47.8 | F |
| | Through | 680 | 400 | 58.9% | 388.7 | 71.9 | F |
| | Right Turn | | | | | | |
| | Subtotal | 1,010 | 595 | 58.9% | 342.3 | 63.3 | F |
| WB | Left Turn | | | | | | |
| | Through | 475 | 309 | 65.0% | 49.5 | 9.1 | D |
| | Right Turn | 220 | 146 | 66.3% | 44.1 | 11.8 | D |
| | Subtotal | 695 | 455 | 65.4% | 47.7 | 9.9 | D |
| Total | | 2,265 | 1,341 | 59.2% | 273.7 | 38.3 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Alternative 1 Year 2040
PM Peak Hour

Intersection 11 Innovation Way/11th Avenue All-way Stop

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 80 | 49 | 61.8% | 33.1 | 28.3 | D |
| | Through | 400 | 245 | 61.2% | 41.1 | 29.6 | E |
| | Right Turn | 50 | 28 | 55.8% | 41.3 | 38.0 | E |
| | Subtotal | 530 | 322 | 60.8% | 39.7 | 29.6 | E |
| SB | Left Turn | 110 | 58 | 53.1% | 51.0 | 68.8 | F |
| | Through | 110 | 54 | 49.0% | 119.7 | 75.8 | F |
| | Right Turn | 20 | 12 | 62.0% | 131.4 | 107.3 | F |
| | Subtotal | 240 | 125 | 52.0% | 87.5 | 65.3 | F |
| EB | Left Turn | 500 | 314 | 62.9% | 493.9 | 164.4 | F |
| | Through | | | | | | |
| | Right Turn | 340 | 144 | 42.2% | 935.7 | 225.9 | F |
| | Subtotal | 840 | 458 | 54.5% | 629.5 | 171.4 | F |
| WB | Left Turn | 40 | 38 | 95.0% | 166.8 | 74.3 | F |
| | Through | | | | | | |
| | Right Turn | 20 | 22 | 108.5% | 9.6 | 6.8 | A |
| | Subtotal | 60 | 60 | 99.5% | 107.9 | 44.6 | F |
| Total | | 1,670 | 964 | 57.7% | 321.5 | 63.9 | F |

Intersection 12 Innovation Way/Juniper Networks Driveway Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 60 | 36 | 59.7% | 139.4 | 48.5 | F |
| | Through | 860 | 569 | 66.2% | 103.4 | 47.7 | F |
| | Right Turn | | | | | | |
| | Subtotal | 920 | 605 | 65.8% | 105.5 | 47.4 | F |
| SB | Left Turn | | | | | | |
| | Through | 160 | 80 | 49.8% | 64.3 | 8.7 | E |
| | Right Turn | 170 | 85 | 49.9% | 7.4 | 1.6 | A |
| | Subtotal | 330 | 164 | 49.8% | 35.1 | 4.5 | D |
| EB | Left Turn | 700 | 230 | 32.8% | 1802.4 | 203.0 | F |
| | Through | | | | | | |
| | Right Turn | 80 | 57 | 71.8% | 975.6 | 382.1 | F |
| | Subtotal | 780 | 287 | 36.8% | 1637.6 | 240.6 | F |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 2,030 | 1,057 | 52.0% | 499.8 | 82.7 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
Alternative 1 Year 2040
PM Peak Hour

| Intersection 13 | | Bordeaux Drive/Innovation Way | | | Signal | | |
|-----------------|------------|-------------------------------|---------------------|---------|-----------------------|-----------|-----|
| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 630 | 159 | 25.2% | 1609.7 | 140.7 | F |
| | Through | 50 | 11 | 21.6% | 1378.4 | 123.3 | F |
| | Right Turn | | | | | | |
| | Subtotal | 680 | 170 | 24.9% | 1594.7 | 139.3 | F |
| SB | Left Turn | | | | | | |
| | Through | 180 | 65 | 35.8% | 1776.5 | 163.9 | F |
| | Right Turn | 230 | 79 | 34.4% | 1792.9 | 159.1 | F |
| | Subtotal | 410 | 144 | 35.0% | 1786.0 | 160.5 | F |
| EB | Left Turn | 90 | 60 | 67.1% | 30.2 | 2.8 | C |
| | Through | 30 | 21 | 69.3% | 30.6 | 3.3 | C |
| | Right Turn | 230 | 154 | 66.7% | 6.5 | 1.8 | A |
| | Subtotal | 350 | 235 | 67.1% | 14.7 | 1.9 | B |
| WB | Left Turn | | | | | | |
| | Through | 30 | 30 | 100.7% | 160.9 | 45.1 | F |
| | Right Turn | | | | | | |
| | Subtotal | 30 | 30 | 100.7% | 160.9 | 45.1 | F |
| Total | | 1,470 | 578 | 39.3% | 919.1 | 27.3 | F |

Intersection 1

Mathilda Avenue/5th Avenue

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 625 | 125 | 14 | 250 | 19 | 300 | 25 | 29% | 0% |
| | Through | 625 | 50 | 8 | 100 | 14 | 125 | 21 | 0% | 0% |
| | Right Turn | 625 | 175 | 109 | 350 | 141 | 400 | 135 | 0% | 0% |
| NB | Left Turn | 425 | 75 | 6 | 125 | 14 | 150 | 20 | 0% | 0% |
| | Through | 1,125 | 75 | 6 | 150 | 11 | 200 | 25 | 0% | 0% |
| | Through/Right | 1,125 | 75 | 9 | 175 | 27 | 225 | 36 | 0% | 0% |
| SB | Left Turn | 250 | 100 | 31 | 275 | 63 | 300 | 0 | 0% | 0% |
| | Through | 1,325 | 1,800 | 362 | 3,075 | 493 | 3,425 | 513 | 84% | 0% |
| | Right Turn | 250 | 100 | 27 | 300 | 49 | 300 | 0 | 0% | 0% |
| WB | Left Turn | 925 | 100 | 29 | 225 | 95 | 325 | 123 | 29% | 0% |
| | Through/Right | 75 | 50 | 5 | 100 | 6 | 100 | 0 | 6% | 0% |

Intersection 2

Mathilda Avenue/Innovation Way-Driveway

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|--------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left/Through | 225 | 275 | 8 | 350 | 13 | 325 | 15 | 0% | 59% |
| | Right Turn | 225 | 225 | 11 | 325 | 14 | 325 | 14 | 0% | 24% |
| NB | Left Turn | 725 | 50 | 9 | 75 | 22 | 100 | 35 | 0% | 0% |
| | Through | 975 | 150 | 20 | 300 | 85 | 400 | 277 | 0% | 0% |
| | Right Turn | 975 | 125 | 24 | 300 | 97 | 425 | 281 | 0% | 0% |
| SB | Left Turn | 75 | 100 | 15 | 175 | 9 | 150 | 0 | 35% | 0% |
| | Through | 975 | 1,200 | 24 | 1,250 | 51 | 1,225 | 24 | 89% | 60% |
| | Right Turn | 225 | 150 | 25 | 350 | 29 | 275 | 0 | 0% | 0% |
| WB | Left Turn | 425 | 750 | 2 | 775 | 4 | 775 | 13 | 65% | 70% |
| | Shared | 225 | 225 | 2 | 250 | 4 | 250 | 0 | 71% | 0% |

Intersection 3

Mathilda Avenue/Moffett Park Drive-SR 237 WB Off-Ramp

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|----------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Shared | 1,125 | 1,175 | 4 | 1,200 | 12 | 1,225 | 18 | 0% | 92% |
| | Right Turn | 1,125 | 1,175 | 5 | 1,200 | 5 | 1,225 | 13 | 0% | 87% |
| NB | Left Turn | 350 | 250 | 60 | 350 | 80 | 375 | 68 | 0% | 12% |
| | Through | 350 | 125 | 5 | 175 | 19 | 225 | 53 | 0% | 0% |
| | Right Diagonal | 350 | 150 | 22 | 225 | 18 | 200 | 13 | 0% | 52% |
| SB | Through | 975 | 1,050 | 9 | 1,100 | 22 | 1,100 | 26 | 0% | 34% |
| | Through/Right | 975 | 1,100 | 5 | 1,150 | 18 | 1,150 | 12 | 0% | 49% |
| WB | Left Turn | 525 | 600 | 3 | 625 | 8 | 625 | 0 | 72% | 0% |
| | Left/Through | 1,225 | 1,150 | 23 | 1,250 | 60 | 1,200 | 7 | 77% | 54% |
| | Through/Right | 1,225 | 200 | 19 | 325 | 34 | 400 | 52 | 0% | 0% |

Intersection 4

Mathilda Avenue/SR 237 EB Ramps

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|--------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,025 | 150 | 51 | 275 | 167 | 375 | 296 | 0% | 0% |
| | Left/Through | 1,025 | 150 | 66 | 325 | 197 | 475 | 319 | 3% | 0% |
| | Right Turn | 450 | 175 | 57 | 400 | 123 | 450 | 130 | 4% | 0% |
| NB | Through | 275 | 150 | 33 | 300 | 73 | 275 | 63 | 0% | 7% |
| | Right Turn | 275 | 225 | 21 | 300 | 31 | 275 | 15 | 25% | 14% |
| SB | Left Turn | 325 | 300 | 19 | 375 | 16 | 350 | 15 | 32% | 9% |
| | Through | 350 | 350 | 50 | 475 | 42 | 500 | 31 | 0% | 14% |
| | | | | | | | | | | |

SimTraffic Post-Processor
Average Results from 10 Runs
Queue Length
Intersection 5

Mathilda Avenue Improvements
Alternative 1 Year 2040
PM Peak Hour
Signal

Mathilda Avenue/Ross Drive

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 250 | 50 | 6 | 125 | 10 | 125 | 0 | 5% | 0% |
| | Through | 225 | 225 | 32 | 400 | 62 | 525 | 102 | 58% | 0% |
| | Right Turn | 700 | 50 | 7 | 125 | 9 | 100 | 0 | 13% | 0% |
| NB | Left Turn | 250 | 275 | 17 | 350 | 14 | 325 | 0 | 23% | 0% |
| | Through | 700 | 650 | 87 | 850 | 74 | 775 | 23 | 63% | 48% |
| | Through/Right | 225 | 275 | 10 | 300 | 38 | 275 | 0 | 79% | 0% |
| SB | Left Turn | 250 | 100 | 11 | 200 | 19 | 225 | 23 | 0% | 1% |
| | Through | 700 | 225 | 24 | 300 | 34 | 275 | 13 | 0% | 23% |
| | Through/Right | 225 | 275 | 24 | 325 | 37 | 300 | 14 | 0% | 61% |
| WB | Left Turn | 250 | 2,100 | 4 | 4,500 | 12 | 5,275 | 0 | 84% | 0% |
| | Through | 225 | 4,275 | 770 | 6,375 | 1,155 | 6,400 | 994 | 8% | 0% |
| | Right Turn | 700 | 250 | 7 | 550 | 8 | 450 | 2 | 8% | 0% |

Intersection 6

Mathilda Avenue/US 101 NB Ramps

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NB | Through | 575 | 475 | 104 | 750 | 139 | 675 | 69 | 0% | 31% |
| | Right Turn | 575 | 100 | 73 | 400 | 238 | 550 | 266 | 0% | 2% |
| SB | Left Turn | 375 | 50 | 14 | 150 | 69 | 275 | 173 | 0% | 0% |
| | Through | 700 | 525 | 81 | 775 | 36 | 725 | 36 | 11% | 1% |
| WB | Left Turn | 1,025 | 1,500 | 494 | 3,650 | 712 | 4,450 | 749 | 0% | 0% |
| | Right Turn | 1,025 | 100 | 14 | 175 | 24 | 150 | 21 | 0% | 33% |
| 0 | | | | | | | | | | |

Mathilda Avenue/US 101 SB Ramps

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,050 | 100 | 14 | 150 | 20 | 150 | 10 | 0% | 40% |
| | Right Turn | 1,050 | 50 | 40 | 125 | 75 | 200 | 100 | 0% | 0% |
| NB | Through | 750 | 325 | 142 | 775 | 308 | 750 | 273 | 0% | 7% |
| | Right Turn | 750 | 250 | 146 | 750 | 286 | 800 | 161 | 0% | 8% |
| SB | Through | 575 | 125 | 31 | 275 | 55 | 350 | 87 | 0% | 0% |
| | Through/Right | 575 | 275 | 53 | 450 | 88 | 525 | 111 | 0% | 0% |
| | | | | | | | | | | |

Intersection 8

Mathilda Avenue/Almanor Avenue-Ahwanee Avenue

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,025 | 300 | 25 | 425 | 40 | 450 | 12 | 56% | 6% |
| | Through/Right | 125 | 175 | 11 | 275 | 8 | 225 | 0 | 10% | 0% |
| NB | Left Turn | 425 | 125 | 36 | 300 | 89 | 400 | 96 | 0% | 0% |
| | Through | 750 | 500 | 102 | 700 | 164 | 700 | 106 | 59% | 13% |
| | Through/Right | 750 | 300 | 15 | 375 | 24 | 325 | 0 | 27% | 0% |
| SB | Left Turn | 275 | 200 | 18 | 325 | 25 | 325 | 12 | 12% | 0% |
| | Through | 750 | 225 | 36 | 375 | 82 | 500 | 176 | 1% | 0% |
| | Through/Right | 750 | 200 | 10 | 300 | 19 | 300 | 29 | 0% | 0% |
| SB | Left Turn | 250 | 75 | 10 | 150 | 31 | 200 | 105 | 0% | 0% |
| | Through | 1,025 | 100 | 20 | 225 | 63 | 350 | 173 | 12% | 0% |
| | Right Turn | 75 | 100 | 6 | 125 | 4 | 125 | 0 | 35% | 0% |

US 101 NB Slip Ramp/Moffett Park Drive

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Through | 850 | 800 | 57 | 1,075 | 100 | 900 | 2 | 69% | 26% |
| | Right Turn | 150 | 225 | 30 | 500 | 24 | 375 | 0 | 0% | 0% |
| WB | Left Turn | 850 | 125 | 13 | 225 | 22 | 250 | 40 | 0% | 0% |
| | Through | 850 | 25 | 1 | 25 | 15 | 50 | 43 | 0% | 0% |
| | | | | | | | | | | |
| | | | | | | | | | | |

Intersection 10

Innovation Way/Moffett Park Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 225 | 325 | 40 | 450 | 50 | 350 | 0 | 12% | 0% |
| | Through | 850 | 875 | 34 | 975 | 62 | 925 | 6 | 98% | 33% |
| SB | Left Turn | 575 | 500 | 6 | 575 | 12 | 550 | 15 | 0% | 32% |
| | Shared | 575 | 525 | 8 | 575 | 14 | 550 | 15 | 0% | 73% |
| WB | Through | 1,150 | 150 | 23 | 250 | 64 | 300 | 100 | 0% | 0% |
| | Through/Right | 1,150 | 200 | 24 | 325 | 96 | 425 | 290 | 0% | 0% |
| | | | | | | | | | | |

SimTraffic Post-Processor
Average Results from 10 Runs
Queue Length
Intersection 11

Mathilda Avenue Improvements
Alternative 1 Year 2040
PM Peak Hour
All-way Stop

Innovation Way/11th Avenue

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 125 | 75 | 12 | 150 | 19 | 150 | 3 | 6% | 0% |
| | Left/Through | 325 | 2,325 | 629 | 5,050 | 1,125 | 5,325 | 1,120 | 10% | 0% |
| | Right Turn | 325 | 2,400 | 603 | 4,925 | 1,079 | 5,275 | 1,104 | 0% | 0% |
| NB | Left Turn | 125 | 50 | 10 | 100 | 29 | 150 | 44 | 0% | 0% |
| | Through | 575 | 150 | 30 | 300 | 72 | 425 | 78 | 9% | 1% |
| | Through/Right | 575 | 75 | 27 | 175 | 72 | 225 | 77 | 0% | 2% |
| SB | Left Turn | 175 | 50 | 22 | 125 | 55 | 150 | 52 | 5% | 0% |
| | Through | 1,000 | 50 | 24 | 125 | 93 | 175 | 148 | 4% | 0% |
| | Through/Right | 1,000 | 75 | 31 | 175 | 82 | 225 | 109 | 0% | 0% |
| WB | Left Turn | 325 | 75 | 16 | 175 | 37 | 225 | 47 | 0% | 0% |
| | Through/Right | 325 | 25 | 3 | 50 | 5 | 75 | 10 | 0% | 0% |

Intersection 12

Innovation Way/Juniper Networks Driveway

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 200 | 9,225 | 438 | 11,975 | 170 | 10,575 | 13 | 0% | 44% |
| | Right Turn | 200 | 6,025 | 1,209 | 11,100 | 1,132 | 10,525 | 35 | 0% | 5% |
| NB | Left Turn | 125 | 75 | 15 | 150 | 23 | 175 | 0 | 3% | 0% |
| | Through | 1,000 | 425 | 127 | 750 | 170 | 900 | 159 | 44% | 3% |
| SB | Through | 300 | 200 | 21 | 225 | 43 | 250 | 71 | 0% | 0% |
| | Right Turn | 300 | 50 | 26 | 150 | 39 | 175 | 40 | 0% | 0% |
| 0 | | | | | | | | | | |

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left/Through | 375 | 75 | 9 | 125 | 16 | 175 | 33 | 3% | 0% |
| | Right Turn | 125 | 75 | 7 | 125 | 16 | 125 | 7 | 1% | 0% |
| NB | Left Turn | 325 | 850 | 3 | 900 | 6 | 900 | 4 | 97% | 0% |
| | Through/Right | 2,025 | 775 | 1 | 775 | 2 | 775 | 2 | 3% | 81% |
| SB | Left Turn | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | Through/Right | 725 | 4,525 | 83 | 4,800 | 132 | 4,625 | 25 | 95% | 76% |
| WB | Left/Through | 125 | 75 | 14 | 125 | 24 | 175 | 39 | 13% | 0% |
| | Right Turn | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |

Arterial Level of Service

Build1 2040 PM

2/26/2016

Arterial Level of Service: NB Mathilda Ave

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|--------------------|------|---------------|-----------------|------------|----------------|
| Ahwanee Ave | 8 | 73.8 | 84.9 | 0.1 | 6 |
| | 7 | 47.6 | 60.0 | 0.2 | 9 |
| US 101 NB Ramps | 6 | 91.9 | 101.8 | 0.1 | 5 |
| Ross Dr | 5 | 144.6 | 156.2 | 0.1 | 3 |
| SR 237 EB Ramps | 4 | 33.7 | 39.1 | 0.1 | 6 |
| SR 237 WB On-Ramp | 33 | 16.1 | 19.5 | 0.0 | 9 |
| SR 237 WB Off-Ramp | 3 | 15.7 | 18.9 | 0.0 | 7 |
| Innovation Way | 2 | 44.2 | 60.7 | 0.2 | 13 |
| 5th Ave | 1 | 18.9 | 38.0 | 0.2 | 22 |
| | 107 | 3.9 | 26.2 | 0.3 | 37 |
| Total | | 490.4 | 605.3 | 1.4 | 9 |

Arterial Level of Service: SB Mathilda Ave

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|-------------------|------|---------------|-----------------|------------|----------------|
| 5th Ave | 1 | 478.4 | 498.3 | 0.3 | 2 |
| Innovation Way | 2 | 381.6 | 400.2 | 0.2 | 2 |
| Moffett Park Dr | 3 | 194.6 | 210.8 | 0.2 | 4 |
| SR 237 WB On-Ramp | 33 | 12.4 | 15.6 | 0.0 | 9 |
| SR 237 EB Ramps | 4 | 17.0 | 20.8 | 0.0 | 8 |
| Ross Dr | 5 | 23.7 | 28.5 | 0.1 | 8 |
| US 101 NB Ramps | 6 | 48.7 | 60.1 | 0.1 | 9 |
| US 101 SB Ramps | 7 | 8.6 | 19.3 | 0.1 | 25 |
| Almanor Ave | 8 | 22.4 | 35.1 | 0.2 | 16 |
| San Aleso Ave | 201 | 4.7 | 16.1 | 0.1 | 31 |
| Total | | 1192.3 | 1304.9 | 1.4 | 4 |

Arterial Level of Service: NB Innovation Way

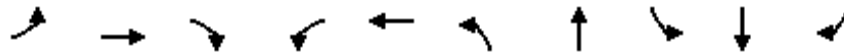
| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|------------------|------|---------------|-----------------|------------|----------------|
| | 910 | 7.0 | 11.1 | 0.0 | 7 |
| | 43 | 3.1 | 8.8 | 0.0 | 17 |
| | 11 | 33.4 | 41.8 | 0.1 | 6 |
| | 200 | 42.2 | 58.7 | 0.2 | 10 |
| Juniper Driveway | 12 | 61.6 | 68.2 | 0.1 | 3 |
| Driveway | 217 | 23.1 | 26.5 | 0.0 | 5 |
| | 902 | 46.9 | 49.3 | 0.0 | 2 |
| Mathilda Ave | 2 | 10.1 | 12.4 | 0.0 | 7 |
| | 52 | 5.3 | 20.1 | 0.1 | 17 |
| Bordeaux Dr | 13 | 30.8 | 41.9 | 0.1 | 7 |
| Total | | 263.5 | 338.7 | 0.6 | 7 |

Arterial Level of Service: SB Innovation Way

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|------------------|------|---------------|-----------------|-----------|----------------|
| | 52 | 83.8 | 93.8 | 0.1 | 3 |
| Mathilda Ave | 2 | 239.0 | 250.1 | 0.1 | 1 |
| | 902 | 7.7 | 12.7 | 0.0 | 7 |
| Driveway | 217 | 0.4 | 2.6 | 0.0 | 30 |
| Juniper Driveway | 12 | 60.6 | 64.6 | 0.0 | 2 |
| | 200 | 1.8 | 8.3 | 0.1 | 25 |
| 11th Ave | 11 | 124.6 | 140.7 | 0.2 | 4 |
| | 43 | 250.2 | 255.5 | 0.1 | 1 |
| | 910 | 142.2 | 146.3 | 0.0 | 1 |
| Moffett Park Dr | 10 | 29.9 | 33.5 | 0.0 | 2 |
| Total | | 940.1 | 1008.0 | 0.6 | 2 |

Lanes, Volumes, Timings
1: Mathilda Ave & 5th Ave

3/4/2016

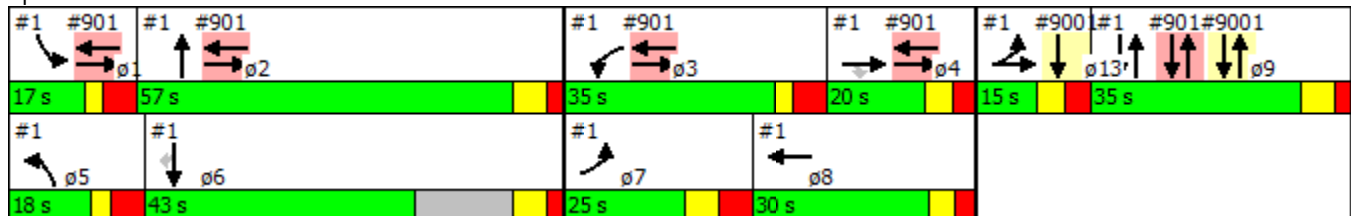


| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT | SBR | ø2 | ø7 |
|----------------------|------|------|--------|-------|-------|-------|-----|------|-----|--------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 30 | 30 | 90 | 60 | 30 | 200 | 860 | 40 | 520 | 110 | | |
| Turn Type | Prot | NA | custom | Prot | NA | Prot | NA | Prot | NA | custom | | |
| Protected Phases | 7 13 | 4 13 | | 3 | 8 | 5 | 2 9 | 1 | 6 9 | | 2 | 7 |
| Permitted Phases | | | 4 | | | | | | | 6 | | |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 5 | 2 | 1 | 6 | 6 | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 13.0 | 12.0 | 8.0 | 11.0 | | 10.0 | | 12.0 | 12.0 | 12.0 |
| Minimum Split (s) | | | 20.0 | 19.0 | 29.5 | 18.0 | | 17.0 | | 41.0 | 34.8 | 21.0 |
| Total Split (s) | | | 20.0 | 35.0 | 30.0 | 18.0 | | 17.0 | | 43.0 | 57.0 | 25.0 |
| Total Split (%) | | | 11.2% | 19.6% | 16.8% | 10.1% | | 9.5% | | 24.0% | 32% | 14% |
| Yellow Time (s) | | | 3.6 | 2.5 | 3.6 | 2.5 | | 2.5 | | 4.7 | 4.5 | 4.5 |
| All-Red Time (s) | | | 3.4 | 4.5 | 2.9 | 4.5 | | 4.5 | | 2.3 | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | | 0.0 | | |
| Total Lost Time (s) | | | 7.0 | 7.0 | 6.5 | 7.0 | | 7.0 | | 7.0 | | |
| Lead/Lag | | | Lag | Lead | Lag | Lead | | Lead | | Lag | Lag | Lead |
| Lead-Lag Optimize? | | | Yes | Yes | Yes | Yes | | Yes | | Yes | Yes | Yes |
| Recall Mode | | | None | None | None | None | | None | | None | Min | None |

Intersection Summary

Cycle Length: 179
 Actuated Cycle Length: 105.3
 Natural Cycle: 160
 Control Type: Actuated-Uncoordinated

Splits and Phases: 1: Mathilda Ave & 5th Ave



| Lane Group | ø9 | ø13 |
|----------------------|------|------|
| Lane Configurations | | |
| Volume (vph) | | |
| Turn Type | | |
| Protected Phases | 9 | 13 |
| Permitted Phases | | |
| Detector Phase | | |
| Switch Phase | | |
| Minimum Initial (s) | 28.0 | 8.0 |
| Minimum Split (s) | 35.0 | 15.0 |
| Total Split (s) | 35.0 | 15.0 |
| Total Split (%) | 20% | 8% |
| Yellow Time (s) | 4.7 | 3.6 |
| All-Red Time (s) | 2.3 | 3.4 |
| Lost Time Adjust (s) | | |
| Total Lost Time (s) | | |
| Lead/Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes |
| Recall Mode | None | None |
| Intersection Summary | | |

Lanes, Volumes, Timings
2: Mathilda Ave & Innovation Way

3/4/2016

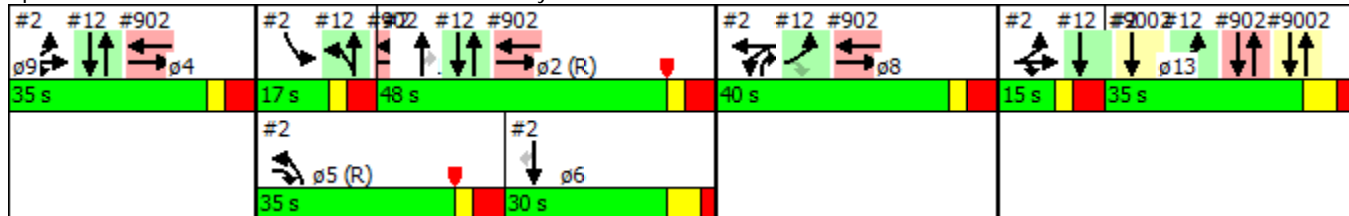


| Lane Group | EBT | EBR | WBL | WBT | NBL | NBT | NBR | SBL | SBT | SBR | ø2 | ø4 |
|----------------------|------|--------|-------|-------|-------|-----|-------|------|-----|------|-------|------|
| Lane Configurations | ↕ | ↕↕ | ↕ | ↕↕ | ↕↕ | ↕↕ | ↕ | ↕ | ↕↕↕ | ↕ | | |
| Volume (vph) | 90 | 140 | 360 | 180 | 1060 | 970 | 1240 | 50 | 390 | 230 | | |
| Turn Type | NA | pt+ov | Split | NA | Prot | NA | pm+ov | Prot | NA | Perm | | |
| Protected Phases | 4 13 | 4 13 5 | 8 | 8 | 5 | 2 9 | 8 | 1 | 6 9 | | 2 | 4 |
| Permitted Phases | | | | | | | 2 9 | | | 6 9 | | |
| Detector Phase | 4 | 4 | 8 | 8 | 5 | 2 | 2 | 1 | 6 | 6 | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 10.0 | 10.0 | 13.0 | | 10.0 | 10.0 | | | 12.0 | 14.0 |
| Minimum Split (s) | | | 35.0 | 35.0 | 20.0 | | 35.0 | 16.8 | | | 19.0 | 39.0 |
| Total Split (s) | | | 40.0 | 40.0 | 35.0 | | 40.0 | 17.0 | | | 48.0 | 35.0 |
| Total Split (%) | | | 21.1% | 21.1% | 18.4% | | 21.1% | 8.9% | | | 25% | 18% |
| Yellow Time (s) | | | 2.5 | 2.5 | 2.5 | | 2.5 | 2.5 | | | 2.5 | 2.5 |
| All-Red Time (s) | | | 4.5 | 4.5 | 4.5 | | 4.5 | 4.3 | | | 4.5 | 4.5 |
| Lost Time Adjust (s) | | | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | | | | |
| Total Lost Time (s) | | | 7.0 | 7.0 | 7.0 | | 7.0 | 6.8 | | | | |
| Lead/Lag | | | | | Lead | | | Lead | | | Lag | |
| Lead-Lag Optimize? | | | | | Yes | | | Yes | | | Yes | |
| Recall Mode | | | None | None | C-Max | | None | Max | | | C-Max | None |

Intersection Summary

Cycle Length: 190
 Actuated Cycle Length: 190
 Offset: 0 (0%), Referenced to phase 2:NBT and 5:NBL, Start of Yellow
 Natural Cycle: 175
 Control Type: Actuated-Coordinated

Splits and Phases: 2: Mathilda Ave & Innovation Way



Lanes, Volumes, Timings
 2: Mathilda Ave & Innovation Way

3/4/2016

| Lane Group | ø6 | ø9 | ø13 |
|----------------------|------|------|------|
| Lane Configurations | | | |
| Volume (vph) | | | |
| Turn Type | | | |
| Protected Phases | 6 | 9 | 13 |
| Permitted Phases | | | |
| Detector Phase | | | |
| Switch Phase | | | |
| Minimum Initial (s) | 12.0 | 28.0 | 8.0 |
| Minimum Split (s) | 30.0 | 35.0 | 15.0 |
| Total Split (s) | 30.0 | 35.0 | 15.0 |
| Total Split (%) | 16% | 18% | 8% |
| Yellow Time (s) | 4.7 | 4.7 | 2.5 |
| All-Red Time (s) | 2.3 | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | |
| Total Lost Time (s) | | | |
| Lead/Lag | Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes | Yes |
| Recall Mode | None | None | None |
| Intersection Summary | | | |

Lanes, Volumes, Timings
 3: Mathilda Ave & SR 237 WB Off-Ramp

3/4/2016



| Lane Group | WBR | SBL | SBR2 | NEL | ø9 |
|----------------------|-------|-------|-------|-------|------|
| Lane Configurations | ↖ | ↖↖↖ | ↖ | ↖↖↖ | |
| Volume (vph) | 610 | 380 | 510 | 2660 | |
| Turn Type | Prot | Prot | Perm | Prot | |
| Protected Phases | 4 | 4 | | 2 | 9 |
| Permitted Phases | | | 4 | | |
| Detector Phase | 4 | 4 | 4 | 2 | |
| Switch Phase | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | 26.7 | 26.7 | 26.7 | 26.7 | 18.0 |
| Total Split (s) | 45.0 | 45.0 | 45.0 | 75.0 | 20.0 |
| Total Split (%) | 32.1% | 32.1% | 32.1% | 53.6% | 14% |
| Yellow Time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 2.0 |
| All-Red Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 0.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | 9.0 | 9.0 | 9.0 | 9.0 | |
| Lead/Lag | | | | | |
| Lead-Lag Optimize? | | | | | |
| Recall Mode | Max | Max | Max | C-Max | Max |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 126 (90%), Referenced to phase 2:NEL, Start of Yellow
 Natural Cycle: 150
 Control Type: Actuated-Coordinated

Splits and Phases: 3: Mathilda Ave & SR 237 WB Off-Ramp



Lanes, Volumes, Timings
 4: Mathilda Ave & SR 237 EB Off-Ramp

3/4/2016



| Lane Group | EBR | NBT | NBR2 | SWL | ø9 |
|----------------------|--------|-------|-------|-------|------|
| Lane Configurations | ↗ | ↑↑↑ | ↖ | ↑↑↑↑ | |
| Volume (vph) | 70 | 2980 | 920 | 970 | |
| Turn Type | custom | NA | Perm | Prot | |
| Protected Phases | 2 9 | 2 | | 4 | 9 |
| Permitted Phases | | | 2 | | |
| Detector Phase | 2 | 2 | 2 | 4 | |
| Switch Phase | | | | | |
| Minimum Initial (s) | | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | | 26.7 | 26.7 | 26.7 | 18.0 |
| Total Split (s) | | 75.0 | 75.0 | 45.0 | 20.0 |
| Total Split (%) | | 53.6% | 53.6% | 32.1% | 14% |
| Yellow Time (s) | | 3.0 | 3.0 | 3.0 | 2.0 |
| All-Red Time (s) | | 6.0 | 6.0 | 6.0 | 0.0 |
| Lost Time Adjust (s) | | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | | 9.0 | 9.0 | 9.0 | |
| Lead/Lag | | | | | |
| Lead-Lag Optimize? | | | | | |
| Recall Mode | | C-Max | C-Max | Max | Max |

Intersection Summary

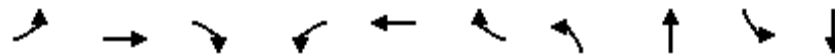
Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 126 (90%), Referenced to phase 2:NEL, Start of Yellow
 Natural Cycle: 150
 Control Type: Actuated-Coordinated

Splits and Phases: 4: Mathilda Ave & SR 237 EB Off-Ramp



Lanes, Volumes, Timings
5: Mathilda Ave & Ross Dr

3/4/2016

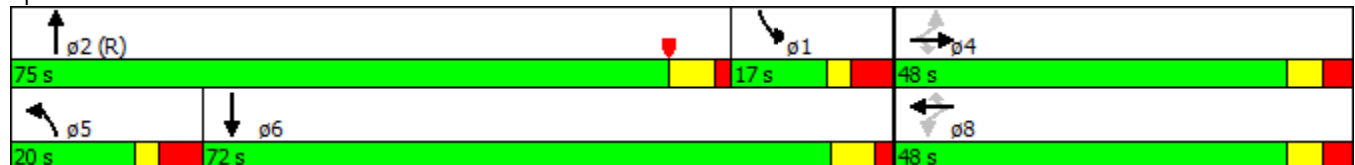


| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | | |
| Volume (vph) | 90 | 70 | 40 | 130 | 40 | 300 | 80 | 3510 | 70 | 920 |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | Prot | NA | Prot | NA |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | 1 | 6 |
| Permitted Phases | 4 | | 4 | 8 | | 8 | | | | |
| Detector Phase | 4 | 4 | 4 | 8 | 8 | 8 | 5 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 4.0 | 5.0 | 4.0 | 5.0 |
| Minimum Split (s) | 48.0 | 48.0 | 48.0 | 19.0 | 19.0 | 19.0 | 11.0 | 31.4 | 11.0 | 11.6 |
| Total Split (s) | 48.0 | 48.0 | 48.0 | 48.0 | 48.0 | 48.0 | 20.0 | 75.0 | 17.0 | 72.0 |
| Total Split (%) | 34.3% | 34.3% | 34.3% | 34.3% | 34.3% | 34.3% | 14.3% | 53.6% | 12.1% | 51.4% |
| Yellow Time (s) | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 2.5 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 3.4 | 3.4 | 3.4 | 3.4 | 3.4 | 3.4 | 4.5 | 1.7 | 4.5 | 1.9 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.4 | 7.0 | 6.6 |
| Lead/Lag | | | | | | | Lead | Lead | Lag | Lag |
| Lead-Lag Optimize? | | | | | | | Yes | Yes | Yes | Yes |
| Recall Mode | Max | Max | Max | None | None | None | None | C-Max | Max | None |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 0 (0%), Referenced to phase 2:NBT, Start of Yellow, Master Intersection
 Natural Cycle: 125
 Control Type: Actuated-Coordinated

Splits and Phases: 5: Mathilda Ave & Ross Dr



Lanes, Volumes, Timings
 6: Mathilda Ave & US 101 NB Ramps

3/4/2016



| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↖↖ | ↖↖ | ↑↑↑ | ↖ | ↖ | ↑↑↑ |
| Volume (vph) | 770 | 780 | 2930 | 570 | 20 | 1070 |
| Turn Type | Prot | pm+ov | NA | Perm | Prot | NA |
| Protected Phases | 8 | 1 | 2 | | 1 | 6 |
| Permitted Phases | | 8 | | 2 | | |
| Detector Phase | 8 | 1 | 2 | 2 | 1 | 6 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 8.0 | 4.0 | 8.0 | 8.0 | 4.0 | 4.0 |
| Minimum Split (s) | 14.9 | 9.7 | 39.9 | 39.9 | 9.7 | 10.9 |
| Total Split (s) | 44.0 | 16.0 | 80.0 | 80.0 | 16.0 | 96.0 |
| Total Split (%) | 31.4% | 11.4% | 57.1% | 57.1% | 11.4% | 68.6% |
| Yellow Time (s) | 4.7 | 3.5 | 4.7 | 4.7 | 3.5 | 4.7 |
| All-Red Time (s) | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.9 | 5.7 | 6.9 | 6.9 | 5.7 | 6.9 |
| Lead/Lag | | Lead | Lag | Lag | Lead | |
| Lead-Lag Optimize? | | Yes | Yes | Yes | Yes | |
| Recall Mode | None | None | C-Max | C-Max | None | None |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 119 (85%), Referenced to phase 2:NBT, Start of Yellow
 Natural Cycle: 150
 Control Type: Actuated-Coordinated

Splits and Phases: 6: Mathilda Ave & US 101 NB Ramps



Lanes, Volumes, Timings
 7: Mathilda Ave & US 101 SB Ramps

3/4/2016

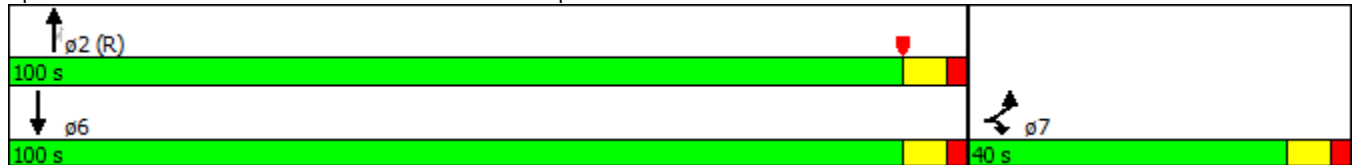


| Lane Group | EBL | EBR | NBT | NBR | SBT |
|----------------------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | |
| Volume (vph) | 380 | 520 | 3120 | 700 | 1650 |
| Turn Type | Prot | Prot | NA | Perm | NA |
| Protected Phases | 7 | 7 | 2 | | 6 |
| Permitted Phases | | | | 2 | |
| Detector Phase | 7 | 7 | 2 | 2 | 6 |
| Switch Phase | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 8.0 | 8.0 | 8.0 |
| Minimum Split (s) | 10.9 | 10.9 | 14.9 | 14.9 | 14.9 |
| Total Split (s) | 40.0 | 40.0 | 100.0 | 100.0 | 100.0 |
| Total Split (%) | 28.6% | 28.6% | 71.4% | 71.4% | 71.4% |
| Yellow Time (s) | 4.7 | 4.7 | 4.7 | 4.7 | 4.7 |
| All-Red Time (s) | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.9 | 6.9 | 6.9 | 6.9 | 6.9 |
| Lead/Lag | | | | | |
| Lead-Lag Optimize? | | | | | |
| Recall Mode | None | None | C-Max | C-Max | None |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 116 (83%), Referenced to phase 2:NBT, Start of Yellow
 Natural Cycle: 90
 Control Type: Actuated-Coordinated

Splits and Phases: 7: Mathilda Ave & US 101 SB Ramps



Lanes, Volumes, Timings
 8: Mathilda Ave & Almanor Ave/Ahwanee Ave

3/4/2016

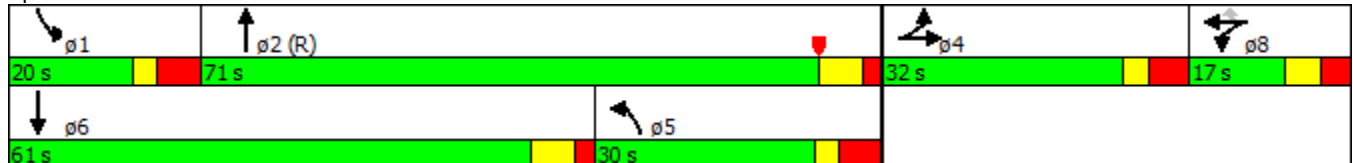


| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | | | | | |
| Volume (vph) | 130 | 30 | 90 | 50 | 260 | 140 | 3430 | 160 | 1680 |
| Turn Type | Split | NA | Split | NA | Perm | Prot | NA | Prot | NA |
| Protected Phases | 4 | 4 | 8 | 8 | | 5 | 2 | 1 | 6 |
| Permitted Phases | | | | | 8 | | | | |
| Detector Phase | 4 | 4 | 8 | 8 | 8 | 5 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | | |
| Minimum Initial (s) | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 12.0 | 8.0 | 12.0 |
| Minimum Split (s) | 32.0 | 32.0 | 15.0 | 15.0 | 15.0 | 15.0 | 36.7 | 15.0 | 18.7 |
| Total Split (s) | 32.0 | 32.0 | 17.0 | 17.0 | 17.0 | 30.0 | 71.0 | 20.0 | 61.0 |
| Total Split (%) | 22.9% | 22.9% | 12.1% | 12.1% | 12.1% | 21.4% | 50.7% | 14.3% | 43.6% |
| Yellow Time (s) | 2.8 | 2.8 | 3.6 | 3.6 | 3.6 | 2.5 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 4.2 | 4.2 | 3.4 | 3.4 | 3.4 | 4.5 | 2.0 | 4.5 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.7 | 7.0 | 6.7 |
| Lead/Lag | | | | | | Lag | Lag | Lead | Lead |
| Lead-Lag Optimize? | | | | | | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | None | C-Max | None | None |

Intersection Summary

Cycle Length: 140
 Actuated Cycle Length: 140
 Offset: 102 (73%), Referenced to phase 2:NBT, Start of Yellow
 Natural Cycle: 150
 Control Type: Actuated-Coordinated

Splits and Phases: 8: Mathilda Ave & Almanor Ave/Ahwanee Ave



Lanes, Volumes, Timings
 9: US 101 On-Ramp & Moffett Park Dr

3/4/2016

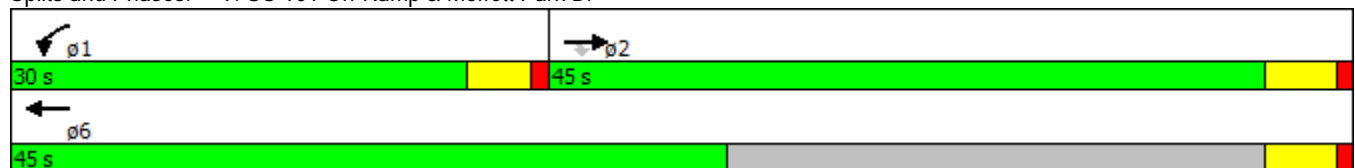


| Lane Group | EBT | EBR | WBL | WBT |
|----------------------|-------|-------|-------|-------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ |
| Volume (vph) | 230 | 20 | 40 | 990 |
| Turn Type | NA | Perm | Prot | NA |
| Protected Phases | 2 | | 1 | 6 |
| Permitted Phases | | 2 | | |
| Detector Phase | 2 | 2 | 1 | 6 |
| Switch Phase | | | | |
| Minimum Initial (s) | 15.0 | 15.0 | 6.0 | 15.0 |
| Minimum Split (s) | 20.0 | 20.0 | 10.5 | 20.0 |
| Total Split (s) | 45.0 | 45.0 | 30.0 | 45.0 |
| Total Split (%) | 60.0% | 60.0% | 40.0% | 60.0% |
| Yellow Time (s) | 4.0 | 4.0 | 3.5 | 4.0 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.0 | 5.0 | 4.5 | 5.0 |
| Lead/Lag | Lag | Lag | Lead | |
| Lead-Lag Optimize? | | | | |
| Recall Mode | Min | Min | None | Min |

Intersection Summary

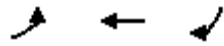
Cycle Length: 75
 Actuated Cycle Length: 41.4
 Natural Cycle: 40
 Control Type: Semi Act-Uncoord

Splits and Phases: 9: US 101 On-Ramp & Moffett Park Dr



Lanes, Volumes, Timings
 10: Moffett Park Dr & Innovation Way

3/4/2016



| Lane Group | EBL | WBT | SBR | ø4 | ø6 | ø9 |
|----------------------|-------|-----|-------|------|------|------|
| Lane Configurations | | | | | | |
| Volume (vph) | 230 | 750 | 280 | | | |
| Turn Type | Prot | NA | pt+ov | | | |
| Protected Phases | 5 | 6 9 | 4 5 | 4 | 6 | 9 |
| Permitted Phases | | | | | | |
| Detector Phase | 5 | 6 | 5 | | | |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 8.0 | | | 8.0 | 10.0 | 28.0 |
| Minimum Split (s) | 14.5 | | | 15.0 | 27.5 | 35.0 |
| Total Split (s) | 30.0 | | | 19.0 | 66.0 | 35.0 |
| Total Split (%) | 20.0% | | | 13% | 44% | 23% |
| Yellow Time (s) | 4.0 | | | 4.7 | 4.5 | 2.5 |
| All-Red Time (s) | 2.5 | | | 2.3 | 1.0 | 4.5 |
| Lost Time Adjust (s) | 0.0 | | | | | |
| Total Lost Time (s) | 6.5 | | | | | |
| Lead/Lag | Lead | | | | Lag | |
| Lead-Lag Optimize? | Yes | | | | Yes | |
| Recall Mode | None | | | None | Min | None |

Intersection Summary

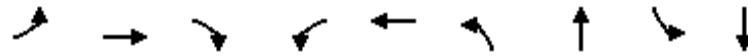
Cycle Length: 150
 Actuated Cycle Length: 90.4
 Natural Cycle: 95
 Control Type: Actuated-Uncoordinated

Splits and Phases: 10: Moffett Park Dr & Innovation Way



Lanes, Volumes, Timings
 11: Innovation Way & 11th Ave

3/4/2016



| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT |
|---------------------|-----|------|-----|-----|------|-----|------|-----|------|
| Lane Configurations | | | | | | | | | |
| Volume (vph) | 50 | 0 | 30 | 20 | 0 | 130 | 260 | 130 | 240 |
| Sign Control | | Stop | | | Stop | | Stop | | Stop |

Intersection Summary

Control Type: Unsignalized

Lanes, Volumes, Timings
 12: Innovation Way & Juniper Driveway

3/4/2016

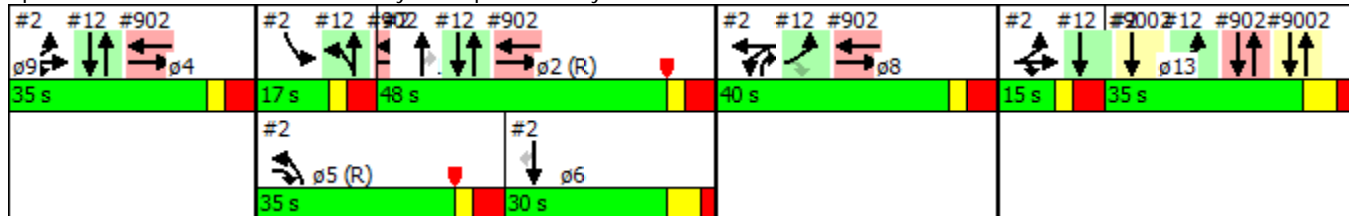


| Lane Group | EBL | EBR | NBL | NBT | SBT | ø2 | ø4 | ø5 | ø6 | ø8 | ø9 | ø13 |
|----------------------|------|------|------|-------|---------|-------|------|-------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 100 | 60 | 110 | 220 | 720 | | | | | | | |
| Turn Type | Prot | Perm | Prot | NA | NA | | | | | | | |
| Protected Phases | 8 9 | | 1 | 1 4 2 | 4 2 1 3 | 2 | 4 | 5 | 6 | 8 | 9 | 13 |
| Permitted Phases | | 8 9 | | | | | | | | | | |
| Detector Phase | 2 | 2 | 1 | 1 4 2 | 4 8 | | | | | | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 10.0 | | | 12.0 | 14.0 | 13.0 | 12.0 | 10.0 | 28.0 | 8.0 |
| Minimum Split (s) | | | 16.8 | | | 19.0 | 39.0 | 20.0 | 30.0 | 35.0 | 35.0 | 15.0 |
| Total Split (s) | | | 17.0 | | | 48.0 | 35.0 | 35.0 | 30.0 | 40.0 | 35.0 | 15.0 |
| Total Split (%) | | | 8.9% | | | 25% | 18% | 18% | 16% | 21% | 18% | 8% |
| Yellow Time (s) | | | 2.5 | | | 2.5 | 2.5 | 2.5 | 4.7 | 2.5 | 4.7 | 2.5 |
| All-Red Time (s) | | | 4.3 | | | 4.5 | 4.5 | 4.5 | 2.3 | 4.5 | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | 0.0 | | | | | | | | | |
| Total Lost Time (s) | | | 6.8 | | | | | | | | | |
| Lead/Lag | | | Lead | | | Lag | | Lead | Lag | | Lag | Lead |
| Lead-Lag Optimize? | | | Yes | | | Yes | | Yes | Yes | | Yes | Yes |
| Recall Mode | | | Max | | | C-Max | None | C-Max | None | None | None | None |

Intersection Summary

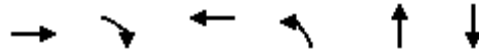
Cycle Length: 190
 Actuated Cycle Length: 190
 Offset: 0 (0%), Referenced to phase 2:NBT and 5:NBL, Start of Yellow
 Natural Cycle: 175
 Control Type: Actuated-Coordinated

Splits and Phases: 12: Innovation Way & Juniper Driveway



Lanes, Volumes, Timings
 13: Bordeaux Dr & Innovation Way

3/4/2016

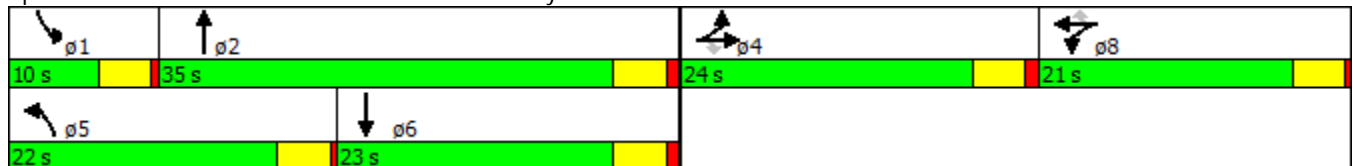


| Lane Group | EBT | EBR | WBT | NBL | NBT | SBT | ø1 |
|----------------------|-------|-------|-------|-------|-------|-------|------|
| Lane Configurations | ↖ | ↗ | ↖ | ↗ | ↖ | ↗ | |
| Volume (vph) | 50 | 690 | 20 | 390 | 130 | 60 | |
| Turn Type | NA | Perm | NA | Prot | NA | NA | |
| Protected Phases | 4 | | 8 | 5 | 2 | 6 | 1 |
| Permitted Phases | | 4 | | | | | |
| Detector Phase | 4 | 4 | 8 | 5 | 2 | 6 | |
| Switch Phase | | | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | 20.5 | 20.5 | 20.0 | 8.0 | 20.5 | 20.5 | 8.0 |
| Total Split (s) | 24.0 | 24.0 | 21.0 | 22.0 | 35.0 | 23.0 | 10.0 |
| Total Split (%) | 26.7% | 26.7% | 23.3% | 24.4% | 38.9% | 25.6% | 11% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.0 | 1.0 | 0.5 | 0.5 | 1.0 | 1.0 | 0.5 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | 4.5 | 4.5 | 4.0 | 4.0 | 4.5 | 4.5 | |
| Lead/Lag | | | | Lead | Lag | Lag | Lead |
| Lead-Lag Optimize? | | | | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | Min | Min | None |

Intersection Summary

Cycle Length: 90
 Actuated Cycle Length: 62.3
 Natural Cycle: 90
 Control Type: Actuated-Uncoordinated

Splits and Phases: 13: Bordeaux Dr & Innovation Way



**SimTraffic Post-Processor
Average Results from 10 Runs
Network Performance**

**Mathilda Avenue Improvements
2040 Build Alternative 2
AM Peak Hour**

| Performance Measure | Average | Std. Dev. | Minimum | Maximum |
|---------------------------------|---------|-----------|---------|---------|
| Average Delay (seconds) | 698.2 | 27.0 | 657.4 | 727.6 |
| Total Delay (hours) | 2,582 | 103 | 2,428 | 2,698 |
| Average Stopped Delay (seconds) | 636.3 | 27.1 | 595.8 | 673.6 |
| Total Stopped Delay (hours) | 2352 | 102 | 2205 | 2463 |
| Total Stops | 46,288 | 1,115 | 43,949 | 47,289 |
| Average Stops | 3.48 | 0.07 | 3.35 | 3.57 |
| Total Distance Traveled (miles) | 46,033 | 473 | 45,083 | 46,532 |
| Average Speed (mph) | 12.5 | 0.5 | 12.0 | 13.0 |
| Total Travel Time (hours) | 3,899.6 | 138.4 | 3,683.8 | 4,042.0 |
| Vehicles Entered | 10,721 | 120 | 10,527 | 10,880 |
| Vehicles Exited | 8,952 | 168 | 8,674 | 9,177 |
| Percent Demand Served | 83.5% | 1.8% | 81.4% | 86.5% |
| Fuel Used (gallons) | 1,728 | 27 | 1,686 | 1,762 |
| HC Emissions (grams) | 19,720 | 972 | 18,678 | 21,633 |
| CO Emissions (grams) | 547,149 | 17,431 | 531,025 | 581,300 |
| NOx Emissions (grams) | 70,094 | 2,711 | 67,431 | 75,022 |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2040 Build Alternative 2
AM Peak Hour

Intersection 1 Mathilda Avenue/5th Avenue Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 200 | 143 | 71.6% | 45.2 | 6.6 | D |
| | Through | 860 | 638 | 74.2% | 16.8 | 1.9 | B |
| | Right Turn | 80 | 60 | 74.8% | 13.7 | 3.9 | B |
| | Subtotal | 1,140 | 841 | 73.8% | 21.4 | 2.0 | C |
| SB | Left Turn | 40 | 39 | 97.8% | 48.7 | 5.1 | D |
| | Through | 520 | 516 | 99.2% | 19.3 | 2.1 | B |
| | Right Turn | 110 | 112 | 102.2% | 2.9 | 0.6 | A |
| | Subtotal | 670 | 667 | 99.6% | 18.2 | 1.8 | B |
| EB | Left Turn | 30 | 30 | 99.3% | 34.0 | 3.3 | C |
| | Through | 30 | 31 | 104.7% | 33.2 | 3.6 | C |
| | Right Turn | 90 | 95 | 106.0% | 10.3 | 2.4 | B |
| | Subtotal | 150 | 157 | 104.4% | 19.3 | 2.9 | B |
| WB | Left Turn | 60 | 41 | 67.5% | 44.6 | 4.8 | D |
| | Through | 30 | 21 | 69.3% | 41.5 | 8.1 | D |
| | Right Turn | 20 | 13 | 66.5% | 13.8 | 3.0 | B |
| | Subtotal | 110 | 75 | 67.8% | 38.5 | 2.9 | D |
| Total | | 2,070 | 1,739 | 84.0% | 20.7 | 1.2 | C |

Intersection 2 Mathilda Avenue/Innovation Way Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 1,060 | 765 | 72.1% | 107.0 | 7.6 | F |
| | Through | 970 | 702 | 72.4% | 37.1 | 2.3 | D |
| | Right Turn | 1,240 | 905 | 73.0% | 62.2 | 12.1 | E |
| | Subtotal | 3,270 | 2,372 | 72.5% | 69.2 | 5.8 | E |
| SB | Left Turn | 50 | 48 | 96.2% | 147.9 | 29.6 | F |
| | Through | 390 | 383 | 98.3% | 71.6 | 6.7 | E |
| | Right Turn | 230 | 222 | 96.3% | 54.5 | 8.5 | D |
| | Subtotal | 670 | 653 | 97.5% | 71.4 | 7.1 | E |
| EB | Left Turn | 90 | 80 | 88.3% | 76.1 | 15.0 | E |
| | Through | 90 | 80 | 88.4% | 78.4 | 16.3 | E |
| | Right Turn | 140 | 121 | 86.1% | 71.4 | 14.2 | E |
| | Subtotal | 320 | 280 | 87.4% | 74.7 | 14.7 | E |
| WB | Left Turn | 360 | 242 | 67.2% | 233.0 | 22.9 | F |
| | Through | 180 | 133 | 73.8% | 263.1 | 25.5 | F |
| | Right Turn | 80 | 58 | 71.9% | 246.1 | 24.5 | F |
| | Subtotal | 620 | 432 | 69.7% | 244.1 | 23.5 | F |
| Total | | 4,880 | 3,737 | 76.6% | 90.0 | 4.5 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2040 Build Alternative 2
AM Peak Hour

Intersection 3 Mathilda Avenue/Moffett Park Drive-SR 237 WB Ramps Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 1,100 | 795 | 72.3% | 12.5 | 0.9 | B |
| | Through | 2,660 | 1,912 | 71.9% | 36.4 | 1.9 | D |
| | Right Turn | | | | | | |
| | Subtotal | 3,760 | 2,707 | 72.0% | 29.4 | 1.6 | C |
| SB | Left Turn | | | | | | |
| | Through | 380 | 330 | 86.8% | 56.2 | 6.5 | E |
| | Right Turn | 510 | 420 | 82.3% | 133.5 | 37.3 | F |
| | Subtotal | 890 | 749 | 84.3% | 99.5 | 23.7 | F |
| EB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| WB | Left Turn | 670 | 494 | 73.7% | 603.5 | 170.6 | F |
| | Through | | | | | | |
| | Right Turn | 610 | 441 | 72.2% | 851.6 | 188.5 | F |
| | Subtotal | 1,280 | 935 | 73.0% | 720.4 | 179.0 | F |
| Total | | 5,930 | 4,391 | 74.3% | 188.4 | 43.1 | F |

Intersection 4 Mathilda Avenue/SR 237 EB On-Ramp Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | 2,980 | 2,104 | 70.6% | 32.8 | 1.1 | C |
| | Right Turn | 920 | 653 | 70.9% | 2.9 | 0.2 | A |
| | Subtotal | 3,900 | 2,757 | 70.7% | 25.7 | 0.9 | C |
| SB | Left Turn | 80 | 67 | 83.6% | 4.2 | 1.1 | A |
| | Through | 970 | 769 | 79.3% | 47.3 | 6.9 | D |
| | Right Turn | | | | | | |
| | Subtotal | 1,050 | 836 | 79.6% | 43.8 | 6.4 | D |
| EB | Left Turn | 780 | 616 | 79.0% | 704.3 | 292.8 | F |
| | Through | | | | | | |
| | Right Turn | 70 | 56 | 80.1% | 464.6 | 255.5 | F |
| | Subtotal | 850 | 672 | 79.1% | 684.3 | 289.7 | F |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 5,800 | 4,265 | 73.8% | 133.0 | 47.5 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2040 Build Alternative 2
AM Peak Hour

Intersection 5 Mathilda Avenue/Ross Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 80 | 53 | 65.6% | 124.5 | 9.1 | F |
| | Through | 3,510 | 2,498 | 71.2% | 75.7 | 3.2 | E |
| | Right Turn | 120 | 84 | 69.9% | 48.6 | 3.9 | D |
| | Subtotal | 3,710 | 2,635 | 71.0% | 75.8 | 3.1 | E |
| SB | Left Turn | 70 | 56 | 80.6% | 52.9 | 16.7 | D |
| | Through | 920 | 722 | 78.5% | 30.4 | 2.6 | C |
| | Right Turn | 50 | 40 | 79.4% | 24.2 | 4.3 | C |
| | Subtotal | 1,040 | 818 | 78.7% | 31.6 | 2.2 | C |
| EB | Left Turn | 90 | 59 | 65.0% | 906.6 | 396.5 | F |
| | Through | 70 | 51 | 72.4% | 795.3 | 389.1 | F |
| | Right Turn | 40 | 29 | 71.8% | 756.6 | 412.9 | F |
| | Subtotal | 200 | 138 | 69.0% | 835.0 | 397.6 | F |
| WB | Left Turn | 130 | 91 | 70.1% | 753.4 | 168.3 | F |
| | Through | 40 | 28 | 69.8% | 746.3 | 161.2 | F |
| | Right Turn | 300 | 213 | 70.9% | 778.5 | 150.7 | F |
| | Subtotal | 470 | 332 | 70.6% | 769.0 | 155.0 | F |
| Total | | 5,420 | 3,922 | 72.4% | 149.8 | 21.4 | F |

Intersection 6 Mathilda Avenue/US 101 NB Ramps Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | 2,930 | 1,883 | 64.3% | 104.7 | 5.3 | F |
| | Right Turn | 570 | 346 | 60.7% | 13.2 | 0.8 | B |
| | Subtotal | 3,500 | 2,229 | 63.7% | 90.5 | 4.7 | F |
| SB | Left Turn | 20 | 17 | 83.5% | 38.7 | 12.5 | D |
| | Through | 1,070 | 833 | 77.9% | 11.2 | 1.3 | B |
| | Right Turn | | | | | | |
| | Subtotal | 1,090 | 850 | 78.0% | 11.7 | 1.5 | B |
| EB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| WB | Left Turn | 770 | 792 | 102.8% | 156.7 | 36.3 | F |
| | Through | | | | | | |
| | Right Turn | 780 | 755 | 96.8% | 141.5 | 36.5 | F |
| | Subtotal | 1,550 | 1,547 | 99.8% | 149.3 | 36.4 | F |
| Total | | 6,140 | 4,626 | 75.3% | 95.6 | 11.5 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2040 Build Alternative 2
AM Peak Hour

Intersection 7 Mathilda Avenue/US 101 SB Ramps Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | 3,120 | 1,855 | 59.5% | 106.6 | 8.8 | F |
| | Right Turn | 700 | 421 | 60.2% | 27.0 | 3.3 | C |
| | Subtotal | 3,820 | 2,276 | 59.6% | 91.9 | 7.9 | F |
| SB | Left Turn | | | | | | |
| | Through | 1,650 | 1,474 | 89.4% | 13.2 | 1.4 | B |
| | Right Turn | 190 | 145 | 76.3% | 10.6 | 1.1 | B |
| | Subtotal | 1,840 | 1,619 | 88.0% | 13.0 | 1.3 | B |
| EB | Left Turn | 380 | 382 | 100.5% | 105.8 | 26.9 | F |
| | Through | | | | | | |
| | Right Turn | 520 | 524 | 100.7% | 44.4 | 18.8 | D |
| | Subtotal | 900 | 906 | 100.6% | 70.2 | 21.7 | E |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 6,560 | 4,801 | 73.2% | 61.1 | 6.8 | E |

Intersection 8 Mathilda Avenue-US 101 On-Ramp/Almanor Avenue-Ahwanee Avenue Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 140 | 78 | 55.5% | 1269.3 | 85.4 | F |
| | Through | 3,430 | 1,878 | 54.7% | 1315.2 | 89.8 | F |
| | Right Turn | 70 | 41 | 59.1% | 1300.2 | 91.3 | F |
| | Subtotal | 3,640 | 1,997 | 54.9% | 1313.1 | 89.7 | F |
| SB | Left Turn | 160 | 149 | 92.9% | 205.2 | 59.7 | F |
| | Through | 1,680 | 1,557 | 92.6% | 39.5 | 5.8 | D |
| | Right Turn | 330 | 298 | 90.3% | 43.0 | 5.3 | D |
| | Subtotal | 2,170 | 2,003 | 92.3% | 52.4 | 8.4 | D |
| EB | Left Turn | 130 | 131 | 100.5% | 62.5 | 6.7 | E |
| | Through | 30 | 35 | 115.3% | 57.8 | 10.6 | E |
| | Right Turn | 40 | 41 | 103.5% | 27.7 | 5.4 | C |
| | Subtotal | 200 | 207 | 103.4% | 54.9 | 5.1 | D |
| WB | Left Turn | 90 | 90 | 100.1% | 73.1 | 9.4 | E |
| | Through | 50 | 53 | 106.8% | 68.2 | 8.1 | E |
| | Right Turn | 260 | 270 | 104.0% | 21.5 | 5.3 | C |
| | Subtotal | 400 | 414 | 103.5% | 38.9 | 5.1 | D |
| Total | | 6,410 | 4,621 | 72.1% | 595.3 | 29.3 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2040 Build Alternative 2
AM Peak Hour

Intersection 9 Innovation Way-US 101 On-Ramp/Moffett Park Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| EB | Left Turn | | | | | | |
| | Through | 230 | 230 | 100.1% | 3.2 | 0.4 | A |
| | Right Turn | 20 | 23 | 115.0% | 2.3 | 0.5 | A |
| | Subtotal | 250 | 253 | 101.3% | 3.1 | 0.3 | A |
| WB | Left Turn | 40 | 31 | 77.8% | 9.4 | 0.9 | A |
| | Through | 990 | 753 | 76.1% | 3.7 | 0.4 | A |
| | Right Turn | | | | | | |
| | Subtotal | 1,030 | 784 | 76.2% | 3.9 | 0.4 | A |
| Total | | 1,280 | 1,038 | 81.1% | 3.7 | 0.3 | A |

Intersection 10 Innovation Way/Moffett Park Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | 280 | 228 | 81.3% | 30.0 | 2.0 | C |
| | Subtotal | 280 | 228 | 81.3% | 30.0 | 2.0 | C |
| EB | Left Turn | 230 | 232 | 100.8% | 34.3 | 3.0 | C |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | 230 | 232 | 100.8% | 34.3 | 3.0 | C |
| WB | Left Turn | | | | | | |
| | Through | 750 | 556 | 74.1% | 12.3 | 0.8 | B |
| | Right Turn | 490 | 368 | 75.0% | 15.6 | 2.2 | B |
| | Subtotal | 1,240 | 923 | 74.5% | 13.6 | 1.1 | B |
| Total | | 1,750 | 1,383 | 79.0% | 19.8 | 1.0 | B |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2040 Build Alternative 2
AM Peak Hour

Intersection 11 Innovation Way/11th Avenue All-way Stop

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 130 | 101 | 77.9% | 9.8 | 0.3 | A |
| | Through | 260 | 223 | 85.7% | 11.6 | 0.5 | B |
| | Right Turn | 240 | 203 | 84.7% | 7.6 | 0.5 | A |
| | Subtotal | 630 | 527 | 83.7% | 9.7 | 0.4 | A |
| SB | Left Turn | 130 | 103 | 79.1% | 9.1 | 0.7 | A |
| | Through | 240 | 186 | 77.4% | 12.5 | 0.7 | B |
| | Right Turn | 410 | 324 | 79.0% | 13.7 | 1.4 | B |
| | Subtotal | 780 | 612 | 78.5% | 12.6 | 1.0 | B |
| EB | Left Turn | 50 | 50 | 100.6% | 10.1 | 2.0 | B |
| | Through | | | | | | |
| | Right Turn | 30 | 29 | 97.3% | 6.8 | 1.1 | A |
| | Subtotal | 80 | 80 | 99.4% | 8.9 | 1.6 | A |
| WB | Left Turn | 20 | 21 | 104.5% | 5.2 | 0.3 | A |
| | Through | | | | | | |
| | Right Turn | 20 | 20 | 101.5% | 2.5 | 0.5 | A |
| | Subtotal | 40 | 41 | 103.0% | 3.8 | 0.3 | A |
| Total | | 1,530 | 1,260 | 82.4% | 10.8 | 0.5 | B |

Intersection 12 Innovation Way/Juniper Networks Driveway Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 110 | 88 | 79.5% | 301.5 | 103.7 | F |
| | Through | 220 | 194 | 88.2% | 103.0 | 59.8 | F |
| | Right Turn | | | | | | |
| | Subtotal | 330 | 282 | 85.3% | 164.9 | 74.5 | F |
| SB | Left Turn | | | | | | |
| | Through | 720 | 549 | 76.3% | 15.1 | 1.5 | B |
| | Right Turn | 750 | 565 | 75.4% | 14.2 | 1.4 | B |
| | Subtotal | 1,470 | 1,115 | 75.8% | 14.6 | 1.4 | B |
| EB | Left Turn | 100 | 88 | 87.7% | 232.5 | 214.7 | F |
| | Through | | | | | | |
| | Right Turn | 60 | 62 | 102.5% | 14.6 | 2.9 | B |
| | Subtotal | 160 | 149 | 93.3% | 137.2 | 108.4 | F |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 1,960 | 1,545 | 78.8% | 53.4 | 17.6 | D |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2040 Build Alternative 2
AM Peak Hour

Intersection 13 Bordeaux Drive/Innovation Way Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 390 | 242 | 61.9% | 1686.4 | 516.0 | F |
| | Through | 130 | 82 | 63.2% | 1534.8 | 503.2 | F |
| | Right Turn | | | | | | |
| | Subtotal | 520 | 324 | 62.3% | 1648.6 | 515.0 | F |
| SB | Left Turn | | | | | | |
| | Through | 60 | 52 | 85.8% | 100.1 | 31.2 | F |
| | Right Turn | 150 | 139 | 92.4% | 97.2 | 39.1 | F |
| | Subtotal | 210 | 190 | 90.5% | 98.1 | 36.9 | F |
| EB | Left Turn | 370 | 274 | 73.9% | 45.3 | 7.7 | D |
| | Through | 50 | 40 | 79.4% | 47.5 | 9.5 | D |
| | Right Turn | 690 | 510 | 73.8% | 29.1 | 6.3 | C |
| | Subtotal | 1,110 | 823 | 74.1% | 35.4 | 7.0 | D |
| WB | Left Turn | | | | | | |
| | Through | 20 | 19 | 97.0% | 80.2 | 25.7 | F |
| | Right Turn | | | | | | |
| | Subtotal | 20 | 19 | 97.0% | 80.2 | 25.7 | F |
| Total | | 1,860 | 1,356 | 72.9% | 422.2 | 103.7 | F |

Intersection 1 Mathilda Avenue/5th Avenue Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 625 | 50 | 8 | 75 | 15 | 100 | 15 | 0% | 0% |
| | Through | 625 | 50 | 3 | 75 | 5 | 100 | 12 | 0% | 0% |
| | Right Turn | 625 | 50 | 6 | 100 | 11 | 150 | 15 | 0% | 0% |
| NB | Left Turn | 425 | 75 | 8 | 125 | 14 | 150 | 22 | 0% | 0% |
| | Through | 1,125 | 100 | 13 | 175 | 23 | 225 | 39 | 0% | 0% |
| | Through/Right | 1,125 | 125 | 9 | 225 | 19 | 250 | 34 | 0% | 0% |
| SB | Left Turn | 250 | 50 | 4 | 100 | 9 | 100 | 21 | 0% | 0% |
| | Through | 1,325 | 100 | 12 | 175 | 20 | 200 | 33 | 0% | 0% |
| | Right Turn | 250 | 25 | 4 | 50 | 15 | 75 | 30 | 0% | 0% |
| WB | Left Turn | 925 | 50 | 5 | 100 | 11 | 100 | 19 | 9% | 0% |
| | Through/Right | 75 | 50 | 7 | 75 | 9 | 100 | 3 | 6% | 0% |

Intersection 2 Mathilda Avenue/Innovation Way Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|--------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left/Through | 225 | 200 | 11 | 300 | 16 | 325 | 23 | 0% | 23% |
| | Right Turn | 225 | 25 | 5 | 50 | 11 | 75 | 16 | 0% | 8% |
| NB | Left Turn | 725 | 550 | 42 | 900 | 25 | 800 | 1 | 11% | 0% |
| | Through | 975 | 425 | 113 | 1,025 | 213 | 1,075 | 111 | 2% | 2% |
| | Right Turn | 975 | 650 | 115 | 1,200 | 171 | 1,150 | 83 | 0% | 3% |
| SB | Left Turn | 75 | 75 | 8 | 150 | 9 | 150 | 1 | 20% | 0% |
| | Through | 975 | 175 | 27 | 300 | 66 | 375 | 103 | 25% | 0% |
| | Right Turn | 225 | 175 | 19 | 275 | 35 | 275 | 17 | 8% | 0% |
| WB | Left Turn | 425 | 775 | 2 | 800 | 4 | 800 | 10 | 32% | 44% |
| | Shared | 225 | 225 | 1 | 250 | 4 | 250 | 0 | 74% | 0% |

Intersection 3 Mathilda Avenue/Moffett Park Drive-SR 237 WB Ramps

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NE | Left Turn | 150 | 50 | 7 | 150 | 13 | 175 | 20 | 0% | 1% |
| | Through | 400 | 425 | 14 | 500 | 15 | 500 | 22 | 0% | 6% |
| SB | Through | 975 | 625 | 139 | 900 | 210 | 950 | 185 | 22% | 0% |
| WB | Left Turn | 1,075 | 700 | 76 | 1,125 | 105 | 1,125 | 51 | 0% | 3% |
| | Right Turn | 550 | 675 | 3 | 675 | 8 | 675 | 14 | 80% | 0% |
| | | | | | | | | | | |

Intersection 4 Mathilda Avenue/SR 237 EB On-Ramp

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|--------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 20,775 | 3,525 | 415 | 6,125 | 522 | 6,475 | 517 | 28% | 0% |
| | Right Turn | 450 | 200 | 52 | 600 | 73 | 575 | 53 | 0% | 0% |
| NB | Through | 150 | 225 | 10 | 275 | 10 | 275 | 16 | 0% | 43% |
| | Right Turn | 150 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| SB | Left/Through | 200 | 25 | 1 | 25 | 8 | 25 | 19 | 0% | 0% |
| | Through | 400 | 250 | 22 | 300 | 30 | 350 | 36 | 0% | 1% |
| | | | | | | | | | | |

Intersection 5

Mathilda Avenue/Ross Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 250 | 125 | 7 | 125 | 9 | 125 | 0 | 88% | 0% |
| | Through | 1,575 | 1,175 | 500 | 1,775 | 511 | 1,675 | 190 | 18% | 34% |
| | Right Turn | 50 | 25 | 5 | 75 | 9 | 100 | 3 | 2% | 0% |
| NB | Left Turn | 250 | 125 | 24 | 300 | 33 | 275 | 1 | 0% | 0% |
| | Through | 700 | 675 | 18 | 800 | 41 | 750 | 15 | 75% | 18% |
| | Through/Right | 700 | 575 | 9 | 775 | 32 | 725 | 12 | 0% | 3% |
| SB | Left Turn | 225 | 50 | 8 | 100 | 26 | 150 | 44 | 0% | 0% |
| | Through | 225 | 125 | 18 | 200 | 26 | 200 | 16 | 0% | 2% |
| | Through/Right | 225 | 150 | 17 | 250 | 24 | 250 | 16 | 0% | 9% |
| WB | Left Turn | 100 | 50 | 10 | 125 | 13 | 100 | 6 | 10% | 0% |
| | Through | 225 | 3,200 | 818 | 5,000 | 1,188 | 5,075 | 1,124 | 2% | 0% |
| | Right Turn | 100 | 100 | 1 | 125 | 5 | 125 | 0 | 89% | 0% |

Intersection 6

Mathilda Avenue/US 101 NB Ramps

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NB | Through | 575 | 650 | 8 | 700 | 19 | 700 | 17 | 0% | 45% |
| | Right Turn | 575 | 350 | 64 | 800 | 51 | 700 | 41 | 0% | 0% |
| SB | Left Turn | 375 | 25 | 4 | 50 | 9 | 75 | 10 | 0% | 0% |
| | Through | 700 | 125 | 18 | 250 | 30 | 275 | 38 | 0% | 0% |
| WB | Left Turn | 1,025 | 800 | 144 | 1,475 | 223 | 1,950 | 258 | 10% | 0% |
| | Right Turn | 1,025 | 400 | 7 | 425 | 13 | 400 | 12 | 0% | 0% |
| | | | | | | | | | | |

Intersection 7 **Mathilda Avenue/US 101 SB Ramps** **Signal**

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,050 | 250 | 69 | 400 | 103 | 425 | 99 | 27% | 1% |
| | Right Turn | 1,050 | 25 | 2 | 25 | 16 | 25 | 33 | 0% | 0% |
| NB | Through | 750 | 750 | 37 | 875 | 55 | 825 | 20 | 0% | 18% |
| | Right Turn | 750 | 725 | 53 | 975 | 91 | 800 | 10 | 0% | 16% |
| SB | Through | 575 | 125 | 18 | 225 | 31 | 250 | 35 | 0% | 0% |
| | Through/Right | 575 | 150 | 23 | 275 | 24 | 300 | 16 | 0% | 0% |
| | | | | | | | | | | |

Intersection 8 **Mathilda Avenue-US 101 On-Ramp/Almanor Avenue-Ahwanee Avenue** **Signal**

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,025 | 100 | 9 | 150 | 14 | 175 | 24 | 4% | 0% |
| | Through/Right | 125 | 75 | 4 | 125 | 13 | 150 | 21 | 1% | 0% |
| NB | Left Turn | 425 | 225 | 39 | 575 | 46 | 500 | 0 | 0% | 0% |
| | Through | 725 | 11,625 | 469 | 16,450 | 334 | 14,100 | 34 | 80% | 43% |
| | Through/Right | 725 | 300 | 0 | 300 | 1 | 300 | 0 | 31% | 0% |
| SB | Left Turn | 275 | 250 | 44 | 375 | 28 | 350 | 0 | 37% | 0% |
| | Through | 750 | 275 | 86 | 525 | 112 | 650 | 138 | 9% | 1% |
| | Through/Right | 750 | 325 | 28 | 525 | 57 | 575 | 96 | 0% | 0% |
| WB | Left Turn | 250 | 100 | 13 | 200 | 32 | 250 | 69 | 0% | 0% |
| | Through | 1,025 | 125 | 34 | 275 | 68 | 325 | 97 | 25% | 0% |
| | Right Turn | 75 | 100 | 5 | 150 | 3 | 125 | 0 | 34% | 0% |

Intersection 9 Innovation Way-US 101 On-Ramp/Moffett Park Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Through | 850 | 25 | 6 | 75 | 17 | 125 | 24 | 0% | 0% |
| | Right Turn | 150 | 25 | 1 | 25 | 3 | 50 | 1 | 0% | 0% |
| WB | Left Turn | 850 | 25 | 4 | 50 | 3 | 75 | 9 | 0% | 0% |
| | Through | 850 | 25 | 18 | 150 | 173 | 400 | 505 | 0% | 0% |
| | | | | | | | | | | |
| | | | | | | | | | | |

Intersection 10 Innovation Way/Moffett Park Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 850 | 100 | 14 | 175 | 26 | 200 | 44 | 0% | 0% |
| SB | Right Turn | 575 | 50 | 6 | 100 | 10 | 125 | 17 | 0% | 0% |
| WB | Through | 1,150 | 100 | 10 | 200 | 19 | 250 | 38 | 0% | 0% |
| | Through/Right | 1,150 | 175 | 12 | 275 | 22 | 325 | 46 | 0% | 0% |
| | | | | | | | | | | |

Intersection 11

Innovation Way/11th Avenue

All-way Stop

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 125 | 25 | 3 | 75 | 5 | 75 | 10 | 0% | 0% |
| | Left/Through | 325 | 25 | 3 | 50 | 5 | 50 | 10 | 0% | 0% |
| | Right Turn | 325 | 25 | 3 | 50 | 3 | 75 | 8 | 0% | 0% |
| NB | Left Turn | 125 | 50 | 3 | 75 | 6 | 100 | 13 | 0% | 0% |
| | Through | 575 | 75 | 7 | 175 | 11 | 250 | 22 | 0% | 0% |
| | Through/Right | 575 | 50 | 6 | 100 | 15 | 125 | 29 | 0% | 0% |
| SB | Left Turn | 175 | 50 | 3 | 75 | 7 | 100 | 18 | 0% | 0% |
| | Through | 1,000 | 50 | 4 | 100 | 15 | 150 | 44 | 0% | 0% |
| | Through/Right | 1,000 | 125 | 14 | 200 | 42 | 275 | 70 | 0% | 0% |
| WB | Left Turn | 325 | 25 | 3 | 50 | 3 | 50 | 10 | 0% | 0% |
| | Through/Right | 325 | 25 | 2 | 50 | 2 | 50 | 1 | 0% | 0% |

Intersection 12

Innovation Way/Juniper Networks Driveway

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 200 | 225 | 193 | 500 | 442 | 550 | 449 | 0% | 0% |
| | Right Turn | 200 | 50 | 5 | 75 | 9 | 100 | 19 | 0% | 0% |
| NB | Left Turn | 125 | 150 | 17 | 200 | 10 | 175 | 1 | 71% | 0% |
| | Through | 1,000 | 400 | 125 | 700 | 178 | 800 | 167 | 5% | 0% |
| SB | Through | 300 | 75 | 17 | 150 | 37 | 175 | 60 | 0% | 2% |
| | Through/Right | 300 | 275 | 22 | 300 | 35 | 325 | 34 | 0% | 3% |
| | | | | | | | | | | |

Intersection 13

Bordeaux Drive/Innovation Way

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left/Through | 375 | 300 | 26 | 450 | 18 | 400 | 3 | 33% | 7% |
| | Right Turn | 125 | 125 | 2 | 150 | 7 | 150 | 0 | 15% | 0% |
| NB | Left Turn | 325 | 1,600 | 112 | 2,875 | 146 | 3,025 | 140 | 95% | 0% |
| | Through/Right | 2,025 | 1,000 | 7 | 1,050 | 35 | 1,025 | 1 | 1% | 54% |
| SB | Left Turn | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | Through/Right | 725 | 225 | 55 | 425 | 100 | 550 | 126 | 46% | 0% |
| WB | Left/Through | 125 | 25 | 7 | 75 | 14 | 100 | 24 | 1% | 0% |
| | Right Turn | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |

Arterial Level of Service

Build 2 2040 AM

2/29/2016

Arterial Level of Service: NB Mathilda Ave

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|--------------------|------|---------------|-----------------|------------|----------------|
| Ahwanee Ave | 8 | 123.9 | 134.8 | 0.1 | 4 |
| | 7 | 104.6 | 116.8 | 0.2 | 5 |
| US 101 NB Ramps | 6 | 104.8 | 114.9 | 0.1 | 4 |
| Ross Dr | 5 | 75.4 | 86.9 | 0.1 | 6 |
| | 4 | 31.5 | 36.1 | 0.0 | 5 |
| SR 237 EB Off-Ramp | 43 | 2.9 | 7.2 | 0.0 | 17 |
| Mathilda Ave | 57 | 5.8 | 10.7 | 0.0 | 12 |
| Mathilda Ave | 3 | 20.1 | 24.3 | 0.0 | 6 |
| Innovation Way | 2 | 32.3 | 51.1 | 0.2 | 15 |
| 5th Ave | 1 | 17.1 | 36.3 | 0.2 | 23 |
| | 107 | 4.4 | 26.7 | 0.3 | 37 |
| Total | | 523.0 | 645.8 | 1.5 | 8 |

Arterial Level of Service: SB Mathilda Ave

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|-----------------|------|---------------|-----------------|------------|----------------|
| 5th Ave | 1 | 19.3 | 40.6 | 0.3 | 24 |
| Innovation Way | 2 | 71.2 | 89.6 | 0.2 | 10 |
| | 3 | 54.9 | 85.5 | 0.2 | 9 |
| Ross Dr | 5 | 30.6 | 36.3 | 0.0 | 5 |
| US 101 NB Ramps | 6 | 12.6 | 24.1 | 0.1 | 22 |
| US 101 SB Ramps | 7 | 12.4 | 23.3 | 0.1 | 21 |
| Almanor Ave | 8 | 36.2 | 48.4 | 0.2 | 11 |
| San Aleso Ave | 201 | 3.6 | 15.0 | 0.1 | 34 |
| Total | | 240.8 | 362.9 | 1.4 | 13 |

Arterial Level of Service: NB Innovation Way

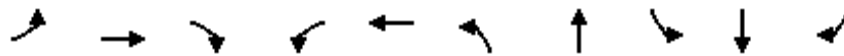
| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|------------------|------|---------------|-----------------|------------|----------------|
| | 910 | 2.5 | 7.2 | 0.0 | 11 |
| | 53 | 0.9 | 5.7 | 0.0 | 26 |
| | 11 | 8.9 | 16.4 | 0.1 | 16 |
| | 200 | 66.8 | 83.1 | 0.2 | 7 |
| Juniper Driveway | 12 | 36.7 | 42.5 | 0.1 | 5 |
| Driveway | 217 | 13.0 | 16.2 | 0.0 | 8 |
| | 902 | 45.0 | 47.3 | 0.0 | 2 |
| Mathilda Ave | 2 | 17.6 | 19.5 | 0.0 | 5 |
| | 16 | 7.6 | 20.8 | 0.1 | 16 |
| Bordeaux Dr | 13 | 39.2 | 51.2 | 0.1 | 6 |
| Total | | 238.3 | 309.8 | 0.6 | 7 |

Arterial Level of Service: SB Innovation Way

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|------------------|------|---------------|-----------------|-----------|----------------|
| | 16 | 47.2 | 57.0 | 0.1 | 5 |
| Mathilda Ave | 2 | 171.1 | 182.6 | 0.1 | 2 |
| | 902 | 9.0 | 14.1 | 0.0 | 7 |
| Driveway | 217 | 1.9 | 3.7 | 0.0 | 19 |
| Juniper Driveway | 12 | 10.5 | 14.4 | 0.0 | 9 |
| | 200 | 2.0 | 8.5 | 0.1 | 24 |
| 11th Ave | 11 | 10.6 | 26.4 | 0.2 | 22 |
| | 53 | 3.2 | 10.7 | 0.1 | 24 |
| | 910 | 15.0 | 19.4 | 0.0 | 8 |
| Moffett Park Dr | 10 | 12.3 | 17.2 | 0.0 | 5 |
| Total | | 282.7 | 353.9 | 0.6 | 6 |

Lanes, Volumes, Timings
1: Mathilda Ave & 5th Ave

3/4/2016

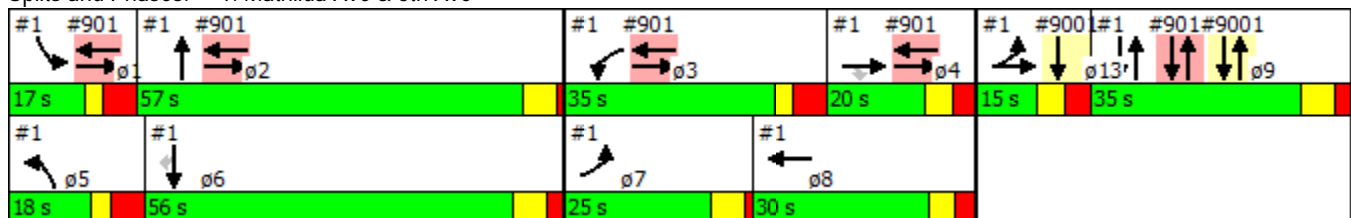


| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT | SBR | ø2 | ø7 |
|----------------------|------|------|--------|-------|-------|-------|-----|------|------|--------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 180 | 40 | 170 | 290 | 20 | 140 | 660 | 20 | 1120 | 30 | | |
| Turn Type | Prot | NA | custom | Prot | NA | Prot | NA | Prot | NA | custom | | |
| Protected Phases | 7 13 | 4 13 | | 3 | 8 | 5 | 2 9 | 1 | 6 9 | | 2 | 7 |
| Permitted Phases | | | 4 | | | | | | | 6 | | |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 5 | 2 | 1 | 6 | 6 | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 13.0 | 12.0 | 8.0 | 11.0 | | 10.0 | | 12.0 | 12.0 | 12.0 |
| Minimum Split (s) | | | 20.0 | 19.0 | 29.5 | 18.0 | | 17.0 | | 41.0 | 33.5 | 17.5 |
| Total Split (s) | | | 20.0 | 35.0 | 30.0 | 18.0 | | 17.0 | | 56.0 | 57.0 | 25.0 |
| Total Split (%) | | | 11.2% | 19.6% | 16.8% | 10.1% | | 9.5% | | 31.3% | 32% | 14% |
| Yellow Time (s) | | | 3.6 | 2.5 | 3.6 | 2.5 | | 2.5 | | 4.7 | 4.5 | 4.5 |
| All-Red Time (s) | | | 3.4 | 4.5 | 2.9 | 4.5 | | 4.5 | | 2.3 | 1.0 | 1.0 |
| Lost Time Adjust (s) | | | 0.0 | 0.0 | 0.0 | 0.0 | | 0.0 | | 0.0 | | |
| Total Lost Time (s) | | | 7.0 | 7.0 | 6.5 | 7.0 | | 7.0 | | 7.0 | | |
| Lead/Lag | | | Lag | Lead | Lag | Lead | | Lead | | Lag | Lag | Lead |
| Lead-Lag Optimize? | | | Yes | Yes | Yes | Yes | | Yes | | Yes | Yes | Yes |
| Recall Mode | | | None | None | None | None | | None | | None | Min | None |

Intersection Summary

Cycle Length: 179
 Actuated Cycle Length: 119
 Natural Cycle: 160
 Control Type: Actuated-Uncoordinated

Splits and Phases: 1: Mathilda Ave & 5th Ave



| Lane Group | ø9 | ø13 |
|----------------------|------|------|
| Lane Configurations | | |
| Volume (vph) | | |
| Turn Type | | |
| Protected Phases | 9 | 13 |
| Permitted Phases | | |
| Detector Phase | | |
| Switch Phase | | |
| Minimum Initial (s) | 28.0 | 8.0 |
| Minimum Split (s) | 35.0 | 15.0 |
| Total Split (s) | 35.0 | 15.0 |
| Total Split (%) | 20% | 8% |
| Yellow Time (s) | 4.7 | 3.6 |
| All-Red Time (s) | 2.3 | 3.4 |
| Lost Time Adjust (s) | | |
| Total Lost Time (s) | | |
| Lead/Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes |
| Recall Mode | None | None |
| Intersection Summary | | |

Lanes, Volumes, Timings
 2: Mathilda Ave & Innovation Way

3/4/2016



| Lane Group | EBT | EBR | WBL | WBT | NBL | NBT | NBR | SBL | SBT | SBR | ø2 | ø4 |
|----------------------|------|--------|-------|-------|------|-----|-------|------|------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 320 | 1240 | 735 | 190 | 190 | 290 | 390 | 80 | 1430 | 70 | | |
| Turn Type | NA | pt+ov | Split | NA | Prot | NA | pm+ov | Prot | NA | Perm | | |
| Protected Phases | 4 13 | 4 13 5 | 8 | 8 | 5 | 2 9 | 8 | 1 | 6 9 | | 2 | 4 |
| Permitted Phases | | | | | | | 2 9 | | | | | 6 9 |
| Detector Phase | 4 | 4 | 8 | 8 | 5 | 2 | 8 | 1 | 6 | 6 | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 10.0 | 10.0 | 10.0 | | 10.0 | 10.0 | | | 12.0 | 14.0 |
| Minimum Split (s) | | | 35.0 | 35.0 | 17.0 | | 35.0 | 16.8 | | | 19.0 | 39.0 |
| Total Split (s) | | | 37.0 | 37.0 | 16.0 | | 37.0 | 16.0 | | | 50.0 | 47.0 |
| Total Split (%) | | | 18.5% | 18.5% | 8.0% | | 18.5% | 8.0% | | | 25% | 24% |
| Yellow Time (s) | | | 2.5 | 2.5 | 2.5 | | 2.5 | 2.5 | | | 2.5 | 2.5 |
| All-Red Time (s) | | | 4.5 | 4.5 | 4.5 | | 4.5 | 4.3 | | | 4.5 | 4.5 |
| Lost Time Adjust (s) | | | 0.0 | 0.0 | 0.0 | | 0.0 | 0.0 | | | | |
| Total Lost Time (s) | | | 7.0 | 7.0 | 7.0 | | 7.0 | 6.8 | | | | |
| Lead/Lag | | | | | Lead | | | Lead | | | Lag | |
| Lead-Lag Optimize? | | | | | Yes | | | Yes | | | Yes | |
| Recall Mode | | | None | None | None | | None | None | | | None | None |

Intersection Summary

Cycle Length: 200
 Actuated Cycle Length: 200
 Offset: 0 (0%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 175
 Control Type: Actuated-Coordinated

Splits and Phases: 2: Mathilda Ave & Innovation Way

| | | | | |
|------|------|------|------|------|
| | | | | |
| 47 s | 16 s | 50 s | 37 s | 15 s |
| | | | | |
| | 16 s | 50 s | | |

Lanes, Volumes, Timings
 2: Mathilda Ave & Innovation Way

3/4/2016

| Lane Group | ø6 | ø9 | ø13 |
|----------------------|-------|------|------|
| Lane Configurations | | | |
| Volume (vph) | | | |
| Turn Type | | | |
| Protected Phases | 6 | 9 | 13 |
| Permitted Phases | | | |
| Detector Phase | | | |
| Switch Phase | | | |
| Minimum Initial (s) | 12.0 | 28.0 | 8.0 |
| Minimum Split (s) | 30.0 | 35.0 | 15.0 |
| Total Split (s) | 50.0 | 35.0 | 15.0 |
| Total Split (%) | 25% | 18% | 8% |
| Yellow Time (s) | 4.7 | 4.7 | 2.5 |
| All-Red Time (s) | 2.3 | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | |
| Total Lost Time (s) | | | |
| Lead/Lag | Lag | Lag | Lead |
| Lead-Lag Optimize? | Yes | Yes | Yes |
| Recall Mode | C-Max | None | None |
| Intersection Summary | | | |

Lanes, Volumes, Timings
 3: Mathilda Ave & SR 237 WB Off-Ramp

3/4/2016

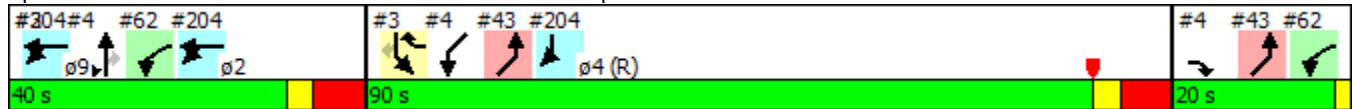


| Lane Group | WBR | SBL | SBR2 | NEL | ø9 |
|----------------------|-------|-------|-------|-------|------|
| Lane Configurations | ↖ | ↙↘↗ | ↖ | ↙↘↗ | |
| Volume (vph) | 240 | 2260 | 1145 | 630 | |
| Turn Type | Prot | Prot | Perm | Prot | |
| Protected Phases | 4 | 4 | | 2 | 9 |
| Permitted Phases | | | 4 | | |
| Detector Phase | 4 | 4 | 4 | 2 | |
| Switch Phase | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | 26.7 | 26.7 | 26.7 | 26.7 | 18.0 |
| Total Split (s) | 90.0 | 90.0 | 90.0 | 40.0 | 20.0 |
| Total Split (%) | 60.0% | 60.0% | 60.0% | 26.7% | 13% |
| Yellow Time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 2.0 |
| All-Red Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 0.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | 9.0 | 9.0 | 9.0 | 9.0 | |
| Lead/Lag | | | | | |
| Lead-Lag Optimize? | | | | | |
| Recall Mode | C-Max | C-Max | C-Max | None | Max |

Intersection Summary

Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 0 (0%), Referenced to phase 4:SBL, Start of Yellow, Master Intersection
 Natural Cycle: 150
 Control Type: Actuated-Coordinated

Splits and Phases: 3: Mathilda Ave & SR 237 WB Off-Ramp



Lanes, Volumes, Timings
 4: Mathilda Ave & SR 237 EB Off-Ramp

3/4/2016

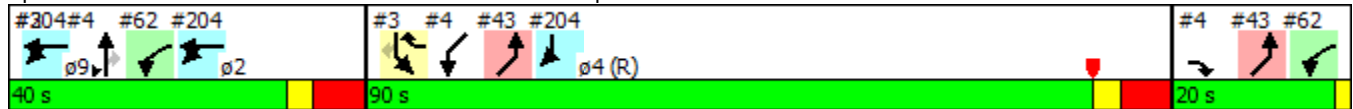


| Lane Group | EBR | NBT | NBR2 | SWL | ø9 |
|----------------------|--------|-------|-------|-------|------|
| Lane Configurations | ↘ | ↑↑↑ | ↘ | ↑↑↑↑ | |
| Volume (vph) | 210 | 700 | 860 | 2620 | |
| Turn Type | custom | NA | Perm | Prot | |
| Protected Phases | 2 9 | 2 | | 4 | 9 |
| Permitted Phases | | | 2 | | |
| Detector Phase | 2 | 2 | 2 | 4 | |
| Switch Phase | | | | | |
| Minimum Initial (s) | | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | | 26.7 | 26.7 | 26.7 | 18.0 |
| Total Split (s) | | 40.0 | 40.0 | 90.0 | 20.0 |
| Total Split (%) | | 26.7% | 26.7% | 60.0% | 13% |
| Yellow Time (s) | | 3.0 | 3.0 | 3.0 | 2.0 |
| All-Red Time (s) | | 6.0 | 6.0 | 6.0 | 0.0 |
| Lost Time Adjust (s) | | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | | 9.0 | 9.0 | 9.0 | |
| Lead/Lag | | | | | |
| Lead-Lag Optimize? | | | | | |
| Recall Mode | | None | None | C-Max | Max |

Intersection Summary

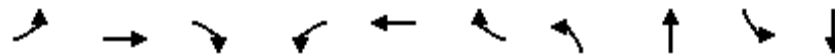
Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 0 (0%), Referenced to phase 4:SBL, Start of Yellow, Master Intersection
 Natural Cycle: 150
 Control Type: Actuated-Coordinated

Splits and Phases: 4: Mathilda Ave & SR 237 EB Off-Ramp



Lanes, Volumes, Timings
5: Mathilda Ave & Ross Dr

3/4/2016

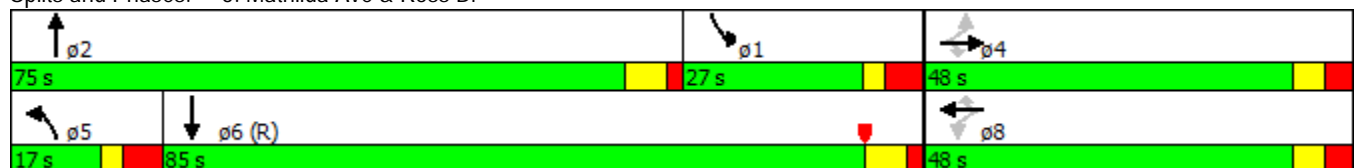


| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↖ | ↑ | ↗ | ↖ | ↑ | ↗ | ↖ | ↑↑↑↑ | ↖ | ↑↑↑ |
| Volume (vph) | 60 | 200 | 60 | 290 | 70 | 130 | 160 | 1370 | 180 | 2570 |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | Prot | NA | Prot | NA |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | 1 | 6 |
| Permitted Phases | 4 | | 4 | 8 | | 8 | | | | |
| Detector Phase | 4 | 4 | 4 | 8 | 8 | 8 | 5 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | | | |
| Minimum Initial (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 4.0 | 4.0 | 4.0 | 5.0 |
| Minimum Split (s) | 48.0 | 48.0 | 48.0 | 19.0 | 19.0 | 19.0 | 11.0 | 31.4 | 11.0 | 11.6 |
| Total Split (s) | 48.0 | 48.0 | 48.0 | 48.0 | 48.0 | 48.0 | 17.0 | 75.0 | 27.0 | 85.0 |
| Total Split (%) | 32.0% | 32.0% | 32.0% | 32.0% | 32.0% | 32.0% | 11.3% | 50.0% | 18.0% | 56.7% |
| Yellow Time (s) | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 3.6 | 2.5 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 3.4 | 3.4 | 3.4 | 3.4 | 3.4 | 3.4 | 4.5 | 1.7 | 4.5 | 1.9 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.4 | 7.0 | 6.6 |
| Lead/Lag | | | | | | | Lead | Lead | Lag | Lag |
| Lead-Lag Optimize? | | | | | | | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | Max | Max | Max | Max | None | None | C-Max |

Intersection Summary

Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 140 (93%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 145
 Control Type: Actuated-Coordinated

Splits and Phases: 5: Mathilda Ave & Ross Dr



Lanes, Volumes, Timings
 6: Mathilda Ave & US 101 NB Ramps

3/4/2016



| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|-------|
| Lane Configurations | ↖↖ | ↖↖ | ↑↑↑ | ↖ | ↖ | ↑↑↑ |
| Volume (vph) | 850 | 280 | 1600 | 340 | 40 | 2880 |
| Turn Type | Prot | pm+ov | NA | Perm | Prot | NA |
| Protected Phases | 8 | 1 | 2 | | 1 | 6 |
| Permitted Phases | | 8 | | 2 | | |
| Detector Phase | 8 | 1 | 2 | 2 | 1 | 6 |
| Switch Phase | | | | | | |
| Minimum Initial (s) | 8.0 | 4.0 | 8.0 | 8.0 | 4.0 | 4.0 |
| Minimum Split (s) | 14.9 | 9.7 | 39.9 | 39.9 | 9.7 | 10.9 |
| Total Split (s) | 48.0 | 18.0 | 84.0 | 84.0 | 18.0 | 102.0 |
| Total Split (%) | 32.0% | 12.0% | 56.0% | 56.0% | 12.0% | 68.0% |
| Yellow Time (s) | 4.7 | 3.5 | 4.7 | 4.7 | 3.5 | 4.7 |
| All-Red Time (s) | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.9 | 5.7 | 6.9 | 6.9 | 5.7 | 6.9 |
| Lead/Lag | | Lead | Lag | Lag | Lead | |
| Lead-Lag Optimize? | | Yes | Yes | Yes | Yes | |
| Recall Mode | None | None | None | None | None | C-Max |

Intersection Summary

Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 120 (80%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 90
 Control Type: Actuated-Coordinated

Splits and Phases: 6: Mathilda Ave & US 101 NB Ramps



Lanes, Volumes, Timings
 7: Mathilda Ave & US 101 SB Ramps

3/4/2016



| Lane Group | EBL | EBR | NBT | NBR | SBT |
|----------------------|-------|-------|-------|-------|-------|
| Lane Configurations | | | | | |
| Volume (vph) | 140 | 550 | 1800 | 680 | 2270 |
| Turn Type | Prot | Prot | NA | Perm | NA |
| Protected Phases | 7 | 7 | 2 | | 6 |
| Permitted Phases | | | | 2 | |
| Detector Phase | 7 | 7 | 2 | 2 | 6 |
| Switch Phase | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | 10.9 | 10.9 | 22.9 | 22.9 | 22.9 |
| Total Split (s) | 35.0 | 35.0 | 115.0 | 115.0 | 115.0 |
| Total Split (%) | 23.3% | 23.3% | 76.7% | 76.7% | 76.7% |
| Yellow Time (s) | 4.7 | 4.7 | 4.7 | 4.7 | 4.7 |
| All-Red Time (s) | 2.2 | 2.2 | 2.2 | 2.2 | 2.2 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.9 | 6.9 | 6.9 | 6.9 | 6.9 |
| Lead/Lag | | | | | |
| Lead-Lag Optimize? | | | | | |
| Recall Mode | None | None | None | None | C-Max |

Intersection Summary

Cycle Length: 150
 Actuated Cycle Length: 150
 Offset: 122 (81%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 150
 Control Type: Actuated-Coordinated

Splits and Phases: 7: Mathilda Ave & US 101 SB Ramps



Lanes, Volumes, Timings
 8: Mathilda Ave & Almanor Ave/Ahwanee Ave

3/4/2016

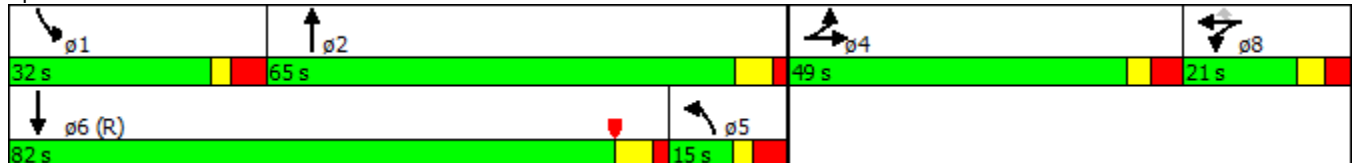


| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
|----------------------|-------|-------|-------|-------|-------|------|-------|-------|-------|
| Lane Configurations | | | | | | | | | |
| Volume (vph) | 430 | 40 | 60 | 30 | 260 | 80 | 1790 | 260 | 2460 |
| Turn Type | Split | NA | Split | NA | Perm | Prot | NA | Prot | NA |
| Protected Phases | 4 | 4 | 8 | 8 | | 5 | 2 | 1 | 6 |
| Permitted Phases | | | | | 8 | | | | |
| Detector Phase | 4 | 4 | 8 | 8 | 8 | 5 | 2 | 1 | 6 |
| Switch Phase | | | | | | | | | |
| Minimum Initial (s) | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 | 12.0 | 8.0 | 12.0 |
| Minimum Split (s) | 49.0 | 49.0 | 15.0 | 15.0 | 15.0 | 15.0 | 36.7 | 15.0 | 27.7 |
| Total Split (s) | 49.0 | 49.0 | 21.0 | 21.0 | 21.0 | 15.0 | 65.0 | 32.0 | 82.0 |
| Total Split (%) | 29.3% | 29.3% | 12.6% | 12.6% | 12.6% | 9.0% | 38.9% | 19.2% | 49.1% |
| Yellow Time (s) | 2.8 | 2.8 | 3.6 | 3.6 | 3.6 | 2.5 | 4.7 | 2.5 | 4.7 |
| All-Red Time (s) | 4.2 | 4.2 | 3.4 | 3.4 | 3.4 | 4.5 | 2.0 | 4.5 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 7.0 | 6.7 | 7.0 | 6.7 |
| Lead/Lag | | | | | | Lag | Lag | Lead | Lead |
| Lead-Lag Optimize? | | | | | | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | None | None | None | C-Max |

Intersection Summary

Cycle Length: 167
 Actuated Cycle Length: 167
 Offset: 0 (0%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 140
 Control Type: Actuated-Coordinated

Splits and Phases: 8: Mathilda Ave & Almanor Ave/Ahwanee Ave



Lanes, Volumes, Timings
 9: US 101 On-Ramp & Moffett Park Dr

3/4/2016

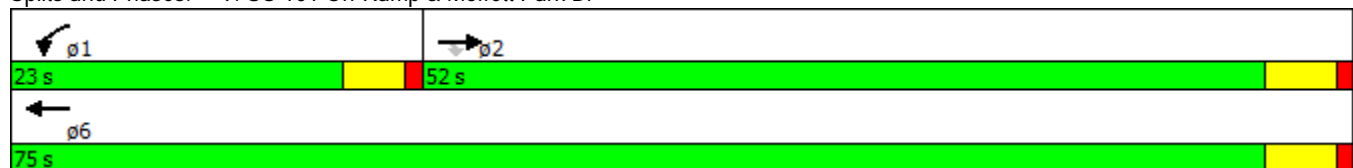


| Lane Group | EBT | EBR | WBL | WBT |
|----------------------|-------|-------|-------|--------|
| Lane Configurations | ↑ | ↑ | ↑ | ↑ |
| Volume (vph) | 1010 | 150 | 350 | 315 |
| Turn Type | NA | Perm | Prot | NA |
| Protected Phases | 2 | | 1 | 6 |
| Permitted Phases | | 2 | | |
| Detector Phase | 2 | 2 | 1 | 6 |
| Switch Phase | | | | |
| Minimum Initial (s) | 15.0 | 15.0 | 6.0 | 15.0 |
| Minimum Split (s) | 20.0 | 20.0 | 10.5 | 20.0 |
| Total Split (s) | 52.0 | 52.0 | 23.0 | 75.0 |
| Total Split (%) | 69.3% | 69.3% | 30.7% | 100.0% |
| Yellow Time (s) | 4.0 | 4.0 | 3.5 | 4.0 |
| All-Red Time (s) | 1.0 | 1.0 | 1.0 | 1.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.0 | 5.0 | 4.5 | 5.0 |
| Lead/Lag | Lag | Lag | Lead | |
| Lead-Lag Optimize? | | | | |
| Recall Mode | Min | Min | None | Min |

Intersection Summary

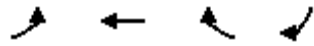
Cycle Length: 75
 Actuated Cycle Length: 67.2
 Natural Cycle: 70
 Control Type: Semi Act-Uncoord

Splits and Phases: 9: US 101 On-Ramp & Moffett Park Dr



Lanes, Volumes, Timings
 10: Moffett Park Dr & Innovation Way

3/4/2016

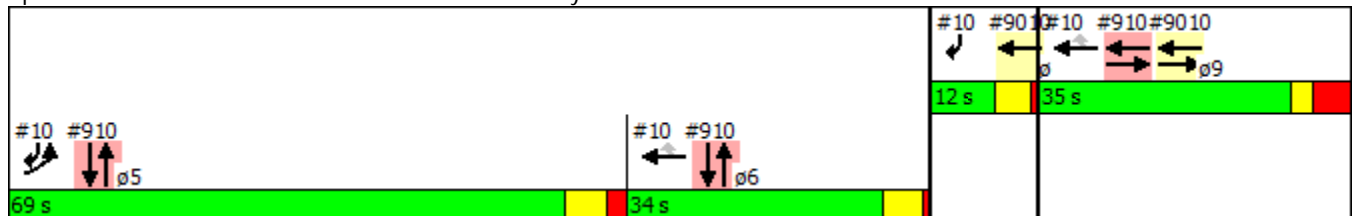


| Lane Group | EBL | WBT | WBR | SBR | ø4 | ø6 | ø9 |
|----------------------|-------|-----|------|-------|------|------|------|
| Lane Configurations | ↗↘ | ↑↑ | ↗ | ↗↘ | | | |
| Volume (vph) | 1010 | 415 | 160 | 250 | | | |
| Turn Type | Prot | NA | Perm | pt+ov | | | |
| Protected Phases | 5 | 6 9 | | 4 5 | 4 | 6 | 9 |
| Permitted Phases | | | 6 9 | | | | |
| Detector Phase | 5 | 6 | 6 9 | 5 | | | |
| Switch Phase | | | | | | | |
| Minimum Initial (s) | 8.0 | | | | 4.0 | 10.0 | 28.0 |
| Minimum Split (s) | 15.0 | | | | 9.0 | 27.5 | 35.0 |
| Total Split (s) | 69.0 | | | | 12.0 | 34.0 | 35.0 |
| Total Split (%) | 46.0% | | | | 8% | 23% | 23% |
| Yellow Time (s) | 4.7 | | | | 4.0 | 4.5 | 2.5 |
| All-Red Time (s) | 2.3 | | | | 1.0 | 1.0 | 4.5 |
| Lost Time Adjust (s) | 0.0 | | | | | | |
| Total Lost Time (s) | 7.0 | | | | | | |
| Lead/Lag | Lead | | | | | Lag | |
| Lead-Lag Optimize? | Yes | | | | | Yes | |
| Recall Mode | Max | | | | None | Min | None |

Intersection Summary

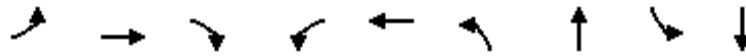
Cycle Length: 150
 Actuated Cycle Length: 137.7
 Natural Cycle: 110
 Control Type: Semi Act-Uncoord

Splits and Phases: 10: Moffett Park Dr & Innovation Way



Lanes, Volumes, Timings
 11: Innovation Way & 11th Ave

3/4/2016



| Lane Group | EBL | EBT | EBR | WBL | WBT | NBL | NBT | SBL | SBT |
|---------------------|-----|------|-----|-----|------|-----|------|-----|------|
| Lane Configurations | | | | | | | | | |
| Volume (vph) | 500 | 0 | 80 | 40 | 0 | 200 | 910 | 110 | 60 |
| Sign Control | | Stop | | | Stop | | Stop | | Stop |

Intersection Summary

Control Type: Unsignalized

Lanes, Volumes, Timings
 12: Innovation Way & Juniper Driveway

3/4/2016

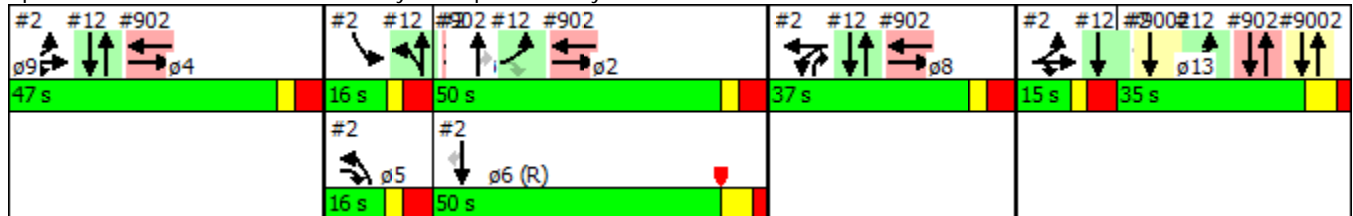


| Lane Group | EBL | EBR | NBL | NBT | SBT | ø2 | ø4 | ø5 | ø6 | ø8 | ø9 | ø13 |
|----------------------|------|------|------|-------|--------|------|------|------|-------|------|------|------|
| Lane Configurations | | | | | | | | | | | | |
| Volume (vph) | 700 | 80 | 60 | 1370 | 280 | | | | | | | |
| Turn Type | Prot | Perm | Prot | NA | NA | | | | | | | |
| Protected Phases | 2 9 | | 1 | 1 4 8 | 4 8 13 | 2 | 4 | 5 | 6 | 8 | 9 | 13 |
| Permitted Phases | | 2 9 | | | | | | | | | | |
| Detector Phase | 2 | 2 | 1 | 1 4 8 | 4 8 | | | | | | | |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | | | 10.0 | | | 12.0 | 14.0 | 10.0 | 12.0 | 10.0 | 28.0 | 8.0 |
| Minimum Split (s) | | | 16.8 | | | 19.0 | 39.0 | 17.0 | 30.0 | 35.0 | 35.0 | 15.0 |
| Total Split (s) | | | 16.0 | | | 50.0 | 47.0 | 16.0 | 50.0 | 37.0 | 35.0 | 15.0 |
| Total Split (%) | | | 8.0% | | | 25% | 24% | 8% | 25% | 19% | 18% | 8% |
| Yellow Time (s) | | | 2.5 | | | 2.5 | 2.5 | 2.5 | 4.7 | 2.5 | 4.7 | 2.5 |
| All-Red Time (s) | | | 4.3 | | | 4.5 | 4.5 | 4.5 | 2.3 | 4.5 | 2.3 | 4.5 |
| Lost Time Adjust (s) | | | 0.0 | | | | | | | | | |
| Total Lost Time (s) | | | 6.8 | | | | | | | | | |
| Lead/Lag | | | Lead | | | Lag | | Lead | Lag | | Lag | Lead |
| Lead-Lag Optimize? | | | Yes | | | Yes | | Yes | Yes | | Yes | Yes |
| Recall Mode | | | None | | | None | None | None | C-Max | None | None | None |

Intersection Summary

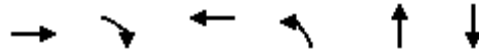
Cycle Length: 200
 Actuated Cycle Length: 200
 Offset: 0 (0%), Referenced to phase 6:SBT, Start of Yellow
 Natural Cycle: 175
 Control Type: Actuated-Coordinated

Splits and Phases: 12: Innovation Way & Juniper Driveway



Lanes, Volumes, Timings
 13: Bordeaux Dr & Innovation Way

3/4/2016

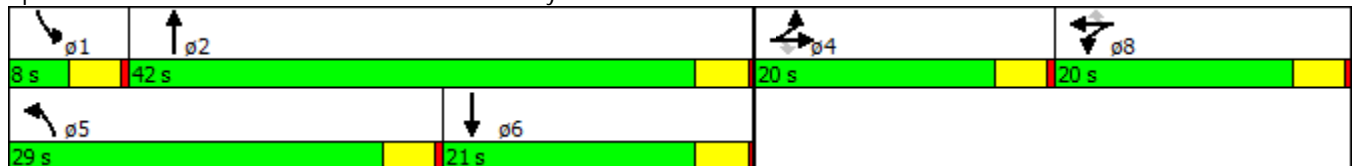


| Lane Group | EBT | EBR | WBT | NBL | NBT | SBT | ø1 |
|----------------------|-------|-------|-------|-------|-------|-------|------|
| Lane Configurations | ↕ | ↗ | ↕ | ↖ | ↗ | ↗ | |
| Volume (vph) | 30 | 230 | 30 | 630 | 50 | 180 | |
| Turn Type | NA | Perm | NA | Prot | NA | NA | |
| Protected Phases | 4 | | 8 | 5 | 2 | 6 | 1 |
| Permitted Phases | | 4 | | | | | |
| Detector Phase | 4 | 4 | 8 | 5 | 2 | 6 | |
| Switch Phase | | | | | | | |
| Minimum Initial (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Minimum Split (s) | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 | 8.0 |
| Total Split (s) | 20.0 | 20.0 | 20.0 | 29.0 | 42.0 | 21.0 | 8.0 |
| Total Split (%) | 22.2% | 22.2% | 22.2% | 32.2% | 46.7% | 23.3% | 9% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 | 0.5 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Lost Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Lead/Lag | | | | Lead | Lag | Lag | Lead |
| Lead-Lag Optimize? | | | | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | None | None |

Intersection Summary

Cycle Length: 90
 Actuated Cycle Length: 69.3
 Natural Cycle: 100
 Control Type: Actuated-Uncoordinated

Splits and Phases: 13: Bordeaux Dr & Innovation Way



**SimTraffic Post-Processor
Average Results from 10 Runs
Network Performance**

**Mathilda Avenue Improvements
2040 Build Alternative 2
PM Peak Hour**

| Performance Measure | Average | Std. Dev. | Minimum | Maximum |
|---------------------------------|---------|-----------|---------|---------|
| Average Delay (seconds) | 805.9 | 20.6 | 779.7 | 842.4 |
| Total Delay (hours) | 3,262 | 77 | 3,146 | 3,353 |
| Average Stopped Delay (seconds) | 765.6 | 20.8 | 737.5 | 804.0 |
| Total Stopped Delay (hours) | 3099 | 77 | 2968 | 3180 |
| Total Stops | 45,667 | 2,869 | 39,342 | 49,375 |
| Average Stops | 3.13 | 0.18 | 2.76 | 3.41 |
| Total Distance Traveled (miles) | 42,106 | 740 | 40,281 | 42,804 |
| Average Speed (mph) | 9.8 | 0.4 | 9.0 | 10.0 |
| Total Travel Time (hours) | 4,661.5 | 85.5 | 4,511.0 | 4,794.6 |
| Vehicles Entered | 11,709 | 139 | 11,398 | 11,870 |
| Vehicles Exited | 8,923 | 247 | 8,295 | 9,163 |
| Percent Demand Served | 76.2% | 1.7% | 72.8% | 78.1% |
| Fuel Used (gallons) | 1,857 | 22 | 1,810 | 1,891 |
| HC Emissions (grams) | 18,337 | 1,136 | 15,905 | 20,074 |
| CO Emissions (grams) | 512,188 | 22,448 | 465,696 | 545,304 |
| NOx Emissions (grams) | 67,436 | 3,261 | 60,577 | 71,637 |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2040 Build Alternative 2
PM Peak Hour

Intersection 1 Mathilda Avenue/5th Avenue Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 140 | 74 | 52.7% | 58.6 | 6.1 | E |
| | Through | 660 | 352 | 53.3% | 19.1 | 4.1 | B |
| | Right Turn | 60 | 34 | 56.8% | 55.1 | 72.1 | E |
| | Subtotal | 860 | 460 | 53.5% | 28.0 | 8.2 | C |
| SB | Left Turn | 20 | 15 | 73.5% | 300.1 | 233.7 | F |
| | Through | 1,120 | 953 | 85.1% | 182.1 | 61.4 | F |
| | Right Turn | 30 | 29 | 95.0% | 137.6 | 71.3 | F |
| | Subtotal | 1,170 | 997 | 85.2% | 182.2 | 61.0 | F |
| EB | Left Turn | 180 | 179 | 99.3% | 66.2 | 35.6 | E |
| | Through | 40 | 32 | 80.5% | 116.3 | 59.7 | F |
| | Right Turn | 170 | 158 | 92.6% | 61.6 | 37.3 | E |
| | Subtotal | 390 | 369 | 94.5% | 68.3 | 37.7 | E |
| WB | Left Turn | 290 | 98 | 33.8% | 115.1 | 30.4 | F |
| | Through | 20 | 7 | 35.0% | 97.8 | 42.8 | F |
| | Right Turn | 110 | 43 | 38.8% | 66.0 | 24.9 | E |
| | Subtotal | 420 | 148 | 35.2% | 99.3 | 26.7 | F |
| Total | | 2,840 | 1,973 | 69.5% | 117.9 | 31.7 | F |

Intersection 2 Mathilda Avenue/Innovation Way Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 190 | 171 | 90.1% | 201.5 | 60.0 | F |
| | Through | 290 | 255 | 87.9% | 32.8 | 2.5 | C |
| | Right Turn | 390 | 347 | 88.9% | 19.8 | 2.6 | B |
| | Subtotal | 870 | 773 | 88.9% | 64.7 | 14.8 | E |
| SB | Left Turn | 80 | 61 | 76.5% | 419.0 | 52.8 | F |
| | Through | 1,430 | 1,058 | 74.0% | 336.6 | 54.0 | F |
| | Right Turn | 70 | 52 | 74.7% | 290.4 | 43.2 | F |
| | Subtotal | 1,580 | 1,171 | 74.1% | 338.9 | 52.5 | F |
| EB | Left Turn | 510 | 186 | 36.5% | 90.0 | 16.0 | F |
| | Through | 320 | 121 | 37.8% | 92.6 | 12.4 | F |
| | Right Turn | 1,240 | 467 | 37.6% | 93.8 | 18.2 | F |
| | Subtotal | 2,070 | 774 | 37.4% | 92.6 | 16.5 | F |
| WB | Left Turn | 735 | 264 | 36.0% | 363.1 | 80.7 | F |
| | Through | 190 | 70 | 36.7% | 354.0 | 63.2 | F |
| | Right Turn | 60 | 23 | 38.8% | 344.7 | 33.8 | F |
| | Subtotal | 985 | 357 | 36.3% | 359.8 | 73.0 | F |
| Total | | 5,505 | 3,076 | 55.9% | 209.0 | 24.9 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2040 Build Alternative 2
PM Peak Hour

Intersection 3 Mathilda Avenue/Moffett Park Drive-SR 237 WB Ramps Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 290 | 231 | 79.7% | 3.7 | 3.9 | A |
| | Through | 630 | 526 | 83.4% | 45.6 | 2.7 | D |
| | Right Turn | | | | | | |
| | Subtotal | 920 | 757 | 82.3% | 32.8 | 3.1 | C |
| SB | Left Turn | | | | | | |
| | Through | 2,260 | 1,031 | 45.6% | 102.0 | 16.6 | F |
| | Right Turn | 1,145 | 754 | 65.8% | 182.9 | 40.3 | F |
| | Subtotal | 3,405 | 1,785 | 54.2% | 136.1 | 26.6 | F |
| EB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| WB | Left Turn | 820 | 820 | 100.0% | 80.1 | 5.3 | F |
| | Through | | | | | | |
| | Right Turn | 240 | 247 | 103.0% | 28.2 | 0.8 | C |
| | Subtotal | 1,060 | 1,067 | 100.7% | 68.1 | 4.3 | E |
| Total | | 5,385 | 3,609 | 73.8% | 94.4 | 15.1 | F |

Intersection 4 Mathilda Avenue/SR 237 EB On-Ramp Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | 700 | 538 | 76.8% | 61.9 | 4.2 | E |
| | Right Turn | 860 | 670 | 77.9% | 2.5 | 0.2 | A |
| | Subtotal | 1,560 | 1,208 | 77.4% | 28.9 | 2.0 | C |
| SB | Left Turn | 460 | 204 | 44.4% | 4.8 | 0.2 | A |
| | Through | 2,620 | 1,643 | 62.7% | 28.7 | 1.1 | C |
| | Right Turn | | | | | | |
| | Subtotal | 3,080 | 1,848 | 60.7% | 26.1 | 1.0 | C |
| EB | Left Turn | 220 | 220 | 100.2% | 30.2 | 7.1 | C |
| | Through | | | | | | |
| | Right Turn | 210 | 217 | 103.2% | 45.9 | 11.2 | D |
| | Subtotal | 430 | 437 | 101.7% | 38.0 | 9.1 | D |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 5,070 | 3,493 | 71.6% | 28.6 | 2.4 | C |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2040 Build Alternative 2
PM Peak Hour

Intersection 5 Mathilda Avenue/Ross Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 160 | 123 | 76.9% | 193.4 | 68.3 | F |
| | Through | 1,370 | 1,074 | 78.4% | 129.2 | 8.6 | F |
| | Right Turn | 350 | 278 | 79.5% | 250.0 | 4.9 | F |
| | Subtotal | 1,880 | 1,476 | 78.5% | 157.7 | 10.1 | F |
| SB | Left Turn | 180 | 120 | 66.5% | 49.0 | 4.0 | D |
| | Through | 2,570 | 1,687 | 65.6% | 16.2 | 2.3 | B |
| | Right Turn | 80 | 54 | 67.1% | 10.3 | 2.8 | B |
| | Subtotal | 2,830 | 1,860 | 65.7% | 18.1 | 2.1 | B |
| EB | Left Turn | 60 | 57 | 95.2% | 49.2 | 3.6 | D |
| | Through | 200 | 206 | 102.8% | 46.0 | 2.9 | D |
| | Right Turn | 60 | 59 | 98.5% | 23.2 | 3.4 | C |
| | Subtotal | 320 | 322 | 100.6% | 42.4 | 2.5 | D |
| WB | Left Turn | 290 | 180 | 62.1% | 1023.4 | 166.3 | F |
| | Through | 70 | 46 | 65.4% | 1056.9 | 195.7 | F |
| | Right Turn | 130 | 82 | 63.0% | 990.1 | 180.5 | F |
| | Subtotal | 490 | 308 | 62.8% | 1019.2 | 172.5 | F |
| Total | | 5,520 | 3,965 | 71.8% | 149.0 | 11.2 | F |

Intersection 6 Mathilda Avenue/US 101 NB Ramps Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | 1,600 | 1,221 | 76.3% | 178.9 | 8.2 | F |
| | Right Turn | 340 | 240 | 70.7% | 10.6 | 0.6 | B |
| | Subtotal | 1,940 | 1,461 | 75.3% | 151.2 | 6.7 | F |
| SB | Left Turn | 40 | 26 | 64.5% | 71.2 | 9.0 | E |
| | Through | 2,880 | 1,894 | 65.8% | 42.5 | 20.2 | D |
| | Right Turn | | | | | | |
| | Subtotal | 2,920 | 1,920 | 65.8% | 42.9 | 20.0 | D |
| EB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| WB | Left Turn | 850 | 798 | 93.9% | 257.5 | 162.8 | F |
| | Through | | | | | | |
| | Right Turn | 280 | 260 | 93.0% | 245.5 | 160.3 | F |
| | Subtotal | 1,130 | 1,058 | 93.6% | 254.5 | 162.1 | F |
| Total | | 5,990 | 4,439 | 74.1% | 127.7 | 40.2 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2040 Build Alternative 2
PM Peak Hour

Intersection 7 Mathilda Avenue/US 101 SB Ramps Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | 1,800 | 1,346 | 74.8% | 161.9 | 12.6 | F |
| | Right Turn | 680 | 528 | 77.7% | 36.3 | 4.1 | D |
| | Subtotal | 2,480 | 1,874 | 75.6% | 126.5 | 9.6 | F |
| SB | Left Turn | | | | | | |
| | Through | 2,270 | 1,747 | 77.0% | 16.9 | 3.0 | B |
| | Right Turn | 1,460 | 948 | 64.9% | 32.9 | 12.6 | C |
| | Subtotal | 3,730 | 2,695 | 72.2% | 22.6 | 5.9 | C |
| EB | Left Turn | 140 | 126 | 89.9% | 330.0 | 726.1 | F |
| | Through | | | | | | |
| | Right Turn | 550 | 513 | 93.2% | 110.9 | 271.4 | F |
| | Subtotal | 690 | 639 | 92.5% | 132.2 | 290.5 | F |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 6,900 | 5,207 | 75.5% | 66.5 | 16.1 | E |

Intersection 8 Mathilda Avenue-US 101 On-Ramp/Almanor Avenue-Ahwanee Avenue Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 80 | 61 | 75.6% | 566.2 | 96.1 | F |
| | Through | 1,790 | 1,236 | 69.0% | 594.1 | 112.6 | F |
| | Right Turn | 60 | 38 | 62.5% | 614.5 | 124.1 | F |
| | Subtotal | 1,930 | 1,334 | 69.1% | 593.4 | 111.9 | F |
| SB | Left Turn | 260 | 202 | 77.8% | 112.3 | 17.1 | F |
| | Through | 2,460 | 1,959 | 79.6% | 37.8 | 2.5 | D |
| | Right Turn | 100 | 84 | 83.7% | 29.1 | 3.9 | C |
| | Subtotal | 2,820 | 2,245 | 79.6% | 44.2 | 3.5 | D |
| EB | Left Turn | 430 | 418 | 97.2% | 136.2 | 42.9 | F |
| | Through | 40 | 43 | 108.3% | 116.4 | 37.6 | F |
| | Right Turn | 90 | 90 | 100.3% | 97.1 | 41.3 | F |
| | Subtotal | 560 | 552 | 98.5% | 128.2 | 41.9 | F |
| WB | Left Turn | 60 | 58 | 96.8% | 76.8 | 11.3 | E |
| | Through | 30 | 26 | 86.0% | 112.6 | 44.4 | F |
| | Right Turn | 260 | 256 | 98.3% | 57.3 | 29.5 | E |
| | Subtotal | 350 | 340 | 97.0% | 65.0 | 26.2 | E |
| Total | | 5,660 | 4,470 | 79.0% | 219.4 | 32.1 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2040 Build Alternative 2
PM Peak Hour

Intersection 9 Innovation Way-US 101 On-Ramp/Moffett Park Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| EB | Left Turn | | | | | | |
| | Through | 1,010 | 377 | 37.4% | 257.1 | 55.2 | F |
| | Right Turn | 150 | 66 | 43.9% | 150.5 | 20.9 | F |
| | Subtotal | 1,160 | 443 | 38.2% | 241.1 | 49.6 | F |
| WB | Left Turn | 350 | 283 | 81.0% | 47.3 | 13.4 | D |
| | Through | 315 | 247 | 78.5% | 3.0 | 0.7 | A |
| | Right Turn | | | | | | |
| | Subtotal | 665 | 531 | 79.8% | 26.6 | 7.4 | C |
| Total | | 1,825 | 974 | 53.4% | 122.3 | 15.7 | F |

Intersection 10 Innovation Way/Moffett Park Drive Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | 250 | 219 | 87.5% | 23.8 | 2.9 | C |
| | Subtotal | 250 | 219 | 87.5% | 23.8 | 2.9 | C |
| EB | Left Turn | 1,010 | 374 | 37.0% | 565.1 | 106.3 | F |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | 1,010 | 374 | 37.0% | 565.1 | 106.3 | F |
| WB | Left Turn | | | | | | |
| | Through | 415 | 311 | 74.9% | 35.1 | 6.0 | D |
| | Right Turn | 160 | 76 | 47.3% | 468.6 | 229.5 | F |
| | Subtotal | 575 | 387 | 67.2% | 116.2 | 45.0 | F |
| Total | | 1,835 | 979 | 53.4% | 262.4 | 33.7 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2040 Build Alternative 2
PM Peak Hour

Intersection 11 Innovation Way/11th Avenue All-way Stop

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 200 | 78 | 38.9% | 192.5 | 44.2 | F |
| | Through | 910 | 352 | 38.7% | 299.4 | 65.9 | F |
| | Right Turn | 50 | 18 | 35.2% | 287.2 | 75.5 | F |
| | Subtotal | 1,160 | 447 | 38.6% | 280.4 | 62.5 | F |
| SB | Left Turn | 110 | 61 | 55.2% | 43.0 | 8.9 | E |
| | Through | 60 | 33 | 54.3% | 32.2 | 14.0 | D |
| | Right Turn | 190 | 104 | 54.6% | 23.9 | 7.9 | C |
| | Subtotal | 360 | 197 | 54.7% | 31.2 | 7.8 | D |
| EB | Left Turn | 500 | 390 | 78.0% | 540.1 | 111.9 | F |
| | Through | | | | | | |
| | Right Turn | 80 | 80 | 100.3% | 88.5 | 25.3 | F |
| | Subtotal | 580 | 470 | 81.1% | 461.6 | 93.6 | F |
| WB | Left Turn | 40 | 39 | 96.3% | 28.5 | 19.4 | D |
| | Through | | | | | | |
| | Right Turn | 20 | 21 | 105.0% | 78.4 | 22.2 | F |
| | Subtotal | 60 | 60 | 99.2% | 46.6 | 16.0 | E |
| Total | | 2,160 | 1,174 | 54.4% | 294.5 | 35.8 | F |

Intersection 12 Innovation Way/Juniper Networks Driveway Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 60 | 31 | 52.2% | 333.7 | 44.2 | F |
| | Through | 1,370 | 731 | 53.4% | 308.9 | 40.6 | F |
| | Right Turn | | | | | | |
| | Subtotal | 1,430 | 762 | 53.3% | 310.0 | 40.6 | F |
| SB | Left Turn | | | | | | |
| | Through | 280 | 182 | 65.1% | 79.7 | 18.3 | E |
| | Right Turn | 170 | 111 | 65.4% | 60.7 | 10.1 | E |
| | Subtotal | 450 | 294 | 65.2% | 72.5 | 14.7 | E |
| EB | Left Turn | 700 | 43 | 6.1% | 2141.6 | 43.0 | F |
| | Through | | | | | | |
| | Right Turn | 80 | 15 | 18.1% | 1737.6 | 130.4 | F |
| | Subtotal | 780 | 57 | 7.3% | 2034.8 | 56.7 | F |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| Total | | 2,660 | 1,113 | 41.8% | 335.8 | 49.0 | F |

SimTraffic Post-Processor
Average Results from 10 Runs
Volume and Delay by Movement

Mathilda Avenue Improvements
2040 Build Alternative 2
PM Peak Hour

Intersection 13 Bordeaux Drive/Innovation Way Signal

| Direction | Movement | Demand Volume (vph) | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|---------------------|---------------------|---------|-----------------------|-----------|-----|
| | | | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | 630 | 177 | 28.1% | 3297.8 | 437.2 | F |
| | Through | 50 | 16 | 32.2% | 3107.8 | 449.1 | F |
| | Right Turn | | | | | | |
| | Subtotal | 680 | 193 | 28.4% | 3282.1 | 439.2 | F |
| SB | Left Turn | | | | | | |
| | Through | 180 | 67 | 37.3% | 1161.3 | 237.5 | F |
| | Right Turn | 230 | 93 | 40.4% | 1162.7 | 254.4 | F |
| | Subtotal | 410 | 160 | 39.0% | 1162.4 | 247.4 | F |
| EB | Left Turn | 90 | 61 | 67.7% | 33.5 | 3.2 | C |
| | Through | 30 | 20 | 67.3% | 32.8 | 6.8 | C |
| | Right Turn | 230 | 153 | 66.4% | 10.3 | 3.3 | B |
| | Subtotal | 350 | 234 | 66.8% | 18.4 | 3.1 | B |
| WB | Left Turn | | | | | | |
| | Through | 30 | 27 | 89.3% | 159.7 | 123.1 | F |
| | Right Turn | | | | | | |
| | Subtotal | 30 | 27 | 89.3% | 159.7 | 123.1 | F |
| Total | | 1,470 | 614 | 41.7% | 1334.8 | 133.7 | F |

Intersection 1 Mathilda Avenue/5th Avenue Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 625 | 150 | 22 | 300 | 46 | 400 | 82 | 32% | 0% |
| | Through | 625 | 100 | 67 | 250 | 130 | 325 | 164 | 0% | 0% |
| | Right Turn | 625 | 125 | 73 | 300 | 135 | 425 | 162 | 0% | 0% |
| NB | Left Turn | 425 | 75 | 6 | 100 | 12 | 125 | 23 | 0% | 0% |
| | Through | 1,125 | 75 | 13 | 150 | 35 | 200 | 58 | 0% | 0% |
| | Through/Right | 1,125 | 75 | 26 | 175 | 60 | 200 | 75 | 0% | 0% |
| SB | Left Turn | 250 | 75 | 35 | 250 | 50 | 300 | 1 | 3% | 0% |
| | Through | 1,325 | 600 | 128 | 1,175 | 263 | 1,250 | 212 | 57% | 5% |
| | Right Turn | 250 | 75 | 27 | 225 | 70 | 300 | 0 | 0% | 0% |
| WB | Left Turn | 925 | 125 | 32 | 250 | 75 | 325 | 146 | 45% | 0% |
| | Through/Right | 75 | 50 | 9 | 100 | 9 | 100 | 0 | 8% | 0% |

Intersection 2 Mathilda Avenue/Innovation Way Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|--------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left/Through | 225 | 300 | 7 | 350 | 10 | 375 | 12 | 0% | 64% |
| | Right Turn | 225 | 200 | 15 | 300 | 21 | 325 | 21 | 0% | 17% |
| NB | Left Turn | 725 | 200 | 54 | 300 | 73 | 350 | 87 | 0% | 0% |
| | Through | 975 | 100 | 12 | 175 | 20 | 200 | 19 | 0% | 0% |
| | Right Turn | 975 | 125 | 22 | 275 | 44 | 375 | 47 | 0% | 0% |
| SB | Left Turn | 75 | 125 | 17 | 175 | 8 | 150 | 0 | 51% | 0% |
| | Through | 975 | 1,150 | 45 | 1,300 | 53 | 1,225 | 15 | 91% | 43% |
| | Right Turn | 225 | 175 | 25 | 375 | 23 | 275 | 0 | 0% | 0% |
| WB | Left Turn | 425 | 775 | 2 | 800 | 3 | 800 | 9 | 68% | 67% |
| | Shared | 225 | 225 | 2 | 250 | 4 | 250 | 0 | 76% | 0% |

Intersection 3 **Mathilda Avenue/Moffett Park Drive-SR 237 WB Ramps** **Signal**

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NB | Left Turn | 350 | 25 | 6 | 50 | 28 | 75 | 48 | 0% | 0% |
| | Through | 400 | 175 | 10 | 200 | 16 | 225 | 23 | 0% | 1% |
| SB | Through | 975 | 1,125 | 7 | 1,175 | 16 | 1,175 | 11 | 9% | 44% |
| WB | Left Turn | 1,075 | 325 | 25 | 450 | 30 | 475 | 35 | 0% | 0% |
| | Right Turn | 550 | 150 | 9 | 225 | 19 | 250 | 25 | 0% | 0% |
| | | | | | | | | | | |

Intersection 4 **Mathilda Avenue/SR 237 EB On-Ramp** **Signal**

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|--------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,050 | 100 | 8 | 175 | 21 | 200 | 42 | 0% | 0% |
| | Right Turn | 450 | 225 | 25 | 300 | 33 | 375 | 38 | 0% | 0% |
| NB | Through | 150 | 125 | 11 | 200 | 15 | 225 | 35 | 0% | 4% |
| | Right Turn | 150 | 25 | 3 | 50 | 33 | 150 | 89 | 0% | 0% |
| SB | Left/Through | 400 | 25 | 2 | 50 | 10 | 75 | 26 | 0% | 0% |
| | Through | 400 | 325 | 12 | 375 | 13 | 375 | 20 | 0% | 3% |
| | | | | | | | | | | |

Intersection 5

Mathilda Avenue/Ross Drive

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 250 | 50 | 9 | 125 | 15 | 125 | 0 | 2% | 0% |
| | Through | 1,575 | 200 | 16 | 350 | 38 | 425 | 68 | 60% | 0% |
| | Right Turn | 50 | 50 | 10 | 125 | 11 | 100 | 0 | 12% | 0% |
| NB | Left Turn | 250 | 175 | 42 | 250 | 39 | 250 | 19 | 22% | 0% |
| | Through | 700 | 725 | 62 | 800 | 71 | 775 | 38 | 14% | 45% |
| | Through/Right | 700 | 725 | 5 | 750 | 9 | 750 | 21 | 0% | 43% |
| SB | Left Turn | 225 | 125 | 7 | 200 | 10 | 225 | 12 | 0% | 1% |
| | Through | 225 | 125 | 14 | 175 | 21 | 175 | 36 | 0% | 1% |
| | Through/Right | 225 | 200 | 22 | 300 | 28 | 275 | 12 | 0% | 27% |
| WB | Left Turn | 100 | 100 | 1 | 125 | 5 | 100 | 0 | 87% | 0% |
| | Through | 225 | 4,500 | 783 | 6,850 | 975 | 6,875 | 739 | 7% | 0% |
| | Right Turn | 100 | 50 | 10 | 100 | 15 | 100 | 0 | 5% | 0% |

Intersection 6

Mathilda Avenue/US 101 NB Ramps

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| NB | Through | 575 | 675 | 4 | 700 | 15 | 700 | 15 | 0% | 73% |
| | Right Turn | 575 | 75 | 24 | 350 | 86 | 700 | 12 | 0% | 0% |
| SB | Left Turn | 375 | 50 | 23 | 150 | 98 | 275 | 163 | 0% | 0% |
| | Through | 700 | 400 | 120 | 525 | 129 | 575 | 145 | 12% | 2% |
| WB | Left Turn | 1,025 | 1,525 | 524 | 2,475 | 661 | 2,750 | 656 | 31% | 0% |
| | Right Turn | 1,025 | 325 | 44 | 500 | 36 | 400 | 25 | 0% | 0% |
| | | | | | | | | | | |

Intersection 7

Mathilda Avenue/US 101 SB Ramps

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,050 | 450 | 161 | 950 | 251 | 1,075 | 249 | 9% | 0% |
| | Right Turn | 1,050 | 25 | 4 | 50 | 29 | 100 | 69 | 0% | 0% |
| NB | Through | 750 | 700 | 53 | 925 | 63 | 800 | 19 | 0% | 22% |
| | Right Turn | 750 | 675 | 78 | 1,050 | 67 | 825 | 52 | 0% | 33% |
| SB | Through | 575 | 425 | 132 | 700 | 158 | 650 | 33 | 0% | 6% |
| | Through/Right | 575 | 475 | 113 | 700 | 79 | 650 | 15 | 0% | 8% |
| | | | | | | | | | | |

Intersection 8

Mathilda Avenue-US 101 On-Ramp/Almanor Avenue-Ahwanee Avenue

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 1,025 | 550 | 197 | 1,000 | 310 | 1,175 | 331 | 61% | 0% |
| | Through/Right | 125 | 150 | 16 | 275 | 16 | 225 | 0 | 7% | 0% |
| NB | Left Turn | 425 | 225 | 21 | 550 | 32 | 500 | 0 | 0% | 0% |
| | Through | 750 | 2,775 | 497 | 5,450 | 610 | 5,650 | 577 | 85% | 0% |
| | Through/Right | 750 | 300 | 3 | 325 | 16 | 300 | 0 | 48% | 0% |
| SB | Left Turn | 275 | 250 | 21 | 375 | 17 | 325 | 0 | 17% | 0% |
| | Through | 750 | 350 | 44 | 550 | 39 | 575 | 53 | 12% | 0% |
| | Through/Right | 750 | 300 | 37 | 450 | 40 | 475 | 59 | 0% | 0% |
| WB | Left Turn | 250 | 100 | 26 | 225 | 79 | 325 | 68 | 0% | 0% |
| | Through | 1,025 | 200 | 85 | 450 | 200 | 550 | 217 | 16% | 0% |
| | Right Turn | 75 | 100 | 6 | 150 | 5 | 125 | 0 | 55% | 0% |

Intersection 9 Innovation Way-US 101 On-Ramp/Moffett Park Drive Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Through | 850 | 875 | 4 | 900 | 24 | 900 | 2 | 85% | 44% |
| | Right Turn | 150 | 250 | 44 | 525 | 20 | 375 | 0 | 0% | 0% |
| WB | Left Turn | 850 | 200 | 30 | 375 | 88 | 450 | 114 | 0% | 0% |
| | Through | 850 | 25 | 16 | 125 | 101 | 275 | 205 | 0% | 0% |
| | | | | | | | | | | |
| | | | | | | | | | | |

Intersection 10 Innovation Way/Moffett Park Drive Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 850 | 925 | 4 | 925 | 4 | 950 | 8 | 0% | 65% |
| | Right Turn | 575 | 50 | 8 | 100 | 13 | 125 | 21 | 0% | 0% |
| WB | Through | 1,150 | 350 | 160 | 650 | 261 | 700 | 228 | 6% | 6% |
| | Right Turn | 1,150 | 225 | 36 | 300 | 36 | 275 | 1 | 58% | 0% |
| | | | | | | | | | | |

Intersection 11

Innovation Way/11th Avenue

All-way Stop

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 125 | 150 | 3 | 150 | 8 | 150 | 0 | 53% | 0% |
| | Left/Through | 325 | 2,175 | 480 | 3,500 | 810 | 3,650 | 973 | 96% | 0% |
| | Right Turn | 325 | 725 | 201 | 1,325 | 352 | 1,800 | 548 | 0% | 0% |
| NB | Left Turn | 125 | 125 | 15 | 250 | 5 | 175 | 0 | 2% | 0% |
| | Through | 575 | 450 | 5 | 475 | 7 | 475 | 12 | 99% | 55% |
| | Through/Right | 575 | 350 | 3 | 350 | 5 | 375 | 11 | 0% | 90% |
| SB | Left Turn | 175 | 75 | 8 | 125 | 14 | 150 | 24 | 1% | 0% |
| | Through | 1,000 | 25 | 4 | 75 | 9 | 100 | 23 | 0% | 0% |
| | Through/Right | 1,000 | 100 | 16 | 175 | 31 | 200 | 39 | 0% | 0% |
| WB | Left Turn | 325 | 50 | 8 | 75 | 23 | 100 | 60 | 0% | 0% |
| | Through/Right | 325 | 50 | 7 | 75 | 17 | 75 | 20 | 0% | 0% |

Intersection 12

Innovation Way/Juniper Networks Driveway

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left Turn | 200 | 11,550 | 337 | 17,150 | 289 | 15,600 | 8 | 0% | 21% |
| | Right Turn | 200 | 6,000 | 479 | 11,575 | 1,162 | 15,300 | 328 | 0% | 0% |
| NB | Left Turn | 125 | 75 | 13 | 175 | 20 | 175 | 1 | 0% | 0% |
| | Through | 1,000 | 1,125 | 5 | 1,150 | 9 | 1,150 | 16 | 77% | 62% |
| SB | Through | 300 | 225 | 13 | 225 | 24 | 225 | 28 | 0% | 4% |
| | Through/Right | 300 | 200 | 16 | 250 | 17 | 275 | 16 | 0% | 2% |
| | | | | | | | | | | |

Intersection 13

Bordeaux Drive/Innovation Way

Signal

| Direction | Lane Group | Storage (ft) | Average Queue (ft) | | 95th Queue (ft) | | Maximum Queue (ft) | | Block Time | |
|-----------|---------------|--------------|--------------------|-----------|-----------------|-----------|--------------------|-----------|------------|----------|
| | | | Average | Std. Dev. | Average | Std. Dev. | Average | Std. Dev. | Pocket | Upstream |
| EB | Left/Through | 375 | 75 | 6 | 125 | 19 | 200 | 40 | 3% | 0% |
| | Right Turn | 125 | 75 | 6 | 125 | 11 | 125 | 1 | 0% | 0% |
| NB | Left Turn | 325 | 8,775 | 35 | 13,600 | 21 | 11,950 | 8 | 100% | 0% |
| | Through/Right | 2,025 | 1,000 | 1 | 1,000 | 1 | 1,025 | 1 | 1% | 75% |
| SB | Left Turn | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |
| | Through/Right | 725 | 725 | 1 | 725 | 2 | 725 | 3 | 94% | 79% |
| WB | Left/Through | 125 | 75 | 31 | 150 | 84 | 175 | 111 | 10% | 1% |
| | Right Turn | 125 | 25 | 0 | 25 | 0 | 25 | 0 | 0% | 0% |

Arterial Level of Service: NB Mathilda Ave

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|--------------------|------|---------------|-----------------|-----------|----------------|
| Ahwanee Ave | 8 | 167.9 | 178.7 | 0.1 | 3 |
| | 7 | 150.9 | 162.8 | 0.2 | 3 |
| US 101 NB Ramps | 6 | 177.1 | 186.9 | 0.1 | 3 |
| Ross Dr | 5 | 123.4 | 134.8 | 0.1 | 4 |
| | 4 | 65.3 | 73.4 | 0.0 | 2 |
| SR 237 EB Off-Ramp | 43 | 1.2 | 5.6 | 0.0 | 21 |
| Mathilda Ave | 57 | 1.3 | 6.2 | 0.0 | 21 |
| Mathilda Ave | 3 | 42.7 | 46.8 | 0.0 | 3 |
| Innovation Way | 2 | 29.0 | 53.5 | 0.2 | 15 |
| 5th Ave | 1 | 21.1 | 41.2 | 0.2 | 21 |
| | 107 | 3.6 | 25.7 | 0.3 | 38 |
| Total | | 783.6 | 915.5 | 1.5 | 6 |

Arterial Level of Service: SB Mathilda Ave

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|-----------------|------|---------------|-----------------|-----------|----------------|
| 5th Ave | 1 | 179.3 | 199.5 | 0.3 | 5 |
| Innovation Way | 2 | 317.5 | 341.0 | 0.2 | 3 |
| | 3 | 99.4 | 130.3 | 0.2 | 6 |
| Ross Dr | 5 | 9.3 | 16.3 | 0.0 | 11 |
| US 101 NB Ramps | 6 | 44.3 | 55.6 | 0.1 | 10 |
| US 101 SB Ramps | 7 | 15.4 | 26.1 | 0.1 | 19 |
| Almanor Ave | 8 | 36.3 | 48.8 | 0.2 | 11 |
| San Aleso Ave | 201 | 5.5 | 16.9 | 0.1 | 30 |
| Total | | 707.1 | 834.4 | 1.4 | 6 |

Arterial Level of Service: NB Innovation Way

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|------------------|------|---------------|-----------------|-----------|----------------|
| | 910 | 19.6 | 23.8 | 0.0 | 4 |
| | 53 | 61.4 | 65.8 | 0.0 | 2 |
| | 11 | 216.5 | 223.6 | 0.1 | 1 |
| | 200 | 196.9 | 213.1 | 0.2 | 3 |
| Juniper Driveway | 12 | 91.6 | 99.7 | 0.1 | 2 |
| Driveway | 217 | 30.1 | 34.1 | 0.0 | 4 |
| | 902 | 42.6 | 44.7 | 0.0 | 2 |
| Mathilda Ave | 2 | 14.5 | 17.1 | 0.0 | 6 |
| | 16 | 5.3 | 19.3 | 0.1 | 17 |
| Bordeaux Dr | 13 | 28.6 | 40.4 | 0.1 | 7 |
| Total | | 707.2 | 781.6 | 0.6 | 3 |

Arterial Level of Service: SB Innovation Way

| Cross Street | Node | Delay (s/veh) | Travel time (s) | Dist (mi) | Arterial Speed |
|------------------|------|---------------|-----------------|-----------|----------------|
| | 16 | 90.8 | 104.4 | 0.1 | 3 |
| Mathilda Ave | 2 | 191.3 | 202.3 | 0.1 | 2 |
| | 902 | 9.8 | 15.1 | 0.0 | 7 |
| Driveway | 217 | 2.0 | 4.1 | 0.0 | 17 |
| Juniper Driveway | 12 | 73.6 | 78.4 | 0.0 | 2 |
| | 200 | 2.5 | 9.0 | 0.1 | 23 |
| 11th Ave | 11 | 28.7 | 44.6 | 0.2 | 13 |
| | 53 | 3.2 | 10.7 | 0.1 | 24 |
| | 910 | 11.7 | 15.9 | 0.0 | 9 |
| Moffett Park Dr | 10 | 10.5 | 15.2 | 0.0 | 6 |
| Total | | 424.2 | 499.6 | 0.6 | 4 |

APPENDIX P – YEAR 2040 FREQ MAINLINE CALCULATION SHEETS



```

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQQ QQQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQQ QQQ QQQQ 1111 2222 PPP EEE
FFF RRR RRR EEE Q*UC* QQQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*QQ 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP EEEEEEEEE
    
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FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 62
LOWER LIMB (AT V/C=1) = 30
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT TRUCKS | DES TRUCKS | SPECIAL RAMP | FF. SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION LOCATION |
|---------|----------|----------|-------------|--------------|---------|---------|-----------|---------|------------|------------|--------------|-------------------|---------------|----------|----------------|------------------------|
| ** 1 | 3 | 6000. | 500. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Seeding |
| ** 2 | 3 | 6000. | 99999. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture |
| ** 3 | 2 | 4000. | 12000. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** 4 | 3 | 4570. | 350. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Maude On-Ramp |
| ** 5 | 3 | 4570. | 300. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Maude to US-101 |
| ** 6 | 3 | 4570. | 350. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US-101 Off-ramp |
| ** 7 | 2 | 4000. | 940. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | US101SB / US101SB |
| ** 8 | 3 | 5330. | 700. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US101 SB On-ramp |
| ** 9 | 3 | 5330. | 700. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US 101 / Mathilda |
| ** 10 | 3 | 5330. | 700. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-ramp |
| ** 11 | 2 | 4000. | 2300. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda |
| ** 12 | 3 | 5000. | 700. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda On-Ramp |
| ** 13 | 3 | 4470. | 800. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda / Persian HOV |
| ** 14 | 3 | 4470. | 1400. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks Off-Ramp |
| ** 15 | 2 | 4000. | 1400. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | West of Lawrence E |
| ** 16 | 2 | 4000. | 1500. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence Off-ramp |
| ** 17 | 2 | 4000. | 1500. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End of DKS |
| ** 18 | 2 | 4000. | 10000. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** 19 | 3 | 5600. | 750. | 62 | OD | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End of the network |

***** INPUT HAS BEEN COMPLETED *****

**
** FREEWAY TRAVEL TIME (MINUTES) **
**

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | |
|-----------|-------|-----------------------|-------|-------|-------|-------|-------|---|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 18.42 | 20.80 | 21.36 | 22.31 | 22.84 | 23.12 | 25.09 | |
| * 2 * | 0.00 | 0.18 | 0.74 | 1.69 | 2.23 | 2.50 | 4.47 | |
| * 3 * | 0.00 | 0.00 | 0.38 | 1.34 | 1.87 | 2.14 | 4.11 | |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.53 | 1.06 | 1.34 | 3.31 | |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.14 | |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | |
|-----------|----------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|------|------|
| * SEC LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | |
| * 1 | 3 | 500. | 3301. | 0. | 3301. | 3301. | 0. | 3301. | 6000. | 0. | 0. | .55 | 62. | 17.7 | B | 20.3 | 13.0 |
| * 2 | 3 | 99999. | 0. | 825. | 3301. | 0. | 825. | 3301. | 6000. | 0. | 0. | .55 | 62. | 17.7 | B | 20.3 | 13.0 |
| * 3 | 2 | 12000. | 0. | 0. | 2476. | 0. | 0. | 2476. | 4000. | 0. | 0. | .62 | 62. | 20.0 | C | 20.3 | 13.0 |
| * 4 | 3 | 350. | 306. | 0. | 2782. | 306. | 0. | 2782. | 4526. | 0. | 0. | .61 | 62. | 15.0 | B | 20.3 | 13.0 |
| * 5 | 3 | 300. | 0. | 0. | 2782. | 0. | 0. | 2782. | 4570. | 0. | 0. | .61 | 62. | 15.0 | B | 20.3 | 13.0 |
| * 6 | 3 | 350. | 0. | 867. | 2782. | 0. | 867. | 2782. | 4317. | 0. | 0. | .64 | 62. | 15.0 | B | 20.3 | 13.0 |
| * 7 | 2 | 940. | 0. | 0. | 1915. | 0. | 0. | 1915. | 4000. | 0. | 0. | .48 | 62. | 15.4 | B | 20.3 | 13.0 |
| * 8 | 3 | 700. | 1878. | 0. | 3793. | 1608. | 0. | 3523. | 4938. | 0. | 0. | .71 | 62. | 18.9 | C | 20.3 | 13.0 |
| * 9 | 3 | 700. | 0. | 0. | 3793. | 0. | 0. | 3523. | 5330. | 0. | 0. | .66 | 62. | 18.9 | C | 20.3 | 13.0 |
| * 10 | 3 | 700. | 0. | 855. | 3793. | 0. | 789. | 3523. | 5215. | 0. | 0. | .68 | 62. | 18.9 | C | 20.3 | 13.0 |
| * 11 | 2 | 2300. | 0. | 0. | 2938. | 0. | 0. | 2734. | 4000. | 0. | 0. | .68 | 62. | 22.0 | C | 20.3 | 13.0 |
| * 12 | 3 | 700. | 307. | 0. | 3245. | 307. | 0. | 3041. | 4916. | 0. | 0. | .62 | 62. | 16.3 | B | 20.3 | 13.0 |
| * 13 | 3 | 800. | 0. | 0. | 3245. | 0. | 0. | 3041. | 4470. | 0. | 0. | .68 | 62. | 16.3 | B | 20.3 | 13.0 |
| * 14 | 3 | 1400. | 0. | 306. | 3245. | 0. | 285. | 3041. | 4433. | 0. | 0. | .69 | 62. | 16.3 | B | 20.3 | 13.0 |
| * 15 | 2 | 1400. | 0. | 0. | 2939. | 0. | 0. | 2756. | 4000. | 0. | 0. | .69 | 62. | 22.2 | C | 20.3 | 13.0 |
| * 16 | 2 | 1500. | 0. | 196. | 2939. | 0. | 182. | 2756. | 3974. | 0. | 0. | .69 | 62. | 22.2 | C | 20.3 | 13.0 |
| * 17 | 2 | 1500. | 0. | 0. | 2743. | 0. | 0. | 2574. | 4000. | 0. | 0. | .64 | 62. | 20.8 | C | 20.3 | 13.0 |
| * 18 | 2 | 10000. | 0. | 0. | 2743. | 0. | 0. | 2574. | 4000. | 0. | 0. | .64 | 62. | 20.8 | C | 20.3 | 13.0 |
| * 19 | 3 | 750. | 914. | 3657. | 3657. | 914. | 3488. | 3488. | 5600. | 0. | 0. | .62 | 62. | 18.8 | C | 20.3 | 13.0 |

* TOTAL 136889. = 25.9 MILES MAX(V/C) = 0.71 LOWEST LOS = C AVG = 62. 18.3 20.3 13.0

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 1310. VEH-HRS | 1568. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 135. VEH-HRS | 135. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1445. VEH-HRS | 1703. PASS-HRS |
| TOTAL TRAV DISTANCE = | 81203. VEH-MI. | 97189. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 56. MPH | 62. MPH |
| AVERAGE DENSITY = | 18. VPMP | 18. VPMP |
| TOTAL FUEL = | 4041. GALLONS | 4041. GALLONS |
| TOTAL EMISSIONS = | 1079. KI LOGRAMS | 1079. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.23 | 2 | 46.54 | 3 | 4.19 | 4 | 0.14 | 5 | 0.12 |
| 6 | 0.14 | 7 | 0.25 | 8 | 0.35 | 9 | 0.35 | 10 | 0.35 |
| 11 | 0.89 | 12 | 0.30 | 13 | 0.34 | 14 | 0.60 | 15 | 0.54 |
| 16 | 0.58 | 17 | 0.54 | 18 | 3.63 | 19 | 0.37 | | |

***** TOTAL DELAY = 60.4 VEH-HRS ***** AVERAGE DELAY = 1.16 MIN/VEH *****

***** RAMP DELAYS *****

| ON-RAMP | NO. | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|---------|-----|-----------------------|---------------|--------------------------------|----------|---------|---------|----------|----------------------|
| | 3 | RAMP | 270. | 135.00 | 3.57 | 48.68 | 3.01 | 15.74 | 0.83 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 270. | 135.00 | 3.57 | 48.68 | 3.01 | 15.74 | 0.83 |

 **
 ** FREEWAY TRAVEL TIME (MINUTES)
 **

 * ORIGINS DESTINATIONS ACROSS
 * DOWN 1 2 3 4 5 6 7
 *
 *
 *
 *
 * 1 * 18.42 20.88 21.44 22.40 22.95 23.23 25.22
 * 2 * 0.00 0.18 0.74 1.70 2.25 2.53 4.52
 * 3 * 0.00 0.00 0.38 1.35 1.90 2.17 4.16
 * 4 * 0.00 0.00 0.00 0.53 1.08 1.36 3.35
 * 5 * 0.00 0.00 0.00 0.00 0.00 0.00 0.14
 *
 *

 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE
 *
 *
 * SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMISSIONS
 * SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMPM LEVEL MPG GS/VM
 *
 * 1 3 500. 4531. 0. 4531. 4531. 0. 4531. 6000. 0. 0. 0. .76 62. 24.4 C 20.3 13.0
 * 2 3 99999. 0. 1133. 4531. 0. 1133. 4531. 6000. 0. 0. 0. .76 62. 24.4 C 20.3 13.0
 * 3 2 12000. 0. 0. 3398. 0. 0. 3398. 4000. 0. 0. 0. .85 60. 28.4 D 21.4 12.3
 * 4 3 350. 498. 0. 3896. 498. 0. 3896. 4499. 0. 0. 0. .87 62. 20.9 C 20.3 13.0
 * 5 3 300. 0. 0. 3896. 0. 0. 3896. 4570. 0. 0. 0. .85 62. 20.9 C 20.3 13.0
 * 6 3 350. 0. 1221. 3896. 0. 1221. 3896. 4221. 0. 0. 0. .92 62. 20.9 C 20.3 13.0
 * 7 2 940. 0. 0. 2675. 0. 0. 2675. 4000. 0. 0. 0. .67 62. 21.6 C 20.3 13.0
 * 8 3 700. 2053. 0. 4728. 1579. 0. 4254. 4910. 0. 0. 0. .87 62. 22.9 C 20.3 13.0
 * 9 3 700. 0. 0. 4728. 0. 0. 4254. 5330. 0. 0. 0. .80 62. 22.9 C 20.3 13.0
 * 10 3 700. 0. 1116. 4728. 0. 991. 4254. 5163. 0. 0. 0. .82 62. 22.9 C 20.3 13.0
 * 11 2 2300. 0. 0. 3612. 0. 0. 3263. 4000. 0. 0. 0. .82 61. 26.9 D 21.0 12.6
 * 12 3 700. 417. 0. 4029. 417. 0. 3680. 4885. 0. 0. 0. .75 62. 19.8 C 20.3 13.0
 * 13 3 800. 0. 0. 4029. 0. 0. 3680. 4470. 0. 0. 0. .82 62. 19.8 C 20.3 13.0
 * 14 3 1400. 0. 367. 4029. 0. 332. 3680. 4421. 0. 0. 0. .83 62. 19.8 C 20.3 13.0
 * 15 2 1400. 0. 0. 3662. 0. 0. 3348. 4000. 0. 0. 0. .84 60. 27.8 D 21.3 12.4
 * 16 2 1500. 0. 254. 3662. 0. 229. 3348. 3962. 0. 0. 0. .84 60. 27.9 D 21.4 12.4
 * 17 2 1500. 0. 0. 3408. 0. 0. 3119. 4000. 0. 0. 0. .78 61. 25.4 C 20.7 12.8
 * 18 2 10000. 0. 0. 3408. 0. 0. 3119. 4000. 0. 0. 0. .78 61. 25.4 C 20.7 12.8
 * 19 3 750. 1136. 4544. 4544. 1136. 4255. 4255. 5600. 0. 0. 0. .76 62. 22.9 C 20.3 13.0
 *
 *
 * TOTAL 136889. = 25.9 MI LBS MAX(V/C) = 0.92 LOWEST LOS = D AVG = 62. 24.8 20.5 13.0
 *

SR-237_EB_AM_NP_2040_PE

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|----------------------------|--------------------|------------------|-------------------|------------------|
| FREEWAY TRAVEL TIME = | 1774. VEH-HRS | 2127. PASS-HRS | 3084. VEH-HRS | 3695. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 507. VEH-HRS | 507. PASS-HRS | 642. VEH-HRS | 642. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 2281. VEH-HRS | 2634. PASS-HRS | 3726. VEH-HRS | 4337. PASS-HRS |
| TOTAL TRAV DISTANCE = | 109549. VEH-MI. | 131450. PASS-MI. | 190753. VEH-MI. | 228639. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 48. MPH. | | 62. MPH. | |
| AVERAGE DENSITY = | 25. VPMP | | 22. VPMP | |
| TOTAL FUEL = | 5537. GALLONS | | 9578. GALLONS | |
| TOTAL EMISSIONS = | 1494. KI LOGRAMS | | 2573. KI LOGRAMS | |

1 INSTITUTE OF TRANSPORTATION STUDIES
 UNIVERSITY OF CALIFORNIA, BERKELEY

FREQ12PE REL 3.01
 SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 2

3/30/2016 16: 4 PAGE 9

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.32 | 2 | 63.88 | 3 | 10.40 | 4 | 0.19 | 5 | 0.16 |
| 6 | 0.19 | 7 | 0.35 | 8 | 0.42 | 9 | 0.42 | 10 | 0.42 |
| 11 | 1.56 | 12 | 0.36 | 13 | 0.42 | 14 | 0.73 | 15 | 1.10 |
| 16 | 1.24 | 17 | 0.81 | 18 | 5.41 | 19 | 0.45 | | |

***** TOTAL DELAY = 88.8 VEH-HRS ***** AVERAGE DELAY = 1.29 MIN/VEH *****

***** RAMP DELAYS *****

| ON-RAMP | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|---------|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|
| 3 | RAMP | 744. | 507.00 | 11.09 | 182.82 | 11.30 | 59.12 | 73.56 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 744. | 507.00 | 11.09 | 182.82 | 11.30 | 59.12 | 73.56 |

```

FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ      1111      222222  Pppppppp LLL
FFFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111  222 222 Pppppppp LLL
FFF       RRR   RRR EEE       QQQQQ   QQQQQ   1111   222 222 Ppp   Ppp LLL
FFF       RRR   RRR EEE       QQQQ    QQQQ    1111   222 222 Ppp   Ppp LLL
FFFFFFFFF RRRRRRRR EEEEEEE   QQQQ    QQQQ    1111           222 Pppppppp LLL
FFFFFFFFF RRRRRRRR EEEEEEE   QQQQ    QQQQ    1111           2222 Pppppppp LLL
FFF       RRR   RRR EEE       QQQQ    QQQ QQQ  1111           2222 Ppp   LLL
FFF       RRR   RRR EEE       Q*UC*   QQQQQ   1111   222    Ppp   LLL
FFF       RRR   RRR EEEEEEEEE Q*REGENTS*Q 1111   222    Ppp   LLLLLLLLLL
FFF       RRR   RRR EEEEEEEEE Q*1988*Q QQQ 11111111 2222222222 Ppp   LLLLLLLLLL
    
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FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 3 AND 18 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 62
LOWER LIMB (AT V/C=1) = 30
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

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*****
**
**                                     FREeway AND ARTERIAL DESIGN FEATURES
**
*****
**
** SUB NO.   SSEC   SSEC   DESIG N   ORG   TRK   SSEC PCT   PCT DES   SPECIAL   FF SPD.   CAP.   ART   GRADE   SUBSECTI ON LOCATI ON
** SEC LNS   CAP     LENGTH SPEED   DES   FAC   GRAD TRK  TRUCKS   RAMP     ALT. RTE  ALT. RTE TYPE ALT. RTE
**
** 1
** 2
** 3  1  1650.  12000.  62    0   0.95  0.0 0   100    NO     0.0     0.   GOOD  0.0  HOV Dummy
** 4  1  1650.   350.  62    0   0.95  0.0 0   100    YES    0.0     0.   GOOD  0.0  Maude On-Ramp
** 5  1  1650.   300.  62     0.95  0.0 0   100    YES    0.0     0.   GOOD  0.0  Maude to US-101
** 6  1  1650.   350.  62    D   0.95  0.0 0   100    YES    0.0     0.   GOOD  0.0  US-101 Off-ramp
** 7  1  1650.   940.  62     0.95  0.0 0   100    NO     0.0     0.   GOOD  0.0  US101SB / US101SB
** 8  1  1650.   700.  62    0   0.95  0.0 0   100    YES    0.0     0.   GOOD  0.0  US101 SB On-ramp
** 9  1  1650.   700.  62     0.95  0.0 0   100    YES    0.0     0.   GOOD  0.0  US 101 / Mathilda
** 10 1  1650.   700.  62    D   0.95  0.0 0   100    YES    0.0     0.   GOOD  0.0  Mathilda Off-ramp
** 11 1  1650.  2300.  62     0.95  0.0 0   100    NO     0.0     0.   GOOD  0.0  Mathilda / Mathilda
** 12 1  1650.   700.  62    0   0.95  0.0 0   100    YES    0.0     0.   GOOD  0.0  Mathilda On-Ramp
** 13 1  1650.   800.  62     0.95  0.0 0   100    YES    0.0     0.   GOOD  0.0  Mathilda / Persian HOV
** 14 1  1650.  1400.  62    D   0.95  0.0 0   100    NO     0.0     0.   GOOD  0.0  Fair Oaks Off-Ramp
** 15 1  1650.  1400.  62     0.95  0.0 0   100    NO     0.0     0.   GOOD  0.0  West of Lawrence E
** 16 1  1650.  1500.  62    D   0.95  0.0 0   100    NO     0.0     0.   GOOD  0.0  Lawrence Off-ramp
** 17 1  1650.  1500.  62    D   0.95  0.0 0   100    NO     0.0     0.   GOOD  0.0  End of DKS
** 18 1  1650. 10000.  62    D   0.95  0.0 0   100    NO     0.0     0.   GOOD  0.0  HOV Dummy
    
```

** 19 **

 ** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|--|-----------------------|------|------|------|------|------|------|------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | | 0.00 | 2.38 | 2.94 | 3.89 | 4.42 | 4.70 | 6.53 | 0.00 |
| * 3 * | | 0.00 | 0.00 | 0.00 | 0.00 | 2.23 | 2.50 | 4.33 | 0.00 |
| * 4 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.14 | 3.98 | 0.00 |
| * 5 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.17 | 0.00 |
| * 6 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | | |
|-----------|----------|------------|-----------|------------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|------|---|------|------|
| * SEC LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * SSEC | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | | | |
| * 1 | | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | | |
| * 3 | 1 | 12000. | 825. | 0. | 825. | 825. | 0. | 825. | 1650. | 0. | 0. | 0. | .50 | 62. | 13.3 | B | 21.6 | 12.8 |
| * 4 | 1 | 350. | 45. | 0. | 870. | 45. | 0. | 870. | 1650. | 0. | 0. | 0. | .53 | 62. | 14.0 | B | 21.6 | 12.8 |
| * 5 | 1 | 300. | 0. | 0. | 870. | 0. | 0. | 870. | 1650. | 0. | 0. | 0. | .53 | 62. | 14.0 | B | 21.6 | 12.8 |
| * 6 | 1 | 350. | 0. | 253. | 870. | 0. | 253. | 870. | 1650. | 0. | 0. | 0. | .53 | 62. | 14.0 | B | 21.6 | 12.8 |
| * 7 | 1 | 940. | 0. | 0. | 616. | 0. | 0. | 616. | 1650. | 0. | 0. | 0. | .37 | 62. | 9.9 | A | 21.6 | 12.8 |
| * 8 | 1 | 700. | 392. | 0. | 1009. | 392. | 0. | 1009. | 1650. | 0. | 0. | 0. | .61 | 62. | 16.3 | B | 21.6 | 12.8 |
| * 9 | 1 | 700. | 0. | 0. | 1009. | 0. | 0. | 1009. | 1650. | 0. | 0. | 0. | .61 | 62. | 16.3 | B | 21.6 | 12.8 |
| * 10 | 1 | 700. | 0. | 116. | 1009. | 0. | 116. | 1009. | 1650. | 0. | 0. | 0. | .61 | 62. | 16.3 | B | 21.6 | 12.8 |
| * 11 | 1 | 2300. | 0. | 0. | 893. | 0. | 0. | 893. | 1650. | 0. | 0. | 0. | .54 | 62. | 14.4 | B | 21.6 | 12.8 |
| * 12 | 1 | 700. | 85. | 0. | 978. | 85. | 0. | 978. | 1650. | 0. | 0. | 0. | .59 | 62. | 15.8 | B | 21.6 | 12.8 |
| * 13 | 1 | 800. | 0. | 0. | 978. | 0. | 0. | 978. | 1650. | 0. | 0. | 0. | .59 | 62. | 15.8 | B | 21.6 | 12.8 |
| * 14 | 1 | 1400. | 0. | 37. | 978. | 0. | 37. | 978. | 1650. | 0. | 0. | 0. | .59 | 62. | 15.8 | B | 21.6 | 12.8 |
| * 15 | 1 | 1400. | 0. | 0. | 941. | 0. | 0. | 941. | 1650. | 0. | 0. | 0. | .57 | 62. | 15.2 | B | 21.6 | 12.8 |
| * 16 | 1 | 1500. | 0. | 27. | 941. | 0. | 27. | 941. | 1650. | 0. | 0. | 0. | .57 | 62. | 15.2 | B | 21.6 | 12.8 |
| * 17 | 1 | 1500. | 0. | 0. | 914. | 0. | 0. | 914. | 1650. | 0. | 0. | 0. | .55 | 62. | 14.7 | B | 21.6 | 12.8 |
| * 18 | 1 | 10000. | 0. | 914. | 914. | 0. | 914. | 914. | 1650. | 0. | 0. | 0. | .55 | 62. | 14.7 | B | 21.6 | 12.8 |
| * 19 | | | | | | | | | | | | | | | | | | |
| * TOTAL | | 35640. | = | 6.8 | MILES | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 97. VEH-HRS | 193. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 97. VEH-HRS | 193. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 5984. VEH-MI. | 11967. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | |
| AVERAGE DENSITY = | 14. VPMP | |
| TOTAL FUEL = | 278. GALLONS | |
| TOTAL EMISSIONS = | 76. KILOGRAMS | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 1.40 | 4 | 0.04 | 5 | 0.04 |
| 6 | 0.04 | 7 | 0.08 | 8 | 0.10 | 9 | 0.10 | 10 | 0.10 |
| 11 | 0.29 | 12 | 0.10 | 13 | 0.11 | 14 | 0.19 | 15 | 0.19 |
| 16 | 0.20 | 17 | 0.19 | 18 | 1.29 | 19 | 0.00 | | |

***** TOTAL DELAY = 4.5 VEH-HRS ***** AVERAGE DELAY = 0.30 MIN/VEH *****

 ** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|------|-----------------------|------|------|------|------|------|------|------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 2.38 | 2.94 | 3.89 | 4.42 | 4.70 | 6.53 | 0.00 | |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 2.23 | 2.50 | 4.33 | 0.00 | |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.14 | 3.98 | 0.00 | |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.17 | 0.00 | |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|-----------|--------|------------|----------------|--------------------|--------|---------|-----------------|----------------|-----------|---------|-----------|---------|--------|-------------|
| * SEC | * LNS | * LENGTH | * ORG DES SSEC | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 1 | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | |
| * 3 | 1 | 12000. | 1133. 0. 1133. | 1133. 0. 1133. | 1650. | 0. | 0. | 0. | .69 | 62. | 18.3 | C | 21.6 | 12.8 |
| * 4 | 1 | 350. | 71. 0. 1204. | 71. 0. 1204. | 1650. | 0. | 0. | 0. | .73 | 62. | 19.4 | C | 21.6 | 12.8 |
| * 5 | 1 | 300. | 0. 0. 1204. | 0. 0. 1204. | 1650. | 0. | 0. | 0. | .73 | 62. | 19.4 | C | 21.6 | 12.8 |
| * 6 | 1 | 350. | 0. 349. 1204. | 0. 349. 1204. | 1650. | 0. | 0. | 0. | .73 | 62. | 19.4 | C | 21.6 | 12.8 |
| * 7 | 1 | 940. | 0. 0. 855. | 0. 0. 855. | 1650. | 0. | 0. | 0. | .52 | 62. | 13.8 | B | 21.6 | 12.8 |
| * 8 | 1 | 700. | 421. 0. 1276. | 421. 0. 1276. | 1650. | 0. | 0. | 0. | .77 | 62. | 20.6 | C | 21.6 | 12.8 |
| * 9 | 1 | 700. | 0. 0. 1276. | 0. 0. 1276. | 1650. | 0. | 0. | 0. | .77 | 62. | 20.6 | C | 21.6 | 12.8 |
| * 10 | 1 | 700. | 0. 168. 1276. | 0. 168. 1276. | 1650. | 0. | 0. | 0. | .77 | 62. | 20.6 | C | 21.6 | 12.8 |
| * 11 | 1 | 2300. | 0. 0. 1108. | 0. 0. 1108. | 1650. | 0. | 0. | 0. | .67 | 62. | 17.9 | B | 21.6 | 12.8 |
| * 12 | 1 | 700. | 115. 0. 1223. | 115. 0. 1223. | 1650. | 0. | 0. | 0. | .74 | 62. | 19.7 | C | 21.6 | 12.8 |
| * 13 | 1 | 800. | 0. 0. 1223. | 0. 0. 1223. | 1650. | 0. | 0. | 0. | .74 | 62. | 19.7 | C | 21.6 | 12.8 |
| * 14 | 1 | 1400. | 0. 49. 1223. | 0. 49. 1223. | 1650. | 0. | 0. | 0. | .74 | 62. | 19.7 | C | 21.6 | 12.8 |
| * 15 | 1 | 1400. | 0. 0. 1174. | 0. 0. 1174. | 1650. | 0. | 0. | 0. | .71 | 62. | 18.9 | C | 21.6 | 12.8 |
| * 16 | 1 | 1500. | 0. 39. 1174. | 0. 39. 1174. | 1650. | 0. | 0. | 0. | .71 | 62. | 18.9 | C | 21.6 | 12.8 |
| * 17 | 1 | 1500. | 0. 0. 1136. | 0. 0. 1136. | 1650. | 0. | 0. | 0. | .69 | 62. | 18.3 | C | 21.6 | 12.8 |
| * 18 | 1 | 10000. | 0. 1136. 1136. | 0. 1136. 1136. | 1650. | 0. | 0. | 0. | .69 | 62. | 18.3 | C | 21.6 | 12.8 |
| * 19 | | | | | | | | | | | | | | |
| * TOTAL | | 35640. = | 6.8 MILES | | | | MAX(V/C) = 0.77 | LOWEST LOS = C | AVG = 62. | 18.5 | | | 21.6 | 12.8 |

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|-----------------------------|--------------------|-----------------|-------------------|-----------------|
| FREWAY TRAVEL TIME = | 125. VEH-HRS | 249. PASS-HRS | 221. VEH-HRS | 443. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 125. VEH-HRS | 249. PASS-HRS | 221. VEH-HRS | 443. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 7734. VEH-MI. | 15469. PASS-MI. | 13718. VEH-MI. | 27436. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | | 62. MPH. | |
| AVERAGE DENSITY = | 18. VPMP | | 16. VPMP | |
| TOTAL FUEL = | 359. GALLONS | | 637. GALLONS | |

TOTAL EMISSIONS = 99. KILOGRAMS

SR-237_EB_AM_NP_2040_PL
175. KILOGRAMS

1 INSTITUTE OF TRANSPORTATION STUDIES
UNIVERSITY OF CALIFORNIA, BERKELEY

FREQ12PL REL 3.01
SHORT TERM SIMULATION OF PRIORITY LANE
TIME SLICE 2 OF 2

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***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 1.92 | 4 | 0.06 | 5 | 0.05 |
| 6 | 0.06 | 7 | 0.11 | 8 | 0.13 | 9 | 0.13 | 10 | 0.13 |
| 11 | 0.36 | 12 | 0.12 | 13 | 0.14 | 14 | 0.24 | 15 | 0.23 |
| 16 | 0.25 | 17 | 0.24 | 18 | 1.60 | 19 | 0.00 | | |

***** TOTAL DELAY = 5.8 VEH-HRS ***** AVERAGE DELAY = 0.30 MIN/VEH *****

```

FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQQ QQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP EEEEEEEEE
    
```

FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 62
LOWER LIMB (AT V/C=1) = 30
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT TRUCKS | DES TRUCKS | SPECIAL RAMP | FF. SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION LOCATION |
|---------|----------|----------|-------------|--------------|---------|---------|-----------|---------|------------|------------|--------------|-------------------|---------------|----------|----------------|------------------------|
| ** 1 | 3 | 6000. | 500. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Seeding |
| ** 2 | 3 | 6000. | 99999. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture |
| ** 3 | 2 | 4000. | 12000. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** 4 | 3 | 4570. | 350. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Maude On-Ramp |
| ** 5 | 3 | 4570. | 300. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Maude to US-101 |
| ** 6 | 3 | 4570. | 350. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US-101 Off-ramp |
| ** 7 | 2 | 4000. | 940. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | US101SB / US101SB |
| ** 8 | 3 | 4930. | 700. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US101 SB On-ramp |
| ** 9 | 3 | 4930. | 700. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US 101 / Mathilda |
| ** 10 | 3 | 4930. | 700. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-ramp |
| ** 11 | 2 | 4000. | 2300. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda |
| ** 12 | 3 | 4470. | 700. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda On-Ramp |
| ** 13 | 3 | 4470. | 800. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda / Persian HOV |
| ** 14 | 3 | 4470. | 1400. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks Off-Ramp |
| ** 15 | 2 | 4000. | 1400. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | West of Lawrence E |
| ** 16 | 2 | 4000. | 1500. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence Off-ramp |
| ** 17 | 2 | 4000. | 1500. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End of DKS |
| ** 18 | 2 | 4000. | 10000. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** 19 | 3 | 5600. | 750. | 62 | OD | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End of the network |

***** INPUT HAS BEEN COMPLETED *****

**
** FREeway TRAVEL TIME (MINUTES) **
**

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | |
|-----------|-------|-----------------------|-------|-------|-------|-------|-------|---|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 18.42 | 20.80 | 21.36 | 22.31 | 22.84 | 23.12 | 25.09 | |
| * 2 * | 0.00 | 0.18 | 0.74 | 1.69 | 2.23 | 2.50 | 4.47 | |
| * 3 * | 0.00 | 0.00 | 0.38 | 1.34 | 1.87 | 2.14 | 4.11 | |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.53 | 1.06 | 1.34 | 3.31 | |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.14 | |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|-----------|---------|------------|------------------|------------------|---------------|----------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|
| * SEC | * LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * SSEC | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 1 | 3 | 500. | 3301. | 0. 3301. | 3301. | 0. 3301. | 6000. | 0. | 0. | .55 | 62. | 17.7 | B | 20.3 | 13.0 |
| * 2 | 3 | 99999. | 0. 825. 3301. | 0. 825. 3301. | 0. 825. 3301. | 6000. | 0. | 0. | 0. | .55 | 62. | 17.7 | B | 20.3 | 13.0 |
| * 3 | 2 | 12000. | 0. 0. 2476. | 0. 0. 2476. | 0. 0. 2476. | 4000. | 0. | 0. | 0. | .62 | 62. | 20.0 | C | 20.3 | 13.0 |
| * 4 | 3 | 350. | 303. 0. 2779. | 303. 0. 2779. | 4523. | 0. | 0. | 0. | 0. | .61 | 62. | 14.9 | B | 20.3 | 13.0 |
| * 5 | 3 | 300. | 0. 0. 2779. | 0. 0. 2779. | 4570. | 0. | 0. | 0. | 0. | .61 | 62. | 14.9 | B | 20.3 | 13.0 |
| * 6 | 3 | 350. | 0. 867. 2779. | 0. 867. 2779. | 4317. | 0. | 0. | 0. | 0. | .64 | 62. | 14.9 | B | 20.3 | 13.0 |
| * 7 | 2 | 940. | 0. 0. 1912. | 0. 0. 1912. | 4000. | 0. | 0. | 0. | 0. | .48 | 62. | 15.4 | B | 20.3 | 13.0 |
| * 8 | 3 | 700. | 1618. 0. 3530. | 1618. 0. 3530. | 4567. | 0. | 0. | 0. | 0. | .77 | 62. | 19.0 | C | 20.3 | 13.0 |
| * 9 | 3 | 700. | 0. 0. 3530. | 0. 0. 3530. | 4930. | 0. | 0. | 0. | 0. | .72 | 62. | 19.0 | C | 20.3 | 13.0 |
| * 10 | 3 | 700. | 0. 595. 3530. | 0. 595. 3530. | 4844. | 0. | 0. | 0. | 0. | .73 | 62. | 19.0 | C | 20.3 | 13.0 |
| * 11 | 2 | 2300. | 0. 0. 2935. | 0. 0. 2935. | 4000. | 0. | 0. | 0. | 0. | .73 | 62. | 23.7 | C | 20.3 | 13.0 |
| * 12 | 3 | 700. | 455. 0. 3390. | 455. 0. 3390. | 4345. | 0. | 0. | 0. | 0. | .78 | 62. | 18.2 | C | 20.3 | 13.0 |
| * 13 | 3 | 800. | 0. 0. 3390. | 0. 0. 3390. | 4470. | 0. | 0. | 0. | 0. | .76 | 62. | 18.2 | C | 20.3 | 13.0 |
| * 14 | 3 | 1400. | 0. 324. 3390. | 0. 324. 3390. | 4430. | 0. | 0. | 0. | 0. | .77 | 62. | 18.2 | C | 20.3 | 13.0 |
| * 15 | 2 | 1400. | 0. 0. 3066. | 0. 0. 3066. | 4000. | 0. | 0. | 0. | 0. | .77 | 62. | 24.7 | C | 20.3 | 13.0 |
| * 16 | 2 | 1500. | 0. 207. 3066. | 0. 207. 3066. | 3971. | 0. | 0. | 0. | 0. | .77 | 62. | 24.7 | C | 20.3 | 13.0 |
| * 17 | 2 | 1500. | 0. 0. 2859. | 0. 0. 2859. | 4000. | 0. | 0. | 0. | 0. | .71 | 62. | 23.1 | C | 20.3 | 13.0 |
| * 18 | 2 | 10000. | 0. 0. 2859. | 0. 0. 2859. | 4000. | 0. | 0. | 0. | 0. | .71 | 62. | 23.1 | C | 20.3 | 13.0 |
| * 19 | 3 | 750. | 953. 3812. 3812. | 953. 3812. 3812. | 5600. | 0. | 0. | 0. | 0. | .68 | 62. | 20.5 | C | 20.3 | 13.0 |
| * TOTAL | 136889. | = | 25.9 MILES | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 1328. VEH-HRS | 1586. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1328. VEH-HRS | 1586. PASS-HRS |
| TOTAL TRAV DISTANCE = | 82322. VEH-MI. | 98322. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 62. MPH. |
| AVERAGE DENSITY = | 19. VPMP | 19. VPMP |
| TOTAL FUEL = | 4047. GALLONS | 4047. GALLONS |
| TOTAL EMISSIONS = | 1074. KI LOGRAMS | 1074. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.23 | 2 | 46.54 | 3 | 4.19 | 4 | 0.14 | 5 | 0.12 |
| 6 | 0.14 | 7 | 0.25 | 8 | 0.35 | 9 | 0.35 | 10 | 0.35 |
| 11 | 0.95 | 12 | 0.33 | 13 | 0.38 | 14 | 0.67 | 15 | 0.61 |
| 16 | 0.65 | 17 | 0.60 | 18 | 4.03 | 19 | 0.40 | | |

***** TOTAL DELAY = 61.3 VEH-HRS ***** AVERAGE DELAY = 1.16 MIN/VEH *****

**
** FREEWAY TRAVEL TIME (MINUTES)
**

| * ORIGINS | * DESTINATIONS ACROSS | | | | | | |
|-----------|-----------------------|-------|-------|-------|-------|-------|-------|
| * DOWN | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 18.42 | 20.88 | 21.44 | 22.41 | 22.99 | 23.28 | 25.31 |
| * 2 * | 0.00 | 0.18 | 0.74 | 1.71 | 2.29 | 2.58 | 4.61 |
| * 3 * | 0.00 | 0.00 | 0.38 | 1.36 | 1.94 | 2.22 | 4.26 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.53 | 1.11 | 1.40 | 3.43 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.14 |

*
* TIME SLICE FREEWAY PERFORMANCE TABLE
*

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|-----------|----------|-------------------|-------------------|--------------------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|
| * SEC LNS | * LENGTH | * ORG DES SSEC | * ORG DES SSEC | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 1 3 | 500. | 4531. 0. 4531. | 4531. 0. 4531. | 4531. 0. 4531. | 6000. | 0. | 0. | 0. | .76 | 62. | 24.4 | C | 20.3 | 13.0 |
| * 2 3 | 99999. | 0. 1133. 4531. | 0. 1133. 4531. | 0. 1133. 4531. | 6000. | 0. | 0. | 0. | .76 | 62. | 24.4 | C | 20.3 | 13.0 |
| * 3 2 | 12000. | 0. 0. 3398. | 0. 0. 3398. | 0. 0. 3398. | 4000. | 0. | 0. | 0. | .85 | 60. | 28.4 | D | 21.4 | 12.3 |
| * 4 3 | 350. | 495. 0. 3893. | 432. 0. 3830. | 4495. 0. 3830. | 4495. | 0. | 0. | 0. | .85 | 62. | 20.6 | C | 20.3 | 13.0 |
| * 5 3 | 300. | 0. 0. 3893. | 0. 0. 3830. | 4570. 0. 3830. | 4570. | 0. | 0. | 0. | .84 | 62. | 20.6 | C | 20.3 | 13.0 |
| * 6 3 | 350. | 0. 1252. 3893. | 0. 1229. 3830. | 4213. 0. 3830. | 4213. | 0. | 0. | 0. | .91 | 62. | 20.6 | C | 20.3 | 13.0 |
| * 7 2 | 940. | 0. 0. 2641. | 0. 0. 2601. | 4000. 0. 2601. | 4000. | 0. | 0. | 0. | .65 | 62. | 21.0 | C | 20.3 | 13.0 |
| * 8 3 | 700. | 1910. 0. 4551. | 1581. 0. 4182. | 4511. 0. 4182. | 4930. | 0. | 0. | 0. | .93 | 62. | 22.5 | C | 20.3 | 13.0 |
| * 9 3 | 700. | 0. 0. 4551. | 0. 0. 4182. | 4930. 0. 4182. | 4930. | 0. | 0. | 0. | .85 | 62. | 22.5 | C | 20.3 | 13.0 |
| * 10 3 | 700. | 0. 818. 4551. | 0. 745. 4182. | 4804. 0. 4182. | 4804. | 0. | 0. | 0. | .87 | 62. | 22.5 | C | 20.3 | 13.0 |
| * 11 2 | 2300. | 0. 0. 3733. | 0. 0. 3437. | 4000. 0. 3437. | 4000. | 0. | 0. | 0. | .86 | 59. | 28.9 | D | 21.5 | 12.3 |
| * 12 3 | 700. | 624. 0. 4357. | 598. 0. 4035. | 4299. 0. 4035. | 4299. | 0. | 0. | 0. | .94 | 62. | 21.7 | C | 20.3 | 13.0 |
| * 13 3 | 800. | 0. 0. 4357. | 0. 0. 4035. | 4470. 0. 4035. | 4470. | 0. | 0. | 0. | .90 | 62. | 21.7 | C | 20.3 | 13.0 |
| * 14 3 | 1400. | 0. 415. 4357. | 0. 381. 4035. | 4416. 0. 4035. | 4416. | 0. | 0. | 0. | .91 | 62. | 21.7 | C | 20.3 | 13.0 |
| * 15 2 | 1400. | 0. 0. 3942. | 0. 0. 3654. | 4000. 0. 3654. | 4000. | 0. | 0. | 0. | .91 | 57. | 32.0 | D | 22.2 | 11.8 |
| * 16 2 | 1500. | 0. 286. 3942. | 0. 263. 3654. | 3958. 0. 3654. | 3958. | 0. | 0. | 0. | .92 | 57. | 32.2 | D | 22.3 | 11.7 |
| * 17 2 | 1500. | 0. 0. 3656. | 0. 0. 3391. | 4000. 0. 3391. | 4000. | 0. | 0. | 0. | .85 | 60. | 28.3 | D | 21.4 | 12.3 |
| * 18 2 | 10000. | 0. 0. 3656. | 0. 0. 3391. | 4000. 0. 3391. | 4000. | 0. | 0. | 0. | .85 | 60. | 28.3 | D | 21.4 | 12.3 |
| * 19 3 | 750. | 1219. 4875. 4875. | 1219. 4610. 4610. | 5600. 0. 4610. | 5600. | 0. | 0. | 0. | .82 | 62. | 24.8 | C | 20.3 | 13.0 |

*
* TOTAL 136889. = 25.9 MILES MAX(V/C) = 0.94 LOWEST LOS = D AVG = 62. 25.2 20.5 12.9
*

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|----------------------------|--------------------|------------------|-------------------|------------------|
| FREWAY TRAVEL TIME = | 1796. VEH-HRS | 2150. PASS-HRS | 3124. VEH-HRS | 3736. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 209. VEH-HRS | 209. PASS-HRS | 209. VEH-HRS | 209. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 2005. VEH-HRS | 2359. PASS-HRS | 3333. VEH-HRS | 3945. PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 110578. VEH-MI. | 132491. PASS-MI. | 192900. VEH-MI. | 230812. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 55. MPH. | | 62. MPH. | |

AVERAGE DENSITY = 25. VPML
 TOTAL FUEL = 5461. GALLONS
 TOTAL EMISSIONS = 1459. KILOGRAMS

SR-237_EB_AM_P1_2040_PE
 22. VPML
 9508. GALLONS
 2533. KILOGRAMS

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***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.32 | 2 | 63.88 | 3 | 10.40 | 4 | 0.19 | 5 | 0.16 |
| 6 | 0.19 | 7 | 0.34 | 8 | 0.41 | 9 | 0.41 | 10 | 0.41 |
| 11 | 2.15 | 12 | 0.40 | 13 | 0.46 | 14 | 0.80 | 15 | 2.04 |
| 16 | 2.34 | 17 | 1.28 | 18 | 8.55 | 19 | 0.49 | | |

***** TOTAL DELAY = 95.2 VEH-HRS ***** AVERAGE DELAY = 1.38 MIN/VEH *****

***** RAMP DELAYS *****

| ON-RAMP | | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-----------|---------|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|
| ON-RAMP 2 | RAMP | 63. | 31.43 | 3.81 | 11.33 | 0.70 | 3.66 | 0.19 | 4.56 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 63. | 31.43 | 3.81 | 11.33 | 0.70 | 3.66 | 0.19 | 4.56 |
| ON-RAMP 3 | RAMP | 329. | 164.50 | 4.24 | 59.32 | 3.67 | 19.18 | 1.02 | 23.87 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 329. | 164.50 | 4.24 | 59.32 | 3.67 | 19.18 | 1.02 | 23.87 |
| ON-RAMP 4 | RAMP | 26. | 13.00 | 1.25 | 4.69 | 0.29 | 1.52 | 0.08 | 1.89 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 26. | 13.00 | 1.25 | 4.69 | 0.29 | 1.52 | 0.08 | 1.89 |

```

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ      1111      222222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP LLL
FFF      RRR      RRR EEE      QQQQQ QQQQ      1111      222 222 PPP PPP LLL
FFF      RRR      RRR EEE      QQQQ QQQQ      1111      222 222 PPP PPP LLL
FFFFFFFF RRRRRRRR EEEEEEEE QQQQ QQQQ      1111      222 222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEEE QQQQ QQQQ      1111      2222 PPPPPPPP LLL
FFF      RRR RRR EEE      QQQQ QQQ QQQQ      1111      2222 PPP LLL
FFF      RRR RRR EEE      Q*UC* QQQQQ      1111      222 PPP LLL
FFF      RRR RRR EEEEEEEEE Q*REGENTS*QQ      1111      222 PPP LLLLLLLLLL
FFF      RRR RRR EEEEEEEEE Q*1988*Q QQQ 1111111 2222222222 PPP LLLLLLLLLL
    
```

FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 3 AND 18 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 62
LOWER LIMB (AT V/C=1) = 30
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

```

*****
**
**
** FREeway AND ARTERIAL DESIGN FEATURES
**
*****
**
** SUB NO. SSEC SSEC DESIG N ORG TRK SSEC PCT PCT DES SPECIAL FF. SPD. CAP. ART GRADE SUBSECTI ON LOCATI ON
** SEC LNS CAP LENGTH SPEED DES FAC GRAD TRK TRUCKS RAMP ALT. RTE ALT. RTE TYPE ALT. RTE
**
** 1
** 2
** 3 1 1650. 12000. 62 0 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 HOV Dummy
** 4 1 1650. 350. 62 0 0.95 0.0 0 100 YES 0.0 0. GOOD 0.0 Maude On-Ramp
** 5 1 1650. 300. 62 0.95 0.0 0 100 YES 0.0 0. GOOD 0.0 Maude to US-101
** 6 1 1650. 350. 62 D 0.95 0.0 0 100 YES 0.0 0. GOOD 0.0 US-101 Off-ramp
** 7 1 1650. 940. 62 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 US101SB / US101SB
** 8 1 1650. 700. 62 0 0.95 0.0 0 100 YES 0.0 0. GOOD 0.0 US101 SB On-ramp
** 9 1 1650. 700. 62 0.95 0.0 0 100 YES 0.0 0. GOOD 0.0 US 101 / Mathilda
** 10 1 1650. 700. 62 D 0.95 0.0 0 100 YES 0.0 0. GOOD 0.0 Mathilda Off-ramp
** 11 1 1650. 2300. 62 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Mathilda / Mathilda
** 12 1 1650. 700. 62 0 0.95 0.0 0 100 YES 0.0 0. GOOD 0.0 Mathilda On-Ramp
** 13 1 1650. 800. 62 0.95 0.0 0 100 YES 0.0 0. GOOD 0.0 Mathilda / Persian HOV
** 14 1 1650. 1400. 62 D 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks Off-Ramp
** 15 1 1650. 1400. 62 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 West of Lawrence E
** 16 1 1650. 1500. 62 D 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Lawrence Off-ramp
** 17 1 1650. 1500. 62 D 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 End of DKS
** 18 1 1650. 10000. 62 D 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 HOV Dummy
    
```

**
** FREEWAY TRAVEL TIME (MINUTES) **
**

Table with columns: ORIGINS DOWN, DESTINATIONS ACROSS (1-8). Rows 1-6 showing travel times between origins and destinations.

*
* TIME SLICE FREEWAY PERFORMANCE TABLE *
*

Table with columns: SUB NO., SSEC, O-D DATA, DEMANDS, ADJUSTED VOLUMES, SSEC, WEAVE, CONGEST, STORAGE, V/C, SPEED, DENSITY, LOS, FUEL, EMISSIONS. Rows 1-19 showing performance metrics for each lane.

* TOTAL 35640. = 6.8 MILES MAX(V/C) = 0.62 LOWEST LOS = B AVG = 62. 14.6 21.6 12.8 *

Summary table with columns: CURRENT TIME SLICE, CUMULATIVE VALUES. Rows for various metrics like FREeway TRAVEL TIME, MERGE DELAY, etc.

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 1.40 | 4 | 0.04 | 5 | 0.04 |
| 6 | 0.04 | 7 | 0.08 | 8 | 0.10 | 9 | 0.10 | 10 | 0.10 |
| 11 | 0.29 | 12 | 0.10 | 13 | 0.12 | 14 | 0.20 | 15 | 0.19 |
| 16 | 0.21 | 17 | 0.20 | 18 | 1.34 | 19 | 0.00 | | |

***** TOTAL DELAY = 4.5 VEH-HRS ***** AVERAGE DELAY = 0.30 MIN/VEH *****

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 ** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|------|-----------------------|------|------|------|------|------|------|------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 2.38 | 2.94 | 3.89 | 4.42 | 4.70 | 6.53 | 0.00 | |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 2.23 | 2.50 | 4.33 | 0.00 | |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.14 | 3.98 | 0.00 | |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.17 | 0.00 | |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |

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TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|-----------|--------|------------|----------------|--------------------|-------------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|
| * SEC | * LNS | * LENGTH | * ORG DES SSEC | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 1 | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | |
| * 3 | 1 | 12000. | 1133. 0. | 1133. 1133. | 0. 1133. | 1650. | 0. | 0. | .69 | 62. | 18.3 | C | 21.6 | 12.8 |
| * 4 | 1 | 350. | 75. 0. | 1208. 75. | 0. 1208. | 1650. | 0. | 0. | .73 | 62. | 19.5 | C | 21.6 | 12.8 |
| * 5 | 1 | 300. | 0. 0. | 1208. 0. | 0. 1208. | 1650. | 0. | 0. | .73 | 62. | 19.5 | C | 21.6 | 12.8 |
| * 6 | 1 | 350. | 0. 357. | 1208. 0. | 357. 1208. | 1650. | 0. | 0. | .73 | 62. | 19.5 | C | 21.6 | 12.8 |
| * 7 | 1 | 940. | 0. 0. | 851. 0. | 0. 851. | 1650. | 0. | 0. | .52 | 62. | 13.7 | B | 21.6 | 12.8 |
| * 8 | 1 | 700. | 419. 0. | 1270. 419. | 0. 1270. | 1650. | 0. | 0. | .77 | 62. | 20.5 | C | 21.6 | 12.8 |
| * 9 | 1 | 700. | 0. 0. | 1270. 0. | 0. 1270. | 1650. | 0. | 0. | .77 | 62. | 20.5 | C | 21.6 | 12.8 |
| * 10 | 1 | 700. | 0. 126. | 1270. 0. | 126. 1270. | 1650. | 0. | 0. | .77 | 62. | 20.5 | C | 21.6 | 12.8 |
| * 11 | 1 | 2300. | 0. 0. | 1144. 0. | 0. 1144. | 1650. | 0. | 0. | .69 | 62. | 18.5 | C | 21.6 | 12.8 |
| * 12 | 1 | 700. | 171. 0. | 1315. 171. | 0. 1315. | 1650. | 0. | 0. | .80 | 62. | 21.2 | C | 21.6 | 12.8 |
| * 13 | 1 | 800. | 0. 0. | 1315. 0. | 0. 1315. | 1650. | 0. | 0. | .80 | 62. | 21.2 | C | 21.6 | 12.8 |
| * 14 | 1 | 1400. | 0. 54. | 1315. 0. | 54. 1315. | 1650. | 0. | 0. | .80 | 62. | 21.2 | C | 21.6 | 12.8 |
| * 15 | 1 | 1400. | 0. 0. | 1261. 0. | 0. 1261. | 1650. | 0. | 0. | .76 | 62. | 20.3 | C | 21.6 | 12.8 |
| * 16 | 1 | 1500. | 0. 43. | 1261. 0. | 43. 1261. | 1650. | 0. | 0. | .76 | 62. | 20.3 | C | 21.6 | 12.8 |
| * 17 | 1 | 1500. | 0. 0. | 1219. 0. | 0. 1219. | 1650. | 0. | 0. | .74 | 62. | 19.7 | C | 21.6 | 12.8 |
| * 18 | 1 | 10000. | 0. 1219. | 1219. 0. | 1219. 1219. | 1650. | 0. | 0. | .74 | 62. | 19.7 | C | 21.6 | 12.8 |
| * 19 | | | | | | | | | | | | | | |

* TOTAL 35640. = 6.8 MILES MAX(V/C) = 0.80 LOWEST LOS = C AVG = 62. 19.2 21.6 12.8

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 129. VEH-HRS | 228. VEH-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 129. VEH-HRS | 228. VEH-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 8027. VEH-MI. | 14132. VEH-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 62. MPH. |
| AVERAGE DENSITY = | 19. VPMP | 17. VPMP |
| TOTAL FUEL = | 372. GALLONS | 656. GALLONS |

TOTAL EMISSIONS = 102. KILOGRAMS

SR-237_EB_AM_P1_2040_PL
180. KILOGRAMS

1 INSTITUTE OF TRANSPORTATION STUDIES
UNIVERSITY OF CALIFORNIA, BERKELEY

FREQ12PL REL 3.01
SHORT TERM SIMULATION OF PRIORITY LANE
TIME SLICE 2 OF 2

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***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 1.92 | 4 | 0.06 | 5 | 0.05 |
| 6 | 0.06 | 7 | 0.11 | 8 | 0.13 | 9 | 0.13 | 10 | 0.13 |
| 11 | 0.37 | 12 | 0.13 | 13 | 0.15 | 14 | 0.26 | 15 | 0.25 |
| 16 | 0.27 | 17 | 0.26 | 18 | 1.72 | 19 | 0.00 | | |

***** TOTAL DELAY = 6.0 VEH-HRS ***** AVERAGE DELAY = 0.30 MIN/VEH *****

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FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQQ QQQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP EEEEEEEEE
    
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FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 62
LOWER LIMB (AT V/C=1) = 30
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT TRUCKS | DES TRUCKS | SPECIAL RAMP | FF. SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION LOCATION |
|---------|----------|----------|-------------|--------------|---------|---------|-----------|---------|------------|------------|--------------|-------------------|---------------|----------|----------------|------------------------|
| ** 1 | 3 | 6000. | 500. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Seeding |
| ** 2 | 3 | 6000. | 99999. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture |
| ** 3 | 2 | 4000. | 12000. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** 4 | 3 | 4570. | 350. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Maude On-Ramp |
| ** 5 | 3 | 4570. | 300. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Maude to US-101 |
| ** 6 | 3 | 4570. | 350. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US-101 Off-ramp |
| ** 7 | 2 | 4000. | 940. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | US101SB / US101SB |
| ** 8 | 3 | 4930. | 700. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US101 SB On-ramp |
| ** 9 | 3 | 4930. | 700. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US 101 / Mathilda |
| ** 10 | 3 | 4930. | 700. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-ramp |
| ** 11 | 2 | 4000. | 2300. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda |
| ** 12 | 3 | 4470. | 700. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda On-Ramp |
| ** 13 | 3 | 4470. | 800. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda / Persian HOV |
| ** 14 | 3 | 4470. | 1400. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks Off-Ramp |
| ** 15 | 2 | 4000. | 1400. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | West of Lawrence E |
| ** 16 | 2 | 4000. | 1500. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence Off-ramp |
| ** 17 | 2 | 4000. | 1500. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End of DKS |
| ** 18 | 2 | 4000. | 10000. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** 19 | 3 | 5600. | 750. | 62 | OD | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End of the network |

***** INPUT HAS BEEN COMPLETED *****

**
** FREeway TRAVEL TIME (MINUTES) **
**

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | |
|-----------|-------|-----------------------|-------|-------|-------|-------|-------|---|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 18.42 | 20.80 | 21.36 | 22.31 | 22.84 | 23.12 | 25.09 | |
| * 2 * | 0.00 | 0.18 | 0.74 | 1.69 | 2.23 | 2.50 | 4.47 | |
| * 3 * | 0.00 | 0.00 | 0.38 | 1.34 | 1.87 | 2.14 | 4.11 | |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.53 | 1.06 | 1.34 | 3.31 | |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.14 | |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | |
|-----------|----------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|------|------|
| * SEC LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | |
| * 1 | 3 | 500. | 3302. | 0. | 3302. | 3302. | 0. | 3302. | 6000. | 0. | 0. | .55 | 62. | 17.8 | B | 20.3 | 13.0 |
| * 2 | 3 | 99999. | 0. | 825. | 3302. | 0. | 825. | 3302. | 6000. | 0. | 0. | .55 | 62. | 17.8 | B | 20.3 | 13.0 |
| * 3 | 2 | 12000. | 0. | 0. | 2477. | 0. | 0. | 2477. | 4000. | 0. | 0. | .62 | 62. | 20.0 | C | 20.3 | 13.0 |
| * 4 | 3 | 350. | 303. | 0. | 2780. | 303. | 0. | 2780. | 4523. | 0. | 0. | .61 | 62. | 14.9 | B | 20.3 | 13.0 |
| * 5 | 3 | 300. | 0. | 0. | 2780. | 0. | 0. | 2780. | 4570. | 0. | 0. | .61 | 62. | 14.9 | B | 20.3 | 13.0 |
| * 6 | 3 | 350. | 0. | 867. | 2780. | 0. | 867. | 2780. | 4317. | 0. | 0. | .64 | 62. | 14.9 | B | 20.3 | 13.0 |
| * 7 | 2 | 940. | 0. | 0. | 1913. | 0. | 0. | 1913. | 4000. | 0. | 0. | .48 | 62. | 15.4 | B | 20.3 | 13.0 |
| * 8 | 3 | 700. | 1618. | 0. | 3531. | 1618. | 0. | 3531. | 4567. | 0. | 0. | .77 | 62. | 19.0 | C | 20.3 | 13.0 |
| * 9 | 3 | 700. | 0. | 0. | 3531. | 0. | 0. | 3531. | 4930. | 0. | 0. | .72 | 62. | 19.0 | C | 20.3 | 13.0 |
| * 10 | 3 | 700. | 0. | 595. | 3531. | 0. | 595. | 3531. | 4844. | 0. | 0. | .73 | 62. | 19.0 | C | 20.3 | 13.0 |
| * 11 | 2 | 2300. | 0. | 0. | 2936. | 0. | 0. | 2936. | 4000. | 0. | 0. | .73 | 62. | 23.7 | C | 20.3 | 13.0 |
| * 12 | 3 | 700. | 416. | 0. | 3352. | 416. | 0. | 3352. | 4356. | 0. | 0. | .77 | 62. | 18.0 | C | 20.3 | 13.0 |
| * 13 | 3 | 800. | 0. | 0. | 3352. | 0. | 0. | 3352. | 4470. | 0. | 0. | .75 | 62. | 18.0 | C | 20.3 | 13.0 |
| * 14 | 3 | 1400. | 0. | 322. | 3352. | 0. | 322. | 3352. | 4430. | 0. | 0. | .76 | 62. | 18.0 | C | 20.3 | 13.0 |
| * 15 | 2 | 1400. | 0. | 0. | 3030. | 0. | 0. | 3030. | 4000. | 0. | 0. | .76 | 62. | 24.4 | C | 20.3 | 13.0 |
| * 16 | 2 | 1500. | 0. | 207. | 3030. | 0. | 207. | 3030. | 3971. | 0. | 0. | .76 | 62. | 24.4 | C | 20.3 | 13.0 |
| * 17 | 2 | 1500. | 0. | 0. | 2823. | 0. | 0. | 2823. | 4000. | 0. | 0. | .71 | 62. | 22.8 | C | 20.3 | 13.0 |
| * 18 | 2 | 10000. | 0. | 0. | 2823. | 0. | 0. | 2823. | 4000. | 0. | 0. | .71 | 62. | 22.8 | C | 20.3 | 13.0 |
| * 19 | 3 | 750. | 941. | 3764. | 3764. | 941. | 3764. | 3764. | 5600. | 0. | 0. | .67 | 62. | 20.2 | C | 20.3 | 13.0 |

* TOTAL 136889. = 25.9 MILES MAX(V/C) = 0.77 LOWEST LOS = C AVG = 62. 18.6 20.3 13.0

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREeway TRAVEL TIME = | 1326. VEH-HRS | 1584. PASS-HRS |
| FREeway MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1326. VEH-HRS | 1584. PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 82218. VEH-MI. | 98215. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 62. MPH. |
| AVERAGE DENSITY = | 19. VPMP | 19. VPMP |
| TOTAL FUEL = | 4042. GALLONS | 4042. GALLONS |
| TOTAL EMISSIONS = | 1073. KI LOGRAMS | 1073. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.23 | 2 | 46.55 | 3 | 4.19 | 4 | 0.14 | 5 | 0.12 |
| 6 | 0.14 | 7 | 0.25 | 8 | 0.35 | 9 | 0.35 | 10 | 0.35 |
| 11 | 0.95 | 12 | 0.33 | 13 | 0.38 | 14 | 0.66 | 15 | 0.60 |
| 16 | 0.64 | 17 | 0.60 | 18 | 3.98 | 19 | 0.40 | | |

***** TOTAL DELAY = 61.2 VEH-HRS ***** AVERAGE DELAY = 1.16 MIN/VEH *****

**
** FREEWAY TRAVEL TIME (MINUTES)
**

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | |
|-----------|-------|-----------------------|-------|-------|-------|-------|-------|---|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 18.42 | 20.88 | 21.44 | 22.42 | 23.00 | 23.29 | 25.34 | |
| * 2 * | 0.00 | 0.18 | 0.74 | 1.72 | 2.30 | 2.59 | 4.64 | |
| * 3 * | 0.00 | 0.00 | 0.38 | 1.36 | 1.95 | 2.23 | 4.28 | |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.53 | 1.12 | 1.40 | 3.45 | |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.14 | |

*
* TIME SLICE FREEWAY PERFORMANCE TABLE
*

| * SUB | * NO. | * SSEC | * O-D | * DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | |
|--|-------|----------|---------|---------|-----------|------------|-----------|---------|---------|-----------|-----------|--------|---------|-----------|--------|---------|-------------|---------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 1 | * 3 | * 500. | * 4530. | * 0. | * 4530. | * 4530. | * 0. | * 4530. | * 6000. | * 0. | * 0. | * 0. | * .75 | * 62. | * 24.4 | * C | * 20.3 | * 13.0 |
| * 2 | * 3 | * 99999. | * 0. | * 1132. | * 4530. | * 0. | * 1132. | * 4530. | * 6000. | * 0. | * 0. | * 0. | * .75 | * 62. | * 24.4 | * C | * 20.3 | * 13.0 |
| * 3 | * 2 | * 12000. | * 0. | * 0. | * 3398. | * 0. | * 0. | * 3398. | * 4000. | * 0. | * 0. | * 0. | * .85 | * 60. | * 28.4 | * D | * 21.4 | * 12.3 |
| * 4 | * 3 | * 350. | * 493. | * 0. | * 3891. | * 493. | * 0. | * 3891. | * 4494. | * 0. | * 0. | * 0. | * .87 | * 62. | * 20.9 | * C | * 20.3 | * 13.0 |
| * 5 | * 3 | * 300. | * 0. | * 0. | * 3891. | * 0. | * 0. | * 3891. | * 4570. | * 0. | * 0. | * 0. | * .85 | * 62. | * 20.9 | * C | * 20.3 | * 13.0 |
| * 6 | * 3 | * 350. | * 0. | * 1221. | * 3891. | * 0. | * 1221. | * 3891. | * 4221. | * 0. | * 0. | * 0. | * .92 | * 62. | * 20.9 | * C | * 20.3 | * 13.0 |
| * 7 | * 2 | * 940. | * 0. | * 0. | * 2670. | * 0. | * 0. | * 2670. | * 4000. | * 0. | * 0. | * 0. | * .67 | * 62. | * 21.5 | * C | * 20.3 | * 13.0 |
| * 8 | * 3 | * 700. | * 1751. | * 0. | * 4421. | * 1616. | * 0. | * 4286. | * 4547. | * 0. | * 0. | * 0. | * .94 | * 62. | * 23.0 | * C | * 20.3 | * 13.0 |
| * 9 | * 3 | * 700. | * 0. | * 0. | * 4421. | * 0. | * 0. | * 4286. | * 4930. | * 0. | * 0. | * 0. | * .87 | * 62. | * 23.0 | * C | * 20.3 | * 13.0 |
| * 10 | * 3 | * 700. | * 0. | * 794. | * 4421. | * 0. | * 767. | * 4286. | * 4803. | * 0. | * 0. | * 0. | * .89 | * 62. | * 23.0 | * C | * 20.3 | * 13.0 |
| * 11 | * 2 | * 2300. | * 0. | * 0. | * 3627. | * 0. | * 0. | * 3519. | * 4000. | * 0. | * 0. | * 0. | * .88 | * 59. | * 30.0 | * D | * 21.7 | * 12.1 |
| * 12 | * 3 | * 700. | * 569. | * 0. | * 4196. | * 569. | * 0. | * 4088. | * 4315. | * 0. | * 0. | * 0. | * .95 | * 62. | * 22.0 | * C | * 20.3 | * 13.0 |
| * 13 | * 3 | * 800. | * 0. | * 0. | * 4196. | * 0. | * 0. | * 4088. | * 4470. | * 0. | * 0. | * 0. | * .91 | * 62. | * 22.0 | * C | * 20.3 | * 13.0 |
| * 14 | * 3 | * 1400. | * 0. | * 400. | * 4196. | * 0. | * 389. | * 4088. | * 4416. | * 0. | * 0. | * 0. | * .93 | * 62. | * 22.0 | * C | * 20.3 | * 13.0 |
| * 15 | * 2 | * 1400. | * 0. | * 0. | * 3796. | * 0. | * 0. | * 3699. | * 4000. | * 0. | * 0. | * 0. | * .92 | * 57. | * 32.7 | * D | * 22.4 | * 11.7 |
| * 16 | * 2 | * 1500. | * 0. | * 275. | * 3796. | * 0. | * 267. | * 3699. | * 3957. | * 0. | * 0. | * 0. | * .93 | * 56. | * 33.0 | * D | * 22.5 | * 11.6 |
| * 17 | * 2 | * 1500. | * 0. | * 0. | * 3521. | * 0. | * 0. | * 3432. | * 4000. | * 0. | * 0. | * 0. | * .86 | * 59. | * 28.8 | * D | * 21.5 | * 12.3 |
| * 18 | * 2 | * 10000. | * 0. | * 0. | * 3521. | * 0. | * 0. | * 3432. | * 4000. | * 0. | * 0. | * 0. | * .86 | * 59. | * 28.8 | * D | * 21.5 | * 12.3 |
| * 19 | * 3 | * 750. | * 1173. | * 4694. | * 4694. | * 1173. | * 4605. | * 4605. | * 5600. | * 0. | * 0. | * 0. | * .82 | * 62. | * 24.8 | * C | * 20.3 | * 13.0 |
| ***** | | | | | | | | | | | | | | | | | | |
| * TOTAL 136889. = 25.9 MILES MAX(V/C) = 0.95 LOWEST LOS = D AVG = 62. 25.3 20.5 12.9 * | | | | | | | | | | | | | | | | | | |
| ***** | | | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 1802. VEH-HRS | 2155. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 68. VEH-HRS | 68. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1869. VEH-HRS | 2222. PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 110803. VEH-MI. | 132706. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 59. MPH. | 62. MPH. |

AVERAGE DENSITY = 25. VPMP
 TOTAL FUEL = 5418. GALLONS
 TOTAL EMISSIONS = 1440. KILOGRAMS

SR-237_EB_AM_P2_2040_PE
 22. VPMP
 9460. GALLONS
 2513. KILOGRAMS

1 INSTITUTE OF TRANSPORTATION STUDIES
 UNIVERSITY OF CALIFORNIA, BERKELEY

FREQ12PE REL 3.01
 SIMULATION AFTER CONTROL, NO DI VERSION
 TIME SLICE 2 OF 2

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***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.32 | 2 | 63.87 | 3 | 10.40 | 4 | 0.19 | 5 | 0.16 |
| 6 | 0.19 | 7 | 0.35 | 8 | 0.42 | 9 | 0.42 | 10 | 0.42 |
| 11 | 2.53 | 12 | 0.40 | 13 | 0.46 | 14 | 0.81 | 15 | 2.24 |
| 16 | 2.59 | 17 | 1.39 | 18 | 9.26 | 19 | 0.49 | | |

***** TOTAL DELAY = 96.9 VEH-HRS ***** AVERAGE DELAY = 1.41 MIN/VEH *****

***** RAMP DELAYS *****

| ON-RAMP | | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|---------|---------|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|
| 3 | RAMP | 135. | 67.50 | 1.90 | 24.34 | 1.50 | 7.87 | 0.42 | 9.79 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 135. | 67.50 | 1.90 | 24.34 | 1.50 | 7.87 | 0.42 | 9.79 |

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FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ      1111      222222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP LLL
FFF      RRR      RRR EEE      QQQQQ QQQQ      1111      222 222 PPP      PPP LLL
FFF      RRR      RRR EEE      QQQQ      QQQQ      1111      222 222 PPP      PPP LLL
FFFFFFFF RRRRRRRR EEEEEEEE QQQQ      QQQQ      1111      222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEEE QQQQ      QQQQ      1111      2222 PPPPPPPP LLL
FFF      RRR      RRR EEE      QQQQ      QQQ QQQQ      1111      2222 PPP      LLL
FFF      RRR      RRR EEE      Q*UC*      QQQQ      1111      222 PPP      LLL
FFF      RRR      RRR EEEEEEEEE Q*REGENTS*Q 1111      222 PPP      LLLLLLLLLL
FFF      RRR      RRR EEEEEEEEE Q*1988*Q QQQ 1111111 2222222222 PPP      LLLLLLLLLL
    
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FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 3 AND 18 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 62
LOWER LIMB (AT V/C=1) = 30
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

```

*****
**
**
**          FREEWAY AND ARTERIAL DESIGN FEATURES          **
**
*****
** SUB NO.   SSEC  SSEC  DESIG N  ORG  TRK  SSEC PCT  PCT DES  SPECIAL  FF.SPD.  CAP.  ART  GRADE  SUBSECTI ON LOCATI ON **
** SEC LNS   CAP   LENGTH SPEED  DES  FAC  GRAD TRK  TRUCKS  RAMP     ALT. RTE  ALT. RTE TYPE ALT. RTE                               **
**          **          **          **          **          **          **          **          **          **          **          **          **          **          **          **
** 1          **          **          **          **          **          **          **          **          **          **          **          **          **          **          **
** 2          **          **          **          **          **          **          **          **          **          **          **          **          **          **          **          **
** 3  1   1650. 12000. 62    0   0.95  0.0 0   100    NO    0.0    0.   GOOD  0.0  HOV Dummy          **
** 4  1   1650.   350. 62    0   0.95  0.0 0   100    YES   0.0    0.   GOOD  0.0  Maude On-Ramp      **
** 5  1   1650.   300. 62          0.95  0.0 0   100    YES   0.0    0.   GOOD  0.0  Maude to US-101    **
** 6  1   1650.   350. 62    D   0.95  0.0 0   100    YES   0.0    0.   GOOD  0.0  US-101 Off-ramp    **
** 7  1   1650.   940. 62          0.95  0.0 0   100    NO    0.0    0.   GOOD  0.0  US101SB / US101SB  **
** 8  1   1650.   700. 62    0   0.95  0.0 0   100    YES   0.0    0.   GOOD  0.0  US101 SB On-ramp   **
** 9  1   1650.   700. 62          0.95  0.0 0   100    YES   0.0    0.   GOOD  0.0  US 101 / Mathilda **
** 10 1   1650.   700. 62    D   0.95  0.0 0   100    YES   0.0    0.   GOOD  0.0  Mathilda Off-ramp  **
** 11 1   1650.  2300. 62          0.95  0.0 0   100    NO    0.0    0.   GOOD  0.0  Mathilda / Mathilda **
** 12 1   1650.   700. 62    0   0.95  0.0 0   100    YES   0.0    0.   GOOD  0.0  Mathilda On-Ramp   **
** 13 1   1650.   800. 62          0.95  0.0 0   100    YES   0.0    0.   GOOD  0.0  Mathilda / Persian HOV **
** 14 1   1650.  1400. 62    D   0.95  0.0 0   100    NO    0.0    0.   GOOD  0.0  Fair Oaks Off-Ramp **
** 15 1   1650.  1400. 62          0.95  0.0 0   100    NO    0.0    0.   GOOD  0.0  West of Lawrence E  **
** 16 1   1650.  1500. 62    D   0.95  0.0 0   100    NO    0.0    0.   GOOD  0.0  Lawrence Off-ramp   **
** 17 1   1650.  1500. 62    D   0.95  0.0 0   100    NO    0.0    0.   GOOD  0.0  End of DKS          **
** 18 1   1650. 10000. 62    D   0.95  0.0 0   100    NO    0.0    0.   GOOD  0.0  HOV Dummy          **
    
```

** 19 **

 ** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|------|-----------------------|------|------|------|------|------|------|------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 2.38 | 2.94 | 3.89 | 4.42 | 4.70 | 6.53 | 0.00 | |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 2.23 | 2.50 | 4.33 | 0.00 | |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.14 | 3.98 | 0.00 | |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.17 | 0.00 | |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | | |
|-----------|----------|------------|------------|--------------------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|------|---|------|------|
| * SEC LNS | * LENGTH | * ORG | * DES SSEC | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | | | |
| * 1 | | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | | |
| * 3 | 1 | 12000. | 825. | 0. | 825. | 825. | 0. | 825. | 1650. | 0. | 0. | 0. | .50 | 62. | 13.3 | B | 21.6 | 12.8 |
| * 4 | 1 | 350. | 47. | 0. | 873. | 47. | 0. | 873. | 1650. | 0. | 0. | 0. | .53 | 62. | 14.1 | B | 21.6 | 12.8 |
| * 5 | 1 | 300. | 0. | 0. | 873. | 0. | 0. | 873. | 1650. | 0. | 0. | 0. | .53 | 62. | 14.1 | B | 21.6 | 12.8 |
| * 6 | 1 | 350. | 0. | 253. | 873. | 0. | 253. | 873. | 1650. | 0. | 0. | 0. | .53 | 62. | 14.1 | B | 21.6 | 12.8 |
| * 7 | 1 | 940. | 0. | 0. | 619. | 0. | 0. | 619. | 1650. | 0. | 0. | 0. | .38 | 62. | 10.0 | A | 21.6 | 12.8 |
| * 8 | 1 | 700. | 363. | 0. | 982. | 363. | 0. | 982. | 1650. | 0. | 0. | 0. | .60 | 62. | 15.8 | B | 21.6 | 12.8 |
| * 9 | 1 | 700. | 0. | 0. | 982. | 0. | 0. | 982. | 1650. | 0. | 0. | 0. | .60 | 62. | 15.8 | B | 21.6 | 12.8 |
| * 10 | 1 | 700. | 0. | 86. | 982. | 0. | 86. | 982. | 1650. | 0. | 0. | 0. | .60 | 62. | 15.8 | B | 21.6 | 12.8 |
| * 11 | 1 | 2300. | 0. | 0. | 896. | 0. | 0. | 896. | 1650. | 0. | 0. | 0. | .54 | 62. | 14.4 | B | 21.6 | 12.8 |
| * 12 | 1 | 700. | 114. | 0. | 1010. | 114. | 0. | 1010. | 1650. | 0. | 0. | 0. | .61 | 62. | 16.3 | B | 21.6 | 12.8 |
| * 13 | 1 | 800. | 0. | 0. | 1010. | 0. | 0. | 1010. | 1650. | 0. | 0. | 0. | .61 | 62. | 16.3 | B | 21.6 | 12.8 |
| * 14 | 1 | 1400. | 0. | 40. | 1010. | 0. | 40. | 1010. | 1650. | 0. | 0. | 0. | .61 | 62. | 16.3 | B | 21.6 | 12.8 |
| * 15 | 1 | 1400. | 0. | 0. | 970. | 0. | 0. | 970. | 1650. | 0. | 0. | 0. | .59 | 62. | 15.6 | B | 21.6 | 12.8 |
| * 16 | 1 | 1500. | 0. | 29. | 970. | 0. | 29. | 970. | 1650. | 0. | 0. | 0. | .59 | 62. | 15.6 | B | 21.6 | 12.8 |
| * 17 | 1 | 1500. | 0. | 0. | 941. | 0. | 0. | 941. | 1650. | 0. | 0. | 0. | .57 | 62. | 15.2 | B | 21.6 | 12.8 |
| * 18 | 1 | 10000. | 0. | 941. | 941. | 0. | 941. | 941. | 1650. | 0. | 0. | 0. | .57 | 62. | 15.2 | B | 21.6 | 12.8 |
| * 19 | | | | | | | | | | | | | | | | | | |
| * TOTAL | | 35640. | = | 6.8 | MILES | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 98. VEH-HRS | 196. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 98. VEH-HRS | 196. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 6068. VEH-MI. | 12136. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | |
| AVERAGE DENSITY = | 14. VPMP | |
| TOTAL FUEL = | 282. GALLONS | |
| TOTAL EMISSIONS = | 77. KILOGRAMS | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 1.40 | 4 | 0.04 | 5 | 0.04 |
| 6 | 0.04 | 7 | 0.08 | 8 | 0.10 | 9 | 0.10 | 10 | 0.10 |
| 11 | 0.29 | 12 | 0.10 | 13 | 0.11 | 14 | 0.20 | 15 | 0.19 |
| 16 | 0.21 | 17 | 0.20 | 18 | 1.33 | 19 | 0.00 | | |

***** TOTAL DELAY = 4.5 VEH-HRS ***** AVERAGE DELAY = 0.30 MIN/VEH *****

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 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE TIME SLICE 2 OF 2

 **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|------|-----------------------|------|------|------|------|------|------|------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 2.38 | 2.94 | 3.89 | 4.42 | 4.70 | 6.53 | 0.00 | |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 2.23 | 2.50 | 4.33 | 0.00 | |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.14 | 3.98 | 0.00 | |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.17 | 0.00 | |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE TIME SLICE 2 OF 2

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|-----------|--------|------------|----------------|--------------------|--------|---------|-----------------|-----------|---------|----------------|-----------|---------|--------|-------------|
| * SEC | * LNS | * LENGTH | * ORG DES SSEC | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 1 | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | |
| * 3 | 1 | 12000. | 1132. 0. 1132. | 1132. 0. 1132. | 1650. | 0. | 0. | 0. | .69 | 62. | 18.3 | C | 21.6 | 12.8 |
| * 4 | 1 | 350. | 76. 0. 1208. | 76. 0. 1208. | 1650. | 0. | 0. | 0. | .73 | 62. | 19.5 | C | 21.6 | 12.8 |
| * 5 | 1 | 300. | 0. 0. 1208. | 0. 0. 1208. | 1650. | 0. | 0. | 0. | .73 | 62. | 19.5 | C | 21.6 | 12.8 |
| * 6 | 1 | 350. | 0. 349. 1208. | 0. 349. 1208. | 1650. | 0. | 0. | 0. | .73 | 62. | 19.5 | C | 21.6 | 12.8 |
| * 7 | 1 | 940. | 0. 0. 859. | 0. 0. 859. | 1650. | 0. | 0. | 0. | .52 | 62. | 13.9 | B | 21.6 | 12.8 |
| * 8 | 1 | 700. | 384. 0. 1243. | 384. 0. 1243. | 1650. | 0. | 0. | 0. | .75 | 62. | 20.0 | C | 21.6 | 12.8 |
| * 9 | 1 | 700. | 0. 0. 1243. | 0. 0. 1243. | 1650. | 0. | 0. | 0. | .75 | 62. | 20.0 | C | 21.6 | 12.8 |
| * 10 | 1 | 700. | 0. 128. 1243. | 0. 128. 1243. | 1650. | 0. | 0. | 0. | .75 | 62. | 20.0 | C | 21.6 | 12.8 |
| * 11 | 1 | 2300. | 0. 0. 1115. | 0. 0. 1115. | 1650. | 0. | 0. | 0. | .68 | 62. | 18.0 | B | 21.6 | 12.8 |
| * 12 | 1 | 700. | 156. 0. 1271. | 156. 0. 1271. | 1650. | 0. | 0. | 0. | .77 | 62. | 20.5 | C | 21.6 | 12.8 |
| * 13 | 1 | 800. | 0. 0. 1271. | 0. 0. 1271. | 1650. | 0. | 0. | 0. | .77 | 62. | 20.5 | C | 21.6 | 12.8 |
| * 14 | 1 | 1400. | 0. 55. 1271. | 0. 55. 1271. | 1650. | 0. | 0. | 0. | .77 | 62. | 20.5 | C | 21.6 | 12.8 |
| * 15 | 1 | 1400. | 0. 0. 1216. | 0. 0. 1216. | 1650. | 0. | 0. | 0. | .74 | 62. | 19.6 | C | 21.6 | 12.8 |
| * 16 | 1 | 1500. | 0. 43. 1216. | 0. 43. 1216. | 1650. | 0. | 0. | 0. | .74 | 62. | 19.6 | C | 21.6 | 12.8 |
| * 17 | 1 | 1500. | 0. 0. 1173. | 0. 0. 1173. | 1650. | 0. | 0. | 0. | .71 | 62. | 18.9 | C | 21.6 | 12.8 |
| * 18 | 1 | 10000. | 0. 1173. 1173. | 0. 1173. 1173. | 1650. | 0. | 0. | 0. | .71 | 62. | 18.9 | C | 21.6 | 12.8 |
| * 19 | | | | | | | | | | | | | | |
| * TOTAL | | 35640. | = 6.8 MILES | | | | MAX(V/C) = 0.77 | | | LOWEST LOS = C | AVG = 62. | 18.8 | 21.6 | 12.8 |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 127. VEH-HRS | 253. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 127. VEH-HRS | 253. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 7856. VEH-MI. | 15713. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 62. MPH. |
| AVERAGE DENSITY = | 19. VPMP | 17. VPMP |
| TOTAL FUEL = | 365. GALLONS | 646. GALLONS |

TOTAL EMISSIONS = 100. KILOGRAMS

SR-237_EB_AM_P2_2040_PL
178. KILOGRAMS

1 INSTITUTE OF TRANSPORTATION STUDIES
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FREQ12PL REL 3.01
SHORT TERM SIMULATION OF PRIORITY LANE
TIME SLICE 2 OF 2

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PAGE 8

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 1.92 | 4 | 0.06 | 5 | 0.05 |
| 6 | 0.06 | 7 | 0.11 | 8 | 0.12 | 9 | 0.12 | 10 | 0.12 |
| 11 | 0.36 | 12 | 0.13 | 13 | 0.14 | 14 | 0.25 | 15 | 0.24 |
| 16 | 0.26 | 17 | 0.25 | 18 | 1.65 | 19 | 0.00 | | |

***** TOTAL DELAY = 5.8 VEH-HRS ***** AVERAGE DELAY = 0.30 MIN/VEH *****

```

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQQ QQQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP EEEEEEEEE
    
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FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 62
LOWER LIMB (AT V/C=1) = 30
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREWAY AND ARTERIAL DESIGN FEATURES

| ** SUB NO. | ** SSEC | ** SSEC | ** DESIG N | ** ORG | ** TRK | ** SSEC | ** PCT | ** PCT | ** DES | ** SPECIAL | ** FF. SPD. | ** CAP. | ** ART | ** GRADE | ** SUBSECTI ON | ** LOCATI ON |
|------------|---------|---------|------------|----------|--------|---------|--------|-----------|---------|-------------|-------------|---------|-------------|-------------|------------------------|--------------|
| ** SEC | ** LNS | ** CAP | ** LENGTH | ** SPEED | ** DES | ** GRAD | ** TRK | ** TRUCKS | ** RAMP | ** ALT. RTE | ** ALT. RTE | ** TYPE | ** ALT. RTE | ** ALT. RTE | ** LOCATION | ** LOCATION |
| ** 1 | 3 | 6000. | 500. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Seeding | |
| ** 2 | 3 | 6000. | 99999. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | |
| ** 3 | 2 | 4000. | 12000. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | |
| ** 4 | 3 | 5010. | 350. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Maude On-ramp | |
| ** 5 | 3 | 5010. | 300. | 62 | | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Maude to US-101 | |
| ** 6 | 3 | 5010. | 350. | 62 | D | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US-101 Off-Ramp | |
| ** 7 | 2 | 4000. | 940. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | US101SB / US101SB | |
| ** 8 | 3 | 5330. | 700. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US101 SB On-ramp | |
| ** 9 | 3 | 5330. | 700. | 62 | | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US 101 / Mathilda | |
| ** 10 | 3 | 5330. | 700. | 62 | D | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-ramp | |
| ** 11 | 2 | 4000. | 2300. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | |
| ** 12 | 3 | 5320. | 700. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda On-Ramp | |
| ** 13 | 3 | 4400. | 800. | 62 | | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda / Persian HOV | |
| ** 14 | 3 | 4400. | 1400. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Persian On-Ramp w/HOV | |
| ** 15 | 2 | 4000. | 1400. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | West of Lawrence E | |
| ** 16 | 2 | 4000. | 1500. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence Off-ramp | |
| ** 17 | 2 | 4000. | 1500. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End of DKS | |
| ** 18 | 2 | 4000. | 5000. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | |
| ** 19 | 2 | 4000. | 5000. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Enter SSec Description | |
| ** 20 | 3 | 2500. | 750. | 62 | OD | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | End of the network | |

***** INPUT HAS BEEN COMPLETED *****

MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 2 IN TIME SLICE 2
--- THE MAXIMUM METERING RATE WILL PREVAIL.

MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 2 IN TIME SLICE 3
--- THE MAXIMUM METERING RATE WILL PREVAIL.

**
** FREEWAY TRAVEL TIME (MINUTES) **
**

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | |
|-----------|---|-----------------------|-------|-------|-------|-------|-------|-------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| + | * | 18.42 | 20.80 | 21.56 | 25.37 | 28.90 | 32.34 | 64.72 |
| + | * | 0.00 | 0.18 | 0.94 | 4.75 | 8.28 | 11.72 | 44.10 |
| + | * | 0.00 | 0.00 | 0.58 | 4.40 | 7.92 | 11.37 | 43.75 |
| + | * | 0.00 | 0.00 | 0.00 | 2.47 | 6.00 | 9.44 | 41.82 |
| + | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 13.92 |
| + | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.14 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | | |
|-----------|---------|------------|-----------|------------|-----------|---------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|--------|--------|--------|--|
| * SEC | * LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * SSEC | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | | | |
| * 1 | * 3 | * 500. | * 2660. | * 0. | * 2660. | * 2660. | * 0. | * 2660. | * 6000. | * 0. | * 0. | * 0. | * .44 | * 62. | * 14.3 | * B | * 20.3 | * 13.0 | |
| * 2 | * 3 | * 99999. | * 0. | * 692. | * 2660. | * 0. | * 692. | * 2660. | * 6000. | * 0. | * 0. | * .44 | * 62. | * 14.3 | * B | * 20.3 | * 13.0 | | |
| * 3 | * 2 | * 12000. | * 0. | * 0. | * 1968. | * 0. | * 0. | * 1968. | * 4000. | * 0. | * 0. | * .49 | * 62. | * 15.9 | * B | * 20.3 | * 13.0 | | |
| * 4 | * 3 | * 350. | * 875. | * 0. | * 2843. | * 775. | * 0. | * 2743. | * 4835. | * 0. | * 0. | * .57 | * 62. | * 14.7 | * B | * 20.3 | * 13.0 | | |
| * 5 | * 3 | * 300. | * 0. | * 0. | * 2843. | * 0. | * 0. | * 2743. | * 5010. | * 0. | * 0. | * .55 | * 62. | * 14.7 | * B | * 20.3 | * 13.0 | | |
| * 6 | * 3 | * 350. | * 0. | * 708. | * 2843. | * 0. | * 680. | * 2743. | * 4848. | * 0. | * 0. | * .57 | * 62. | * 14.7 | * B | * 20.3 | * 13.0 | | |
| * 7 | * 2 | * 940. | * 0. | * 0. | * 2135. | * 0. | * 0. | * 2063. | * 4000. | * 0. | * 0. | * .52 | * 62. | * 16.6 | * B | * 20.3 | * 13.0 | | |
| * 8 | * 3 | * 700. | * 712. | * 0. | * 2847. | * 712. | * 0. | * 987. | * 5168. | * 0. | * 116. | * 1788. | * .19 | * 62. | * 5.3 | * F | * 20.3 | * 13.1 | |
| * 9 | * 3 | * 700. | * 0. | * 0. | * 2847. | * 0. | * 0. | * 987. | * 5330. | * 0. | * 700. | * 1788. | * .19 | * 43. | * 7.6 | * F | * 20.0 | * 13.2 | |
| * 10 | * 3 | * 700. | * 0. | * 383. | * 2847. | * 0. | * 372. | * 987. | * 5266. | * 0. | * 700. | * 1788. | * .19 | * 30. | * 11.1 | * F | * 19.6 | * 13.5 | |
| * 11 | * 2 | * 2300. | * 0. | * 0. | * 2464. | * 0. | * 0. | * 615. | * 4000. | * 0. | * 2300. | * 1788. | * .15 | * 19. | * 15.8 | * F | * 19.1 | * 13.7 | |
| * 12 | * 3 | * 700. | * 639. | * 0. | * 3103. | * 539. | * 0. | * 1154. | * 5149. | * 0. | * 700. | * 1788. | * .22 | * 14. | * 26.8 | * F | * 17.7 | * 14.7 | |
| * 13 | * 3 | * 800. | * 0. | * 0. | * 3103. | * 0. | * 0. | * 1154. | * 4400. | * 0. | * 800. | * 1788. | * .26 | * 14. | * 26.5 | * F | * 17.2 | * 15.1 | |
| * 14 | * 3 | * 1400. | * 0. | * 174. | * 3103. | * 0. | * 164. | * 1154. | * 4377. | * 0. | * 1400. | * 1788. | * .26 | * 12. | * 31.3 | * F | * 16.6 | * 15.5 | |
| * 15 | * 2 | * 1400. | * 0. | * 0. | * 2929. | * 0. | * 0. | * 990. | * 4000. | * 0. | * 1400. | * 1788. | * .25 | * 10. | * 48.8 | * F | * 16.1 | * 15.9 | |
| * 16 | * 2 | * 1500. | * 0. | * 477. | * 2929. | * 0. | * 451. | * 990. | * 3910. | * 0. | * 1500. | * 1788. | * .25 | * 9. | * 56.7 | * F | * 15.4 | * 16.6 | |
| * 17 | * 2 | * 1500. | * 0. | * 0. | * 2452. | * 0. | * 0. | * 539. | * 4000. | * 0. | * 1500. | * 1788. | * .13 | * 5. | * 54.5 | * F | * 15.8 | * 16.2 | |
| * 18 | * 2 | * 5000. | * 0. | * 0. | * 2452. | * 0. | * 0. | * 539. | * 4000. | * 0. | * 5000. | * 1788. | * .13 | * 3. | * 87.6 | * F | * 13.8 | * 18.3 | |
| * 19 | * 2 | * 5000. | * 861. | * 0. | * 3313. | * 861. | * 0. | * 1400. | * 4000. | * 0. | * 5000. | * 1788. | * .35 | * 4. | * 169.8 | * F | * 9.4 | * 25.7 | |
| * 20 | * 3 | * 750. | * 1100. | * 4413. | * 4413. | * 1100. | * 2500. | * 2500. | * 2500. | * 0. | * 0. | * 1.00 | * 62. | * 13.4 | * E | * 20.3 | * 13.0 | | |
| * TOTAL | 136889. | = | 25.9 | MI LBS | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | |

FREWAY TRAVEL TIME = CURRENT TIME SLICE CUMULATIVE VALUES
1984. VEH-HRS 2304. PASS-HRS 1984. VEH-HRS 2304. PASS-HRS

SR-237_EB_PM_NP_2040_PE

| | | | | | | | | |
|----------------------------|--------|------------|--------|----------|--------|------------|--------|----------|
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 100. | VEH-HRS | 100. | PASS-HRS | 100. | VEH-HRS | 100. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 2084. | VEH-HRS | 2404. | PASS-HRS | 2084. | VEH-HRS | 2404. | PASS-HRS |
| TOTAL TRAV DISTANCE = | 63737. | VEH-MI. | 77590. | PASS-MI. | 63737. | VEH-MI. | 77590. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 31. | MPH | | | 32. | MPH | | |
| AVERAGE DENSITY = | 24. | VPMP | | | 24. | VPMP | | |
| TOTAL FUEL = | 3317. | GALLONS | | | 3317. | GALLONS | | |
| TOTAL EMISSIONS = | 879. | KI LOGRAMS | | | 879. | KI LOGRAMS | | |

***** MAINTENANCE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|--------|------------|--------|------------|-------|
| 1 | 0.19 | 2 | 37.50 | 3 | 3.33 | 4 | 0.14 | 5 | 0.12 |
| 6 | 0.14 | 7 | 0.27 | 8 | 0.32 | 9 | 2.76 | 10 | 6.42 |
| 11 | 33.44 | 12 | 18.18 | 13 | 19.97 | 14 | 41.36 | 15 | 46.05 |
| 16 | 55.64 | 17 | 74.28 | 18 | 324.70 | 19 | 338.27 | 20 | 0.26 |

***** TOTAL DELAY = 1003.3 VEH-HRS ***** AVERAGE DELAY = 74.02 MIN/VEH *****

***** RAMP DELAYS *****

| | | QUEUE LENGTH | DELAY | AVERAGE | GAS | HC | CO | NOX | TOTAL |
|---------|---|--------------|---------|----------|------|-------|------|------|-----------|
| | | VEHICLES | VEH-HRS | METERING | GALS | KGMS | KGMS | KGMS | EMISSIONS |
| | | | | DELAYS | | | | | KGMS |
| ON-RAMP | 2 | RAMP | 100. | 50.00 | 3.43 | 18.03 | 1.11 | 5.83 | 7.25 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 50.00 | 3.43 | 18.03 | 1.11 | 5.83 | 7.25 |
| ON-RAMP | 4 | RAMP | 100. | 50.00 | 4.69 | 18.03 | 1.11 | 5.83 | 7.25 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 50.00 | 4.69 | 18.03 | 1.11 | 5.83 | 7.25 |

 ** **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 ** **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN *
 * 1 2 3 4 5 6 7 *
 + * * * * * * * *
 * * * * * * * * *
 + * * * * * * * *
 + * * * * * * * *
 + * * * * * * * *
 + * * * * * * * *
 + * * * * * * * *
 + * * * * * * * *
 + * * * * * * * *
 * * * * * * * * *

 * *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 * *

| * SUB | * NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | |
|-------|-------|----------|------------|-----------|------------|---------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|-----|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * ORG | * DES | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | |
| * 1 | * 3 | * 500. | * 3011. | * 0. | * 3011. | * 3011. | * 0. | * 0. | * 0. | * .50 | * 62. | * 16.2 | * B | * 20.3 | * 13.0 | |
| * 2 | * 3 | * 99999. | * 0. | * 783. | * 3011. | * 0. | * 783. | * 3011. | * 6000. | * 0. | * 0. | * .50 | * 62. | * 16.2 | * B | |
| * 3 | * 2 | * 12000. | * 0. | * 0. | * 2228. | * 0. | * 0. | * 1273. | * 4000. | * 0. | * ** | * 10266. | * .32 | * 11. | * 57.5 | * F |
| * 4 | * 3 | * 350. | * 1053. | * 0. | * 3281. | * 900. | * 0. | * 2173. | * 4803. | * 0. | * ** | * 350. | * .45 | * 6. | * 115.4 | * F |
| * 5 | * 3 | * 300. | * 0. | * 0. | * 3281. | * 0. | * 0. | * 2173. | * 5010. | * 0. | * ** | * 300. | * .43 | * 6. | * 127.7 | * F |
| * 6 | * 3 | * 350. | * 0. | * 825. | * 3281. | * 0. | * 782. | * 2173. | * 4825. | * 0. | * ** | * 350. | * .45 | * 6. | * 125.4 | * F |
| * 7 | * 2 | * 940. | * 0. | * 0. | * 2456. | * 0. | * 0. | * 1392. | * 4000. | * 0. | * ** | * 940. | * .35 | * 4. | * 183.3 | * F |

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Table with 14 columns: Lane, Volume, Delay, etc. Rows 8-20 showing traffic data for various lanes.

TOTAL 136889. = 25.9 MI LES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 25. 44.5 17.4 15.1

Summary table with columns: CURRENT TIME SLICE, CUMULATIVE VALUES. Rows for FREeway TRAVEL TIME, MERGE DELAY, etc.

1 INSTITUTE OF TRANSPORTATION STUDIES UNIVERSITY OF CALIFORNIA, BERKELEY FREQ12PE REL 3.01 3/30/2016 10: 6 PAGE 9 SIMULATION AFTER CONTROL, NO DIVERSION TIME SLICE 2 OF 3

Table with columns: SUBSECTION, DELAY. Rows 1-16 showing mainline delay data. Summary: TOTAL DELAY = 1794.4 VEH-HRS AVERAGE DELAY = 57.52 MIN/VEH

Table with columns: QUEUE LENGTH, DELAY, AVERAGE METERING DELAY, GAS GALS, HC KGMS, CO KGMS, NOX KGMS, TOTAL EMISSIONS KGMS. Rows for ON-RAMP 2 and ON-RAMP 4.

1 INSTITUTE OF TRANSPORTATION STUDIES UNIVERSITY OF CALIFORNIA, BERKELEY FREQ12PE REL 3.01 3/30/2016 10: 6 PAGE 10 SIMULATION AFTER CONTROL, NO DIVERSION TIME SLICE 3 OF 3

FREeway TRAVEL TIME (MI NUTES)

Table with columns: ORIGINS DOWN, DESTINATIONS ACROSS. Rows 1-6 showing travel time matrices between origins and destinations.

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS | | |
|--|--------|----------|----------|------------------|----------|----------|---------|---------|--------|-------|---------|-------|-------|--------|------|------|
| SEC LNS | LENGTH | ORG DES | SSEC | ORG DES SSEC | CAP. | EFF | LENGTH | RATE | RATIO | MPH | VPMP | LEVEL | MPG | GS/VM | | |
| 1 | 3 | 500. | 2260. | 0. 2260. | 2260. | 0. | 0. | 0. | .38 | 62. | 12.2 | B | 20.3 | 13.0 | | |
| 2 | 3 | 99999. | 0. 588. | 2260. | 0. 588. | 2035. | 6000. | 0. * | 872. | 225. | .34 | 60. | 11.3 | F | 20.3 | 13.1 |
| 3 | 2 | 12000. | 0. 0. | 1672. | 0. 0. | 1447. | 4000. | 0. ** | 12000. | 225. | .36 | 4. | 196.7 | F | 8.6 | 28.1 |
| 4 | 3 | 350. | 817. | 0. 2489. | 900. | 0. 2347. | 4856. | 0. ** | 350. | 225. | .48 | 5. | 145.0 | F | 8.6 | 28.4 |
| 5 | 3 | 300. | 0. 0. | 2489. | 0. 0. | 2347. | 5010. | 0. ** | 300. | 225. | .47 | 5. | 152.3 | F | 8.4 | 28.7 |
| 6 | 3 | 350. | 0. 679. | 2489. | 0. 700. | 2347. | 4859. | 0. ** | 350. | 225. | .48 | 5. | 145.2 | F | 8.6 | 28.4 |
| 7 | 2 | 940. | 0. 0. | 1810. | 0. 0. | 1648. | 4000. | 0. ** | 940. | 225. | .41 | 4. | 194.8 | F | 8.3 | 28.9 |
| 8 | 3 | 700. | 1151. | 0. 2961. | 1151. | 0. 2799. | 5077. | 0. ** | 700. | 225. | .55 | 7. | 139.1 | F | 9.5 | 26.8 |
| 9 | 3 | 700. | 0. 0. | 2961. | 0. 0. | 2799. | 5330. | 0. ** | 700. | 225. | .53 | 6. | 151.1 | F | 9.1 | 27.5 |
| 10 | 3 | 700. | 0. 391. | 2961. | 0. 400. | 2799. | 5279. | 0. ** | 700. | 225. | .53 | 6. | 148.7 | F | 9.2 | 27.4 |
| 11 | 2 | 2300. | 0. 0. | 2570. | 0. 0. | 2399. | 4000. | 0. ** | 2300. | 225. | .60 | 8. | 153.9 | F | 10.4 | 25.5 |
| 12 | 3 | 700. | 571. | 0. 3141. | 571. | 0. 2970. | 5201. | 0. ** | 700. | 225. | .57 | 7. | 138.8 | F | 9.8 | 26.3 |
| 13 | 3 | 800. | 0. 0. | 3141. | 0. 0. | 2970. | 4400. | 0. ** | 800. | 225. | .67 | 10. | 100.8 | F | 12.7 | 23.1 |
| 14 | 3 | 1400. | 0. 254. | 3141. | 0. 257. | 2970. | 4373. | 0. ** | 1400. | 225. | .68 | 10. | 99.5 | F | 12.9 | 23.0 |
| 15 | 2 | 1400. | 0. 0. | 2887. | 0. 0. | 2712. | 4000. | 0. ** | 1400. | 225. | .68 | 10. | 136.8 | F | 12.9 | 23.0 |
| 16 | 2 | 1500. | 0. 514. | 2887. | 0. 518. | 2712. | 3919. | 0. ** | 1500. | 225. | .69 | 10. | 131.0 | F | 13.2 | 22.6 |
| 17 | 2 | 1500. | 0. 391. | 2373. | 0. 390. | 2194. | 3892. | 0. ** | 1500. | 225. | .56 | 7. | 157.3 | F | 9.7 | 26.5 |
| 18 | 2 | 5000. | 0. 0. | 1982. | 0. 0. | 1804. | 4000. | 0. ** | 5000. | 225. | .45 | 5. | 186.3 | F | 8.3 | 28.9 |
| 19 | 2 | 5000. | 696. | 0. 2678. | 696. | 0. 2500. | 4000. | 0. ** | 5000. | 225. | .63 | 8. | 148.4 | F | 11.0 | 24.8 |
| 20 | 3 | 750. | 0. 2678. | 2678. | 0. 2500. | 2500. | 2500. | 0. 0. | 0. | 1.00 | 62. | 13.4 | E | 20.3 | 13.0 | |
| ***** | | | | | | | | | | | | | | | | |
| * TOTAL 136889. = 25.9 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 18. 51.9 16.1 16.3 * | | | | | | | | | | | | | | | | |
| ***** | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 3133. VEH-HRS | 8017. VEH-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 312. VEH-HRS | 688. VEH-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 3444. VEH-HRS | 8705. VEH-HRS |
| TOTAL TRAVEL DISTANCE = | 57390. VEH-MI. | 193044. VEH-MI. |
| AVERAGE SYSTEM SPEED = | 17. MPH | 24. MPH |
| AVERAGE DENSITY = | 52. VPMP | 40. VPMP |
| TOTAL FUEL = | 3677. GALLONS | 11225. GALLONS |
| TOTAL EMISSIONS = | 981. KI LOGRAMS | 2986. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|--------|------------|-------|------------|--------|------------|--------|------------|-------|
| 1 | 0.16 | 2 | 53.51 | 3 | 848.56 | 4 | 26.45 | 5 | 23.92 |
| 6 | 26.48 | 7 | 64.84 | 8 | 49.63 | 9 | 54.40 | 10 | 53.44 |
| 11 | 117.99 | 12 | 49.15 | 13 | 38.91 | 14 | 67.07 | 15 | 61.48 |
| 16 | 62.60 | 17 | 79.81 | 18 | 326.51 | 19 | 244.57 | 20 | 0.26 |

***** TOTAL DELAY = 2249.7 VEH-HRS ***** AVERAGE DELAY = 72.21 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH | DELAY | AVERAGE | GAS | HC | CO | NOX | TOTAL |
|-----------|--------------|---------|----------|-------|------|-------|------|-----------|
| | VEHICLES | VEH-HRS | METERING | GALS | KGMS | KGMS | KGMS | EMISSIONS |
| | | | DELAY | | | | | KGMS |
| ON-RAMP 2 | RAMP | 170. | 11.86 | 76.27 | 4.71 | 24.66 | 1.31 | 30.68 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 170. | 11.86 | 76.27 | 4.71 | 24.66 | 1.31 | 30.68 |
| ON-RAMP 4 | RAMP | 100. | 8.94 | 36.06 | 2.23 | 11.66 | 0.62 | 14.51 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 8.94 | 36.06 | 2.23 | 11.66 | 0.62 | 14.51 |

```

FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFFFFFFFF RRRRRRRR EEEEEEE QQQ QQQQ 1111 222 PPPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 2222 PPPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*QQ 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 11111111 222222222 PPP LLLLLLLLLL

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FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 3 AND 18 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 62
LOWER LIMB (AT V/C=1) = 30
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

```

*****
**
**                                     FREeway AND ARTERIAL DESIGN FEATURES
**
*****
** SUB NO.  SSEC  SSEC  DESIGN  ORG  TRK  SSEC PCT  PCT DES  SPECIAL  FF. SPD.  CAP.  ART  GRADE  SUBSECTI ON LOCATI ON
** SEC  LNS  CAP  LENGTH  SPEED  DES  FAC  GRAD TRK  TRUCKS  RAMP    ALT. RTE  ALT. RTE  TYPE ALT. RTE
**
** 1
** 2
** 3  1  1650.  12000.  62    0  0.95  0.0 0  100    NO    0.0    0.  GOOD  0.0  HOV Dummy
** 4  1  1650.   350.  62    0  0.95  0.0 0  100    YES   0.0    0.  GOOD  0.0  Maude On-ramp
** 5  1  1650.   300.  62    0  0.95  0.0 0  100    YES   0.0    0.  GOOD  0.0  Maude to US-101
** 6  1  1650.   350.  62    D  0.95  0.0 0  100    YES   0.0    0.  GOOD  0.0  US-101 Off-Ramp
** 7  1  1650.   940.  62    0  0.95  0.0 0  100    NO    0.0    0.  GOOD  0.0  US101SB / US101SB
** 8  1  1650.   700.  62    0  0.95  0.0 0  100    YES   0.0    0.  GOOD  0.0  US101 SB On-ramp
** 9  1  1650.   700.  62    0  0.95  0.0 0  100    YES   0.0    0.  GOOD  0.0  US 101 / Mathilda
** 10 1  1650.   700.  62    D  0.95  0.0 0  100    YES   0.0    0.  GOOD  0.0  Mathilda Off-ramp
** 11 1  1650.  2300.  62    0  0.95  0.0 0  100    NO    0.0    0.  GOOD  0.0  Mathilda / Mathilda
** 12 1  1650.   700.  62    0  0.95  0.0 0  100    YES   0.0    0.  GOOD  0.0  Mathilda On-Ramp
** 13 1  1650.   800.  62    0  0.95  0.0 0  100    YES   0.0    0.  GOOD  0.0  Mathilda / Persian HOV
** 14 1  1650.  1400.  62    D  0.95  0.0 0  100    NO    0.0    0.  GOOD  0.0  Persian On-Ramp w/HOV
** 15 1  1650.  1400.  62    0  0.95  0.0 0  100    NO    0.0    0.  GOOD  0.0  West of Lawrence E
** 16 1  1650.  1500.  62    D  0.95  0.0 0  100    NO    0.0    0.  GOOD  0.0  Lawrence Off-ramp
** 17 1  1650.  1500.  62    D  0.95  0.0 0  100    NO    0.0    0.  GOOD  0.0  End of DKS
** 18 1  1650.  5000.  62    D  0.95  0.0 0  100    NO    0.0    0.  GOOD  0.0  HOV Dummy

```

** 19 **
 ** 20 **

 ** FREeway TRAVEL TIME (MINUTES) **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|-------|-----------------------|------|------|------|------|------|------|------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| + | * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 2 * | 0.00 | 2.38 | 2.94 | 3.89 | 4.42 | 4.70 | 5.62 | 0.00 |
| + | * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 2.23 | 2.50 | 3.42 | 0.00 |
| + | * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.14 | 3.06 | 0.00 |
| + | * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.25 | 0.00 |
| + | * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | | |
|-----------|--------|------------|-----------|--------------------|---------|---------|-----------|-----------|---------|-----------------|-----------|----------------|--------|-------------|------|---|------|------|
| * SEC | * LNS | * LENGTH | * ORG DES | * ORG DES | * CAP | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | | | |
| * 1 | | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | | |
| * 3 | 1 | 12000. | 692. | 0. | 692. | 692. | 0. | 692. | 1650. | 0. | 0. | 0. | .42 | 62. | 11.2 | B | 21.6 | 12.8 |
| * 4 | 1 | 350. | 175. | 0. | 866. | 175. | 0. | 866. | 1650. | 0. | 0. | 0. | .53 | 62. | 14.0 | B | 21.6 | 12.8 |
| * 5 | 1 | 300. | 0. | 0. | 866. | 0. | 0. | 866. | 1650. | 0. | 0. | 0. | .53 | 62. | 14.0 | B | 21.6 | 12.8 |
| * 6 | 1 | 350. | 0. | 162. | 866. | 0. | 162. | 866. | 1650. | 0. | 0. | 0. | .53 | 62. | 14.0 | B | 21.6 | 12.8 |
| * 7 | 1 | 940. | 0. | 0. | 704. | 0. | 0. | 704. | 1650. | 0. | 0. | 0. | .43 | 62. | 11.4 | B | 21.6 | 12.8 |
| * 8 | 1 | 700. | 163. | 0. | 867. | 163. | 0. | 867. | 1650. | 0. | 0. | 0. | .53 | 62. | 14.0 | B | 21.6 | 12.8 |
| * 9 | 1 | 700. | 0. | 0. | 867. | 0. | 0. | 867. | 1650. | 0. | 0. | 0. | .53 | 62. | 14.0 | B | 21.6 | 12.8 |
| * 10 | 1 | 700. | 0. | 64. | 867. | 0. | 64. | 867. | 1650. | 0. | 0. | 0. | .53 | 62. | 14.0 | B | 21.6 | 12.8 |
| * 11 | 1 | 2300. | 0. | 0. | 803. | 0. | 0. | 803. | 1650. | 0. | 0. | 0. | .49 | 62. | 12.9 | B | 21.6 | 12.8 |
| * 12 | 1 | 700. | 171. | 0. | 974. | 171. | 0. | 974. | 1650. | 0. | 0. | 0. | .59 | 62. | 15.7 | B | 21.6 | 12.8 |
| * 13 | 1 | 800. | 0. | 0. | 974. | 0. | 0. | 974. | 1650. | 0. | 0. | 0. | .59 | 62. | 15.7 | B | 21.6 | 12.8 |
| * 14 | 1 | 1400. | 0. | 23. | 974. | 0. | 23. | 974. | 1650. | 0. | 0. | 0. | .59 | 62. | 15.7 | B | 21.6 | 12.8 |
| * 15 | 1 | 1400. | 0. | 0. | 951. | 0. | 0. | 951. | 1650. | 0. | 0. | 0. | .58 | 62. | 15.3 | B | 21.6 | 12.8 |
| * 16 | 1 | 1500. | 0. | 90. | 951. | 0. | 90. | 951. | 1650. | 0. | 0. | 0. | .58 | 62. | 15.3 | B | 21.6 | 12.8 |
| * 17 | 1 | 1500. | 0. | 0. | 861. | 0. | 0. | 861. | 1650. | 0. | 0. | 0. | .52 | 62. | 13.9 | B | 21.6 | 12.8 |
| * 18 | 1 | 5000. | 0. | 861. | 861. | 0. | 861. | 861. | 1650. | 0. | 0. | 0. | .52 | 62. | 13.9 | B | 21.6 | 12.8 |
| * 19 | | | | | | | | | | | | | | | | | | |
| * 20 | | | | | | | | | | | | | | | | | | |
| * TOTAL | | 30640. | = | 5.8 | MI L ES | | | | | MAX(V/C) = 0.59 | | LOWEST LOS = B | | AVG = 62. | 13.0 | | 21.6 | 12.8 |

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|-----------------------------|--------------------|------------|-------------------|------------|
| FREWAY TRAVEL TIME = | 75. | VEH-HRS | 151. | PASS-HRS |
| FREWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 75. | VEH-HRS | 151. | PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 4673. | VEH-MI. | 9346. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. | MPH. | 62. | MPH. |
| AVERAGE DENSITY = | 13. | VPMP | 13. | VPMP |
| TOTAL FUEL = | 217. | GALLONS | 217. | GALLONS |
| TOTAL EMISSIONS = | 60. | KI LOGRAMS | 60. | KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
1 0.00 2 0.00 3 1.17 4 0.04 5 0.04
6 0.04 7 0.09 8 0.09 9 0.09 10 0.09
11 0.26 12 0.10 13 0.11 14 0.19 15 0.19
16 0.20 17 0.18 18 0.61 19 0.00 20 0.00
***** TOTAL DELAY = 3.5 VEH-HRS ***** AVERAGE DELAY = 0.26 MIN/VEH *****

**
** FREEWAY TRAVEL TIME (MINUTES) **
**

* ORIGINS DESTINATIONS ACROSS *
* DOWN 1 2 3 4 5 6 7 8 *
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 2 * 0.00 2.38 2.94 3.89 4.42 4.70 5.62 0.00 *
+
* 3 * 0.00 0.00 0.00 0.00 2.23 2.50 3.42 0.00 *
+
* 4 * 0.00 0.00 0.00 0.00 0.00 2.14 3.06 0.00 *
+
* 5 * 0.00 0.00 0.00 0.00 0.00 0.00 2.25 0.00 *
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
* *

* TIME SLICE FREEWAY PERFORMANCE TABLE *

* SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMISS *
* SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP EFF LENGTH RATE RATIO MPH VPMPL LEVEL LEVEL MPG GS/VM *
* 1 *
* 2 *
* 3 1 12000. 783. 0. 783. 783. 0. 783. 1650. 0. 0. 0. .47 62. 12.6 B 21.6 12.8 *
* 4 1 350. 207. 0. 990. 207. 0. 990. 1650. 0. 0. 0. .60 62. 16.0 B 21.6 12.8 *
* 5 1 300. 0. 0. 990. 0. 0. 990. 1650. 0. 0. 0. .60 62. 16.0 B 21.6 12.8 *
* 6 1 350. 0. 185. 990. 0. 185. 990. 1650. 0. 0. 0. .60 62. 16.0 B 21.6 12.8 *
* 7 1 940. 0. 0. 804. 0. 0. 804. 1650. 0. 0. 0. .49 62. 13.0 B 21.6 12.8 *
* 8 1 700. 257. 0. 1061. 257. 0. 1061. 1650. 0. 0. 0. .64 62. 17.1 B 21.6 12.8 *
* 9 1 700. 0. 0. 1061. 0. 0. 1061. 1650. 0. 0. 0. .64 62. 17.1 B 21.6 12.8 *
* 10 1 700. 0. 69. 1061. 0. 69. 1061. 1650. 0. 0. 0. .64 62. 17.1 B 21.6 12.8 *
* 11 1 2300. 0. 0. 992. 0. 0. 992. 1650. 0. 0. 0. .60 62. 16.0 B 21.6 12.8 *
* 12 1 700. 158. 0. 1150. 158. 0. 1150. 1650. 0. 0. 0. .70 62. 18.5 C 21.6 12.8 *
* 13 1 800. 0. 0. 1150. 0. 0. 1150. 1650. 0. 0. 0. .70 62. 18.5 C 21.6 12.8 *
* 14 1 1400. 0. 34. 1150. 0. 34. 1150. 1650. 0. 0. 0. .70 62. 18.5 C 21.6 12.8 *
* 15 1 1400. 0. 0. 1116. 0. 0. 1116. 1650. 0. 0. 0. .68 62. 18.0 B 21.6 12.8 *
* 16 1 1500. 0. 98. 1116. 0. 98. 1116. 1650. 0. 0. 0. .68 62. 18.0 B 21.6 12.8 *
* 17 1 1500. 0. 107. 1018. 0. 107. 1018. 1650. 0. 0. 0. .62 62. 16.4 B 21.6 12.8 *
* 18 1 5000. 0. 911. 911. 0. 911. 911. 1650. 0. 0. 0. .55 62. 14.7 B 21.6 12.8 *
* 19 *
* 20 *
*
* TOTAL 30640. = 5.8 MI LES MAX(V/C) = 0.70 LOWEST LOS = C AVG = 62. 14.9 21.6 12.8 *

SR-237_EB_PM_NP_2040_PL

FREWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
 ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
 OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
 TOTAL SYSTEM TRAVEL TIME = 86. VEH-HRS 173. PASS-HRS 162. VEH-HRS 324. PASS-HRS
 TOTAL FRWAY TRAV DISTANCE = 5360. VEH-MI. 10719. PASS-MI. 10033. VEH-MI. 20066. PASS-MI.
 AVERAGE SYSTEM SPEED = 62. MPH. 62. MPH.
 AVERAGE DENSITY = 15. VPMP 14. VPMP
 TOTAL FUEL = 249. GALLONS 466. GALLONS
 TOTAL EMISSIONS = 68. KILOGRAMS 128. KILOGRAMS

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/30/2016 10: 6 PAGE 8
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 3

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
 SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
 1 0.00 2 0.00 3 1.32 4 0.05 5 0.04
 6 0.05 7 0.11 8 0.10 9 0.10 10 0.10
 11 0.32 12 0.11 13 0.13 14 0.23 15 0.22
 16 0.24 17 0.22 18 0.64 19 0.00 20 0.00
 ***** TOTAL DELAY = 4.0 VEH-HRS ***** AVERAGE DELAY = 0.26 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/30/2016 10: 6 PAGE 9
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 3 OF 3

 **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 **

| ***** | | | | | | | | | |
|-----------|---------------------|------|------|------|------|------|------|------|------|
| * ORIGINS | DESTINATIONS ACROSS | | | | | | | | * |
| * DOWN | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | * |
| + * | ***** | | | | | | | | |
| + * | ***** | | | | | | | | |
| + * | 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + * | 2 * | 0.00 | 2.38 | 2.94 | 3.89 | 4.42 | 4.70 | 5.62 | 0.00 |
| + * | 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 2.23 | 2.50 | 3.42 | 0.00 |
| + * | 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.14 | 3.06 | 0.00 |
| + * | 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.25 | 0.00 |
| + * | 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + * | 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + * | ***** | | | | | | | | |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/30/2016 10: 6 PAGE 10
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 3 OF 3

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | | |
|-----------|--------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|-------|----------|-----------|---------|--------|-------------|---------|-------|---------|--|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | |
| * 1 | | | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | | | |
| * 3 | 1 | 12000. | 588. | 0. | 588. | 588. | 0. | 588. | 1650. | 0. | 0. | 0. | .36 | 62. | 9.5 | A | 21.6 | 12.8 | |
| * 4 | 1 | 350. | 154. | 0. | 742. | 154. | 0. | 742. | 1650. | 0. | 0. | 0. | .45 | 62. | 12.0 | B | 21.6 | 12.8 | |
| * 5 | 1 | 300. | 0. | 0. | 742. | 0. | 0. | 742. | 1650. | 0. | 0. | 0. | .45 | 62. | 12.0 | B | 21.6 | 12.8 | |
| * 6 | 1 | 350. | 0. | 151. | 742. | 0. | 151. | 742. | 1650. | 0. | 0. | 0. | .45 | 62. | 12.0 | B | 21.6 | 12.8 | |
| * 7 | 1 | 940. | 0. | 0. | 591. | 0. | 0. | 591. | 1650. | 0. | 0. | 0. | .36 | 62. | 9.5 | A | 21.6 | 12.8 | |
| * 8 | 1 | 700. | 253. | 0. | 844. | 253. | 0. | 844. | 1650. | 0. | 0. | 0. | .51 | 62. | 13.6 | B | 21.6 | 12.8 | |
| * 9 | 1 | 700. | 0. | 0. | 844. | 0. | 0. | 844. | 1650. | 0. | 0. | 0. | .51 | 62. | 13.6 | B | 21.6 | 12.8 | |
| * 10 | 1 | 700. | 0. | 51. | 844. | 0. | 51. | 844. | 1650. | 0. | 0. | 0. | .51 | 62. | 13.6 | B | 21.6 | 12.8 | |
| * 11 | 1 | 2300. | 0. | 0. | 794. | 0. | 0. | 794. | 1650. | 0. | 0. | 0. | .48 | 62. | 12.8 | B | 21.6 | 12.8 | |
| * 12 | 1 | 700. | 119. | 0. | 912. | 119. | 0. | 912. | 1650. | 0. | 0. | 0. | .55 | 62. | 14.7 | B | 21.6 | 12.8 | |
| * 13 | 1 | 800. | 0. | 0. | 912. | 0. | 0. | 912. | 1650. | 0. | 0. | 0. | .55 | 62. | 14.7 | B | 21.6 | 12.8 | |
| * 14 | 1 | 1400. | 0. | 27. | 912. | 0. | 27. | 912. | 1650. | 0. | 0. | 0. | .55 | 62. | 14.7 | B | 21.6 | 12.8 | |
| * 15 | 1 | 1400. | 0. | 0. | 885. | 0. | 0. | 885. | 1650. | 0. | 0. | 0. | .54 | 62. | 14.3 | B | 21.6 | 12.8 | |
| * 16 | 1 | 1500. | 0. | 81. | 885. | 0. | 81. | 885. | 1650. | 0. | 0. | 0. | .54 | 62. | 14.3 | B | 21.6 | 12.8 | |
| * 17 | 1 | 1500. | 0. | 108. | 804. | 0. | 108. | 804. | 1650. | 0. | 0. | 0. | .49 | 62. | 13.0 | B | 21.6 | 12.8 | |
| * 18 | 1 | 5000. | 0. | 696. | 696. | 0. | 696. | 696. | 1650. | 0. | 0. | 0. | .42 | 62. | 11.2 | B | 21.6 | 12.8 | |
| * 19 | | | | | | | | | | | | | | | | | | | |
| * 20 | | | | | | | | | | | | | | | | | | | |

 * TOTAL 30640. = 5.8 MILES MAX(V/C) = 0.55 LOWEST LOS = B AVG = 62. 11.5 21.6 12.8 *

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|-----------------------------|--------------------|----------------|-------------------|-----------------|
| FREEWAY TRAVEL TIME = | 67. VEH-HRS | 133. PASS-HRS | 229. VEH-HRS | 457. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 67. VEH-HRS | 133. PASS-HRS | 229. VEH-HRS | 457. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 4138. VEH-MI. | 8277. PASS-MI. | 14171. VEH-MI. | 28342. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | | 62. MPH. | |
| AVERAGE DENSITY = | 12. VPMP/L | | 13. VPMP/L | |
| TOTAL FUEL = | 192. GALLONS | | 658. GALLONS | |
| TOTAL EMISSIONS = | 53. KILOGRAMS | | 181. KILOGRAMS | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.99 | 4 | 0.04 | 5 | 0.03 |
| 6 | 0.04 | 7 | 0.08 | 8 | 0.08 | 9 | 0.08 | 10 | 0.08 |
| 11 | 0.26 | 12 | 0.09 | 13 | 0.10 | 14 | 0.18 | 15 | 0.17 |
| 16 | 0.19 | 17 | 0.17 | 18 | 0.49 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 3.1 VEH-HRS ***** AVERAGE DELAY = 0.26 MIN/VEH *****

```

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQQ QQQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP EEEEEEEEE
    
```

FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 62
LOWER LIMB (AT V/C=1) = 30
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREWAY AND ARTERIAL DESIGN FEATURES

| ** SUB NO. | ** SSEC | ** SSEC | ** DESIG N | ** ORG | ** TRK | ** SSEC | ** PCT | ** PCT | ** DES | ** SPECIAL | ** FF. SPD. | ** CAP. | ** ART | ** GRADE | ** SUBSECTI ON | ** LOCATI ON |
|------------|---------|---------|------------|----------|--------|---------|--------|-----------|---------|-------------|-------------|---------|-------------|-------------|------------------------|--------------|
| ** SEC | ** LNS | ** CAP | ** LENGTH | ** SPEED | ** DES | ** GRAD | ** TRK | ** TRUCKS | ** RAMP | ** ALT. RTE | ** ALT. RTE | ** TYPE | ** ALT. RTE | ** ALT. RTE | ** LOCATION | ** LOCATION |
| ** 1 | 3 | 6000. | 500. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Seeding | ** |
| ** 2 | 3 | 6000. | 99999. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | ** |
| ** 3 | 2 | 4000. | 12000. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | ** |
| ** 4 | 3 | 5010. | 350. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Maude On-ramp | ** |
| ** 5 | 3 | 5010. | 300. | 62 | | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Maude to US-101 | ** |
| ** 6 | 3 | 5010. | 350. | 62 | D | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US-101 Off-Ramp | ** |
| ** 7 | 2 | 4000. | 940. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | US101SB / US101SB | ** |
| ** 8 | 3 | 5330. | 700. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US101 SB On-ramp | ** |
| ** 9 | 3 | 5330. | 700. | 62 | | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US 101 / Mathilda | ** |
| ** 10 | 3 | 5330. | 700. | 62 | D | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-ramp | ** |
| ** 11 | 2 | 4000. | 2300. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | ** |
| ** 12 | 3 | 5320. | 700. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda On-Ramp | ** |
| ** 13 | 3 | 4400. | 800. | 62 | | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda / Persian HOV | ** |
| ** 14 | 3 | 4400. | 1400. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Persian On-Ramp w/HOV | ** |
| ** 15 | 2 | 4000. | 1400. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | West of Lawrence E | ** |
| ** 16 | 2 | 4000. | 1500. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence Off-ramp | ** |
| ** 17 | 2 | 4000. | 1500. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End of DKS | ** |
| ** 18 | 2 | 4000. | 5000. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | ** |
| ** 19 | 2 | 4000. | 5000. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Enter SSec Description | ** |
| ** 20 | 3 | 2500. | 750. | 62 | OD | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | End of the network | ** |

***** INPUT HAS BEEN COMPLETED *****

MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 2 IN TIME SLICE 2
--- THE MAXIMUM METERING RATE WILL PREVAIL.

MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 2 IN TIME SLICE 3
--- THE MAXIMUM METERING RATE WILL PREVAIL.

**
** FREEWAY TRAVEL TIME (MINUTES) **
**

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | |
|-----------|--|-----------------------|-------|-------|-------|-------|-------|-------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | | 18.42 | 20.80 | 21.42 | 24.50 | 27.44 | 30.61 | 61.73 |
| * 2 * | | 0.00 | 0.18 | 0.80 | 3.88 | 6.83 | 10.00 | 41.11 |
| * 3 * | | 0.00 | 0.00 | 0.45 | 3.53 | 6.47 | 9.64 | 40.75 |
| * 4 * | | 0.00 | 0.00 | 0.00 | 2.01 | 4.96 | 8.13 | 39.24 |
| * 5 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 13.81 |
| * 6 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.14 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | |
|-----------|--------|------------|-----------|------------|-----------|---------|---------|-----------|-----------|---------|---------|-----------|---------|---------|-------------|--------|--------|
| * SEC | * LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * SSEC | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | |
| * 1 | * 3 | * 500. | * 2661. | * 0. | * 2661. | * 2661. | * 0. | * 2661. | * 6000. | * 0. | * 0. | * .44 | * 62. | * 14.3 | * B | * 20.3 | * 13.0 |
| * 2 | * 3 | * 99999. | * 0. | * 692. | * 2661. | * 0. | * 692. | * 2661. | * 6000. | * 0. | * 0. | * .44 | * 62. | * 14.3 | * B | * 20.3 | * 13.0 |
| * 3 | * 2 | * 12000. | * 0. | * 0. | * 1969. | * 0. | * 0. | * 1969. | * 4000. | * 0. | * 0. | * .49 | * 62. | * 15.9 | * B | * 20.3 | * 13.0 |
| * 4 | * 3 | * 350. | * 875. | * 0. | * 2844. | * 775. | * 0. | * 2744. | * 4836. | * 0. | * 0. | * .57 | * 62. | * 14.8 | * B | * 20.3 | * 13.0 |
| * 5 | * 3 | * 300. | * 0. | * 0. | * 2844. | * 0. | * 0. | * 2744. | * 5010. | * 0. | * 0. | * .55 | * 62. | * 14.8 | * B | * 20.3 | * 13.0 |
| * 6 | * 3 | * 350. | * 0. | * 708. | * 2844. | * 0. | * 680. | * 2744. | * 4848. | * 0. | * 0. | * .57 | * 62. | * 14.8 | * B | * 20.3 | * 13.0 |
| * 7 | * 2 | * 940. | * 0. | * 0. | * 2136. | * 0. | * 0. | * 2064. | * 4000. | * 0. | * 0. | * .52 | * 62. | * 16.6 | * B | * 20.3 | * 13.0 |
| * 8 | * 3 | * 700. | * 677. | * 0. | * 2813. | * 677. | * 0. | * 2741. | * 5185. | * 0. | * 0. | * .53 | * 62. | * 14.7 | * B | * 20.3 | * 13.0 |
| * 9 | * 3 | * 700. | * 0. | * 0. | * 2813. | * 0. | * 0. | * 1063. | * 5330. | * 0. | * 136. | * .20 | * 61. | * 5.8 | * F | * 20.3 | * 13.1 |
| * 10 | * 3 | * 700. | * 0. | * 347. | * 2813. | * 0. | * 337. | * 1063. | * 5271. | * 0. | * 700. | * .20 | * 42. | * 8.4 | * F | * 20.0 | * 13.3 |
| * 11 | * 2 | * 2300. | * 0. | * 0. | * 2466. | * 0. | * 0. | * 726. | * 4000. | * 0. | * 2300. | * .18 | * 24. | * 14.8 | * F | * 19.3 | * 13.6 |
| * 12 | * 3 | * 700. | * 745. | * 0. | * 3211. | * 645. | * 0. | * 1371. | * 5135. | * 0. | * 700. | * .27 | * 18. | * 25.6 | * F | * 17.8 | * 14.6 |
| * 13 | * 3 | * 800. | * 0. | * 0. | * 3211. | * 0. | * 0. | * 1371. | * 4400. | * 0. | * 800. | * .31 | * 18. | * 25.7 | * F | * 17.3 | * 15.0 |
| * 14 | * 3 | * 1400. | * 0. | * 228. | * 3211. | * 0. | * 215. | * 1371. | * 4371. | * 0. | * 1400. | * .31 | * 15. | * 30.4 | * F | * 16.7 | * 15.5 |
| * 15 | * 2 | * 1400. | * 0. | * 0. | * 2983. | * 0. | * 0. | * 1155. | * 4000. | * 0. | * 1400. | * .29 | * 12. | * 47.8 | * F | * 16.1 | * 15.9 |
| * 16 | * 2 | * 1500. | * 0. | * 619. | * 2983. | * 0. | * 586. | * 1155. | * 3885. | * 0. | * 1500. | * .30 | * 10. | * 55.2 | * F | * 15.4 | * 16.6 |
| * 17 | * 2 | * 1500. | * 0. | * 0. | * 2364. | * 0. | * 0. | * 569. | * 4000. | * 0. | * 1500. | * .14 | * 5. | * 52.9 | * F | * 15.9 | * 16.1 |
| * 18 | * 2 | * 5000. | * 0. | * 0. | * 2364. | * 0. | * 0. | * 569. | * 4000. | * 0. | * 5000. | * .14 | * 3. | * 86.7 | * F | * 13.8 | * 18.3 |
| * 19 | * 2 | * 5000. | * 831. | * 0. | * 3195. | * 831. | * 0. | * 1400. | * 4000. | * 0. | * 5000. | * .35 | * 4. | * 168.4 | * F | * 9.5 | * 25.7 |
| * 20 | * 3 | * 750. | * 1100. | * 4295. | * 4295. | * 1100. | * 2500. | * 2500. | * 2500. | * 0. | * 0. | * 1.00 | * 62. | * 13.4 | * E | * 20.3 | * 13.0 |
| * TOTAL | | 136889. | = | 25.9 | MI LBS | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | |

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                SR-237_EB_PM_P1_2040_PE
FREEWAY MERGE DELAY =      0. VEH-HRS      0. PASS-HRS      0. VEH-HRS      0. PASS-HRS
ON-RAMP MRG/CAP DELAY =  100. VEH-HRS    100. PASS-HRS    100. VEH-HRS    100. PASS-HRS
OFF-RAMP DELAY =        0. VEH-HRS      0. PASS-HRS      0. VEH-HRS      0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 2027. VEH-HRS  2346. PASS-HRS  2027. VEH-HRS  2346. PASS-HRS
TOTAL TRAVEL DISTANCE = 64035. VEH-MI .  77915. PASS-MI .  64035. VEH-MI .  77915. PASS-MI .
AVERAGE SYSTEM SPEED =   32. MPH.          33. MPH.
AVERAGE DENSITY =       24. VPMPPL         24. VPMPPL
TOTAL FUEL =             3332. GALLONS      3332. GALLONS
TOTAL EMISSIONS =       883. KI LOGRAMS     883. KI LOGRAMS

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***** MAINTLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
   1      0.19         2      37.52         3      3.33         4      0.14         5      0.12
   6      0.14         7      0.27         8      0.27         9      0.34        10      2.92
  11     24.54        12     14.64        13     16.43        14     34.77        15     40.04
  16     48.63        17     69.26        18    312.08        19    335.58        20     0.26

***** TOTAL DELAY = 941.5 VEH-HRS ***** AVERAGE DELAY = 65.27 MIN/VEH *****

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***** RAMP DELAYS *****
              QUEUE LENGTH DELAY AVERAGE METERING DELAY GAS HC CO NOX TOTAL
              VEHICLES VEH-HRS MI NUTES GALS KGMS KGMS KGMS EMISSIONS
              KGMS
ON-RAMP  2    RAMP         100.    50.00    3.43    18.03    1.11    5.83    0.31    7.25
              FREEWAY      0.     0.00    0.00    0.00    0.00    0.00    0.00    0.00
              TOTAL       100.    50.00    3.43    18.03    1.11    5.83    0.31    7.25
ON-RAMP  4    RAMP         100.    50.00    4.03    18.03    1.11    5.83    0.31    7.25
              FREEWAY      0.     0.00    0.00    0.00    0.00    0.00    0.00
              TOTAL       100.    50.00    4.03    18.03    1.11    5.83    0.31    7.25

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*****
**
**      FREEWAY TRAVEL TIME (MI NUTES)
**
*****

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```

*****
* ORIGINS DESTINATIONS ACROSS
* DOWN
*      1      2      3      4      5      6      7
+
*
*
+
* 1 * 18.42 30.15 36.95 44.85 48.37 51.30 72.22
+
* 2 * 0.00 1.71 8.51 16.41 19.92 22.86 43.78
+
* 3 * 0.00 0.00 4.35 12.25 15.76 18.70 39.61
+
* 4 * 0.00 0.00 0.00 3.71 7.23 10.17 31.08
+
* 5 * 0.00 0.00 0.00 0.00 0.00 0.00 6.88
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.14
+
*
*
*****

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*
*      TIME SLICE FREEWAY PERFORMANCE TABLE
*
*****

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* SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMI SS
* SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMPPL LEVEL MPG GS/VM
*****
* 1 3 500. 3010. 0. 3010. 3010. 0. 3010. 6000. 0. 0. 0. .50 62. 16.2 B 20.3 13.0
* 2 3 99999. 0. 783. 3010. 0. 783. 3010. 6000. 0. 0. 0. .50 62. 16.2 B 20.3 13.0
* 3 2 12000. 0. 0. 2227. 0. 0. 1312. 4000. 0. 9109. 915. .33 14. 48.2 F 16.1 16.0
* 4 3 350. 1051. 0. 3278. 900. 0. 2212. 4801. 0. 350. 915. .46 7. 103.9 F 10.3 23.8
* 5 3 300. 0. 0. 3278. 0. 0. 2212. 5010. 0. 300. 915. .44 6. 113.3 F 10.1 24.3
* 6 3 350. 0. 825. 3278. 0. 782. 2212. 4825. 0. 350. 915. .46 6. 113.6 F 9.8 24.8
* 7 2 940. 0. 0. 2453. 0. 0. 1430. 4000. 0. 940. 915. .36 4. 164.3 F 9.6 25.4
*****

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SR-237_EB_PM_P1_2040_PE

| | | | | | | | | | | | | | | | | | | | | | |
|---|----|---|-------|-------|-------|-------|-------|-------|-------|-------|----|----|-------|------|------|-----|-------|---|------|------|---|
| * | 8 | 3 | 700. | 1061. | 0. | 3514. | 1061. | 0. | 2491. | 5093. | 0. | ** | 700. | 915. | .49 | 6. | 136.6 | F | 9.2 | 26.7 | * |
| * | 9 | 3 | 700. | 0. | 0. | 3514. | 0. | 0. | 2491. | 5330. | 0. | ** | 700. | 915. | .47 | 5. | 158.2 | F | 8.5 | 28.3 | * |
| * | 10 | 3 | 700. | 0. | 388. | 3514. | 0. | 375. | 2491. | 5272. | 0. | ** | 700. | 915. | .47 | 5. | 159.6 | F | 8.5 | 28.6 | * |
| * | 11 | 2 | 2300. | 0. | 0. | 3126. | 0. | 0. | 2115. | 4000. | 0. | ** | 2300. | 915. | .53 | 6. | 169.3 | F | 9.2 | 27.4 | * |
| * | 12 | 3 | 700. | 812. | 0. | 3938. | 812. | 0. | 2927. | 5146. | 0. | ** | 700. | 915. | .57 | 7. | 137.7 | F | 9.8 | 26.4 | * |
| * | 13 | 3 | 800. | 0. | 0. | 3938. | 0. | 0. | 2927. | 4400. | 0. | ** | 800. | 915. | .67 | 10. | 102.4 | F | 12.3 | 23.5 | * |
| * | 14 | 3 | 1400. | 0. | 337. | 3938. | 0. | 326. | 2927. | 4360. | 0. | ** | 1400. | 915. | .67 | 10. | 100.5 | F | 12.6 | 23.3 | * |
| * | 15 | 2 | 1400. | 0. | 0. | 3601. | 0. | 0. | 2602. | 4000. | 0. | ** | 1400. | 915. | .65 | 9. | 142.8 | F | 11.8 | 24.0 | * |
| * | 16 | 2 | 1500. | 0. | 641. | 3601. | 0. | 632. | 2602. | 3887. | 0. | ** | 1500. | 915. | .67 | 10. | 134.8 | F | 12.5 | 23.3 | * |
| * | 17 | 2 | 1500. | 0. | 395. | 2960. | 0. | 371. | 1970. | 3895. | 0. | ** | 1500. | 915. | .51 | 6. | 169.8 | F | 8.8 | 27.9 | * |
| * | 18 | 2 | 5000. | 0. | 0. | 2565. | 0. | 0. | 1599. | 4000. | 0. | ** | 5000. | 915. | .40 | 4. | 197.4 | F | 8.3 | 28.9 | * |
| * | 19 | 2 | 5000. | 901. | 0. | 3466. | 901. | 0. | 2500. | 4000. | 0. | ** | 5000. | 915. | .63 | 8. | 148.4 | F | 11.0 | 24.8 | * |
| * | 20 | 3 | 750. | 0. | 3466. | 3466. | 0. | 2500. | 2500. | 2500. | 0. | ** | 0. | 0. | 1.00 | 62. | 13.4 | E | 20.3 | 13.0 | * |

| | | | | | | | | | | | | | | | | | | | | | |
|---|-------|---------|---|------|--------|--|--|--|--|--|--|--|-----------------|----------------|-----------|------|--|--|------|------|---|
| * | TOTAL | 136889. | = | 25.9 | MI LES | | | | | | | | MAX(V/C) = 1.00 | LOWEST LOS = F | AVG = 26. | 43.0 | | | 17.6 | 15.0 | * |
|---|-------|---------|---|------|--------|--|--|--|--|--|--|--|-----------------|----------------|-----------|------|--|--|------|------|---|

| CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | | |
|----------------------------|--------|------------|--------|-------------------|---------|------------|---------|----------|
| FREEWAY TRAVEL TIME = | 2807. | VEH-HRS | 3155. | PASS-HRS | 4733. | VEH-HRS | 5400. | PASS-HRS |
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 275. | VEH-HRS | 275. | PASS-HRS | 375. | VEH-HRS | 375. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 3082. | VEH-HRS | 3430. | PASS-HRS | 5109. | VEH-HRS | 5776. | PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 72266. | VEH-MI. | 88111. | PASS-MI. | 136300. | VEH-MI. | 166026. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 23. | MPH | | | 29. | MPH | | |
| AVERAGE DENSITY = | 43. | VPMP/L | | | 34. | VPMP/L | | |
| TOTAL FUEL = | 4216. | GALLONS | | | 7549. | GALLONS | | |
| TOTAL EMISSIONS = | 1126. | KI LOGRAMS | | | 2009. | KI LOGRAMS | | |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 3/30/2016 12:50 PAGE 9
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 3

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|--------|------------|-------|------------|--------|------------|--------|------------|-------|
| 1 | 0.21 | 2 | 42.44 | 3 | 260.33 | 4 | 20.32 | 5 | 19.36 |
| 6 | 21.97 | 7 | 59.63 | 8 | 50.67 | 9 | 58.27 | 10 | 58.38 |
| 11 | 133.33 | 12 | 48.81 | 13 | 39.70 | 14 | 67.97 | 15 | 65.13 |
| 16 | 65.21 | 17 | 87.86 | 18 | 350.64 | 19 | 244.57 | 20 | 0.26 |

***** TOTAL DELAY = 1695.1 VEH-HRS ***** AVERAGE DELAY = 52.67 MIN/VEH *****

***** RAMP DELAYS *****

| | | QUEUE LENGTH | DELAY | AVERAGE | GAS | HC | CO | NOX | TOTAL |
|---------|---|--------------|---------|----------|-------|------|-------|------|-----------|
| | | VEHICLES | VEH-HRS | METERING | GALS | KGMS | KGMS | KGMS | EMISSIONS |
| | | | | DELAYS | | | | | KGMS |
| ON-RAMP | 2 | RAMP | 251. | 9.15 | 63.29 | 3.91 | 20.47 | 1.08 | 25.46 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 251. | 9.15 | 63.29 | 3.91 | 20.47 | 1.08 | 25.46 |
| ON-RAMP | 4 | RAMP | 100. | 6.58 | 36.06 | 2.23 | 11.66 | 0.62 | 14.51 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 6.58 | 36.06 | 2.23 | 11.66 | 0.62 | 14.51 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 3/30/2016 12:50 PAGE 10
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 3 OF 3

 ** **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 ** **

| * ORIGINS | * DESTINATIONS ACROSS | | | | | | | * | |
|-----------|-----------------------|-------|-------|-------|-------|-------|-------|-------|-------|
| * DOWN | 1 | 2 | 3 | 4 | 5 | 6 | 7 | * | |
| + | * | * | * | * | * | * | * | * | |
| + | * 1 * | 18.42 | 52.58 | 58.84 | 65.41 | 68.43 | 70.86 | 89.37 | * |
| + | * 2 * | 0.00 | 2.08 | 8.33 | 14.91 | 17.93 | 20.35 | 38.87 | * |
| + | * 3 * | 0.00 | 0.00 | 3.81 | 10.39 | 13.41 | 15.83 | 34.35 | * |
| + | * 4 * | 0.00 | 0.00 | 0.00 | 3.34 | 6.36 | 8.78 | 27.30 | * |
| + | * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 6.88 | * |
| + | * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.14 | * |
| + | * * | | | | | | | | * |
| + | ***** | | | | | | | | ***** |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | |
|-----------|----------|------------|-----------|--------------------|----------|----------|-----------|-----------------|----------------|-----------|-----------|---------|--------|-------------|------|------|
| * SEC LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP/L | * LEVEL | * MPG | * GS/VM | | |
| * 1 | 3 | 500. | 2261. | 0. 2261. | 2261. | 0. 2261. | 6000. | 0. | 0. | .38 | 62. | 12.2 | B | 20.3 | 13.0 | |
| * 2 | 3 | 99999. | 0. 588. | 2261. | 0. 588. | 2261. | 6000. | 0. | 0. | .38 | 62. | 12.2 | B | 20.3 | 13.0 | |
| * 3 | 2 | 12000. | 0. 0. | 1673. | 0. 0. | 1488. | 4000. | 0. | * 11674. | 185. | .37 | 4. | 175.1 | F | 9.1 | 26.5 |
| * 4 | 3 | 350. | 813. | 0. 2486. | 900. | 0. 2388. | 4854. | 0. | ** 350. | 185. | .49 | 6. | 143.5 | F | 8.7 | 28.2 |
| * 5 | 3 | 300. | 0. 0. | 2486. | 0. 0. | 2388. | 5010. | 0. | ** 300. | 185. | .48 | 5. | 150.9 | F | 8.5 | 28.5 |
| * 6 | 3 | 350. | 0. 679. | 2486. | 0. 701. | 2388. | 4859. | 0. | ** 350. | 185. | .49 | 6. | 143.7 | F | 8.7 | 28.2 |
| * 7 | 2 | 940. | 0. 0. | 1807. | 0. 0. | 1688. | 4000. | 0. | ** 940. | 185. | .42 | 4. | 192.6 | F | 8.3 | 28.9 |
| * 8 | 3 | 700. | 1085. | 0. 2892. | 1085. | 0. 2773. | 5095. | 0. | ** 700. | 185. | .54 | 7. | 140.9 | F | 9.4 | 27.0 |
| * 9 | 3 | 700. | 0. 0. | 2892. | 0. 0. | 2773. | 5330. | 0. | ** 700. | 185. | .52 | 6. | 152.1 | F | 9.0 | 27.6 |
| * 10 | 3 | 700. | 0. 319. | 2892. | 0. 327. | 2773. | 5288. | 0. | ** 700. | 185. | .52 | 6. | 150.1 | F | 9.1 | 27.5 |
| * 11 | 2 | 2300. | 0. 0. | 2573. | 0. 0. | 2445. | 4000. | 0. | ** 2300. | 185. | .61 | 8. | 151.4 | F | 10.7 | 25.2 |
| * 12 | 3 | 700. | 651. | 0. 3224. | 651. | 0. 3096. | 5191. | 0. | ** 700. | 185. | .60 | 8. | 133.7 | F | 10.4 | 25.6 |
| * 13 | 3 | 800. | 0. 0. | 3224. | 0. 0. | 3096. | 4400. | 0. | ** 800. | 185. | .70 | 11. | 96.2 | F | 13.4 | 22.3 |
| * 14 | 3 | 1400. | 0. 290. | 3224. | 0. 295. | 3096. | 4369. | 0. | ** 1400. | 185. | .71 | 11. | 94.8 | F | 13.4 | 22.2 |
| * 15 | 2 | 1400. | 0. 0. | 2934. | 0. 0. | 2802. | 4000. | 0. | ** 1400. | 185. | .70 | 11. | 131.9 | F | 13.3 | 22.4 |
| * 16 | 2 | 1500. | 0. 588. | 2934. | 0. 594. | 2802. | 3907. | 0. | ** 1500. | 185. | .72 | 11. | 125.3 | F | 13.6 | 22.0 |
| * 17 | 2 | 1500. | 0. 394. | 2346. | 0. 393. | 2207. | 3894. | 0. | ** 1500. | 185. | .57 | 7. | 156.8 | F | 9.8 | 26.4 |
| * 18 | 2 | 5000. | 0. 0. | 1952. | 0. 0. | 1814. | 4000. | 0. | ** 5000. | 185. | .45 | 5. | 185.7 | F | 8.3 | 28.9 |
| * 19 | 2 | 5000. | 686. | 0. 2638. | 686. | 0. 2500. | 4000. | 0. | ** 5000. | 185. | .63 | 8. | 148.4 | F | 11.0 | 24.8 |
| * 20 | 3 | 750. | 0. 2638. | 2638. | 0. 2500. | 2500. | 2500. | 0. | 0. | 0. | 1.00 | 62. | 13.4 | E | 20.3 | 13.0 |
| ***** | | | | | | | | | | | | | | | | |
| * TOTAL | 136889. | = | 25.9 | MILES | | | | MAX(V/C) = 1.00 | LOWEST LOS = F | AVG = 19. | 50.4 | | 16.2 | 16.2 | | |
| ***** | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 3004. VEH-HRS | 7737. VEH-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 307. VEH-HRS | 683. VEH-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 3311. VEH-HRS | 8420. VEH-HRS |
| TOTAL TRAVEL DISTANCE = | 57702. VEH-MI. | 194002. VEH-MI. |
| AVERAGE SYSTEM SPEED = | 17. MPH | 25. MPH |
| AVERAGE DENSITY = | 50. VPMP/L | 39. VPMP/L |
| TOTAL FUEL = | 3663. GALLONS | 11212. GALLONS |
| TOTAL EMISSIONS = | 979. KI LOGRAMS | 2988. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|--------|------------|-------|------------|--------|------------|--------|------------|-------|
| 1 | 0.16 | 2 | 31.88 | 3 | 756.19 | 4 | 26.09 | 5 | 23.63 |
| 6 | 26.14 | 7 | 63.96 | 8 | 50.40 | 9 | 54.83 | 10 | 54.04 |
| 11 | 115.47 | 12 | 46.88 | 13 | 36.52 | 14 | 62.75 | 15 | 58.54 |
| 16 | 58.96 | 17 | 79.42 | 18 | 325.33 | 19 | 244.57 | 20 | 0.26 |

***** TOTAL DELAY = 2116.0 VEH-HRS ***** AVERAGE DELAY = 65.94 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH | DELAY | AVERAGE | GAS | HC | CO | NOX | TOTAL |
|-----------|--------------|---------|----------|-------|------|-------|------|-----------|
| | VEHICLES | VEH-HRS | METERING | GALS | KGMS | KGMS | KGMS | EMISSIONS |
| | | | DELAY | | | | | KGMS |
| | | | MINUTES | | | | | |
| ON-RAMP 2 | RAMP | 164. | 11.70 | 74.82 | 4.63 | 24.20 | 1.28 | 30.10 |
| | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 164. | 11.70 | 74.82 | 4.63 | 24.20 | 1.28 | 30.10 |
| ON-RAMP 4 | RAMP | 100. | 7.99 | 36.06 | 2.23 | 11.66 | 0.62 | 14.51 |
| | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 7.99 | 36.06 | 2.23 | 11.66 | 0.62 | 14.51 |

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPPP LLL
FFF RRR RRR EEE QQQQQ QQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 2222 PPPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 11111111 2222222222 PPP LLLLLLLLLL

FREQ12PLB

- A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 3 AND 18 WILL BE SIMULATED.
- SHORT TERM CONSEQUENCES ARE REQUESTED.
- THERE ARE 1.0 TIME SLICES PER HOUR.
- WEAVING ANALYSIS IS NOT ENGAGED.
- NO ALTERNATE ROUTE IS PROVIDED.
- SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 62
LOWER LIMB (AT V/C=1) = 30
- THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
- FUEL DATA ARE SUPPLIED BY THE PROGRAM.
- EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
- NUMBER OF PRIORITY LANES = 1.
- PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

```
*****
**                                     **
**                                FREeway AND ARTERIAL DESIGN FEATURES                               **
**                                **                                             **
*****
** SUB NO.   SSEC   SSEC  DESIG N  ORG   TRK   SSEC PCT   PCT DES  SPECIAL   FF. SPD.   CAP.   ART  GRADE   SUBSECTI ON LOCATI ON   **
** SEC LNS   CAP   LENGTH SPEED   DES   FAC   GRAD TRK   TRUCKS   RAMP   ALT. RTE  ALT. RTE  TYPE  ALT. RTE          **
**            **            **            **            **            **            **            **            **            **            **            **            **
** 1            **            **            **            **            **            **            **            **            **            **            **            **
** 2            **            **            **            **            **            **            **            **            **            **            **            **
** 3  1   1650.   12000. 62    0   0.95   0.0 0   100    NO    0.0    0.   GOOD   0.0   HOV Dummy           **
** 4  1   1650.    350.   62    0   0.95   0.0 0   100    YES   0.0    0.   GOOD   0.0   Maude On-ramp       **
** 5  1   1650.    300.   62        0.95   0.0 0   100    YES   0.0    0.   GOOD   0.0   Maude to US-101    **
** 6  1   1650.    350.   62    D 0.95   0.0 0   100    YES   0.0    0.   GOOD   0.0   US-101 Off-Ramp    **
** 7  1   1650.    940.   62        0.95   0.0 0   100    NO    0.0    0.   GOOD   0.0   US101SB / US101SB  **
** 8  1   1650.    700.   62    0   0.95   0.0 0   100    YES   0.0    0.   GOOD   0.0   US101 SB On-ramp   **
** 9  1   1650.    700.   62        0.95   0.0 0   100    YES   0.0    0.   GOOD   0.0   US 101 / Mathilda **
** 10 1   1650.    700.   62    D 0.95   0.0 0   100    YES   0.0    0.   GOOD   0.0   Mathilda Off-ramp  **
** 11 1   1650.   2300.  62        0.95   0.0 0   100    NO    0.0    0.   GOOD   0.0   Mathilda / Mathilda **
** 12 1   1650.    700.   62    0   0.95   0.0 0   100    YES   0.0    0.   GOOD   0.0   Mathilda On-Ramp   **
** 13 1   1650.    800.   62        0.95   0.0 0   100    YES   0.0    0.   GOOD   0.0   Mathilda / Persian HOV **
** 14 1   1650.   1400.  62    D 0.95   0.0 0   100    NO    0.0    0.   GOOD   0.0   Persian On-Ramp w/HOV **
** 15 1   1650.   1400.  62        0.95   0.0 0   100    NO    0.0    0.   GOOD   0.0   West of Lawrence E  **
** 16 1   1650.   1500.  62    D 0.95   0.0 0   100    NO    0.0    0.   GOOD   0.0   Lawrence Off-ramp   **
** 17 1   1650.   1500.  62    D 0.95   0.0 0   100    NO    0.0    0.   GOOD   0.0   End of DKS          **
** 18 1   1650.   5000.  62    D 0.95   0.0 0   100    NO    0.0    0.   GOOD   0.0   HOV Dummy           **
```

** 19 **
 ** 20 **

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/30/2016 12:50 PAGE 3
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 1 OF 3

 ** FREeway TRAVEL TIME (MINUTES) **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|------|-----------------------|------|------|------|------|------|------|------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| + * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + * 2 * | 0.00 | 2.38 | 2.94 | 3.89 | 4.42 | 4.70 | 5.62 | 0.00 | 0.00 |
| + * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 2.23 | 2.50 | 3.42 | 0.00 | 0.00 |
| + * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.14 | 3.06 | 0.00 | 0.00 |
| + * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.25 | 0.00 | 0.00 |
| + * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/30/2016 12:50 PAGE 4
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 1 OF 3

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | | |
|-----------|--------|------------|-----------|------------|--------|---------|-----------|-----------|-----------------|---------|----------------|---------|-----------|-------------|------|---|------|------|
| * SEC | * LNS | * LENGTH | * ORG DES | * ORG DES | * CAP | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | | | |
| * 1 | | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | | |
| * 3 | 1 | 12000. | 692. | 0. | 692. | 692. | 0. | 692. | 1650. | 0. | 0. | 0. | .42 | 62. | 11.2 | B | 21.6 | 12.8 |
| * 4 | 1 | 350. | 174. | 0. | 866. | 174. | 0. | 866. | 1650. | 0. | 0. | 0. | .52 | 62. | 14.0 | B | 21.6 | 12.8 |
| * 5 | 1 | 300. | 0. | 0. | 866. | 0. | 0. | 866. | 1650. | 0. | 0. | 0. | .52 | 62. | 14.0 | B | 21.6 | 12.8 |
| * 6 | 1 | 350. | 0. | 162. | 866. | 0. | 162. | 866. | 1650. | 0. | 0. | 0. | .52 | 62. | 14.0 | B | 21.6 | 12.8 |
| * 7 | 1 | 940. | 0. | 0. | 704. | 0. | 0. | 704. | 1650. | 0. | 0. | 0. | .43 | 62. | 11.3 | B | 21.6 | 12.8 |
| * 8 | 1 | 700. | 145. | 0. | 849. | 145. | 0. | 849. | 1650. | 0. | 0. | 0. | .51 | 62. | 13.7 | B | 21.6 | 12.8 |
| * 9 | 1 | 700. | 0. | 0. | 849. | 0. | 0. | 849. | 1650. | 0. | 0. | 0. | .51 | 62. | 13.7 | B | 21.6 | 12.8 |
| * 10 | 1 | 700. | 0. | 59. | 849. | 0. | 59. | 849. | 1650. | 0. | 0. | 0. | .51 | 62. | 13.7 | B | 21.6 | 12.8 |
| * 11 | 1 | 2300. | 0. | 0. | 790. | 0. | 0. | 790. | 1650. | 0. | 0. | 0. | .48 | 62. | 12.7 | B | 21.6 | 12.8 |
| * 12 | 1 | 700. | 185. | 0. | 974. | 185. | 0. | 974. | 1650. | 0. | 0. | 0. | .59 | 62. | 15.7 | B | 21.6 | 12.8 |
| * 13 | 1 | 800. | 0. | 0. | 974. | 0. | 0. | 974. | 1650. | 0. | 0. | 0. | .59 | 62. | 15.7 | B | 21.6 | 12.8 |
| * 14 | 1 | 1400. | 0. | 29. | 974. | 0. | 29. | 974. | 1650. | 0. | 0. | 0. | .59 | 62. | 15.7 | B | 21.6 | 12.8 |
| * 15 | 1 | 1400. | 0. | 0. | 946. | 0. | 0. | 946. | 1650. | 0. | 0. | 0. | .57 | 62. | 15.3 | B | 21.6 | 12.8 |
| * 16 | 1 | 1500. | 0. | 115. | 946. | 0. | 115. | 946. | 1650. | 0. | 0. | 0. | .57 | 62. | 15.3 | B | 21.6 | 12.8 |
| * 17 | 1 | 1500. | 0. | 0. | 831. | 0. | 0. | 831. | 1650. | 0. | 0. | 0. | .50 | 62. | 13.4 | B | 21.6 | 12.8 |
| * 18 | 1 | 5000. | 0. | 831. | 831. | 0. | 831. | 831. | 1650. | 0. | 0. | 0. | .50 | 62. | 13.4 | B | 21.6 | 12.8 |
| * 19 | | | | | | | | | | | | | | | | | | |
| * 20 | | | | | | | | | | | | | | | | | | |
| * TOTAL | 30640. | = | 5.8 | MI L ES | | | | | MAX(V/C) = 0.59 | | LOWEST LOS = B | | AVG = 62. | 12.8 | | | 21.6 | 12.8 |

| | CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | |
|-----------------------------|--------------------|------------|-------|----------|-------------------|------------|-------|----------|
| FREWAY TRAVEL TIME = | 75. | VEH-HRS | 149. | PASS-HRS | 75. | VEH-HRS | 149. | PASS-HRS |
| FREWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 75. | VEH-HRS | 149. | PASS-HRS | 75. | VEH-HRS | 149. | PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 4620. | VEH-MI. | 9240. | PASS-MI. | 4620. | VEH-MI. | 9240. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. | MPH. | | | 62. | MPH. | | |
| AVERAGE DENSITY = | 13. | VPMP | | | 13. | VPMP | | |
| TOTAL FUEL = | 214. | GALLONS | | | 214. | GALLONS | | |
| TOTAL EMISSIONS = | 59. | KI LOGRAMS | | | 59. | KI LOGRAMS | | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
1 0.00 2 0.00 3 1.17 4 0.04 5 0.04
6 0.04 7 0.09 8 0.08 9 0.08 10 0.08
11 0.26 12 0.10 13 0.11 14 0.19 15 0.19
16 0.20 17 0.18 18 0.59 19 0.00 20 0.00
***** TOTAL DELAY = 3.4 VEH-HRS ***** AVERAGE DELAY = 0.26 MIN/VEH *****

**
** FREEWAY TRAVEL TIME (MINUTES) **
**

* ORIGINS DESTINATIONS ACROSS *
* DOWN 1 2 3 4 5 6 7 8 *
+
* * *
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 2 * 0.00 2.38 2.94 3.89 4.42 4.70 5.62 0.00 *
+
* 3 * 0.00 0.00 0.00 0.00 2.23 2.50 3.42 0.00 *
+
* 4 * 0.00 0.00 0.00 0.00 0.00 2.14 3.06 0.00 *
+
* 5 * 0.00 0.00 0.00 0.00 0.00 0.00 2.25 0.00 *
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* * *

TIME SLICE FREEWAY PERFORMANCE TABLE

* SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMISS *
* SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP EFF LENGTH RATE RATIO MPH VPMP LEVEL LEVEL MPG GS/VM *
* 1 *
* 2 *
* 3 1 12000. 783. 0. 783. 783. 0. 783. 1650. 0. 0. 0. .47 62. 12.6 B 21.6 12.8 *
* 4 1 350. 209. 0. 991. 209. 0. 991. 1650. 0. 0. 0. .60 62. 16.0 B 21.6 12.8 *
* 5 1 300. 0. 0. 991. 0. 0. 991. 1650. 0. 0. 0. .60 62. 16.0 B 21.6 12.8 *
* 6 1 350. 0. 185. 991. 0. 185. 991. 1650. 0. 0. 0. .60 62. 16.0 B 21.6 12.8 *
* 7 1 940. 0. 0. 806. 0. 0. 806. 1650. 0. 0. 0. .49 62. 13.0 B 21.6 12.8 *
* 8 1 700. 237. 0. 1043. 237. 0. 1043. 1650. 0. 0. 0. .63 62. 16.8 B 21.6 12.8 *
* 9 1 700. 0. 0. 1043. 0. 0. 1043. 1650. 0. 0. 0. .63 62. 16.8 B 21.6 12.8 *
* 10 1 700. 0. 58. 1043. 0. 58. 1043. 1650. 0. 0. 0. .63 62. 16.8 B 21.6 12.8 *
* 11 1 2300. 0. 0. 985. 0. 0. 985. 1650. 0. 0. 0. .60 62. 15.9 B 21.6 12.8 *
* 12 1 700. 174. 0. 1159. 174. 0. 1159. 1650. 0. 0. 0. .70 62. 18.7 C 21.6 12.8 *
* 13 1 800. 0. 0. 1159. 0. 0. 1159. 1650. 0. 0. 0. .70 62. 18.7 C 21.6 12.8 *
* 14 1 1400. 0. 40. 1159. 0. 40. 1159. 1650. 0. 0. 0. .70 62. 18.7 C 21.6 12.8 *
* 15 1 1400. 0. 0. 1119. 0. 0. 1119. 1650. 0. 0. 0. .68 62. 18.0 C 21.6 12.8 *
* 16 1 1500. 0. 113. 1119. 0. 113. 1119. 1650. 0. 0. 0. .68 62. 18.0 C 21.6 12.8 *
* 17 1 1500. 0. 105. 1006. 0. 105. 1006. 1650. 0. 0. 0. .61 62. 16.2 B 21.6 12.8 *
* 18 1 5000. 0. 901. 901. 0. 901. 901. 1650. 0. 0. 0. .55 62. 14.5 B 21.6 12.8 *
* 19 *
* 20 *
*
* TOTAL 30640. = 5.8 MI LBS MAX(V/C) = 0.70 LOWEST LOS = C AVG = 62. 14.9 21.6 12.8 *

SR-237_EB_PM_P1_2040_PL

| | | | | | | | | |
|-----------------------------|-------|-----------|--------|----------|-------|-----------|--------|----------|
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 86. | VEH-HRS | 172. | PASS-HRS | 161. | VEH-HRS | 321. | PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 5344. | VEH-MI. | 10688. | PASS-MI. | 9964. | VEH-MI. | 19928. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. | MPH. | | | 62. | MPH. | | |
| AVERAGE DENSITY = | 15. | VPMPL | | | 14. | VPMPL | | |
| TOTAL FUEL = | 248. | GALLONS | | | 462. | GALLONS | | |
| TOTAL EMISSIONS = | 68. | KILOGRAMS | | | 127. | KILOGRAMS | | |

***** MAINTLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 1.32 | 4 | 0.05 | 5 | 0.04 |
| 6 | 0.05 | 7 | 0.11 | 8 | 0.10 | 9 | 0.10 | 10 | 0.10 |
| 11 | 0.32 | 12 | 0.11 | 13 | 0.13 | 14 | 0.23 | 15 | 0.22 |
| 16 | 0.24 | 17 | 0.21 | 18 | 0.64 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 4.0 VEH-HRS ***** AVERAGE DELAY = 0.26 MIN/VEH *****

 ** **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 ** **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN *
 * 1 2 3 4 5 6 7 8 *

| | | | | | | | | | | | |
|---|---|-------|------|------|------|------|------|------|------|------|---|
| + | * | ***** | | | | | | | | | * |
| + | * | * * * | | | | | | | | | * |
| + | * | * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | * |
| + | * | * 2 * | 0.00 | 2.38 | 2.94 | 3.89 | 4.42 | 4.70 | 5.62 | 0.00 | * |
| + | * | * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 2.23 | 2.50 | 3.42 | 0.00 | * |
| + | * | * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.14 | 3.06 | 0.00 | * |
| + | * | * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.25 | 0.00 | * |
| + | * | * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | * |
| + | * | * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | * |
| + | * | * * * | | | | | | | | | * |
| | | ***** | | | | | | | | | |

 * *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 * *

| * SUB NO. | * SEC LNS | * SSEC LENGTH | * O-D DATA ORG | * DEMANDS DES | * SSEC SSEC | * ADJUSTED ORG | * VOLUMES DES | * SSEC SSEC | * WEAVE CAP. | * EFF | * CONGEST LENGTH | * STORAGE RATE | * V/C RATIO | * SPEED MPH | * DENSITY VPMPL | * LOS LEVEL | * FUEL MPG | * EMISSIONS GS/VM |
|-----------|-----------|---------------|----------------|---------------|-------------|----------------|---------------|-------------|--------------|-------|------------------|----------------|-------------|-------------|-----------------|-------------|------------|-------------------|
| * | 1 | | | | | | | | | | | | | | | | | |
| * | 2 | | | | | | | | | | | | | | | | | |
| * | 3 | 1 | 12000. | 588. | 0. | 588. | 588. | 0. | 588. | 1650. | 0. | 0. | .36 | 62. | 9.5 | A | 21.6 | 12.8 |
| * | 4 | 1 | 350. | 156. | 0. | 744. | 156. | 0. | 744. | 1650. | 0. | 0. | .45 | 62. | 12.0 | B | 21.6 | 12.8 |
| * | 5 | 1 | 300. | 0. | 0. | 744. | 0. | 0. | 744. | 1650. | 0. | 0. | .45 | 62. | 12.0 | B | 21.6 | 12.8 |
| * | 6 | 1 | 350. | 0. | 151. | 744. | 0. | 151. | 744. | 1650. | 0. | 0. | .45 | 62. | 12.0 | B | 21.6 | 12.8 |
| * | 7 | 1 | 940. | 0. | 0. | 593. | 0. | 0. | 593. | 1650. | 0. | 0. | .36 | 62. | 9.6 | A | 21.6 | 12.8 |
| * | 8 | 1 | 700. | 235. | 0. | 828. | 235. | 0. | 828. | 1650. | 0. | 0. | .50 | 62. | 13.4 | B | 21.6 | 12.8 |
| * | 9 | 1 | 700. | 0. | 0. | 828. | 0. | 0. | 828. | 1650. | 0. | 0. | .50 | 62. | 13.4 | B | 21.6 | 12.8 |
| * | 10 | 1 | 700. | 0. | 42. | 828. | 0. | 42. | 828. | 1650. | 0. | 0. | .50 | 62. | 13.4 | B | 21.6 | 12.8 |
| * | 11 | 1 | 2300. | 0. | 0. | 785. | 0. | 0. | 785. | 1650. | 0. | 0. | .48 | 62. | 12.7 | B | 21.6 | 12.8 |
| * | 12 | 1 | 700. | 129. | 0. | 915. | 129. | 0. | 915. | 1650. | 0. | 0. | .55 | 62. | 14.8 | B | 21.6 | 12.8 |
| * | 13 | 1 | 800. | 0. | 0. | 915. | 0. | 0. | 915. | 1650. | 0. | 0. | .55 | 62. | 14.8 | B | 21.6 | 12.8 |
| * | 14 | 1 | 1400. | 0. | 31. | 915. | 0. | 31. | 915. | 1650. | 0. | 0. | .55 | 62. | 14.8 | B | 21.6 | 12.8 |
| * | 15 | 1 | 1400. | 0. | 0. | 884. | 0. | 0. | 884. | 1650. | 0. | 0. | .54 | 62. | 14.3 | B | 21.6 | 12.8 |
| * | 16 | 1 | 1500. | 0. | 93. | 884. | 0. | 93. | 884. | 1650. | 0. | 0. | .54 | 62. | 14.3 | B | 21.6 | 12.8 |
| * | 17 | 1 | 1500. | 0. | 106. | 791. | 0. | 106. | 791. | 1650. | 0. | 0. | .48 | 62. | 12.8 | B | 21.6 | 12.8 |
| * | 18 | 1 | 5000. | 0. | 686. | 686. | 0. | 686. | 686. | 1650. | 0. | 0. | .42 | 62. | 11.1 | B | 21.6 | 12.8 |
| * | 19 | | | | | | | | | | | | | | | | | |
| * | 20 | | | | | | | | | | | | | | | | | |

 * TOTAL 30640. = 5.8 MILES MAX(V/C) = 0.55 LOWEST LOS = B AVG = 62. 11.4 21.6 12.8 *

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|-----------------------------|--------------------|----------------|-------------------|-----------------|
| FREEWAY TRAVEL TIME = | 66. VEH-HRS | 133. PASS-HRS | 227. VEH-HRS | 454. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 66. VEH-HRS | 133. PASS-HRS | 227. VEH-HRS | 454. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 4116. VEH-MI. | 8232. PASS-MI. | 14080. VEH-MI. | 28160. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | | 62. MPH. | |
| AVERAGE DENSITY = | 11. VPMP/L | | 13. VPMP/L | |
| TOTAL FUEL = | 191. GALLONS | | 653. GALLONS | |
| TOTAL EMISSIONS = | 53. KILOGRAMS | | 180. KILOGRAMS | |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 3 OF 3

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.99 | 4 | 0.04 | 5 | 0.03 |
| 6 | 0.04 | 7 | 0.08 | 8 | 0.08 | 9 | 0.08 | 10 | 0.08 |
| 11 | 0.25 | 12 | 0.09 | 13 | 0.10 | 14 | 0.18 | 15 | 0.17 |
| 16 | 0.19 | 17 | 0.17 | 18 | 0.48 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 3.1 VEH-HRS ***** AVERAGE DELAY = 0.26 MIN/VEH *****

```

FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQQ QQQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*QQ 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP EEEEEEEEE
    
```

FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 62
LOWER LIMB (AT V/C=1) = 30
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREWAY AND ARTERIAL DESIGN FEATURES

| ** SUB NO. | ** SSEC | ** SSEC | ** DESIG N | ** ORG | ** TRK | ** SSEC | ** PCT | ** PCT | ** DES | ** SPECIAL | ** FF. SPD. | ** CAP. | ** ART | ** GRADE | ** SUBSECTI ON | ** LOCATI ON |
|------------|---------|---------|------------|----------|--------|---------|--------|-----------|---------|-------------|-------------|---------|-------------|-------------|------------------------|--------------|
| ** SEC | ** LNS | ** CAP | ** LENGTH | ** SPEED | ** DES | ** GRAD | ** TRK | ** TRUCKS | ** RAMP | ** ALT. RTE | ** ALT. RTE | ** TYPE | ** ALT. RTE | ** ALT. RTE | ** LOCATION | ** LOCATION |
| ** 1 | 3 | 6000. | 500. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Seeding | ** |
| ** 2 | 3 | 6000. | 99999. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | ** |
| ** 3 | 2 | 4000. | 12000. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | ** |
| ** 4 | 3 | 5010. | 350. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Maude On-ramp | ** |
| ** 5 | 3 | 5010. | 300. | 62 | | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Maude to US-101 | ** |
| ** 6 | 3 | 5010. | 350. | 62 | D | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US-101 Off-Ramp | ** |
| ** 7 | 2 | 4000. | 940. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | US101SB / US101SB | ** |
| ** 8 | 3 | 5330. | 700. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US101 SB On-ramp | ** |
| ** 9 | 3 | 5330. | 700. | 62 | | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US 101 / Mathilda | ** |
| ** 10 | 3 | 5330. | 700. | 62 | D | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-ramp | ** |
| ** 11 | 2 | 4000. | 2300. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | ** |
| ** 12 | 3 | 5320. | 700. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda On-Ramp | ** |
| ** 13 | 3 | 4400. | 800. | 62 | | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda / Persian HOV | ** |
| ** 14 | 3 | 4400. | 1400. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Persian On-Ramp w/HOV | ** |
| ** 15 | 2 | 4000. | 1400. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | West of Lawrence E | ** |
| ** 16 | 2 | 4000. | 1500. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence Off-ramp | ** |
| ** 17 | 2 | 4000. | 1500. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End of DKS | ** |
| ** 18 | 2 | 4000. | 5000. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | ** |
| ** 19 | 2 | 4000. | 5000. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Enter SSec Description | ** |
| ** 20 | 3 | 2500. | 750. | 62 | OD | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | End of the network | ** |

***** INPUT HAS BEEN COMPLETED *****

MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 2 IN TIME SLICE 2
--- THE MAXIMUM METERING RATE WILL PREVAIL.

MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 2 IN TIME SLICE 3
--- THE MAXIMUM METERING RATE WILL PREVAIL.

**
** FREEWAY TRAVEL TIME (MINUTES) **
**

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | |
|-----------|--|-----------------------|-------|-------|-------|-------|-------|-------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | | 18.42 | 20.80 | 21.36 | 23.89 | 26.59 | 29.53 | 59.64 |
| * 2 * | | 0.00 | 0.18 | 0.74 | 3.27 | 5.97 | 8.91 | 39.02 |
| * 3 * | | 0.00 | 0.00 | 0.39 | 2.91 | 5.62 | 8.56 | 38.66 |
| * 4 * | | 0.00 | 0.00 | 0.00 | 1.75 | 4.46 | 7.40 | 37.50 |
| * 5 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 13.71 |
| * 6 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.14 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | | |
|-----------|--------|------------|-----------|------------|-----------|---------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|---------|--------|--------|--------|
| * SEC | * LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * SSEC | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | | | |
| * 1 | * 3 | * 500. | * 2661. | * 0. | * 2661. | * 2661. | * 0. | * 2661. | * 6000. | * 0. | * 0. | * .44 | * 62. | * 14.3 | * B | * 20.3 | * 13.0 | | |
| * 2 | * 3 | * 99999. | * 0. | * 692. | * 2661. | * 0. | * 692. | * 2661. | * 6000. | * 0. | * 0. | * .44 | * 62. | * 14.3 | * B | * 20.3 | * 13.0 | | |
| * 3 | * 2 | * 12000. | * 0. | * 0. | * 1969. | * 0. | * 0. | * 1969. | * 4000. | * 0. | * 0. | * .49 | * 62. | * 15.9 | * B | * 20.3 | * 13.0 | | |
| * 4 | * 3 | * 350. | * 876. | * 0. | * 2845. | * 776. | * 0. | * 2745. | * 4836. | * 0. | * 0. | * .57 | * 62. | * 14.8 | * B | * 20.3 | * 13.0 | | |
| * 5 | * 3 | * 300. | * 0. | * 0. | * 2845. | * 0. | * 0. | * 2745. | * 5010. | * 0. | * 0. | * .55 | * 62. | * 14.8 | * B | * 20.3 | * 13.0 | | |
| * 6 | * 3 | * 350. | * 0. | * 708. | * 2845. | * 0. | * 680. | * 2745. | * 4848. | * 0. | * 0. | * .57 | * 62. | * 14.8 | * B | * 20.3 | * 13.0 | | |
| * 7 | * 2 | * 940. | * 0. | * 0. | * 2137. | * 0. | * 0. | * 2065. | * 4000. | * 0. | * 0. | * .52 | * 62. | * 16.7 | * B | * 20.3 | * 13.0 | | |
| * 8 | * 3 | * 700. | * 678. | * 0. | * 2815. | * 678. | * 0. | * 2743. | * 5186. | * 0. | * 0. | * .53 | * 62. | * 14.7 | * B | * 20.3 | * 13.0 | | |
| * 9 | * 3 | * 700. | * 0. | * 0. | * 2815. | * 0. | * 0. | * 2743. | * 5330. | * 0. | * 0. | * .51 | * 62. | * 14.7 | * B | * 20.3 | * 13.0 | | |
| * 10 | * 3 | * 700. | * 0. | * 347. | * 2815. | * 0. | * 337. | * 1154. | * 5271. | * 0. | * * | * 84. | * 1589. | * .22 | * 62. | * 6.2 | * F | * 20.3 | * 13.1 |
| * 11 | * 2 | * 2300. | * 0. | * 0. | * 2468. | * 0. | * 0. | * 817. | * 4000. | * 0. | * ** | * 2300. | * 1589. | * .20 | * 34. | * 12.1 | * F | * 19.7 | * 13.4 |
| * 12 | * 3 | * 700. | * 667. | * 0. | * 3135. | * 567. | * 0. | * 1384. | * 5156. | * 0. | * ** | * 700. | * 1589. | * .27 | * 21. | * 21.5 | * F | * 18.4 | * 14.2 |
| * 13 | * 3 | * 800. | * 0. | * 0. | * 3135. | * 0. | * 0. | * 1384. | * 4400. | * 0. | * ** | * 800. | * 1589. | * .31 | * 21. | * 22.5 | * F | * 17.8 | * 14.6 |
| * 14 | * 3 | * 1400. | * 0. | * 227. | * 3135. | * 0. | * 214. | * 1384. | * 4371. | * 0. | * ** | * 1400. | * 1589. | * .32 | * 17. | * 27.3 | * F | * 17.1 | * 15.1 |
| * 15 | * 2 | * 1400. | * 0. | * 0. | * 2908. | * 0. | * 0. | * 1170. | * 4000. | * 0. | * ** | * 1400. | * 1589. | * .29 | * 13. | * 44.0 | * F | * 16.5 | * 15.6 |
| * 16 | * 2 | * 1500. | * 0. | * 610. | * 2908. | * 0. | * 577. | * 1170. | * 3883. | * 0. | * ** | * 1500. | * 1589. | * .30 | * 11. | * 51.7 | * F | * 15.6 | * 16.3 |
| * 17 | * 2 | * 1500. | * 0. | * 0. | * 2298. | * 0. | * 0. | * 593. | * 4000. | * 0. | * ** | * 1500. | * 1589. | * .15 | * 6. | * 51.1 | * F | * 16.0 | * 16.0 |
| * 18 | * 2 | * 5000. | * 0. | * 0. | * 2298. | * 0. | * 0. | * 593. | * 4000. | * 0. | * ** | * 5000. | * 1589. | * .15 | * 3. | * 85.5 | * F | * 13.8 | * 18.2 |
| * 19 | * 2 | * 5000. | * 807. | * 0. | * 3105. | * 807. | * 0. | * 1400. | * 4000. | * 0. | * ** | * 5000. | * 1589. | * .35 | * 4. | * 167.2 | * F | * 9.5 | * 25.6 |
| * 20 | * 3 | * 750. | * 1100. | * 4205. | * 4205. | * 1100. | * 2500. | * 2500. | * 2500. | * 0. | * 0. | * 1.00 | * 62. | * 13.4 | * E | * 20.3 | * 13.0 | | |

TOTAL 136889. = 25.9 MI LBS MAX(V/C) = 1.00 LOWEST LOS = F AVG = 34. 23.9 19.5 13.5

FREWAY TRAVEL TIME = CURRENT TIME SLICE CUMULATIVE VALUES
1878. VEH-HRS 2195. PASS-HRS 1878. VEH-HRS 2195. PASS-HRS

SR-237_EB_PM_P2_2040_PE

| | | | | | | | | |
|----------------------------|--------|------------|--------|----------|--------|------------|--------|----------|
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 100. | VEH-HRS | 100. | PASS-HRS | 100. | VEH-HRS | 100. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1978. | VEH-HRS | 2295. | PASS-HRS | 1978. | VEH-HRS | 2295. | PASS-HRS |
| TOTAL TRAV DISTANCE = | 64127. | VEH-MI. | 78009. | PASS-MI. | 64127. | VEH-MI. | 78009. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 32. | MPH | | | 34. | MPH | | |
| AVERAGE DENSITY = | 24. | VPMP/L | | | 24. | VPMP/L | | |
| TOTAL FUEL = | 3332. | GALLONS | | | 3332. | GALLONS | | |
| TOTAL EMISSIONS = | 883. | KI LOGRAMS | | | 883. | KI LOGRAMS | | |

```
***** MAINTLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION   DELAY   SUBSECTION   DELAY   SUBSECTION   DELAY   SUBSECTION   DELAY   SUBSECTION   DELAY
      1         0.19      2        37.52      3         3.33      4         0.14      5         0.12
      6         0.14      7         0.27      8         0.27      9         0.27     10         0.30
     11        14.22     12        11.34     13        13.46     14        29.94     15        35.84
     16        44.63     17         64.83     18        301.08     19        333.25     20         0.26

***** TOTAL DELAY = 891.4 VEH-HRS ***** AVERAGE DELAY = 59.85 MIN/VEH *****
```

```
***** RAMP DELAYS *****
```

| | | QUEUE LENGTH | DELAY | AVERAGE | GAS | HC | CO | NOX | TOTAL |
|---------|---|--------------|---------|----------|-------|------|------|------|-----------|
| | | VEHICLES | VEH-HRS | METERING | GALS | KGMS | KGMS | KGMS | EMISSIONS |
| | | | | DELAY | | | | | KGMS |
| | | | | MI | | | | | |
| | | | | MINUTES | | | | | |
| ON-RAMP | 2 | RAMP | 100. | 3.42 | 18.03 | 1.11 | 5.83 | 0.31 | 7.25 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 3.42 | 18.03 | 1.11 | 5.83 | 0.31 | 7.25 |
| ON-RAMP | 4 | RAMP | 100. | 4.50 | 18.03 | 1.11 | 5.83 | 0.31 | 7.25 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 4.50 | 18.03 | 1.11 | 5.83 | 0.31 | 7.25 |

```
*****
**
**      FREEWAY TRAVEL TIME (MI MINUTES)
**
*****
```

```
*****
* ORIGIN   DESTINATIONS ACROSS
* DOWN
*      1     2     3     4     5     6     7
+
*
+
* 1 * 18.42 27.09 32.90 40.48 43.96 46.84 67.44
+
* 2 * 0.00 1.41 7.22 14.80 18.28 21.16 41.76
+
* 3 * 0.00 0.00 3.82 11.40 14.88 17.76 38.36
+
* 4 * 0.00 0.00 0.00 3.70 7.18 10.06 30.66
+
* 5 * 0.00 0.00 0.00 0.00 0.00 0.00 6.88
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.14
+
*
*****
```

```
*****
*
*      TIME SLICE FREEWAY PERFORMANCE TABLE
*
*****
```

| * SUB | * NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | |
|-------|-------|----------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|--------|--------|--------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * ORG | * DES | * CAP | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP/L | * LEVEL | * MPG | * GS/VM | | | |
| * 1 | * 3 | * 500. | * 3011. | * 0. | * 3011. | * 3011. | * 0. | * 3011. | * 6000. | * 0. | * 0. | * .50 | * 62. | * 16.2 | * B | * 20.3 | * 13.0 | | |
| * 2 | * 3 | * 99999. | * 0. | * 783. | * 3011. | * 0. | * 783. | * 3011. | * 6000. | * 0. | * 0. | * .50 | * 62. | * 16.2 | * B | * 20.3 | * 13.0 | | |
| * 3 | * 2 | * 12000. | * 0. | * 0. | * 2228. | * 0. | * 0. | * 1408. | * 4000. | * 0. | * ** | * 7309. | * 820. | * .35 | * 19. | * 37.5 | * F | * 17.1 | * 15.1 |
| * 4 | * 3 | * 350. | * 1051. | * 0. | * 3279. | * 900. | * 0. | * 2308. | * 4801. | * 0. | * ** | * 350. | * 820. | * .48 | * 9. | * 89.3 | * F | * 11.3 | * 22.1 |
| * 5 | * 3 | * 300. | * 0. | * 0. | * 3279. | * 0. | * 0. | * 2308. | * 5010. | * 0. | * ** | * 300. | * 820. | * .46 | * 8. | * 99.6 | * F | * 10.8 | * 22.8 |
| * 6 | * 3 | * 350. | * 0. | * 825. | * 3279. | * 0. | * 782. | * 2308. | * 4825. | * 0. | * ** | * 350. | * 820. | * .48 | * 8. | * 98.6 | * F | * 10.7 | * 23.1 |
| * 7 | * 2 | * 940. | * 0. | * 0. | * 2454. | * 0. | * 0. | * 1526. | * 4000. | * 0. | * ** | * 940. | * 820. | * .38 | * 5. | * 142.1 | * F | * 10.2 | * 23.9 |

SR-237_EB_PM_P2_2040_PE

| | | | | | | | | | | | | | | | | | | | | | |
|---|----|---|-------|-------|-------|-------|-------|-------|-------|-------|----|----|-------|------|------|-----|-------|---|------|------|---|
| * | 8 | 3 | 700. | 1061. | 0. | 3515. | 1061. | 0. | 2587. | 5094. | 0. | ** | 700. | 820. | .51 | 7. | 121.1 | F | 10.0 | 24.9 | * |
| * | 9 | 3 | 700. | 0. | 0. | 3515. | 0. | 0. | 2587. | 5330. | 0. | ** | 700. | 820. | .49 | 6. | 141.6 | F | 9.2 | 26.5 | * |
| * | 10 | 3 | 700. | 0. | 388. | 3515. | 0. | 375. | 2587. | 5272. | 0. | ** | 700. | 820. | .49 | 6. | 151.3 | F | 8.8 | 27.7 | * |
| * | 11 | 2 | 2300. | 0. | 0. | 3127. | 0. | 0. | 2211. | 4000. | 0. | ** | 2300. | 820. | .55 | 7. | 164.1 | F | 9.5 | 26.8 | * |
| * | 12 | 3 | 700. | 725. | 0. | 3852. | 725. | 0. | 2936. | 5166. | 0. | ** | 700. | 820. | .57 | 7. | 138.4 | F | 9.8 | 26.4 | * |
| * | 13 | 3 | 800. | 0. | 0. | 3852. | 0. | 0. | 2936. | 4400. | 0. | ** | 800. | 820. | .67 | 10. | 102.0 | F | 12.4 | 23.4 | * |
| * | 14 | 3 | 1400. | 0. | 333. | 3852. | 0. | 322. | 2936. | 4360. | 0. | ** | 1400. | 820. | .67 | 10. | 100.1 | F | 12.7 | 23.2 | * |
| * | 15 | 2 | 1400. | 0. | 0. | 3519. | 0. | 0. | 2614. | 4000. | 0. | ** | 1400. | 820. | .65 | 9. | 142.1 | F | 11.9 | 23.9 | * |
| * | 16 | 2 | 1500. | 0. | 631. | 3519. | 0. | 622. | 2614. | 3886. | 0. | ** | 1500. | 820. | .67 | 10. | 134.0 | F | 12.6 | 23.2 | * |
| * | 17 | 2 | 1500. | 0. | 393. | 2888. | 0. | 368. | 1992. | 3893. | 0. | ** | 1500. | 820. | .51 | 6. | 168.4 | F | 8.9 | 27.8 | * |
| * | 18 | 2 | 5000. | 0. | 0. | 2495. | 0. | 0. | 1624. | 4000. | 0. | ** | 5000. | 820. | .41 | 4. | 196.1 | F | 8.3 | 28.9 | * |
| * | 19 | 2 | 5000. | 876. | 0. | 3371. | 876. | 0. | 2500. | 4000. | 0. | ** | 5000. | 820. | .63 | 8. | 148.4 | F | 11.0 | 24.8 | * |
| * | 20 | 3 | 750. | 0. | 3371. | 3371. | 0. | 2500. | 2500. | 2500. | 0. | ** | 0. | 0. | 1.00 | 62. | 13.4 | E | 20.3 | 13.0 | * |

| | | | | | | | | | | | | | | | | | | | | | |
|---|-------|---------|---|------|--------|--|--|--|--|--|--|--|-----------------|----------------|-----------|------|--|--|------|------|---|
| * | TOTAL | 136889. | = | 25.9 | MI LES | | | | | | | | MAX(V/C) = 1.00 | LOWEST LOS = F | AVG = 27. | 41.5 | | | 17.7 | 15.0 | * |
|---|-------|---------|---|------|--------|--|--|--|--|--|--|--|-----------------|----------------|-----------|------|--|--|------|------|---|

| CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | | |
|----------------------------|--------|------------|--------|-------------------|---------|------------|---------|----------|
| FREEWAY TRAVEL TIME = | 2690. | VEH-HRS | 3037. | PASS-HRS | 4568. | VEH-HRS | 5232. | PASS-HRS |
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 275. | VEH-HRS | 275. | PASS-HRS | 375. | VEH-HRS | 375. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 2966. | VEH-HRS | 3313. | PASS-HRS | 4944. | VEH-HRS | 5607. | PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 72699. | VEH-MI. | 88554. | PASS-MI. | 136826. | VEH-MI. | 166563. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 25. | MPH | | | 30. | MPH | | |
| AVERAGE DENSITY = | 41. | VPMPPL | | | 33. | VPMPPL | | |
| TOTAL FUEL = | 4214. | GALLONS | | | 7546. | GALLONS | | |
| TOTAL EMISSIONS = | 1127. | KI LOGRAMS | | | 2010. | KI LOGRAMS | | |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 3

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|--------|------------|-------|------------|--------|------------|--------|------------|-------|
| 1 | 0.21 | 2 | 42.45 | 3 | 177.83 | 4 | 17.29 | 5 | 16.64 |
| 6 | 19.00 | 7 | 52.13 | 8 | 45.04 | 9 | 52.55 | 10 | 55.34 |
| 11 | 128.15 | 12 | 49.04 | 13 | 39.54 | 14 | 67.68 | 15 | 64.71 |
| 16 | 64.72 | 17 | 86.98 | 18 | 347.70 | 19 | 244.57 | 20 | 0.26 |

***** TOTAL DELAY = 1571.8 VEH-HRS ***** AVERAGE DELAY = 46.39 MIN/VEH *****

***** RAMP DELAYS *****

| | | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS | |
|---------|---|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|-------|
| ON-RAMP | 2 | RAMP | 251. | 175.50 | 9.15 | 63.29 | 3.91 | 20.47 | 1.08 | 25.46 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 251. | 175.50 | 9.15 | 63.29 | 3.91 | 20.47 | 1.08 | 25.46 |
| ON-RAMP | 4 | RAMP | 100. | 100.00 | 7.27 | 36.06 | 2.23 | 11.66 | 0.62 | 14.51 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 100.00 | 7.27 | 36.06 | 2.23 | 11.66 | 0.62 | 14.51 |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 3 OF 3

 ** **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 ** **

| * ORIGINS DOWN | | * DESTINATIONS ACROSS | | | | | | | |
|----------------|---|-----------------------|-------|-------|-------|-------|-------|-------|-------|
| | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | |
| + | * | ***** | | | | | | | |
| + | * | ***** | | | | | | | |
| + | * | 1 | 18.42 | 44.13 | 50.06 | 56.45 | 59.46 | 61.84 | 80.17 |
| + | * | 2 | 0.00 | 1.98 | 7.92 | 14.31 | 17.31 | 19.70 | 38.03 |
| + | * | 3 | 0.00 | 0.00 | 3.65 | 10.04 | 13.04 | 15.43 | 33.76 |
| + | * | 4 | 0.00 | 0.00 | 0.00 | 3.33 | 6.33 | 8.72 | 27.05 |
| + | * | 5 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 6.88 |
| + | * | 6 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.14 |
| + | * | ***** | | | | | | | |
| + | * | ***** | | | | | | | |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | |
|-----------|----------|------------|-----------|--------------------|----------|----------|-----------|-----------------|----------------|-----------|-----------|---------|--------|-------------|------|------|
| * SEC LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | |
| * 1 | 3 | 500. | 2260. | 0. 2260. | 2260. | 0. 2260. | 6000. | 0. | 0. | .38 | 62. | 12.2 | B | 20.3 | 13.0 | |
| * 2 | 3 | 99999. | 0. 588. | 2260. | 0. 588. | 2260. | 6000. | 0. | 0. | .38 | 62. | 12.2 | B | 20.3 | 13.0 | |
| * 3 | 2 | 12000. | 0. 0. | 1672. | 0. 0. | 1561. | 4000. | 0. | ** 8879. | 111. | .39 | 6. | 135.8 | F | 10.4 | 23.5 |
| * 4 | 3 | 350. | 813. | 0. 2485. | 900. | 0. 2461. | 4854. | 0. | ** 350. | 111. | .51 | 6. | 140.8 | F | 8.9 | 27.9 |
| * 5 | 3 | 300. | 0. 0. | 2485. | 0. 0. | 2461. | 5010. | 0. | ** 300. | 111. | .49 | 6. | 148.2 | F | 8.7 | 28.2 |
| * 6 | 3 | 350. | 0. 679. | 2485. | 0. 701. | 2461. | 4859. | 0. | ** 350. | 111. | .51 | 6. | 141.0 | F | 8.9 | 27.9 |
| * 7 | 2 | 940. | 0. 0. | 1806. | 0. 0. | 1761. | 4000. | 0. | ** 940. | 111. | .44 | 5. | 188.6 | F | 8.3 | 28.9 |
| * 8 | 3 | 700. | 1085. | 0. 2891. | 1085. | 0. 2846. | 5096. | 0. | ** 700. | 111. | .56 | 7. | 138.3 | F | 9.6 | 26.7 |
| * 9 | 3 | 700. | 0. 0. | 2891. | 0. 0. | 2846. | 5330. | 0. | ** 700. | 111. | .53 | 6. | 149.4 | F | 9.2 | 27.3 |
| * 10 | 3 | 700. | 0. 319. | 2891. | 0. 327. | 2846. | 5288. | 0. | ** 700. | 111. | .54 | 6. | 147.4 | F | 9.3 | 27.2 |
| * 11 | 2 | 2300. | 0. 0. | 2572. | 0. 0. | 2518. | 4000. | 0. | ** 2300. | 111. | .63 | 9. | 147.4 | F | 11.2 | 24.7 |
| * 12 | 3 | 700. | 584. | 0. 3156. | 584. | 0. 3102. | 5205. | 0. | ** 700. | 111. | .60 | 8. | 134.2 | F | 10.3 | 25.6 |
| * 13 | 3 | 800. | 0. 0. | 3156. | 0. 0. | 3102. | 4400. | 0. | ** 800. | 111. | .71 | 11. | 96.0 | F | 13.4 | 22.3 |
| * 14 | 3 | 1400. | 0. 287. | 3156. | 0. 292. | 3102. | 4369. | 0. | ** 1400. | 111. | .71 | 11. | 94.5 | F | 13.5 | 22.2 |
| * 15 | 2 | 1400. | 0. 0. | 2869. | 0. 0. | 2810. | 4000. | 0. | ** 1400. | 111. | .70 | 11. | 131.5 | F | 13.3 | 22.4 |
| * 16 | 2 | 1500. | 0. 580. | 2869. | 0. 586. | 2810. | 3906. | 0. | ** 1500. | 111. | .72 | 11. | 124.8 | F | 13.6 | 21.9 |
| * 17 | 2 | 1500. | 0. 392. | 2289. | 0. 391. | 2224. | 3892. | 0. | ** 1500. | 111. | .57 | 7. | 155.7 | F | 9.9 | 26.3 |
| * 18 | 2 | 5000. | 0. 0. | 1897. | 0. 0. | 1833. | 4000. | 0. | ** 5000. | 111. | .46 | 5. | 184.7 | F | 8.3 | 28.9 |
| * 19 | 2 | 5000. | 667. | 0. 2564. | 667. | 0. 2500. | 4000. | 0. | ** 5000. | 111. | .63 | 8. | 148.4 | F | 11.0 | 24.8 |
| * 20 | 3 | 750. | 0. 2564. | 2564. | 0. 2500. | 2500. | 2500. | 0. | 0. | 1.00 | 62. | 13.4 | E | 20.3 | 13.0 | |
| * TOTAL | 136889. | = | 25.9 | MILES | | | | MAX(V/C) = 1.00 | LOWEST LOS = F | AVG = 21. | 46.7 | | 16.4 | 16.0 | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 2813. VEH-HRS | 3100. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 307. VEH-HRS | 307. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 3121. VEH-HRS | 3407. PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 57993. VEH-MI. | 70148. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 19. MPH | 26. MPH |
| AVERAGE DENSITY = | 47. VPMP | 37. VPMP |
| TOTAL FUEL = | 3637. GALLONS | 11183. GALLONS |
| TOTAL EMISSIONS = | 974. KILOGRAMS | 2985. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|---------------------|--------|------------|-----------------------|------------|---------|------------|--------|------------|-------|
| 1 | 0.16 | 2 | 31.86 | 3 | 575.73 | 4 | 25.49 | 5 | 23.11 |
| 6 | 25.54 | 7 | 62.34 | 8 | 49.22 | 9 | 53.63 | 10 | 52.84 |
| 11 | 111.52 | 12 | 47.04 | 13 | 36.41 | 14 | 62.55 | 15 | 58.25 |
| 16 | 58.61 | 17 | 78.75 | 18 | 323.10 | 19 | 244.57 | 20 | 0.26 |
| ***** TOTAL DELAY = | 1921.0 | VEH-HRS | ***** AVERAGE DELAY = | 56.74 | MIN/VEH | ***** | | | |

***** RAMP DELAYS *****

| | QUEUE LENGTH | DELAY | AVERAGE | GAS | HC | CO | NOX | TOTAL | |
|-----------|--------------|---------|----------|-------|-------|------|-------|-----------|-------|
| | VEHICLES | VEH-HRS | METERING | GALS | KGMS | KGMS | KGMS | EMISSIONS | |
| | | | DELAY | | | | | KGMS | |
| | | | MINUTES | | | | | | |
| ON-RAMP 2 | RAMP | 164. | 207.50 | 11.70 | 74.82 | 4.63 | 24.20 | 1.28 | 30.10 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 164. | 207.50 | 11.70 | 74.82 | 4.63 | 24.20 | 1.28 | 30.10 |
| ON-RAMP 4 | RAMP | 100. | 100.00 | 8.77 | 36.06 | 2.23 | 11.66 | 0.62 | 14.51 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 100.00 | 8.77 | 36.06 | 2.23 | 11.66 | 0.62 | 14.51 |

```

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ      1111      222222  PPPPPPPP   LLL
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111  222  222  PPPPPPPP   LLL
FFF      RRR      RRR EEE      QQQQQ  QQQQQ  1111  222  222  PPP   PPP   LLL
FFF      RRR      RRR EEE      QQQQ   QQQQ   1111  222  222  PPP   PPP   LLL
FFFFFFFF RRRRRRRR EEEEEEEEE QQQQ   QQQQ   1111  222  PPPPPPPP   LLL
FFFFFFFF RRRRRRRR EEEEEEEEE QQQQ   QQQQ   1111  2222  PPPPPPPP   LLL
FFF      RRR      RRR EEE      QQQQ   QQ  QQQQ 1111  2222  PPP   LLL
FFF      RRR      RRR EEE      Q*UC*  QQQQQ  1111  222  PPP   LLL
FFF      RRR      RRR EEEEEEEEE Q*REGENTS*Q 1111  222  PPP   LLLLLLLLLL
FFF      RRR      RRR EEEEEEEEE Q*1988*Q  QQQ 11111111 222222222222 PPP   LLLLLLLLLL
  
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FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 3 AND 18 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 62
LOWER LIMB (AT V/C=1) = 30
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

FREeway AND ARTERIAL DESIGN FEATURES

| ** SUB NO. | ** SSEC | ** SSEC | ** DESIG N | ** ORG | ** TRK | ** SSEC PCT | ** PCT DES | ** SPECIAL | ** FF. SPD. | ** CAP. | ** ART | ** GRADE | ** SUBSECTI ON |
|------------|---------|-----------|------------|--------|--------|-------------|------------|------------|-------------|-------------|---------|-------------|----------------------------|
| ** SEC LNS | ** CAP | ** LENGTH | ** SPEED | ** DES | ** FAC | ** GRAD TRK | ** TRUCKS | ** RAMP | ** ALT. RTE | ** ALT. RTE | ** TYPE | ** ALT. RTE | ** LOCATI ON |
| ** 1 | | | | | | | | | | | | | |
| ** 2 | | | | | | | | | | | | | |
| ** 3 | 1 | 1650. | 12000. | 62 | 0 | 0.95 | 0.0 | 0 100 | NO | 0.0 | 0. | GOOD | 0.0 HOV Dummy |
| ** 4 | 1 | 1650. | 350. | 62 | 0 | 0.95 | 0.0 | 0 100 | YES | 0.0 | 0. | GOOD | 0.0 Maude On-ramp |
| ** 5 | 1 | 1650. | 300. | 62 | | 0.95 | 0.0 | 0 100 | YES | 0.0 | 0. | GOOD | 0.0 Maude to US-101 |
| ** 6 | 1 | 1650. | 350. | 62 | D | 0.95 | 0.0 | 0 100 | YES | 0.0 | 0. | GOOD | 0.0 US-101 Off-Ramp |
| ** 7 | 1 | 1650. | 940. | 62 | | 0.95 | 0.0 | 0 100 | NO | 0.0 | 0. | GOOD | 0.0 US101SB / US101SB |
| ** 8 | 1 | 1650. | 700. | 62 | 0 | 0.95 | 0.0 | 0 100 | YES | 0.0 | 0. | GOOD | 0.0 US101 SB On-ramp |
| ** 9 | 1 | 1650. | 700. | 62 | | 0.95 | 0.0 | 0 100 | YES | 0.0 | 0. | GOOD | 0.0 US 101 / Mathilda |
| ** 10 | 1 | 1650. | 700. | 62 | D | 0.95 | 0.0 | 0 100 | YES | 0.0 | 0. | GOOD | 0.0 Mathilda Off-ramp |
| ** 11 | 1 | 1650. | 2300. | 62 | | 0.95 | 0.0 | 0 100 | NO | 0.0 | 0. | GOOD | 0.0 Mathilda / Mathilda |
| ** 12 | 1 | 1650. | 700. | 62 | 0 | 0.95 | 0.0 | 0 100 | YES | 0.0 | 0. | GOOD | 0.0 Mathilda On-Ramp |
| ** 13 | 1 | 1650. | 800. | 62 | | 0.95 | 0.0 | 0 100 | YES | 0.0 | 0. | GOOD | 0.0 Mathilda / Persian HOV |
| ** 14 | 1 | 1650. | 1400. | 62 | D | 0.95 | 0.0 | 0 100 | NO | 0.0 | 0. | GOOD | 0.0 Persian On-Ramp w/HOV |
| ** 15 | 1 | 1650. | 1400. | 62 | | 0.95 | 0.0 | 0 100 | NO | 0.0 | 0. | GOOD | 0.0 West of Lawrence E |
| ** 16 | 1 | 1650. | 1500. | 62 | D | 0.95 | 0.0 | 0 100 | NO | 0.0 | 0. | GOOD | 0.0 Lawrence Off-ramp |
| ** 17 | 1 | 1650. | 1500. | 62 | D | 0.95 | 0.0 | 0 100 | NO | 0.0 | 0. | GOOD | 0.0 End of DKS |
| ** 18 | 1 | 1650. | 5000. | 62 | D | 0.95 | 0.0 | 0 100 | NO | 0.0 | 0. | GOOD | 0.0 HOV Dummy |

Page 1

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1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/30/2016 16:16 PAGE 3
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 1 OF 3

 ** FREeway TRAVEL TIME (MINUTES) **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|------|-----------------------|------|------|------|------|------|------|------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| + * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + * 2 * | 0.00 | 2.38 | 2.94 | 3.89 | 4.42 | 4.70 | 5.62 | 0.00 | 0.00 |
| + * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 2.23 | 2.50 | 3.42 | 0.00 | 0.00 |
| + * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.14 | 3.06 | 0.00 | 0.00 |
| + * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.25 | 0.00 | 0.00 |
| + * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 1 OF 3

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | | |
|-----------|--------|------------|-----------|--------------------|---------|---------|-----------|-----------|---------|-----------------|-----------|----------------|--------|-------------|------|---|------|------|
| * SEC | * LNS | * LENGTH | * ORG DES | * ORG DES | * CAP | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | | | |
| * 1 | | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | | |
| * 3 | 1 | 12000. | 692. | 0. | 692. | 692. | 0. | 692. | 1650. | 0. | 0. | 0. | .42 | 62. | 11.2 | B | 21.6 | 12.8 |
| * 4 | 1 | 350. | 174. | 0. | 866. | 174. | 0. | 866. | 1650. | 0. | 0. | 0. | .52 | 62. | 14.0 | B | 21.6 | 12.8 |
| * 5 | 1 | 300. | 0. | 0. | 866. | 0. | 0. | 866. | 1650. | 0. | 0. | 0. | .52 | 62. | 14.0 | B | 21.6 | 12.8 |
| * 6 | 1 | 350. | 0. | 162. | 866. | 0. | 162. | 866. | 1650. | 0. | 0. | 0. | .52 | 62. | 14.0 | B | 21.6 | 12.8 |
| * 7 | 1 | 940. | 0. | 0. | 704. | 0. | 0. | 704. | 1650. | 0. | 0. | 0. | .43 | 62. | 11.3 | B | 21.6 | 12.8 |
| * 8 | 1 | 700. | 144. | 0. | 848. | 144. | 0. | 848. | 1650. | 0. | 0. | 0. | .51 | 62. | 13.7 | B | 21.6 | 12.8 |
| * 9 | 1 | 700. | 0. | 0. | 848. | 0. | 0. | 848. | 1650. | 0. | 0. | 0. | .51 | 62. | 13.7 | B | 21.6 | 12.8 |
| * 10 | 1 | 700. | 0. | 59. | 848. | 0. | 59. | 848. | 1650. | 0. | 0. | 0. | .51 | 62. | 13.7 | B | 21.6 | 12.8 |
| * 11 | 1 | 2300. | 0. | 0. | 789. | 0. | 0. | 789. | 1650. | 0. | 0. | 0. | .48 | 62. | 12.7 | B | 21.6 | 12.8 |
| * 12 | 1 | 700. | 164. | 0. | 953. | 164. | 0. | 953. | 1650. | 0. | 0. | 0. | .58 | 62. | 15.4 | B | 21.6 | 12.8 |
| * 13 | 1 | 800. | 0. | 0. | 953. | 0. | 0. | 953. | 1650. | 0. | 0. | 0. | .58 | 62. | 15.4 | B | 21.6 | 12.8 |
| * 14 | 1 | 1400. | 0. | 29. | 953. | 0. | 29. | 953. | 1650. | 0. | 0. | 0. | .58 | 62. | 15.4 | B | 21.6 | 12.8 |
| * 15 | 1 | 1400. | 0. | 0. | 924. | 0. | 0. | 924. | 1650. | 0. | 0. | 0. | .56 | 62. | 14.9 | B | 21.6 | 12.8 |
| * 16 | 1 | 1500. | 0. | 117. | 924. | 0. | 117. | 924. | 1650. | 0. | 0. | 0. | .56 | 62. | 14.9 | B | 21.6 | 12.8 |
| * 17 | 1 | 1500. | 0. | 0. | 807. | 0. | 0. | 807. | 1650. | 0. | 0. | 0. | .49 | 62. | 13.0 | B | 21.6 | 12.8 |
| * 18 | 1 | 5000. | 0. | 807. | 807. | 0. | 807. | 807. | 1650. | 0. | 0. | 0. | .49 | 62. | 13.0 | B | 21.6 | 12.8 |
| * 19 | | | | | | | | | | | | | | | | | | |
| * 20 | | | | | | | | | | | | | | | | | | |
| * TOTAL | | 30640. | = | 5.8 | MI L ES | | | | | MAX(V/C) = 0.58 | | LOWEST LOS = B | | AVG = 62. | 12.7 | | 21.6 | 12.8 |

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|-----------------------------|--------------------|------------|-------------------|------------|
| FREWAY TRAVEL TIME = | 74. | VEH-HRS | 147. | PASS-HRS |
| FREWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 74. | VEH-HRS | 147. | PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 4566. | VEH-MI. | 9133. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. | MPH. | 62. | MPH. |
| AVERAGE DENSITY = | 13. | VPMP | 13. | VPMP |
| TOTAL FUEL = | 212. | GALLONS | 212. | GALLONS |
| TOTAL EMISSIONS = | 58. | KI LOGRAMS | 58. | KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 1.17 | 4 | 0.04 | 5 | 0.04 |
| 6 | 0.04 | 7 | 0.09 | 8 | 0.08 | 9 | 0.08 | 10 | 0.08 |
| 11 | 0.26 | 12 | 0.09 | 13 | 0.11 | 14 | 0.19 | 15 | 0.18 |
| 16 | 0.20 | 17 | 0.17 | 18 | 0.57 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 3.4 VEH-HRS ***** AVERAGE DELAY = 0.26 MIN/VEH *****

 **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 **

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | | |
|--------------|---------------------|------|------|------|------|------|------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| 1 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | 0.00 | 2.38 | 2.94 | 3.89 | 4.42 | 4.70 | 5.62 | 0.00 |
| 3 | 0.00 | 0.00 | 0.00 | 0.00 | 2.23 | 2.50 | 3.42 | 0.00 |
| 4 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.14 | 3.06 | 0.00 |
| 5 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.25 | 0.00 |
| 6 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 7 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMISS | | | |
|---------|--------|----------|--------------|------------------|-------|-------|---------|---------|-----------------|-------|---------|----------------|-----------|-------|---|------|------|
| SEC | LNS | LENGTH | ORG DES SSEC | ORG DES SSEC | CAP | EFF | LENGTH | RATE | RATIO | MPH | VPMP | LEVEL | MPG | GS/VM | | | |
| 1 | | | | | | | | | | | | | | | | | |
| 2 | | | | | | | | | | | | | | | | | |
| 3 | 1 | 12000. | 783. | 0. | 783. | 783. | 0. | 783. | 1650. | 0. | 0. | .47 | 62. | 12.6 | B | 21.6 | 12.8 |
| 4 | 1 | 350. | 209. | 0. | 991. | 209. | 0. | 991. | 1650. | 0. | 0. | .60 | 62. | 16.0 | B | 21.6 | 12.8 |
| 5 | 1 | 300. | 0. | 0. | 991. | 0. | 0. | 991. | 1650. | 0. | 0. | .60 | 62. | 16.0 | B | 21.6 | 12.8 |
| 6 | 1 | 350. | 0. | 185. | 991. | 0. | 185. | 991. | 1650. | 0. | 0. | .60 | 62. | 16.0 | B | 21.6 | 12.8 |
| 7 | 1 | 940. | 0. | 0. | 806. | 0. | 0. | 806. | 1650. | 0. | 0. | .49 | 62. | 13.0 | B | 21.6 | 12.8 |
| 8 | 1 | 700. | 236. | 0. | 1042. | 236. | 0. | 1042. | 1650. | 0. | 0. | .63 | 62. | 16.8 | B | 21.6 | 12.8 |
| 9 | 1 | 700. | 0. | 0. | 1042. | 0. | 0. | 1042. | 1650. | 0. | 0. | .63 | 62. | 16.8 | B | 21.6 | 12.8 |
| 10 | 1 | 700. | 0. | 58. | 1042. | 0. | 58. | 1042. | 1650. | 0. | 0. | .63 | 62. | 16.8 | B | 21.6 | 12.8 |
| 11 | 1 | 2300. | 0. | 0. | 984. | 0. | 0. | 984. | 1650. | 0. | 0. | .60 | 62. | 15.9 | B | 21.6 | 12.8 |
| 12 | 1 | 700. | 154. | 0. | 1138. | 154. | 0. | 1138. | 1650. | 0. | 0. | .69 | 62. | 18.4 | C | 21.6 | 12.8 |
| 13 | 1 | 800. | 0. | 0. | 1138. | 0. | 0. | 1138. | 1650. | 0. | 0. | .69 | 62. | 18.4 | C | 21.6 | 12.8 |
| 14 | 1 | 1400. | 0. | 40. | 1138. | 0. | 40. | 1138. | 1650. | 0. | 0. | .69 | 62. | 18.4 | C | 21.6 | 12.8 |
| 15 | 1 | 1400. | 0. | 0. | 1098. | 0. | 0. | 1098. | 1650. | 0. | 0. | .67 | 62. | 17.7 | B | 21.6 | 12.8 |
| 16 | 1 | 1500. | 0. | 114. | 1098. | 0. | 114. | 1098. | 1650. | 0. | 0. | .67 | 62. | 17.7 | B | 21.6 | 12.8 |
| 17 | 1 | 1500. | 0. | 107. | 983. | 0. | 107. | 983. | 1650. | 0. | 0. | .60 | 62. | 15.9 | B | 21.6 | 12.8 |
| 18 | 1 | 5000. | 0. | 876. | 876. | 0. | 876. | 876. | 1650. | 0. | 0. | .53 | 62. | 14.1 | B | 21.6 | 12.8 |
| 19 | | | | | | | | | | | | | | | | | |
| 20 | | | | | | | | | | | | | | | | | |
| TOTAL | 30640. | = | 5.8 | MI LBS | | | | | MAX(V/C) = 0.69 | | | LOWEST LOS = C | AVG = 62. | 14.7 | | 21.6 | 12.8 |

 * TOTAL 30640. = 5.8 MILES MAX(V/C) = 0.54 LOWEST LOS = B AVG = 62. 11.3 21.6 12.8 *

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|-----------------------------|--------------------|----------------|-------------------|-----------------|
| FREEWAY TRAVEL TIME = | 66. VEH-HRS | 131. PASS-HRS | 225. VEH-HRS | 449. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 66. VEH-HRS | 131. PASS-HRS | 225. VEH-HRS | 449. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 4073. VEH-MI. | 8147. PASS-MI. | 13930. VEH-MI. | 27859. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | | 62. MPH. | |
| AVERAGE DENSITY = | 11. VPMP/L | | 13. VPMP/L | |
| TOTAL FUEL = | 189. GALLONS | | 646. GALLONS | |
| TOTAL EMISSIONS = | 52. KILOGRAMS | | 178. KILOGRAMS | |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 3 OF 3

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.99 | 4 | 0.04 | 5 | 0.03 |
| 6 | 0.04 | 7 | 0.08 | 8 | 0.08 | 9 | 0.08 | 10 | 0.08 |
| 11 | 0.25 | 12 | 0.09 | 13 | 0.10 | 14 | 0.18 | 15 | 0.17 |
| 16 | 0.18 | 17 | 0.16 | 18 | 0.47 | 19 | 0.00 | 20 | 0.00 |

***** TOTAL DELAY = 3.0 VEH-HRS ***** AVERAGE DELAY = 0.26 MIN/VEH *****

```

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ      1111      222222 PPPPPPPP EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF      RRR      RRR EEE      QQQQQ QQQQQ 1111 222 222 PPP      PPP EEE
FFF      RRR      RRR EEE      QQQQ      QQQQ 1111      222 PPP      PPP EEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ      QQQQ 1111      222 PPPPPPPP EEEEEEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ      QQQQ 1111      222 PPPPPPPP EEEEEEE
FFF      RRR      RRR EEE      QQQQ      QQQ QQQ 1111      2222 PPP      EEE
FFF      RRR      RRR EEE      Q*UC*      QQQQ 1111      222 PPP      EEE
FFF      RRR      RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP      EEEEEEEEE
FFF      RRR      RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP      EEEEEEEEE
    
```

FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 2.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 30
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREWAY AND ARTERIAL DESIGN FEATURES

| ** SUB NO. | ** SSEC | ** SSEC | ** DESIG N | ** ORG | ** TRK | ** SSEC | ** PCT | ** PCT | ** DES | ** SPECIAL | ** FF. SPD. | ** CAP. | ** ART | ** GRADE | ** SUBSECTI ON | ** LOCATI ON |
|------------|---------|---------|------------|----------|--------|---------|--------|-----------|---------|-------------|-------------|---------|-------------|-------------|--------------------------|--------------|
| ** SEC | ** LNS | ** CAP | ** LENGTH | ** SPEED | ** DES | ** GRAD | ** TRK | ** TRUCKS | ** RAMP | ** ALT. RTE | ** ALT. RTE | ** TYPE | ** ALT. RTE | ** ALT. RTE | ** LOCATION | ** LOCATION |
| ** 1 | 3 | 6000. | 500. | 65 | 0 | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Seed | ** |
| ** 2 | 3 | 6000. | 99999. | 65 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | ** |
| ** 3 | 2 | 4000. | 11000. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | ** |
| ** 4 | 2 | 4000. | 1500. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence On-ramp | ** |
| ** 5 | 2 | 4000. | 1400. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence to Crossman | ** |
| ** 6 | 2 | 4000. | 1500. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Crossman On-Ramp | ** |
| ** 7 | 2 | 4000. | 1300. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Crossman / Mathilda | ** |
| ** 8 | 3 | 5630. | 500. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-Ramp | ** |
| ** 9 | 2 | 4000. | 2300. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | ** |
| ** 10 | 3 | 4390. | 250. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda On-Ramp | ** |
| ** 11 | 3 | 4390. | 200. | 62 | | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda to US-101 | ** |
| ** 12 | 3 | 4390. | 250. | 62 | D | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US-101 Off-Ramp | ** |
| ** 13 | 2 | 4000. | 50. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bottleneck by-pass | ** |
| ** 14 | 2 | 2400. | 50. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bottleneck | ** |
| ** 15 | 2 | 4000. | 1000. | 62 | OD | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US 101 / US 101 | ** |
| ** 16 | 2 | 4000. | 10. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Dummy end of travel time | ** |
| ** 17 | 2 | 4000. | 1500. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US 101 NB On-Ramp | ** |
| ** 18 | 2 | 4000. | 1500. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Maude Off-ramp | ** |
| ** 19 | 2 | 4000. | 12000. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | ** |
| ** 20 | 3 | 6000. | 500. | 65 | OD | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End Of HOV | ** |

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 UNIVERSITY OF CALIFORNIA, BERKELEY

***** INPUT HAS BEEN COMPLETED *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 3/30/2016 10:25 PAGE 4
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 1 OF 4

QUEUE COLLISION IN SECTION 4 T2 =0.116

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 3/30/2016 10:25 PAGE 5
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 1 OF 4

 ** FREeway TRAVEL TIME (MINUTES) **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | |
|-----------|---|-----------------------|-------|-------|-------|-------|-------|-------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| + | * | 19.27 | 25.53 | 26.08 | 26.09 | 26.28 | 26.83 | 29.12 |
| + | * | 0.00 | 2.39 | 2.94 | 2.95 | 3.14 | 3.70 | 5.98 |
| + | * | 0.00 | 0.70 | 1.26 | 1.27 | 1.46 | 2.01 | 4.30 |
| + | * | 0.00 | 0.00 | 0.13 | 0.14 | 0.33 | 0.88 | 3.17 |
| + | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.18 | 0.73 | 3.02 |
| + | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.55 | 2.84 |
| + | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.09 |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 1 OF 4

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB | * NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|---------|-------|----------|------------|-------------|------------|-----------|---------|-----------------|-----------|----------------|---------|-----------|-----------|---------|--------|-------------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 1 | * 3 | * 500. | * 5389. | * 0. | * 5389. | * 5389. | * 0. | * 5389. | * 6000. | * 0. | * 0. | * .90 | * 59. | * 30.3 | * D | * 21.6 |
| * 2 | * 3 | * 99999. | * 0. | * 1401. | * 5389. | * 0. | * 1401. | * 5389. | * 6000. | * 0. | * 0. | * .90 | * 59. | * 30.3 | * D | * 21.6 |
| * 3 | * 2 | * 11000. | * 0. | * 0. | * 3988. | * 0. | * 0. | * 3424. | * 4000. | * 0. | * * | * 9691. | * 564. | * .86 | * 32. | * 53.1 |
| * 4 | * 2 | * 1500. | * 26. | * 0. | * 4014. | * 26. | * 0. | * 3450. | * 3996. | * 0. | * ** | * 1500. | * 546. | * .86 | * 21. | * 84.1 |
| * 5 | * 2 | * 1400. | * 0. | * 0. | * 4014. | * 0. | * 0. | * 3450. | * 4000. | * 0. | * ** | * 1400. | * 546. | * .86 | * 19. | * 92.5 |
| * 6 | * 2 | * 1500. | * 489. | * 0. | * 4503. | * 489. | * 0. | * 3939. | * 3939. | * 0. | * 0. | * 1.00 | * 52. | * 38.2 | * E | * 23.6 |
| * 7 | * 2 | * 1300. | * 0. | * 0. | * 4503. | * 0. | * 0. | * 3939. | * 4000. | * 0. | * 0. | * .98 | * 53. | * 37.3 | * E | * 23.4 |
| * 8 | * 3 | * 500. | * 0. | * 918. | * 4503. | * 0. | * 805. | * 3939. | * 5348. | * 0. | * 0. | * .74 | * 62. | * 21.2 | * C | * 20.3 |
| * 9 | * 2 | * 2300. | * 0. | * 0. | * 3585. | * 0. | * 0. | * 3134. | * 4000. | * 0. | * 0. | * .78 | * 61. | * 25.6 | * C | * 20.7 |
| * 10 | * 3 | * 250. | * 172. | * 0. | * 3757. | * 172. | * 0. | * 3306. | * 4362. | * 0. | * 0. | * .76 | * 62. | * 17.8 | * B | * 20.3 |
| * 11 | * 3 | * 200. | * 0. | * 0. | * 3757. | * 0. | * 0. | * 3306. | * 4390. | * 0. | * 0. | * .75 | * 62. | * 17.8 | * B | * 20.3 |
| * 12 | * 3 | * 250. | * 0. | * 1245. | * 3757. | * 0. | * 1099. | * 3306. | * 4028. | * 0. | * 0. | * .82 | * 62. | * 17.8 | * B | * 20.3 |
| * 13 | * 2 | * 50. | * 0. | * 0. | * 2512. | * 0. | * 0. | * 2207. | * 4000. | * 0. | * 0. | * .55 | * 62. | * 17.8 | * B | * 20.3 |
| * 14 | * 2 | * 50. | * 0. | * 0. | * 2512. | * 0. | * 0. | * 2207. | * 2400. | * 0. | * 0. | * .92 | * 62. | * 17.8 | * B | * 20.3 |
| * 15 | * 2 | * 1000. | * 0. | * 0. | * 2512. | * 0. | * 0. | * 2207. | * 4000. | * 0. | * 0. | * .55 | * 62. | * 17.8 | * B | * 20.3 |
| * 16 | * 2 | * 10. | * 0. | * 0. | * 2512. | * 0. | * 0. | * 2207. | * 4000. | * 0. | * 0. | * .55 | * 62. | * 17.8 | * B | * 20.3 |
| * 17 | * 2 | * 1500. | * 537. | * 0. | * 3049. | * 537. | * 0. | * 2744. | * 3862. | * 0. | * 0. | * .71 | * 62. | * 22.1 | * C | * 20.3 |
| * 18 | * 2 | * 1500. | * 0. | * 698. | * 3049. | * 0. | * 633. | * 2744. | * 3838. | * 0. | * 0. | * .72 | * 62. | * 22.1 | * C | * 20.3 |
| * 19 | * 2 | * 12000. | * 0. | * 0. | * 2351. | * 0. | * 0. | * 2111. | * 4000. | * 0. | * 0. | * .53 | * 62. | * 17.0 | * B | * 20.3 |
| * 20 | * 3 | * 500. | * 826. | * 3177. | * 3177. | * 826. | * 2937. | * 2937. | * 6000. | * 0. | * 0. | * .49 | * 65. | * 15.1 | * B | * 19.0 |
| * TOTAL | | 137309. | = | 26.0 MI LBS | | | | MAX(V/C) = 1.00 | | LOWEST LOS = F | | AVG = 55. | | 31.8 | 21.4 | 12.4 |

SR-237_WB_AM_NP_2040_PE

| | CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | |
|----------------------------|--------------------|------------|--------|----------|-------------------|------------|--------|----------|
| FREEWAY TRAVEL TIME = | 1132. | VEH-HRS | 1359. | PASS-HRS | 1132. | VEH-HRS | 1359. | PASS-HRS |
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1132. | VEH-HRS | 1359. | PASS-HRS | 1132. | VEH-HRS | 1359. | PASS-HRS |
| TOTAL TRAV DISTANCE = | 61888. | VEH-MI. | 75352. | PASS-MI. | 61888. | VEH-MI. | 75352. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 55. | MPH | | | 55. | MPH | | |
| AVERAGE DENSITY = | 32. | VPMP | | | 32. | VPMP | | |
| TOTAL FUEL = | 2891. | GALLONS | | | 2891. | GALLONS | | |
| TOTAL EMISSIONS = | 767. | KI LOGRAMS | | | 767. | KI LOGRAMS | | |

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SIMULATION AFTER CONTROL, NO DIVERSION
TIME SLICE 1 OF 4

***** MAINTLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.38 | 2 | 75.76 | 3 | 61.73 | 4 | 16.80 | 5 | 17.66 |
| 6 | 2.24 | 7 | 1.73 | 8 | 0.14 | 9 | 0.64 | 10 | 0.06 |
| 11 | 0.05 | 12 | 0.06 | 13 | 0.01 | 14 | 0.01 | 15 | 0.16 |
| 16 | 0.00 | 17 | 0.29 | 18 | 0.29 | 19 | 1.79 | 20 | 0.00 |

***** TOTAL DELAY = 179.8 VEH-HRS ***** AVERAGE DELAY = 2.67 MIN/VEH *****

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SIMULATION AFTER CONTROL, NO DIVERSION
TIME SLICE 2 OF 4

**
** FREEWAY TRAVEL TIME (MINUTES) **
**

| * ORIGINS * DOWN | * DESTINATIONS ACROSS | | | | | | |
|---------------------|-----------------------|-------|-------|-------|-------|-------|-------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 20.58 | 30.25 | 30.80 | 30.81 | 31.00 | 31.55 | 33.84 |
| * 2 * | 0.00 | 2.55 | 3.10 | 3.11 | 3.30 | 3.85 | 6.14 |
| * 3 * | 0.00 | 0.70 | 1.26 | 1.27 | 1.46 | 2.01 | 4.30 |
| * 4 * | 0.00 | 0.00 | 0.13 | 0.14 | 0.33 | 0.88 | 3.17 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.18 | 0.73 | 3.02 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.55 | 2.84 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.09 |

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SIMULATION AFTER CONTROL, NO DIVERSION
TIME SLICE 2 OF 4

* TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB * SEC | * NO. * LNS | * SSEC * LENGTH | * O-D DATA * ORG DES | * DEMANDS * SSEC | * ADJUSTED * ORG DES | * VOLUMES * SSEC | * SSEC * CAP. | * WEAVE * EFF | * CONGEST * LENGTH | * STORAGE * RATE | * V/C * RATIO | * SPEED * MPH | * DENSITY * VPMP | * LOS * LEVEL | * FUEL * MPG | * EMISSIONS * GS/VM | | |
|----------------|----------------|--------------------|-------------------------|---------------------|-------------------------|---------------------|------------------|------------------|-----------------------|---------------------|------------------|------------------|---------------------|------------------|-----------------|------------------------|------|------|
| * 1 | 3 | 500. | 5389. | 0. | 5389. | 5389. | 0. | 5389. | 6000. | 0. | 0. | .90 | 59. | 30.3 | D | 21.6 | 12.2 | |
| * 2 | 3 | 99999. | 0. | 1401. | 5389. | 0. | 1401. | 4825. | 6000. | 0. | * 5623. | 564. | .80 | 55. | 29.0 | F | 21.4 | 12.4 |
| * 3 | 2 | 11000. | 0. | 0. | 3988. | 0. | 0. | 3424. | 4000. | 0. | * 11000. | 564. | .86 | 18. | 97.6 | F | 17.1 | 17.5 |
| * 4 | 2 | 1500. | 26. | 0. | 4014. | 26. | 0. | 3450. | 3996. | 0. | * 1500. | 546. | .86 | 18. | 96.3 | F | 17.3 | 17.3 |
| * 5 | 2 | 1400. | 0. | 0. | 4014. | 0. | 0. | 3450. | 4000. | 0. | * 1400. | 546. | .86 | 18. | 96.6 | F | 17.3 | 17.3 |
| * 6 | 2 | 1500. | 489. | 0. | 4503. | 489. | 0. | 3939. | 3939. | 0. | 0. | 1.00 | 52. | 38.2 | E | 23.6 | 11.1 | |
| * 7 | 2 | 1300. | 0. | 0. | 4503. | 0. | 0. | 3939. | 4000. | 0. | 0. | .98 | 53. | 37.3 | E | 23.4 | 11.2 | |
| * 8 | 3 | 500. | 0. | 918. | 4503. | 0. | 805. | 3939. | 5348. | 0. | 0. | .74 | 62. | 21.2 | C | 20.3 | 13.0 | |
| * 9 | 2 | 2300. | 0. | 0. | 3585. | 0. | 0. | 3134. | 4000. | 0. | 0. | .78 | 61. | 25.6 | C | 20.7 | 12.8 | |
| * 10 | 3 | 250. | 172. | 0. | 3757. | 172. | 0. | 3306. | 4362. | 0. | 0. | .76 | 62. | 17.8 | B | 20.3 | 13.0 | |
| * 11 | 3 | 200. | 0. | 0. | 3757. | 0. | 0. | 3306. | 4390. | 0. | 0. | .75 | 62. | 17.8 | B | 20.3 | 13.0 | |
| * 12 | 3 | 250. | 0. | 1245. | 3757. | 0. | 1099. | 3306. | 4028. | 0. | 0. | .82 | 62. | 17.8 | B | 20.3 | 13.0 | |
| * 13 | 2 | 50. | 0. | 0. | 2512. | 0. | 0. | 2207. | 4000. | 0. | 0. | .55 | 62. | 17.8 | B | 20.3 | 13.0 | |
| * 14 | 2 | 50. | 0. | 0. | 2512. | 0. | 0. | 2207. | 2400. | 0. | 0. | .92 | 62. | 17.8 | B | 20.3 | 13.0 | |
| * 15 | 2 | 1000. | 0. | 0. | 2512. | 0. | 0. | 2207. | 4000. | 0. | 0. | .55 | 62. | 17.8 | B | 20.3 | 13.0 | |
| * 16 | 2 | 10. | 0. | 0. | 2512. | 0. | 0. | 2207. | 4000. | 0. | 0. | .55 | 62. | 17.8 | B | 20.3 | 13.0 | |
| * 17 | 2 | 1500. | 537. | 0. | 3049. | 537. | 0. | 2744. | 3862. | 0. | 0. | .71 | 62. | 22.1 | C | 20.3 | 13.0 | |

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| | | | | | | | | | | | | | | | | | |
|------|---|--------|------|-------|-------|------|-------|-------|-------|----|----|-----|-----|------|---|------|------|
| * 18 | 2 | 1500. | 0. | 698. | 3049. | 0. | 633. | 2744. | 3838. | 0. | 0. | .72 | 62. | 22.1 | C | 20.3 | 13.0 |
| * 19 | 2 | 12000. | 0. | 0. | 2351. | 0. | 0. | 2111. | 4000. | 0. | 0. | .53 | 62. | 17.0 | B | 20.3 | 13.0 |
| * 20 | 3 | 500. | 826. | 3177. | 3177. | 826. | 2937. | 2937. | 6000. | 0. | 0. | .49 | 65. | 15.1 | B | 19.0 | 14.1 |

| | | | | | | | | | | | | | | | | | |
|---------|---------|---|------|-------|--|--|--|--|--|-----------------|----------------|-----------|------|--|--|------|------|
| * TOTAL | 137309. | = | 26.0 | MILES | | | | | | | | | | | | | |
| | | | | | | | | | | MAX(V/C) = 1.00 | LOWEST LOS = F | AVG = 48. | 34.6 | | | 21.0 | 12.8 |

| | CURRENT TIME SLICE | | CUMULATIVE VALUES |
|----------------------------|--------------------|-----------------|----------------------------------|
| FREEWAY TRAVEL TIME = | 1273. VEH-HRS | 1515. PASS-HRS | 2405. VEH-HRS 2874. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1273. VEH-HRS | 1515. PASS-HRS | 2405. VEH-HRS 2874. PASS-HRS |
| TOTAL TRAV DISTANCE = | 61353. VEH-MI. | 74781. PASS-MI. | 123241. VEH-MI. 150133. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 48. MPH. | | 51. MPH. |
| AVERAGE DENSITY = | 35. VPMPPL | | 33. VPMPPL |
| TOTAL FUEL = | 2927. GALLONS | | 5818. GALLONS |
| TOTAL EMISSIONS = | 785. KI LOGRAMS | | 1552. KI LOGRAMS |

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 TIME SLICE 2 OF 4

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|--------|------------|--------|------------|-------|------------|-------|
| 1 | 0.38 | 2 | 134.34 | 3 | 148.55 | 4 | 19.83 | 5 | 18.58 |
| 6 | 2.24 | 7 | 1.73 | 8 | 0.14 | 9 | 0.64 | 10 | 0.06 |
| 11 | 0.05 | 12 | 0.06 | 13 | 0.01 | 14 | 0.01 | 15 | 0.16 |
| 16 | 0.00 | 17 | 0.29 | 18 | 0.29 | 19 | 1.79 | 20 | 0.00 |

***** TOTAL DELAY = 329.1 VEH-HRS ***** AVERAGE DELAY = 5.09 MIN/VEH *****

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 TIME SLICE 3 OF 4

 ** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS DOWN | * DESTINATIONS ACROSS * | | | | | | |
|----------------|-------------------------|-------|-------|-------|-------|-------|-------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 26.56 | 37.85 | 38.40 | 38.41 | 38.60 | 39.18 | 41.47 |
| * 2 * | 0.00 | 2.86 | 3.41 | 3.42 | 3.61 | 4.19 | 6.47 |
| * 3 * | 0.00 | 0.70 | 1.25 | 1.26 | 1.45 | 2.03 | 4.32 |
| * 4 * | 0.00 | 0.00 | 0.13 | 0.14 | 0.33 | 0.91 | 3.19 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.18 | 0.76 | 3.05 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.58 | 2.86 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.09 |

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 TIME SLICE 3 OF 4

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB SEC | * NO. LNS | * SSEC LENGTH | * O-D DATA ORG DES | * DEMANDS SSEC | * ADJUSTED ORG DES | * VOLUMES SSEC | * SSEC CAP. | * WEAVE EFF | * CONGEST LENGTH | * STORAGE RATE | * V/C RATIO | * SPEED MPH | * DENSITY VPMPPL | * LOS LEVEL | * FUEL MPG | * EMISSIONS GS/VM | |
|-----------|-----------|---------------|--------------------|----------------|--------------------|----------------|-------------|-------------|------------------|----------------|-------------|-------------|------------------|-------------|------------|-------------------|------|
| * 1 | 3 | 500. | 5780. | 0. | 5780. | 5780. | 0. | 5780. | 6000. | 0. | 0. | .96 | 55. | 34.9 | D | 22.8 | |
| * 2 | 3 | 99999. | 0. | 1503. | 5780. | 0. | 1503. | 4730. | 6000. | 0. | * 17491. | 1050. | .79 | 43. | 36.7 | F | 21.8 |
| * 3 | 2 | 11000. | 0. | 0. | 4277. | 0. | 0. | 3227. | 4000. | 0. | * 11000. | 773. | .81 | 15. | 108.8 | F | 15.9 |
| * 4 | 2 | 1500. | 34. | 0. | 4311. | 34. | 0. | 3261. | 3995. | 0. | * 1500. | 734. | .82 | 15. | 106.6 | F | 16.2 |
| * 5 | 2 | 1400. | 0. | 0. | 4311. | 0. | 0. | 3261. | 4000. | 0. | * 1400. | 734. | .82 | 15. | 106.9 | F | 16.2 |

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| | | | | | | | | | | | | | | | | | | | | |
|---|----|---|--------|------|-------|-------|------|-------|-------|-------|----|----|------|-----|------|------|------|------|------|---|
| * | 6 | 2 | 1500. | 672. | 0. | 4983. | 672. | 0. | 3933. | 3933. | 0. | 0. | 1.00 | 52. | 38.1 | E | 23.6 | 11.1 | * | |
| * | 7 | 2 | 1300. | 0. | 0. | 4983. | 0. | 0. | 3933. | 4000. | 0. | 0. | 0. | .98 | 53. | 37.2 | E | 23.3 | 11.2 | * |
| * | 8 | 3 | 500. | 0. | 1264. | 4983. | 0. | 1001. | 3933. | 5254. | 0. | 0. | 0. | .75 | 62. | 21.1 | C | 20.3 | 13.0 | * |
| * | 9 | 2 | 2300. | 0. | 0. | 3719. | 0. | 0. | 2932. | 4000. | 0. | 0. | 0. | .73 | 62. | 23.6 | C | 20.3 | 13.0 | * |
| * | 10 | 3 | 250. | 237. | 0. | 3956. | 237. | 0. | 3169. | 4358. | 0. | 0. | 0. | .73 | 62. | 17.0 | B | 20.3 | 13.0 | * |
| * | 11 | 3 | 200. | 0. | 0. | 3956. | 0. | 0. | 3169. | 4390. | 0. | 0. | 0. | .72 | 62. | 17.0 | B | 20.3 | 13.0 | * |
| * | 12 | 3 | 250. | 0. | 1099. | 3956. | 0. | 886. | 3169. | 4085. | 0. | 0. | 0. | .78 | 62. | 17.0 | B | 20.3 | 13.0 | * |
| * | 13 | 2 | 50. | 0. | 273. | 2857. | 0. | 220. | 2283. | 3924. | 0. | 0. | 0. | .58 | 62. | 18.4 | C | 20.3 | 13.0 | * |
| * | 14 | 2 | 50. | 0. | 0. | 2584. | 0. | 0. | 2063. | 2400. | 0. | 0. | 0. | .86 | 62. | 16.6 | B | 20.3 | 13.0 | * |
| * | 15 | 2 | 1000. | 287. | 0. | 2871. | 287. | 0. | 2350. | 3937. | 0. | 0. | 0. | .60 | 62. | 19.0 | C | 20.3 | 13.0 | * |
| * | 16 | 2 | 10. | 0. | 0. | 2871. | 0. | 0. | 2350. | 4000. | 0. | 0. | 0. | .59 | 62. | 19.0 | C | 20.3 | 13.0 | * |
| * | 17 | 2 | 1500. | 923. | 0. | 3794. | 923. | 0. | 3273. | 3796. | 0. | 0. | 0. | .86 | 59. | 27.6 | D | 21.6 | 12.2 | * |
| * | 18 | 2 | 1500. | 0. | 1259. | 3794. | 0. | 1101. | 3273. | 3773. | 0. | 0. | 0. | .87 | 59. | 27.7 | D | 21.6 | 12.2 | * |
| * | 19 | 2 | 12000. | 0. | 0. | 2535. | 0. | 0. | 2172. | 4000. | 0. | 0. | 0. | .54 | 62. | 17.5 | B | 20.3 | 13.0 | * |
| * | 20 | 3 | 500. | 891. | 3426. | 3426. | 891. | 3063. | 3063. | 6000. | 0. | 0. | 0. | .51 | 65. | 15.7 | B | 19.0 | 14.1 | * |

 * TOTAL 137309. = 26.0 MI LES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 39. 41.5 21.2 12.7 *

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------------------|----------------------------------|
| FREEWAY TRAVEL TIME = | 1636. VEH-HRS 1964. PASS-HRS | 4041. VEH-HRS 4838. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1636. VEH-HRS 1964. PASS-HRS | 4041. VEH-HRS 4838. PASS-HRS |
| TOTAL TRAV DISTANCE = | 63982. VEH-MI. 78121. PASS-MI. | 187222. VEH-MI. 228254. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 39. MPH | 46. MPH |
| AVERAGE DENSITY = | 42. VPML | 36. VPML |
| TOTAL FUEL = | 3018. GALLONS | 8836. GALLONS |
| TOTAL EMISSIONS = | 814. KI LOGRAMS | 2366. KI LOGRAMS |

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 TIME SLICE 3 OF 4

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|--------|------------|--------|------------|-------|------------|-------|
| 1 | 0.75 | 2 | 423.43 | 3 | 174.89 | 4 | 23.15 | 5 | 21.70 |
| 6 | 2.24 | 7 | 1.71 | 8 | 0.14 | 9 | 0.48 | 10 | 0.06 |
| 11 | 0.04 | 12 | 0.06 | 13 | 0.01 | 14 | 0.01 | 15 | 0.17 |
| 16 | 0.00 | 17 | 0.68 | 18 | 0.71 | 19 | 1.84 | 20 | 0.00 |

***** TOTAL DELAY = 652.0 VEH-HRS ***** AVERAGE DELAY = 9.61 MIN/VEH *****

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 TIME SLICE 4 OF 4

 ** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS DOWN | * DESTINATIONS ACROSS * | | | | | | |
|----------------|-------------------------|-------|-------|-------|-------|-------|-------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 32.85 | 44.14 | 44.69 | 44.70 | 44.89 | 45.47 | 47.75 |
| * 2 * | 0.00 | 2.86 | 3.41 | 3.42 | 3.61 | 4.19 | 6.47 |
| * 3 * | 0.00 | 0.70 | 1.25 | 1.26 | 1.45 | 2.03 | 4.32 |
| * 4 * | 0.00 | 0.00 | 0.13 | 0.14 | 0.33 | 0.91 | 3.19 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.18 | 0.76 | 3.05 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.58 | 2.86 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.09 |

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 TIME SLICE 4 OF 4

SR-237_WB_AM_NP_2040_PE
TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED | VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSI TY | LOS | FUEL | EMI SS |
|---|--------|----------|---------|----------|---------|-------|-------|---------|---------|-------|----------|----------|-------|------|--------|
| SEC LNS | LENGTH | ORG DES | SSEC | ORG DES | SSEC | CAP. | EFF | LENGTH | RATE | RATIO | MPH | VPMP | LEVEL | MPG | GS/VM |
| * 1 | 3 | 500. | 5780. | 0. | 5780. | 5780. | 0. | 5780. | 6000. | 0. | 0. | 34.9 | D | 22.8 | 11.4 |
| * 2 | 3 | 99999. | 0. | 1503. | 5780. | 0. | 1503. | 4730. | 6000. | 0. | * 29359. | 35. | F | 20.8 | 13.1 |
| * 3 | 2 | 11000. | 0. | 0. | 4277. | 0. | 0. | 3227. | 4000. | 0. | **11000. | 15. | F | 15.9 | 19.1 |
| * 4 | 2 | 1500. | 34. | 0. | 4311. | 34. | 0. | 3261. | 3995. | 0. | ** 1500. | 15. | F | 16.2 | 18.8 |
| * 5 | 2 | 1400. | 0. | 0. | 4311. | 0. | 0. | 3261. | 4000. | 0. | ** 1400. | 15. | F | 16.2 | 18.8 |
| * 6 | 2 | 1500. | 672. | 0. | 4983. | 672. | 0. | 3933. | 3933. | 0. | 0. | 52. | E | 23.6 | 11.1 |
| * 7 | 2 | 1300. | 0. | 0. | 4983. | 0. | 0. | 3933. | 4000. | 0. | 0. | 53. | E | 23.3 | 11.2 |
| * 8 | 3 | 500. | 0. | 1264. | 4983. | 0. | 1001. | 3933. | 5254. | 0. | 0. | 62. | C | 20.3 | 13.0 |
| * 9 | 2 | 2300. | 0. | 0. | 3719. | 0. | 0. | 2932. | 4000. | 0. | 0. | 62. | C | 20.3 | 13.0 |
| * 10 | 3 | 250. | 237. | 0. | 3956. | 237. | 0. | 3169. | 4358. | 0. | 0. | 62. | B | 20.3 | 13.0 |
| * 11 | 3 | 200. | 0. | 0. | 3956. | 0. | 0. | 3169. | 4390. | 0. | 0. | 62. | B | 20.3 | 13.0 |
| * 12 | 3 | 250. | 0. | 1099. | 3956. | 0. | 886. | 3169. | 4085. | 0. | 0. | 62. | B | 20.3 | 13.0 |
| * 13 | 2 | 50. | 0. | 273. | 2857. | 0. | 220. | 2283. | 3924. | 0. | 0. | 62. | C | 20.3 | 13.0 |
| * 14 | 2 | 50. | 0. | 0. | 2584. | 0. | 0. | 2063. | 2400. | 0. | 0. | 62. | B | 20.3 | 13.0 |
| * 15 | 2 | 1000. | 287. | 0. | 2871. | 287. | 0. | 2350. | 3937. | 0. | 0. | 62. | C | 20.3 | 13.0 |
| * 16 | 2 | 10. | 0. | 0. | 2871. | 0. | 0. | 2350. | 4000. | 0. | 0. | 62. | C | 20.3 | 13.0 |
| * 17 | 2 | 1500. | 923. | 0. | 3794. | 923. | 0. | 3273. | 3796. | 0. | 0. | 59. | D | 21.6 | 12.2 |
| * 18 | 2 | 1500. | 0. | 1259. | 3794. | 0. | 1101. | 3273. | 3773. | 0. | 0. | 59. | D | 21.6 | 12.2 |
| * 19 | 2 | 12000. | 0. | 0. | 2535. | 0. | 0. | 2172. | 4000. | 0. | 0. | 62. | B | 20.3 | 13.0 |
| * 20 | 3 | 500. | 891. | 3426. | 3426. | 891. | 3063. | 3063. | 6000. | 0. | 0. | 65. | B | 19.0 | 14.1 |
| ***** | | | | | | | | | | | | | | | |
| * TOTAL 137309. = 26.0 MI LES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 33. 47.9 20.4 13.4 * | | | | | | | | | | | | | | | |
| ***** | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 1899. VEH-HRS | 2295. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1899. VEH-HRS | 2295. PASS-HRS |
| TOTAL TRAV DISTANCE = | 62802. VEH-MI. | 76634. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 33. MPH | 42. MPH |
| AVERAGE DENSITY = | 48. VPMP | 39. VPMP |
| TOTAL FUEL = | 3080. GALLONS | 11916. GALLONS |
| TOTAL EMISSIONS = | 845. KI LOGRAMS | 3211. KI LOGRAMS |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 3/30/2016 10:25 PAGE 16
UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
TIME SLICE 4 OF 4

***** MAINTENANCE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|--------|------------|--------|------------|-------|------------|-------|
| 1 | 0.75 | 2 | 704.09 | 3 | 174.89 | 4 | 23.15 | 5 | 21.70 |
| 6 | 2.24 | 7 | 1.71 | 8 | 0.14 | 9 | 0.48 | 10 | 0.06 |
| 11 | 0.04 | 12 | 0.06 | 13 | 0.01 | 14 | 0.01 | 15 | 0.17 |
| 16 | 0.00 | 17 | 0.68 | 18 | 0.71 | 19 | 1.84 | 20 | 0.00 |

***** TOTAL DELAY = 932.7 VEH-HRS ***** AVERAGE DELAY = 13.17 MIN/VEH *****

```

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQQ QQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 2222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 11111111 2222222222 PPP LLLLLLLLLL
    
```

FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 3 AND 19 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 2.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 30
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

```

*****
**
**                                     FREeway AND ARTERIAL DESIGN FEATURES
**
*****
**
** SUB NO.   SSEC   SSEC   DESIGN   ORG   TRK   SSEC   PCT   PCT   DES   SPECIAL   FF   CAP.   ART   GRADE   SUBSECTI ON LOCATI ON
** SEC  LNS   CAP   LENGTH  SPEED  DES   FAC   GRAD  TRK   TRUCKS  RAMP   ALT.  ALT.  RTE  TYPE  ALT.  RTE
**
**
** 1
** 2
** 3 1 1650. 11000. 62 0 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 HOV Dummy
** 4 1 1650. 1500. 62 0 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Lawrence On-ramp
** 5 1 1650. 1400. 62 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Lawrence to Crossman
** 6 1 1650. 1500. 62 0 0.95 0.0 0 100 YES 0.0 0. GOOD 0.0 Crossman On-Ramp
** 7 1 1650. 1300. 62 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Crossman / Mathilda
** 8 1 1650. 500. 62 D 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Mathilda Off-Ramp
** 9 1 1650. 2300. 62 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Mathilda / Mathilda
** 10 1 1650. 250. 62 0 0.95 0.0 0 100 YES 0.0 0. GOOD 0.0 Mathilda On-Ramp
** 11 1 1650. 200. 62 0.95 0.0 0 100 YES 0.0 0. GOOD 0.0 Mathilda to US-101
** 12 1 1650. 250. 62 D 0.95 0.0 0 100 YES 0.0 0. GOOD 0.0 US-101 Off-Ramp
** 13 1 1650. 50. 62 D 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Bottleneck by-pass
** 14 1 1650. 50. 62 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Bottleneck
** 15 1 1650. 1000. 62 OD 0.95 0.0 0 100 YES 0.0 0. GOOD 0.0 US 101 / US 101
** 16 1 1650. 10. 62 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Dummy end of travel time
** 17 1 1650. 1500. 62 0 0.95 0.0 0 100 YES 0.0 0. GOOD 0.0 US 101 NB On-Ramp
** 18 1 1650. 1500. 62 D 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Maude Off-ramp
    
```

```

**
** 19 1 1650. 12000. 62 D 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 HOV Dummy
**
** 20
**
*****

```

```

*****
**
** FREEWAY TRAVEL TIME (MINUTES)
**
*****

```

| ***** | | | | | | | | | |
|-----------|-------------------------|------|------|------|------|------|------|------|---|
| * ORIGINS | * DESTINATIONS ACROSS * | | | | | | | | |
| * DOWN | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | * |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | * |
| * 2 * | 0.00 | 3.15 | 3.70 | 3.71 | 3.90 | 4.46 | 6.66 | 0.00 | * |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.44 | 4.64 | 0.00 | * |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 4.11 | 0.00 | * |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.08 | 0.00 | * |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.93 | 0.00 | * |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.75 | 0.00 | * |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | * |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | | |
|-----------|--------|------------|-----------|------------|--------|---------|-----------|-----------|---------|-----------------|-----------|----------------|--------|-------------|------|---|------|------|
| * SEC | * LNS | * LENGTH | * ORG DES | * ORG DES | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP/L | * LEVEL | * MPG | * GS/VM | | | | |
| * 1 | | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | | |
| * 3 | 1 | 11000. | 1401. | 0. | 1401. | 1401. | 0. | 1401. | 1650. | 0. | 0. | 0. | .85 | 62. | 22.6 | C | 21.6 | 12.8 |
| * 4 | 1 | 1500. | 4. | 0. | 1405. | 4. | 0. | 1405. | 1650. | 0. | 0. | 0. | .85 | 62. | 22.7 | C | 21.6 | 12.8 |
| * 5 | 1 | 1400. | 0. | 0. | 1405. | 0. | 0. | 1405. | 1650. | 0. | 0. | 0. | .85 | 62. | 22.7 | C | 21.6 | 12.8 |
| * 6 | 1 | 1500. | 61. | 0. | 1466. | 61. | 0. | 1466. | 1650. | 0. | 0. | 0. | .89 | 62. | 23.6 | C | 21.6 | 12.8 |
| * 7 | 1 | 1300. | 0. | 0. | 1466. | 0. | 0. | 1466. | 1650. | 0. | 0. | 0. | .89 | 62. | 23.6 | C | 21.6 | 12.8 |
| * 8 | 1 | 500. | 0. | 282. | 1466. | 0. | 282. | 1466. | 1650. | 0. | 0. | 0. | .89 | 62. | 23.6 | C | 21.6 | 12.8 |
| * 9 | 1 | 2300. | 0. | 0. | 1185. | 0. | 0. | 1185. | 1650. | 0. | 0. | 0. | .72 | 62. | 19.1 | C | 21.6 | 12.8 |
| * 10 | 1 | 250. | 28. | 0. | 1212. | 28. | 0. | 1212. | 1650. | 0. | 0. | 0. | .73 | 62. | 19.6 | C | 21.6 | 12.8 |
| * 11 | 1 | 200. | 0. | 0. | 1212. | 0. | 0. | 1212. | 1650. | 0. | 0. | 0. | .73 | 62. | 19.6 | C | 21.6 | 12.8 |
| * 12 | 1 | 250. | 0. | 362. | 1212. | 0. | 362. | 1212. | 1650. | 0. | 0. | 0. | .73 | 62. | 19.6 | C | 21.6 | 12.8 |
| * 13 | 1 | 50. | 0. | 0. | 850. | 0. | 0. | 850. | 1650. | 0. | 0. | 0. | .52 | 62. | 13.7 | B | 21.6 | 12.8 |
| * 14 | 1 | 50. | 0. | 0. | 850. | 0. | 0. | 850. | 1650. | 0. | 0. | 0. | .52 | 62. | 13.7 | B | 21.6 | 12.8 |
| * 15 | 1 | 1000. | 0. | 0. | 850. | 0. | 0. | 850. | 1650. | 0. | 0. | 0. | .52 | 62. | 13.7 | B | 21.6 | 12.8 |
| * 16 | 1 | 10. | 0. | 0. | 850. | 0. | 0. | 850. | 1650. | 0. | 0. | 0. | .52 | 62. | 13.7 | B | 21.6 | 12.8 |
| * 17 | 1 | 1500. | 138. | 0. | 988. | 138. | 0. | 988. | 1650. | 0. | 0. | 0. | .60 | 62. | 15.9 | B | 21.6 | 12.8 |
| * 18 | 1 | 1500. | 0. | 162. | 988. | 0. | 162. | 988. | 1650. | 0. | 0. | 0. | .60 | 62. | 15.9 | B | 21.6 | 12.8 |
| * 19 | 1 | 12000. | 0. | 826. | 826. | 0. | 826. | 826. | 1650. | 0. | 0. | 0. | .50 | 62. | 13.3 | B | 21.6 | 12.8 |
| * 20 | | | | | | | | | | | | | | | | | | |
| * TOTAL | | 36310. | = | 6.9 | MI LBS | | | | | MAX(V/C) = 0.89 | | LOWEST LOS = C | | AVG = 62. | 18.5 | | 21.6 | 12.8 |

| CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | | |
|-----------------------------|-------|---------|-------|-------------------|-------|---------|-------|----------|
| FREWAY TRAVEL TIME = | 64. | VEH-HRS | 127. | PASS-HRS | 64. | VEH-HRS | 127. | PASS-HRS |
| FREWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 64. | VEH-HRS | 127. | PASS-HRS | 64. | VEH-HRS | 127. | PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 3951. | VEH-MI. | 7901. | PASS-MI. | 3951. | VEH-MI. | 7901. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. | MPH. | | | 62. | MPH. | | |
| AVERAGE DENSITY = | 19. | VPMP/L | | | 19. | VPMP/L | | |
| TOTAL FUEL = | 183. | GALLONS | | | 183. | GALLONS | | |

TOTAL EMISSIONS = 50. KILOGRAMS

SR-237_WB_AM_NP_2040_PL 50. KILOGRAMS

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/30/2016 10:25 PAGE 5
UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE TIME SLICE 1 OF 4

Table with columns: SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY. Includes summary rows for MAINTENANCE DELAY and TOTAL DELAY.

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/30/2016 10:25 PAGE 6
UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE TIME SLICE 2 OF 4

**
** FREEWAY TRAVEL TIME (MINUTES) **
**

Table with columns: ORIGINS DOWN, DESTINATIONS ACROSS (1-8). Includes summary rows for ORIGIN DOWN and DESTINATIONS ACROSS.

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/30/2016 10:25 PAGE 7
UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE TIME SLICE 2 OF 4

TIME SLICE FREEWAY PERFORMANCE TABLE

Table with columns: SUB SEC, NO. LNS, SSEC LENGTH, O-D DATA ORG, DEMANDS DES, ADJUSTED VOLUMES ORG, SSEC CAP, WEAVE EFF, CONGEST LENGTH, STORAGE RATE, V/C RATIO, SPEED MPH, DENSITY VPMP, LOS LEVEL, FUEL MPG, EMISSIONS GS/VM.

TOTAL 36310. = 6.9 MI LBS MAX(V/C) = 0.89 LOWEST LOS = C AVG = 62. 18.5 21.6 12.8

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| | | | | | | | | | | | | | | | | | | |
|------|---|--------|------|------|-------|------|------|-------|-------|----|----|-----|-----|------|---|------|------|---|
| * 16 | 1 | 10. | 0. | 0. | 914. | 0. | 0. | 914. | 1650. | 0. | 0. | .55 | 62. | 14.7 | B | 21.6 | 12.8 | * |
| * 17 | 1 | 1500. | 204. | 0. | 1118. | 204. | 0. | 1118. | 1650. | 0. | 0. | .68 | 62. | 18.0 | C | 21.6 | 12.8 | * |
| * 18 | 1 | 1500. | 0. | 227. | 1118. | 0. | 227. | 1118. | 1650. | 0. | 0. | .68 | 62. | 18.0 | C | 21.6 | 12.8 | * |
| * 19 | 1 | 12000. | 0. | 891. | 890. | 0. | 891. | 890. | 1650. | 0. | 0. | .54 | 62. | 14.4 | B | 21.6 | 12.8 | * |
| * 20 | | | | | | | | | | | | | | | | | | * |

| | | | | | | | | | | | | | | | | | | | | |
|-------|--------|---|-----|---------|--|--|--|--|-----------------|--|--|----------------|--|-----------|--|------|--|------|------|---|
| TOTAL | 36310. | = | 6.9 | MI L ES | | | | | MAX(V/C) = 0.95 | | | LOWEST LOS = D | | AVG = 61. | | 20.2 | | 21.8 | 12.6 | * |
|-------|--------|---|-----|---------|--|--|--|--|-----------------|--|--|----------------|--|-----------|--|------|--|------|------|---|

| | CURRENT TIME SLICE | | CUMULATIVE VALUES |
|-----------------------------|--------------------|-----------------|---------------------------------------|
| FREEWAY TRAVEL TIME = | 69. VEH-HRS | 139. PASS-HRS | 197. VEH-HRS 394. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 69. VEH-HRS | 139. PASS-HRS | 197. VEH-HRS 394. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 4240. VEH-MI . | 8479. PASS-MI . | 12141. VEH-MI . 24282. PASS-MI . |
| AVERAGE SYSTEM SPEED = | 61. MPH. | | 62. MPH. |
| AVERAGE DENSITY = | 20. VP MPL | | 19. VP MPL |
| TOTAL FUEL = | 194. GALLONS | | 561. GALLONS |
| TOTAL EMISSIONS = | 53. KI LOGRAMS | | 154. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESI RED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 1.17 | 4 | 0.16 | 5 | 0.15 |
| 6 | 0.64 | 7 | 0.55 | 8 | 0.21 | 9 | 0.19 | 10 | 0.02 |
| 11 | 0.02 | 12 | 0.02 | 13 | 0.00 | 14 | 0.00 | 15 | 0.06 |
| 16 | 0.00 | 17 | 0.12 | 18 | 0.12 | 19 | 0.75 | 20 | 0.00 |

***** TOTAL DELAY = 4.2 VEH-HRS ***** AVERAGE DELAY = 0.19 MIN/VEH *****

**
** FREEWAY TRAVEL TIME (MINUTES) **
**

| ORIGINS | DESTINATIONS ACROSS | | | | | | | | |
|---------|---------------------|---|---|---|---|---|---|--|--|
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | |

| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
|-------|------|------|------|------|------|------|------|------|------|
| * 2 * | 0.00 | 3.23 | 3.78 | 3.79 | 3.98 | 4.53 | 6.73 | 0.00 | |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.52 | 4.72 | 0.00 | |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 4.19 | 0.00 | |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.08 | 0.00 | |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.93 | 0.00 | |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.75 | 0.00 | |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS | | | |
|-----------|------|----------|---------|------------------|-------|-------|---------|---------|-------|-------|---------|-----|------|--------|---|------|------|
| * 1 | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | |
| * 3 | 1 | 11000. | 1503. | 0. | 1503. | 1503. | 0. | 1503. | 1650. | 0. | 0. | .91 | 62. | 24.2 | C | 21.6 | 12.8 |

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| | | | | | | | | | | | | | | | | | | | |
|-------|-------|---|--------|------|------------|-------|-----------------|------|----------------|-------|-----------|----|------|-----|------|---|------|------|---|
| * | 4 | 1 | 1500. | 5. | 0. | 1508. | 5. | 0. | 1508. | 1650. | 0. | 0. | .91 | 62. | 24.3 | C | 21.6 | 12.8 | * |
| * | 5 | 1 | 1400. | 0. | 0. | 1508. | 0. | 0. | 1508. | 1650. | 0. | 0. | .91 | 62. | 24.3 | C | 21.6 | 12.8 | * |
| * | 6 | 1 | 1500. | 67. | 0. | 1575. | 67. | 0. | 1575. | 1650. | 0. | 0. | .95 | 55. | 28.7 | D | 24.4 | 11.2 | * |
| * | 7 | 1 | 1300. | 0. | 0. | 1575. | 0. | 0. | 1575. | 1650. | 0. | 0. | .95 | 55. | 28.7 | D | 24.4 | 11.2 | * |
| * | 8 | 1 | 500. | 0. | 376. | 1575. | 0. | 376. | 1575. | 1650. | 0. | 0. | .95 | 55. | 28.7 | D | 24.4 | 11.2 | * |
| * | 9 | 1 | 2300. | 0. | 0. | 1199. | 0. | 0. | 1199. | 1650. | 0. | 0. | .73 | 62. | 19.3 | C | 21.6 | 12.8 | * |
| * | 10 | 1 | 250. | 32. | 0. | 1231. | 32. | 0. | 1231. | 1650. | 0. | 0. | .75 | 62. | 19.9 | C | 21.6 | 12.8 | * |
| * | 11 | 1 | 200. | 0. | 0. | 1231. | 0. | 0. | 1231. | 1650. | 0. | 0. | .75 | 62. | 19.9 | C | 21.6 | 12.8 | * |
| * | 12 | 1 | 250. | 0. | 305. | 1231. | 0. | 305. | 1231. | 1650. | 0. | 0. | .75 | 62. | 19.9 | C | 21.6 | 12.8 | * |
| * | 13 | 1 | 50. | 0. | 76. | 926. | 0. | 76. | 926. | 1650. | 0. | 0. | .56 | 62. | 14.9 | B | 21.6 | 12.8 | * |
| * | 14 | 1 | 50. | 0. | 0. | 850. | 0. | 0. | 850. | 1650. | 0. | 0. | .52 | 62. | 13.7 | B | 21.6 | 12.8 | * |
| * | 15 | 1 | 1000. | 63. | 0. | 914. | 63. | 0. | 914. | 1650. | 0. | 0. | .55 | 62. | 14.7 | B | 21.6 | 12.8 | * |
| * | 16 | 1 | 10. | 0. | 0. | 914. | 0. | 0. | 914. | 1650. | 0. | 0. | .55 | 62. | 14.7 | B | 21.6 | 12.8 | * |
| * | 17 | 1 | 1500. | 204. | 0. | 1118. | 204. | 0. | 1118. | 1650. | 0. | 0. | .68 | 62. | 18.0 | C | 21.6 | 12.8 | * |
| * | 18 | 1 | 1500. | 0. | 227. | 1118. | 0. | 227. | 1118. | 1650. | 0. | 0. | .68 | 62. | 18.0 | C | 21.6 | 12.8 | * |
| * | 19 | 1 | 12000. | 0. | 891. | 890. | 0. | 891. | 890. | 1650. | 0. | 0. | .54 | 62. | 14.4 | B | 21.6 | 12.8 | * |
| * | 20 | | | | | | | | | | | | | | | | | | * |
| ***** | | | | | | | | | | | | | | | | | | | |
| * | TOTAL | | 36310. | = | 6.9 MI LBS | | MAX(V/C) = 0.95 | | LOWEST LOS = D | | AVG = 61. | | 20.2 | | 21.8 | | 12.6 | | * |
| ***** | | | | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | | | CUMULATIVE VALUES | | | | |
|-----------------------------|--------------------|-----------|-------|-------------------|--------|-----------|--------|----------|
| FREEWAY TRAVEL TIME = | 69. | VEH-HRS | 139. | PASS-HRS | 266. | VEH-HRS | 533. | PASS-HRS |
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 69. | VEH-HRS | 139. | PASS-HRS | 266. | VEH-HRS | 533. | PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 4240. | VEH-MI. | 8479. | PASS-MI. | 16381. | VEH-MI. | 32762. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 61. | MPH. | | | 62. | MPH. | | |
| AVERAGE DENSITY = | 20. | VPMPL | | | 19. | VPMPL | | |
| TOTAL FUEL = | 194. | GALLONS | | | 755. | GALLONS | | |
| TOTAL EMISSIONS = | 53. | KILOGRAMS | | | 208. | KILOGRAMS | | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 1.17 | 4 | 0.16 | 5 | 0.15 |
| 6 | 0.64 | 7 | 0.55 | 8 | 0.21 | 9 | 0.19 | 10 | 0.02 |
| 11 | 0.02 | 12 | 0.02 | 13 | 0.00 | 14 | 0.00 | 15 | 0.06 |
| 16 | 0.00 | 17 | 0.12 | 18 | 0.12 | 19 | 0.75 | 20 | 0.00 |

***** TOTAL DELAY = 4.2 VEH-HRS ***** AVERAGE DELAY = 0.19 MIN/VEH *****

```

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQQ QQQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP EEEEEEEEE
    
```

FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 2.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 30
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT TRUCKS | DES TRUCKS | SPECIAL RAMP | FF. SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION LOCATION |
|---------|----------|----------|-------------|--------------|---------|---------|-----------|---------|------------|------------|--------------|-------------------|---------------|----------|----------------|--------------------------|
| ** 1 | 3 | 6000. | 500. | 65 | 0 | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0.0 | 0. | GOOD | 0.0 | Seed |
| ** 2 | 3 | 6000. | 99999. | 65 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0.0 | 0. | GOOD | 0.0 | Queue Capture |
| ** 3 | 2 | 4000. | 11000. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** 4 | 2 | 4000. | 1500. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0.0 | 0. | GOOD | 0.0 | Lawrence On-ramp |
| ** 5 | 2 | 4000. | 1400. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0.0 | 0. | GOOD | 0.0 | Lawrence to Crossman |
| ** 6 | 2 | 4000. | 1500. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0.0 | 0. | GOOD | 0.0 | Crossman On-Ramp |
| ** 7 | 2 | 4000. | 1300. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0.0 | 0. | GOOD | 0.0 | Crossman / Mathilda |
| ** 8 | 3 | 5630. | 500. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-Ramp |
| ** 9 | 2 | 4000. | 2300. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda |
| ** 10 | 3 | 4390. | 250. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0.0 | 0. | GOOD | 0.0 | Mathilda On-Ramp |
| ** 11 | 3 | 4390. | 200. | 62 | | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0.0 | 0. | GOOD | 0.0 | Mathilda to US-101 |
| ** 12 | 3 | 4390. | 250. | 62 | D | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0.0 | 0. | GOOD | 0.0 | US-101 Off-Ramp |
| ** 13 | 2 | 4000. | 50. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0.0 | 0. | GOOD | 0.0 | Bottleneck by-pass |
| ** 14 | 2 | 2400. | 50. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0.0 | 0. | GOOD | 0.0 | Bottleneck |
| ** 15 | 2 | 4000. | 1000. | 62 | OD | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0.0 | 0. | GOOD | 0.0 | US 101 / US 101 |
| ** 16 | 2 | 4000. | 10. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0.0 | 0. | GOOD | 0.0 | Dummy end of travel time |
| ** 17 | 2 | 4000. | 1500. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0.0 | 0. | GOOD | 0.0 | US 101 NB On-Ramp |
| ** 18 | 2 | 4000. | 1500. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0.0 | 0. | GOOD | 0.0 | Maude Off-ramp |
| ** 19 | 2 | 4000. | 12000. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** 20 | 3 | 6000. | 500. | 65 | OD | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0.0 | 0. | GOOD | 0.0 | End Of HOV |

***** INPUT HAS BEEN COMPLETED *****

QUEUE COLLISION IN SECTION 4 T2 =0.116

 ** FREeway TRAVEL TIME (MINUTES) **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | |
|-----------|-------|-----------------------|-------|-------|-------|-------|-------|-------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| + | * 1 * | 19.26 | 25.52 | 26.07 | 26.08 | 26.28 | 26.83 | 29.11 |
| + | * 2 * | 0.00 | 2.39 | 2.94 | 2.95 | 3.14 | 3.70 | 5.98 |
| + | * 3 * | 0.00 | 0.70 | 1.26 | 1.27 | 1.46 | 2.01 | 4.30 |
| + | * 4 * | 0.00 | 0.00 | 0.13 | 0.14 | 0.33 | 0.88 | 3.17 |
| + | * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.18 | 0.73 | 3.02 |
| + | * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.55 | 2.84 |
| + | * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.09 |

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|-----------|-----------|------------|-----------|------------|-----------|---------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|
| * SEC | * LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * CAP | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 1 | * 3 | * 500. | * 5388. | * 0. | * 5388. | * 5388. | * 0. | * 5388. | * 6000. | * 0. | * 90. | * 59. | * 30.3 | * D | * 21.6 |
| * 2 | * 3 | * 99999. | * 0. | * 1401. | * 5388. | * 0. | * 1401. | * 5388. | * 6000. | * 0. | * 90. | * 59. | * 30.3 | * D | * 21.6 |
| * 3 | * 2 | * 11000. | * 0. | * 0. | * 3987. | * 0. | * 0. | * 3424. | * 4000. | * 0. | * 9665. | * 563. | * .86 | * 32. | * 53.0 |
| * 4 | * 2 | * 1500. | * 26. | * 0. | * 4013. | * 26. | * 0. | * 3450. | * 3996. | * 0. | * 1500. | * 546. | * .86 | * 21. | * 84.1 |
| * 5 | * 2 | * 1400. | * 0. | * 0. | * 4013. | * 0. | * 0. | * 3450. | * 4000. | * 0. | * 1400. | * 546. | * .86 | * 19. | * 92.5 |
| * 6 | * 2 | * 1500. | * 489. | * 0. | * 4502. | * 489. | * 0. | * 3939. | * 3939. | * 0. | * 0. | * 1.00 | * 52. | * 38.2 | * E |
| * 7 | * 2 | * 1300. | * 0. | * 0. | * 4502. | * 0. | * 0. | * 3939. | * 4000. | * 0. | * 0. | * .98 | * 53. | * 37.3 | * E |
| * 8 | * 3 | * 500. | * 0. | * 918. | * 4502. | * 0. | * 805. | * 3939. | * 5348. | * 0. | * 0. | * .74 | * 62. | * 21.2 | * C |
| * 9 | * 2 | * 2300. | * 0. | * 0. | * 3584. | * 0. | * 0. | * 3134. | * 4000. | * 0. | * 0. | * .78 | * 61. | * 25.6 | * C |
| * 10 | * 3 | * 250. | * 198. | * 0. | * 3782. | * 198. | * 0. | * 3332. | * 4358. | * 0. | * 0. | * .76 | * 62. | * 17.9 | * B |
| * 11 | * 3 | * 200. | * 0. | * 0. | * 3782. | * 0. | * 0. | * 3332. | * 4390. | * 0. | * 0. | * .76 | * 62. | * 17.9 | * B |
| * 12 | * 3 | * 250. | * 0. | * 1246. | * 3782. | * 0. | * 1101. | * 3332. | * 4030. | * 0. | * 0. | * .83 | * 62. | * 17.9 | * B |
| * 13 | * 2 | * 50. | * 0. | * 0. | * 2536. | * 0. | * 0. | * 2231. | * 4000. | * 0. | * 0. | * .56 | * 62. | * 18.0 | * B |
| * 14 | * 2 | * 50. | * 0. | * 0. | * 2536. | * 0. | * 0. | * 2231. | * 2400. | * 0. | * 0. | * .93 | * 62. | * 18.0 | * B |
| * 15 | * 2 | * 1000. | * 0. | * 0. | * 2536. | * 0. | * 0. | * 2231. | * 4000. | * 0. | * 0. | * .56 | * 62. | * 18.0 | * B |
| * 16 | * 2 | * 10. | * 0. | * 0. | * 2536. | * 0. | * 0. | * 2231. | * 4000. | * 0. | * 0. | * .56 | * 62. | * 18.0 | * B |
| * 17 | * 2 | * 1500. | * 539. | * 0. | * 3075. | * 539. | * 0. | * 2770. | * 3861. | * 0. | * 0. | * .72 | * 62. | * 22.3 | * C |
| * 18 | * 2 | * 1500. | * 0. | * 707. | * 3075. | * 0. | * 642. | * 2770. | * 3836. | * 0. | * 0. | * .72 | * 62. | * 22.3 | * C |
| * 19 | * 2 | * 12000. | * 0. | * 0. | * 2368. | * 0. | * 0. | * 2128. | * 4000. | * 0. | * 0. | * .53 | * 62. | * 17.2 | * B |
| * 20 | * 3 | * 500. | * 832. | * 3200. | * 3200. | * 832. | * 2960. | * 2960. | * 6000. | * 0. | * 0. | * .49 | * 65. | * 15.2 | * B |
| * TOTAL | * 137309. | * = | * 26.0 | * MI LBS | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |

SR-237_WB_AM_P1_2040_PE

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | | | |
|----------------------------|--------------------|-----------------|-------------------|-----------------|--|--|
| FREEWAY TRAVEL TIME = | 1132. VEH-HRS | 1359. PASS-HRS | 1132. VEH-HRS | 1359. PASS-HRS | | |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | | |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | | |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | | |
| TOTAL SYSTEM TRAVEL TIME = | 1132. VEH-HRS | 1359. PASS-HRS | 1132. VEH-HRS | 1359. PASS-HRS | | |
| TOTAL TRAV DISTANCE = | 61910. VEH-MI. | 75373. PASS-MI. | 61910. VEH-MI. | 75373. PASS-MI. | | |
| AVERAGE SYSTEM SPEED = | 55. MPH. | | 55. MPH. | | | |
| AVERAGE DENSITY = | 32. VP/ML | | 32. VP/ML | | | |
| TOTAL FUEL = | 2893. GALLONS | | 2893. GALLONS | | | |
| TOTAL EMISSIONS = | 768. KI LOGRAMS | | 768. KI LOGRAMS | | | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.38 | 2 | 75.62 | 3 | 61.56 | 4 | 16.80 | 5 | 17.66 |
| 6 | 2.24 | 7 | 1.73 | 8 | 0.14 | 9 | 0.64 | 10 | 0.06 |
| 11 | 0.05 | 12 | 0.06 | 13 | 0.01 | 14 | 0.01 | 15 | 0.16 |
| 16 | 0.00 | 17 | 0.29 | 18 | 0.29 | 19 | 1.80 | 20 | 0.00 |

***** TOTAL DELAY = 179.5 VEH-HRS ***** AVERAGE DELAY = 2.67 MIN/VEH *****

 **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN *
 * 1 2 3 4 5 6 7 *

| | | | |
|---|---|---|---|
| + | * | ***** | * |
| + | * | * | * |
| + | * | 1 * 20.57 30.23 30.79 30.80 30.99 31.54 33.83 | * |
| + | * | 2 * 0.00 2.55 3.10 3.11 3.30 3.85 6.14 | * |
| + | * | 3 * 0.00 0.70 1.26 1.27 1.46 2.01 4.30 | * |
| + | * | 4 * 0.00 0.00 0.13 0.14 0.33 0.88 3.17 | * |
| + | * | 5 * 0.00 0.00 0.00 0.00 0.18 0.73 3.02 | * |
| + | * | 6 * 0.00 0.00 0.00 0.00 0.00 0.55 2.84 | * |
| + | * | 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.09 | * |
| + | * | * | * |
| + | * | ***** | * |

 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 * *

| * SUB NO. | * SEC LNS | * SSEC LENGTH | * O-D DATA ORG DES | * DEMANDS SSEC | * ADJUSTED VOLUMES ORG DES | * SSEC CAP. | * WEAVE EFF | * CONGEST LENGTH | * STORAGE RATE | * V/C RATIO | * SPEED MPH | * DENSITY VP/ML | * LOS LEVEL | * FUEL MPG | * EMISSIONS GS/VM | | |
|-----------|-----------|---------------|--------------------|----------------|----------------------------|-------------|-------------|------------------|----------------|-------------|-------------|-----------------|-------------|------------|-------------------|--------|--------|
| * 1 | * 3 | * 500. | * 5388. | * 0. | * 5388. | * 5388. | * 0. | * 5388. | * 6000. | * 0. | * 0. | * .90 | * 59. | * 30.3 | * D | * 21.6 | * 12.2 |
| * 2 | * 3 | * 99999. | * 0. | * 1401. | * 5388. | * 0. | * 1401. | * 4825. | * 6000. | * 0. | * 5597. | * .80 | * 56. | * 29.0 | * F | * 21.4 | * 12.4 |
| * 3 | * 2 | * 11000. | * 0. | * 0. | * 3987. | * 0. | * 0. | * 3424. | * 4000. | * 0. | * 11000. | * .86 | * 18. | * 97.5 | * F | * 17.1 | * 17.5 |
| * 4 | * 2 | * 1500. | * 26. | * 0. | * 4013. | * 26. | * 0. | * 3450. | * 3996. | * 0. | * 1500. | * .86 | * 18. | * 96.3 | * F | * 17.3 | * 17.3 |
| * 5 | * 2 | * 1400. | * 0. | * 0. | * 4013. | * 0. | * 0. | * 3450. | * 4000. | * 0. | * 1400. | * .86 | * 18. | * 96.6 | * F | * 17.3 | * 17.3 |
| * 6 | * 2 | * 1500. | * 489. | * 0. | * 4502. | * 489. | * 0. | * 3939. | * 3939. | * 0. | * 0. | * 1.00 | * 52. | * 38.2 | * E | * 23.6 | * 11.1 |
| * 7 | * 2 | * 1300. | * 0. | * 0. | * 4502. | * 0. | * 0. | * 3939. | * 4000. | * 0. | * 0. | * .98 | * 53. | * 37.3 | * E | * 23.4 | * 11.2 |
| * 8 | * 3 | * 500. | * 0. | * 918. | * 4502. | * 0. | * 805. | * 3939. | * 5348. | * 0. | * 0. | * .74 | * 62. | * 21.2 | * C | * 20.3 | * 13.0 |
| * 9 | * 2 | * 2300. | * 0. | * 0. | * 3584. | * 0. | * 0. | * 3134. | * 4000. | * 0. | * 0. | * .78 | * 61. | * 25.6 | * C | * 20.7 | * 12.8 |
| * 10 | * 3 | * 250. | * 198. | * 0. | * 3782. | * 198. | * 0. | * 3332. | * 4358. | * 0. | * 0. | * .76 | * 62. | * 17.9 | * B | * 20.3 | * 13.0 |
| * 11 | * 3 | * 200. | * 0. | * 0. | * 3782. | * 0. | * 0. | * 3332. | * 4390. | * 0. | * 0. | * .76 | * 62. | * 17.9 | * B | * 20.3 | * 13.0 |
| * 12 | * 3 | * 250. | * 0. | * 1246. | * 3782. | * 0. | * 1101. | * 3332. | * 4030. | * 0. | * 0. | * .83 | * 62. | * 17.9 | * B | * 20.3 | * 13.0 |
| * 13 | * 2 | * 50. | * 0. | * 0. | * 2536. | * 0. | * 0. | * 2231. | * 4000. | * 0. | * 0. | * .56 | * 62. | * 18.0 | * B | * 20.3 | * 13.0 |
| * 14 | * 2 | * 50. | * 0. | * 0. | * 2536. | * 0. | * 0. | * 2231. | * 2400. | * 0. | * 0. | * .93 | * 62. | * 18.0 | * B | * 20.3 | * 13.0 |
| * 15 | * 2 | * 1000. | * 0. | * 0. | * 2536. | * 0. | * 0. | * 2231. | * 4000. | * 0. | * 0. | * .56 | * 62. | * 18.0 | * B | * 20.3 | * 13.0 |
| * 16 | * 2 | * 10. | * 0. | * 0. | * 2536. | * 0. | * 0. | * 2231. | * 4000. | * 0. | * 0. | * .56 | * 62. | * 18.0 | * B | * 20.3 | * 13.0 |
| * 17 | * 2 | * 1500. | * 539. | * 0. | * 3075. | * 539. | * 0. | * 2770. | * 3861. | * 0. | * 0. | * .72 | * 62. | * 22.3 | * C | * 20.3 | * 13.0 |

SR-237_WB_AM_P1_2040_PE

| | | | | | | | | | | | | | | | | | | | | |
|---|----|---|--------|------|-------|-------|------|-------|-------|-------|----|----|----|-----|-----|------|---|------|------|---|
| * | 18 | 2 | 1500. | 0. | 707. | 3075. | 0. | 642. | 2770. | 3836. | 0. | 0. | 0. | .72 | 62. | 22.3 | C | 20.3 | 13.0 | * |
| * | 19 | 2 | 12000. | 0. | 0. | 2368. | 0. | 0. | 2128. | 4000. | 0. | 0. | 0. | .53 | 62. | 17.2 | B | 20.3 | 13.0 | * |
| * | 20 | 3 | 500. | 832. | 3200. | 3200. | 832. | 2960. | 2960. | 6000. | 0. | 0. | 0. | .49 | 65. | 15.2 | B | 19.0 | 14.1 | * |

* TOTAL 137309. = 26.0 MI LES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 48. 34.6 21.0 12.8 *

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------------------|----------------------------------|
| FREEWAY TRAVEL TIME = | 1273. VEH-HRS 1514. PASS-HRS | 2405. VEH-HRS 2874. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1273. VEH-HRS 1514. PASS-HRS | 2405. VEH-HRS 2874. PASS-HRS |
| TOTAL TRAV DISTANCE = | 61376. VEH-MI. 74805. PASS-MI. | 123286. VEH-MI. 150178. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 48. MPH. | 51. MPH. |
| AVERAGE DENSITY = | 35. VPMP | 33. VPMP |
| TOTAL FUEL = | 2928. GALLONS | 5821. GALLONS |
| TOTAL EMISSIONS = | 785. KI LOGRAMS | 1553. KI LOGRAMS |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION TIME SLICE 2 OF 4

***** MAINTENANCE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|--------|------------|--------|------------|-------|------------|-------|
| 1 | 0.38 | 2 | 133.78 | 3 | 148.51 | 4 | 19.83 | 5 | 18.58 |
| 6 | 2.24 | 7 | 1.73 | 8 | 0.14 | 9 | 0.64 | 10 | 0.06 |
| 11 | 0.05 | 12 | 0.06 | 13 | 0.01 | 14 | 0.01 | 15 | 0.16 |
| 16 | 0.00 | 17 | 0.29 | 18 | 0.29 | 19 | 1.80 | 20 | 0.00 |

***** TOTAL DELAY = 328.6 VEH-HRS ***** AVERAGE DELAY = 5.08 MIN/VEH *****

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION TIME SLICE 3 OF 4

 ** FREEWAY TRAVEL TIME (MINUTES) **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN *
 * 1 2 3 4 5 6 7 *

| | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|
| * 1 * | 26.55 | 37.84 | 38.39 | 38.40 | 38.59 | 39.17 | 41.46 |
| * 2 * | 0.00 | 2.86 | 3.41 | 3.42 | 3.61 | 4.19 | 6.48 |
| * 3 * | 0.00 | 0.70 | 1.25 | 1.26 | 1.45 | 2.03 | 4.32 |
| * 4 * | 0.00 | 0.00 | 0.13 | 0.14 | 0.33 | 0.91 | 3.20 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.18 | 0.76 | 3.05 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.58 | 2.87 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.09 |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION TIME SLICE 3 OF 4

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | |
|-----------|--------|------------|-----------|------------|-----------|---------|---------|-----------|-----------|-------|------------|-----------|---------|--------|-------------|---------|--------|---------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 1 | * 3 | * 500. | * 5780. | * 0. | * 5780. | * 5780. | * 0. | * 5780. | * 6000. | * 0. | * 0. | * 0. | * .96 | * 55. | * 34.9 | * D | * 22.8 | * 11.4 |
| * 2 | * 3 | * 99999. | * 0. | * 1503. | * 5780. | * 0. | * 1503. | * 4730. | * 6000. | * 0. | * * 17465. | * 1050. | * .79 | * 43. | * 36.7 | * F | * 21.8 | * 12.2 |
| * 3 | * 2 | * 11000. | * 0. | * 0. | * 4277. | * 0. | * 0. | * 3227. | * 4000. | * 0. | * * 11000. | * 773. | * .81 | * 15. | * 108.8 | * F | * 15.9 | * 19.1 |
| * 4 | * 2 | * 1500. | * 34. | * 0. | * 4311. | * 34. | * 0. | * 3261. | * 3995. | * 0. | * * 1500. | * 734. | * .82 | * 15. | * 106.6 | * F | * 16.2 | * 18.8 |
| * 5 | * 2 | * 1400. | * 0. | * 0. | * 4311. | * 0. | * 0. | * 3261. | * 4000. | * 0. | * * 1400. | * 734. | * .82 | * 15. | * 106.9 | * F | * 16.2 | * 18.8 |

SR-237_WB_AM_P1_2040_PE

| | | | | | | | | | | | | | | | | | | | |
|---|----|---|--------|------|-------|-------|------|-------|-------|-------|----|----|------|-----|------|---|------|------|---|
| * | 6 | 2 | 1500. | 672. | 0. | 4983. | 672. | 0. | 3933. | 3933. | 0. | 0. | 1.00 | 52. | 38.1 | E | 23.6 | 11.1 | * |
| * | 7 | 2 | 1300. | 0. | 0. | 4983. | 0. | 0. | 3933. | 4000. | 0. | 0. | .98 | 53. | 37.2 | E | 23.3 | 11.2 | * |
| * | 8 | 3 | 500. | 0. | 1264. | 4983. | 0. | 1001. | 3933. | 5254. | 0. | 0. | .75 | 62. | 21.1 | C | 20.3 | 13.0 | * |
| * | 9 | 2 | 2300. | 0. | 0. | 3719. | 0. | 0. | 2932. | 4000. | 0. | 0. | .73 | 62. | 23.6 | C | 20.3 | 13.0 | * |
| * | 10 | 3 | 250. | 278. | 0. | 3997. | 278. | 0. | 3210. | 4352. | 0. | 0. | .74 | 62. | 17.3 | B | 20.3 | 13.0 | * |
| * | 11 | 3 | 200. | 0. | 0. | 3997. | 0. | 0. | 3210. | 4390. | 0. | 0. | .73 | 62. | 17.3 | B | 20.3 | 13.0 | * |
| * | 12 | 3 | 250. | 0. | 1103. | 3997. | 0. | 891. | 3210. | 4088. | 0. | 0. | .79 | 62. | 17.3 | B | 20.3 | 13.0 | * |
| * | 13 | 2 | 50. | 0. | 275. | 2894. | 0. | 222. | 2318. | 3925. | 0. | 0. | .59 | 62. | 18.7 | C | 20.3 | 13.0 | * |
| * | 14 | 2 | 50. | 0. | 0. | 2619. | 0. | 0. | 2096. | 2400. | 0. | 0. | .87 | 62. | 16.9 | B | 20.3 | 13.0 | * |
| * | 15 | 2 | 1000. | 287. | 0. | 2906. | 287. | 0. | 2383. | 3937. | 0. | 0. | .61 | 62. | 19.2 | C | 20.3 | 13.0 | * |
| * | 16 | 2 | 10. | 0. | 0. | 2906. | 0. | 0. | 2383. | 4000. | 0. | 0. | .60 | 62. | 19.2 | C | 20.3 | 13.0 | * |
| * | 17 | 2 | 1500. | 927. | 0. | 3833. | 927. | 0. | 3310. | 3796. | 0. | 0. | .87 | 59. | 28.1 | D | 21.7 | 12.2 | * |
| * | 18 | 2 | 1500. | 0. | 1282. | 3833. | 0. | 1123. | 3310. | 3770. | 0. | 0. | .88 | 59. | 28.2 | D | 21.7 | 12.1 | * |
| * | 19 | 2 | 12000. | 0. | 0. | 2551. | 0. | 0. | 2187. | 4000. | 0. | 0. | .55 | 62. | 17.6 | B | 20.3 | 13.0 | * |
| * | 20 | 3 | 500. | 896. | 3447. | 3447. | 896. | 3083. | 3083. | 6000. | 0. | 0. | .51 | 65. | 15.8 | B | 19.0 | 14.1 | * |

| | | | | | | | | | | | | | | | | | | | | |
|---|-------|---------|---|------|-------|--|--|--|--|--|--|--|--|-----------------|----------------|-----------|------|------|------|---|
| * | TOTAL | 137309. | = | 26.0 | MILES | | | | | | | | | MAX(V/C) = 1.00 | LOWEST LOS = F | AVG = 39. | 41.5 | 21.2 | 12.7 | * |
|---|-------|---------|---|------|-------|--|--|--|--|--|--|--|--|-----------------|----------------|-----------|------|------|------|---|

| | | CURRENT TIME SLICE | | CUMULATIVE VALUES | | | | | | |
|----------------------------|--------|--------------------|--------|-------------------|---------|------------|---------|----------|--|--|
| FREEWAY TRAVEL TIME = | 1637. | VEH-HRS | 1964. | PASS-HRS | 4041. | VEH-HRS | 4838. | PASS-HRS | | |
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS | | |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS | | |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS | | |
| TOTAL SYSTEM TRAVEL TIME = | 1637. | VEH-HRS | 1964. | PASS-HRS | 4041. | VEH-HRS | 4838. | PASS-HRS | | |
| TOTAL TRAV DISTANCE = | 64020. | VEH-MI. | 78162. | PASS-MI. | 187306. | VEH-MI. | 228339. | PASS-MI. | | |
| AVERAGE SYSTEM SPEED = | 39. | MPH | | | 46. | MPH | | | | |
| AVERAGE DENSITY = | 42. | VPMP/L | | | 36. | VPMP/L | | | | |
| TOTAL FUEL = | 3020. | GALLONS | | | 8840. | GALLONS | | | | |
| TOTAL EMISSIONS = | 814. | KI LOGRAMS | | | 2367. | KI LOGRAMS | | | | |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 3 OF 4

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|--------|------------|--------|------------|-------|------------|-------|
| 1 | 0.75 | 2 | 422.83 | 3 | 174.89 | 4 | 23.15 | 5 | 21.70 |
| 6 | 2.24 | 7 | 1.71 | 8 | 0.14 | 9 | 0.48 | 10 | 0.06 |
| 11 | 0.05 | 12 | 0.06 | 13 | 0.01 | 14 | 0.01 | 15 | 0.17 |
| 16 | 0.00 | 17 | 0.74 | 18 | 0.77 | 19 | 1.85 | 20 | 0.00 |

***** TOTAL DELAY = 651.6 VEH-HRS ***** AVERAGE DELAY = 9.61 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 3/30/2016 12:52 PAGE 14
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 4 OF 4

 ** **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 ** **

| * ORIGINS DOWN | * DESTINATIONS ACROSS | | | | | | | * |
|----------------|-----------------------|-------|-------|-------|-------|-------|-------|---|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | |
| * 1 * | 32.84 | 44.12 | 44.67 | 44.68 | 44.88 | 45.46 | 47.74 | * |
| * 2 * | 0.00 | 2.86 | 3.41 | 3.42 | 3.61 | 4.19 | 6.48 | * |
| * 3 * | 0.00 | 0.70 | 1.25 | 1.26 | 1.45 | 2.03 | 4.32 | * |
| * 4 * | 0.00 | 0.00 | 0.13 | 0.14 | 0.33 | 0.91 | 3.20 | * |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.18 | 0.76 | 3.05 | * |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.58 | 2.87 | * |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.09 | * |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 3/30/2016 12:52 PAGE 15
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 4 OF 4

SR-237_WB_AM_P1_2040_PE
TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | | |
|-----------|----------|------------|-----------|--------------------|--------|---------|-----------|-----------|---------|-----------------|----------------|-----------|--------|-------------|-------|-------|------|------|
| * SEC LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * SSEC | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | | | |
| * 1 | 3 | 500. | 5780. | 0. | 5780. | 5780. | 0. | 5780. | 6000. | 0. | 0. | 0. | .96 | 55. | 34.9 | D | 22.8 | 11.4 |
| * 2 | 3 | 99999. | 0. | 1503. | 5780. | 0. | 1503. | 4730. | 6000. | 0. | * 29334. | 1050. | .79 | 35. | 45.4 | F | 20.8 | 13.1 |
| * 3 | 2 | 11000. | 0. | 0. | 4277. | 0. | 0. | 3227. | 4000. | 0. | **11000. | 773. | .81 | 15. | 108.8 | F | 15.9 | 19.1 |
| * 4 | 2 | 1500. | 34. | 0. | 4311. | 34. | 0. | 3261. | 3995. | 0. | ** 1500. | 734. | .82 | 15. | 106.6 | F | 16.2 | 18.8 |
| * 5 | 2 | 1400. | 0. | 0. | 4311. | 0. | 0. | 3261. | 4000. | 0. | ** 1400. | 734. | .82 | 15. | 106.9 | F | 16.2 | 18.8 |
| * 6 | 2 | 1500. | 672. | 0. | 4983. | 672. | 0. | 3933. | 3933. | 0. | 0. | 0. | 1.00 | 52. | 38.1 | E | 23.6 | 11.1 |
| * 7 | 2 | 1300. | 0. | 0. | 4983. | 0. | 0. | 3933. | 4000. | 0. | 0. | 0. | .98 | 53. | 37.2 | E | 23.3 | 11.2 |
| * 8 | 3 | 500. | 0. | 1264. | 4983. | 0. | 1001. | 3933. | 5254. | 0. | 0. | 0. | .75 | 62. | 21.1 | C | 20.3 | 13.0 |
| * 9 | 2 | 2300. | 0. | 0. | 3719. | 0. | 0. | 2932. | 4000. | 0. | 0. | 0. | .73 | 62. | 23.6 | C | 20.3 | 13.0 |
| * 10 | 3 | 250. | 278. | 0. | 3997. | 278. | 0. | 3210. | 4352. | 0. | 0. | 0. | .74 | 62. | 17.3 | B | 20.3 | 13.0 |
| * 11 | 3 | 200. | 0. | 0. | 3997. | 0. | 0. | 3210. | 4390. | 0. | 0. | 0. | .73 | 62. | 17.3 | B | 20.3 | 13.0 |
| * 12 | 3 | 250. | 0. | 1103. | 3997. | 0. | 891. | 3210. | 4088. | 0. | 0. | 0. | .79 | 62. | 17.3 | B | 20.3 | 13.0 |
| * 13 | 2 | 50. | 0. | 275. | 2894. | 0. | 222. | 2318. | 3925. | 0. | 0. | 0. | .59 | 62. | 18.7 | C | 20.3 | 13.0 |
| * 14 | 2 | 50. | 0. | 0. | 2619. | 0. | 0. | 2096. | 2400. | 0. | 0. | 0. | .87 | 62. | 16.9 | B | 20.3 | 13.0 |
| * 15 | 2 | 1000. | 287. | 0. | 2906. | 287. | 0. | 2383. | 3937. | 0. | 0. | 0. | .61 | 62. | 19.2 | C | 20.3 | 13.0 |
| * 16 | 2 | 10. | 0. | 0. | 2906. | 0. | 0. | 2383. | 4000. | 0. | 0. | 0. | .60 | 62. | 19.2 | C | 20.3 | 13.0 |
| * 17 | 2 | 1500. | 927. | 0. | 3833. | 927. | 0. | 3310. | 3796. | 0. | 0. | 0. | .87 | 59. | 28.1 | D | 21.7 | 12.2 |
| * 18 | 2 | 1500. | 0. | 1282. | 3833. | 0. | 1123. | 3310. | 3770. | 0. | 0. | 0. | .88 | 59. | 28.2 | D | 21.7 | 12.1 |
| * 19 | 2 | 12000. | 0. | 0. | 2551. | 0. | 0. | 2187. | 4000. | 0. | 0. | 0. | .55 | 62. | 17.6 | B | 20.3 | 13.0 |
| * 20 | 3 | 500. | 896. | 3447. | 3447. | 896. | 3083. | 3083. | 6000. | 0. | 0. | 0. | .51 | 65. | 15.8 | B | 19.0 | 14.1 |
| ***** | | | | | | | | | | | | | | | | | | |
| * TOTAL | 137309. | = | 26.0 | MI LES | | | | | | MAX(V/C) = 1.00 | LOWEST LOS = F | AVG = 33. | 47.9 | 20.4 | 13.4 | ***** | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 1899. VEH-HRS | 2295. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1899. VEH-HRS | 2295. PASS-HRS |
| TOTAL TRAV DISTANCE = | 62840. VEH-MI. | 76675. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 33. MPH | 42. MPH |
| AVERAGE DENSITY = | 48. VPMP | 39. VPMP |
| TOTAL FUEL = | 3082. GALLONS | 11922. GALLONS |
| TOTAL EMISSIONS = | 845. KI LOGRAMS | 3212. KI LOGRAMS |

***** MAINTENANCE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|--------|------------|--------|------------|-------|------------|-------|
| 1 | 0.75 | 2 | 703.49 | 3 | 174.89 | 4 | 23.15 | 5 | 21.70 |
| 6 | 2.24 | 7 | 1.71 | 8 | 0.14 | 9 | 0.48 | 10 | 0.06 |
| 11 | 0.05 | 12 | 0.06 | 13 | 0.01 | 14 | 0.01 | 15 | 0.17 |
| 16 | 0.00 | 17 | 0.74 | 18 | 0.77 | 19 | 1.85 | 20 | 0.00 |

***** TOTAL DELAY = 932.2 VEH-HRS ***** AVERAGE DELAY = 13.17 MIN/VEH *****

```

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ      1111      222222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111    222  222 PPPPPPPP LLL
FFF      RRR      RRR EEE      QQQQQ      QQQQQ      1111      222  222 PPP      PPP LLL
FFF      RRR      RRR EEE      QQQQ      QQQQ      1111      222  222 PPP      PPP LLL
FFFFFFFF RRRRRRRR EEEEEEE      QQQQ      QQQQ      1111      222  222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEE      QQQQ      QQQQ      1111      2222 PPPPPPPP LLL
FFF      RRR      RRR EEE      QQQQ      QQQ      1111      2222 PPP      LLL
FFF      RRR      RRR EEE      Q*UC*      QQQQ      1111      222 PPP      LLL
FFF      RRR      RRR EEEEEEEEE Q*REGENTS*Q 1111      222 PPP      LLLLLLLLLL
FFF      RRR      RRR EEEEEEEEE Q*1988*Q QQQ 11111111 2222222222 PPP      LLLLLLLLLL
    
```

FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 3 AND 19 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 2.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 30
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

```

*****
**
**                                     FREeway AND ARTERIAL DESIGN FEATURES
**
*****
** SUB NO.  SSEC  SSEC  DESIG N  ORG  TRK  SSEC PCT  PCT DES  SPECIAL  FF. SPD.  CAP.  ART  GRADE  SUBSECTI ON LOCATI ON
** SEC LNS  CAP  LENGTH SPEED  DES  FAC  GRAD TRK  TRUCKS  RAMP  ALT. RTE  ALT. RTE  TYPE ALT. RTE
**
** 1
** 2
** 3 1 1650. 11000. 62 0 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 HOV Dummy
** 4 1 1650. 1500. 62 0 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Lawrence On-ramp
** 5 1 1650. 1400. 62 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Lawrence to Crossman
** 6 1 1650. 1500. 62 0 0.95 0.0 0 100 YES 0.0 0. GOOD 0.0 Crossman On-Ramp
** 7 1 1650. 1300. 62 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Crossman / Mathilda
** 8 1 1650. 500. 62 D 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Mathilda Off-Ramp
** 9 1 1650. 2300. 62 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Mathilda / Mathilda
** 10 1 1650. 250. 62 0 0.95 0.0 0 100 YES 0.0 0. GOOD 0.0 Mathilda On-Ramp
** 11 1 1650. 200. 62 0.95 0.0 0 100 YES 0.0 0. GOOD 0.0 Mathilda to US-101
** 12 1 1650. 250. 62 D 0.95 0.0 0 100 YES 0.0 0. GOOD 0.0 US-101 Off-Ramp
** 13 1 1650. 50. 62 D 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Bottleneck by-pass
** 14 1 1650. 50. 62 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Bottleneck
** 15 1 1650. 1000. 62 OD 0.95 0.0 0 100 YES 0.0 0. GOOD 0.0 US 101 / US 101
** 16 1 1650. 10. 62 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Dummy end of travel time
** 17 1 1650. 1500. 62 0 0.95 0.0 0 100 YES 0.0 0. GOOD 0.0 US 101 NB On-Ramp
** 18 1 1650. 1500. 62 D 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Maude Off-ramp
    
```

```

**
** 19 1 1650. 12000. 62 D 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 HOV Dummy
**
** 20
**
*****

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*****
**
** FREEWAY TRAVEL TIME (MINUTES)
**
*****

```

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|------|-----------------------|------|------|------|------|------|------|------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 3.15 | 3.70 | 3.71 | 3.90 | 4.46 | 6.66 | 0.00 | |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.44 | 4.64 | 0.00 | |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 4.11 | 0.00 | |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.08 | 0.00 | |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.93 | 0.00 | |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.75 | 0.00 | |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | |
|-----------|--------|------------|------------|------------|-----------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|------|------|
| * SEC | * LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * SSEC | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP/L | * LEVEL | * MPG | * GS/VM | | |
| * 1 | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | |
| * 3 | 1 | 11000. | 1401. | 0. | 1401. | 1401. | 0. | 1401. | 1650. | 0. | 0. | 0. | .85 | 62. | 22.6 C | 21.6 | 12.8 |
| * 4 | 1 | 1500. | 4. | 0. | 1405. | 4. | 0. | 1405. | 1650. | 0. | 0. | 0. | .85 | 62. | 22.7 C | 21.6 | 12.8 |
| * 5 | 1 | 1400. | 0. | 0. | 1405. | 0. | 0. | 1405. | 1650. | 0. | 0. | 0. | .85 | 62. | 22.7 C | 21.6 | 12.8 |
| * 6 | 1 | 1500. | 61. | 0. | 1466. | 61. | 0. | 1466. | 1650. | 0. | 0. | 0. | .89 | 62. | 23.6 C | 21.6 | 12.8 |
| * 7 | 1 | 1300. | 0. | 0. | 1466. | 0. | 0. | 1466. | 1650. | 0. | 0. | 0. | .89 | 62. | 23.6 C | 21.6 | 12.8 |
| * 8 | 1 | 500. | 0. | 282. | 1466. | 0. | 282. | 1466. | 1650. | 0. | 0. | 0. | .89 | 62. | 23.6 C | 21.6 | 12.8 |
| * 9 | 1 | 2300. | 0. | 0. | 1185. | 0. | 0. | 1185. | 1650. | 0. | 0. | 0. | .72 | 62. | 19.1 C | 21.6 | 12.8 |
| * 10 | 1 | 250. | 32. | 0. | 1217. | 32. | 0. | 1217. | 1650. | 0. | 0. | 0. | .74 | 62. | 19.6 C | 21.6 | 12.8 |
| * 11 | 1 | 200. | 0. | 0. | 1217. | 0. | 0. | 1217. | 1650. | 0. | 0. | 0. | .74 | 62. | 19.6 C | 21.6 | 12.8 |
| * 12 | 1 | 250. | 0. | 360. | 1217. | 0. | 360. | 1217. | 1650. | 0. | 0. | 0. | .74 | 62. | 19.6 C | 21.6 | 12.8 |
| * 13 | 1 | 50. | 0. | 0. | 857. | 0. | 0. | 857. | 1650. | 0. | 0. | 0. | .52 | 62. | 13.8 B | 21.6 | 12.8 |
| * 14 | 1 | 50. | 0. | 0. | 857. | 0. | 0. | 857. | 1650. | 0. | 0. | 0. | .52 | 62. | 13.8 B | 21.6 | 12.8 |
| * 15 | 1 | 1000. | 0. | 0. | 857. | 0. | 0. | 857. | 1650. | 0. | 0. | 0. | .52 | 62. | 13.8 B | 21.6 | 12.8 |
| * 16 | 1 | 10. | 0. | 0. | 857. | 0. | 0. | 857. | 1650. | 0. | 0. | 0. | .52 | 62. | 13.8 B | 21.6 | 12.8 |
| * 17 | 1 | 1500. | 139. | 0. | 996. | 139. | 0. | 996. | 1650. | 0. | 0. | 0. | .60 | 62. | 16.1 B | 21.6 | 12.8 |
| * 18 | 1 | 1500. | 0. | 164. | 996. | 0. | 164. | 996. | 1650. | 0. | 0. | 0. | .60 | 62. | 16.1 B | 21.6 | 12.8 |
| * 19 | 1 | 12000. | 0. | 832. | 832. | 0. | 832. | 832. | 1650. | 0. | 0. | 0. | .50 | 62. | 13.4 B | 21.6 | 12.8 |
| * 20 | | | | | | | | | | | | | | | | | |
| * TOTAL | 36310. | = | 6.9 MI LBS | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|-----------------------------|--------------------|---------|-------------------|----------|
| FREWAY TRAVEL TIME = | 64. | VEH-HRS | 128. | PASS-HRS |
| FREWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 64. | VEH-HRS | 128. | PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 3961. | VEH-MI. | 7921. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. | MPH. | 62. | MPH. |
| AVERAGE DENSITY = | 19. | VPMP/L | 19. | VPMP/L |
| TOTAL FUEL = | 184. | GALLONS | 184. | GALLONS |

TOTAL EMISSIONS = 51. KILOGRAMS

SR-237_WB_AM_P1_2040_PL 51. KILOGRAMS

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/30/2016 12:52 PAGE 5
UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE TIME SLICE 1 OF 4

Table with columns: SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY. Includes summary rows for MAINTENANCE DELAY and TOTAL DELAY.

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/30/2016 12:52 PAGE 6
UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE TIME SLICE 2 OF 4

**
** FREEWAY TRAVEL TIME (MINUTES)
**

Table with columns: ORIGINS DOWN, DESTINATIONS ACROSS (1-8). Includes summary rows for ORIGIN DOWN and DESTINATIONS ACROSS.

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/30/2016 12:52 PAGE 7
UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE TIME SLICE 2 OF 4

TIME SLICE FREEWAY PERFORMANCE TABLE

Table with columns: SUB SEC, NO. LNS, SSEC LENGTH, O-D DATA ORG, DEMANDS DES, SSEC, ADJUSTED VOLUMES ORG, DES, SSEC, SSEC CAP, WEAVE EFF, CONGEST LENGTH, STORAGE RATE, V/C RATIO, SPEED MPH, DENSITY VPMP, LOS LEVEL, FUEL MPG, EMISSIONS GS/VM.

TOTAL 36310. = 6.9 MI LBS MAX(V/C) = 0.89 LOWEST LOS = C AVG = 62. 18.6 21.6 12.8

SR-237_WB_AM_P1_2040_PL

| | | | | | | | | | | | | | | | | | |
|------|---|--------|------|------|-------|------|------|-------|-------|----|----|-----|-----|------|---|------|------|
| * 16 | 1 | 10. | 0. | 0. | 922. | 0. | 0. | 922. | 1650. | 0. | 0. | .56 | 62. | 14.9 | B | 21.6 | 12.8 |
| * 17 | 1 | 1500. | 204. | 0. | 1126. | 204. | 0. | 1126. | 1650. | 0. | 0. | .68 | 62. | 18.2 | C | 21.6 | 12.8 |
| * 18 | 1 | 1500. | 0. | 230. | 1126. | 0. | 228. | 1126. | 1650. | 0. | 0. | .68 | 62. | 18.2 | C | 21.6 | 12.8 |
| * 19 | 1 | 12000. | 0. | 896. | 896. | 0. | 896. | 896. | 1650. | 0. | 0. | .54 | 62. | 14.5 | B | 21.6 | 12.8 |
| * 20 | | | | | | | | | | | | | | | | | |

| | | | | | | | | | | | | | | |
|---------|--------|---|-----|--------|--|--|--|--|-----------------|----------------|-----------|------|------|------|
| * TOTAL | 36310. | = | 6.9 | MI LES | | | | | MAX(V/C) = 0.95 | LOWEST LOS = D | AVG = 61. | 20.2 | 21.8 | 12.6 |
|---------|--------|---|-----|--------|--|--|--|--|-----------------|----------------|-----------|------|------|------|

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 70. VEH-HRS | 139. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 70. VEH-HRS | 140. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 4250. VEH-MI. | 8499. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 61. MPH. | |
| AVERAGE DENSITY = | 20. VPMP | |
| TOTAL FUEL = | 195. GALLONS | |
| TOTAL EMISSIONS = | 54. KILOGRAMS | |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/30/2016 12:52 PAGE 11
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 3 OF 4

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 1.17 | 4 | 0.16 | 5 | 0.15 |
| 6 | 0.64 | 7 | 0.55 | 8 | 0.21 | 9 | 0.19 | 10 | 0.02 |
| 11 | 0.02 | 12 | 0.02 | 13 | 0.00 | 14 | 0.00 | 15 | 0.06 |
| 16 | 0.00 | 17 | 0.12 | 18 | 0.12 | 19 | 0.76 | 20 | 0.00 |

***** TOTAL DELAY = 4.2 VEH-HRS ***** AVERAGE DELAY = 0.19 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-------------------------|-----------------------|---------------|----------|---------|---------|----------|----------------------|
| OFF-RAMP 6 OUTPUT POINT | 1. | 0.23 | 0.08 | 0.00 | 0.03 | 0.00 | 0.03 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/30/2016 12:52 PAGE 12
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 4 OF 4

 ** **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 ** **

| * ORIGINS DOWN | * DESTINATIONS ACROSS | | | | | | | |
|----------------|-----------------------|------|------|------|------|------|------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 3.23 | 3.78 | 3.79 | 3.98 | 4.53 | 6.73 | 0.00 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.52 | 4.72 | 0.00 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 4.19 | 0.00 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.08 | 0.00 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.93 | 0.00 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.75 | 0.00 |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/30/2016 12:52 PAGE 13
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 4 OF 4

 * *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 * *

SR-237_WB_AM_P1_2040_PL

| * SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMI SS | * SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP EFF LENGTH RATE RATIO MPH VPMP L LEVEL MPG GS/VM | * * * * * | | | | | | | | | | | | | | | | | |
|---|---|-----------|-------|------|--------|-------|------|-------|-------|-----------------|----------------|-----------|------|-----|------|---|------|------|--|
| * 1 | | | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | | | |
| * 3 | 1 | 11000. | 1503. | 0. | 1503. | 1503. | 0. | 1503. | 1650. | 0. | 0. | 0. | .91 | 62. | 24.2 | C | 21.6 | 12.8 | |
| * 4 | 1 | 1500. | 5. | 0. | 1508. | 5. | 0. | 1508. | 1650. | 0. | 0. | 0. | .91 | 62. | 24.3 | C | 21.6 | 12.8 | |
| * 5 | 1 | 1400. | 0. | 0. | 1508. | 0. | 0. | 1508. | 1650. | 0. | 0. | 0. | .91 | 62. | 24.3 | C | 21.6 | 12.8 | |
| * 6 | 1 | 1500. | 67. | 0. | 1574. | 67. | 0. | 1574. | 1650. | 0. | 0. | 0. | .95 | 55. | 28.7 | D | 24.4 | 11.2 | |
| * 7 | 1 | 1300. | 0. | 0. | 1574. | 0. | 0. | 1574. | 1650. | 0. | 0. | 0. | .95 | 55. | 28.7 | D | 24.4 | 11.2 | |
| * 8 | 1 | 500. | 0. | 376. | 1574. | 0. | 376. | 1574. | 1650. | 0. | 0. | 0. | .95 | 55. | 28.7 | D | 24.4 | 11.2 | |
| * 9 | 1 | 2300. | 0. | 0. | 1199. | 0. | 0. | 1199. | 1650. | 0. | 0. | 0. | .73 | 62. | 19.3 | C | 21.6 | 12.8 | |
| * 10 | 1 | 250. | 38. | 0. | 1237. | 38. | 0. | 1237. | 1650. | 0. | 0. | 0. | .75 | 62. | 19.9 | C | 21.6 | 12.8 | |
| * 11 | 1 | 200. | 0. | 0. | 1237. | 0. | 0. | 1237. | 1650. | 0. | 0. | 0. | .75 | 62. | 19.9 | C | 21.6 | 12.8 | |
| * 12 | 1 | 250. | 0. | 302. | 1237. | 0. | 302. | 1237. | 1650. | 0. | 0. | 0. | .75 | 62. | 19.9 | C | 21.6 | 12.8 | |
| * 13 | 1 | 50. | 0. | 75. | 934. | 0. | 75. | 934. | 1650. | 0. | 0. | 0. | .57 | 62. | 15.1 | B | 21.6 | 12.8 | |
| * 14 | 1 | 50. | 0. | 0. | 859. | 0. | 0. | 859. | 1650. | 0. | 0. | 0. | .52 | 62. | 13.9 | B | 21.6 | 12.8 | |
| * 15 | 1 | 1000. | 63. | 0. | 922. | 63. | 0. | 922. | 1650. | 0. | 0. | 0. | .56 | 62. | 14.9 | B | 21.6 | 12.8 | |
| * 16 | 1 | 10. | 0. | 0. | 922. | 0. | 0. | 922. | 1650. | 0. | 0. | 0. | .56 | 62. | 14.9 | B | 21.6 | 12.8 | |
| * 17 | 1 | 1500. | 204. | 0. | 1126. | 204. | 0. | 1126. | 1650. | 0. | 0. | 0. | .68 | 62. | 18.2 | C | 21.6 | 12.8 | |
| * 18 | 1 | 1500. | 0. | 230. | 1126. | 0. | 228. | 1126. | 1650. | 0. | 0. | 0. | .68 | 62. | 18.2 | C | 21.6 | 12.8 | |
| * 19 | 1 | 12000. | 0. | 896. | 896. | 0. | 896. | 896. | 1650. | 0. | 0. | 0. | .54 | 62. | 14.5 | B | 21.6 | 12.8 | |
| * 20 | | | | | | | | | | | | | | | | | | | |
| * TOTAL | | 36310. | = | 6.9 | MI LES | | | | | MAX(V/C) = 0.95 | LOWEST LOS = D | AVG = 61. | 20.2 | | | | 21.8 | 12.6 | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 70. VEH-HRS | 139. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 1. VEH-HRS | 1. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 70. VEH-HRS | 141. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 4250. VEH-MI. | 8499. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 60. MPH. | 62. MPH. |
| AVERAGE DENSITY = | 20. VPMP | 19. VPMP |
| TOTAL FUEL = | 195. GALLONS | 757. GALLONS |
| TOTAL EMISSIONS = | 54. KILOGRAMS | 208. KILOGRAMS |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/30/2016 12:52 PAGE 14
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 4 OF 4

***** MAINTENANCE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 1.17 | 4 | 0.16 | 5 | 0.15 |
| 6 | 0.64 | 7 | 0.55 | 8 | 0.21 | 9 | 0.19 | 10 | 0.02 |
| 11 | 0.02 | 12 | 0.02 | 13 | 0.00 | 14 | 0.00 | 15 | 0.06 |
| 16 | 0.00 | 17 | 0.12 | 18 | 0.12 | 19 | 0.76 | 20 | 0.00 |

***** TOTAL DELAY = 4.2 VEH-HRS ***** AVERAGE DELAY = 0.19 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-------------------------|-----------------------|---------------|----------|---------|---------|----------|----------------------|
| OFF-RAMP 6 OUTPUT POINT | 2. | 0.68 | 0.23 | 0.01 | 0.08 | 0.00 | 0.10 |

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FFF       RRR   RRR  EEE      QQQQ   QQQQ   1111   222 222  PPP   PPP  EEE
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FFFFFFFFF RRRRRRRR EEEEEEE  QQQQ   QQQQ   1111           222  PPPPPPPP  EEEEEEE
FFF       RRR   RRR  EEE      QQQQ   QQQ   QQQ  1111   2222  PPP       EEE
FFF       RRR   RRR  EEE      Q*UC*   QQQQ   1111   222  PPP       EEE
FFF       RRR   RRR  EEEEEEEEE Q*REGENTS*Q  1111   222  PPP       EEEEEEEEE
FFF       RRR   RRR  EEEEEEEEE Q*1999*Q QQQ 11111111 2222222222 PPP       EEEEEEEEE
    
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FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 2.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 30
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT DES TRUCKS | SPECIAL RAMP | FF. SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION LOCATION |
|---------|----------|----------|-------------|--------------|---------|---------|-----------|---------|----------------|--------------|-------------------|---------------|----------|----------------|--------------------------|
| ** 1 | 3 | 6000. | 500. | 65 | 0 | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Seed |
| ** 2 | 3 | 6000. | 9999. | 65 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture |
| ** 3 | 2 | 4000. | 11000. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** 4 | 2 | 4000. | 1500. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence On-ramp |
| ** 5 | 2 | 4000. | 1400. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence to Crossman |
| ** 6 | 2 | 4000. | 1500. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Crossman On-Ramp |
| ** 7 | 2 | 4000. | 1300. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Crossman / Mathilda |
| ** 8 | 3 | 5630. | 500. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-Ramp |
| ** 9 | 2 | 4000. | 2300. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda |
| ** 10 | 3 | 4390. | 250. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda On-Ramp |
| ** 11 | 3 | 4390. | 200. | 62 | | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda to US-101 |
| ** 12 | 3 | 4390. | 250. | 62 | D | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US-101 Off-Ramp |
| ** 13 | 2 | 4000. | 50. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bottleneck by-pass |
| ** 14 | 2 | 2400. | 50. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bottleneck |
| ** 15 | 2 | 4000. | 1000. | 62 | OD | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US 101 / US 101 |
| ** 16 | 2 | 4000. | 10. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Dummy end of travel time |
| ** 17 | 2 | 4000. | 1500. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US 101 NB On-Ramp |
| ** 18 | 2 | 4000. | 1500. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Maude Off-ramp |
| ** 19 | 2 | 4000. | 12000. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** 20 | 3 | 6000. | 500. | 65 | OD | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End Of HOV |

***** INPUT HAS BEEN COMPLETED *****

QUEUE COLLISION IN SECTION 4 T2 =0.116

** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | * |
|-----------|--|-----------------------|---|---|---|---|---|---|---|
| * DOWN | | | | | | | | | * |
| | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | * |
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* TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB | * NO. | * SSEC | * O-D | * DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|---------|-------|----------|---------|-------------|-----------|-----------------|-----------|---------|----------------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 1 | * 3 | * 500. | * 5389. | * 0. | * 5389. | * 5389. | * 0. | * 5389. | * 6000. | * 0. | * 0. | * .90 | * 59. | * 30.3 | * D | * 21.6 | * 12.2 |
| * 2 | * 3 | * 99999. | * 0. | * 1401. | * 5389. | * 0. | * 1401. | * 5389. | * 6000. | * 0. | * 0. | * .90 | * 59. | * 30.3 | * D | * 21.6 | * 12.2 |
| * 3 | * 2 | * 11000. | * 0. | * 0. | * 3988. | * 0. | * 0. | * 3424. | * 4000. | * 0. | * 9691. | * .86 | * 32. | * 53.1 | * F | * 21.1 | * 13.1 |
| * 4 | * 2 | * 1500. | * 26. | * 0. | * 4014. | * 26. | * 0. | * 3450. | * 3996. | * 0. | * 1500. | * .86 | * 21. | * 84.1 | * F | * 18.2 | * 16.1 |
| * 5 | * 2 | * 1400. | * 0. | * 0. | * 4014. | * 0. | * 0. | * 3450. | * 4000. | * 0. | * 1400. | * .86 | * 19. | * 92.5 | * F | * 17.6 | * 16.9 |
| * 6 | * 2 | * 1500. | * 489. | * 0. | * 4503. | * 489. | * 0. | * 3939. | * 3939. | * 0. | * 0. | * 1.00 | * 52. | * 38.2 | * E | * 23.6 | * 11.1 |
| * 7 | * 2 | * 1300. | * 0. | * 0. | * 4503. | * 0. | * 0. | * 3939. | * 4000. | * 0. | * 0. | * .98 | * 53. | * 37.3 | * E | * 23.4 | * 11.2 |
| * 8 | * 3 | * 500. | * 0. | * 918. | * 4503. | * 0. | * 805. | * 3939. | * 5348. | * 0. | * 0. | * .74 | * 62. | * 21.2 | * C | * 20.3 | * 13.0 |
| * 9 | * 2 | * 2300. | * 0. | * 0. | * 3585. | * 0. | * 0. | * 3134. | * 4000. | * 0. | * 0. | * .78 | * 61. | * 25.6 | * C | * 20.7 | * 12.8 |
| * 10 | * 3 | * 250. | * 190. | * 0. | * 3775. | * 190. | * 0. | * 3324. | * 4360. | * 0. | * 0. | * .76 | * 62. | * 17.9 | * B | * 20.3 | * 13.0 |
| * 11 | * 3 | * 200. | * 0. | * 0. | * 3775. | * 0. | * 0. | * 3324. | * 4390. | * 0. | * 0. | * .76 | * 62. | * 17.9 | * B | * 20.3 | * 13.0 |
| * 12 | * 3 | * 250. | * 0. | * 1245. | * 3775. | * 0. | * 1100. | * 3324. | * 4030. | * 0. | * 0. | * .82 | * 62. | * 17.9 | * B | * 20.3 | * 13.0 |
| * 13 | * 2 | * 50. | * 0. | * 0. | * 2530. | * 0. | * 0. | * 2225. | * 4000. | * 0. | * 0. | * .56 | * 62. | * 17.9 | * B | * 20.3 | * 13.0 |
| * 14 | * 2 | * 50. | * 0. | * 0. | * 2530. | * 0. | * 0. | * 2225. | * 2400. | * 0. | * 0. | * .93 | * 62. | * 17.9 | * B | * 20.3 | * 13.0 |
| * 15 | * 2 | * 1000. | * 0. | * 0. | * 2530. | * 0. | * 0. | * 2225. | * 4000. | * 0. | * 0. | * .56 | * 62. | * 17.9 | * B | * 20.3 | * 13.0 |
| * 16 | * 2 | * 10. | * 0. | * 0. | * 2530. | * 0. | * 0. | * 2225. | * 4000. | * 0. | * 0. | * .56 | * 62. | * 17.9 | * B | * 20.3 | * 13.0 |
| * 17 | * 2 | * 1500. | * 540. | * 0. | * 3070. | * 540. | * 0. | * 2765. | * 3862. | * 0. | * 0. | * .72 | * 62. | * 22.3 | * C | * 20.3 | * 13.0 |
| * 18 | * 2 | * 1500. | * 0. | * 708. | * 3070. | * 0. | * 643. | * 2765. | * 3836. | * 0. | * 0. | * .72 | * 62. | * 22.3 | * C | * 20.3 | * 13.0 |
| * 19 | * 2 | * 12000. | * 0. | * 0. | * 2362. | * 0. | * 0. | * 2122. | * 4000. | * 0. | * 0. | * .53 | * 62. | * 17.1 | * B | * 20.3 | * 13.0 |
| * 20 | * 3 | * 500. | * 829. | * 3191. | * 3191. | * 829. | * 2951. | * 2951. | * 6000. | * 0. | * 0. | * .49 | * 65. | * 15.1 | * B | * 19.0 | * 14.1 |
| * TOTAL | | 137309. | = | 26.0 MI LBS | | MAX(V/C) = 1.00 | | | LOWEST LOS = F | | AVG = 55. | | 31.8 | 21.4 | 12.4 | | |

SR-237_WB_AM_P2_2040_PE

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | | | |
|----------------------------|--------------------|-----------------|-------------------|-----------------|--|--|
| FREEWAY TRAVEL TIME = | 1132. VEH-HRS | 1359. PASS-HRS | 1132. VEH-HRS | 1359. PASS-HRS | | |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | | |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | | |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | | |
| TOTAL SYSTEM TRAVEL TIME = | 1132. VEH-HRS | 1359. PASS-HRS | 1132. VEH-HRS | 1359. PASS-HRS | | |
| TOTAL TRAV DISTANCE = | 61910. VEH-MI. | 75375. PASS-MI. | 61910. VEH-MI. | 75375. PASS-MI. | | |
| AVERAGE SYSTEM SPEED = | 55. MPH | | 55. MPH | | | |
| AVERAGE DENSITY = | 32. VPML | | 32. VPML | | | |
| TOTAL FUEL = | 2892. GALLONS | | 2892. GALLONS | | | |
| TOTAL EMISSIONS = | 768. KI LOGRAMS | | 768. KI LOGRAMS | | | |

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 TIME SLICE 1 OF 4

***** MAINTENANCE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.38 | 2 | 75.76 | 3 | 61.73 | 4 | 16.80 | 5 | 17.66 |
| 6 | 2.24 | 7 | 1.73 | 8 | 0.14 | 9 | 0.64 | 10 | 0.06 |
| 11 | 0.05 | 12 | 0.06 | 13 | 0.01 | 14 | 0.01 | 15 | 0.16 |
| 16 | 0.00 | 17 | 0.29 | 18 | 0.29 | 19 | 1.80 | 20 | 0.00 |

***** TOTAL DELAY = 179.8 VEH-HRS ***** AVERAGE DELAY = 2.67 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 3/30/2016 16:18 PAGE 8
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 4

 **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN *
 * 1 2 3 4 5 6 7 *

| | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|
| * 1 * | 20.58 | 30.25 | 30.80 | 30.81 | 31.00 | 31.55 | 33.84 |
| * 2 * | 0.00 | 2.55 | 3.10 | 3.11 | 3.30 | 3.85 | 6.14 |
| * 3 * | 0.00 | 0.70 | 1.26 | 1.27 | 1.46 | 2.01 | 4.30 |
| * 4 * | 0.00 | 0.00 | 0.13 | 0.14 | 0.33 | 0.88 | 3.17 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.18 | 0.73 | 3.02 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.55 | 2.84 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.09 |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 4

 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *

| * SUB NO. | * SEC LNS | * SSEC LENGTH | * O-D DATA ORG DES | * DEMANDS SSEC | * ADJUSTED VOLUMES ORG DES | * SSEC CAP. | * WEAVE EFF | * CONGEST LENGTH | * STORAGE RATE | * V/C RATIO | * SPEED MPH | * DENSITY VPML | * LOS LEVEL | * FUEL MPG | * EMISSIONS GS/VM | | | |
|-----------|-----------|---------------|--------------------|----------------|----------------------------|-------------|-------------|------------------|----------------|-------------|-------------|----------------|-------------|------------|-------------------|---|------|------|
| * 1 | 3 | 500. | 5389. | 0. | 5389. | 5389. | 0. | 5389. | 6000. | 0. | 5623. | 564. | .80 | 59. | 30.3 | D | 21.6 | 12.2 |
| * 2 | 3 | 99999. | 0. | 1401. | 5389. | 0. | 1401. | 4825. | 6000. | 0. | 5623. | 564. | .80 | 55. | 29.0 | F | 21.4 | 12.4 |
| * 3 | 2 | 11000. | 0. | 0. | 3988. | 0. | 0. | 3424. | 4000. | 0. | 11000. | 564. | .86 | 18. | 97.6 | F | 17.1 | 17.5 |
| * 4 | 2 | 1500. | 26. | 0. | 4014. | 26. | 0. | 3450. | 3996. | 0. | 1500. | 546. | .86 | 18. | 96.3 | F | 17.3 | 17.3 |
| * 5 | 2 | 1400. | 0. | 0. | 4014. | 0. | 0. | 3450. | 4000. | 0. | 1400. | 546. | .86 | 18. | 96.6 | F | 17.3 | 17.3 |
| * 6 | 2 | 1500. | 489. | 0. | 4503. | 489. | 0. | 3939. | 3939. | 0. | 0. | 0. | 1.00 | 52. | 38.2 | E | 23.6 | 11.1 |
| * 7 | 2 | 1300. | 0. | 0. | 4503. | 0. | 0. | 3939. | 4000. | 0. | 0. | 0. | .98 | 53. | 37.3 | E | 23.4 | 11.2 |
| * 8 | 3 | 500. | 0. | 918. | 4503. | 0. | 805. | 3939. | 5348. | 0. | 0. | 0. | .74 | 62. | 21.2 | C | 20.3 | 13.0 |
| * 9 | 2 | 2300. | 0. | 0. | 3585. | 0. | 0. | 3134. | 4000. | 0. | 0. | 0. | .78 | 61. | 25.6 | C | 20.7 | 12.8 |
| * 10 | 3 | 250. | 190. | 0. | 3775. | 190. | 0. | 3324. | 4360. | 0. | 0. | 0. | .76 | 62. | 17.9 | B | 20.3 | 13.0 |
| * 11 | 3 | 200. | 0. | 0. | 3775. | 0. | 0. | 3324. | 4390. | 0. | 0. | 0. | .76 | 62. | 17.9 | B | 20.3 | 13.0 |
| * 12 | 3 | 250. | 0. | 1245. | 3775. | 0. | 1100. | 3324. | 4030. | 0. | 0. | 0. | .82 | 62. | 17.9 | B | 20.3 | 13.0 |
| * 13 | 2 | 50. | 0. | 0. | 2530. | 0. | 0. | 2225. | 4000. | 0. | 0. | 0. | .56 | 62. | 17.9 | B | 20.3 | 13.0 |
| * 14 | 2 | 50. | 0. | 0. | 2530. | 0. | 0. | 2225. | 2400. | 0. | 0. | 0. | .93 | 62. | 17.9 | B | 20.3 | 13.0 |
| * 15 | 2 | 1000. | 0. | 0. | 2530. | 0. | 0. | 2225. | 4000. | 0. | 0. | 0. | .56 | 62. | 17.9 | B | 20.3 | 13.0 |
| * 16 | 2 | 10. | 0. | 0. | 2530. | 0. | 0. | 2225. | 4000. | 0. | 0. | 0. | .56 | 62. | 17.9 | B | 20.3 | 13.0 |
| * 17 | 2 | 1500. | 540. | 0. | 3070. | 540. | 0. | 2765. | 3862. | 0. | 0. | 0. | .72 | 62. | 22.3 | C | 20.3 | 13.0 |

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| | | | | | | | | | | | | | | | | | | | |
|------|---|--------|------|-------|-------|------|-------|-------|-------|----|----|----|-----|-----|------|---|------|------|---|
| * 18 | 2 | 1500. | 0. | 708. | 3070. | 0. | 643. | 2765. | 3836. | 0. | 0. | 0. | .72 | 62. | 22.3 | C | 20.3 | 13.0 | * |
| * 19 | 2 | 12000. | 0. | 0. | 2362. | 0. | 0. | 2122. | 4000. | 0. | 0. | 0. | .53 | 62. | 17.1 | B | 20.3 | 13.0 | * |
| * 20 | 3 | 500. | 829. | 3191. | 3191. | 829. | 2951. | 2951. | 6000. | 0. | 0. | 0. | .49 | 65. | 15.1 | B | 19.0 | 14.1 | * |

| | | | | | | | | | | | | | | | | | | | |
|---------|---------|---|------|-------|--|--|--|--|-----------------|--|----------------|--|-----------|------|--|--|------|------|---|
| * TOTAL | 137309. | = | 26.0 | MILES | | | | | | | | | | | | | | | |
| | | | | | | | | | MAX(V/C) = 1.00 | | LOWEST LOS = F | | AVG = 48. | 34.6 | | | 21.0 | 12.8 | * |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 1273. VEH-HRS | 1515. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1273. VEH-HRS | 1515. PASS-HRS |
| TOTAL TRAV DISTANCE = | 61374. VEH-MI. | 74805. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 48. MPH. | |
| AVERAGE DENSITY = | 35. VPMPPL | |
| TOTAL FUEL = | 2928. GALLONS | |
| TOTAL EMISSIONS = | 785. KI LOGRAMS | |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 4

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|--------|------------|--------|------------|-------|------------|-------|
| 1 | 0.38 | 2 | 134.34 | 3 | 148.55 | 4 | 19.83 | 5 | 18.58 |
| 6 | 2.24 | 7 | 1.73 | 8 | 0.14 | 9 | 0.64 | 10 | 0.06 |
| 11 | 0.05 | 12 | 0.06 | 13 | 0.01 | 14 | 0.01 | 15 | 0.16 |
| 16 | 0.00 | 17 | 0.29 | 18 | 0.29 | 19 | 1.80 | 20 | 0.00 |

***** TOTAL DELAY = 329.1 VEH-HRS ***** AVERAGE DELAY = 5.09 MIN/VEH *****

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 3 OF 4

 ** FREEWAY TRAVEL TIME (MINUTES) **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN *
 * 1 2 3 4 5 6 7 *

| | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|
| * 1 * | 26.57 | 37.86 | 38.41 | 38.42 | 38.61 | 39.19 | 41.48 |
| * 2 * | 0.00 | 2.86 | 3.41 | 3.42 | 3.61 | 4.19 | 6.48 |
| * 3 * | 0.00 | 0.70 | 1.25 | 1.26 | 1.45 | 2.03 | 4.32 |
| * 4 * | 0.00 | 0.00 | 0.13 | 0.14 | 0.33 | 0.91 | 3.20 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.18 | 0.76 | 3.05 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.58 | 2.86 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.09 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 3/30/2016 16:18 PAGE 12
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 3 OF 4

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | |
|-----------|--------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|--------|----------|-----------|----------|---------|-------------|------|------|------|
| * SEC | * LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMPPL | * LEVEL | * GS/VM | | | |
| * 1 | 3 | 500. | 5780. | 0. | 5780. | 5780. | 0. | 5780. | 6000. | 0. | 0. | .96 | 55. | 34.9 | D | 22.8 | 11.4 | |
| * 2 | 3 | 99999. | 0. | 1503. | 5780. | 0. | 1503. | 4729. | 6000. | 0. | * 17496. | 1051. | .79 | 43. | 36.7 | F | 21.8 | 12.2 |
| * 3 | 2 | 11000. | 0. | 0. | 4277. | 0. | 0. | 3226. | 4000. | 0. | * 11000. | 774. | .81 | 15. | 108.8 | F | 15.9 | 19.1 |
| * 4 | 2 | 1500. | 34. | 0. | 4311. | 34. | 0. | 3260. | 3995. | 0. | * 1500. | 735. | .82 | 15. | 106.6 | F | 16.2 | 18.8 |
| * 5 | 2 | 1400. | 0. | 0. | 4311. | 0. | 0. | 3260. | 4000. | 0. | * 1400. | 735. | .81 | 15. | 107.0 | F | 16.2 | 18.8 |

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| | | | | | | | | | | | | | | | | | | | |
|---|----|---|--------|------|-------|-------|------|-------|-------|-------|----|----|------|-----|------|---|------|------|---|
| * | 6 | 2 | 1500. | 673. | 0. | 4984. | 673. | 0. | 3933. | 3933. | 0. | 0. | 1.00 | 52. | 38.1 | E | 23.6 | 11.1 | * |
| * | 7 | 2 | 1300. | 0. | 0. | 4984. | 0. | 0. | 3933. | 4000. | 0. | 0. | .98 | 53. | 37.2 | E | 23.3 | 11.2 | * |
| * | 8 | 3 | 500. | 0. | 1264. | 4984. | 0. | 1001. | 3933. | 5254. | 0. | 0. | .75 | 62. | 21.1 | C | 20.3 | 13.0 | * |
| * | 9 | 2 | 2300. | 0. | 0. | 3720. | 0. | 0. | 2932. | 4000. | 0. | 0. | .73 | 62. | 23.6 | C | 20.3 | 13.0 | * |
| * | 10 | 3 | 250. | 260. | 0. | 3980. | 260. | 0. | 3192. | 4355. | 0. | 0. | .73 | 62. | 17.2 | B | 20.3 | 13.0 | * |
| * | 11 | 3 | 200. | 0. | 0. | 3980. | 0. | 0. | 3192. | 4390. | 0. | 0. | .73 | 62. | 17.2 | B | 20.3 | 13.0 | * |
| * | 12 | 3 | 250. | 0. | 1100. | 3980. | 0. | 887. | 3192. | 4087. | 0. | 0. | .78 | 62. | 17.2 | B | 20.3 | 13.0 | * |
| * | 13 | 2 | 50. | 0. | 274. | 2880. | 0. | 221. | 2304. | 3924. | 0. | 0. | .59 | 62. | 18.6 | C | 20.3 | 13.0 | * |
| * | 14 | 2 | 50. | 0. | 0. | 2606. | 0. | 0. | 2083. | 2400. | 0. | 0. | .87 | 62. | 16.8 | B | 20.3 | 13.0 | * |
| * | 15 | 2 | 1000. | 287. | 0. | 2893. | 287. | 0. | 2370. | 3937. | 0. | 0. | .60 | 62. | 19.1 | C | 20.3 | 13.0 | * |
| * | 16 | 2 | 10. | 0. | 0. | 2893. | 0. | 0. | 2370. | 4000. | 0. | 0. | .59 | 62. | 19.1 | C | 20.3 | 13.0 | * |
| * | 17 | 2 | 1500. | 927. | 0. | 3820. | 927. | 0. | 3297. | 3796. | 0. | 0. | .87 | 59. | 27.9 | D | 21.6 | 12.2 | * |
| * | 18 | 2 | 1500. | 0. | 1280. | 3820. | 0. | 1120. | 3297. | 3770. | 0. | 0. | .87 | 59. | 28.0 | D | 21.7 | 12.2 | * |
| * | 19 | 2 | 12000. | 0. | 0. | 2540. | 0. | 0. | 2177. | 4000. | 0. | 0. | .54 | 62. | 17.6 | B | 20.3 | 13.0 | * |
| * | 20 | 3 | 500. | 892. | 3432. | 3432. | 892. | 3069. | 3069. | 6000. | 0. | 0. | .51 | 65. | 15.7 | B | 19.0 | 14.1 | * |

 * TOTAL 137309. = 26.0 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 39. 41.5 21.2 12.7 *

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 1637. VEH-HRS | 1965. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1637. VEH-HRS | 1965. PASS-HRS |
| TOTAL TRAV DISTANCE = | 63996. VEH-MI. | 78136. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 39. MPH | 46. MPH |
| AVERAGE DENSITY = | 42. VPML | 36. VPML |
| TOTAL FUEL = | 3019. GALLONS | 8839. GALLONS |
| TOTAL EMISSIONS = | 814. KI LOGRAMS | 2367. KI LOGRAMS |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 3 OF 4

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|--------|------------|--------|------------|-------|------------|-------|
| 1 | 0.75 | 2 | 423.64 | 3 | 175.02 | 4 | 23.16 | 5 | 21.71 |
| 6 | 2.24 | 7 | 1.71 | 8 | 0.14 | 9 | 0.48 | 10 | 0.06 |
| 11 | 0.05 | 12 | 0.06 | 13 | 0.01 | 14 | 0.01 | 15 | 0.17 |
| 16 | 0.00 | 17 | 0.72 | 18 | 0.75 | 19 | 1.84 | 20 | 0.00 |

***** TOTAL DELAY = 652.5 VEH-HRS ***** AVERAGE DELAY = 9.62 MIN/VEH *****

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 4 OF 4

 ** FREEWAY TRAVEL TIME (MINUTES) **

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | |
|--------------|---------------------|-------|-------|-------|-------|-------|-------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 1 | 32.86 | 44.16 | 44.71 | 44.72 | 44.91 | 45.49 | 47.78 |
| 2 | 0.00 | 2.86 | 3.41 | 3.42 | 3.61 | 4.19 | 6.48 |
| 3 | 0.00 | 0.70 | 1.25 | 1.26 | 1.45 | 2.03 | 4.32 |
| 4 | 0.00 | 0.00 | 0.13 | 0.14 | 0.33 | 0.91 | 3.20 |
| 5 | 0.00 | 0.00 | 0.00 | 0.00 | 0.18 | 0.76 | 3.05 |
| 6 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.58 | 2.86 |
| 7 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.09 |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 4 OF 4

SR-237_WB_AM_P2_2040_PE
TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI | | | | |
|---|--------|----------|---------|------------------|-------|-------|---------|---------|-------|-------|----------|-------|------|-------|-------|---|------|------|
| SEC LNS | LENGTH | ORG DES | SSEC | ORG DES | SSEC | EFF | LENGTH | RATE | RATIO | MPH | VPMP | LEVEL | MPG | GS/VM | | | | |
| * 1 | 3 | 500. | 5780. | 0. | 5780. | 5780. | 0. | 5780. | 6000. | 0. | 0. | 0. | .96 | 55. | 34.9 | D | 22.8 | 11.4 |
| * 2 | 3 | 99999. | 0. | 1503. | 5780. | 0. | 1503. | 4729. | 6000. | 0. | * 29370. | 1051. | .79 | 35. | 45.4 | F | 20.8 | 13.1 |
| * 3 | 2 | 11000. | 0. | 0. | 4277. | 0. | 0. | 3226. | 4000. | 0. | **11000. | 774. | .81 | 15. | 108.8 | F | 15.9 | 19.1 |
| * 4 | 2 | 1500. | 34. | 0. | 4311. | 34. | 0. | 3260. | 3995. | 0. | ** 1500. | 735. | .82 | 15. | 106.6 | F | 16.2 | 18.8 |
| * 5 | 2 | 1400. | 0. | 0. | 4311. | 0. | 0. | 3260. | 4000. | 0. | ** 1400. | 735. | .81 | 15. | 107.0 | F | 16.2 | 18.8 |
| * 6 | 2 | 1500. | 673. | 0. | 4984. | 673. | 0. | 3933. | 3933. | 0. | 0. | 0. | 1.00 | 52. | 38.1 | E | 23.6 | 11.1 |
| * 7 | 2 | 1300. | 0. | 0. | 4984. | 0. | 0. | 3933. | 4000. | 0. | 0. | 0. | .98 | 53. | 37.2 | E | 23.3 | 11.2 |
| * 8 | 3 | 500. | 0. | 1264. | 4984. | 0. | 1001. | 3933. | 5254. | 0. | 0. | 0. | .75 | 62. | 21.1 | C | 20.3 | 13.0 |
| * 9 | 2 | 2300. | 0. | 0. | 3720. | 0. | 0. | 2932. | 4000. | 0. | 0. | 0. | .73 | 62. | 23.6 | C | 20.3 | 13.0 |
| * 10 | 3 | 250. | 260. | 0. | 3980. | 260. | 0. | 3192. | 4355. | 0. | 0. | 0. | .73 | 62. | 17.2 | B | 20.3 | 13.0 |
| * 11 | 3 | 200. | 0. | 0. | 3980. | 0. | 0. | 3192. | 4390. | 0. | 0. | 0. | .73 | 62. | 17.2 | B | 20.3 | 13.0 |
| * 12 | 3 | 250. | 0. | 1100. | 3980. | 0. | 887. | 3192. | 4087. | 0. | 0. | 0. | .78 | 62. | 17.2 | B | 20.3 | 13.0 |
| * 13 | 2 | 50. | 0. | 274. | 2880. | 0. | 221. | 2304. | 3924. | 0. | 0. | 0. | .59 | 62. | 18.6 | C | 20.3 | 13.0 |
| * 14 | 2 | 50. | 0. | 0. | 2606. | 0. | 0. | 2083. | 2400. | 0. | 0. | 0. | .87 | 62. | 16.8 | B | 20.3 | 13.0 |
| * 15 | 2 | 1000. | 287. | 0. | 2893. | 287. | 0. | 2370. | 3937. | 0. | 0. | 0. | .60 | 62. | 19.1 | C | 20.3 | 13.0 |
| * 16 | 2 | 10. | 0. | 0. | 2893. | 0. | 0. | 2370. | 4000. | 0. | 0. | 0. | .59 | 62. | 19.1 | C | 20.3 | 13.0 |
| * 17 | 2 | 1500. | 927. | 0. | 3820. | 927. | 0. | 3297. | 3796. | 0. | 0. | 0. | .87 | 59. | 27.9 | D | 21.6 | 12.2 |
| * 18 | 2 | 1500. | 0. | 1280. | 3820. | 0. | 1120. | 3297. | 3770. | 0. | 0. | 0. | .87 | 59. | 28.0 | D | 21.7 | 12.2 |
| * 19 | 2 | 12000. | 0. | 0. | 2540. | 0. | 0. | 2177. | 4000. | 0. | 0. | 0. | .54 | 62. | 17.6 | B | 20.3 | 13.0 |
| * 20 | 3 | 500. | 892. | 3432. | 3432. | 892. | 3069. | 3069. | 6000. | 0. | 0. | 0. | .51 | 65. | 15.7 | B | 19.0 | 14.1 |
| ***** | | | | | | | | | | | | | | | | | | |
| * TOTAL 137309. = 26.0 MI LES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 33. 47.9 20.4 13.5 * | | | | | | | | | | | | | | | | | | |
| ***** | | | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------------------|----------------------------------|
| FREWAY TRAVEL TIME = | 1900. VEH-HRS 2296. PASS-HRS | 5942. VEH-HRS 7136. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1900. VEH-HRS 2296. PASS-HRS | 5942. VEH-HRS 7136. PASS-HRS |
| TOTAL TRAV DISTANCE = | 62814. VEH-MI. 76647. PASS-MI. | 250094. VEH-MI. 304963. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 33. MPH | 42. MPH |
| AVERAGE DENSITY = | 48. VPMP | 39. VPMP |
| TOTAL FUEL = | 3081. GALLONS | 11920. GALLONS |
| TOTAL EMISSIONS = | 845. KI LOGRAMS | 3212. KI LOGRAMS |

***** MAINTENANCE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|--------|------------|--------|------------|-------|------------|-------|
| 1 | 0.75 | 2 | 704.57 | 3 | 175.02 | 4 | 23.16 | 5 | 21.71 |
| 6 | 2.24 | 7 | 1.71 | 8 | 0.14 | 9 | 0.48 | 10 | 0.06 |
| 11 | 0.05 | 12 | 0.06 | 13 | 0.01 | 14 | 0.01 | 15 | 0.17 |
| 16 | 0.00 | 17 | 0.72 | 18 | 0.75 | 19 | 1.84 | 20 | 0.00 |

***** TOTAL DELAY = 933.4 VEH-HRS ***** AVERAGE DELAY = 13.19 MIN/VEH *****

```

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ      1111      222222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111    222 222 PPPPPPPP LLL
FFF      RRR      RRR EEE      QQQQ      QQQQ      1111    222 222 PPP  PPP LLL
FFF      RRR      RRR EEE      QQQQ      QQQQ      1111    222 222 PPP  PPP LLL
FFFFFFFF RRRRRRRR EEEEEEEEE QQQQ      QQQQ      1111      222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEEEE QQQQ      QQQQ      1111    2222 PPPPPPPP LLL
FFF      RRR      RRR EEE      QQQQ      QQQ QQQQ    1111    2222 PPP  LLL
FFF      RRR      RRR EEE      Q*UC*      QQQQ      1111    222 PPP  LLL
FFF      RRR      RRR EEEEEEEEE Q*REGENTS*Q      1111    222 PPP  LLLLLLLLLL
FFF      RRR      RRR EEEEEEEEE Q*1988*Q QQQ 11111111 2222222222 PPP  LLLLLLLLLL
    
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FREQ12PLB

- 1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 3 AND 19 WILL BE SIMULATED.
- 2. SHORT TERM CONSEQUENCES ARE REQUESTED.
- 3. THERE ARE 2.0 TIME SLICES PER HOUR.
- 4. WEAVING ANALYSIS IS NOT ENGAGED.
- 5. NO ALTERNATE ROUTE IS PROVIDED.
- 6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 30
- 7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
- 8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
- 9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
- 10. NUMBER OF PRIORITY LANES = 1.
- 11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

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*****
**
**                                     FREEWAY AND ARTERIAL DESIGN FEATURES
**
*****
**
** SUB NO.   SSEC   SSEC   DESI GN   ORG   TRK   SSEC PCT   PCT DES   SPECIAL   FF. SPD.   CAP.   ART   GRADE   SUBSECTI ON LOCATI ON
** SEC LNS   CAP     LENGTH SPEED  DES     FAC  GRAD TRK  TRUCKS   RAMP     ALT. RTE  ALT. RTE  TYPE  ALT. RTE
**
** 1
** 2
** 3  1  1650.  11000.  62    0  0.95  0.0 0  100    NO     0.0     0.  GOOD  0.0 HOV Dummy
** 4  1  1650.  1500.   62    0  0.95  0.0 0  100    NO     0.0     0.  GOOD  0.0 Lawrence On-ramp
** 5  1  1650.  1400.   62      0.95  0.0 0  100    NO     0.0     0.  GOOD  0.0 Lawrence to Crossman
** 6  1  1650.  1500.   62    0  0.95  0.0 0  100    YES    0.0     0.  GOOD  0.0 Crossman On-Ramp
** 7  1  1650.  1300.   62      0.95  0.0 0  100    NO     0.0     0.  GOOD  0.0 Crossman / Mathilda
** 8  1  1650.  500.    62    D  0.95  0.0 0  100    NO     0.0     0.  GOOD  0.0 Mathilda Off-Ramp
** 9  1  1650.  2300.   62      0.95  0.0 0  100    NO     0.0     0.  GOOD  0.0 Mathilda / Mathilda
** 10 1  1650.  250.    62    0  0.95  0.0 0  100    YES    0.0     0.  GOOD  0.0 Mathilda On-Ramp
** 11 1  1650.  200.    62      0.95  0.0 0  100    YES    0.0     0.  GOOD  0.0 Mathilda to US-101
** 12 1  1650.  250.    62    D  0.95  0.0 0  100    YES    0.0     0.  GOOD  0.0 US-101 Off-Ramp
** 13 1  1650.  50.     62    D  0.95  0.0 0  100    NO     0.0     0.  GOOD  0.0 Bottleneck by-pass
** 14 1  1650.  50.     62      0.95  0.0 0  100    NO     0.0     0.  GOOD  0.0 Bottleeck
** 15 1  1650.  1000.   62   OD 0.95  0.0 0  100    YES    0.0     0.  GOOD  0.0 US 101 / US 101
** 16 1  1650.  10.     62      0.95  0.0 0  100    NO     0.0     0.  GOOD  0.0 Dummy end of travel time
** 17 1  1650.  1500.   62    0  0.95  0.0 0  100    YES    0.0     0.  GOOD  0.0 US 101 NB On-Ramp
** 18 1  1650.  1500.   62    D  0.95  0.0 0  100    NO     0.0     0.  GOOD  0.0 Maude Off-ramp
    
```

```

**
** 19 1 1650. 12000. 62 D 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 HOV Dummy
**
** 20
**
*****

```

 ** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|------|-----------------------|------|------|------|------|------|------|------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 3.15 | 3.70 | 3.71 | 3.90 | 4.46 | 6.66 | 0.00 | |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.44 | 4.64 | 0.00 | |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 4.11 | 0.00 | |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.08 | 0.00 | |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.93 | 0.00 | |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.75 | 0.00 | |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | | |
|-----------|--------|------------|-----------|------------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|------|---|------|------|
| * SEC | * LNS | * LENGTH | * ORG DES | * ORG DES | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | | | |
| * 1 | | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | | |
| * 3 | 1 | 11000. | 1401. | 0. | 1401. | 1401. | 0. | 1401. | 1650. | 0. | 0. | 0. | .85 | 62. | 22.6 | C | 21.6 | 12.8 |
| * 4 | 1 | 1500. | 4. | 0. | 1405. | 4. | 0. | 1405. | 1650. | 0. | 0. | 0. | .85 | 62. | 22.7 | C | 21.6 | 12.8 |
| * 5 | 1 | 1400. | 0. | 0. | 1405. | 0. | 0. | 1405. | 1650. | 0. | 0. | 0. | .85 | 62. | 22.7 | C | 21.6 | 12.8 |
| * 6 | 1 | 1500. | 61. | 0. | 1466. | 61. | 0. | 1466. | 1650. | 0. | 0. | 0. | .89 | 62. | 23.6 | C | 21.6 | 12.8 |
| * 7 | 1 | 1300. | 0. | 0. | 1466. | 0. | 0. | 1466. | 1650. | 0. | 0. | 0. | .89 | 62. | 23.6 | C | 21.6 | 12.8 |
| * 8 | 1 | 500. | 0. | 282. | 1466. | 0. | 282. | 1466. | 1650. | 0. | 0. | 0. | .89 | 62. | 23.6 | C | 21.6 | 12.8 |
| * 9 | 1 | 2300. | 0. | 0. | 1185. | 0. | 0. | 1185. | 1650. | 0. | 0. | 0. | .72 | 62. | 19.1 | C | 21.6 | 12.8 |
| * 10 | 1 | 250. | 30. | 0. | 1215. | 30. | 0. | 1215. | 1650. | 0. | 0. | 0. | .74 | 62. | 19.6 | C | 21.6 | 12.8 |
| * 11 | 1 | 200. | 0. | 0. | 1215. | 0. | 0. | 1215. | 1650. | 0. | 0. | 0. | .74 | 62. | 19.6 | C | 21.6 | 12.8 |
| * 12 | 1 | 250. | 0. | 360. | 1215. | 0. | 360. | 1215. | 1650. | 0. | 0. | 0. | .74 | 62. | 19.6 | C | 21.6 | 12.8 |
| * 13 | 1 | 50. | 0. | 0. | 855. | 0. | 0. | 855. | 1650. | 0. | 0. | 0. | .52 | 62. | 13.8 | B | 21.6 | 12.8 |
| * 14 | 1 | 50. | 0. | 0. | 855. | 0. | 0. | 855. | 1650. | 0. | 0. | 0. | .52 | 62. | 13.8 | B | 21.6 | 12.8 |
| * 15 | 1 | 1000. | 0. | 0. | 855. | 0. | 0. | 855. | 1650. | 0. | 0. | 0. | .52 | 62. | 13.8 | B | 21.6 | 12.8 |
| * 16 | 1 | 10. | 0. | 0. | 855. | 0. | 0. | 855. | 1650. | 0. | 0. | 0. | .52 | 62. | 13.8 | B | 21.6 | 12.8 |
| * 17 | 1 | 1500. | 138. | 0. | 993. | 138. | 0. | 993. | 1650. | 0. | 0. | 0. | .60 | 62. | 16.0 | B | 21.6 | 12.8 |
| * 18 | 1 | 1500. | 0. | 164. | 993. | 0. | 164. | 993. | 1650. | 0. | 0. | 0. | .60 | 62. | 16.0 | B | 21.6 | 12.8 |
| * 19 | 1 | 12000. | 0. | 829. | 829. | 0. | 829. | 829. | 1650. | 0. | 0. | 0. | .50 | 62. | 13.4 | B | 21.6 | 12.8 |
| * 20 | | | | | | | | | | | | | | | | | | |

* TOTAL 36310. = 6.9 MILES MAX(V/C) = 0.89 LOWEST LOS = C AVG = 62. 18.6 21.6 12.8 *

| | CURRENT TIME SLICE | | | CUMULATIVE VALUES | | |
|-----------------------------|--------------------|---------|-------|-------------------|-------|---------|
| FREWAY TRAVEL TIME = | 64. | VEH-HRS | 128. | PASS-HRS | 64. | VEH-HRS |
| FREWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 64. | VEH-HRS | 128. | PASS-HRS | 64. | VEH-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 3957. | VEH-MI. | 7913. | PASS-MI. | 3957. | VEH-MI. |
| AVERAGE SYSTEM SPEED = | 62. | MPH. | | | 62. | MPH. |
| AVERAGE DENSITY = | 19. | VPMP | | | 19. | VPMP |
| TOTAL FUEL = | 184. | GALLONS | | | 184. | GALLONS |

TOTAL EMISSIONS = 51. KILOGRAMS

SR-237_WB_AM_P2_2040_PL 51. KILOGRAMS

Table with columns: SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY. Includes summary rows for MAI NLINE DELAY and TOTAL DELAY.

**
** FREEWAY TRAVEL TIME (MINUTES)
**

Table with columns: ORIGINS DOWN, DESTINATIONS ACROSS (1-8). Includes asterisks for alignment and a plus sign on the left margin.

TIME SLICE FREEWAY PERFORMANCE TABLE

Table with columns: SUB NO., SSEC LENGTH, O-D DATA ORG DES, DEMANDS SSEC, ADJUSTED VOLUMES ORG DES SSEC, SSEC CAP., WEAVE EFF, CONGEST LENGTH, STORAGE RATE, V/C RATIO, SPEED MPH, DENSITY VPMP, LOS LEVEL, FUEL MPG, EMISSIONS GS/VM. Includes a TOTAL row at the bottom.

| | CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | |
|-----------------------------|--------------------|-----------|-------|----------|-------------------|-----------|--------|----------|
| FREEWAY TRAVEL TIME = | 64. | VEH-HRS | 128. | PASS-HRS | 128. | VEH-HRS | 255. | PASS-HRS |
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 64. | VEH-HRS | 128. | PASS-HRS | 128. | VEH-HRS | 255. | PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 3957. | VEH-MI. | 7913. | PASS-MI. | 7913. | VEH-MI. | 15827. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. | MPH. | | | 62. | MPH. | | |
| AVERAGE DENSITY = | 19. | VPMP/L | | | 19. | VPMP/L | | |
| TOTAL FUEL = | 184. | GALLONS | | | 367. | GALLONS | | |
| TOTAL EMISSIONS = | 51. | KILOGRAMS | | | 101. | KILOGRAMS | | |

***** MAINTLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 1.09 | 4 | 0.15 | 5 | 0.14 |
| 6 | 0.16 | 7 | 0.13 | 8 | 0.05 | 9 | 0.19 | 10 | 0.02 |
| 11 | 0.02 | 12 | 0.02 | 13 | 0.00 | 14 | 0.00 | 15 | 0.06 |
| 16 | 0.00 | 17 | 0.11 | 18 | 0.11 | 19 | 0.70 | 20 | 0.00 |

***** TOTAL DELAY = 2.9 VEH-HRS ***** AVERAGE DELAY = 0.15 MIN/VEH *****

 **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN *
 * 1 2 3 4 5 6 7 8 *
 + *
 * *
 + *
 * 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
 + *
 * 2 * 0.00 3.23 3.78 3.79 3.98 4.53 6.73 0.00 *
 + *
 * 3 * 0.00 0.00 0.00 0.00 0.00 2.52 4.72 0.00 *
 + *
 * 4 * 0.00 0.00 0.00 0.00 0.00 0.00 4.19 0.00 *
 + *
 * 5 * 0.00 0.00 0.00 0.00 0.00 0.00 3.08 0.00 *
 + *
 * 6 * 0.00 0.00 0.00 0.00 0.00 0.00 2.93 0.00 *
 + *
 * 7 * 0.00 0.00 0.00 0.00 0.00 0.00 2.75 0.00 *
 + *
 * 8 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
 + *
 * *

 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | | |
|-----------|--------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|-------|----------|-----------|---------|--------|-------------|---------|-------|---------|--|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP/L | * LEVEL | * MPG | * GS/VM | |
| * 1 | | | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | | | |
| * 3 | 1 | 11000. | 1503. | 0. | 1503. | 1503. | 0. | 1503. | 1650. | 0. | 0. | 0. | .91 | 62. | 24.2 | C | 21.6 | 12.8 | |
| * 4 | 1 | 1500. | 5. | 0. | 1508. | 5. | 0. | 1508. | 1650. | 0. | 0. | 0. | .91 | 62. | 24.3 | C | 21.6 | 12.8 | |
| * 5 | 1 | 1400. | 0. | 0. | 1508. | 0. | 0. | 1508. | 1650. | 0. | 0. | 0. | .91 | 62. | 24.3 | C | 21.6 | 12.8 | |
| * 6 | 1 | 1500. | 67. | 0. | 1575. | 67. | 0. | 1575. | 1650. | 0. | 0. | 0. | .95 | 55. | 28.7 | D | 24.4 | 11.2 | |
| * 7 | 1 | 1300. | 0. | 0. | 1575. | 0. | 0. | 1575. | 1650. | 0. | 0. | 0. | .95 | 55. | 28.7 | D | 24.4 | 11.2 | |
| * 8 | 1 | 500. | 0. | 376. | 1575. | 0. | 376. | 1575. | 1650. | 0. | 0. | 0. | .95 | 55. | 28.7 | D | 24.4 | 11.2 | |
| * 9 | 1 | 2300. | 0. | 0. | 1199. | 0. | 0. | 1199. | 1650. | 0. | 0. | 0. | .73 | 62. | 19.3 | C | 21.6 | 12.8 | |
| * 10 | 1 | 250. | 35. | 0. | 1234. | 35. | 0. | 1234. | 1650. | 0. | 0. | 0. | .75 | 62. | 19.9 | C | 21.6 | 12.8 | |
| * 11 | 1 | 200. | 0. | 0. | 1234. | 0. | 0. | 1234. | 1650. | 0. | 0. | 0. | .75 | 62. | 19.9 | C | 21.6 | 12.8 | |
| * 12 | 1 | 250. | 0. | 303. | 1234. | 0. | 303. | 1234. | 1650. | 0. | 0. | 0. | .75 | 62. | 19.9 | C | 21.6 | 12.8 | |
| * 13 | 1 | 50. | 0. | 76. | 931. | 0. | 76. | 931. | 1650. | 0. | 0. | 0. | .56 | 62. | 15.0 | B | 21.6 | 12.8 | |
| * 14 | 1 | 50. | 0. | 0. | 855. | 0. | 0. | 855. | 1650. | 0. | 0. | 0. | .52 | 62. | 13.8 | B | 21.6 | 12.8 | |
| * 15 | 1 | 1000. | 63. | 0. | 918. | 63. | 0. | 918. | 1650. | 0. | 0. | 0. | .56 | 62. | 14.8 | B | 21.6 | 12.8 | |

```

SR-237_WB_AM_P2_2040_PL
* 16 1 10. 0. 0. 918. 0. 0. 918. 1650. 0. 0. .56 62. 14.8 B 21.6 12.8 *
* 17 1 1500. 204. 0. 1122. 204. 0. 1122. 1650. 0. 0. .68 62. 18.1 C 21.6 12.8 *
* 18 1 1500. 0. 230. 1122. 0. 228. 1122. 1650. 0. 0. .68 62. 18.1 C 21.6 12.8 *
* 19 1 12000. 0. 892. 892. 0. 892. 892. 1650. 0. 0. .54 62. 14.4 B 21.6 12.8 *
* 20
*
*****
*
* TOTAL 36310. = 6.9 MILES MAX(V/C) = 0.95 LOWEST LOS = D AVG = 61. 20.2 21.8 12.6 *
*
*****

```

```

CURRENT TIME SLICE CUMULATIVE VALUES
FREEWAY TRAVEL TIME = 69. VEH-HRS 139. PASS-HRS 197. VEH-HRS 394. PASS-HRS
FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 70. VEH-HRS 139. PASS-HRS 197. VEH-HRS 395. PASS-HRS
TOTAL FRWAY TRAV DISTANCE = 4244. VEH-MI . 8487. PASS-MI . 12157. VEH-MI . 24314. PASS-MI .
AVERAGE SYSTEM SPEED = 61. MPH. 62. MPH.
AVERAGE DENSITY = 20. VPMP 19. VPMP
TOTAL FUEL = 194. GALLONS 561. GALLONS
TOTAL EMISSIONS = 53. KILOGRAMS 154. KILOGRAMS

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TIME SLICE 3 OF 4

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***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
1 0.00 2 0.00 3 1.17 4 0.16 5 0.15
6 0.64 7 0.55 8 0.21 9 0.19 10 0.02
11 0.02 12 0.02 13 0.00 14 0.00 15 0.06
16 0.00 17 0.12 18 0.12 19 0.75 20 0.00
***** TOTAL DELAY = 4.2 VEH-HRS ***** AVERAGE DELAY = 0.19 MIN/VEH *****

```

```

***** RAMP DELAYS *****
OFF-RAMP 6 OUTPUT POINT 1. 0.21 0.07 0.00 0.02 0.00 0.03
          QUEUE LENGTH DELAY GAS HC CO NOX TOTAL
          VEHICLES VEH-HRS GALS KGMS KGMS KGMS EMISSIONS
          KGMS

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TIME SLICE 4 OF 4

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*****
**
** FREEWAY TRAVEL TIME (MINUTES) **
**
*****

```

```

*****
* ORIGINS DESTINATIONS ACROSS *
* DOWN *
* 1 2 3 4 5 6 7 8 *
+
* * * * *
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 2 * 0.00 3.23 3.78 3.79 3.98 4.53 6.73 0.00
+
* 3 * 0.00 0.00 0.00 0.00 0.00 2.52 4.72 0.00
+
* 4 * 0.00 0.00 0.00 0.00 0.00 0.00 4.19 0.00
+
* 5 * 0.00 0.00 0.00 0.00 0.00 0.00 3.08 0.00
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 2.93 0.00
+
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 2.75 0.00
+
* 8 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* * *
*****

```

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UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
TIME SLICE 4 OF 4

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*****
*
* TIME SLICE FREEWAY PERFORMANCE TABLE *
*

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SR-237_WB_AM_P2_2040_PL

| * SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMISSIONS | * SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMP L LEVEL MPG GS/VM | * | | | | | | | | | | | | | | | | | | | |
|--|--|--------|-------|------|--------|-------|------|-------|-------|-----------------|----------------|-----------|------|-----|------|---|------|------|--|--|--|
| * 1 | | | | | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | | | | | |
| * 3 | 1 | 11000. | 1503. | 0. | 1503. | 1503. | 0. | 1503. | 1650. | 0. | 0. | 0. | .91 | 62. | 24.2 | C | 21.6 | 12.8 | | | |
| * 4 | 1 | 1500. | 5. | 0. | 1508. | 5. | 0. | 1508. | 1650. | 0. | 0. | 0. | .91 | 62. | 24.3 | C | 21.6 | 12.8 | | | |
| * 5 | 1 | 1400. | 0. | 0. | 1508. | 0. | 0. | 1508. | 1650. | 0. | 0. | 0. | .91 | 62. | 24.3 | C | 21.6 | 12.8 | | | |
| * 6 | 1 | 1500. | 67. | 0. | 1575. | 67. | 0. | 1575. | 1650. | 0. | 0. | 0. | .95 | 55. | 28.7 | D | 24.4 | 11.2 | | | |
| * 7 | 1 | 1300. | 0. | 0. | 1575. | 0. | 0. | 1575. | 1650. | 0. | 0. | 0. | .95 | 55. | 28.7 | D | 24.4 | 11.2 | | | |
| * 8 | 1 | 500. | 0. | 376. | 1575. | 0. | 376. | 1575. | 1650. | 0. | 0. | 0. | .95 | 55. | 28.7 | D | 24.4 | 11.2 | | | |
| * 9 | 1 | 2300. | 0. | 0. | 1199. | 0. | 0. | 1199. | 1650. | 0. | 0. | 0. | .73 | 62. | 19.3 | C | 21.6 | 12.8 | | | |
| * 10 | 1 | 250. | 35. | 0. | 1234. | 35. | 0. | 1234. | 1650. | 0. | 0. | 0. | .75 | 62. | 19.9 | C | 21.6 | 12.8 | | | |
| * 11 | 1 | 200. | 0. | 0. | 1234. | 0. | 0. | 1234. | 1650. | 0. | 0. | 0. | .75 | 62. | 19.9 | C | 21.6 | 12.8 | | | |
| * 12 | 1 | 250. | 0. | 303. | 1234. | 0. | 303. | 1234. | 1650. | 0. | 0. | 0. | .75 | 62. | 19.9 | C | 21.6 | 12.8 | | | |
| * 13 | 1 | 50. | 0. | 76. | 931. | 0. | 76. | 931. | 1650. | 0. | 0. | 0. | .56 | 62. | 15.0 | B | 21.6 | 12.8 | | | |
| * 14 | 1 | 50. | 0. | 0. | 855. | 0. | 0. | 855. | 1650. | 0. | 0. | 0. | .52 | 62. | 13.8 | B | 21.6 | 12.8 | | | |
| * 15 | 1 | 1000. | 63. | 0. | 918. | 63. | 0. | 918. | 1650. | 0. | 0. | 0. | .56 | 62. | 14.8 | B | 21.6 | 12.8 | | | |
| * 16 | 1 | 10. | 0. | 0. | 918. | 0. | 0. | 918. | 1650. | 0. | 0. | 0. | .56 | 62. | 14.8 | B | 21.6 | 12.8 | | | |
| * 17 | 1 | 1500. | 204. | 0. | 1122. | 204. | 0. | 1122. | 1650. | 0. | 0. | 0. | .68 | 62. | 18.1 | C | 21.6 | 12.8 | | | |
| * 18 | 1 | 1500. | 0. | 230. | 1122. | 0. | 228. | 1122. | 1650. | 0. | 0. | 0. | .68 | 62. | 18.1 | C | 21.6 | 12.8 | | | |
| * 19 | 1 | 12000. | 0. | 892. | 892. | 0. | 892. | 892. | 1650. | 0. | 0. | 0. | .54 | 62. | 14.4 | B | 21.6 | 12.8 | | | |
| * 20 | | | | | | | | | | | | | | | | | | | | | |
| * TOTAL | | 36310. | = | 6.9 | MI LES | | | | | MAX(V/C) = 0.95 | LOWEST LOS = D | AVG = 61. | 20.2 | | | | 21.8 | 12.6 | | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 69. VEH-HRS | 139. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 1. VEH-HRS | 1. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 70. VEH-HRS | 140. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 4244. VEH-MI. | 8487. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 61. MPH. | 62. MPH. |
| AVERAGE DENSITY = | 20. VPMP | 19. VPMP |
| TOTAL FUEL = | 194. GALLONS | 756. GALLONS |
| TOTAL EMISSIONS = | 53. KILOGRAMS | 208. KILOGRAMS |

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 TIME SLICE 4 OF 4

***** MAINTENANCE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 1.17 | 4 | 0.16 | 5 | 0.15 |
| 6 | 0.64 | 7 | 0.55 | 8 | 0.21 | 9 | 0.19 | 10 | 0.02 |
| 11 | 0.02 | 12 | 0.02 | 13 | 0.00 | 14 | 0.00 | 15 | 0.06 |
| 16 | 0.00 | 17 | 0.12 | 18 | 0.12 | 19 | 0.75 | 20 | 0.00 |

***** TOTAL DELAY = 4.2 VEH-HRS ***** AVERAGE DELAY = 0.19 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-------------------------|-----------------------|---------------|----------|---------|---------|----------|----------------------|
| OFF-RAMP 6 OUTPUT POINT | 2. | 0.63 | 0.22 | 0.01 | 0.07 | 0.00 | 0.09 |

```

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQQ QQQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 2222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP EEEEEEEEE
    
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FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 2.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 30
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT TRUCKS | DES TRUCKS | SPECIAL RAMP | FF. SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION LOCATION |
|---------|----------|----------|-------------|--------------|---------|---------|-----------|---------|------------|------------|--------------|-------------------|---------------|----------|----------------|--------------------------|
| ** 1 | 3 | 6000. | 500. | 65 | 0 | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Seed |
| ** 2 | 3 | 6000. | 99999. | 65 | D | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture |
| ** 3 | 2 | 4000. | 11000. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** 4 | 2 | 4000. | 1500. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence On-ramp |
| ** 5 | 2 | 4000. | 1400. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence to Crossman |
| ** 6 | 2 | 4000. | 1500. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Crossman On-Ramp |
| ** 7 | 2 | 4000. | 1300. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Crossman / Mathilda |
| ** 8 | 3 | 5270. | 500. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-Ramp |
| ** 9 | 2 | 4000. | 2300. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda |
| ** 10 | 3 | 4900. | 250. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda On-ramp |
| ** 11 | 3 | 4900. | 200. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda to US-101 |
| ** 12 | 3 | 4900. | 250. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US-101 Off-Ramp |
| ** 13 | 2 | 4000. | 50. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bottleneck by-pass |
| ** 14 | 2 | 2470. | 50. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bottleneck |
| ** 15 | 2 | 4000. | 1000. | 62 | OD | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US 101 / US 101 |
| ** 16 | 2 | 4000. | 10. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Dummy end of travel time |
| ** 17 | 2 | 4000. | 1500. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US 101 NB On-Ramp |
| ** 18 | 2 | 4000. | 1500. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Maude Off-ramp |
| ** 19 | 2 | 4000. | 12000. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** 20 | 3 | 6000. | 500. | 65 | OD | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End of Network |

***** INPUT HAS BEEN COMPLETED *****

**
** FREeway TRAVEL TIME (MINUTES) **
**

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | |
|-----------|-------|-----------------------|-------|-------|-------|-------|-------|---|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 17.79 | 23.97 | 24.52 | 24.53 | 24.72 | 25.27 | 27.56 | |
| * 2 * | 0.00 | 2.61 | 3.16 | 3.17 | 3.36 | 3.91 | 6.20 | |
| * 3 * | 0.00 | 0.70 | 1.25 | 1.26 | 1.46 | 2.01 | 4.29 | |
| * 4 * | 0.00 | 0.00 | 0.13 | 0.14 | 0.33 | 0.88 | 3.17 | |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.18 | 0.73 | 3.02 | |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.55 | 2.84 | |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.09 | |

*
* TIME SLICE FREEWAY PERFORMANCE TABLE *
*

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|-----------|--------|------------|--------------|------------|--------------|------------|---------|-----------------|----------------|-----------|---------|-----------|---------|--------|-------------|
| * SEC | * LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * SSEC | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 1 | * 3 | * 500. | * 4500. | * 0. 4500. | * 4500. | * 0. 4500. | * 6000. | * 0. | * 0. | * .75 | * 64. | * 23.4 | * C | * 19.3 | * 13.8 |
| * 2 | * 3 | * 99999. | * 0. 720. | * 4500. | * 0. 720. | * 4500. | * 6000. | * 0. | * 0. | * .75 | * 64. | * 23.4 | * C | * 19.3 | * 13.8 |
| * 3 | * 2 | * 11000. | * 0. 0. | * 3780. | * 0. 0. | * 3212. | * 4000. | * 0. | * 7199. | * .80 | * 35. | * 45.8 | * F | * 20.8 | * 13.1 |
| * 4 | * 2 | * 1500. | * 57. 0. | * 3837. | * 57. 0. | * 3269. | * 3996. | * 0. | * 1500. | * .82 | * 18. | * 88.6 | * F | * 17.4 | * 17.0 |
| * 5 | * 2 | * 1400. | * 0. 0. | * 3837. | * 0. 0. | * 3269. | * 4000. | * 0. | * 1400. | * .82 | * 16. | * 100.6 | * F | * 16.6 | * 18.2 |
| * 6 | * 2 | * 1500. | * 687. 0. | * 4524. | * 687. 0. | * 3956. | * 3956. | * 0. | * 0. | * 1.00 | * 52. | * 38.4 | * E | * 23.6 | * 11.1 |
| * 7 | * 2 | * 1300. | * 0. 0. | * 4524. | * 0. 0. | * 3956. | * 4000. | * 0. | * 0. | * .99 | * 52. | * 37.7 | * E | * 23.4 | * 11.2 |
| * 8 | * 3 | * 500. | * 0. 1038. | * 4524. | * 0. 909. | * 3956. | * 5107. | * 0. | * 0. | * .77 | * 62. | * 21.3 | * C | * 20.3 | * 13.0 |
| * 9 | * 2 | * 2300. | * 0. 0. | * 3486. | * 0. 0. | * 3047. | * 4000. | * 0. | * 0. | * .76 | * 62. | * 24.6 | * C | * 20.3 | * 13.0 |
| * 10 | * 3 | * 250. | * 432. 0. | * 3918. | * 432. 0. | * 3479. | * 4863. | * 0. | * 0. | * .72 | * 62. | * 18.7 | * C | * 20.3 | * 13.0 |
| * 11 | * 3 | * 200. | * 0. 0. | * 3918. | * 0. 0. | * 3479. | * 4900. | * 0. | * 0. | * .71 | * 62. | * 18.7 | * C | * 20.3 | * 13.0 |
| * 12 | * 3 | * 250. | * 0. 1715. | * 3918. | * 0. 1527. | * 3479. | * 4661. | * 0. | * 0. | * .75 | * 62. | * 18.7 | * C | * 20.3 | * 13.0 |
| * 13 | * 2 | * 50. | * 0. 44. | * 2203. | * 0. 39. | * 1952. | * 3994. | * 0. | * 0. | * .49 | * 62. | * 15.7 | * B | * 20.3 | * 13.0 |
| * 14 | * 2 | * 50. | * 0. 0. | * 2159. | * 0. 0. | * 1913. | * 2470. | * 0. | * 0. | * .77 | * 62. | * 15.4 | * B | * 20.3 | * 13.0 |
| * 15 | * 2 | * 1000. | * 43. 0. | * 2202. | * 43. 0. | * 1956. | * 3993. | * 0. | * 0. | * .49 | * 62. | * 15.8 | * B | * 20.3 | * 13.0 |
| * 16 | * 2 | * 10. | * 0. 0. | * 2202. | * 0. 0. | * 1956. | * 4000. | * 0. | * 0. | * .49 | * 62. | * 15.8 | * B | * 20.3 | * 13.0 |
| * 17 | * 2 | * 1500. | * 754. 0. | * 2956. | * 754. 0. | * 2710. | * 3877. | * 0. | * 0. | * .70 | * 62. | * 21.9 | * C | * 20.3 | * 13.0 |
| * 18 | * 2 | * 1500. | * 0. 389. | * 2956. | * 0. 359. | * 2710. | * 3961. | * 0. | * 0. | * .68 | * 62. | * 21.9 | * C | * 20.3 | * 13.0 |
| * 19 | * 2 | * 12000. | * 0. 0. | * 2567. | * 0. 0. | * 2351. | * 4000. | * 0. | * 0. | * .59 | * 62. | * 19.0 | * C | * 20.3 | * 13.0 |
| * 20 | * 3 | * 500. | * 489. 3056. | * 3056. | * 489. 2840. | * 2840. | * 6000. | * 0. | * 0. | * .47 | * 65. | * 14.6 | * B | * 19.0 | * 14.1 |
| * TOTAL | | 137309. | = | 26.0 | MILES | | | MAX(V/C) = 1.00 | LOWEST LOS = F | AVG = 58. | 26.4 | | | 19.5 | 13.7 |

| | CURRENT TIME SLICE | | | CUMULATIVE VALUES | | | | |
|----------------------------|--------------------|---------|--------|-------------------|--------|---------|--------|----------|
| FREWAY TRAVEL TIME = | 927. | VEH-HRS | 1035. | PASS-HRS | 927. | VEH-HRS | 1035. | PASS-HRS |
| FREWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 927. | VEH-HRS | 1035. | PASS-HRS | 927. | VEH-HRS | 1035. | PASS-HRS |
| TOTAL TRAV DISTANCE = | 53455. | VEH-MI. | 60379. | PASS-MI. | 53455. | VEH-MI. | 60379. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 58. | MPH. | | | 58. | MPH. | | |

AVERAGE DENSITY = 26. VPML
TOTAL FUEL = 2736. GALLONS
TOTAL EMISSIONS = 732. KI LOGRAMS

SR-237_WB_PM_NP_2040_PE
26. VPML
2736. GALLONS
732. KI LOGRAMS

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 3/30/2016 10:31 PAGE 6
UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
TIME SLICE 1 OF 6

***** MAINTLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
1 0.04 2 8.34 3 49.92 4 18.66 5 20.23
6 2.25 7 1.80 8 0.14 9 0.49 10 0.06
11 0.05 12 0.06 13 0.01 14 0.01 15 0.14
16 0.00 17 0.29 18 0.29 19 1.99 20 0.00
***** TOTAL DELAY = 104.8 VEH-HRS ***** AVERAGE DELAY = 1.90 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 3/30/2016 10:31 PAGE 7
UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
TIME SLICE 2 OF 6

** **
** FREEWAY TRAVEL TIME (MINUTES) **
** **

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | |
|--------------|---------------------|-------|-------|-------|-------|-------|-------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 1 | 18.53 | 29.43 | 29.98 | 29.99 | 30.18 | 30.73 | 33.02 |
| 2 | 0.00 | 2.85 | 3.40 | 3.41 | 3.60 | 4.15 | 6.44 |
| 3 | 0.00 | 0.70 | 1.25 | 1.26 | 1.46 | 2.01 | 4.29 |
| 4 | 0.00 | 0.00 | 0.13 | 0.14 | 0.33 | 0.88 | 3.17 |
| 5 | 0.00 | 0.00 | 0.00 | 0.00 | 0.18 | 0.73 | 3.02 |
| 6 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.55 | 2.84 |
| 7 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.09 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 3/30/2016 10:31 PAGE 8
UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
TIME SLICE 2 OF 6

* *
* TIME SLICE FREEWAY PERFORMANCE TABLE *
* *

| SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS | | | | |
|---------|------|----------|---------|------------------|-------|-------|---------|---------|-------|-------|----------|------|-------|--------|-------|------|------|------|
| SEC | LNS | LENGTH | ORG | DES | SSEC | ORG | DES | SSEC | RATE | RATIO | MPH | VPML | LEVEL | GS/VM | | | | |
| 1 | 3 | 500. | 4500. | 0. | 4500. | 4500. | 0. | 4500. | 6000. | 0. | 0. | .75 | 64. | 23.4 | C | 19.3 | 13.8 | |
| 2 | 3 | 99999. | 0. | 720. | 4500. | 0. | 720. | 3932. | 6000. | 0. | * 2606. | 568. | .66 | 62. | 21.3 | F | 19.2 | 13.9 |
| 3 | 2 | 11000. | 0. | 0. | 3780. | 0. | 0. | 3212. | 4000. | 0. | **11000. | 568. | .80 | 16. | 103.4 | F | 16.2 | 18.6 |
| 4 | 2 | 1500. | 57. | 0. | 3837. | 57. | 0. | 3269. | 3996. | 0. | ** 1500. | 568. | .82 | 15. | 106.2 | F | 16.2 | 18.7 |
| 5 | 2 | 1400. | 0. | 0. | 3837. | 0. | 0. | 3269. | 4000. | 0. | ** 1400. | 568. | .82 | 15. | 106.6 | F | 16.2 | 18.7 |
| 6 | 2 | 1500. | 687. | 0. | 4524. | 687. | 0. | 3956. | 3956. | 0. | 0. | 1.00 | 52. | 38.4 | E | 23.6 | 11.1 | |
| 7 | 2 | 1300. | 0. | 0. | 4524. | 0. | 0. | 3956. | 4000. | 0. | 0. | .99 | 52. | 37.7 | E | 23.4 | 11.2 | |
| 8 | 3 | 500. | 0. | 1038. | 4524. | 0. | 909. | 3956. | 5107. | 0. | 0. | .77 | 62. | 21.3 | C | 20.3 | 13.0 | |
| 9 | 2 | 2300. | 0. | 0. | 3486. | 0. | 0. | 3047. | 4000. | 0. | 0. | .76 | 62. | 24.6 | C | 20.3 | 13.0 | |
| 10 | 3 | 250. | 432. | 0. | 3918. | 432. | 0. | 3479. | 4863. | 0. | 0. | .72 | 62. | 18.7 | C | 20.3 | 13.0 | |
| 11 | 3 | 200. | 0. | 0. | 3918. | 0. | 0. | 3479. | 4900. | 0. | 0. | .71 | 62. | 18.7 | C | 20.3 | 13.0 | |
| 12 | 3 | 250. | 0. | 1715. | 3918. | 0. | 1527. | 3479. | 4661. | 0. | 0. | .75 | 62. | 18.7 | C | 20.3 | 13.0 | |
| 13 | 2 | 50. | 0. | 44. | 2203. | 0. | 39. | 1952. | 3994. | 0. | 0. | .49 | 62. | 15.7 | B | 20.3 | 13.0 | |
| 14 | 2 | 50. | 0. | 0. | 2159. | 0. | 0. | 1913. | 2470. | 0. | 0. | .77 | 62. | 15.4 | B | 20.3 | 13.0 | |
| 15 | 2 | 1000. | 43. | 0. | 2202. | 43. | 0. | 1956. | 3993. | 0. | 0. | .49 | 62. | 15.8 | B | 20.3 | 13.0 | |
| 16 | 2 | 10. | 0. | 0. | 2202. | 0. | 0. | 1956. | 4000. | 0. | 0. | .49 | 62. | 15.8 | B | 20.3 | 13.0 | |
| 17 | 2 | 1500. | 754. | 0. | 2956. | 754. | 0. | 2710. | 3877. | 0. | 0. | .70 | 62. | 21.9 | C | 20.3 | 13.0 | |
| 18 | 2 | 1500. | 0. | 389. | 2956. | 0. | 359. | 2710. | 3961. | 0. | 0. | .68 | 62. | 21.9 | C | 20.3 | 13.0 | |
| 19 | 2 | 12000. | 0. | 0. | 2567. | 0. | 0. | 2351. | 4000. | 0. | 0. | .59 | 62. | 19.0 | C | 20.3 | 13.0 | |
| 20 | 3 | 500. | 489. | 3056. | 3056. | 489. | 2840. | 2840. | 6000. | 0. | 0. | .47 | 65. | 14.6 | B | 19.0 | 14.1 | |

* *
* TOTAL 137309. = 26.0 MI LBS MAX(V/C) = 1.00 LOWEST LOS = F AVG = 50. 29.8 19.1 14.1 *
* *

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|----------------------------|--------------------|-----------------|-------------------|------------------|
| FREEWAY TRAVEL TIME = | 1069. VEH-HRS | 1182. PASS-HRS | 1996. VEH-HRS | 2217. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1069. VEH-HRS | 1182. PASS-HRS | 1996. VEH-HRS | 2217. PASS-HRS |
| TOTAL TRAV DISTANCE = | 52978. VEH-MI. | 59896. PASS-MI. | 106433. VEH-MI. | 120275. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 50. MPH. | | 53. MPH. | |
| AVERAGE DENSITY = | 30. VPMP | | 28. VPMP | |
| TOTAL FUEL = | 2772. GALLONS | | 5508. GALLONS | |
| TOTAL EMISSIONS = | 748. KI LOGRAMS | | 1479. KI LOGRAMS | |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 3/30/2016 10:31 PAGE 9
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION TIME SLICE 2 OF 6

***** MAINTLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|--------|------------|-------|------------|-------|
| 1 | 0.04 | 2 | 36.06 | 3 | 165.83 | 4 | 23.03 | 5 | 21.57 |
| 6 | 2.25 | 7 | 1.80 | 8 | 0.14 | 9 | 0.49 | 10 | 0.06 |
| 11 | 0.05 | 12 | 0.06 | 13 | 0.01 | 14 | 0.01 | 15 | 0.14 |
| 16 | 0.00 | 17 | 0.29 | 18 | 0.29 | 19 | 1.99 | 20 | 0.00 |

***** TOTAL DELAY = 254.1 VEH-HRS ***** AVERAGE DELAY = 4.61 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 3/30/2016 10:31 PAGE 10
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION TIME SLICE 3 OF 6

 ** FREEWAY TRAVEL TIME (MINUTES) **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN *
 * 1 2 3 4 5 6 7 *

| | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|
| * 1 * | 22.88 | 35.01 | 35.56 | 35.57 | 35.76 | 36.31 | 38.60 |
| * 2 * | 0.00 | 2.99 | 3.54 | 3.55 | 3.74 | 4.29 | 6.58 |
| * 3 * | 0.00 | 0.70 | 1.25 | 1.26 | 1.46 | 2.01 | 4.29 |
| * 4 * | 0.00 | 0.00 | 0.13 | 0.14 | 0.33 | 0.88 | 3.17 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.18 | 0.73 | 3.02 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.55 | 2.84 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.09 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 3/30/2016 10:31 PAGE 11
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION TIME SLICE 3 OF 6

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | |
|-----------|--------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|---------|----------|-----------|---------|--------|-------------|------|------|------|
| * SEC | * LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * SSEC | * CAP. | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | | |
| * 1 | 3 | 500. | 4628. | 0. | 4628. | 4628. | 0. | 4628. | 6000. | 0. | 0. | .77 | 64. | 24.2 | C | 19.5 | 13.7 | |
| * 2 | 3 | 99999. | 0. | 741. | 4628. | 0. | 741. | 3866. | 6000. | 0. | * 8195. | 762. | .64 | 50. | 25.8 | F | 18.9 | 14.1 |
| * 3 | 2 | 11000. | 0. | 0. | 3887. | 0. | 0. | 3125. | 4000. | 0. | **11000. | 762. | .78 | 14. | 114.3 | F | 15.1 | 20.0 |
| * 4 | 2 | 1500. | 65. | 0. | 3952. | 65. | 0. | 3190. | 3995. | 0. | ** 1500. | 762. | .80 | 14. | 110.4 | F | 15.7 | 19.4 |
| * 5 | 2 | 1400. | 0. | 0. | 3952. | 0. | 0. | 3190. | 4000. | 0. | ** 1400. | 762. | .80 | 14. | 110.8 | F | 15.6 | 19.4 |
| * 6 | 2 | 1500. | 762. | 0. | 4714. | 762. | 0. | 3952. | 3952. | 0. | 0. | 1.00 | 52. | 38.3 | E | 23.6 | 11.1 | |
| * 7 | 2 | 1300. | 0. | 0. | 4714. | 0. | 0. | 3952. | 4000. | 0. | 0. | .99 | 52. | 37.6 | E | 23.4 | 11.2 | |
| * 8 | 3 | 500. | 0. | 1099. | 4714. | 0. | 923. | 3952. | 5099. | 0. | 0. | .78 | 62. | 21.2 | C | 20.3 | 13.0 | |
| * 9 | 2 | 2300. | 0. | 0. | 3615. | 0. | 0. | 3029. | 4000. | 0. | 0. | .76 | 62. | 24.4 | C | 20.3 | 13.0 | |
| * 10 | 3 | 250. | 461. | 0. | 4076. | 461. | 0. | 3490. | 4862. | 0. | 0. | .72 | 62. | 18.8 | C | 20.3 | 13.0 | |
| * 11 | 3 | 200. | 0. | 0. | 4076. | 0. | 0. | 3490. | 4900. | 0. | 0. | .71 | 62. | 18.8 | C | 20.3 | 13.0 | |
| * 12 | 3 | 250. | 0. | 1532. | 4076. | 0. | 1316. | 3490. | 4690. | 0. | 0. | .74 | 62. | 18.8 | C | 20.3 | 13.0 | |
| * 13 | 2 | 50. | 0. | 175. | 2544. | 0. | 150. | 2174. | 3976. | 0. | 0. | .55 | 62. | 17.5 | B | 20.3 | 13.0 | |

| SR-237_WB_PM_NP_2040_PE | | | | | | | | | | | | | | | | | | | | |
|-------------------------|----|---|--------|------|-------|-------|------|-------|-------|-------|----|----------|------|------|-----|-------|---|------|------|---|
| * | 2 | 3 | 99999. | 0. | 741. | 4628. | 0. | 741. | 3866. | 6000. | 0. | * 13785. | 762. | .64 | 41. | 31.8 | F | 18.3 | 14.6 | * |
| * | 3 | 2 | 11000. | 0. | 0. | 3887. | 0. | 0. | 3125. | 4000. | 0. | **11000. | 762. | .78 | 14. | 114.3 | F | 15.1 | 20.0 | * |
| * | 4 | 2 | 1500. | 65. | 0. | 3952. | 65. | 0. | 3190. | 3995. | 0. | ** 1500. | 762. | .80 | 14. | 110.4 | F | 15.7 | 19.4 | * |
| * | 5 | 2 | 1400. | 0. | 0. | 3952. | 0. | 0. | 3190. | 4000. | 0. | ** 1400. | 762. | .80 | 14. | 110.8 | F | 15.6 | 19.4 | * |
| * | 6 | 2 | 1500. | 762. | 0. | 4714. | 762. | 0. | 3952. | 3952. | 0. | 0. | 0. | 1.00 | 52. | 38.3 | E | 23.6 | 11.1 | * |
| * | 7 | 2 | 1300. | 0. | 0. | 4714. | 0. | 0. | 3952. | 4000. | 0. | 0. | 0. | .99 | 52. | 37.6 | E | 23.4 | 11.2 | * |
| * | 8 | 3 | 500. | 0. | 1099. | 4714. | 0. | 923. | 3952. | 5099. | 0. | 0. | 0. | .78 | 62. | 21.2 | C | 20.3 | 13.0 | * |
| * | 9 | 2 | 2300. | 0. | 0. | 3615. | 0. | 0. | 3029. | 4000. | 0. | 0. | 0. | .76 | 62. | 24.4 | C | 20.3 | 13.0 | * |
| * | 10 | 3 | 250. | 461. | 0. | 4076. | 461. | 0. | 3490. | 4862. | 0. | 0. | 0. | .72 | 62. | 18.8 | C | 20.3 | 13.0 | * |
| * | 11 | 3 | 200. | 0. | 0. | 4076. | 0. | 0. | 3490. | 4900. | 0. | 0. | 0. | .71 | 62. | 18.8 | C | 20.3 | 13.0 | * |
| * | 12 | 3 | 250. | 0. | 1532. | 4076. | 0. | 1316. | 3490. | 4690. | 0. | 0. | 0. | .74 | 62. | 18.8 | C | 20.3 | 13.0 | * |
| * | 13 | 2 | 50. | 0. | 175. | 2544. | 0. | 150. | 2174. | 3976. | 0. | 0. | 0. | .55 | 62. | 17.5 | B | 20.3 | 13.0 | * |
| * | 14 | 2 | 50. | 0. | 0. | 2369. | 0. | 0. | 2023. | 2470. | 0. | 0. | 0. | .82 | 62. | 16.3 | B | 20.3 | 13.0 | * |
| * | 15 | 2 | 1000. | 174. | 0. | 2543. | 174. | 0. | 2197. | 3974. | 0. | 0. | 0. | .55 | 62. | 17.7 | B | 20.3 | 13.0 | * |
| * | 16 | 2 | 10. | 0. | 0. | 2543. | 0. | 0. | 2197. | 4000. | 0. | 0. | 0. | .55 | 62. | 17.7 | B | 20.3 | 13.0 | * |
| * | 17 | 2 | 1500. | 828. | 0. | 3371. | 828. | 0. | 3025. | 3877. | 0. | 0. | 0. | .78 | 62. | 24.4 | C | 20.3 | 13.0 | * |
| * | 18 | 2 | 1500. | 0. | 695. | 3371. | 0. | 628. | 3025. | 3934. | 0. | 0. | 0. | .77 | 62. | 24.4 | C | 20.3 | 13.0 | * |
| * | 19 | 2 | 12000. | 0. | 0. | 2676. | 0. | 0. | 2397. | 4000. | 0. | 0. | 0. | .60 | 62. | 19.3 | C | 20.3 | 13.0 | * |
| * | 20 | 3 | 500. | 510. | 3186. | 3186. | 510. | 2907. | 2907. | 6000. | 0. | 0. | 0. | .48 | 65. | 14.9 | B | 19.0 | 14.1 | * |

* TOTAL 137309. = 26.0 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 36. 38.5 18.3 14.8 *

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------------------|----------------------------------|
| FREEWAY TRAVEL TIME = | 1465. VEH-HRS 1637. PASS-HRS | 4736. VEH-HRS 5269. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1465. VEH-HRS 1637. PASS-HRS | 4736. VEH-HRS 5269. PASS-HRS |
| TOTAL TRAV DISTANCE = | 53460. VEH-MI. 60454. PASS-MI. | 213756. VEH-MI. 241651. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 36. MPH | 45. MPH |
| AVERAGE DENSITY = | 39. VPMP | 32. VPMP |
| TOTAL FUEL = | 2922. GALLONS | 11301. GALLONS |
| TOTAL EMISSIONS = | 792. KI LOGRAMS | 3048. KI LOGRAMS |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 3/30/2016 10:31 PAGE 15
UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
TIME SLICE 4 OF 6

***** MAINTENANCE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|--------|------------|--------|------------|-------|------------|-------|
| 1 | 0.06 | 2 | 399.49 | 3 | 188.10 | 4 | 24.40 | 5 | 22.87 |
| 6 | 2.25 | 7 | 1.78 | 8 | 0.14 | 9 | 0.49 | 10 | 0.06 |
| 11 | 0.05 | 12 | 0.06 | 13 | 0.01 | 14 | 0.01 | 15 | 0.15 |
| 16 | 0.00 | 17 | 0.32 | 18 | 0.32 | 19 | 2.03 | 20 | 0.00 |

***** TOTAL DELAY = 642.6 VEH-HRS ***** AVERAGE DELAY = 10.85 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 3/30/2016 10:31 PAGE 16
UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
TIME SLICE 5 OF 6

**
** FREEWAY TRAVEL TIME (MINUTES) **
**

| * ORIGINS DOWN | * DESTINATIONS ACROSS | | | | | | | |
|----------------|-----------------------|-------|-------|-------|-------|-------|-------|-------|
| * | 1 | 2 | 3 | 4 | 5 | 6 | 7 | |
| + | * | * | * | * | * | * | * | |
| + | * 1 * | 31.36 | 41.37 | 41.93 | 41.94 | 42.13 | 42.68 | 44.97 |
| + | * 2 * | 0.00 | 2.56 | 3.12 | 3.13 | 3.32 | 3.87 | 6.16 |
| + | * 3 * | 0.00 | 0.71 | 1.26 | 1.27 | 1.46 | 2.01 | 4.30 |
| + | * 4 * | 0.00 | 0.00 | 0.13 | 0.14 | 0.33 | 0.88 | 3.17 |
| + | * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.18 | 0.73 | 3.02 |
| + | * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.55 | 2.84 |
| + | * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.09 |
| + | * * | * | * | * | * | * | * | * |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 3/30/2016 10:31 PAGE 17
UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
TIME SLICE 5 OF 6

TIME SLICE FREEWAY PERFORMANCE TABLE

Table with columns: SUB SEC, NO. LNS, SSEC LENGTH, O-D DATA ORG DES, DEMANDS SSEC, ADJUSTED VOLUMES ORG DES SSEC, SSEC CAP, WEAVE EFF, CONGEST LENGTH, STORAGE RATE, V/C RATIO, SPEED MPH, DENSITY VPMP, LOS LEVEL, FUEL MPG, EMISSIONS GS/VM.

TOTAL 137309. = 26.0 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 35. 40.9 18.0 15.2

CURRENT TIME SLICE

CUMULATIVE VALUES

Summary statistics: FREeway TRAVEL TIME = 1418. VEH-HRS, FREeway MERGE DELAY = 0. VEH-HRS, ON-RAMP DELAY = 0. VEH-HRS, OFF-RAMP DELAY = 0. VEH-HRS, TOTAL SYSTEM TRAVEL TIME = 1418. VEH-HRS, TOTAL TRAVEL DISTANCE = 48943. VEH-MI., AVERAGE SYSTEM SPEED = 35. MPH, AVERAGE DENSITY = 41. VPMP, TOTAL FUEL = 2722. GALLONS, TOTAL EMISSIONS = 745. KI LOGRAMS.

1 INSTITUTE OF TRANSPORTATION STUDIES UNIVERSITY OF CALIFORNIA, BERKELEY FREQ12PE REL 3.01 3/30/2016 10:31 PAGE 18 SIMULATION AFTER CONTROL, NO DIVERSION TIME SLICE 5 OF 6

Table showing delay and speed data: ***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 ***** SUBJECTI ON DELAY SUBJECTI ON DELAY SUBJECTI ON DELAY SUBJECTI ON DELAY SUBJECTI ON DELAY

1 INSTITUTE OF TRANSPORTATION STUDIES UNIVERSITY OF CALIFORNIA, BERKELEY FREQ12PE REL 3.01 3/30/2016 10:31 PAGE 19 SIMULATION AFTER CONTROL, NO DIVERSION TIME SLICE 6 OF 6

FREeway TRAVEL TIME (MINUTES)

Table with columns: ORIGINS DOWN, DESTINATIONS ACROSS. Rows 1-6 showing travel times across 7 destinations.

SR-237_WB_PM_NP_2040_PE
 * 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.09

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| SUB | NO. | SSEC | O-D | DATA | DEMANDS | ADJUSTED | VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI | |
|-----|-----|--------|--------|-------|---------|----------|---------|-------|-------|---------|---------|-----------|-------|---------|-------|------|-------|------|
| SEC | LNS | LENGTH | ORG | DES | SSEC | ORG | DES | SSEC | EFF | LENGTH | RATE | RATIO | MPH | VPMP | LEVEL | MPG | SS/VM | |
| * | 1 | 3 | 500. | 4030. | 0. | 4030. | 4030. | 0. | 4030. | 6000. | 0. | 0. | .67 | 65. | 20.7 | C | 19.0 | 14.1 |
| * | 2 | 3 | 99999. | 0. | 645. | 4030. | 0. | 645. | 4021. | 6000. | 0. | * 13919. | .67 | 36. | 37.0 | F | 17.7 | 15.3 |
| * | 3 | 2 | 11000. | 0. | 0. | 3385. | 0. | 0. | 3376. | 4000. | 0. | ** 11000. | .84 | 17. | 100.7 | F | 16.8 | 17.9 |
| * | 4 | 2 | 1500. | 64. | 0. | 3449. | 64. | 0. | 3440. | 3995. | 0. | ** 1500. | .86 | 18. | 96.8 | F | 17.2 | 17.4 |
| * | 5 | 2 | 1400. | 0. | 0. | 3449. | 0. | 0. | 3440. | 4000. | 0. | ** 1400. | .86 | 18. | 97.2 | F | 17.2 | 17.4 |
| * | 6 | 2 | 1500. | 528. | 0. | 3977. | 528. | 0. | 3968. | 3968. | 0. | 0. | 1.00 | 52. | 38.5 | E | 23.6 | 11.1 |
| * | 7 | 2 | 1300. | 0. | 0. | 3977. | 0. | 0. | 3968. | 4000. | 0. | 0. | .99 | 52. | 38.0 | E | 23.5 | 11.2 |
| * | 8 | 3 | 500. | 0. | 869. | 3977. | 0. | 867. | 3968. | 5130. | 0. | 0. | .77 | 62. | 21.3 | C | 20.3 | 13.0 |
| * | 9 | 2 | 2300. | 0. | 0. | 3108. | 0. | 0. | 3101. | 4000. | 0. | 0. | .78 | 61. | 25.2 | C | 20.6 | 12.8 |
| * | 10 | 3 | 250. | 371. | 0. | 3479. | 371. | 0. | 3472. | 4723. | 0. | 0. | .71 | 62. | 18.7 | C | 20.3 | 13.0 |
| * | 11 | 3 | 200. | 0. | 0. | 3479. | 0. | 0. | 3472. | 4900. | 0. | 0. | .71 | 62. | 18.7 | C | 20.3 | 13.0 |
| * | 12 | 3 | 250. | 0. | 1243. | 3479. | 0. | 1241. | 3472. | 4723. | 0. | 0. | .74 | 62. | 18.7 | C | 20.3 | 13.0 |
| * | 13 | 2 | 50. | 0. | 350. | 2236. | 0. | 349. | 2231. | 3950. | 0. | 0. | .56 | 62. | 18.0 | B | 20.3 | 13.0 |
| * | 14 | 2 | 50. | 0. | 0. | 1886. | 0. | 0. | 1882. | 2470. | 0. | 0. | .76 | 62. | 15.2 | B | 20.3 | 13.0 |
| * | 15 | 2 | 1000. | 347. | 0. | 2233. | 347. | 0. | 2229. | 3947. | 0. | 0. | .56 | 62. | 18.0 | B | 20.3 | 13.0 |
| * | 16 | 2 | 10. | 0. | 0. | 2233. | 0. | 0. | 2229. | 4000. | 0. | 0. | .56 | 62. | 18.0 | B | 20.3 | 13.0 |
| * | 17 | 2 | 1500. | 771. | 0. | 3004. | 771. | 0. | 3000. | 3882. | 0. | 0. | .77 | 62. | 24.2 | C | 20.3 | 13.0 |
| * | 18 | 2 | 1500. | 0. | 561. | 3004. | 0. | 560. | 3000. | 3951. | 0. | 0. | .76 | 62. | 24.2 | C | 20.3 | 13.0 |
| * | 19 | 2 | 12000. | 0. | 0. | 2443. | 0. | 0. | 2440. | 4000. | 0. | 0. | .61 | 62. | 19.7 | C | 20.3 | 13.0 |
| * | 20 | 3 | 500. | 465. | 2908. | 2908. | 465. | 2905. | 2905. | 6000. | 0. | 0. | .48 | 65. | 14.9 | B | 19.0 | 14.1 |

 * TOTAL 137309. = 26.0 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 34. 40.9 18.0 15.2 *

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 1420. VEH-HRS | 1590. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1420. VEH-HRS | 1590. PASS-HRS |
| TOTAL TRAV DISTANCE = | 48943. VEH-MI. | 55152. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 34. MPH. | 41. MPH. |
| AVERAGE DENSITY = | 41. VPMP | 35. VPMP |
| TOTAL FUEL = | 2723. GALLONS | 16746. GALLONS |
| TOTAL EMISSIONS = | 746. KI LOGRAMS | 4539. KI LOGRAMS |

***** MAINTENANCE DELAY (VEH-HRS) ***** DESIGN SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|--------|------------|--------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 465.11 | 3 | 155.59 | 4 | 19.99 | 5 | 18.75 |
| 6 | 2.26 | 7 | 1.84 | 8 | 0.14 | 9 | 0.61 | 10 | 0.06 |
| 11 | 0.05 | 12 | 0.06 | 13 | 0.01 | 14 | 0.01 | 15 | 0.16 |
| 16 | 0.00 | 17 | 0.32 | 18 | 0.32 | 19 | 2.06 | 20 | 0.00 |

***** TOTAL DELAY = 667.3 VEH-HRS ***** AVERAGE DELAY = 10.53 MIN/VEH *****

```

FFFFFFFFF RRRRRRRR EEEEEEEEEE QQQQQQQ 1111 222222 PPPPPPPPP LLL
FFFFFFFFF RRRRRRRRRR EEEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPPP LLL
FFF RRR RRR EEE QQQQQ QQQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 PPP PPP LLL
FFFFFFFFF RRRRRRRRRR EEEEEEEE QQQQ QQQQ 1111 222 PPPPPPPPP LLL
FFFFFFFFF RRRRRRRRRR EEEEEEEE QQQQ QQQQ 1111 2222 PPPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQ QQQQ 1111 2222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEEE Q*1988*Q QQQ 11111111 2222222222 PPP LLLLLLLLLL
    
```

FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 3 AND 19 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 2.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 30
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

```

*****
**
**          FREeway AND ARTERIAL DESIGN FEATURES          **
**
*****
** SUB NO.   SSEC  SSEC  DESIG N  ORG  TRK  SSEC PCT  PCT DES  SPECIAL  FF. SPD.  CAP.  ART  GRADE  SUBSECTI ON LOCATI ON
** SEC LNS   CAP   LENGTH SPEED  DES  FAC  GRAD TRK  TRUCKS  RAMP    ALT. RTE  ALT. RTE TYPE ALT. RTE
**
** 1
** 2
** 3 1 1500. 11000. 62 0 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 HOV Dummy
** 4 1 1500. 1500. 62 0 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Lawrence On-ramp
** 5 1 1500. 1400. 62 0 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Lawrence to Crossman
** 6 1 1500. 1500. 62 0 0.95 0.0 0 100 YES 0.0 0. GOOD 0.0 Crossman On-Ramp
** 7 1 1500. 1300. 62 0 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Crossman / Mathilda
** 8 1 1500. 500. 62 D 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Mathilda Off-Ramp
** 9 1 1500. 2300. 62 0 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Mathilda / Mathilda
** 10 1 1500. 250. 62 0 0.95 0.0 0 100 YES 0.0 0. GOOD 0.0 Mathilda On-ramp
** 11 1 1500. 200. 62 0 0.95 0.0 0 100 YES 0.0 0. GOOD 0.0 Mathilda to US-101
** 12 1 1500. 250. 62 D 0.95 0.0 0 100 YES 0.0 0. GOOD 0.0 US-101 Off-Ramp
** 13 1 1500. 50. 62 D 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Bottleneck by-pass
** 14 1 1500. 50. 62 0 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Bottleneck
** 15 1 1500. 1000. 62 OD 0.95 0.0 0 100 YES 0.0 0. GOOD 0.0 US 101 / US 101
** 16 1 1500. 10. 62 0 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Dummy end of travel time
** 17 1 1500. 1500. 62 0 0.95 0.0 0 100 YES 0.0 0. GOOD 0.0 US 101 NB On-Ramp
** 18 1 1500. 1500. 62 D 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 Maude Off-ramp
**
    
```

```

**
** 19 1 1500. 12000. 62 D 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 HOV Dummy
**
** 20
**
*****

```

```

*****
**
** FREEWAY TRAVEL TIME (MINUTES)
**
*****

```

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|-------|-----------------------|------|------|------|------|------|------|------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| + | * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 2 * | 0.00 | 3.15 | 3.70 | 3.71 | 3.90 | 4.46 | 6.66 | 0.00 |
| + | * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.44 | 4.64 | 0.00 |
| + | * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 4.11 | 0.00 |
| + | * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.08 | 0.00 |
| + | * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.93 | 0.00 |
| + | * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.75 | 0.00 |
| + | * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | | |
|-----------|--------|------------|-----------|------------|--------|---------|-----------|-----------|---------|-----------------|-----------|----------------|--------|-------------|------|---|------|------|
| * SEC | * LNS | * LENGTH | * ORG DES | * ORG DES | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | | | |
| * 1 | | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | | |
| * 3 | 1 | 11000. | 720. | 0. | 720. | 720. | 0. | 720. | 1500. | 0. | 0. | 0. | .48 | 62. | 11.6 | B | 21.6 | 12.8 |
| * 4 | 1 | 1500. | 4. | 0. | 724. | 4. | 0. | 724. | 1500. | 0. | 0. | 0. | .48 | 62. | 11.7 | B | 21.6 | 12.8 |
| * 5 | 1 | 1400. | 0. | 0. | 724. | 0. | 0. | 724. | 1500. | 0. | 0. | 0. | .48 | 62. | 11.7 | B | 21.6 | 12.8 |
| * 6 | 1 | 1500. | 44. | 0. | 769. | 44. | 0. | 769. | 1500. | 0. | 0. | 0. | .51 | 62. | 12.4 | B | 21.6 | 12.8 |
| * 7 | 1 | 1300. | 0. | 0. | 769. | 0. | 0. | 769. | 1500. | 0. | 0. | 0. | .51 | 62. | 12.4 | B | 21.6 | 12.8 |
| * 8 | 1 | 500. | 0. | 163. | 769. | 0. | 163. | 769. | 1500. | 0. | 0. | 0. | .51 | 62. | 12.4 | B | 21.6 | 12.8 |
| * 9 | 1 | 2300. | 0. | 0. | 605. | 0. | 0. | 605. | 1500. | 0. | 0. | 0. | .40 | 62. | 9.8 | A | 21.6 | 12.8 |
| * 10 | 1 | 250. | 37. | 0. | 642. | 37. | 0. | 642. | 1500. | 0. | 0. | 0. | .43 | 62. | 10.4 | A | 21.6 | 12.8 |
| * 11 | 1 | 200. | 0. | 0. | 642. | 0. | 0. | 642. | 1500. | 0. | 0. | 0. | .43 | 62. | 10.4 | A | 21.6 | 12.8 |
| * 12 | 1 | 250. | 0. | 239. | 642. | 0. | 239. | 642. | 1500. | 0. | 0. | 0. | .43 | 62. | 10.4 | A | 21.6 | 12.8 |
| * 13 | 1 | 50. | 0. | 6. | 404. | 0. | 6. | 404. | 1500. | 0. | 0. | 0. | .27 | 62. | 6.5 | A | 21.6 | 12.8 |
| * 14 | 1 | 50. | 0. | 0. | 398. | 0. | 0. | 398. | 1500. | 0. | 0. | 0. | .27 | 62. | 6.4 | A | 21.6 | 12.8 |
| * 15 | 1 | 1000. | 7. | 0. | 405. | 7. | 0. | 405. | 1500. | 0. | 0. | 0. | .27 | 62. | 6.5 | A | 21.6 | 12.8 |
| * 16 | 1 | 10. | 0. | 0. | 405. | 0. | 0. | 405. | 1500. | 0. | 0. | 0. | .27 | 62. | 6.5 | A | 21.6 | 12.8 |
| * 17 | 1 | 1500. | 123. | 0. | 528. | 123. | 0. | 528. | 1500. | 0. | 0. | 0. | .35 | 62. | 8.5 | A | 21.6 | 12.8 |
| * 18 | 1 | 1500. | 0. | 39. | 528. | 0. | 39. | 528. | 1500. | 0. | 0. | 0. | .35 | 62. | 8.5 | A | 21.6 | 12.8 |
| * 19 | 1 | 12000. | 0. | 489. | 489. | 0. | 489. | 489. | 1500. | 0. | 0. | 0. | .33 | 62. | 7.9 | A | 21.6 | 12.8 |
| * 20 | | | | | | | | | | | | | | | | | | |
| * TOTAL | 36310. | = | 6.9 | MI LBS | | | | | | MAX(V/C) = 0.51 | | LOWEST LOS = B | | AVG = 62. | 9.9 | | 21.6 | 12.8 |

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|-----------------------------|--------------------|---------|-------------------|----------|
| FREWAY TRAVEL TIME = | 34. | VEH-HRS | 68. | PASS-HRS |
| FREWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 34. | VEH-HRS | 68. | PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 2112. | VEH-MI. | 4223. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. | MPH. | 62. | MPH. |
| AVERAGE DENSITY = | 10. | VPMP | 10. | VPMP |
| TOTAL FUEL = | 98. | GALLONS | 98. | GALLONS |

TOTAL EMISSIONS = 27. KILOGRAMS

SR-237_WB_PM_NP_2040_PL 27. KILOGRAMS

Table with columns: SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY. Includes summary rows for MAINTENANCE DELAY and TOTAL DELAY.

**
** FREEWAY TRAVEL TIME (MINUTES) **
**

Table with columns: ORIGINS DOWN, DESTINATIONS ACROSS (1-8). Shows travel times between various origins and destinations.

TIME SLICE FREEWAY PERFORMANCE TABLE

Table with columns: SUB SEC, NO. LNS, SSEC LENGTH, O-D DATA ORG, DEMANDS DES, SSEC, ADJUSTED VOLUMES ORG, DES, SSEC, SSEC CAP, WEAFF EFF, CONGEST LENGTH, STORAGE RATE, V/C RATIO, SPEED MPH, DENSITY VPMP, LOS LEVEL, FUEL MPG, EMISSIONS GS/VM. Includes a summary row for TOTAL.

SR-237_WB_PM_NP_2040_PL

| | | | | | | | | | | | | | | | | | | | |
|-------|-------|--------|--------|------|--------|------|------|------|------|-------|----|----|-----------------|----------------|-----------|------|------|------|---|
| * | 16 | 1 | 10. | 0. | 0. | 453. | 0. | 0. | 453. | 1500. | 0. | 0. | .30 | 62. | 7.3 | A | 21.6 | 12.8 | * |
| * | 17 | 1 | 1500. | 123. | 0. | 576. | 123. | 0. | 576. | 1500. | 0. | 0. | .38 | 62. | 9.3 | A | 21.6 | 12.8 | * |
| * | 18 | 1 | 1500. | 0. | 66. | 576. | 0. | 66. | 576. | 1500. | 0. | 0. | .38 | 62. | 9.3 | A | 21.6 | 12.8 | * |
| * | 19 | 1 | 12000. | 0. | 510. | 510. | 0. | 510. | 510. | 1500. | 0. | 0. | .34 | 62. | 8.2 | A | 21.6 | 12.8 | * |
| * | 20 | | | | | | | | | | | | | | | | | | * |
| ***** | | | | | | | | | | | | | | | | | | | |
| * | TOTAL | 36310. | = | 6.9 | MI LES | | | | | | | | MAX(V/C) = 0.53 | LOWEST LOS = B | AVG = 62. | 10.3 | 21.6 | 12.8 | * |
| ***** | | | | | | | | | | | | | | | | | | | |

| CURRENT TIME SLICE | | | CUMULATIVE VALUES | | | | | |
|-----------------------------|-------|------------|-------------------|----------|-------|------------|--------|----------|
| FREEWAY TRAVEL TIME = | 35. | VEH-HRS | 71. | PASS-HRS | 104. | VEH-HRS | 207. | PASS-HRS |
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 35. | VEH-HRS | 71. | PASS-HRS | 104. | VEH-HRS | 207. | PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 2194. | VEH-MI. | 4388. | PASS-MI. | 6417. | VEH-MI. | 12834. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. | MPH. | | | 62. | MPH. | | |
| AVERAGE DENSITY = | 10. | VPMP/L | | | 10. | VPMP/L | | |
| TOTAL FUEL = | 102. | GALLONS | | | 298. | GALLONS | | |
| TOTAL EMISSIONS = | 28. | KI LOGRAMS | | | 82. | KI LOGRAMS | | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.57 | 4 | 0.08 | 5 | 0.07 |
| 6 | 0.08 | 7 | 0.07 | 8 | 0.03 | 9 | 0.10 | 10 | 0.01 |
| 11 | 0.01 | 12 | 0.01 | 13 | 0.00 | 14 | 0.00 | 15 | 0.03 |
| 16 | 0.00 | 17 | 0.06 | 18 | 0.06 | 19 | 0.43 | 20 | 0.00 |

***** TOTAL DELAY = 1.6 VEH-HRS ***** AVERAGE DELAY = 0.15 MIN/VEH *****

 ** FREEWAY TRAVEL TIME (MINUTES) **
 ** ** **

| * ORIGINS DOWN | * DESTINATIONS ACROSS * | | | | | | | |
|----------------|-------------------------|------|------|------|------|------|------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 3.15 | 3.70 | 3.71 | 3.90 | 4.46 | 6.66 | 0.00 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.44 | 4.64 | 0.00 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 4.11 | 0.00 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.08 | 0.00 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.93 | 0.00 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.75 | 0.00 |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS | | | |
|-----------|------|----------|---------|------------------|------|-------|---------|---------|-------|-------|---------|--------|------|--------|---|------|------|
| * SEC | LNS | LENGTH | ORG | DES | SSEC | CAP. | EFF | LENGTH | RATE | RATIO | MPH | VPMP/L | MPG | GS/VM | | | |
| * 1 | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | |
| * 3 | 1 | 11000. | 741. | 0. | 741. | 741. | 0. | 741. | 1500. | 0. | 0. | .49 | 62. | 11.9 | B | 21.6 | 12.8 |

SR-237_WB_PM_NP_2040_PL

Table with 14 columns: Lane, Volume, Delay, etc. Rows 4-20. Summary row: TOTAL 36310 = 6.9 MI LES, MAX(V/C) = 0.53, LOWEST LOS = B, AVG = 62, 10.3, 21.6, 12.8

Summary statistics table: FREeway TRAVEL TIME = 35. VEH-HRS, FREeway MERGE DELAY = 0. VEH-HRS, ON-RAMP MRG/CAP DELAY = 0. VEH-HRS, OFF-RAMP DELAY = 0. VEH-HRS, TOTAL SYSTEM TRAVEL TIME = 35. VEH-HRS, TOTAL FRWAY TRAV DISTANCE = 2194. VEH-MI, AVERAGE SYSTEM SPEED = 62. MPH, AVERAGE DENSITY = 10. VPMP, TOTAL FUEL = 102. GALLONS, TOTAL EMISSIONS = 28. KILOGRAMS

Table with 10 columns: SUBSECTION, DELAY. Summary row: TOTAL DELAY = 1.6 VEH-HRS, AVERAGE DELAY = 0.15 MIN/VEH

FREeway TRAVEL TIME (MINUTES)

Table with 9 columns: ORIGINS DOWN, DESTINATIONS ACROSS (1-8). Rows 1-8 showing travel times between sections.

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB SEC | NO. LNS | SSEC LENGTH | O-D ORG | DATA DES | DEMANDS SSEC | ADJUSTED ORG | VOLUMES DES | SSEC SSEC | WEAVE CAP | CONGEST EFF | STORAGE LENGTH | V/C RATE | SPEED MPH | DENSITY VPMP | LOS LEVEL | FUEL MPG | EMI SS GS/VM | |
|---------|---------|-------------|---------|----------|--------------|--------------|-------------|-----------|-----------------|----------------|----------------|----------|-----------|--------------|-----------|----------|--------------|------|
| 1 | | | | | | | | | | | | | | | | | | |
| 2 | | | | | | | | | | | | | | | | | | |
| 3 | 1 | 11000. | 645. | 0. | 645. | 645. | 0. | 645. | 1500. | 0. | 0. | 0. | .43 | 62. | 10.4 | A | 21.6 | 12.8 |
| 4 | 1 | 1500. | 5. | 0. | 650. | 5. | 0. | 650. | 1500. | 0. | 0. | 0. | .43 | 62. | 10.5 | A | 21.6 | 12.8 |
| 5 | 1 | 1400. | 0. | 0. | 650. | 0. | 0. | 650. | 1500. | 0. | 0. | 0. | .43 | 62. | 10.5 | A | 21.6 | 12.8 |
| 6 | 1 | 1500. | 32. | 0. | 682. | 32. | 0. | 682. | 1500. | 0. | 0. | 0. | .45 | 62. | 11.0 | A | 21.6 | 12.8 |
| 7 | 1 | 1300. | 0. | 0. | 682. | 0. | 0. | 682. | 1500. | 0. | 0. | 0. | .45 | 62. | 11.0 | A | 21.6 | 12.8 |
| 8 | 1 | 500. | 0. | 140. | 682. | 0. | 140. | 682. | 1500. | 0. | 0. | 0. | .45 | 62. | 11.0 | A | 21.6 | 12.8 |
| 9 | 1 | 2300. | 0. | 0. | 542. | 0. | 0. | 542. | 1500. | 0. | 0. | 0. | .36 | 62. | 8.7 | A | 21.6 | 12.8 |
| 10 | 1 | 250. | 29. | 0. | 571. | 29. | 0. | 571. | 1500. | 0. | 0. | 0. | .38 | 62. | 9.2 | A | 21.6 | 12.8 |
| 11 | 1 | 200. | 0. | 0. | 571. | 0. | 0. | 571. | 1500. | 0. | 0. | 0. | .38 | 62. | 9.2 | A | 21.6 | 12.8 |
| 12 | 1 | 250. | 0. | 177. | 571. | 0. | 177. | 571. | 1500. | 0. | 0. | 0. | .38 | 62. | 9.2 | A | 21.6 | 12.8 |
| 13 | 1 | 50. | 0. | 50. | 394. | 0. | 50. | 394. | 1500. | 0. | 0. | 0. | .26 | 62. | 6.4 | A | 21.6 | 12.8 |
| 14 | 1 | 50. | 0. | 0. | 344. | 0. | 0. | 344. | 1500. | 0. | 0. | 0. | .23 | 62. | 5.5 | A | 21.6 | 12.8 |
| 15 | 1 | 1000. | 53. | 0. | 397. | 53. | 0. | 397. | 1500. | 0. | 0. | 0. | .26 | 62. | 6.4 | A | 21.6 | 12.8 |
| 16 | 1 | 10. | 0. | 0. | 397. | 0. | 0. | 397. | 1500. | 0. | 0. | 0. | .26 | 62. | 6.4 | A | 21.6 | 12.8 |
| 17 | 1 | 1500. | 118. | 0. | 515. | 118. | 0. | 515. | 1500. | 0. | 0. | 0. | .34 | 62. | 8.3 | A | 21.6 | 12.8 |
| 18 | 1 | 1500. | 0. | 49. | 515. | 0. | 49. | 515. | 1500. | 0. | 0. | 0. | .34 | 62. | 8.3 | A | 21.6 | 12.8 |
| 19 | 1 | 12000. | 0. | 465. | 465. | 0. | 465. | 465. | 1500. | 0. | 0. | 0. | .31 | 62. | 7.5 | A | 21.6 | 12.8 |
| 20 | | | | | | | | | | | | | | | | | | |
| TOTAL | 36310. | = | 6.9 | MI | LES | | | | MAX(V/C) = 0.45 | LOWEST LOS = A | AVG = 62. | 9.1 | 21.6 | 12.8 | | | | |

| | | |
|-----------------------------|--------------------|-------------------|
| | CURRENT TIME SLICE | CUMULATIVE VALUES |
| FREWAY TRAVEL TIME = | 31. VEH-HRS | 62. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 31. VEH-HRS | 62. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 1935. VEH-MI. | 3871. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 62. MPH. |
| AVERAGE DENSITY = | 9. VPMP | 10. VPMP |
| TOTAL FUEL = | 90. GALLONS | 489. GALLONS |
| TOTAL EMISSIONS = | 25. KILOGRAMS | 135. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.50 | 4 | 0.07 | 5 | 0.06 |
| 6 | 0.07 | 7 | 0.06 | 8 | 0.02 | 9 | 0.09 | 10 | 0.01 |
| 11 | 0.01 | 12 | 0.01 | 13 | 0.00 | 14 | 0.00 | 15 | 0.03 |
| 16 | 0.00 | 17 | 0.05 | 18 | 0.05 | 19 | 0.39 | 20 | 0.00 |

***** TOTAL DELAY = 1.4 VEH-HRS ***** AVERAGE DELAY = 0.15 MIN/VEH *****

 ** FREWAY TRAVEL TIME (MINUTES) **

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | | |
|--------------|---------------------|------|------|------|------|------|------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 3.15 | 3.70 | 3.71 | 3.90 | 4.46 | 6.66 | 0.00 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.44 | 4.64 | 0.00 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 4.11 | 0.00 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.08 | 0.00 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.93 | 0.00 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.75 | 0.00 |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

* * *

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS |
|---------|--------|----------|--------------|------------------|-------|-------|-----------------|---------|----------------|-----------|---------|-------|------|--------|
| SEC | LNS | LENGTH | ORG DES SSEC | ORG DES SSEC | CAP | EFF | LENGTH | RATE | RATIO | MPH | VPMPL | LEVEL | MPG | GS/VM |
| 1 | | | | | | | | | | | | | | |
| 2 | | | | | | | | | | | | | | |
| 3 | 1 | 11000. | 645. 0. 645. | 645. 0. 645. | 1500. | 0. | 0. | 0. | .43 | 62. | 10.4 | A | 21.6 | 12.8 |
| 4 | 1 | 1500. | 5. 0. 650. | 5. 0. 650. | 1500. | 0. | 0. | 0. | .43 | 62. | 10.5 | A | 21.6 | 12.8 |
| 5 | 1 | 1400. | 0. 0. 650. | 0. 0. 650. | 1500. | 0. | 0. | 0. | .43 | 62. | 10.5 | A | 21.6 | 12.8 |
| 6 | 1 | 1500. | 32. 0. 682. | 32. 0. 682. | 1500. | 0. | 0. | 0. | .45 | 62. | 11.0 | A | 21.6 | 12.8 |
| 7 | 1 | 1300. | 0. 0. 682. | 0. 0. 682. | 1500. | 0. | 0. | 0. | .45 | 62. | 11.0 | A | 21.6 | 12.8 |
| 8 | 1 | 500. | 0. 140. 682. | 0. 140. 682. | 1500. | 0. | 0. | 0. | .45 | 62. | 11.0 | A | 21.6 | 12.8 |
| 9 | 1 | 2300. | 0. 0. 542. | 0. 0. 542. | 1500. | 0. | 0. | 0. | .36 | 62. | 8.7 | A | 21.6 | 12.8 |
| 10 | 1 | 250. | 29. 0. 571. | 29. 0. 571. | 1500. | 0. | 0. | 0. | .38 | 62. | 9.2 | A | 21.6 | 12.8 |
| 11 | 1 | 200. | 0. 0. 571. | 0. 0. 571. | 1500. | 0. | 0. | 0. | .38 | 62. | 9.2 | A | 21.6 | 12.8 |
| 12 | 1 | 250. | 0. 177. 571. | 0. 177. 571. | 1500. | 0. | 0. | 0. | .38 | 62. | 9.2 | A | 21.6 | 12.8 |
| 13 | 1 | 50. | 0. 50. 394. | 0. 50. 394. | 1500. | 0. | 0. | 0. | .26 | 62. | 6.4 | A | 21.6 | 12.8 |
| 14 | 1 | 50. | 0. 0. 344. | 0. 0. 344. | 1500. | 0. | 0. | 0. | .23 | 62. | 5.5 | A | 21.6 | 12.8 |
| 15 | 1 | 1000. | 53. 0. 397. | 53. 0. 397. | 1500. | 0. | 0. | 0. | .26 | 62. | 6.4 | A | 21.6 | 12.8 |
| 16 | 1 | 10. | 0. 0. 397. | 0. 0. 397. | 1500. | 0. | 0. | 0. | .26 | 62. | 6.4 | A | 21.6 | 12.8 |
| 17 | 1 | 1500. | 118. 0. 515. | 118. 0. 515. | 1500. | 0. | 0. | 0. | .34 | 62. | 8.3 | A | 21.6 | 12.8 |
| 18 | 1 | 1500. | 0. 49. 515. | 0. 49. 515. | 1500. | 0. | 0. | 0. | .34 | 62. | 8.3 | A | 21.6 | 12.8 |
| 19 | 1 | 12000. | 0. 465. 465. | 0. 465. 465. | 1500. | 0. | 0. | 0. | .31 | 62. | 7.5 | A | 21.6 | 12.8 |
| 20 | | | | | | | | | | | | | | |
| TOTAL | 36310. | = | 6.9 MILES | | | | MAX(V/C) = 0.45 | | LOWEST LOS = A | AVG = 62. | 9.1 | | 21.6 | 12.8 |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 31. VEH-HRS | 62. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 31. VEH-HRS | 62. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 1935. VEH-MI. | 3871. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 62. MPH. |
| AVERAGE DENSITY = | 9. VPMPL | 10. VPMPL |
| TOTAL FUEL = | 90. GALLONS | 579. GALLONS |
| TOTAL EMISSIONS = | 25. KILOGRAMS | 159. KILOGRAMS |

***** MAINTENANCE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.50 | 4 | 0.07 | 5 | 0.06 |
| 6 | 0.07 | 7 | 0.06 | 8 | 0.02 | 9 | 0.09 | 10 | 0.01 |
| 11 | 0.01 | 12 | 0.01 | 13 | 0.00 | 14 | 0.00 | 15 | 0.03 |
| 16 | 0.00 | 17 | 0.05 | 18 | 0.05 | 19 | 0.39 | 20 | 0.00 |

***** TOTAL DELAY = 1.4 VEH-HRS ***** AVERAGE DELAY = 0.15 MIN/VEH *****

```

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ      1111      222222  PPPPPPPP EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111  222 222  PPPPPPPP EEEEEEEEE
FFF      RRR      RRR EEE      QQQQQ QQQQQ  1111  222 222  PPP  PPP  EEE
FFF      RRR      RRR EEE      QQQQ  QQQQ   1111  222  PPP  PPP  EEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ  QQQQ   1111  222  PPPPPPPP EEEEEEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ  QQQQ   1111  222  PPPPPPPP EEEEEEE
FFF      RRR RRR  EEE      QQQQ  QQQ QQQ  1111  2222  PPP  EEE
FFF      RRR RRR  EEE      Q*UC*  QQQQQ  1111  222  PPP  EEE
FFF      RRR RRR  EEEEEEEEE Q*REGENTS*Q  1111  222  PPP  EEEEEEEEE
FFF      RRR RRR  EEEEEEEEE Q*1999*Q QQQ 1111111 2222222222 PPP  EEEEEEEEE
    
```

FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 2.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 30
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREWAY AND ARTERIAL DESIGN FEATURES

| ** SUB NO. | ** SSEC | ** SSEC | ** DESIG N | ** ORG | ** TRK | ** SSEC | ** PCT | ** PCT | ** DES | ** SPECIAL | ** FF. SPD. | ** CAP. | ** ART | ** GRADE | ** SUBSECTI ON | ** LOCATI ON |
|------------|---------|---------|------------|----------|--------|---------|--------|-----------|---------|-------------|-------------|---------|-------------|-------------|--------------------------|--------------|
| ** SEC | ** LNS | ** CAP | ** LENGTH | ** SPEED | ** DES | ** GRAD | ** TRK | ** TRUCKS | ** RAMP | ** ALT. RTE | ** ALT. RTE | ** TYPE | ** ALT. RTE | ** ALT. RTE | ** LOCATION | ** LOCATION |
| ** 1 | 3 | 6000. | 500. | 65 | 0 | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Seed | ** |
| ** 2 | 3 | 6000. | 99999. | 65 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | ** |
| ** 3 | 2 | 4000. | 11000. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | ** |
| ** 4 | 2 | 4000. | 1500. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence On-ramp | ** |
| ** 5 | 2 | 4000. | 1400. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence to Crossman | ** |
| ** 6 | 2 | 4000. | 1500. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Crossman On-Ramp | ** |
| ** 7 | 2 | 4000. | 1300. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Crossman / Mathilda | ** |
| ** 8 | 3 | 5270. | 500. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-Ramp | ** |
| ** 9 | 2 | 4000. | 2300. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | ** |
| ** 10 | 3 | 4860. | 250. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda On-ramp | ** |
| ** 11 | 3 | 4860. | 200. | 62 | | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda to US-101 | ** |
| ** 12 | 3 | 4860. | 250. | 62 | D | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US-101 Off-Ramp | ** |
| ** 13 | 2 | 4000. | 50. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bottleneck by-pass | ** |
| ** 14 | 2 | 2470. | 50. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bottleneck | ** |
| ** 15 | 2 | 4000. | 1000. | 62 | OD | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US 101 / US 101 | ** |
| ** 16 | 2 | 4000. | 10. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Dummy end of travel time | ** |
| ** 17 | 2 | 4000. | 1500. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US 101 NB On-Ramp | ** |
| ** 18 | 2 | 4000. | 1500. | 62 | D | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Maude Off-ramp | ** |
| ** 19 | 2 | 4000. | 12000. | 62 | | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | ** |
| ** 20 | 3 | 6000. | 500. | 65 | OD | 0.95 | 0.0 | 5 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End of Network | ** |

***** INPUT HAS BEEN COMPLETED *****

**
** FREeway TRAVEL TIME (MINUTES) **
**

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | |
|-----------|-------|-----------------------|-------|-------|-------|-------|-------|---|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 17.79 | 23.96 | 24.51 | 24.51 | 24.71 | 25.26 | 27.55 | |
| * 2 * | 0.00 | 2.60 | 3.15 | 3.16 | 3.36 | 3.91 | 6.19 | |
| * 3 * | 0.00 | 0.70 | 1.25 | 1.26 | 1.46 | 2.01 | 4.29 | |
| * 4 * | 0.00 | 0.00 | 0.13 | 0.14 | 0.33 | 0.88 | 3.17 | |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.18 | 0.73 | 3.02 | |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.55 | 2.84 | |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.09 | |

* TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|-----------|----------|------------|-----------|------------|-----------|--------|---------|-----------------|-----------|----------------|-----------|-----------|---------|--------|-------------|
| * SEC LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 1 3 | 500. | 4500. | 0. 4500. | 4500. | 0. 4500. | 6000. | 0. | 0. | 0. | .75 | 64. | 23.4 | C | 19.3 | 13.8 |
| * 2 3 | 99999. | 0. 720. | 4500. | 0. 720. | 4500. | 6000. | 0. | 0. | 0. | .75 | 64. | 23.4 | C | 19.3 | 13.8 |
| * 3 2 | 11000. | 0. 0. | 3780. | 0. 0. | 3214. | 4000. | 0. | * 7176. | 566. | .80 | 35. | 45.7 | F | 20.8 | 13.1 |
| * 4 2 | 1500. | 56. 0. | 3836. | 56. 0. | 3270. | 3996. | 0. | ** 1500. | 566. | .82 | 18. | 88.5 | F | 17.4 | 17.0 |
| * 5 2 | 1400. | 0. 0. | 3836. | 0. 0. | 3270. | 4000. | 0. | ** 1400. | 566. | .82 | 16. | 100.5 | F | 16.6 | 18.1 |
| * 6 2 | 1500. | 687. 0. | 4523. | 687. 0. | 3957. | 3957. | 0. | 0. | 0. | 1.00 | 52. | 38.4 | E | 23.6 | 11.1 |
| * 7 2 | 1300. | 0. 0. | 4523. | 0. 0. | 3957. | 4000. | 0. | 0. | 0. | .99 | 52. | 37.8 | E | 23.4 | 11.2 |
| * 8 3 | 500. | 0. 1038. | 4523. | 0. 909. | 3957. | 5107. | 0. | 0. | 0. | .77 | 62. | 21.3 | C | 20.3 | 13.0 |
| * 9 2 | 2300. | 0. 0. | 3485. | 0. 0. | 3048. | 4000. | 0. | 0. | 0. | .76 | 62. | 24.6 | C | 20.3 | 13.0 |
| * 10 3 | 250. | 433. 0. | 3918. | 433. 0. | 3481. | 4824. | 0. | 0. | 0. | .72 | 62. | 18.7 | C | 20.3 | 13.0 |
| * 11 3 | 200. | 0. 0. | 3918. | 0. 0. | 3481. | 4860. | 0. | 0. | 0. | .72 | 62. | 18.7 | C | 20.3 | 13.0 |
| * 12 3 | 250. | 0. 1753. | 3918. | 0. 1561. | 3481. | 4616. | 0. | 0. | 0. | .75 | 62. | 18.7 | C | 20.3 | 13.0 |
| * 13 2 | 50. | 0. 44. | 2165. | 0. 39. | 1919. | 3994. | 0. | 0. | 0. | .48 | 62. | 15.5 | B | 20.3 | 13.0 |
| * 14 2 | 50. | 0. 0. | 2121. | 0. 0. | 1880. | 2470. | 0. | 0. | 0. | .76 | 62. | 15.2 | B | 20.3 | 13.0 |
| * 15 2 | 1000. | 43. 0. | 2164. | 43. 0. | 1923. | 3993. | 0. | 0. | 0. | .48 | 62. | 15.5 | B | 20.3 | 13.0 |
| * 16 2 | 10. | 0. 0. | 2164. | 0. 0. | 1923. | 4000. | 0. | 0. | 0. | .48 | 62. | 15.5 | B | 20.3 | 13.0 |
| * 17 2 | 1500. | 749. 0. | 2913. | 749. 0. | 2672. | 3879. | 0. | 0. | 0. | .69 | 62. | 21.6 | C | 20.3 | 13.0 |
| * 18 2 | 1500. | 0. 403. | 2913. | 0. 372. | 2672. | 3960. | 0. | 0. | 0. | .67 | 62. | 21.6 | C | 20.3 | 13.0 |
| * 19 2 | 12000. | 0. 0. | 2510. | 0. 0. | 2300. | 4000. | 0. | 0. | 0. | .58 | 62. | 18.6 | C | 20.3 | 13.0 |
| * 20 3 | 500. | 478. 2988. | 2988. | 478. 2778. | 2778. | 6000. | 0. | 0. | 0. | .46 | 65. | 14.2 | B | 19.0 | 14.1 |
| * TOTAL | 137309. | = 26.0 | MILES | | | | | MAX(V/C) = 1.00 | | LOWEST LOS = F | AVG = 58. | 26.4 | | 19.5 | 13.7 |

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|----------------------------|--------------------|-----------------|-------------------|-----------------|
| FREWAY TRAVEL TIME = | 926. VEH-HRS | 1034. PASS-HRS | 926. VEH-HRS | 1034. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 926. VEH-HRS | 1034. PASS-HRS | 926. VEH-HRS | 1034. PASS-HRS |
| TOTAL TRAV DISTANCE = | 53382. VEH-MI. | 60307. PASS-MI. | 53382. VEH-MI. | 60307. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 58. MPH. | | 58. MPH. | |

AVERAGE DENSITY = 26. VP MPL
 TOTAL FUEL = 2733. GALLONS
 TOTAL EMISSIONS = 731. KI LOGRAMS

***** MAINTENANCE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|--|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.04 | 2 | 8.34 | 3 | 49.68 | 4 | 18.63 | 5 | 20.21 |
| 6 | 2.26 | 7 | 1.80 | 8 | 0.14 | 9 | 0.49 | 10 | 0.06 |
| 11 | 0.05 | 12 | 0.06 | 13 | 0.01 | 14 | 0.01 | 15 | 0.14 |
| 16 | 0.00 | 17 | 0.28 | 18 | 0.28 | 19 | 1.95 | 20 | 0.00 |
| ***** TOTAL DELAY = 104.4 VEH-HRS ***** AVERAGE DELAY = 1.90 MIN/VEH ***** | | | | | | | | | |

 ** FREeway TRAVEL TIME (MINUTES) **

| * ORIGINS DOWN | | * DESTINATIONS ACROSS | | | | | | |
|----------------|-------|-----------------------|-------|-------|-------|-------|-------|---|
| | | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 1 | 18.52 | 29.40 | 29.95 | 29.96 | 30.15 | 30.70 | 32.99 | |
| 2 | 0.00 | 2.85 | 3.40 | 3.41 | 3.60 | 4.15 | 6.44 | |
| 3 | 0.00 | 0.70 | 1.25 | 1.26 | 1.46 | 2.01 | 4.29 | |
| 4 | 0.00 | 0.00 | 0.13 | 0.14 | 0.33 | 0.88 | 3.17 | |
| 5 | 0.00 | 0.00 | 0.00 | 0.00 | 0.18 | 0.73 | 3.02 | |
| 6 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.55 | 2.84 | |
| 7 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.09 | |

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB SEC | NO. LNS | SSEC LENGTH | O-D DATA ORG DES | DEMANDS SSEC | ADJUSTED VOLUMES ORG DES SSEC | SSEC CAP. | WEAVE EFF | CONGEST LENGTH | STORAGE RATE | V/C RATIO | SPEED MPH | DENSITY VP MPL | LOS LEVEL | FUEL MPG | EMI SS GS/VM |
|---------|---------|-------------|------------------|--------------|-------------------------------|-------------|-----------|----------------|--------------|-----------|-----------|----------------|-----------|----------|--------------|
| 1 | 3 | 500. | 4500. | 0. 4500. | 4500. | 0. 4500. | 6000. | 0. 0. | 0. 0. | .75 | 64. | 23.4 | C | 19.3 | 13.8 |
| 2 | 3 | 99999. | 0. | 720. 4500. | 0. | 720. 3934. | 6000. | 0. * | 2585. | .66 | 62. | 21.3 | F | 19.2 | 13.9 |
| 3 | 2 | 11000. | 0. | 0. 3780. | 0. | 0. 3214. | 4000. | 0. ** | 11000. | .80 | 16. | 103.2 | F | 16.2 | 18.6 |
| 4 | 2 | 1500. | 56. | 0. 3836. | 56. | 0. 3270. | 3996. | 0. ** | 1500. | .82 | 15. | 106.1 | F | 16.2 | 18.7 |
| 5 | 2 | 1400. | 0. | 0. 3836. | 0. | 0. 3270. | 4000. | 0. ** | 1400. | .82 | 15. | 106.4 | F | 16.2 | 18.7 |
| 6 | 2 | 1500. | 687. | 0. 4523. | 687. | 0. 3957. | 3957. | 0. 0. | 0. 0. | 1.00 | 52. | 38.4 | E | 23.6 | 11.1 |
| 7 | 2 | 1300. | 0. | 0. 4523. | 0. | 0. 3957. | 4000. | 0. 0. | 0. 0. | .99 | 52. | 37.8 | E | 23.4 | 11.2 |
| 8 | 3 | 500. | 0. | 1038. 4523. | 0. | 909. 3957. | 5107. | 0. 0. | 0. 0. | .77 | 62. | 21.3 | C | 20.3 | 13.0 |
| 9 | 2 | 2300. | 0. | 0. 3485. | 0. | 0. 3048. | 4000. | 0. 0. | 0. 0. | .76 | 62. | 24.6 | C | 20.3 | 13.0 |
| 10 | 3 | 250. | 433. | 0. 3918. | 433. | 0. 3481. | 4824. | 0. 0. | 0. 0. | .72 | 62. | 18.7 | C | 20.3 | 13.0 |
| 11 | 3 | 200. | 0. | 0. 3918. | 0. | 0. 3481. | 4860. | 0. 0. | 0. 0. | .72 | 62. | 18.7 | C | 20.3 | 13.0 |
| 12 | 3 | 250. | 0. | 1753. 3918. | 0. | 1561. 3481. | 4616. | 0. 0. | 0. 0. | .75 | 62. | 18.7 | C | 20.3 | 13.0 |
| 13 | 2 | 50. | 0. | 44. 2165. | 0. | 39. 1919. | 3994. | 0. 0. | 0. 0. | .48 | 62. | 15.5 | B | 20.3 | 13.0 |
| 14 | 2 | 50. | 0. | 0. 2121. | 0. | 0. 1880. | 2470. | 0. 0. | 0. 0. | .76 | 62. | 15.2 | B | 20.3 | 13.0 |
| 15 | 2 | 1000. | 43. | 0. 2164. | 43. | 0. 1923. | 3993. | 0. 0. | 0. 0. | .48 | 62. | 15.5 | B | 20.3 | 13.0 |
| 16 | 2 | 10. | 0. | 0. 2164. | 0. | 0. 1923. | 4000. | 0. 0. | 0. 0. | .48 | 62. | 15.5 | B | 20.3 | 13.0 |
| 17 | 2 | 1500. | 749. | 0. 2913. | 749. | 0. 2672. | 3879. | 0. 0. | 0. 0. | .69 | 62. | 21.6 | C | 20.3 | 13.0 |
| 18 | 2 | 1500. | 0. | 403. 2913. | 0. | 372. 2672. | 3960. | 0. 0. | 0. 0. | .67 | 62. | 21.6 | C | 20.3 | 13.0 |
| 19 | 2 | 12000. | 0. | 0. 2510. | 0. | 0. 2300. | 4000. | 0. 0. | 0. 0. | .58 | 62. | 18.6 | C | 20.3 | 13.0 |
| 20 | 3 | 500. | 478. 2988. | 2988. | 478. | 2778. | 7778. | 0. 0. | 0. 0. | .46 | 65. | 14.2 | B | 19.0 | 14.1 |

TOTAL 137309. = 26.0 MI LÉS MAX(V/C) = 1.00 LOWEST LOS = F AVG = 50. 29.7 19.1 14.1

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|----------------------------|--------------------|-----------------|-------------------|------------------|
| FREEWAY TRAVEL TIME = | 1067. VEH-HRS | 1180. PASS-HRS | 1993. VEH-HRS | 2213. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1067. VEH-HRS | 1180. PASS-HRS | 1993. VEH-HRS | 2213. PASS-HRS |
| TOTAL TRAV DISTANCE = | 52907. VEH-MI. | 59825. PASS-MI. | 106289. VEH-MI. | 120131. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 50. MPH. | | 53. MPH. | |
| AVERAGE DENSITY = | 30. VPML | | 28. VPML | |
| TOTAL FUEL = | 2768. GALLONS | | 5500. GALLONS | |
| TOTAL EMISSIONS = | 747. KI LOGRAMS | | 1477. KI LOGRAMS | |

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 TIME SLICE 2 OF 6

***** MAINTLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|--------|------------|-------|------------|-------|
| 1 | 0.04 | 2 | 35.68 | 3 | 165.43 | 4 | 23.01 | 5 | 21.55 |
| 6 | 2.26 | 7 | 1.80 | 8 | 0.14 | 9 | 0.49 | 10 | 0.06 |
| 11 | 0.05 | 12 | 0.06 | 13 | 0.01 | 14 | 0.01 | 15 | 0.14 |
| 16 | 0.00 | 17 | 0.28 | 18 | 0.28 | 19 | 1.95 | 20 | 0.00 |

***** TOTAL DELAY = 253.2 VEH-HRS ***** AVERAGE DELAY = 4.60 MIN/VEH *****

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 TIME SLICE 3 OF 6

 **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN *
 * 1 2 3 4 5 6 7 *

 * * *
 * 1 * 22.85 34.98 35.53 35.54 35.73 36.28 38.57 *
 * 2 * 0.00 2.99 3.54 3.55 3.74 4.29 6.58 *
 * 3 * 0.00 0.70 1.25 1.26 1.46 2.01 4.29 *
 * 4 * 0.00 0.00 0.13 0.14 0.33 0.88 3.17 *
 * 5 * 0.00 0.00 0.00 0.00 0.18 0.73 3.02 *
 * 6 * 0.00 0.00 0.00 0.00 0.00 0.55 2.84 *
 * 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.09 *
 * * *

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 TIME SLICE 3 OF 6

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|-----------|----------|------------|------------|------------|------------|---------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|
| * SEC LNS | * LENGTH | * ORG | * DES | * ORG | * DES | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPML | * LEVEL | * MPG | * GS/VM |
| * 1 3 | * 500. | * 4628. | * 0. 4628. | * 4628. | * 0. 4628. | * 6000. | * 0. | * 0. | * 0. | * .77 | * 64. | * 24.2 | * C | * 19.5 | * 13.7 |
| * 2 3 | * 99999. | * 0. 741. | * 4628. | * 0. 741. | * 3867. | * 6000. | * 0. * | * 8169. | * 761. | * .64 | * 50. | * 25.8 | * F | * 18.9 | * 14.1 |
| * 3 2 | * 11000. | * 0. 0. | * 3887. | * 0. 0. | * 3126. | * 4000. | * 0. ** | * 11000. | * 761. | * .78 | * 14. | * 114.3 | * F | * 15.1 | * 20.0 |
| * 4 2 | * 1500. | * 64. 0. | * 3951. | * 64. 0. | * 3190. | * 3995. | * 0. ** | * 1500. | * 761. | * .80 | * 14. | * 110.4 | * F | * 15.7 | * 19.4 |
| * 5 2 | * 1400. | * 0. 0. | * 3951. | * 0. 0. | * 3190. | * 4000. | * 0. ** | * 1400. | * 761. | * .80 | * 14. | * 110.8 | * F | * 15.6 | * 19.4 |
| * 6 2 | * 1500. | * 764. 0. | * 4715. | * 764. 0. | * 3954. | * 3954. | * 0. 0. | * 0. | * 1.00 | * 0. | * 52. | * 38.3 | * E | * 23.6 | * 11.1 |
| * 7 2 | * 1300. | * 0. 0. | * 4715. | * 0. 0. | * 3954. | * 4000. | * 0. 0. | * 0. | * .99 | * 0. | * 52. | * 37.7 | * E | * 23.4 | * 11.2 |
| * 8 3 | * 500. | * 0. 1099. | * 4715. | * 0. 923. | * 3954. | * 5099. | * 0. 0. | * 0. | * .78 | * 0. | * 62. | * 21.3 | * C | * 20.3 | * 13.0 |
| * 9 2 | * 2300. | * 0. 0. | * 3616. | * 0. 0. | * 3031. | * 4000. | * 0. 0. | * 0. | * .76 | * 0. | * 62. | * 24.4 | * C | * 20.3 | * 13.0 |
| * 10 3 | * 250. | * 459. 0. | * 4075. | * 459. 0. | * 3490. | * 4823. | * 0. 0. | * 0. | * .72 | * 0. | * 62. | * 18.8 | * C | * 20.3 | * 13.0 |
| * 11 3 | * 200. | * 0. 0. | * 4075. | * 0. 0. | * 3490. | * 4860. | * 0. 0. | * 0. | * .72 | * 0. | * 62. | * 18.8 | * C | * 20.3 | * 13.0 |
| * 12 3 | * 250. | * 0. 1562. | * 4075. | * 0. 1342. | * 3490. | * 4646. | * 0. 0. | * 0. | * .75 | * 0. | * 62. | * 18.8 | * C | * 20.3 | * 13.0 |
| * 13 2 | * 50. | * 0. 175. | * 2513. | * 0. 150. | * 2148. | * 3976. | * 0. 0. | * 0. | * .54 | * 0. | * 62. | * 17.3 | * B | * 20.3 | * 13.0 |

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| | | | | | | | | | | | | | | | | | | | | |
|---|----|---|--------|------|-------|-------|------|-------|-------|-------|----|----|----|-----|-----|------|---|------|------|---|
| * | 14 | 2 | 50. | 0. | 0. | 2338. | 0. | 0. | 1997. | 2470. | 0. | 0. | 0. | .81 | 62. | 16.1 | B | 20.3 | 13.0 | * |
| * | 15 | 2 | 1000. | 175. | 0. | 2513. | 175. | 0. | 2172. | 3975. | 0. | 0. | 0. | .55 | 62. | 17.5 | B | 20.3 | 13.0 | * |
| * | 16 | 2 | 10. | 0. | 0. | 2513. | 0. | 0. | 2172. | 4000. | 0. | 0. | 0. | .54 | 62. | 17.5 | B | 20.3 | 13.0 | * |
| * | 17 | 2 | 1500. | 824. | 0. | 3337. | 824. | 0. | 2996. | 3880. | 0. | 0. | 0. | .77 | 62. | 24.2 | C | 20.3 | 13.0 | * |
| * | 18 | 2 | 1500. | 0. | 725. | 3337. | 0. | 656. | 2996. | 3932. | 0. | 0. | 0. | .76 | 62. | 24.2 | C | 20.3 | 13.0 | * |
| * | 19 | 2 | 12000. | 0. | 0. | 2612. | 0. | 0. | 2340. | 4000. | 0. | 0. | 0. | .59 | 62. | 18.9 | C | 20.3 | 13.0 | * |
| * | 20 | 3 | 500. | 497. | 3109. | 3109. | 497. | 2837. | 2837. | 6000. | 0. | 0. | 0. | .47 | 65. | 14.6 | B | 19.0 | 14.1 | * |

 * TOTAL 137309. = 26.0 MI LSES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 42. 34.1 18.8 14.4 *

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------------------|----------------------------------|
| FREEWAY TRAVEL TIME = | 1272. VEH-HRS 1413. PASS-HRS | 3265. VEH-HRS 3627. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1272. VEH-HRS 1413. PASS-HRS | 3265. VEH-HRS 3627. PASS-HRS |
| TOTAL TRAV DISTANCE = | 53789. VEH-MI. 60848. PASS-MI. | 160078. VEH-MI. 180980. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 42. MPH. | 49. MPH. |
| AVERAGE DENSITY = | 34. VPML | 30. VPML |
| TOTAL FUEL = | 2867. GALLONS | 8367. GALLONS |
| TOTAL EMISSIONS = | 775. KI LOGRAMS | 2253. KI LOGRAMS |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION TIME SLICE 3 OF 6

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|--------|------------|--------|------------|-------|------------|-------|
| 1 | 0.06 | 2 | 201.89 | 3 | 187.97 | 4 | 24.40 | 5 | 22.87 |
| 6 | 2.25 | 7 | 1.79 | 8 | 0.14 | 9 | 0.49 | 10 | 0.06 |
| 11 | 0.05 | 12 | 0.06 | 13 | 0.01 | 14 | 0.01 | 15 | 0.15 |
| 16 | 0.00 | 17 | 0.32 | 18 | 0.32 | 19 | 1.98 | 20 | 0.00 |

***** TOTAL DELAY = 444.8 VEH-HRS ***** AVERAGE DELAY = 7.77 MIN/VEH *****

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION TIME SLICE 4 OF 6

 ** FREEWAY TRAVEL TIME (MINUTES) **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN *
 * 1 2 3 4 5 6 7 *

 + * 1 * 28.09 40.22 40.77 40.78 40.97 41.52 43.81 *
 + * 2 * 0.00 2.99 3.54 3.55 3.74 4.29 6.58 *
 + * 3 * 0.00 0.70 1.25 1.26 1.46 2.01 4.29 *
 + * 4 * 0.00 0.00 0.13 0.14 0.33 0.88 3.17 *
 + * 5 * 0.00 0.00 0.00 0.00 0.18 0.73 3.02 *
 + * 6 * 0.00 0.00 0.00 0.00 0.00 0.55 2.84 *
 + * 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.09 *
 + * * *

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 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|-----------|--------|------------|-----------|------------|-----------|---------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPML | * LEVEL | * MPG | * GS/VM |
| * 1 | * 3 | * 500. | * 4628. | * 0. | * 4628. | * 4628. | * 0. | * 0. | * 0. | * .77 | * 64. | * 24.2 | * C | * 19.5 | * 13.7 |

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| | | | | | | | | | | | | | | | | | | | | | |
|---|----|---|--------|------|-------|-------|------|-------|-------|-------|----|----|--------|------|-----|------|-------|------|------|------|---|
| * | 2 | 3 | 99999. | 0. | 741. | 4628. | 0. | 741. | 3867. | 6000. | 0. | * | 13753. | 761. | .64 | 41. | 31.8 | F | 18.3 | 14.6 | * |
| * | 3 | 2 | 11000. | 0. | 0. | 3887. | 0. | 0. | 3126. | 4000. | 0. | ** | 11000. | 761. | .78 | 14. | 114.3 | F | 15.1 | 20.0 | * |
| * | 4 | 2 | 1500. | 64. | 0. | 3951. | 64. | 0. | 3190. | 3995. | 0. | ** | 1500. | 761. | .80 | 14. | 110.4 | F | 15.7 | 19.4 | * |
| * | 5 | 2 | 1400. | 0. | 0. | 3951. | 0. | 0. | 3190. | 4000. | 0. | ** | 1400. | 761. | .80 | 14. | 110.8 | F | 15.6 | 19.4 | * |
| * | 6 | 2 | 1500. | 764. | 0. | 4715. | 764. | 0. | 3954. | 3954. | 0. | 0. | 0. | 1.00 | 52. | 38.3 | E | 23.6 | 11.1 | * | |
| * | 7 | 2 | 1300. | 0. | 0. | 4715. | 0. | 0. | 3954. | 4000. | 0. | 0. | 0. | .99 | 52. | 37.7 | E | 23.4 | 11.2 | * | |
| * | 8 | 3 | 500. | 0. | 1099. | 4715. | 0. | 923. | 3954. | 5099. | 0. | 0. | 0. | .78 | 62. | 21.3 | C | 20.3 | 13.0 | * | |
| * | 9 | 2 | 2300. | 0. | 0. | 3616. | 0. | 0. | 3031. | 4000. | 0. | 0. | 0. | .76 | 62. | 24.4 | C | 20.3 | 13.0 | * | |
| * | 10 | 3 | 250. | 459. | 0. | 4075. | 459. | 0. | 3490. | 4823. | 0. | 0. | 0. | .72 | 62. | 18.8 | C | 20.3 | 13.0 | * | |
| * | 11 | 3 | 200. | 0. | 0. | 4075. | 0. | 0. | 3490. | 4860. | 0. | 0. | 0. | .72 | 62. | 18.8 | C | 20.3 | 13.0 | * | |
| * | 12 | 3 | 250. | 0. | 1562. | 4075. | 0. | 1342. | 3490. | 4646. | 0. | 0. | 0. | .75 | 62. | 18.8 | C | 20.3 | 13.0 | * | |
| * | 13 | 2 | 50. | 0. | 175. | 2513. | 0. | 150. | 2148. | 3976. | 0. | 0. | 0. | .54 | 62. | 17.3 | B | 20.3 | 13.0 | * | |
| * | 14 | 2 | 50. | 0. | 0. | 2338. | 0. | 0. | 1997. | 2470. | 0. | 0. | 0. | .81 | 62. | 16.1 | B | 20.3 | 13.0 | * | |
| * | 15 | 2 | 1000. | 175. | 0. | 2513. | 175. | 0. | 2172. | 3975. | 0. | 0. | 0. | .55 | 62. | 17.5 | B | 20.3 | 13.0 | * | |
| * | 16 | 2 | 10. | 0. | 0. | 2513. | 0. | 0. | 2172. | 4000. | 0. | 0. | 0. | .54 | 62. | 17.5 | B | 20.3 | 13.0 | * | |
| * | 17 | 2 | 1500. | 824. | 0. | 3337. | 824. | 0. | 2996. | 3880. | 0. | 0. | 0. | .77 | 62. | 24.2 | C | 20.3 | 13.0 | * | |
| * | 18 | 2 | 1500. | 0. | 725. | 3337. | 0. | 656. | 2996. | 3932. | 0. | 0. | 0. | .76 | 62. | 24.2 | C | 20.3 | 13.0 | * | |
| * | 19 | 2 | 12000. | 0. | 0. | 2612. | 0. | 0. | 2340. | 4000. | 0. | 0. | 0. | .59 | 62. | 18.9 | C | 20.3 | 13.0 | * | |
| * | 20 | 3 | 500. | 497. | 3109. | 3109. | 497. | 2837. | 2837. | 6000. | 0. | 0. | 0. | .47 | 65. | 14.6 | B | 19.0 | 14.1 | * | |

| | | | | | | | | | | | | | | | | |
|---|-------|---------|---|------|-------|--|--|-----------------|----------------|-----------|------|--|--|------|------|---|
| * | TOTAL | 137309. | = | 26.0 | MILES | | | MAX(V/C) = 1.00 | LOWEST LOS = F | AVG = 37. | 38.4 | | | 18.3 | 14.8 | * |
|---|-------|---------|---|------|-------|--|--|-----------------|----------------|-----------|------|--|--|------|------|---|

| CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | | |
|----------------------------|--------|------------|--------|-------------------|---------|------------|---------|----------|
| FREWAY TRAVEL TIME = | 1463. | VEH-HRS | 1634. | PASS-HRS | 4728. | VEH-HRS | 5261. | PASS-HRS |
| FREWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1463. | VEH-HRS | 1634. | PASS-HRS | 4728. | VEH-HRS | 5261. | PASS-HRS |
| TOTAL TRAV DISTANCE = | 53386. | VEH-MI. | 60382. | PASS-MI. | 213464. | VEH-MI. | 241362. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 37. | MPH | | | 45. | MPH | | |
| AVERAGE DENSITY = | 38. | VPMP | | | 32. | VPMP | | |
| TOTAL FUEL = | 2918. | GALLONS | | | 11285. | GALLONS | | |
| TOTAL EMISSIONS = | 791. | KI LOGRAMS | | | 3044. | KI LOGRAMS | | |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 4 OF 6

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|--------|------------|--------|------------|-------|------------|-------|
| 1 | 0.06 | 2 | 398.33 | 3 | 187.97 | 4 | 24.40 | 5 | 22.87 |
| 6 | 2.25 | 7 | 1.79 | 8 | 0.14 | 9 | 0.49 | 10 | 0.06 |
| 11 | 0.05 | 12 | 0.06 | 13 | 0.01 | 14 | 0.01 | 15 | 0.15 |
| 16 | 0.00 | 17 | 0.32 | 18 | 0.32 | 19 | 1.98 | 20 | 0.00 |

***** TOTAL DELAY = 641.3 VEH-HRS ***** AVERAGE DELAY = 10.82 MIN/VEH *****

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 5 OF 6

 ** **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 ** **

| * ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | | * | |
|----------------|---------------------|-------|-------|-------|-------|-------|-------|-------|---|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | * | |
| + * | ***** | | | | | | | * | |
| + * | ***** | | | | | | | * | |
| + * | 1 | 31.32 | 41.32 | 41.88 | 41.89 | 42.08 | 42.63 | 44.92 | * |
| + * | 2 | 0.00 | 2.56 | 3.12 | 3.13 | 3.32 | 3.87 | 6.16 | * |
| + * | 3 | 0.00 | 0.71 | 1.26 | 1.27 | 1.46 | 2.01 | 4.30 | * |
| + * | 4 | 0.00 | 0.00 | 0.13 | 0.14 | 0.33 | 0.88 | 3.17 | * |
| + * | 5 | 0.00 | 0.00 | 0.00 | 0.00 | 0.18 | 0.73 | 3.02 | * |
| + * | 6 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.55 | 2.84 | * |
| + * | 7 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.09 | * |
| + * | ***** | | | | | | | * | |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 5 OF 6

 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *

| * SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMI SS | * SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMP L LEVEL MPG GS/VM |
|--|--|
| * 1 3 500. 4030. 0. 4030. 4030. 0. 4030. 6000. 0. 0. 0. .67 65. 20.7 C 19.0 14.1 | |
| * 2 3 99999. 0. 645. 4030. 0. 645. 4022. 6000. 0. * 13812. 8. .67 36. 36.8 F 17.7 15.3 | |
| * 3 2 11000. 0. 0. 3385. 0. 0. 3377. 4000. 0. **11000. 8. .84 17. 100.6 F 16.8 17.9 | |
| * 4 2 1500. 64. 0. 3449. 64. 0. 3441. 3995. 0. ** 1500. 8. .86 18. 96.8 F 17.2 17.4 | |
| * 5 2 1400. 0. 0. 3449. 0. 0. 3441. 4000. 0. ** 1400. 8. .86 18. 97.1 F 17.2 17.4 | |
| * 6 2 1500. 528. 0. 3977. 528. 0. 3969. 3969. 0. 0. 0. 1.00 52. 38.5 E 23.6 11.1 | |
| * 7 2 1300. 0. 0. 3977. 0. 0. 3969. 4000. 0. 0. 0. .99 52. 38.0 E 23.5 11.2 | |
| * 8 3 500. 0. 869. 3977. 0. 867. 3969. 5130. 0. 0. 0. .77 62. 21.3 C 20.3 13.0 | |
| * 9 2 2300. 0. 0. 3108. 0. 0. 3102. 4000. 0. 0. 0. .78 61. 25.3 C 20.6 12.8 | |
| * 10 3 250. 373. 0. 3481. 373. 0. 3475. 4832. 0. 0. 0. .72 62. 18.7 C 20.3 13.0 | |
| * 11 3 200. 0. 0. 3481. 0. 0. 3475. 4860. 0. 0. 0. .71 62. 18.7 C 20.3 13.0 | |
| * 12 3 250. 0. 1268. 3481. 0. 1266. 3475. 4680. 0. 0. 0. .74 62. 18.7 C 20.3 13.0 | |
| * 13 2 50. 0. 350. 2213. 0. 349. 2209. 3950. 0. 0. 0. .56 62. 17.8 B 20.3 13.0 | |
| * 14 2 50. 0. 0. 1863. 0. 0. 1860. 2470. 0. 0. 0. .75 62. 15.0 B 20.3 13.0 | |
| * 15 2 1000. 348. 0. 2211. 348. 0. 2208. 3948. 0. 0. 0. .56 62. 17.8 B 20.3 13.0 | |
| * 16 2 10. 0. 0. 2211. 0. 0. 2208. 4000. 0. 0. 0. .55 62. 17.8 B 20.3 13.0 | |
| * 17 2 1500. 769. 0. 2980. 769. 0. 2977. 3884. 0. 0. 0. .77 62. 24.0 C 20.3 13.0 | |
| * 18 2 1500. 0. 584. 2980. 0. 583. 2977. 3949. 0. 0. 0. .75 62. 24.0 C 20.3 13.0 | |
| * 19 2 12000. 0. 0. 2396. 0. 0. 2393. 4000. 0. 0. 0. .60 62. 19.3 C 20.3 13.0 | |
| * 20 3 500. 456. 2852. 2852. 456. 2849. 2849. 6000. 0. 0. 0. .47 65. 14.6 B 19.0 14.1 | |
| * * * TOTAL 137309. = 26.0 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 35. 40.8 18.0 15.2 * * ***** | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 1416. VEH-HRS | 1585. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1416. VEH-HRS | 1585. PASS-HRS |
| TOTAL TRAV DISTANCE = | 48882. VEH-MI. | 55092. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 35. MPH | 43. MPH |
| AVERAGE DENSITY = | 41. VPMP | 34. VPMP |
| TOTAL FUEL = | 2719. GALLONS | 14004. GALLONS |
| TOTAL EMISSIONS = | 744. KI LOGRAMS | 3788. KI LOGRAMS |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION TIME SLICE 5 OF 6

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|--------|------------|--------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 461.49 | 3 | 155.46 | 4 | 19.97 | 5 | 18.73 |
| 6 | 2.26 | 7 | 1.85 | 8 | 0.14 | 9 | 0.61 | 10 | 0.06 |
| 11 | 0.05 | 12 | 0.06 | 13 | 0.01 | 14 | 0.01 | 15 | 0.16 |
| 16 | 0.00 | 17 | 0.31 | 18 | 0.31 | 19 | 2.02 | 20 | 0.00 |

***** TOTAL DELAY = 663.5 VEH-HRS ***** AVERAGE DELAY = 10.47 MIN/VEH *****

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION TIME SLICE 6 OF 6

 **
 ** FREeway TRAVEL TIME (MINUTES) **
 **

| * ORIGINS DOWN | * DESTINATIONS ACROSS * | | | | | | |
|----------------|-------------------------|-------|-------|-------|-------|-------|-------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 31.37 | 41.38 | 41.94 | 41.95 | 42.14 | 42.69 | 44.98 |
| * 2 * | 0.00 | 2.56 | 3.12 | 3.13 | 3.32 | 3.87 | 6.16 |
| * 3 * | 0.00 | 0.71 | 1.26 | 1.27 | 1.46 | 2.01 | 4.30 |
| * 4 * | 0.00 | 0.00 | 0.13 | 0.14 | 0.33 | 0.88 | 3.17 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.18 | 0.73 | 3.02 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.55 | 2.84 |

SR-237_WB_PM_P1_2040_PE

* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.09

* * *

1 INSTITUTE OF TRANSPORTATION STUDIES
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FREQ12PE REL 3.01
 SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 6 OF 6

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| ***** | | | | | | | | | | | | | | | | | | |
|--|---|---|------|---------|--|--|--|--|-----------------|----------------|-----------|------|--|--|--|------|------|---|
| * | | | | | | | | | | | | | | | | | | |
| * | | | | | | | | | | | | | | | | | | |
| * TIME SLICE FREEWAY PERFORMANCE TABLE * | | | | | | | | | | | | | | | | | | |
| ***** | | | | | | | | | | | | | | | | | | |
| * SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMISSIONS | * SEC LNS LENGTH ORG DES SSEC ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMP L LEVEL MPG GS/VM | * | | | | | | | | | | | | | | | | |
| ***** | | | | | | | | | | | | | | | | | | |
| * 1 3 500. 4030. 0. 4030. 4030. 0. 4030. 6000. 0. 0. 0. .67 65. 20.7 C 19.0 14.1 | | | | | | | | | | | | | | | | | | |
| * 2 3 99999. 0. 645. 4030. 0. 645. 4022. 6000. 0. * 13872. 8. .67 36. 36.9 F 17.7 15.3 | | | | | | | | | | | | | | | | | | |
| * 3 2 11000. 0. 0. 3385. 0. 0. 3377. 4000. 0. **11000. 8. .84 17. 100.6 F 16.8 17.9 | | | | | | | | | | | | | | | | | | |
| * 4 2 1500. 64. 0. 3449. 64. 0. 3441. 3995. 0. ** 1500. 8. .86 18. 96.8 F 17.2 17.4 | | | | | | | | | | | | | | | | | | |
| * 5 2 1400. 0. 0. 3449. 0. 0. 3441. 4000. 0. ** 1400. 8. .86 18. 97.1 F 17.2 17.4 | | | | | | | | | | | | | | | | | | |
| * 6 2 1500. 528. 0. 3977. 528. 0. 3969. 3969. 0. 0. 1.00 52. 38.5 E 23.6 11.1 | | | | | | | | | | | | | | | | | | |
| * 7 2 1300. 0. 0. 3977. 0. 0. 3969. 4000. 0. 0. 0. .99 52. 38.0 E 23.5 11.2 | | | | | | | | | | | | | | | | | | |
| * 8 3 500. 0. 869. 3977. 0. 867. 3969. 5130. 0. 0. 0. .77 62. 21.3 C 20.3 13.0 | | | | | | | | | | | | | | | | | | |
| * 9 2 2300. 0. 0. 3108. 0. 0. 3102. 4000. 0. 0. 0. .78 61. 25.3 C 20.6 12.8 | | | | | | | | | | | | | | | | | | |
| * 10 3 250. 373. 0. 3481. 373. 0. 3475. 4832. 0. 0. 0. .72 62. 18.7 C 20.3 13.0 | | | | | | | | | | | | | | | | | | |
| * 11 3 200. 0. 0. 3481. 0. 0. 3475. 4860. 0. 0. 0. .71 62. 18.7 C 20.3 13.0 | | | | | | | | | | | | | | | | | | |
| * 12 3 250. 0. 1268. 3481. 0. 1266. 3475. 4680. 0. 0. 0. .74 62. 18.7 C 20.3 13.0 | | | | | | | | | | | | | | | | | | |
| * 13 2 50. 0. 350. 2213. 0. 349. 2209. 3950. 0. 0. 0. .56 62. 17.8 B 20.3 13.0 | | | | | | | | | | | | | | | | | | |
| * 14 2 50. 0. 0. 1863. 0. 0. 1860. 2470. 0. 0. 0. .75 62. 15.0 B 20.3 13.0 | | | | | | | | | | | | | | | | | | |
| * 15 2 1000. 348. 0. 2211. 348. 0. 2208. 3948. 0. 0. 0. .56 62. 17.8 B 20.3 13.0 | | | | | | | | | | | | | | | | | | |
| * 16 2 10. 0. 0. 2211. 0. 0. 2208. 4000. 0. 0. 0. .55 62. 17.8 B 20.3 13.0 | | | | | | | | | | | | | | | | | | |
| * 17 2 1500. 769. 0. 2980. 769. 0. 2977. 3884. 0. 0. 0. .77 62. 24.0 C 20.3 13.0 | | | | | | | | | | | | | | | | | | |
| * 18 2 1500. 0. 584. 2980. 0. 583. 2977. 3949. 0. 0. 0. .75 62. 24.0 C 20.3 13.0 | | | | | | | | | | | | | | | | | | |
| * 19 2 12000. 0. 0. 2396. 0. 0. 2393. 4000. 0. 0. 0. .60 62. 19.3 C 20.3 13.0 | | | | | | | | | | | | | | | | | | |
| * 20 3 500. 456. 2852. 2852. 456. 2849. 2849. 6000. 0. 0. 0. .47 65. 14.6 B 19.0 14.1 | | | | | | | | | | | | | | | | | | |
| ***** | | | | | | | | | | | | | | | | | | |
| * TOTAL | 137309. | = | 26.0 | MI L ES | | | | | MAX(V/C) = 1.00 | LOWEST LOS = F | AVG = 34. | 40.8 | | | | 18.0 | 15.2 | * |
| ***** | | | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 1418. VEH-HRS | 1587. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1418. VEH-HRS | 1587. PASS-HRS |
| TOTAL TRAV DISTANCE = | 48882. VEH-MI. | 55092. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 34. MPH. | 41. MPH. |
| AVERAGE DENSITY = | 41. VPMP L | 35. VPMP L |
| TOTAL FUEL = | 2719. GALLONS | 16723. GALLONS |
| TOTAL EMISSIONS = | 745. KI LOGRAMS | 4533. KI LOGRAMS |

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FREQ12PE REL 3.01
 SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 6 OF 6

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| | | | | | | | | | |
|---|-------|------------|--------|------------|--------|------------|-------|------------|-------|
| ***** MAINLINE DELAY (VEH-HRS) ***** | | | | | | | | | |
| DESIRED SPEED = 65.0 ***** | | | | | | | | | |
| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
| 1 | 0.00 | 2 | 463.49 | 3 | 155.46 | 4 | 19.97 | 5 | 18.73 |
| 6 | 2.26 | 7 | 1.85 | 8 | 0.14 | 9 | 0.61 | 10 | 0.06 |
| 11 | 0.05 | 12 | 0.06 | 13 | 0.01 | 14 | 0.01 | 15 | 0.16 |
| 16 | 0.00 | 17 | 0.31 | 18 | 0.31 | 19 | 2.02 | 20 | 0.00 |
| ***** TOTAL DELAY = 665.5 VEH-HRS ***** | | | | | | | | | |
| ***** AVERAGE DELAY = 10.50 MIN/VEH ***** | | | | | | | | | |

```
FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ      1111      222222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEEEE Q* A. D. MAY* Q 111111 222 222 PPPPPPPP LLL
FFF      RRR      RRR EEE      QQQQQ QQQQ      1111      222 222 PPP      PPP LLL
FFF      RRR      RRR EEE      QQQQ      QQQQ      1111      222 222 PPP      PPP LLL
FFFFFFFF RRRRRRRR EEEEEEEE QQQQ      QQQQ      1111      222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEEE QQQQ      QQQQ      1111      2222 PPPPPPPP LLL
FFF      RRR      RRR EEE      QQQQ      QQQ QQQQ      1111      2222 PPP      LLL
FFF      RRR      RRR EEE      Q*UC*      QQQQQ      1111      222 PPP      LLL
FFF      RRR      RRR EEEEEEEEE Q*REGENTS*Q      1111      222 PPP      LLLLLLLLLL
FFF      RRR      RRR EEEEEEEEE Q*1988*Q QQQ 11111111 2222222222 PPP      LLLLLLLLLL
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FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 3 AND 19 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 2.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 30
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

FREeway AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT DES TRUCKS | SPECIAL RAMP | FF SPD. ALT. RTE | CAP. ALT. RTE | ART GRADE TYPE | ART GRADE ALT. RTE | SUBSECTION LOCATION |
|---------|----------|----------|-------------|--------------|---------|---------|-----------|---------|----------------|--------------|------------------|---------------|----------------|--------------------|--------------------------|
| 1 | | | | | | | | | | | | | | | |
| 2 | | | | | | | | | | | | | | | |
| 3 | 1 | 1500. | 11000. | 62 | 0 | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| 4 | 1 | 1500. | 1500. | 62 | 0 | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence On-ramp |
| 5 | 1 | 1500. | 1400. | 62 | | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence to Crossman |
| 6 | 1 | 1500. | 1500. | 62 | 0 | 0.95 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Crossman On-Ramp |
| 7 | 1 | 1500. | 1300. | 62 | | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Crossman / Mathilda |
| 8 | 1 | 1500. | 500. | 62 | D | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-Ramp |
| 9 | 1 | 1500. | 2300. | 62 | | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda |
| 10 | 1 | 1500. | 250. | 62 | 0 | 0.95 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda On-ramp |
| 11 | 1 | 1500. | 200. | 62 | | 0.95 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda to US-101 |
| 12 | 1 | 1500. | 250. | 62 | D | 0.95 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | US-101 Off-Ramp |
| 13 | 1 | 1500. | 50. | 62 | D | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Bottleneck by-pass |
| 14 | 1 | 1500. | 50. | 62 | | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Bottleneck |
| 15 | 1 | 1500. | 1000. | 62 | OD | 0.95 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | US 101 / US 101 |
| 16 | 1 | 1500. | 10. | 62 | | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Dummy end of travel time |
| 17 | 1 | 1500. | 1500. | 62 | 0 | 0.95 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | US 101 NB On-Ramp |
| 18 | 1 | 1500. | 1500. | 62 | D | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Maude Off-ramp |

```

**
** 19 1 1500. 12000. 62 D 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 HOV Dummy
**
** 20
**
*****

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*****
**
** FREEWAY TRAVEL TIME (MINUTES)
**
*****

```

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | |
|-----------|-------|-----------------------|------|------|------|------|------|------|------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| + | * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + | * 2 * | 0.00 | 3.15 | 3.70 | 3.71 | 3.90 | 4.46 | 6.66 | 0.00 |
| + | * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.44 | 4.64 | 0.00 |
| + | * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 4.11 | 0.00 |
| + | * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.08 | 0.00 |
| + | * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.93 | 0.00 |
| + | * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.75 | 0.00 |
| + | * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | | | |
|-----------|--------|------------|-----------|------------|--------|---------|-----------|-----------|---------|-----------------|----------------|-----------|--------|-------------|------|---|------|------|--|
| * SEC | * LNS | * LENGTH | * ORG DES | * ORG DES | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP/L | * LEVEL | * MPG | * GS/VM | | | | | |
| * 1 | | | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | | | |
| * 3 | 1 | 11000. | 720. | 0. | 720. | 720. | 0. | 720. | 1500. | 0. | 0. | 0. | .48 | 62. | 11.6 | B | 21.6 | 12.8 | |
| * 4 | 1 | 1500. | 4. | 0. | 724. | 4. | 0. | 724. | 1500. | 0. | 0. | 0. | .48 | 62. | 11.7 | B | 21.6 | 12.8 | |
| * 5 | 1 | 1400. | 0. | 0. | 724. | 0. | 0. | 724. | 1500. | 0. | 0. | 0. | .48 | 62. | 11.7 | B | 21.6 | 12.8 | |
| * 6 | 1 | 1500. | 43. | 0. | 767. | 43. | 0. | 767. | 1500. | 0. | 0. | 0. | .51 | 62. | 12.4 | B | 21.6 | 12.8 | |
| * 7 | 1 | 1300. | 0. | 0. | 767. | 0. | 0. | 767. | 1500. | 0. | 0. | 0. | .51 | 62. | 12.4 | B | 21.6 | 12.8 | |
| * 8 | 1 | 500. | 0. | 163. | 767. | 0. | 163. | 767. | 1500. | 0. | 0. | 0. | .51 | 62. | 12.4 | B | 21.6 | 12.8 | |
| * 9 | 1 | 2300. | 0. | 0. | 604. | 0. | 0. | 604. | 1500. | 0. | 0. | 0. | .40 | 62. | 9.7 | A | 21.6 | 12.8 | |
| * 10 | 1 | 250. | 36. | 0. | 640. | 36. | 0. | 640. | 1500. | 0. | 0. | 0. | .43 | 62. | 10.3 | A | 21.6 | 12.8 | |
| * 11 | 1 | 200. | 0. | 0. | 640. | 0. | 0. | 640. | 1500. | 0. | 0. | 0. | .43 | 62. | 10.3 | A | 21.6 | 12.8 | |
| * 12 | 1 | 250. | 0. | 244. | 640. | 0. | 244. | 640. | 1500. | 0. | 0. | 0. | .43 | 62. | 10.3 | A | 21.6 | 12.8 | |
| * 13 | 1 | 50. | 0. | 6. | 396. | 0. | 6. | 396. | 1500. | 0. | 0. | 0. | .26 | 62. | 6.4 | A | 21.6 | 12.8 | |
| * 14 | 1 | 50. | 0. | 0. | 390. | 0. | 0. | 390. | 1500. | 0. | 0. | 0. | .26 | 62. | 6.3 | A | 21.6 | 12.8 | |
| * 15 | 1 | 1000. | 7. | 0. | 397. | 7. | 0. | 397. | 1500. | 0. | 0. | 0. | .26 | 62. | 6.4 | A | 21.6 | 12.8 | |
| * 16 | 1 | 10. | 0. | 0. | 397. | 0. | 0. | 397. | 1500. | 0. | 0. | 0. | .26 | 62. | 6.4 | A | 21.6 | 12.8 | |
| * 17 | 1 | 1500. | 121. | 0. | 518. | 121. | 0. | 518. | 1500. | 0. | 0. | 0. | .35 | 62. | 8.4 | A | 21.6 | 12.8 | |
| * 18 | 1 | 1500. | 0. | 40. | 518. | 0. | 40. | 518. | 1500. | 0. | 0. | 0. | .35 | 62. | 8.4 | A | 21.6 | 12.8 | |
| * 19 | 1 | 12000. | 0. | 478. | 478. | 0. | 478. | 478. | 1500. | 0. | 0. | 0. | .32 | 62. | 7.7 | A | 21.6 | 12.8 | |
| * 20 | | | | | | | | | | | | | | | | | | | |
| * TOTAL | | 36310. | = | 6.9 | MI LBS | | | | | | | | | | | | | | |
| | | | | | | | | | | MAX(V/C) = 0.51 | LOWEST LOS = B | AVG = 62. | 9.8 | 21.6 | 12.8 | | | | |

| CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | | |
|-----------------------------|-------|---------|-------|-------------------|-------|---------|-------|----------|
| FREWAY TRAVEL TIME = | 34. | VEH-HRS | 68. | PASS-HRS | 34. | VEH-HRS | 68. | PASS-HRS |
| FREWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 34. | VEH-HRS | 68. | PASS-HRS | 34. | VEH-HRS | 68. | PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 2095. | VEH-MI. | 4190. | PASS-MI. | 2095. | VEH-MI. | 4190. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. | MPH. | | | 62. | MPH. | | |
| AVERAGE DENSITY = | 10. | VPMP/L | | | 10. | VPMP/L | | |
| TOTAL FUEL = | 97. | GALLONS | | | 97. | GALLONS | | |

TOTAL EMISSIONS = 27. KILOGRAMS

SR-237_WB_PM_P1_2040_PL 27. KILOGRAMS

Table with columns: SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY. Includes summary rows for MAINTENANCE DELAY and TOTAL DELAY.

FREEMAN TRAVEL TIME (MINUTES)

Table with columns: ORIGINS DOWN, DESTINATIONS ACROSS (1-8). Shows travel times between various origin and destination points.

TIME SLICE FREEWAY PERFORMANCE TABLE

Table with columns: SUB SEC, NO. LNS, SSEC LENGTH, O-D DATA ORG, DEMANDS DES, SSEC, ADJUSTED VOLUMES ORG, DES, SSEC, SSEC CAP, WEAVE EFF, CONGEST LENGTH, STORAGE RATE, V/C RATIO, SPEED MPH, DENSITY VPMP, LOS LEVEL, FUEL MPG, EMISSIONS GS/VM. Includes a summary row for TOTAL.

CURRENT TIME SLICE CUMULATIVE VALUES
FREIGHTWAY TRAVEL TIME = 34. VEH-HRS 68. PASS-HRS 68. VEH-HRS 135. PASS-HRS
FREIGHTWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 34. VEH-HRS 68. PASS-HRS 68. VEH-HRS 135. PASS-HRS
TOTAL FRWAY TRAV DISTANCE = 2095. VEH-MI. 4190. PASS-MI. 4190. VEH-MI. 8379. PASS-MI.

***** MAINTLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
1 0.00 2 0.00 3 0.56 4 0.08 5 0.07
6 0.08 7 0.07 8 0.03 9 0.10 10 0.01
11 0.01 12 0.01 13 0.00 14 0.00 15 0.03
16 0.00 17 0.05 18 0.05 19 0.40 20 0.00
***** TOTAL DELAY = 1.6 VEH-HRS ***** AVERAGE DELAY = 0.15 MIN/VEH *****

**
** FREIGHTWAY TRAVEL TIME (MINUTES) **
**

Table with columns: ORIGINS DOWN, DESTINATIONS ACROSS (1-8). Shows travel times between various origins and destinations.

TIME SLICE FREEWAY PERFORMANCE TABLE

Table with columns: SUB NO., SEC LNS, SSEC, O-D DATA, DEMANDS, ADJUSTED VOLUMES, SSEC, WEAVE EFF, CONGEST LENGTH, STORAGE RATE, V/C, SPEED MPH, DENSITY VPMP, LOS LEVEL, FUEL MPG, EMISSIONS GS/VM.

| SR-237_WB_PM_P1_2040_PL | | | | | | | | | | | | | | | | | | | | |
|-------------------------|-------|---|--------|--------|------|------------|------|-----------------|------|-------|----|----------------|-----|-----------|-----|------|------|------|------|---|
| * | 16 | 1 | 10. | 0. | 0. | 446. | 0. | 0. | 446. | 1500. | 0. | 0. | .30 | 62. | 7.2 | A | 21.6 | 12.8 | * | |
| * | 17 | 1 | 1500. | 120. | 0. | 566. | 120. | 0. | 566. | 1500. | 0. | 0. | .38 | 62. | 9.1 | A | 21.6 | 12.8 | * | |
| * | 18 | 1 | 1500. | 0. | 68. | 566. | 0. | 68. | 566. | 1500. | 0. | 0. | .38 | 62. | 9.1 | A | 21.6 | 12.8 | * | |
| * | 19 | 1 | 12000. | 0. | 497. | 497. | 0. | 497. | 497. | 1500. | 0. | 0. | .33 | 62. | 8.0 | A | 21.6 | 12.8 | * | |
| * | 20 | | | | | | | | | | | | | | | | | | * | |
| ***** | | | | | | | | | | | | | | | | | | | | |
| * | TOTAL | | | 36310. | = | 6.9 MI LES | | MAX(V/C) = 0.53 | | | | LOWEST LOS = B | | AVG = 62. | | 10.2 | | 21.6 | 12.8 | * |
| ***** | | | | | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | |
|-----------------------------|--------------------|-----------|-------|----------|-------------------|-----------|--------|----------|
| FREEWAY TRAVEL TIME = | 35. | VEH-HRS | 70. | PASS-HRS | 103. | VEH-HRS | 205. | PASS-HRS |
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 35. | VEH-HRS | 70. | PASS-HRS | 103. | VEH-HRS | 205. | PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 2175. | VEH-MI. | 4351. | PASS-MI. | 6365. | VEH-MI. | 12730. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. | MPH. | | | 62. | MPH. | | |
| AVERAGE DENSITY = | 10. | VPMP | | | 10. | VPMP | | |
| TOTAL FUEL = | 101. | GALLONS | | | 295. | GALLONS | | |
| TOTAL EMISSIONS = | 28. | KILOGRAMS | | | 81. | KILOGRAMS | | |

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 TIME SLICE 3 OF 6

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.57 | 4 | 0.08 | 5 | 0.07 |
| 6 | 0.08 | 7 | 0.07 | 8 | 0.03 | 9 | 0.10 | 10 | 0.01 |
| 11 | 0.01 | 12 | 0.01 | 13 | 0.00 | 14 | 0.00 | 15 | 0.03 |
| 16 | 0.00 | 17 | 0.06 | 18 | 0.06 | 19 | 0.42 | 20 | 0.00 |

***** TOTAL DELAY = 1.6 VEH-HRS ***** AVERAGE DELAY = 0.15 MIN/VEH *****

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 TIME SLICE 4 OF 6

 **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | | | | |
|-----------|-----|-----------------------|------|------|------|------|------|------|------|---|---|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | |
| * | * | | | | | | | | | * | * |
| + | | | | | | | | | | | |
| * | 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | * |
| + | | | | | | | | | | | |
| * | 2 * | 0.00 | 3.15 | 3.70 | 3.71 | 3.90 | 4.46 | 6.66 | 0.00 | | * |
| + | | | | | | | | | | | |
| * | 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.44 | 4.64 | 0.00 | | * |
| + | | | | | | | | | | | |
| * | 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 4.11 | 0.00 | | * |
| + | | | | | | | | | | | |
| * | 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.08 | 0.00 | | * |
| + | | | | | | | | | | | |
| * | 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.93 | 0.00 | | * |
| + | | | | | | | | | | | |
| * | 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.75 | 0.00 | | * |
| + | | | | | | | | | | | |
| * | 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | * |
| + | | | | | | | | | | | |
| * | * | | | | | | | | | | * |

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 TIME SLICE 4 OF 6

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | |
|-----------|--------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|----------|---------|-----------|-------|--------|-------------|-------|---------|------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | |
| * | 1 | | | | | | | | | | | | | | | | | |
| * | 2 | | | | | | | | | | | | | | | | | |
| * | 3 | 1 | 11000. | 741. | 0. | 741. | 741. | 0. | 741. | 1500. | 0. | 0. | .49 | 62. | 11.9 | B | 21.6 | 12.8 |

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| | | | | | | | | | | | | | | | | | | | |
|-------|-------|--------|--------|------|------|------|------|------|------|-----------------|----------------|-----------|------|-----|------|------|------|------|---|
| * | 4 | 1 | 1500. | 5. | 0. | 746. | 5. | 0. | 746. | 1500. | 0. | 0. | .50 | 62. | 12.0 | B | 21.6 | 12.8 | * |
| * | 5 | 1 | 1400. | 0. | 0. | 746. | 0. | 0. | 746. | 1500. | 0. | 0. | .50 | 62. | 12.0 | B | 21.6 | 12.8 | * |
| * | 6 | 1 | 1500. | 46. | 0. | 792. | 46. | 0. | 792. | 1500. | 0. | 0. | .53 | 62. | 12.8 | B | 21.6 | 12.8 | * |
| * | 7 | 1 | 1300. | 0. | 0. | 792. | 0. | 0. | 792. | 1500. | 0. | 0. | .53 | 62. | 12.8 | B | 21.6 | 12.8 | * |
| * | 8 | 1 | 500. | 0. | 171. | 792. | 0. | 171. | 792. | 1500. | 0. | 0. | .53 | 62. | 12.8 | B | 21.6 | 12.8 | * |
| * | 9 | 1 | 2300. | 0. | 0. | 621. | 0. | 0. | 621. | 1500. | 0. | 0. | .41 | 62. | 10.0 | A | 21.6 | 12.8 | * |
| * | 10 | 1 | 250. | 37. | 0. | 658. | 37. | 0. | 658. | 1500. | 0. | 0. | .44 | 62. | 10.6 | A | 21.6 | 12.8 | * |
| * | 11 | 1 | 200. | 0. | 0. | 658. | 0. | 0. | 658. | 1500. | 0. | 0. | .44 | 62. | 10.6 | A | 21.6 | 12.8 | * |
| * | 12 | 1 | 250. | 0. | 214. | 658. | 0. | 214. | 658. | 1500. | 0. | 0. | .44 | 62. | 10.6 | A | 21.6 | 12.8 | * |
| * | 13 | 1 | 50. | 0. | 24. | 444. | 0. | 24. | 444. | 1500. | 0. | 0. | .30 | 62. | 7.2 | A | 21.6 | 12.8 | * |
| * | 14 | 1 | 50. | 0. | 0. | 420. | 0. | 0. | 420. | 1500. | 0. | 0. | .28 | 62. | 6.8 | A | 21.6 | 12.8 | * |
| * | 15 | 1 | 1000. | 25. | 0. | 446. | 25. | 0. | 446. | 1500. | 0. | 0. | .30 | 62. | 7.2 | A | 21.6 | 12.8 | * |
| * | 16 | 1 | 10. | 0. | 0. | 446. | 0. | 0. | 446. | 1500. | 0. | 0. | .30 | 62. | 7.2 | A | 21.6 | 12.8 | * |
| * | 17 | 1 | 1500. | 120. | 0. | 566. | 120. | 0. | 566. | 1500. | 0. | 0. | .38 | 62. | 9.1 | A | 21.6 | 12.8 | * |
| * | 18 | 1 | 1500. | 0. | 68. | 566. | 0. | 68. | 566. | 1500. | 0. | 0. | .38 | 62. | 9.1 | A | 21.6 | 12.8 | * |
| * | 19 | 1 | 12000. | 0. | 497. | 497. | 0. | 497. | 497. | 1500. | 0. | 0. | .33 | 62. | 8.0 | A | 21.6 | 12.8 | * |
| * | 20 | | | | | | | | | | | | | | | | | | * |
| ***** | | | | | | | | | | | | | | | | | | | |
| * | TOTAL | 36310. | = | 6.9 | MI | LES | | | | MAX(V/C) = 0.53 | LOWEST LOS = B | AVG = 62. | 10.2 | | | 21.6 | 12.8 | * | |
| ***** | | | | | | | | | | | | | | | | | | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 35. VEH-HRS | 70. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 35. VEH-HRS | 70. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 2175. VEH-MI. | 4351. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 62. MPH. |
| AVERAGE DENSITY = | 10. VPMP | 10. VPMP |
| TOTAL FUEL = | 101. GALLONS | 396. GALLONS |
| TOTAL EMISSIONS = | 28. KILOGRAMS | 109. KILOGRAMS |

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 TIME SLICE 4 OF 6

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.57 | 4 | 0.08 | 5 | 0.07 |
| 6 | 0.08 | 7 | 0.07 | 8 | 0.03 | 9 | 0.10 | 10 | 0.01 |
| 11 | 0.01 | 12 | 0.01 | 13 | 0.00 | 14 | 0.00 | 15 | 0.03 |
| 16 | 0.00 | 17 | 0.06 | 18 | 0.06 | 19 | 0.42 | 20 | 0.00 |

***** TOTAL DELAY = 1.6 VEH-HRS ***** AVERAGE DELAY = 0.15 MIN/VEH *****

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 TIME SLICE 5 OF 6

 ** **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 ** **

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | | |
|--------------|---------------------|------|------|------|------|------|------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| 1 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | 0.00 | 3.15 | 3.70 | 3.71 | 3.90 | 4.46 | 6.66 | 0.00 |
| 3 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.44 | 4.64 | 0.00 |
| 4 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 4.11 | 0.00 |
| 5 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.08 | 0.00 |
| 6 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.93 | 0.00 |
| 7 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.75 | 0.00 |
| 8 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 5 OF 6

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB SEC | NO. LNS | SSEC LENGTH | O-D ORG | DATA DES | DEMANDS SSEC | ADJUSTED ORG | VOLUMES DES | SSEC CAP | WEAVE EFF | CONGEST LENGTH | STORAGE RATE | V/C RATIO | SPEED MPH | DENSITY VPMP | LOS LEVEL | FUEL MPG | EMI SS GS/VM |
|---------|---------|-------------|---------|----------|--------------|--------------|-------------|----------|-----------|-----------------|--------------|----------------|-----------|--------------|-----------|----------|--------------|
| 1 | | | | | | | | | | | | | | | | | |
| 2 | | | | | | | | | | | | | | | | | |
| 3 | 1 | 11000. | 645. | 0. | 645. | 645. | 0. | 645. | 1500. | 0. | 0. | .43 | 62. | 10.4 | A | 21.6 | 12.8 |
| 4 | 1 | 1500. | 5. | 0. | 649. | 5. | 0. | 649. | 1500. | 0. | 0. | .43 | 62. | 10.5 | A | 21.6 | 12.8 |
| 5 | 1 | 1400. | 0. | 0. | 649. | 0. | 0. | 649. | 1500. | 0. | 0. | .43 | 62. | 10.5 | A | 21.6 | 12.8 |
| 6 | 1 | 1500. | 31. | 0. | 681. | 31. | 0. | 681. | 1500. | 0. | 0. | .45 | 62. | 11.0 | A | 21.6 | 12.8 |
| 7 | 1 | 1300. | 0. | 0. | 681. | 0. | 0. | 681. | 1500. | 0. | 0. | .45 | 62. | 11.0 | A | 21.6 | 12.8 |
| 8 | 1 | 500. | 0. | 140. | 681. | 0. | 140. | 681. | 1500. | 0. | 0. | .45 | 62. | 11.0 | A | 21.6 | 12.8 |
| 9 | 1 | 2300. | 0. | 0. | 541. | 0. | 0. | 541. | 1500. | 0. | 0. | .36 | 62. | 8.7 | A | 21.6 | 12.8 |
| 10 | 1 | 250. | 28. | 0. | 569. | 28. | 0. | 569. | 1500. | 0. | 0. | .38 | 62. | 9.2 | A | 21.6 | 12.8 |
| 11 | 1 | 200. | 0. | 0. | 569. | 0. | 0. | 569. | 1500. | 0. | 0. | .38 | 62. | 9.2 | A | 21.6 | 12.8 |
| 12 | 1 | 250. | 0. | 180. | 569. | 0. | 180. | 569. | 1500. | 0. | 0. | .38 | 62. | 9.2 | A | 21.6 | 12.8 |
| 13 | 1 | 50. | 0. | 50. | 389. | 0. | 50. | 389. | 1500. | 0. | 0. | .26 | 62. | 6.3 | A | 21.6 | 12.8 |
| 14 | 1 | 50. | 0. | 0. | 339. | 0. | 0. | 339. | 1500. | 0. | 0. | .23 | 62. | 5.5 | A | 21.6 | 12.8 |
| 15 | 1 | 1000. | 52. | 0. | 391. | 52. | 0. | 391. | 1500. | 0. | 0. | .26 | 62. | 6.3 | A | 21.6 | 12.8 |
| 16 | 1 | 10. | 0. | 0. | 391. | 0. | 0. | 391. | 1500. | 0. | 0. | .26 | 62. | 6.3 | A | 21.6 | 12.8 |
| 17 | 1 | 1500. | 116. | 0. | 507. | 116. | 0. | 507. | 1500. | 0. | 0. | .34 | 62. | 8.2 | A | 21.6 | 12.8 |
| 18 | 1 | 1500. | 0. | 51. | 507. | 0. | 51. | 507. | 1500. | 0. | 0. | .34 | 62. | 8.2 | A | 21.6 | 12.8 |
| 19 | 1 | 12000. | 0. | 456. | 456. | 0. | 456. | 456. | 1500. | 0. | 0. | .30 | 62. | 7.4 | A | 21.6 | 12.8 |
| 20 | | | | | | | | | | | | | | | | | |
| TOTAL | 36310. | = | 6.9 | MI | LES | | | | | MAX(V/C) = 0.45 | | LOWEST LOS = A | AVG = 62. | 9.0 | | 21.6 | 12.8 |

| | | | |
|-----------------------------|--------------------|----------------|--------------------------------|
| | CURRENT TIME SLICE | | CUMULATIVE VALUES |
| FREWAY TRAVEL TIME = | 31. VEH-HRS | 62. PASS-HRS | 169. VEH-HRS 337. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 31. VEH-HRS | 62. PASS-HRS | 169. VEH-HRS 337. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 1922. VEH-MI. | 3844. PASS-MI. | 10462. VEH-MI. 20924. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | | 62. MPH. |
| AVERAGE DENSITY = | 9. VPMP | | 10. VPMP |
| TOTAL FUEL = | 89. GALLONS | | 485. GALLONS |
| TOTAL EMISSIONS = | 25. KILOGRAMS | | 134. KILOGRAMS |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/30/2016 12:57 PAGE 17
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE TIME SLICE 5 OF 6

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.50 | 4 | 0.07 | 5 | 0.06 |
| 6 | 0.07 | 7 | 0.06 | 8 | 0.02 | 9 | 0.09 | 10 | 0.01 |
| 11 | 0.01 | 12 | 0.01 | 13 | 0.00 | 14 | 0.00 | 15 | 0.03 |
| 16 | 0.00 | 17 | 0.05 | 18 | 0.05 | 19 | 0.39 | 20 | 0.00 |

***** TOTAL DELAY = 1.4 VEH-HRS ***** AVERAGE DELAY = 0.15 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/30/2016 12:57 PAGE 18
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE TIME SLICE 6 OF 6

 ** FREWAY TRAVEL TIME (MINUTES) **

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | | |
|--------------|---------------------|------|------|------|------|------|------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 3.15 | 3.70 | 3.71 | 3.90 | 4.46 | 6.66 | 0.00 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.44 | 4.64 | 0.00 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 4.11 | 0.00 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.08 | 0.00 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.93 | 0.00 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.75 | 0.00 |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI | | | | |
|---------|--------|----------|--------------|------------------|------|-------|---------|---------|-----------------|-------|---------|----------------|------|-------|-----------|-----|------|------|
| SEC | LNS | LENGTH | ORG DES SSEC | ORG DES SSEC | CAP | EFF | LENGTH | RATE | RATIO | MPH | VPMPL | LEVEL | MPG | SS/VM | | | | |
| 1 | | | | | | | | | | | | | | | | | | |
| 2 | | | | | | | | | | | | | | | | | | |
| 3 | 1 | 11000. | 645. | 0. | 645. | 645. | 0. | 645. | 1500. | 0. | 0. | 0. | .43 | 62. | 10.4 | A | 21.6 | 12.8 |
| 4 | 1 | 1500. | 5. | 0. | 649. | 5. | 0. | 649. | 1500. | 0. | 0. | 0. | .43 | 62. | 10.5 | A | 21.6 | 12.8 |
| 5 | 1 | 1400. | 0. | 0. | 649. | 0. | 0. | 649. | 1500. | 0. | 0. | 0. | .43 | 62. | 10.5 | A | 21.6 | 12.8 |
| 6 | 1 | 1500. | 31. | 0. | 681. | 31. | 0. | 681. | 1500. | 0. | 0. | 0. | .45 | 62. | 11.0 | A | 21.6 | 12.8 |
| 7 | 1 | 1300. | 0. | 0. | 681. | 0. | 0. | 681. | 1500. | 0. | 0. | 0. | .45 | 62. | 11.0 | A | 21.6 | 12.8 |
| 8 | 1 | 500. | 0. | 140. | 681. | 0. | 140. | 681. | 1500. | 0. | 0. | 0. | .45 | 62. | 11.0 | A | 21.6 | 12.8 |
| 9 | 1 | 2300. | 0. | 0. | 541. | 0. | 0. | 541. | 1500. | 0. | 0. | 0. | .36 | 62. | 8.7 | A | 21.6 | 12.8 |
| 10 | 1 | 250. | 28. | 0. | 569. | 28. | 0. | 569. | 1500. | 0. | 0. | 0. | .38 | 62. | 9.2 | A | 21.6 | 12.8 |
| 11 | 1 | 200. | 0. | 0. | 569. | 0. | 0. | 569. | 1500. | 0. | 0. | 0. | .38 | 62. | 9.2 | A | 21.6 | 12.8 |
| 12 | 1 | 250. | 0. | 180. | 569. | 0. | 180. | 569. | 1500. | 0. | 0. | 0. | .38 | 62. | 9.2 | A | 21.6 | 12.8 |
| 13 | 1 | 50. | 0. | 50. | 389. | 0. | 50. | 389. | 1500. | 0. | 0. | 0. | .26 | 62. | 6.3 | A | 21.6 | 12.8 |
| 14 | 1 | 50. | 0. | 0. | 339. | 0. | 0. | 339. | 1500. | 0. | 0. | 0. | .23 | 62. | 5.5 | A | 21.6 | 12.8 |
| 15 | 1 | 1000. | 52. | 0. | 391. | 52. | 0. | 391. | 1500. | 0. | 0. | 0. | .26 | 62. | 6.3 | A | 21.6 | 12.8 |
| 16 | 1 | 10. | 0. | 0. | 391. | 0. | 0. | 391. | 1500. | 0. | 0. | 0. | .26 | 62. | 6.3 | A | 21.6 | 12.8 |
| 17 | 1 | 1500. | 116. | 0. | 507. | 116. | 0. | 507. | 1500. | 0. | 0. | 0. | .34 | 62. | 8.2 | A | 21.6 | 12.8 |
| 18 | 1 | 1500. | 0. | 51. | 507. | 0. | 51. | 507. | 1500. | 0. | 0. | 0. | .34 | 62. | 8.2 | A | 21.6 | 12.8 |
| 19 | 1 | 12000. | 0. | 456. | 456. | 0. | 456. | 456. | 1500. | 0. | 0. | 0. | .30 | 62. | 7.4 | A | 21.6 | 12.8 |
| 20 | | | | | | | | | | | | | | | | | | |
| TOTAL | 36310. | = | 6.9 | MI LBS | | | | | MAX(V/C) = 0.45 | | | LOWEST LOS = A | | | AVG = 62. | 9.0 | 21.6 | 12.8 |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 31. VEH-HRS | 62. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 31. VEH-HRS | 62. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 1922. VEH-MI. | 3844. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | 62. MPH. |
| AVERAGE DENSITY = | 9. VPMPL | 10. VPMPL |
| TOTAL FUEL = | 89. GALLONS | 575. GALLONS |
| TOTAL EMISSIONS = | 25. KILOGRAMS | 158. KILOGRAMS |

***** MAINTENANCE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.50 | 4 | 0.07 | 5 | 0.06 |
| 6 | 0.07 | 7 | 0.06 | 8 | 0.02 | 9 | 0.09 | 10 | 0.01 |
| 11 | 0.01 | 12 | 0.01 | 13 | 0.00 | 14 | 0.00 | 15 | 0.03 |
| 16 | 0.00 | 17 | 0.05 | 18 | 0.05 | 19 | 0.39 | 20 | 0.00 |

***** TOTAL DELAY = 1.4 VEH-HRS ***** AVERAGE DELAY = 0.15 MIN/VEH *****

```

FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ      1111      222222  PPPPPPPP  EEEEEEEEE
FFFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111  222 222  PPPPPPPP  EEEEEEEEE
FFF       RRR   RRR  EEE      QQQQQ  QQQQQ  1111   222 222  PPP   PPP  EEE
FFF       RRR   RRR  EEE      QQQQ   QQQQ   1111   222 222  PPP   PPP  EEE
FFFFFFFFF RRRRRRRR EEEEEEE   QQQQ   QQQQ   1111           222  PPPPPPPP  EEEEEEE
FFFFFFFFF RRRRRRRR EEEEEEE   QQQQ   QQQQ   1111           2222  PPPPPPPP  EEEEEEE
FFF       RRR   RRR  EEE      QQQQ   QQQ   QQQ  1111           2222  PPP   EEE
FFF       RRR   RRR  EEE      Q*UC*   QQQQ   1111           222  PPP   EEE
FFF       RRR   RRR  EEEEEEEEE Q*REGENTS*Q  1111           222  PPP   EEEEEEEEE
FFF       RRR   RRR  EEEEEEEEE Q*1999*Q QQQ 11111111 2222222222  PPP   EEEEEEEEE
    
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FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 2.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 30
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT TRUCKS | DES TRUCKS | SPECIAL RAMP | FF. SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION LOCATION |
|---------|----------|----------|-------------|--------------|---------|---------|-----------|---------|------------|------------|--------------|-------------------|---------------|----------|----------------|--------------------------|
| ** 1 | 3 | 6000. | 500. | 65 | 0 | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Seed |
| ** 2 | 3 | 6000. | 99999. | 65 | D | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture |
| ** 3 | 2 | 4000. | 11000. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** 4 | 2 | 4000. | 1500. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence On-ramp |
| ** 5 | 2 | 4000. | 1400. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence to Crossman |
| ** 6 | 2 | 4000. | 1500. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Crossman On-Ramp |
| ** 7 | 2 | 4000. | 1300. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Crossman / Mathilda |
| ** 8 | 3 | 5270. | 500. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-Ramp |
| ** 9 | 2 | 4000. | 2300. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda |
| ** 10 | 3 | 4860. | 250. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda On-ramp |
| ** 11 | 3 | 4860. | 200. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda to US-101 |
| ** 12 | 3 | 4860. | 250. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US-101 Off-Ramp |
| ** 13 | 2 | 4000. | 50. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bottleneck by-pass |
| ** 14 | 2 | 2470. | 50. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bottleneck |
| ** 15 | 2 | 4000. | 1000. | 62 | OD | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US 101 / US 101 |
| ** 16 | 2 | 4000. | 10. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Dummy end of travel time |
| ** 17 | 2 | 4000. | 1500. | 62 | 0 | 0.95 | 0.0 | 5 | 0 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US 101 NB On-Ramp |
| ** 18 | 2 | 4000. | 1500. | 62 | D | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Maude Off-ramp |
| ** 19 | 2 | 4000. | 12000. | 62 | | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** 20 | 3 | 6000. | 500. | 65 | OD | 0.95 | 0.0 | 5 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End of Network |

1 INSTITUTE OF TRANSPORTATION STUDIES
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***** INPUT HAS BEEN COMPLETED *****

1 INSTITUTE OF TRANSPORTATION STUDIES
UNIVERSITY OF CALIFORNIA, BERKELEY

FREQ12PE REL 3.01
SIMULATION AFTER CONTROL, NO DIVERSION
TIME SLICE 1 OF 6

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**
** FREEWAY TRAVEL TIME (MINUTES)
**

| * ORIGIN DOWN | * DESTINATIONS ACROSS * | | | | | | |
|---------------|-------------------------|-------|-------|-------|-------|-------|-------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 17.79 | 23.94 | 24.49 | 24.50 | 24.70 | 25.25 | 27.53 |
| * 2 * | 0.00 | 2.60 | 3.15 | 3.16 | 3.36 | 3.91 | 6.19 |
| * 3 * | 0.00 | 0.70 | 1.25 | 1.26 | 1.46 | 2.01 | 4.29 |
| * 4 * | 0.00 | 0.00 | 0.13 | 0.14 | 0.33 | 0.88 | 3.17 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.18 | 0.73 | 3.02 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.55 | 2.84 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.09 |

1 INSTITUTE OF TRANSPORTATION STUDIES
UNIVERSITY OF CALIFORNIA, BERKELEY

FREQ12PE REL 3.01
SIMULATION AFTER CONTROL, NO DIVERSION
TIME SLICE 1 OF 6

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* TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB NO. | * SEC | * LNS | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | |
|-----------|-------|--------|--------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|-------|---------|-----------|-------|--------|-------------|------|
| | | | | ORG | DES | ORG | DES | CAP | EFF | LENGTH | RATE | RATIO | MPH | VPMP | LEVEL | MPG | GS/VM | |
| * 1 | 3 | 500. | 4499. | 0. | 4499. | 4499. | 0. | 4499. | 6000. | 0. | 0. | 0. | .75 | 64. | 23.4 | C | 19.3 | 13.8 |
| * 2 | 3 | 99999. | 0. | 720. | 4499. | 0. | 720. | 4499. | 6000. | 0. | 0. | 0. | .75 | 64. | 23.4 | C | 19.3 | 13.8 |
| * 3 | 2 | 11000. | 0. | 0. | 3779. | 0. | 0. | 3215. | 4000. | 0. | * 7143. | 564. | .80 | 35. | 45.6 | F | 20.8 | 13.1 |
| * 4 | 2 | 1500. | 55. | 0. | 3834. | 55. | 0. | 3270. | 3996. | 0. | ** 1500. | 564. | .82 | 18. | 88.4 | F | 17.4 | 17.0 |
| * 5 | 2 | 1400. | 0. | 0. | 3834. | 0. | 0. | 3270. | 4000. | 0. | ** 1400. | 564. | .82 | 16. | 100.5 | F | 16.6 | 18.1 |
| * 6 | 2 | 1500. | 686. | 0. | 4520. | 686. | 0. | 3956. | 3956. | 0. | 0. | 1.00 | 52. | 38.4 | E | 23.6 | 11.1 | |
| * 7 | 2 | 1300. | 0. | 0. | 4520. | 0. | 0. | 3956. | 4000. | 0. | 0. | .99 | 52. | 37.7 | E | 23.4 | 11.2 | |
| * 8 | 3 | 500. | 0. | 1038. | 4520. | 0. | 910. | 3956. | 5107. | 0. | 0. | .77 | 62. | 21.3 | C | 20.3 | 13.0 | |
| * 9 | 2 | 2300. | 0. | 0. | 3482. | 0. | 0. | 3046. | 4000. | 0. | 0. | .76 | 62. | 24.6 | C | 20.3 | 13.0 | |
| * 10 | 3 | 250. | 507. | 0. | 3989. | 507. | 0. | 3553. | 4817. | 0. | 0. | .74 | 62. | 19.1 | C | 20.3 | 13.0 | |
| * 11 | 3 | 200. | 0. | 0. | 3989. | 0. | 0. | 3553. | 4860. | 0. | 0. | .73 | 62. | 19.1 | C | 20.3 | 13.0 | |
| * 12 | 3 | 250. | 0. | 1768. | 3989. | 0. | 1579. | 3553. | 4619. | 0. | 0. | .77 | 62. | 19.1 | C | 20.3 | 13.0 | |
| * 13 | 2 | 50. | 0. | 43. | 2221. | 0. | 38. | 1974. | 3994. | 0. | 0. | .49 | 62. | 15.9 | B | 20.3 | 13.0 | |
| * 14 | 2 | 50. | 0. | 0. | 2178. | 0. | 0. | 1936. | 2470. | 0. | 0. | .78 | 62. | 15.6 | B | 20.3 | 13.0 | |
| * 15 | 2 | 1000. | 43. | 0. | 2221. | 43. | 0. | 1979. | 3993. | 0. | 0. | .50 | 62. | 16.0 | B | 20.3 | 13.0 | |
| * 16 | 2 | 10. | 0. | 0. | 2221. | 0. | 0. | 1979. | 4000. | 0. | 0. | .49 | 62. | 16.0 | B | 20.3 | 13.0 | |
| * 17 | 2 | 1500. | 749. | 0. | 2970. | 749. | 0. | 2728. | 3879. | 0. | 0. | .70 | 62. | 22.0 | C | 20.3 | 13.0 | |
| * 18 | 2 | 1500. | 0. | 406. | 2970. | 0. | 375. | 2728. | 3960. | 0. | 0. | .69 | 62. | 22.0 | C | 20.3 | 13.0 | |
| * 19 | 2 | 12000. | 0. | 0. | 2564. | 0. | 0. | 2353. | 4000. | 0. | 0. | .59 | 62. | 19.0 | C | 20.3 | 13.0 | |
| * 20 | 3 | 500. | 488. | 3052. | 3052. | 488. | 2841. | 2841. | 6000. | 0. | 0. | .47 | 65. | 14.6 | B | 19.0 | 14.1 | |

* TOTAL 137309. = 26.0 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 58. 26.4 19.5 13.7 *

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|----------------------------|--------------------|-----------------|-------------------|-----------------|
| FREWAY TRAVEL TIME = | 927. VEH-HRS | 1035. PASS-HRS | 927. VEH-HRS | 1035. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 927. VEH-HRS | 1035. PASS-HRS | 927. VEH-HRS | 1035. PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 53461. VEH-MI. | 60385. PASS-MI. | 53461. VEH-MI. | 60385. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 58. MPH. | | 58. MPH. | |

SR-237_WB_PM_P2_2040_PE
 AVERAGE DENSITY = 26. VPML
 TOTAL FUEL = 2736. GALLONS
 TOTAL EMISSIONS = 732. KI LOGRAMS

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DI VERSION
 TIME SLICE 1 OF 6

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.04 | 2 | 8.31 | 3 | 49.39 | 4 | 18.61 | 5 | 20.20 |
| 6 | 2.25 | 7 | 1.80 | 8 | 0.14 | 9 | 0.49 | 10 | 0.06 |
| 11 | 0.05 | 12 | 0.06 | 13 | 0.01 | 14 | 0.01 | 15 | 0.14 |
| 16 | 0.00 | 17 | 0.29 | 18 | 0.29 | 19 | 1.99 | 20 | 0.00 |

***** TOTAL DELAY = 104.1 VEH-HRS ***** AVERAGE DELAY = 1.89 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 3/30/2016 16:20 PAGE 7
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DI VERSION
 TIME SLICE 2 OF 6

 ** FREeway TRAVEL TIME (MINUTES) **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN 1 2 3 4 5 6 7 *

| ORIGINS DOWN | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
|--------------|-------|-------|-------|-------|-------|-------|-------|
| 1 | 18.51 | 29.37 | 29.92 | 29.93 | 30.12 | 30.67 | 32.96 |
| 2 | 0.00 | 2.85 | 3.40 | 3.41 | 3.60 | 4.15 | 6.44 |
| 3 | 0.00 | 0.70 | 1.25 | 1.26 | 1.46 | 2.01 | 4.29 |
| 4 | 0.00 | 0.00 | 0.13 | 0.14 | 0.33 | 0.88 | 3.17 |
| 5 | 0.00 | 0.00 | 0.00 | 0.00 | 0.18 | 0.73 | 3.02 |
| 6 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.55 | 2.84 |
| 7 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.09 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 3/30/2016 16:20 PAGE 8
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DI VERSION
 TIME SLICE 2 OF 6

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS |
|---------|--------|---------------|----------------|------------------|----------|-------------|------------|-----------|-------|-------|---------|-------|------|--------|
| SEC LNS | LENGTH | ORG DES | SSEC | ORG DES SSEC | CAP. | EFF | LENGTH | RATE | RATIO | MPH | VPML | LEVEL | MPG | GS/VM |
| * 1 3 | 500. | 4499. | 0. 4499. | 4499. | 0. 4499. | 6000. | 0. 0. | 0. 0. | .75 | 64. | 23.4 | C | 19.3 | 13.8 |
| * 2 3 | 99999. | 0. 720. | 4499. | 0. 720. | 3935. | 6000. | 0. * 2558. | 564. .66 | 62. | 21.3 | F | 19.2 | 13.9 | |
| * 3 2 | 11000. | 0. 0. 3779. | 0. 0. 3779. | 0. 0. 3215. | 4000. | 0. **11000. | 564. .80 | 16. 103.0 | F | 16.2 | 18.6 | * | 16.2 | 18.6 |
| * 4 2 | 1500. | 55. 0. 3834. | 55. 0. 3834. | 0. 0. 3270. | 3996. | 0. ** 1500. | 564. .82 | 15. 106.1 | F | 16.2 | 18.7 | * | 16.2 | 18.7 |
| * 5 2 | 1400. | 0. 0. 3834. | 0. 0. 3834. | 0. 0. 3270. | 4000. | 0. ** 1400. | 564. .82 | 15. 106.4 | F | 16.2 | 18.7 | * | 16.2 | 18.7 |
| * 6 2 | 1500. | 686. 0. 4520. | 686. 0. 4520. | 0. 0. 3956. | 3956. | 0. 0. 0. | 1.00 | 52. 38.4 | E | 23.6 | 11.1 | * | 23.6 | 11.1 |
| * 7 2 | 1300. | 0. 0. 4520. | 0. 0. 4520. | 0. 0. 3956. | 4000. | 0. 0. 0. | .99 | 52. 37.7 | E | 23.4 | 11.2 | * | 23.4 | 11.2 |
| * 8 3 | 500. | 0. 1038. | 4520. 0. 910. | 3956. 5107. | 0. 0. 0. | .77 | 62. 21.3 | C | 20.3 | 13.0 | * | 20.3 | 13.0 | |
| * 9 2 | 2300. | 0. 0. 3482. | 0. 0. 3482. | 0. 0. 3046. | 4000. | 0. 0. 0. | .76 | 62. 24.6 | C | 20.3 | 13.0 | * | 20.3 | 13.0 |
| * 10 3 | 250. | 507. 0. 3989. | 507. 0. 3989. | 0. 0. 3553. | 4817. | 0. 0. 0. | .74 | 62. 19.1 | C | 20.3 | 13.0 | * | 20.3 | 13.0 |
| * 11 3 | 200. | 0. 0. 3989. | 0. 0. 3989. | 0. 0. 3553. | 4860. | 0. 0. 0. | .73 | 62. 19.1 | C | 20.3 | 13.0 | * | 20.3 | 13.0 |
| * 12 3 | 250. | 0. 1768. | 3989. 0. 1579. | 3553. 4619. | 0. 0. 0. | .77 | 62. 19.1 | C | 20.3 | 13.0 | * | 20.3 | 13.0 | |
| * 13 2 | 50. | 0. 43. 2221. | 0. 43. 2221. | 0. 38. 1974. | 3994. | 0. 0. 0. | .49 | 62. 15.9 | B | 20.3 | 13.0 | * | 20.3 | 13.0 |
| * 14 2 | 50. | 0. 0. 2178. | 0. 0. 2178. | 0. 0. 1936. | 2470. | 0. 0. 0. | .78 | 62. 15.6 | B | 20.3 | 13.0 | * | 20.3 | 13.0 |
| * 15 2 | 1000. | 43. 0. 2221. | 43. 0. 2221. | 0. 0. 1979. | 3993. | 0. 0. 0. | .50 | 62. 16.0 | B | 20.3 | 13.0 | * | 20.3 | 13.0 |
| * 16 2 | 10. | 0. 0. 2221. | 0. 0. 2221. | 0. 0. 1979. | 4000. | 0. 0. 0. | .49 | 62. 16.0 | B | 20.3 | 13.0 | * | 20.3 | 13.0 |
| * 17 2 | 1500. | 749. 0. 2970. | 749. 0. 2970. | 0. 0. 2728. | 3879. | 0. 0. 0. | .70 | 62. 22.0 | C | 20.3 | 13.0 | * | 20.3 | 13.0 |
| * 18 2 | 1500. | 0. 406. | 2970. 0. 375. | 2728. 3960. | 0. 0. 0. | .69 | 62. 22.0 | C | 20.3 | 13.0 | * | 20.3 | 13.0 | |
| * 19 2 | 12000. | 0. 0. 2564. | 0. 0. 2564. | 0. 0. 2353. | 4000. | 0. 0. 0. | .59 | 62. 19.0 | C | 20.3 | 13.0 | * | 20.3 | 13.0 |
| * 20 3 | 500. | 488. 3052. | 3052. 488. | 2841. 2841. | 6000. | 0. 0. 0. | .47 | 65. 14.6 | B | 19.0 | 14.1 | * | 19.0 | 14.1 |

* TOTAL 137309. = 26.0 MI LBS MAX(V/C) = 1.00 LOWEST LOS = F AVG = 50. 29.8 19.1 14.1 *

```

*****
CURRENT TIME SLICE                CUMULATIVE VALUES
FREEWAY TRAVEL TIME = 1068. VEH-HRS 1180. PASS-HRS 1994. VEH-HRS 2215. PASS-HRS
FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 1068. VEH-HRS 1180. PASS-HRS 1994. VEH-HRS 2215. PASS-HRS
TOTAL TRAV DISTANCE = 52989. VEH-MI. 59906. PASS-MI. 106450. VEH-MI. 120292. PASS-MI.
AVERAGE SYSTEM SPEED = 50. MPH. 53. MPH.
AVERAGE DENSITY = 30. VPML 28. VPML
TOTAL FUEL = 2771. GALLONS 5508. GALLONS
TOTAL EMISSIONS = 748. KI LOGRAMS 1479. KI LOGRAMS
    
```

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 6

```

***** MAINTLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
1 0.04 2 35.15 3 165.08 4 23.01 5 21.55
6 2.25 7 1.80 8 0.14 9 0.49 10 0.06
11 0.05 12 0.06 13 0.01 14 0.01 15 0.14
16 0.00 17 0.29 18 0.29 19 1.99 20 0.00
***** TOTAL DELAY = 252.4 VEH-HRS ***** AVERAGE DELAY = 4.58 MIN/VEH *****
    
```

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 3/30/2016 16:20 PAGE 10
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 3 OF 6

```

*****
**
** FREEWAY TRAVEL TIME (MINUTES) **
**
*****
    
```

```

*****
* ORIGINS DESTINATIONS ACROSS *
* DOWN 1 2 3 4 5 6 7 *
+
* * * * *
+
* 1 * 22.84 34.98 35.53 35.53 35.73 36.28 38.57 *
+
* 2 * 0.00 2.99 3.54 3.55 3.74 4.29 6.58 *
+
* 3 * 0.00 0.70 1.25 1.26 1.46 2.01 4.29 *
+
* 4 * 0.00 0.00 0.13 0.14 0.33 0.88 3.17 *
+
* 5 * 0.00 0.00 0.00 0.00 0.18 0.73 3.02 *
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.55 2.84 *
+
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.09 *
+
* * * * *
*****
    
```

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 3/30/2016 16:20 PAGE 11
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 3 OF 6

TIME SLICE FREEWAY PERFORMANCE TABLE

```

*****
* SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMISSIONS *
* SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPML LEVEL MPG GS/VM *
*****
* 1 3 500. 4630. 0. 4630. 4630. 0. 4630. 6000. 0. 0. 0. .77 64. 24.2 C 19.5 13.7 *
* 2 3 99999. 0. 741. 4630. 0. 741. 3866. 6000. 0. * 8162. 764. .64 50. 25.8 F 18.9 14.1 *
* 3 2 11000. 0. 0. 3889. 0. 0. 3125. 4000. 0. **11000. 764. .78 14. 114.3 F 15.1 20.0 *
* 4 2 1500. 64. 0. 3953. 64. 0. 3189. 3995. 0. ** 1500. 764. .80 14. 110.5 F 15.6 19.4 *
* 5 2 1400. 0. 0. 3953. 0. 0. 3189. 4000. 0. ** 1400. 764. .80 14. 110.8 F 15.6 19.4 *
* 6 2 1500. 764. 0. 4717. 764. 0. 3953. 3953. 0. 0. 1.00 52. 38.3 E 23.6 11.1 *
* 7 2 1300. 0. 0. 4717. 0. 0. 3953. 4000. 0. 0. 0. .99 52. 37.7 E 23.4 11.2 *
* 8 3 500. 0. 1099. 4717. 0. 923. 3953. 5099. 0. 0. 0. .78 62. 21.3 C 20.3 13.0 *
* 9 2 2300. 0. 0. 3618. 0. 0. 3030. 4000. 0. 0. 0. .76 62. 24.4 C 20.3 13.0 *
* 10 3 250. 542. 0. 4160. 542. 0. 3572. 4816. 0. 0. 0. .74 62. 19.2 C 20.3 13.0 *
* 11 3 200. 0. 0. 4160. 0. 0. 3572. 4860. 0. 0. 0. .74 62. 19.2 C 20.3 13.0 *
* 12 3 250. 0. 1576. 4160. 0. 1358. 3572. 4649. 0. 0. 0. .77 62. 19.2 C 20.3 13.0 *
* 13 2 50. 0. 176. 2584. 0. 152. 2214. 3976. 0. 0. 0. .56 62. 17.9 B 20.3 13.0 *
*****
    
```

| SR-237_WB_PM_P2_2040_PE | | | | | | | | | | | | | | | | | | |
|-------------------------|---|--------|------|-------|-------|------|-------|-------|-------|----|----|-----|-----|------|---|------|------|---|
| * 14 | 2 | 50. | 0. | 0. | 2408. | 0. | 0. | 2063. | 2470. | 0. | 0. | .84 | 62. | 16.6 | B | 20.3 | 13.0 | * |
| * 15 | 2 | 1000. | 174. | 0. | 2582. | 174. | 0. | 2237. | 3974. | 0. | 0. | .56 | 62. | 18.0 | C | 20.3 | 13.0 | * |
| * 16 | 2 | 10. | 0. | 0. | 2582. | 0. | 0. | 2237. | 4000. | 0. | 0. | .56 | 62. | 18.0 | C | 20.3 | 13.0 | * |
| * 17 | 2 | 1500. | 823. | 0. | 3405. | 823. | 0. | 3060. | 3879. | 0. | 0. | .79 | 62. | 24.7 | C | 20.3 | 13.0 | * |
| * 18 | 2 | 1500. | 0. | 732. | 3405. | 0. | 663. | 3060. | 3932. | 0. | 0. | .78 | 62. | 24.7 | C | 20.3 | 13.0 | * |
| * 19 | 2 | 12000. | 0. | 0. | 2673. | 0. | 0. | 2397. | 4000. | 0. | 0. | .60 | 62. | 19.3 | C | 20.3 | 13.0 | * |
| * 20 | 3 | 500. | 509. | 3182. | 3182. | 509. | 2906. | 2906. | 6000. | 0. | 0. | .48 | 65. | 14.9 | B | 19.0 | 14.1 | * |

 * TOTAL 137309. = 26.0 MI LBS MAX(V/C) = 1.00 LOWEST LOS = F AVG = 42. 34.2 18.8 14.4 *

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------------------|----------------------------------|
| FREEWAY TRAVEL TIME = | 1274. VEH-HRS 1415. PASS-HRS | 3268. VEH-HRS 3629. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1274. VEH-HRS 1415. PASS-HRS | 3268. VEH-HRS 3629. PASS-HRS |
| TOTAL TRAV DISTANCE = | 53904. VEH-MI. 60968. PASS-MI. | 160353. VEH-MI. 181259. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 42. MPH. | 49. MPH. |
| AVERAGE DENSITY = | 34. VPMP | 30. VPMP |
| TOTAL FUEL = | 2872. GALLONS | 8380. GALLONS |
| TOTAL EMISSIONS = | 777. KI LOGRAMS | 2256. KI LOGRAMS |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 3/30/2016 16:20 PAGE 12
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 3 OF 6

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|--------|------------|--------|------------|-------|------------|-------|
| 1 | 0.06 | 2 | 201.42 | 3 | 188.10 | 4 | 24.42 | 5 | 22.88 |
| 6 | 2.25 | 7 | 1.79 | 8 | 0.14 | 9 | 0.49 | 10 | 0.06 |
| 11 | 0.05 | 12 | 0.06 | 13 | 0.01 | 14 | 0.01 | 15 | 0.16 |
| 16 | 0.00 | 17 | 0.32 | 18 | 0.32 | 19 | 2.03 | 20 | 0.00 |

***** TOTAL DELAY = 444.6 VEH-HRS ***** AVERAGE DELAY = 7.77 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 3/30/2016 16:20 PAGE 13
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 4 OF 6

 ** FREEWAY TRAVEL TIME (MINUTES) **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN *
 * 1 2 3 4 5 6 7 *

| | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|
| * 1 * | 28.09 | 40.23 | 40.78 | 40.79 | 40.98 | 41.53 | 43.82 |
| * 2 * | 0.00 | 2.99 | 3.54 | 3.55 | 3.74 | 4.29 | 6.58 |
| * 3 * | 0.00 | 0.70 | 1.25 | 1.26 | 1.46 | 2.01 | 4.29 |
| * 4 * | 0.00 | 0.00 | 0.13 | 0.14 | 0.33 | 0.88 | 3.17 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.18 | 0.73 | 3.02 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.55 | 2.84 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.09 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 3/30/2016 16:20 PAGE 14
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 4 OF 6

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | |
|-----------|--------|------------|-----------|------------|-----------|---------|---------|-----------|-----------|----------|---------|-----------|--------|--------|-------------|--------|---------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 1 | * 3 | * 500. | * 4630. | * 0. | * 4630. | * 4630. | * 0. | * 6000. | * 0. | * 0. | * .77 | * 64. | * 24.2 | * C | * 19.5 | * 13.7 | |

SR-237_WB_PM_P2_2040_PE

| | | | | | | | | | | | | | | | | | | | | | |
|---|----|---|--------|------|-------|-------|------|-------|-------|-------|----|----|--------|------|-----|-----|-------|---|------|------|---|
| * | 2 | 3 | 99999. | 0. | 741. | 4630. | 0. | 741. | 3866. | 6000. | 0. | * | 13767. | 764. | .64 | 41. | 31.8 | F | 18.3 | 14.6 | * |
| * | 3 | 2 | 11000. | 0. | 0. | 3889. | 0. | 0. | 3125. | 4000. | 0. | ** | 11000. | 764. | .78 | 14. | 114.3 | F | 15.1 | 20.0 | * |
| * | 4 | 2 | 1500. | 64. | 0. | 3953. | 64. | 0. | 3189. | 3995. | 0. | ** | 1500. | 764. | .80 | 14. | 110.5 | F | 15.6 | 19.4 | * |
| * | 5 | 2 | 1400. | 0. | 0. | 3953. | 0. | 0. | 3189. | 4000. | 0. | ** | 1400. | 764. | .80 | 14. | 110.8 | F | 15.6 | 19.4 | * |
| * | 6 | 2 | 1500. | 764. | 0. | 4717. | 764. | 0. | 3953. | 3953. | 0. | 0. | 0. | 1.00 | 0. | 52. | 38.3 | E | 23.6 | 11.1 | * |
| * | 7 | 2 | 1300. | 0. | 0. | 4717. | 0. | 0. | 3953. | 4000. | 0. | 0. | 0. | .99 | 0. | 52. | 37.7 | E | 23.4 | 11.2 | * |
| * | 8 | 3 | 500. | 0. | 1099. | 4717. | 0. | 923. | 3953. | 5099. | 0. | 0. | 0. | .78 | 0. | 62. | 21.3 | C | 20.3 | 13.0 | * |
| * | 9 | 2 | 2300. | 0. | 0. | 3618. | 0. | 0. | 3030. | 4000. | 0. | 0. | 0. | .76 | 0. | 62. | 24.4 | C | 20.3 | 13.0 | * |
| * | 10 | 3 | 250. | 542. | 0. | 4160. | 542. | 0. | 3572. | 4816. | 0. | 0. | 0. | .74 | 0. | 62. | 19.2 | C | 20.3 | 13.0 | * |
| * | 11 | 3 | 200. | 0. | 0. | 4160. | 0. | 0. | 3572. | 4860. | 0. | 0. | 0. | .74 | 0. | 62. | 19.2 | C | 20.3 | 13.0 | * |
| * | 12 | 3 | 250. | 0. | 1576. | 4160. | 0. | 1358. | 3572. | 4649. | 0. | 0. | 0. | .77 | 0. | 62. | 19.2 | C | 20.3 | 13.0 | * |
| * | 13 | 2 | 50. | 0. | 176. | 2584. | 0. | 152. | 2214. | 3976. | 0. | 0. | 0. | .56 | 0. | 62. | 17.9 | B | 20.3 | 13.0 | * |
| * | 14 | 2 | 50. | 0. | 0. | 2408. | 0. | 0. | 2063. | 2470. | 0. | 0. | 0. | .84 | 0. | 62. | 16.6 | B | 20.3 | 13.0 | * |
| * | 15 | 2 | 1000. | 174. | 0. | 2582. | 174. | 0. | 2237. | 3974. | 0. | 0. | 0. | .56 | 0. | 62. | 18.0 | C | 20.3 | 13.0 | * |
| * | 16 | 2 | 10. | 0. | 0. | 2582. | 0. | 0. | 2237. | 4000. | 0. | 0. | 0. | .56 | 0. | 62. | 18.0 | C | 20.3 | 13.0 | * |
| * | 17 | 2 | 1500. | 823. | 0. | 3405. | 823. | 0. | 3060. | 3879. | 0. | 0. | 0. | .79 | 0. | 62. | 24.7 | C | 20.3 | 13.0 | * |
| * | 18 | 2 | 1500. | 0. | 732. | 3405. | 0. | 663. | 3060. | 3932. | 0. | 0. | 0. | .78 | 0. | 62. | 24.7 | C | 20.3 | 13.0 | * |
| * | 19 | 2 | 12000. | 0. | 0. | 2673. | 0. | 0. | 2397. | 4000. | 0. | 0. | 0. | .60 | 0. | 62. | 19.3 | C | 20.3 | 13.0 | * |
| * | 20 | 3 | 500. | 509. | 3182. | 3182. | 509. | 2906. | 2906. | 6000. | 0. | 0. | 0. | .48 | 0. | 65. | 14.9 | B | 19.0 | 14.1 | * |

 * TOTAL 137309. = 26.0 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 37. 38.5 18.3 14.8 *

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------------------|----------------------------------|
| FREWAY TRAVEL TIME = | 1465. VEH-HRS 1637. PASS-HRS | 4733. VEH-HRS 5266. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1465. VEH-HRS 1637. PASS-HRS | 4733. VEH-HRS 5266. PASS-HRS |
| TOTAL TRAV DISTANCE = | 53498. VEH-MI. 60497. PASS-MI. | 213852. VEH-MI. 241756. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 37. MPH | 45. MPH |
| AVERAGE DENSITY = | 39. VPMPPL | 32. VPMPPL |
| TOTAL FUEL = | 2923. GALLONS | 11303. GALLONS |
| TOTAL EMISSIONS = | 793. KI LOGRAMS | 3049. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|--------|------------|--------|------------|-------|------------|-------|
| 1 | 0.06 | 2 | 398.66 | 3 | 188.10 | 4 | 24.42 | 5 | 22.88 |
| 6 | 2.25 | 7 | 1.79 | 8 | 0.14 | 9 | 0.49 | 10 | 0.06 |
| 11 | 0.05 | 12 | 0.06 | 13 | 0.01 | 14 | 0.01 | 15 | 0.16 |
| 16 | 0.00 | 17 | 0.32 | 18 | 0.32 | 19 | 2.03 | 20 | 0.00 |

***** TOTAL DELAY = 641.8 VEH-HRS ***** AVERAGE DELAY = 10.83 MIN/VEH *****

 ** FREWAY TRAVEL TIME (MINUTES) **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN 1 2 3 4 5 6 7 *

| | | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|---|
| * 1 * | 31.34 | 41.35 | 41.91 | 41.92 | 42.11 | 42.66 | 44.95 | * |
| * 2 * | 0.00 | 2.56 | 3.12 | 3.13 | 3.32 | 3.87 | 6.16 | * |
| * 3 * | 0.00 | 0.71 | 1.26 | 1.27 | 1.46 | 2.01 | 4.30 | * |
| * 4 * | 0.00 | 0.00 | 0.13 | 0.14 | 0.33 | 0.88 | 3.17 | * |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.18 | 0.73 | 3.02 | * |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.55 | 2.84 | * |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.09 | * |

 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *

| * SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMI SS | * SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMP L LEVEL MPG GS/VM |
|--|--|
| * 1 3 500. 4029. 0. 4029. 4029. 0. 4029. 6000. 0. 0. 0. .67 65. 20.7 C 19.0 14.1 | |
| * 2 3 99999. 0. 645. 4029. 0. 645. 4021. 6000. 0. * 13827. 8. .67 36. 36.9 F 17.7 15.3 | |
| * 3 2 11000. 0. 0. 3384. 0. 0. 3376. 4000. 0. **11000. 8. .84 17. 100.7 F 16.8 17.9 | |
| * 4 2 1500. 64. 0. 3448. 64. 0. 3440. 3995. 0. ** 1500. 8. .86 18. 96.8 F 17.2 17.4 | |
| * 5 2 1400. 0. 0. 3448. 0. 0. 3440. 4000. 0. ** 1400. 8. .86 18. 97.2 F 17.2 17.4 | |
| * 6 2 1500. 528. 0. 3976. 528. 0. 3968. 3968. 0. 0. 1.00 52. 38.5 E 23.6 11.1 | |
| * 7 2 1300. 0. 0. 3976. 0. 0. 3968. 4000. 0. 0. 0. .99 52. 38.0 E 23.5 11.2 | |
| * 8 3 500. 0. 869. 3976. 0. 867. 3968. 5130. 0. 0. 0. .77 62. 21.3 C 20.3 13.0 | |
| * 9 2 2300. 0. 0. 3107. 0. 0. 3101. 4000. 0. 0. 0. .78 61. 25.2 C 20.6 12.8 | |
| * 10 3 250. 437. 0. 3544. 437. 0. 3538. 4826. 0. 0. 0. .73 62. 19.0 C 20.3 13.0 | |
| * 11 3 200. 0. 0. 3544. 0. 0. 3538. 4860. 0. 0. 0. .73 62. 19.0 C 20.3 13.0 | |
| * 12 3 250. 0. 1277. 3544. 0. 1275. 3538. 4682. 0. 0. 0. .76 62. 19.0 C 20.3 13.0 | |
| * 13 2 50. 0. 351. 2267. 0. 350. 2263. 3951. 0. 0. 0. .57 62. 18.2 C 20.3 13.0 | |
| * 14 2 50. 0. 0. 1916. 0. 0. 1913. 2470. 0. 0. 0. .77 62. 15.4 B 20.3 13.0 | |
| * 15 2 1000. 348. 0. 2264. 348. 0. 2261. 3948. 0. 0. 0. .57 62. 18.2 C 20.3 13.0 | |
| * 16 2 10. 0. 0. 2264. 0. 0. 2261. 4000. 0. 0. 0. .57 62. 18.2 C 20.3 13.0 | |
| * 17 2 1500. 769. 0. 3033. 769. 0. 3030. 3884. 0. 0. 0. .78 62. 24.4 C 20.3 13.0 | |
| * 18 2 1500. 0. 587. 3033. 0. 586. 3030. 3949. 0. 0. 0. .77 62. 24.4 C 20.3 13.0 | |
| * 19 2 12000. 0. 0. 2446. 0. 0. 2443. 4000. 0. 0. 0. .61 62. 19.7 C 20.3 13.0 | |
| * 20 3 500. 466. 2912. 2912. 466. 2909. 2909. 6000. 0. 0. 0. .48 65. 14.9 B 19.0 14.1 | |
| * * * TOTAL 137309. = 26.0 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 35. 40.9 18.0 15.2 * * ***** | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 1418. VEH-HRS | 1587. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1418. VEH-HRS | 1587. PASS-HRS |
| TOTAL TRAV DISTANCE = | 48955. VEH-MI. | 55165. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 35. MPH | 43. MPH |
| AVERAGE DENSITY = | 41. VPMP | 34. VPMP |
| TOTAL FUEL = | 2723. GALLONS | 14026. GALLONS |
| TOTAL EMISSIONS = | 745. KI LOGRAMS | 3794. KI LOGRAMS |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 3/30/2016 16:20 PAGE 18
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION TIME SLICE 5 OF 6

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|--------|------------|--------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 462.13 | 3 | 155.59 | 4 | 19.99 | 5 | 18.75 |
| 6 | 2.26 | 7 | 1.84 | 8 | 0.14 | 9 | 0.61 | 10 | 0.06 |
| 11 | 0.05 | 12 | 0.06 | 13 | 0.01 | 14 | 0.01 | 15 | 0.16 |
| 16 | 0.00 | 17 | 0.32 | 18 | 0.32 | 19 | 2.07 | 20 | 0.00 |

***** TOTAL DELAY = 664.4 VEH-HRS ***** AVERAGE DELAY = 10.48 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 3/30/2016 16:20 PAGE 19
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION TIME SLICE 6 OF 6

 **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN *
 * 1 2 3 4 5 6 7 *

| |
|---|
| * 1 * 31.40 41.41 41.97 41.98 42.17 42.72 45.01 |
| * 2 * 0.00 2.56 3.12 3.13 3.32 3.87 6.16 |
| * 3 * 0.00 0.71 1.26 1.27 1.46 2.01 4.30 |
| * 4 * 0.00 0.00 0.13 0.14 0.33 0.88 3.17 |
| * 5 * 0.00 0.00 0.00 0.00 0.18 0.73 3.02 |
| * 6 * 0.00 0.00 0.00 0.00 0.00 0.55 2.84 |

```
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.09
* * *
*****
```

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB | * NO. | * SSEC | * O-D | * DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | |
|---------|---------|----------|---------|---------|-----------|------------|-----------|---------|---------|-----------------|-----------|----------------|---------|-----------|---------|--------|-------------|--------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP/L | * LEVEL | * MPG | * GS/VM | |
| * 1 | * 3 | * 500. | * 4029. | * 0. | * 4029. | * 4029. | * 0. | * 4029. | * 6000. | * 0. | * 0. | * .67 | * 65. | * 20.7 | * C | * 19.0 | * 14.1 | |
| * 2 | * 3 | * 99999. | * 0. | * 645. | * 4029. | * 0. | * 645. | * 4021. | * 6000. | * 0. | * 13886. | * 8. | * .67 | * 36. | * 36.9 | * F | * 17.7 | * 15.3 |
| * 3 | * 2 | * 11000. | * 0. | * 0. | * 3384. | * 0. | * 0. | * 3376. | * 4000. | * 0. | * 11000. | * 8. | * .84 | * 17. | * 100.7 | * F | * 16.8 | * 17.9 |
| * 4 | * 2 | * 1500. | * 64. | * 0. | * 3448. | * 64. | * 0. | * 3440. | * 3995. | * 0. | * 1500. | * 8. | * .86 | * 18. | * 96.8 | * F | * 17.2 | * 17.4 |
| * 5 | * 2 | * 1400. | * 0. | * 0. | * 3448. | * 0. | * 0. | * 3440. | * 4000. | * 0. | * 1400. | * 8. | * .86 | * 18. | * 97.2 | * F | * 17.2 | * 17.4 |
| * 6 | * 2 | * 1500. | * 528. | * 0. | * 3976. | * 528. | * 0. | * 3968. | * 3968. | * 0. | * 0. | * 1.00 | * 52. | * 38.5 | * E | * 23.6 | * 11.1 | |
| * 7 | * 2 | * 1300. | * 0. | * 0. | * 3976. | * 0. | * 0. | * 3968. | * 4000. | * 0. | * 0. | * .99 | * 52. | * 38.0 | * E | * 23.5 | * 11.2 | |
| * 8 | * 3 | * 500. | * 0. | * 869. | * 3976. | * 0. | * 867. | * 3968. | * 5130. | * 0. | * 0. | * .77 | * 62. | * 21.3 | * C | * 20.3 | * 13.0 | |
| * 9 | * 2 | * 2300. | * 0. | * 0. | * 3107. | * 0. | * 0. | * 3101. | * 4000. | * 0. | * 0. | * .78 | * 61. | * 25.2 | * C | * 20.6 | * 12.8 | |
| * 10 | * 3 | * 250. | * 437. | * 0. | * 3544. | * 437. | * 0. | * 3538. | * 4826. | * 0. | * 0. | * .73 | * 62. | * 19.0 | * C | * 20.3 | * 13.0 | |
| * 11 | * 3 | * 200. | * 0. | * 0. | * 3544. | * 0. | * 0. | * 3538. | * 4860. | * 0. | * 0. | * .73 | * 62. | * 19.0 | * C | * 20.3 | * 13.0 | |
| * 12 | * 3 | * 250. | * 0. | * 1277. | * 3544. | * 0. | * 1275. | * 3538. | * 4682. | * 0. | * 0. | * .76 | * 62. | * 19.0 | * C | * 20.3 | * 13.0 | |
| * 13 | * 2 | * 50. | * 0. | * 351. | * 2267. | * 0. | * 350. | * 2263. | * 3951. | * 0. | * 0. | * .57 | * 62. | * 18.2 | * C | * 20.3 | * 13.0 | |
| * 14 | * 2 | * 50. | * 0. | * 0. | * 1916. | * 0. | * 0. | * 1913. | * 2470. | * 0. | * 0. | * .77 | * 62. | * 15.4 | * B | * 20.3 | * 13.0 | |
| * 15 | * 2 | * 1000. | * 348. | * 0. | * 2264. | * 348. | * 0. | * 2261. | * 3948. | * 0. | * 0. | * .57 | * 62. | * 18.2 | * C | * 20.3 | * 13.0 | |
| * 16 | * 2 | * 10. | * 0. | * 0. | * 2264. | * 0. | * 0. | * 2261. | * 4000. | * 0. | * 0. | * .57 | * 62. | * 18.2 | * C | * 20.3 | * 13.0 | |
| * 17 | * 2 | * 1500. | * 769. | * 0. | * 3033. | * 769. | * 0. | * 3030. | * 3884. | * 0. | * 0. | * .78 | * 62. | * 24.4 | * C | * 20.3 | * 13.0 | |
| * 18 | * 2 | * 1500. | * 0. | * 587. | * 3033. | * 0. | * 586. | * 3030. | * 3949. | * 0. | * 0. | * .77 | * 62. | * 24.4 | * C | * 20.3 | * 13.0 | |
| * 19 | * 2 | * 12000. | * 0. | * 0. | * 2446. | * 0. | * 0. | * 2443. | * 4000. | * 0. | * 0. | * .61 | * 62. | * 19.7 | * C | * 20.3 | * 13.0 | |
| * 20 | * 3 | * 500. | * 466. | * 2912. | * 2912. | * 466. | * 2909. | * 2909. | * 6000. | * 0. | * 0. | * .48 | * 65. | * 14.9 | * B | * 19.0 | * 14.1 | |
| * TOTAL | 137309. | = | 26.0 | MILES | | | | | | MAX(V/C) = 1.00 | | LOWEST LOS = F | | AVG = 34. | 40.9 | 18.0 | 15.2 | |

| | CURRENT TIME SLICE | | CUMULATIVE VALUES |
|----------------------------|--------------------|-----------------|-------------------------------------|
| FREEWAY TRAVEL TIME = | 1420. VEH-HRS | 1589. PASS-HRS | 7570. VEH-HRS 8443. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 1420. VEH-HRS | 1589. PASS-HRS | 7570. VEH-HRS 8443. PASS-HRS |
| TOTAL TRAV DISTANCE = | 48955. VEH-MI. | 55165. PASS-MI. | 311762. VEH-MI. 352086. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 34. MPH. | | 41. MPH. |
| AVERAGE DENSITY = | 41. VPMP/L | | 35. VPMP/L |
| TOTAL FUEL = | 2723. GALLONS | | 16750. GALLONS |
| TOTAL EMISSIONS = | 746. KI LOGRAMS | | 4540. KI LOGRAMS |

***** MAINTENANCE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|---------------------|-------|------------|-----------------------|------------|---------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 464.13 | 3 | 155.59 | 4 | 19.99 | 5 | 18.75 |
| 6 | 2.26 | 7 | 1.84 | 8 | 0.14 | 9 | 0.61 | 10 | 0.06 |
| 11 | 0.05 | 12 | 0.06 | 13 | 0.01 | 14 | 0.01 | 15 | 0.16 |
| 16 | 0.00 | 17 | 0.32 | 18 | 0.32 | 19 | 2.07 | 20 | 0.00 |
| ***** TOTAL DELAY = | 666.4 | VEH-HRS | ***** AVERAGE DELAY = | 10.51 | MIN/VEH | ***** | | | |

```

FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQQ QQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 PPP PPP LLL
FFFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 2222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 1111111 222222222 PPP LLLLLLLLLL

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FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 3 AND 19 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 2.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 30
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 1.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

FREeway AND ARTERIAL DESIGN FEATURES

| ** SUB NO. | ** SSEC | ** SSEC | ** DESIG N | ** ORG | ** TRK | ** SSEC | ** PCT | ** PCT | ** DES | ** SPECIAL | ** FF. SPD. | ** CAP. | ** ART | ** GRADE | ** SUBSECTI ON | ** LOCATI ON |
|------------|---------|-----------|------------|--------|--------|---------|--------|-----------|---------|-------------|-------------|---------|-------------|----------------|--------------------------|--------------|
| ** SEC LNS | ** CAP | ** LENGTH | ** SPEED | ** DES | ** FAC | ** GRAD | ** TRK | ** TRUCKS | ** RAMP | ** ALT. RTE | ** ALT. RTE | ** TYPE | ** ALT. RTE | ** SUBSECTI ON | ** LOCATI ON | |
| ** 1 | | | | | | | | | | | | | | | | |
| ** 2 | | | | | | | | | | | | | | | | |
| ** 3 | 1 | 1500. | 11000. | 62 | 0 | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | |
| ** 4 | 1 | 1500. | 1500. | 62 | 0 | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence On-ramp | |
| ** 5 | 1 | 1500. | 1400. | 62 | | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Lawrence to Crossman | |
| ** 6 | 1 | 1500. | 1500. | 62 | 0 | 0.95 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Crossman On-Ramp | |
| ** 7 | 1 | 1500. | 1300. | 62 | | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Crossman / Mathilda | |
| ** 8 | 1 | 1500. | 500. | 62 | D | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-Ramp | |
| ** 9 | 1 | 1500. | 2300. | 62 | | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | |
| ** 10 | 1 | 1500. | 250. | 62 | 0 | 0.95 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda On-ramp | |
| ** 11 | 1 | 1500. | 200. | 62 | | 0.95 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda to US-101 | |
| ** 12 | 1 | 1500. | 250. | 62 | D | 0.95 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | US-101 Off-Ramp | |
| ** 13 | 1 | 1500. | 50. | 62 | D | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Bottleneck by-pass | |
| ** 14 | 1 | 1500. | 50. | 62 | | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Bottleeck | |
| ** 15 | 1 | 1500. | 1000. | 62 | OD | 0.95 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | US 101 / US 101 | |
| ** 16 | 1 | 1500. | 10. | 62 | | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Dummy end of travel time | |
| ** 17 | 1 | 1500. | 1500. | 62 | 0 | 0.95 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | US 101 NB On-Ramp | |
| ** 18 | 1 | 1500. | 1500. | 62 | D | 0.95 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Maude Off-ramp | |

**
 ** 19 1 1500. 12000. 62 D 0.95 0.0 0 100 NO 0.0 0. GOOD 0.0 HOV Dummy **
 ** 20 **
 **

 ** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS DOWN | | * DESTINATIONS ACROSS | | | | | | | |
|----------------|-----|-----------------------|------|------|------|------|------|------|------|
| | | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| + * | 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + * | 2 * | 0.00 | 3.15 | 3.70 | 3.71 | 3.90 | 4.46 | 6.66 | 0.00 |
| + * | 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.44 | 4.64 | 0.00 |
| + * | 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 4.11 | 0.00 |
| + * | 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.08 | 0.00 |
| + * | 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.93 | 0.00 |
| + * | 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.75 | 0.00 |
| + * | 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | |
|-----------|--------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|-----------------|----------------|-----------|-----------|--------|-------------|------|------|--|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * ORG | * DES | * CAP | * EFF | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | | |
| * 1 | | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | | |
| * 3 | 1 | 11000. | 720. | 0. | 720. | 720. | 0. | 720. | 1500. | 0. | 0. | 0. | .48 | 62. | 11.6 B | 21.6 | 12.8 | |
| * 4 | 1 | 1500. | 4. | 0. | 724. | 4. | 0. | 724. | 1500. | 0. | 0. | 0. | .48 | 62. | 11.7 B | 21.6 | 12.8 | |
| * 5 | 1 | 1400. | 0. | 0. | 724. | 0. | 0. | 724. | 1500. | 0. | 0. | 0. | .48 | 62. | 11.7 B | 21.6 | 12.8 | |
| * 6 | 1 | 1500. | 44. | 0. | 768. | 44. | 0. | 768. | 1500. | 0. | 0. | 0. | .51 | 62. | 12.4 B | 21.6 | 12.8 | |
| * 7 | 1 | 1300. | 0. | 0. | 768. | 0. | 0. | 768. | 1500. | 0. | 0. | 0. | .51 | 62. | 12.4 B | 21.6 | 12.8 | |
| * 8 | 1 | 500. | 0. | 163. | 768. | 0. | 163. | 768. | 1500. | 0. | 0. | 0. | .51 | 62. | 12.4 B | 21.6 | 12.8 | |
| * 9 | 1 | 2300. | 0. | 0. | 604. | 0. | 0. | 604. | 1500. | 0. | 0. | 0. | .40 | 62. | 9.7 A | 21.6 | 12.8 | |
| * 10 | 1 | 250. | 43. | 0. | 647. | 43. | 0. | 647. | 1500. | 0. | 0. | 0. | .43 | 62. | 10.4 A | 21.6 | 12.8 | |
| * 11 | 1 | 200. | 0. | 0. | 647. | 0. | 0. | 647. | 1500. | 0. | 0. | 0. | .43 | 62. | 10.4 A | 21.6 | 12.8 | |
| * 12 | 1 | 250. | 0. | 241. | 647. | 0. | 240. | 647. | 1500. | 0. | 0. | 0. | .43 | 62. | 10.4 A | 21.6 | 12.8 | |
| * 13 | 1 | 50. | 0. | 6. | 406. | 0. | 6. | 406. | 1500. | 0. | 0. | 0. | .27 | 62. | 6.5 A | 21.6 | 12.8 | |
| * 14 | 1 | 50. | 0. | 0. | 400. | 0. | 0. | 400. | 1500. | 0. | 0. | 0. | .27 | 62. | 6.5 A | 21.6 | 12.8 | |
| * 15 | 1 | 1000. | 7. | 0. | 407. | 7. | 0. | 407. | 1500. | 0. | 0. | 0. | .27 | 62. | 6.6 A | 21.6 | 12.8 | |
| * 16 | 1 | 10. | 0. | 0. | 407. | 0. | 0. | 407. | 1500. | 0. | 0. | 0. | .27 | 62. | 6.6 A | 21.6 | 12.8 | |
| * 17 | 1 | 1500. | 121. | 0. | 528. | 121. | 0. | 528. | 1500. | 0. | 0. | 0. | .35 | 62. | 8.5 A | 21.6 | 12.8 | |
| * 18 | 1 | 1500. | 0. | 40. | 528. | 0. | 40. | 528. | 1500. | 0. | 0. | 0. | .35 | 62. | 8.5 A | 21.6 | 12.8 | |
| * 19 | 1 | 12000. | 0. | 488. | 488. | 0. | 488. | 488. | 1500. | 0. | 0. | 0. | .33 | 62. | 7.9 A | 21.6 | 12.8 | |
| * 20 | | | | | | | | | | | | | | | | | | |
| * TOTAL | | 36310. | = | 6.9 | MI LBS | | | | | | | | | | | | | |
| | | | | | | | | | | MAX(V/C) = 0.51 | LOWEST LOS = B | | AVG = 62. | 9.9 | 21.6 | 12.8 | | |

| CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | | |
|-----------------------------|-------|---------|-------|-------------------|-------|---------|-------|----------|
| FREWAY TRAVEL TIME = | 34. | VEH-HRS | 68. | PASS-HRS | 34. | VEH-HRS | 68. | PASS-HRS |
| FREWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 34. | VEH-HRS | 68. | PASS-HRS | 34. | VEH-HRS | 68. | PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 2111. | VEH-MI. | 4222. | PASS-MI. | 2111. | VEH-MI. | 4222. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. | MPH. | | | 62. | MPH. | | |
| AVERAGE DENSITY = | 10. | VPMP | | | 10. | VPMP | | |
| TOTAL FUEL = | 98. | GALLONS | | | 98. | GALLONS | | |

TOTAL EMISSIONS = 27. KILOGRAMS

SR-237_WB_PM_P2_2040_PL 27. KILOGRAMS

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

Table with 10 columns: SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY, SUBSECTION, DELAY. Rows 1-16 showing delay values for various subsections.

***** TOTAL DELAY = 1.6 VEH-HRS ***** AVERAGE DELAY = 0.15 MIN/VEH *****

***** RAMP DELAYS *****

Table with 9 columns: OFF-RAMP, OUTPUT POINT, QUEUE LENGTH VEHICLES, DELAY VEH-HRS, GAS GALS, HC KGMS, CO KGMS, NOX KGMS, TOTAL EMISSIONS KGMS. Row 3 showing ramp delay data.

***** FREEWAY TRAVEL TIME (MINUTES) *****

Table with 9 columns: ORIGINS DOWN, DESTINATIONS ACROSS (1-8). Rows 1-8 showing travel times between origins and destinations.

TIME SLICE FREEWAY PERFORMANCE TABLE

Table with 17 columns: SUB SEC, NO. LNS, SSEC LENGTH, O-D DATA ORG, DEMANDS DES, SSEC, ADJUSTED VOLUMES ORG, SSEC, WEAVE CAP, EFF, CONGEST LENGTH, STORAGE RATE, V/C RATIO, SPEED MPH, DENSITY VPMP, LOS LEVEL, FUEL MPG, EMISSIONS GS/VM. Rows 1-19 showing freeway performance metrics.

* 20 *

 * TOTAL 36310. = 6.9 MILES MAX(V/C) = 0.51 LOWEST LOS = B AVG = 62. 9.9 21.6 12.8 *

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|-----------------------------|--------------------|----------------|-------------------|----------------|
| FREEWAY TRAVEL TIME = | 34. VEH-HRS | 68. PASS-HRS | 68. VEH-HRS | 136. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 1. PASS-HRS | 1. VEH-HRS | 1. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 34. VEH-HRS | 69. PASS-HRS | 69. VEH-HRS | 137. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 2111. VEH-MI. | 4222. PASS-MI. | 4222. VEH-MI. | 8444. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 61. MPH. | | 62. MPH. | |
| AVERAGE DENSITY = | 10. VPMP/L | | 10. VPMP/L | |
| TOTAL FUEL = | 98. GALLONS | | 196. GALLONS | |
| TOTAL EMISSIONS = | 27. KILOGRAMS | | 54. KILOGRAMS | |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/30/2016 16:20 PAGE 8
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 6

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.56 | 4 | 0.08 | 5 | 0.07 |
| 6 | 0.08 | 7 | 0.07 | 8 | 0.03 | 9 | 0.10 | 10 | 0.01 |
| 11 | 0.01 | 12 | 0.01 | 13 | 0.00 | 14 | 0.00 | 15 | 0.03 |
| 16 | 0.00 | 17 | 0.06 | 18 | 0.06 | 19 | 0.41 | 20 | 0.00 |

***** TOTAL DELAY = 1.6 VEH-HRS ***** AVERAGE DELAY = 0.15 MIN/VEH *****

***** RAMP DELAYS *****

| OFF-RAMP | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|----------------|-----------------------|---------------|----------|---------|---------|----------|----------------------|
| 3 OUTPUT POINT | 1. | 0.41 | 0.14 | 0.01 | 0.05 | 0.00 | 0.06 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/30/2016 16:20 PAGE 9
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 3 OF 6

 ** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS DOWN | * DESTINATIONS ACROSS * | | | | | | | |
|----------------|-------------------------|------|------|------|------|------|------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 3.15 | 3.70 | 3.71 | 3.90 | 4.46 | 6.66 | 0.00 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.44 | 4.64 | 0.00 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 4.11 | 0.00 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.08 | 0.00 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.93 | 0.00 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.75 | 0.00 |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/30/2016 16:20 PAGE 10
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 3 OF 6

TIME SLICE FREEWAY PERFORMANCE TABLE

* SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMISSIONS
 * SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMP/L LEVEL MPG GS/VM *

SR-237_WB_PM_P2_2040_PL

| | | | | | | | | | | | | | | | | | | | | |
|---|----|---|--------|------|------|------|------|------|------|-------|----|----|----|-----|-----|------|---|------|------|---|
| * | 1 | | | | | | | | | | | | | | | | | | * | |
| * | 2 | | | | | | | | | | | | | | | | | | * | |
| * | 3 | 1 | 11000. | 741. | 0. | 741. | 741. | 0. | 741. | 1500. | 0. | 0. | 0. | .49 | 62. | 11.9 | B | 21.6 | 12.8 | * |
| * | 4 | 1 | 1500. | 5. | 0. | 746. | 5. | 0. | 746. | 1500. | 0. | 0. | 0. | .50 | 62. | 12.0 | B | 21.6 | 12.8 | * |
| * | 5 | 1 | 1400. | 0. | 0. | 746. | 0. | 0. | 746. | 1500. | 0. | 0. | 0. | .50 | 62. | 12.0 | B | 21.6 | 12.8 | * |
| * | 6 | 1 | 1500. | 47. | 0. | 793. | 47. | 0. | 793. | 1500. | 0. | 0. | 0. | .53 | 62. | 12.8 | B | 21.6 | 12.8 | * |
| * | 7 | 1 | 1300. | 0. | 0. | 793. | 0. | 0. | 793. | 1500. | 0. | 0. | 0. | .53 | 62. | 12.8 | B | 21.6 | 12.8 | * |
| * | 8 | 1 | 500. | 0. | 171. | 793. | 0. | 171. | 793. | 1500. | 0. | 0. | 0. | .53 | 62. | 12.8 | B | 21.6 | 12.8 | * |
| * | 9 | 1 | 2300. | 0. | 0. | 622. | 0. | 0. | 622. | 1500. | 0. | 0. | 0. | .41 | 62. | 10.0 | A | 21.6 | 12.8 | * |
| * | 10 | 1 | 250. | 44. | 0. | 666. | 44. | 0. | 666. | 1500. | 0. | 0. | 0. | .44 | 62. | 10.7 | A | 21.6 | 12.8 | * |
| * | 11 | 1 | 200. | 0. | 0. | 666. | 0. | 0. | 666. | 1500. | 0. | 0. | 0. | .44 | 62. | 10.7 | A | 21.6 | 12.8 | * |
| * | 12 | 1 | 250. | 0. | 211. | 666. | 0. | 211. | 666. | 1500. | 0. | 0. | 0. | .44 | 62. | 10.7 | A | 21.6 | 12.8 | * |
| * | 13 | 1 | 50. | 0. | 24. | 455. | 0. | 24. | 455. | 1500. | 0. | 0. | 0. | .30 | 62. | 7.3 | A | 21.6 | 12.8 | * |
| * | 14 | 1 | 50. | 0. | 0. | 431. | 0. | 0. | 431. | 1500. | 0. | 0. | 0. | .29 | 62. | 7.0 | A | 21.6 | 12.8 | * |
| * | 15 | 1 | 1000. | 26. | 0. | 457. | 26. | 0. | 457. | 1500. | 0. | 0. | 0. | .30 | 62. | 7.4 | A | 21.6 | 12.8 | * |
| * | 16 | 1 | 10. | 0. | 0. | 457. | 0. | 0. | 457. | 1500. | 0. | 0. | 0. | .30 | 62. | 7.4 | A | 21.6 | 12.8 | * |
| * | 17 | 1 | 1500. | 121. | 0. | 578. | 121. | 0. | 578. | 1500. | 0. | 0. | 0. | .39 | 62. | 9.3 | A | 21.6 | 12.8 | * |
| * | 18 | 1 | 1500. | 0. | 68. | 578. | 0. | 68. | 578. | 1500. | 0. | 0. | 0. | .39 | 62. | 9.3 | A | 21.6 | 12.8 | * |
| * | 19 | 1 | 12000. | 0. | 509. | 509. | 0. | 509. | 509. | 1500. | 0. | 0. | 0. | .34 | 62. | 8.2 | A | 21.6 | 12.8 | * |
| * | 20 | | | | | | | | | | | | | | | | | | | * |

 * TOTAL 36310. = 6.9 MILES MAX(V/C) = 0.53 LOWEST LOS = B AVG = 62. 10.3 21.6 12.8 *

| | | | | | | | | | |
|-----------------------------|-------|--------------------|-------|----------|-------|-------------------|--------|----------|--|
| | | CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | |
| FREWAY TRAVEL TIME = | 35. | VEH-HRS | 71. | PASS-HRS | 103. | VEH-HRS | 207. | PASS-HRS | |
| FREWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS | |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS | |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 1. | PASS-HRS | 1. | VEH-HRS | 2. | PASS-HRS | |
| TOTAL SYSTEM TRAVEL TIME = | 36. | VEH-HRS | 71. | PASS-HRS | 104. | VEH-HRS | 209. | PASS-HRS | |
| TOTAL FRWAY TRAV DISTANCE = | 2194. | VEH-MI. | 4389. | PASS-MI. | 6417. | VEH-MI. | 12833. | PASS-MI. | |
| AVERAGE SYSTEM SPEED = | 62. | MPH. | | | 62. | MPH. | | | |
| AVERAGE DENSITY = | 10. | VPMP | | | 10. | VPMP | | | |
| TOTAL FUEL = | 102. | GALLONS | | | 298. | GALLONS | | | |
| TOTAL EMISSIONS = | 28. | KILOGRAMS | | | 82. | KILOGRAMS | | | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.57 | 4 | 0.08 | 5 | 0.07 |
| 6 | 0.08 | 7 | 0.07 | 8 | 0.03 | 9 | 0.10 | 10 | 0.01 |
| 11 | 0.01 | 12 | 0.01 | 13 | 0.00 | 14 | 0.00 | 15 | 0.03 |
| 16 | 0.00 | 17 | 0.06 | 18 | 0.06 | 19 | 0.43 | 20 | 0.00 |

***** TOTAL DELAY = 1.6 VEH-HRS ***** AVERAGE DELAY = 0.15 MIN/VEH *****

***** RAMP DELAYS *****

| OFF-RAMP | OUTPUT POINT | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|----------|--------------|-----------------------|---------------|----------|---------|---------|----------|----------------------|
| OFF-RAMP | 3 | OUTPUT POINT | 0. | 0.27 | 0.09 | 0.01 | 0.03 | 0.04 |

 ** FREEWAY TRAVEL TIME (MINUTES) **

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | | |
|--------------|---------------------|------|------|------|------|------|------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 3.15 | 3.70 | 3.71 | 3.90 | 4.46 | 6.66 | 0.00 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.44 | 4.64 | 0.00 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 4.11 | 0.00 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.08 | 0.00 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.93 | 0.00 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.75 | 0.00 |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS | | | | | | |
|---------|--------|----------|---------|------------------|------|-------|---------|---------|-------|-----------------|---------|-------|----------------|--------|------|---|-----------|------|------|------|
| SEC LNS | LENGTH | ORG DES | SSEC | ORG DES SSEC | CAP. | EFF | LENGTH | RATE | RATIO | MPH | VPMPL | LEVEL | MPG | GS/VM | | | | | | |
| 1 | | | | | | | | | | | | | | | | | | | | |
| 2 | | | | | | | | | | | | | | | | | | | | |
| 3 | 1 | 11000. | 741. | 0. | 741. | 741. | 0. | 741. | 1500. | 0. | 0. | 0. | .49 | 62. | 11.9 | B | 21.6 | 12.8 | | |
| 4 | 1 | 1500. | 5. | 0. | 746. | 5. | 0. | 746. | 1500. | 0. | 0. | 0. | .50 | 62. | 12.0 | B | 21.6 | 12.8 | | |
| 5 | 1 | 1400. | 0. | 0. | 746. | 0. | 0. | 746. | 1500. | 0. | 0. | 0. | .50 | 62. | 12.0 | B | 21.6 | 12.8 | | |
| 6 | 1 | 1500. | 47. | 0. | 793. | 47. | 0. | 793. | 1500. | 0. | 0. | 0. | .53 | 62. | 12.8 | B | 21.6 | 12.8 | | |
| 7 | 1 | 1300. | 0. | 0. | 793. | 0. | 0. | 793. | 1500. | 0. | 0. | 0. | .53 | 62. | 12.8 | B | 21.6 | 12.8 | | |
| 8 | 1 | 500. | 0. | 171. | 793. | 0. | 171. | 793. | 1500. | 0. | 0. | 0. | .53 | 62. | 12.8 | B | 21.6 | 12.8 | | |
| 9 | 1 | 2300. | 0. | 0. | 622. | 0. | 0. | 622. | 1500. | 0. | 0. | 0. | .41 | 62. | 10.0 | A | 21.6 | 12.8 | | |
| 10 | 1 | 250. | 44. | 0. | 666. | 44. | 0. | 666. | 1500. | 0. | 0. | 0. | .44 | 62. | 10.7 | A | 21.6 | 12.8 | | |
| 11 | 1 | 200. | 0. | 0. | 666. | 0. | 0. | 666. | 1500. | 0. | 0. | 0. | .44 | 62. | 10.7 | A | 21.6 | 12.8 | | |
| 12 | 1 | 250. | 0. | 211. | 666. | 0. | 211. | 666. | 1500. | 0. | 0. | 0. | .44 | 62. | 10.7 | A | 21.6 | 12.8 | | |
| 13 | 1 | 50. | 0. | 24. | 455. | 0. | 24. | 455. | 1500. | 0. | 0. | 0. | .30 | 62. | 7.3 | A | 21.6 | 12.8 | | |
| 14 | 1 | 50. | 0. | 0. | 431. | 0. | 0. | 431. | 1500. | 0. | 0. | 0. | .29 | 62. | 7.0 | A | 21.6 | 12.8 | | |
| 15 | 1 | 1000. | 26. | 0. | 457. | 26. | 0. | 457. | 1500. | 0. | 0. | 0. | .30 | 62. | 7.4 | A | 21.6 | 12.8 | | |
| 16 | 1 | 10. | 0. | 0. | 457. | 0. | 0. | 457. | 1500. | 0. | 0. | 0. | .30 | 62. | 7.4 | A | 21.6 | 12.8 | | |
| 17 | 1 | 1500. | 121. | 0. | 578. | 121. | 0. | 578. | 1500. | 0. | 0. | 0. | .39 | 62. | 9.3 | A | 21.6 | 12.8 | | |
| 18 | 1 | 1500. | 0. | 68. | 578. | 0. | 68. | 578. | 1500. | 0. | 0. | 0. | .39 | 62. | 9.3 | A | 21.6 | 12.8 | | |
| 19 | 1 | 12000. | 0. | 509. | 509. | 0. | 509. | 509. | 1500. | 0. | 0. | 0. | .34 | 62. | 8.2 | A | 21.6 | 12.8 | | |
| 20 | | | | | | | | | | | | | | | | | | | | |
| TOTAL | 36310. | = | 6.9 | MI LES | | | | | | MAX(V/C) = 0.53 | | | LOWEST LOS = B | | | | AVG = 62. | 10.3 | 21.6 | 12.8 |

| | | | |
|-----------------------------|--------------------|----------------|-------------------------------|
| | CURRENT TIME SLICE | | CUMULATIVE VALUES |
| FREEWAY TRAVEL TIME = | 35. VEH-HRS | 71. PASS-HRS | 139. VEH-HRS 278. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 1. VEH-HRS 2. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 35. VEH-HRS | 71. PASS-HRS | 140. VEH-HRS 279. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 2194. VEH-MI. | 4389. PASS-MI. | 8611. VEH-MI. 17222. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | | 62. MPH. |
| AVERAGE DENSITY = | 10. VPMPL | | 10. VPMPL |
| TOTAL FUEL = | 102. GALLONS | | 400. GALLONS |
| TOTAL EMISSIONS = | 28. KILOGRAMS | | 110. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.57 | 4 | 0.08 | 5 | 0.07 |
| 6 | 0.08 | 7 | 0.07 | 8 | 0.03 | 9 | 0.10 | 10 | 0.01 |
| 11 | 0.01 | 12 | 0.01 | 13 | 0.00 | 14 | 0.00 | 15 | 0.03 |
| 16 | 0.00 | 17 | 0.06 | 18 | 0.06 | 19 | 0.43 | 20 | 0.00 |

***** TOTAL DELAY = 1.6 VEH-HRS ***** AVERAGE DELAY = 0.15 MIN/VEH *****

FREEWAY TRAVEL TIME (MINUTES)

ORIGINS DESTINATIONS ACROSS

| ORIGINS DOWN | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|--------------|------|------|------|------|------|------|------|------|
| 1 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | 0.00 | 3.15 | 3.70 | 3.71 | 3.90 | 4.46 | 6.66 | 0.00 |

```

SR-237_WB_PM_P2_2040_PL
+      * 3 *   0.00  0.00  0.00  0.00  0.00  0.00  2.44  4.64  0.00      *
+      * 4 *   0.00  0.00  0.00  0.00  0.00  0.00  0.00  4.11  0.00      *
+      * 5 *   0.00  0.00  0.00  0.00  0.00  0.00  0.00  3.08  0.00      *
+      * 6 *   0.00  0.00  0.00  0.00  0.00  0.00  0.00  2.93  0.00      *
+      * 7 *   0.00  0.00  0.00  0.00  0.00  0.00  0.00  2.75  0.00      *
+      * 8 *   0.00  0.00  0.00  0.00  0.00  0.00  0.00  0.00  0.00      *
+      *  *
+      *****

```

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED | VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS | | | | |
|---------|--------|----------|---------|----------|---------|------|-------|---------|-----------------|-----|--------|---------|----------------|------|-----------|-------|------|-------|--|
| SEC | LNS | LENGTH | ORG | DES | SSEC | ORG | DES | SSEC | CAP. | EFF | LENGTH | RATE | RATIO | MPH | VPMPL | LEVEL | MPG | GS/VM | |
| * 1 | | | | | | | | | | | | | | | | | | | |
| * 2 | | | | | | | | | | | | | | | | | | | |
| * 3 | 1 | 11000. | 645. | 0. | 645. | 645. | 0. | 645. | 1500. | 0. | 0. | 0. | .43 | 62. | 10.4 | A | 21.6 | 12.8 | |
| * 4 | 1 | 1500. | 5. | 0. | 649. | 5. | 0. | 649. | 1500. | 0. | 0. | 0. | .43 | 62. | 10.5 | A | 21.6 | 12.8 | |
| * 5 | 1 | 1400. | 0. | 0. | 649. | 0. | 0. | 649. | 1500. | 0. | 0. | 0. | .43 | 62. | 10.5 | A | 21.6 | 12.8 | |
| * 6 | 1 | 1500. | 32. | 0. | 681. | 32. | 0. | 681. | 1500. | 0. | 0. | 0. | .45 | 62. | 11.0 | A | 21.6 | 12.8 | |
| * 7 | 1 | 1300. | 0. | 0. | 681. | 0. | 0. | 681. | 1500. | 0. | 0. | 0. | .45 | 62. | 11.0 | A | 21.6 | 12.8 | |
| * 8 | 1 | 500. | 0. | 140. | 681. | 0. | 140. | 681. | 1500. | 0. | 0. | 0. | .45 | 62. | 11.0 | A | 21.6 | 12.8 | |
| * 9 | 1 | 2300. | 0. | 0. | 541. | 0. | 0. | 541. | 1500. | 0. | 0. | 0. | .36 | 62. | 8.7 | A | 21.6 | 12.8 | |
| * 10 | 1 | 250. | 34. | 0. | 575. | 34. | 0. | 575. | 1500. | 0. | 0. | 0. | .38 | 62. | 9.3 | A | 21.6 | 12.8 | |
| * 11 | 1 | 200. | 0. | 0. | 575. | 0. | 0. | 575. | 1500. | 0. | 0. | 0. | .38 | 62. | 9.3 | A | 21.6 | 12.8 | |
| * 12 | 1 | 250. | 0. | 178. | 575. | 0. | 178. | 575. | 1500. | 0. | 0. | 0. | .38 | 62. | 9.3 | A | 21.6 | 12.8 | |
| * 13 | 1 | 50. | 0. | 49. | 397. | 0. | 49. | 397. | 1500. | 0. | 0. | 0. | .26 | 62. | 6.4 | A | 21.6 | 12.8 | |
| * 14 | 1 | 50. | 0. | 0. | 348. | 0. | 0. | 348. | 1500. | 0. | 0. | 0. | .23 | 62. | 5.6 | A | 21.6 | 12.8 | |
| * 15 | 1 | 1000. | 52. | 0. | 400. | 52. | 0. | 400. | 1500. | 0. | 0. | 0. | .27 | 62. | 6.5 | A | 21.6 | 12.8 | |
| * 16 | 1 | 10. | 0. | 0. | 400. | 0. | 0. | 400. | 1500. | 0. | 0. | 0. | .27 | 62. | 6.5 | A | 21.6 | 12.8 | |
| * 17 | 1 | 1500. | 116. | 0. | 517. | 116. | 0. | 517. | 1500. | 0. | 0. | 0. | .34 | 62. | 8.3 | A | 21.6 | 12.8 | |
| * 18 | 1 | 1500. | 0. | 51. | 517. | 0. | 51. | 517. | 1500. | 0. | 0. | 0. | .34 | 62. | 8.3 | A | 21.6 | 12.8 | |
| * 19 | 1 | 12000. | 0. | 466. | 466. | 0. | 466. | 466. | 1500. | 0. | 0. | 0. | .31 | 62. | 7.5 | A | 21.6 | 12.8 | |
| * 20 | | | | | | | | | | | | | | | | | | | |
| * TOTAL | 36310. | = | 6.9 | MILES | | | | | MAX(V/C) = 0.45 | | | | LOWEST LOS = A | | AVG = 62. | 9.1 | 21.6 | 12.8 | |

| | | |
|-----------------------------|--------------------|-------------------|
| | CURRENT TIME SLICE | CUMULATIVE VALUES |
| FREEWAY TRAVEL TIME = | 31. VEH-HRS | 62. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 31. VEH-HRS | 62. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 1937. VEH-MI. | 3874. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 62. MPH. | |
| AVERAGE DENSITY = | 9. VPMPL | |
| TOTAL FUEL = | 90. GALLONS | 490. GALLONS |
| TOTAL EMISSIONS = | 25. KILOGRAMS | 135. KILOGRAMS |

***** MAINTENANCE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|---------------------|-------|------------|-----------------------|------------|---------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.50 | 4 | 0.07 | 5 | 0.06 |
| 6 | 0.07 | 7 | 0.06 | 8 | 0.02 | 9 | 0.09 | 10 | 0.01 |
| 11 | 0.01 | 12 | 0.01 | 13 | 0.00 | 14 | 0.00 | 15 | 0.03 |
| 16 | 0.00 | 17 | 0.05 | 18 | 0.05 | 19 | 0.39 | 20 | 0.00 |
| ***** TOTAL DELAY = | 1.4 | VEH-HRS | ***** AVERAGE DELAY = | 0.15 | MIN/VEH | ***** | | | |

FREEWAY TRAVEL TIME (MINUTES)

SR-237_WB_PM_P2_2040_PL

```

*****
* ORIGIN S DESTINATIONS ACROSS
* DOWN
* 1 2 3 4 5 6 7 8
*
*
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
* 2 * 0.00 3.15 3.70 3.71 3.90 4.46 6.66 0.00
* 3 * 0.00 0.00 0.00 0.00 0.00 2.44 4.64 0.00
* 4 * 0.00 0.00 0.00 0.00 0.00 0.00 4.11 0.00
* 5 * 0.00 0.00 0.00 0.00 0.00 0.00 3.08 0.00
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 2.93 0.00
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 2.75 0.00
* 8 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
*
*****

```

TIME SLICE FREEWAY PERFORMANCE TABLE

```

*****
* SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMISSIONS
* SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMP L LEVEL MPG GS/VM
*
* 1
* 2
* 3 1 11000. 645. 0. 645. 645. 0. 645. 1500. 0. 0. 0. .43 62. 10.4 A 21.6 12.8
* 4 1 1500. 5. 0. 649. 5. 0. 649. 1500. 0. 0. 0. .43 62. 10.5 A 21.6 12.8
* 5 1 1400. 0. 0. 649. 0. 0. 649. 1500. 0. 0. 0. .43 62. 10.5 A 21.6 12.8
* 6 1 1500. 32. 0. 681. 32. 0. 681. 1500. 0. 0. 0. .45 62. 11.0 A 21.6 12.8
* 7 1 1300. 0. 0. 681. 0. 0. 681. 1500. 0. 0. 0. .45 62. 11.0 A 21.6 12.8
* 8 1 500. 0. 140. 681. 0. 140. 681. 1500. 0. 0. 0. .45 62. 11.0 A 21.6 12.8
* 9 1 2300. 0. 0. 541. 0. 0. 541. 1500. 0. 0. 0. .36 62. 8.7 A 21.6 12.8
* 10 1 250. 34. 0. 575. 34. 0. 575. 1500. 0. 0. 0. .38 62. 9.3 A 21.6 12.8
* 11 1 200. 0. 0. 575. 0. 0. 575. 1500. 0. 0. 0. .38 62. 9.3 A 21.6 12.8
* 12 1 250. 0. 178. 575. 0. 178. 575. 1500. 0. 0. 0. .38 62. 9.3 A 21.6 12.8
* 13 1 50. 0. 49. 397. 0. 49. 397. 1500. 0. 0. 0. .26 62. 6.4 A 21.6 12.8
* 14 1 50. 0. 0. 348. 0. 0. 348. 1500. 0. 0. 0. .23 62. 5.6 A 21.6 12.8
* 15 1 1000. 52. 0. 400. 52. 0. 400. 1500. 0. 0. 0. .27 62. 6.5 A 21.6 12.8
* 16 1 10. 0. 0. 400. 0. 0. 400. 1500. 0. 0. 0. .27 62. 6.5 A 21.6 12.8
* 17 1 1500. 116. 0. 517. 116. 0. 517. 1500. 0. 0. 0. .34 62. 8.3 A 21.6 12.8
* 18 1 1500. 0. 51. 517. 0. 51. 517. 1500. 0. 0. 0. .34 62. 8.3 A 21.6 12.8
* 19 1 12000. 0. 466. 466. 0. 466. 466. 1500. 0. 0. 0. .31 62. 7.5 A 21.6 12.8
* 20
*
* TOTAL 36310. = 6.9 MILES MAX(V/C) = 0.45 LOWEST LOS = A AVG = 62. 9.1 21.6 12.8
*
*****

```

```

CURRENT TIME SLICE CUMULATIVE VALUES
FREEWAY TRAVEL TIME = 31. VEH-HRS 62. PASS-HRS 201. VEH-HRS 403. PASS-HRS
FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 1. VEH-HRS 2. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 31. VEH-HRS 62. PASS-HRS 202. VEH-HRS 404. PASS-HRS
TOTAL FRWAY TRAV DISTANCE = 1937. VEH-MI. 3874. PASS-MI. 12485. VEH-MI. 24969. PASS-MI.
AVERAGE SYSTEM SPEED = 62. MPH. 62. MPH.
AVERAGE DENSITY = 9. VPMP L 10. VPMP L
TOTAL FUEL = 90. GALLONS 580. GALLONS
TOTAL EMISSIONS = 25. KILOGRAMS 160. KILOGRAMS

```

```

***** MAINTENANCE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY SUBSECTION DELAY
1 0.00 2 0.00 3 0.50 4 0.07 5 0.06
6 0.07 7 0.06 8 0.02 9 0.09 10 0.01
11 0.01 12 0.01 13 0.00 14 0.00 15 0.03
16 0.00 17 0.05 18 0.05 19 0.39 20 0.00
***** TOTAL DELAY = 1.4 VEH-HRS ***** AVERAGE DELAY = 0.15 MIN/VEH *****

```

```

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQQ QQQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP EEEEEEEEE
    
```

FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 35
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREWAY AND ARTERIAL DESIGN FEATURES

| ** SUB NO. | ** SSEC | ** SSEC | ** DESIG N | ** ORG | ** TRK | ** SSEC | ** PCT | ** PCT | ** DES | ** SPECIAL | ** FF. SPD. | ** CAP. | ** ART | ** GRADE | ** SUBSECTI ON | ** LOCATI ON |
|------------|---------|---------|------------|----------|--------|---------|--------|-----------|---------|-------------|-------------|---------|-------------|-------------|--------------------------|--------------|
| ** SEC | ** LNS | ** CAP | ** LENGTH | ** SPEED | ** DES | ** GRAD | ** TRK | ** TRUCKS | ** RAMP | ** ALT. RTE | ** ALT. RTE | ** TYPE | ** ALT. RTE | ** ALT. RTE | ** LOCATION | ** LOCATION |
| ** 1 | 5 | 12500. | 500. | 65 | OD | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Seeding | ** |
| ** 2 | 3 | 8660. | 99999. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | ** |
| ** 3 | 3 | 7000. | 2830. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-87 to DLC loop-on | ** |
| ** 4 | 3 | 7000. | 930. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | DLC loop-on to dia-on | ** |
| ** 5 | 3 | 7000. | 1490. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | DLC dia-on to Tomas off | ** |
| ** 6 | 3 | 7000. | 3020. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas off to on | ** |
| ** 7 | 3 | 7000. | 1030. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas on to bowers off | ** |
| ** 8 | 3 | 7000. | 1440. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers off to loop-on | ** |
| ** 9 | 3 | 7000. | 1430. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers loop-on to dia | ** |
| ** 10 | 3 | 7000. | 3480. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers dia-on to law-off | ** |
| ** 11 | 3 | 7000. | 1020. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Law off to loop-on | ** |
| ** 12 | 3 | 7000. | 980. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawr Loop to diag | ** |
| ** 13 | 3 | 7000. | 1800. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Lawrence On-ramp | ** |
| ** 14 | 3 | 7000. | 1500. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks Off-Ramp | ** |
| ** 15 | 3 | 6000. | 1300. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Fair Oaks | ** |
| ** 16 | 3 | 6000. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Fair Oaks On-Ramp | ** |
| ** 17 | 3 | 6000. | 1100. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Mathilda | ** |
| ** 18 | 3 | 6000. | 1000. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda NB Off-Ramp | ** |
| ** 19 | 3 | 6000. | 900. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | ** |
| ** 20 | 3 | 6000. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda NB On-Ramp | ** |

FREeway AND ARTERIAL DESIGN FEATURES

| SUB NO. | SEC | LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT TRUCKS | DES RAMP | SPECIAL | FF. SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION LOCATION |
|---------|-----|--------|----------|-------------|--------------|---------|---------|-----------|---------|------------|----------|---------|-------------------|---------------|----------------------|----------------|---------------------|
| ** 21 | 3 | 6000. | 100. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | GOOD | 0.0 | Mathilda / Mathilda | | |
| ** 22 | 3 | 6000. | 100. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | GOOD | 0.0 | Mathilda SB Off-ramp | | |
| ** 23 | 3 | 6000. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | GOOD | 0.0 | Mathilda / SR-237 | | |
| ** 24 | 3 | 6000. | 1500. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | GOOD | 0.0 | SR-237 WB Off-Ramp | | |
| ** 25 | 3 | 6000. | 800. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | GOOD | 0.0 | SR-237 / SR-237 | | |
| ** 26 | 3 | 6000. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0.0 | GOOD | 0.0 | SR-237 WB On-Ramp | | |
| ** 27 | 3 | 6000. | 800. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0.0 | GOOD | 0.0 | SR-237 / Ellis | | |
| ** 28 | 3 | 6000. | 1000. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | GOOD | 0.0 | Ellis Off-ramp | | |
| ** 29 | 3 | 6000. | 8000. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | GOOD | 0.0 | HOV Dummy | | |
| ** 30 | 5 | 10000. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | GOOD | 0.0 | HOV Dummy | | |
| ** 31 | 5 | 6000. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0.0 | GOOD | 0.0 | Dummy Bottleneck | | |
| ** 32 | 5 | 6000. | 2640. | 65 | D | 1.00 | 0.0 | 0 | 0 | NO | 0.0 | 0.0 | GOOD | 0.0 | End of Network | | |

***** INPUT HAS BEEN COMPLETED *****

| | | |
|----------------------------|----|-----------|
| QUEUE COLLISION IN SECTION | 16 | T2 =0.641 |
| QUEUE COLLISION IN SECTION | 15 | T2 =0.432 |
| QUEUE COLLISION IN SECTION | 14 | T2 =0.446 |
| QUEUE COLLISION IN SECTION | 3 | T2 =0.848 |

FREeway TRAVEL TIME (MINUTES)

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | |
|--------------|---------------------|-------|-------|-------|-------|-------|-------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 0.09 | 31.80 | 33.97 | 34.59 | 35.90 | 38.37 | 47.36 |
| * 2 * | 0.00 | 0.00 | 1.29 | 1.90 | 3.21 | 5.68 | 14.67 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.15 | 1.47 | 3.93 | 12.92 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.71 | 10.70 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.80 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.64 |

 *
 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *
 *
 * SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMI SS *
 * SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMP L LEVEL MPG GS/VM *
 *
 * 1 5 500. 9729. 1849. 9729. 9729. 1849. 9729. 12500. 0. 0. 0. .78 64. 30.6 D 19.8 13.5 *
 * 2 3 99999. 0. 0. 7880. 0. 0. 4291. 8660. 0. * 13081. 3589. .50 53. 26.9 F 21.7 12.3 *
 * 3 3 2830. 0. 0. 7880. 0. 0. 4291. 7000. 0. ** 2830. 2709. .61 34. 42.3 F 21.4 12.6 *
 * 4 3 930. 0. 0. 7880. 0. 0. 4291. 7000. 0. ** 930. 2709. .61 31. 46.1 F 20.9 13.0 *
 * 5 3 1490. 0. 0. 7880. 0. 0. 4291. 7000. 0. ** 1490. 2709. .61 29. 48.5 F 20.6 13.2 *
 * 6 3 3020. 0. 0. 7880. 0. 0. 4291. 7000. 0. ** 3020. 2709. .61 27. 53.3 F 20.0 13.7 *
 * 7 3 1030. 0. 0. 7880. 0. 0. 4291. 7000. 0. ** 1030. 2709. .61 25. 57.8 F 19.4 14.2 *
 * 8 3 1440. 0. 0. 7880. 0. 0. 4291. 7000. 0. ** 1440. 2709. .61 24. 60.6 F 19.1 14.4 *
 * 9 3 1430. 0. 0. 7880. 0. 0. 4291. 7000. 0. ** 1430. 2709. .61 22. 64.0 F 18.7 14.8 *
 * 10 3 3480. 0. 0. 7880. 0. 0. 4291. 7000. 0. ** 3480. 2709. .61 20. 70.0 F 18.1 15.4 *
 * 11 3 1020. 0. 0. 7880. 0. 0. 4291. 7000. 0. ** 1020. 2709. .61 19. 75.8 F 17.5 15.9 *
 * 12 3 980. 0. 0. 7880. 0. 0. 4291. 7000. 0. ** 980. 2709. .61 18. 78.4 F 17.3 16.2 *
 * 13 3 1800. 0. 0. 7880. 0. 0. 4291. 7000. 0. ** 1800. 2709. .61 17. 82.2 F 16.9 16.6 *
 * 14 3 1500. 0. 802. 7880. 0. 693. 4291. 6812. 0. ** 1500. 2521. .63 18. 80.3 F 17.4 16.5 *
 * 15 3 1300. 0. 0. 7078. 0. 0. 3598. 6000. 0. ** 1300. 2402. .60 17. 72.5 F 16.4 16.9 *
 * 16 3 1000. 864. 0. 7942. 764. 0. 4362. 5874. 0. ** 1000. 1512. .74 29. 50.8 F 20.5 13.7 *
 * 17 3 1100. 0. 0. 7942. 0. 0. 4362. 6000. 0. ** 1100. 1512. .73 27. 53.7 F 19.8 14.2 *
 * 18 3 1000. 0. 572. 7942. 0. 424. 4362. 5882. 0. ** 1000. 1512. .74 27. 54.6 F 20.0 14.1 *
 * 19 3 900. 0. 0. 7370. 0. 0. 3938. 6000. 0. ** 900. 1512. .66 22. 59.4 F 17.9 15.9 *
 * 20 3 100. 164. 0. 7534. 164. 0. 4102. 5974. 0. ** 100. 1512. .69 23. 59.9 F 18.3 15.5 *
 * 21 3 100. 0. 0. 7534. 0. 0. 4102. 6000. 0. ** 100. 1512. .68 23. 60.5 F 18.2 15.6 *
 * 22 3 100. 0. 546. 7534. 0. 409. 4102. 5890. 0. ** 100. 1512. .70 23. 59.3 F 18.5 15.3 *
 * 23 3 700. 0. 0. 6988. 0. 0. 3693. 6000. 0. ** 700. 1512. .62 19. 64.4 F 16.5 16.9 *
 * 24 3 1500. 0. 1068. 6988. 0. 799. 3693. 5785. 0. ** 1500. 1512. .64 19. 65.0 F 17.0 16.8 *
 * 25 3 800. 0. 0. 5920. 0. 0. 2894. 6000. 0. ** 800. 1512. .48 12. 80.3 F 12.8 20.1 *
 * 26 3 1000. 1197. 0. 7117. 1197. 0. 4091. 5748. 0. ** 1000. 1512. .71 20. 68.3 F 17.8 16.2 *
 * 27 3 800. 0. 0. 7117. 0. 0. 4091. 6000. 0. ** 800. 1512. .68 18. 75.7 F 16.8 17.2 *
 * 28 3 1000. 0. 640. 7117. 0. 510. 4091. 5896. 0. ** 1000. 1512. .69 18. 76.1 F 16.9 17.2 *
 * 29 3 8000. 0. 0. 6477. 0. 0. 3581. 6000. 0. ** 8000. 1512. .60 11. 107.5 F 13.1 21.5 *
 * 30 5 100. 1519. 0. 7996. 1519. 0. 5100. 10000. 0. ** 100. 1512. .51 7. 148.0 F 9.8 26.4 *
 * 31 5 1000. 1000. 0. 8996. 900. 0. 6000. 6000. 0. 0. 0. 1.00 65. 18.5 E 19.2 14.0 *
 * 32 5 2640. 0. 8996. 8996. 0. 6000. 6000. 6000. 0. 0. 0. 1.00 65. 18.5 E 20.0 13.7 *
 *
 *
 * TOTAL 144589. = 27.4 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 39. 39.4 20.6 13.1 *
 *

| | | | |
|----------------------------|--------------------|------------------|----------------------------------|
| | CURRENT TIME SLICE | | CUMULATIVE VALUES |
| FREWAY TRAVEL TIME = | 4909. VEH-HRS | 4930. PASS-HRS | 4909. VEH-HRS 4930. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 100. VEH-HRS | 110. PASS-HRS | 100. VEH-HRS 110. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 5009. VEH-HRS | 5040. PASS-HRS | 5009. VEH-HRS 5040. PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 192397. VEH-MI. | 193459. PASS-MI. | 192397. VEH-MI. 193459. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 38. MPH | | 39. MPH |
| AVERAGE DENSITY = | 39. VPMP | | 39. VPMP |
| TOTAL FUEL = | 9384. GALLONS | | 9384. GALLONS |
| TOTAL EMISSIONS = | 2527. KILOGRAMS | | 2527. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| | | | | | | | | | |
|------------|-------|------------|--------|------------|-------|------------|--------|------------|--------|
| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
| 1 | 0.30 | 2 | 505.86 | 3 | 49.52 | 4 | 18.93 | 5 | 33.08 |
| 6 | 77.42 | 7 | 29.58 | 8 | 44.06 | 9 | 46.88 | 10 | 127.09 |
| 11 | 40.74 | 12 | 40.64 | 13 | 78.45 | 14 | 62.19 | 15 | 51.10 |
| 16 | 19.64 | 17 | 23.67 | 18 | 21.96 | 19 | 24.28 | 20 | 2.64 |
| 21 | 2.68 | 22 | 2.59 | 23 | 21.86 | 24 | 46.78 | 25 | 36.37 |
| 26 | 30.76 | 27 | 28.22 | 28 | 35.23 | 29 | 433.72 | 30 | 12.54 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 1948.8 VEH-HRS ***** AVERAGE DELAY = 29.04 MIN/VEH *****

***** RAMP DELAYS *****

| | | | | | | | | | |
|---------|---|--------------|---------|----------|-------|------|------|------|-----------|
| | | QUEUE LENGTH | DELAY | AVERAGE | GAS | HC | CO | NOX | TOTAL |
| | | VEHICLES | VEH-HRS | METERING | GALS | KGMS | KGMS | KGMS | EMISSIONS |
| | | | | DELAY | | | | | KGMS |
| | | | | MINUTES | | | | | |
| ON-RAMP | 2 | RAMP | 100. | 3.47 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 3.47 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| ON-RAMP | 6 | RAMP | 100. | 3.70 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 3.70 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |

**
** FREeway TRAVEL TIME (MINUTES) **
**

Table with columns: ORIGINS DOWN, DESTINATIONS ACROSS (1-7). Rows 1-6 showing travel times between various origin-destination pairs.

*
* TIME SLICE FREEWAY PERFORMANCE TABLE *

Table with columns: SUB SEC, NO. LNS, SSEC LENGTH, O-D DATA ORG DES DEMANDS SSEC, ADJUSTED VOLUMES ORG DES SSEC, SSEC CAP, WEAVE EFF, CONGEST LENGTH, STORAGE RATE, V/C RATIO, SPEED MPH, DENSITY VPMP, LOS LEVEL, FUEL MPG, EMISSIONS GS/VM. Includes a summary row: TOTAL 144589. = 27.4 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 29. 66.1 18.1 15.5

Table comparing CURRENT TIME SLICE and CUMULATIVE VALUES for metrics like FREeway TRAVEL TIME, MERGE DELAY, MRG/CAP DELAY, OFF-RAMP DELAY, SYSTEM TRAVEL TIME, and TRAVEL DISTANCE.

AVERAGE SYSTEM SPEED = 28. MPH.
 AVERAGE DENSITY = 66. VPMP/L
 TOTAL FUEL = 9355. GALLONS
 TOTAL EMISSIONS = 2640. KI LOGRAMS

US-101_NB_AM_NP_2040_PE
 33. MPH.
 53. VPMP/L
 18739. GALLONS
 5167. KI LOGRAMS

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|--------|------------|-------|------------|--------|------------|--------|------------|--------|
| 1 | 0.01 | 2 | ***** | 3 | 122.66 | 4 | 40.31 | 5 | 64.58 |
| 6 | 130.90 | 7 | 44.64 | 8 | 62.41 | 9 | 61.98 | 10 | 150.83 |
| 11 | 44.21 | 12 | 42.48 | 13 | 78.02 | 14 | 59.09 | 15 | 45.84 |
| 16 | 16.26 | 17 | 20.35 | 18 | 14.82 | 19 | 29.11 | 20 | 2.71 |
| 21 | 2.78 | 22 | 2.44 | 23 | 28.72 | 24 | 54.23 | 25 | 48.34 |
| 26 | 35.77 | 27 | 32.27 | 28 | 38.06 | 29 | 417.31 | 30 | 12.18 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 3284.0 VEH-HRS ***** AVERAGE DELAY = 36.69 MIN/VEH *****

***** RAMP DELAYS *****

| | | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|---------|---|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|
| ON-RAMP | 2 | RAMP | 100. | 100.00 | 6.56 | 35.71 | 2.22 | 11.58 | 14.41 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 100.00 | 6.56 | 35.71 | 2.22 | 11.58 | 14.41 |
| ON-RAMP | 6 | RAMP | 100. | 100.00 | 9.00 | 35.71 | 2.22 | 11.58 | 14.41 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 100.00 | 9.00 | 35.71 | 2.22 | 11.58 | 14.41 |


```

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQQ QQQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 2222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*QQ 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 11111111 2222222222 PPP LLLLLLLLLL
    
```

FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 2 AND 29 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 35
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 2.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

**
** FREEWAY AND ARTERIAL DESIGN FEATURES **
**

| SUB NO. | SSEC | SSEC | DESIGN | ORG | TRK | SSEC | PCT | PCT | DES | SPECIAL | FF SPD. | CAP. | ART | GRADE | SUBSECTION | LOCATION |
|---------|------|-------|--------|-----|-----|------|-----|--------|------|---------|----------|----------|------|----------|--------------------------|----------|
| SEC | LNS | CAP | LENGTH | DES | FAC | GRAD | TRK | TRUCKS | RAMP | | ALT. RTE | ALT. RTE | TYPE | ALT. RTE | | |
| ** 1 | | | | | | | | | | | | | | | | |
| ** 2 | 2 | 3000. | 99999. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | ** |
| ** 3 | 2 | 3000. | 2830. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-87 to DLC loop-on | ** |
| ** 4 | 2 | 3000. | 930. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | DLC loop on to dia-on | ** |
| ** 5 | 2 | 3000. | 1490. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | DLC dia-on to Tomas off | ** |
| ** 6 | 2 | 3000. | 3020. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas off to on | ** |
| ** 7 | 2 | 3000. | 1030. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas on to bowers off | ** |
| ** 8 | 2 | 3000. | 1440. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers off to loop-on | ** |
| ** 9 | 2 | 3000. | 1430. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers loop-on to dia | ** |
| ** 10 | 2 | 3000. | 3480. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers dia-on to law-off | ** |
| ** 11 | 2 | 3000. | 1020. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Law off to loop-on | ** |
| ** 12 | 2 | 3000. | 980. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Lawr Loop to diag | ** |
| ** 13 | 2 | 3000. | 1800. | 65 | | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Lawrence On-ramp | ** |
| ** 14 | 2 | 3000. | 1500. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks Off-Ramp | ** |
| ** 15 | 2 | 3000. | 1300. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Fair Oaks | ** |
| ** 16 | 2 | 3000. | 1000. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Fair Oaks On-Ramp | ** |
| ** 17 | 2 | 3000. | 1100. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Mathilda | ** |
| ** 18 | 2 | 3000. | 1000. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda NB Off-Ramp | ** |

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```

**
** 19 2 3000. 900. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Mathilda / Mathilda **
** 20 2 3000. 100. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Mathilda NB On-Ramp **
**
*****

```

FREEWAY AND ARTERIAL DESIGN FEATURES

```

**
** SUB NO. SSEC SSEC DESIG DES TRK SSEC PCT PCT DES SPECIAL FF.SPD. CAP. ART GRADE SUBSECTI ON LOCATI ON **
** SEC LNS CAP LENGTH SPEED DES FAC GRAD TRK TRUCKS RAMP ALT. RTE ALT. RTE TYPE ALT. RTE **
**
** 21 2 3000. 100. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Mathilda / Mathilda **
** 22 2 3000. 100. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Mathilda SB Off-ramp **
** 23 2 3000. 700. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Mathilda / SR-237 **
** 24 2 3000. 1500. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 SR-237 WB Off-Ramp **
** 25 2 3000. 800. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 SR-237 / SR-237 **
** 26 2 3000. 1000. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 SR-237 WB On-Ramp **
** 27 2 3000. 800. 65 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 SR-237 / Ellis **
** 28 2 3000. 1000. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Ellis Off-ramp **
** 29 2 3000. 8000. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 HOV Dummy **
** 30 **
** 31 **
** 32 **
**
*****

```

FREEWAY TRAVEL TIME (MINUTES)

```

* ORIGIN S DESTINATIONS ACROSS *
* DOWN 1 2 3 4 5 6 7 8 *
+
* * * * *
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 2 * 0.00 21.14 21.91 22.12 22.51 23.14 24.54 0.00 *
+
* 3 * 0.00 0.00 0.00 0.00 0.00 0.00 3.16 0.00 *
+
* 4 * 0.00 0.00 0.00 0.00 0.00 0.00 2.47 0.00 *
+
* 5 * 0.00 0.00 0.00 0.00 0.00 0.00 1.89 0.00 *
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
* * * * *

```

US-101_NB_AM_NP_2040_PL

Table with columns: SUB NO., SSEC, O-D DATA DEMANDS, ADJUSTED VOLUMES, SSEC, WEAVE, CONGEST, STORAGE, V/C, SPEED, DENSITY, LOS, FUEL, EMISSIONS. Includes summary row: TOTAL 140349. = 26.6 MILES MAX(V/C) = 0.62 LOWEST LOS = B AVG = 65. 14.0 20.0 13.7

Summary table with columns: CURRENT TIME SLICE, CUMULATIVE VALUES. Rows include: FREeway TRAVEL TIME, FREeway MERGE DELAY, ON-RAMP MRG/CAP DELAY, OFF-RAMP DELAY, TOTAL SYSTEM TRAVEL TIME, TOTAL FRWAY TRAVEL DISTANCE, AVERAGE SYSTEM SPEED, AVERAGE DENSITY, TOTAL FUEL, TOTAL EMISSIONS.

Table with columns: SUBJECT ION, DELAY. Rows 1-32. Summary: ***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

FREeway TRAVEL TIME (MINUTES)

Table with columns: ORIG I NS, DEST I NAT I ONS ACROSS. Rows 1, 2. Summary: * 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 * 2 * 0.00 21.14 21.91 22.12 22.51 23.14 24.54 0.00


```

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQQ QQQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP EEEEEEEEE
    
```

FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 35
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREWAY AND ARTERIAL DESIGN FEATURES

| ** SUB NO. | ** SSEC | ** SSEC | ** DESIG N | ** ORG | ** TRK | ** SSEC | ** PCT | ** PCT | ** DES | ** SPECIAL | ** FF. SPD. | ** CAP. | ** ART | ** GRADE | ** SUBSECTI ON | ** LOCATI ON |
|------------|---------|---------|------------|----------|--------|---------|--------|-----------|---------|-------------|-------------|---------|-------------|-------------|--------------------------|--------------|
| ** SEC | ** LNS | ** CAP | ** LENGTH | ** SPEED | ** DES | ** GRAD | ** TRK | ** TRUCKS | ** RAMP | ** ALT. RTE | ** ALT. RTE | ** TYPE | ** ALT. RTE | ** ALT. RTE | ** | ** |
| ** 1 | 5 | 12500. | 500. | 65 | OD | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Seeding | ** |
| ** 2 | 3 | 8660. | 99999. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | ** |
| ** 3 | 3 | 7000. | 2830. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-87 to DLC loop-on | ** |
| ** 4 | 3 | 7000. | 930. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | DLC loop on to dia-on | ** |
| ** 5 | 3 | 7000. | 1490. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | DLC dia-on to Tomas off | ** |
| ** 6 | 3 | 7000. | 3020. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas off to on | ** |
| ** 7 | 3 | 7000. | 1030. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas on to bowers off | ** |
| ** 8 | 3 | 7000. | 1440. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers off to loop-on | ** |
| ** 9 | 3 | 7000. | 1430. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers loop-on to dia | ** |
| ** 10 | 3 | 7000. | 3480. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers dia-on to law-off | ** |
| ** 11 | 3 | 7000. | 1020. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Law off to loop-on | ** |
| ** 12 | 3 | 7000. | 980. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawr Loop to diag | ** |
| ** 13 | 3 | 7000. | 1800. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Lawrence On-ramp | ** |
| ** 14 | 3 | 7000. | 1500. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks Off-Ramp | ** |
| ** 15 | 3 | 6000. | 1300. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Fair Oaks | ** |
| ** 16 | 3 | 6000. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Fair Oaks On-Ramp | ** |
| ** 17 | 3 | 6000. | 1100. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Mathilda | ** |
| ** 18 | 4 | 7860. | 1000. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda NB Off-Ramp | ** |
| ** 19 | 3 | 6000. | 900. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | ** |
| ** 20 | 3 | 6000. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda NB On-Ramp | ** |

FREeway AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT TRUCKS | DES RAMP | SPECIAL | FF.SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION LOCATION |
|---------|----------|----------|-------------|--------------|---------|---------|-----------|---------|------------|----------|---------|------------------|---------------|----------|----------------|----------------------|
| ** 21 | 3 | 6000. | 100. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda |
| ** 22 | 3 | 6000. | 100. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | | 0.0 | 0. | GOOD | 0.0 | Mathilda SB Off-ramp |
| ** 23 | 3 | 6000. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | | 0.0 | 0. | GOOD | 0.0 | Mathilda / SR-237 |
| ** 24 | 3 | 6000. | 1500. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | | 0.0 | 0. | GOOD | 0.0 | SR-237 WB Off-Ramp |
| ** 25 | 3 | 6000. | 800. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | | 0.0 | 0. | GOOD | 0.0 | SR-237 / SR-237 |
| ** 26 | 3 | 6000. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | | 0.0 | 0. | GOOD | 0.0 | SR-237 WB On-Ramp |
| ** 27 | 3 | 6000. | 800. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | | 0.0 | 0. | GOOD | 0.0 | SR-237 / Ellis |
| ** 28 | 3 | 6000. | 1000. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | | 0.0 | 0. | GOOD | 0.0 | Ellis Off-ramp |
| ** 29 | 3 | 6000. | 8000. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** 30 | 5 | 10000. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | NO | | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** 31 | 5 | 6000. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | | 0.0 | 0. | GOOD | 0.0 | Dummy Bottleneck |
| ** 32 | 5 | 6000. | 2640. | 65 | D | 1.00 | 0.0 | 0 | 0 | NO | | 0.0 | 0. | GOOD | 0.0 | End of Network |

***** INPUT HAS BEEN COMPLETED *****

| | | |
|----------------------------|----|-----------|
| QUEUE COLLISION IN SECTION | 16 | T2 =0.659 |
| QUEUE COLLISION IN SECTION | 15 | T2 =0.448 |
| QUEUE COLLISION IN SECTION | 14 | T2 =0.461 |
| QUEUE COLLISION IN SECTION | 3 | T2 =0.861 |

FREeway TRAVEL TIME (MINUTES)

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | |
|--------------|---------------------|-------|-------|-------|-------|-------|
| | 1 | 2 | 3 | 4 | 5 | 6 |
| * 1 * | 0.09 | 31.54 | 33.88 | 35.93 | 38.43 | 47.50 |
| * 2 * | 0.00 | 0.00 | 1.45 | 3.50 | 6.00 | 15.07 |
| * 3 * | 0.00 | 0.00 | 0.00 | 1.50 | 4.00 | 13.07 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 1.73 | 10.80 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.80 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.64 |

 *
 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *
 *
 * SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMI SS *
 * SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP EFF LENGTH RATE RATIO MPH VPMP L LEVEL MPG GS/VM *
 *
 * 1 5 500. 9730. 1849. 9730. 9730. 1849. 9730. 12500. 0. 0. 0. .78 64. 30.6 D 19.8 13.5 *
 * 2 3 99999. 0. 0. 7881. 0. 0. 4246. 8660. 0. * 12700. 3635. .49 53. 26.5 F 21.7 12.2 *
 * 3 3 2830. 0. 0. 7881. 0. 0. 4246. 7000. 0. ** 2830. 2754. .61 35. 41.0 F 21.5 12.5 *
 * 4 3 930. 0. 0. 7881. 0. 0. 4246. 7000. 0. ** 930. 2754. .61 32. 44.7 F 21.0 12.9 *
 * 5 3 1490. 0. 0. 7881. 0. 0. 4246. 7000. 0. ** 1490. 2754. .61 30. 47.1 F 20.6 13.1 *
 * 6 3 3020. 0. 0. 7881. 0. 0. 4246. 7000. 0. ** 3020. 2754. .61 27. 51.9 F 20.0 13.6 *
 * 7 3 1030. 0. 0. 7881. 0. 0. 4246. 7000. 0. ** 1030. 2754. .61 25. 56.3 F 19.5 14.1 *
 * 8 3 1440. 0. 0. 7881. 0. 0. 4246. 7000. 0. ** 1440. 2754. .61 24. 59.1 F 19.1 14.3 *
 * 9 3 1430. 0. 0. 7881. 0. 0. 4246. 7000. 0. ** 1430. 2754. .61 23. 62.5 F 18.7 14.7 *
 * 10 3 3480. 0. 0. 7881. 0. 0. 4246. 7000. 0. ** 3480. 2754. .61 21. 68.4 F 18.1 15.3 *
 * 11 3 1020. 0. 0. 7881. 0. 0. 4246. 7000. 0. ** 1020. 2754. .61 19. 74.1 F 17.5 15.8 *
 * 12 3 980. 0. 0. 7881. 0. 0. 4246. 7000. 0. ** 980. 2754. .61 18. 76.8 F 17.3 16.1 *
 * 13 3 1800. 0. 0. 7881. 0. 0. 4246. 7000. 0. ** 1800. 2754. .61 18. 80.6 F 16.9 16.5 *
 * 14 3 1500. 0. 801. 7881. 0. 692. 4246. 6812. 0. ** 1500. 2566. .62 18. 78.7 F 17.3 16.4 *
 * 15 3 1300. 0. 0. 7080. 0. 0. 3554. 6000. 0. ** 1300. 2446. .59 17. 70.9 F 16.4 16.8 *
 * 16 3 1000. 864. 0. 7944. 764. 0. 4318. 5874. 0. ** 1000. 1556. .74 29. 49.6 F 20.6 13.6 *
 * 17 3 1100. 0. 0. 7944. 0. 0. 4318. 6000. 0. ** 1100. 1556. .72 27. 52.4 F 19.9 14.1 *
 * 18 4 1000. 0. 1127. 7944. 0. 836. 4318. 7628. 0. ** 1000. 1556. .57 19. 57.0 F 15.4 17.6 *
 * 19 3 900. 0. 0. 6817. 0. 0. 3482. 6000. 0. ** 900. 1556. .58 19. 62.7 F 15.8 17.3 *
 * 20 3 100. 256. 0. 7073. 240. 0. 3722. 5956. 0. ** 100. 1556. .62 20. 62.9 F 17.0 16.6 *
 * 21 3 100. 0. 0. 7073. 0. 0. 3722. 6000. 0. ** 100. 1556. .62 19. 63.9 F 16.8 16.7 *
 * 22 3 100. 0. 0. 7073. 0. 0. 3722. 6000. 0. ** 100. 1556. .62 19. 64.3 F 16.8 16.8 *
 * 23 3 700. 0. 0. 7073. 0. 0. 3722. 6000. 0. ** 700. 1556. .62 19. 65.8 F 16.7 16.9 *
 * 24 3 1500. 0. 1089. 7073. 0. 816. 3722. 5785. 0. ** 1500. 1556. .64 19. 66.0 F 17.0 16.8 *
 * 25 3 800. 0. 0. 5984. 0. 0. 2906. 6000. 0. ** 800. 1556. .48 12. 81.7 F 12.8 20.2 *
 * 26 3 1000. 1181. 0. 7165. 1181. 0. 4087. 5751. 0. ** 1000. 1556. .71 20. 69.3 F 17.8 16.3 *
 * 27 3 800. 0. 0. 7165. 0. 0. 4087. 6000. 0. ** 800. 1556. .68 18. 76.7 F 16.8 17.3 *
 * 28 3 1000. 0. 647. 7165. 0. 516. 4087. 5897. 0. ** 1000. 1556. .69 18. 77.0 F 16.9 17.2 *
 * 29 3 8000. 0. 0. 6518. 0. 0. 3571. 6000. 0. ** 8000. 1556. .60 11. 108.3 F 13.0 21.6 *
 * 30 5 100. 1529. 0. 8047. 1529. 0. 5100. 10000. 0. ** 100. 1556. .51 7. 148.0 F 9.8 26.4 *
 * 31 5 1000. 1000. 0. 9047. 900. 0. 6000. 6000. 0. 0. 0. 1.00 65. 18.5 E 19.2 14.0 *
 * 32 5 2640. 0. 9047. 9047. 0. 6000. 6000. 6000. 0. 0. 0. 1.00 65. 18.5 E 20.0 13.7 *
 *
 *
 * TOTAL 144589. = 27.4 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 39. 38.9 20.6 13.1 *
 *

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 1 OF 2

CURRENT TIME SLICE CUMULATIVE VALUES

| | | | | |
|----------------------------|-----------------|------------------|-----------------|------------------|
| FREWAY TRAVEL TIME = | 4911. VEH-HRS | 4932. PASS-HRS | 4911. VEH-HRS | 4932. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 108. VEH-HRS | 118. PASS-HRS | 108. VEH-HRS | 118. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 5019. VEH-HRS | 5050. PASS-HRS | 5019. VEH-HRS | 5050. PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 192479. VEH-MI. | 193542. PASS-MI. | 192479. VEH-MI. | 193542. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 38. MPH | | 39. MPH | |
| AVERAGE DENSITY = | 39. VPMP | | 39. VPMP | |
| TOTAL FUEL = | 9404. GALLONS | | 9404. GALLONS | |
| TOTAL EMISSIONS = | 2529. KILOGRAMS | | 2529. KILOGRAMS | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|--------|------------|-------|------------|--------|------------|--------|
| 1 | 0.30 | 2 | 492.32 | 3 | 47.46 | 4 | 18.28 | 5 | 32.07 |
| 6 | 75.47 | 7 | 28.95 | 8 | 43.20 | 9 | 46.06 | 10 | 125.23 |
| 11 | 40.23 | 12 | 40.16 | 13 | 77.62 | 14 | 61.53 | 15 | 50.56 |
| 16 | 19.22 | 17 | 23.15 | 18 | 36.95 | 19 | 28.38 | 20 | 3.02 |
| 21 | 3.09 | 22 | 3.11 | 23 | 22.39 | 24 | 47.63 | 25 | 37.05 |
| 26 | 31.44 | 27 | 28.74 | 28 | 35.84 | 29 | 437.56 | 30 | 12.54 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 1949.5 VEH-HRS ***** AVERAGE DELAY = 29.34 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-----------|-----------------------|---------------|--------------------------------|----------|---------|---------|----------|----------------------|
| ON-RAMP 2 | RAMP 100. | 50.00 | 3.47 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | FREWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 100. | 50.00 | 3.47 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| ON-RAMP 3 | RAMP 16. | 8.00 | 1.88 | 2.86 | 0.18 | 0.93 | 0.05 | 1.15 |
| | FREWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 16. | 8.00 | 1.88 | 2.86 | 0.18 | 0.93 | 0.05 | 1.15 |
| ON-RAMP 6 | RAMP 100. | 50.00 | 3.70 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | FREWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 100. | 50.00 | 3.70 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |

**
** FREeway TRAVEL TIME (MINUTES) **
**

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | |
|-----------|--|-----------------------|-------|-------|-------|-------|-------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 |
| * 1 * | | 0.09 | 44.78 | 47.01 | 49.33 | 52.06 | 60.26 |
| * 2 * | | 0.00 | 0.00 | 1.46 | 3.78 | 6.51 | 14.72 |
| * 3 * | | 0.00 | 0.00 | 0.00 | 1.61 | 4.34 | 12.55 |
| * 4 * | | 0.00 | 0.00 | 0.00 | 0.00 | 1.83 | 10.04 |
| * 5 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.79 |
| * 6 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.64 |

* TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB | * NO. | * SSEC | * O-D | * DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | |
|---------|-------|-----------|-----------------|---------|-----------|------------|-----------|---------|-------------------|-----------|------------------|---------|-------------|-----------|---------|--------|-------------|--|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * SSEC | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | |
| * 1 | * 5 | * 500. | * 8240. | * 1566. | * 8240. | * 8240. | * 1566. | * 8240. | * 12500. | * 0. | * 0. | * .66 | * 65. | * 25.4 | * C | * 19.2 | * 14.0 | |
| * 2 | * 3 | * 99999. | * 0. | * 0. | * 6674. | * 0. | * 0. | * 5758. | * 8660. | * 0. | * 24393. | * .66 | * 36. | * 53.5 | * F | * 18.4 | * 15.0 | |
| * 3 | * 3 | * 2830. | * 0. | * 0. | * 6674. | * 0. | * 0. | * 5758. | * 7000. | * 0. | * 2830. | * .82 | * 18. | * 105.3 | * F | * 17.7 | * 17.1 | |
| * 4 | * 3 | * 930. | * 0. | * 0. | * 6674. | * 0. | * 0. | * 5758. | * 7000. | * 0. | * 930. | * .82 | * 18. | * 105.3 | * F | * 17.7 | * 17.1 | |
| * 5 | * 3 | * 1490. | * 0. | * 0. | * 6674. | * 0. | * 0. | * 5758. | * 7000. | * 0. | * 1490. | * .82 | * 18. | * 105.3 | * F | * 17.7 | * 17.1 | |
| * 6 | * 3 | * 3020. | * 0. | * 0. | * 6674. | * 0. | * 0. | * 5758. | * 7000. | * 0. | * 3020. | * .82 | * 18. | * 105.3 | * F | * 17.7 | * 17.1 | |
| * 7 | * 3 | * 1030. | * 0. | * 0. | * 6674. | * 0. | * 0. | * 5758. | * 7000. | * 0. | * 1030. | * .82 | * 18. | * 105.3 | * F | * 17.7 | * 17.1 | |
| * 8 | * 3 | * 1440. | * 0. | * 0. | * 6674. | * 0. | * 0. | * 5758. | * 7000. | * 0. | * 1440. | * .82 | * 18. | * 105.3 | * F | * 17.7 | * 17.1 | |
| * 9 | * 3 | * 1430. | * 0. | * 0. | * 6674. | * 0. | * 0. | * 5758. | * 7000. | * 0. | * 1430. | * .82 | * 18. | * 105.3 | * F | * 17.7 | * 17.1 | |
| * 10 | * 3 | * 3480. | * 0. | * 0. | * 6674. | * 0. | * 0. | * 5758. | * 7000. | * 0. | * 3480. | * .82 | * 18. | * 105.3 | * F | * 17.7 | * 17.1 | |
| * 11 | * 3 | * 1020. | * 0. | * 0. | * 6674. | * 0. | * 0. | * 5758. | * 7000. | * 0. | * 1020. | * .82 | * 18. | * 105.3 | * F | * 17.7 | * 17.1 | |
| * 12 | * 3 | * 980. | * 0. | * 0. | * 6674. | * 0. | * 0. | * 5758. | * 7000. | * 0. | * 980. | * .82 | * 18. | * 105.3 | * F | * 17.7 | * 17.1 | |
| * 13 | * 3 | * 1800. | * 0. | * 0. | * 6674. | * 0. | * 0. | * 5758. | * 7000. | * 0. | * 1800. | * .82 | * 18. | * 105.3 | * F | * 17.7 | * 17.1 | |
| * 14 | * 3 | * 1500. | * 0. | * 727. | * 6674. | * 0. | * 727. | * 5758. | * 6829. | * 0. | * 1500. | * .84 | * 20. | * 98.4 | * F | * 18.3 | * 16.3 | |
| * 15 | * 3 | * 1300. | * 0. | * 0. | * 5947. | * 0. | * 0. | * 5031. | * 6000. | * 0. | * 1300. | * .84 | * 19. | * 87.3 | * F | * 18.1 | * 16.5 | |
| * 16 | * 3 | * 1000. | * 814. | * 0. | * 6761. | * 814. | * 0. | * 5845. | * 5904. | * 0. | * 1000. | * .99 | * 34. | * 58.1 | * F | * 22.3 | * 12.1 | |
| * 17 | * 3 | * 1100. | * 0. | * 0. | * 6761. | * 0. | * 0. | * 5845. | * 6000. | * 0. | * 1100. | * .97 | * 31. | * 62.0 | * F | * 21.8 | * 12.5 | |
| * 18 | * 4 | * 1000. | * 0. | * 1543. | * 6761. | * 0. | * 1342. | * 5845. | * 7546. | * 0. | * 1000. | * .77 | * 16. | * 93.6 | * F | * 16.5 | * 18.5 | |
| * 19 | * 3 | * 900. | * 0. | * 0. | * 5218. | * 0. | * 0. | * 4503. | * 6000. | * 0. | * 900. | * .75 | * 14. | * 103.7 | * F | * 15.9 | * 19.3 | |
| * 20 | * 3 | * 100. | * 352. | * 0. | * 5570. | * 268. | * 0. | * 4771. | * 5945. | * 0. | * 100. | * .80 | * 17. | * 93.2 | * F | * 17.1 | * 17.7 | |
| * 21 | * 3 | * 100. | * 0. | * 0. | * 5570. | * 0. | * 0. | * 4771. | * 6000. | * 0. | * 100. | * .80 | * 17. | * 95.4 | * F | * 17.0 | * 17.9 | |
| * 22 | * 3 | * 100. | * 0. | * 0. | * 5570. | * 0. | * 0. | * 4771. | * 6000. | * 0. | * 100. | * .80 | * 17. | * 95.4 | * F | * 17.0 | * 17.9 | |
| * 23 | * 3 | * 700. | * 0. | * 0. | * 5570. | * 0. | * 0. | * 4771. | * 6000. | * 0. | * 700. | * .80 | * 17. | * 95.4 | * F | * 17.0 | * 17.9 | |
| * 24 | * 3 | * 1500. | * 0. | * 1119. | * 5570. | * 0. | * 968. | * 4771. | * 5789. | * 0. | * 1500. | * .82 | * 18. | * 86.8 | * F | * 17.7 | * 17.0 | |
| * 25 | * 3 | * 800. | * 0. | * 0. | * 4451. | * 0. | * 0. | * 3803. | * 6000. | * 0. | * 800. | * .63 | * 10. | * 125.5 | * F | * 13.2 | * 22.7 | |
| * 26 | * 3 | * 1000. | * 960. | * 0. | * 5411. | * 960. | * 0. | * 4763. | * 5805. | * 0. | * 1000. | * .82 | * 18. | * 87.7 | * F | * 17.6 | * 17.1 | |
| * 27 | * 3 | * 800. | * 0. | * 0. | * 5411. | * 0. | * 0. | * 4763. | * 6000. | * 0. | * 800. | * .79 | * 17. | * 95.6 | * F | * 16.9 | * 18.0 | |
| * 28 | * 3 | * 1000. | * 0. | * 650. | * 5411. | * 0. | * 580. | * 4763. | * 5902. | * 0. | * 1000. | * .81 | * 17. | * 91.7 | * F | * 17.3 | * 17.6 | |
| * 29 | * 3 | * 8000. | * 0. | * 0. | * 4761. | * 0. | * 0. | * 4183. | * 6000. | * 0. | * 8000. | * .70 | * 12. | * 113.7 | * F | * 14.4 | * 21.0 | |
| * 30 | * 5 | * 100. | * 1117. | * 0. | * 5878. | * 1117. | * 0. | * 5300. | * 10000. | * 0. | * 100. | * .53 | * 7. | * 144.9 | * F | * 10.1 | * 26.0 | |
| * 31 | * 5 | * 1000. | * 700. | * 0. | * 6578. | * 700. | * 0. | * 6000. | * 6000. | * 0. | * 0. | * 1.00 | * 65. | * 18.5 | * E | * 19.2 | * 14.0 | |
| * 32 | * 5 | * 2640. | * 0. | * 6578. | * 6578. | * 0. | * 6000. | * 6000. | * 6000. | * 0. | * 0. | * 1.00 | * 65. | * 18.5 | * E | * 20.0 | * 13.7 | |
| * TOTAL | | * 144589. | * = 27.4 MI LBS | | | | | | * MAX(V/C) = 1.00 | | * LOWEST LOS = F | | * AVG = 29. | | * 66.1 | | * 18.1 15.6 | |

FREeway TRAVEL TIME = 5879. VEH-HRS
FREeway MERGE DELAY = 0. VEH-HRS

CURRENT TIME SLICE
5901. PASS-HRS
0. PASS-HRS

CUMULATIVE VALUES
10790. VEH-HRS
0. VEH-HRS

10834. PASS-HRS
0. PASS-HRS

US-101_NB_AM_P1_2040_PE

ON-RAMP MRG/CAP DELAY = 258. VEH-HRS 277. PASS-HRS 366. VEH-HRS 395. PASS-HRS
 OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
 TOTAL SYSTEM TRAVEL TIME = 6137. VEH-HRS 6178. PASS-HRS 11156. VEH-HRS 11228. PASS-HRS
 TOTAL TRAV DISTANCE = 168179. VEH-MI. 169223. PASS-MI. 360657. VEH-MI. 362765. PASS-MI.
 AVERAGE SYSTEM SPEED = 27. MPH. 33. MPH.
 AVERAGE DENSITY = 66. VPMP 53. VPMP
 TOTAL FUEL = 9388. GALLONS 18792. GALLONS
 TOTAL EMISSIONS = 2654. KI LOGRAMS 5183. KI LOGRAMS

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|--------|------------|-------|------------|--------|------------|--------|------------|--------|
| 1 | 0.01 | 2 | ***** | 3 | 121.90 | 4 | 40.06 | 5 | 64.18 |
| 6 | 130.09 | 7 | 44.37 | 8 | 62.03 | 9 | 61.60 | 10 | 149.90 |
| 11 | 43.94 | 12 | 42.21 | 13 | 77.54 | 14 | 58.69 | 15 | 45.44 |
| 16 | 15.97 | 17 | 20.01 | 18 | 53.89 | 19 | 41.25 | 20 | 3.90 |
| 21 | 4.03 | 22 | 4.03 | 23 | 28.22 | 24 | 53.15 | 25 | 48.19 |
| 26 | 35.96 | 27 | 32.37 | 28 | 38.20 | 29 | 419.29 | 30 | 12.18 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 3292.0 VEH-HRS ***** AVERAGE DELAY = 36.83 MIN/VEH *****

***** RAMP DELAYS *****

| | | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-----------|---------|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|
| ON-RAMP 2 | RAMP | 100. | 100.00 | 6.56 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 100.00 | 6.56 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP 3 | RAMP | 100. | 58.00 | 9.46 | 20.71 | 1.28 | 6.72 | 0.36 | 8.36 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 58.00 | 9.46 | 20.71 | 1.28 | 6.72 | 0.36 | 8.36 |
| ON-RAMP 6 | RAMP | 100. | 100.00 | 9.00 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 100.00 | 9.00 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |

US-101_NB_AM_P1_2040_PL

| * SUB SEC | * NO. LNS | * SSEC LENGTH | * O-D ORG | * DATA DES | * DEMANDS SSEC | * ADJUSTED ORG | * VOLUMES DES | * SSEC SSEC | * WEAVE CAP. | * CONGEST EFF | * STORAGE LENGTH | * V/C RATE | * SPEED MPH | * DENSITY VPMP | * LOS LEVEL | * FUEL MPG | * EMISSIONS GS/VM | |
|-----------|-----------|---------------|-----------|------------|----------------|----------------|---------------|-------------|--------------|-----------------|------------------|----------------|-------------|----------------|-------------|------------|-------------------|------|
| * 1 | | | | | | | | | | | | | | | | | | |
| * 2 | 2 | 99999. | 1849. | 0. | 1849. | 1849. | 0. | 1849. | 3000. | 0. | 0. | 0. | .62 | 65. | 14.2 | B | 20.0 | 13.7 |
| * 3 | 2 | 2830. | 0. | 0. | 1849. | 0. | 0. | 1849. | 3000. | 0. | 0. | 0. | .62 | 65. | 14.2 | B | 20.0 | 13.7 |
| * 4 | 2 | 930. | 0. | 0. | 1849. | 0. | 0. | 1849. | 3000. | 0. | 0. | 0. | .62 | 65. | 14.2 | B | 20.0 | 13.7 |
| * 5 | 2 | 1490. | 0. | 0. | 1849. | 0. | 0. | 1849. | 3000. | 0. | 0. | 0. | .62 | 65. | 14.2 | B | 20.0 | 13.7 |
| * 6 | 2 | 3020. | 0. | 0. | 1849. | 0. | 0. | 1849. | 3000. | 0. | 0. | 0. | .62 | 65. | 14.2 | B | 20.0 | 13.7 |
| * 7 | 2 | 1030. | 0. | 0. | 1849. | 0. | 0. | 1849. | 3000. | 0. | 0. | 0. | .62 | 65. | 14.2 | B | 20.0 | 13.7 |
| * 8 | 2 | 1440. | 0. | 0. | 1849. | 0. | 0. | 1849. | 3000. | 0. | 0. | 0. | .62 | 65. | 14.2 | B | 20.0 | 13.7 |
| * 9 | 2 | 1430. | 0. | 0. | 1849. | 0. | 0. | 1849. | 3000. | 0. | 0. | 0. | .62 | 65. | 14.2 | B | 20.0 | 13.7 |
| * 10 | 2 | 3480. | 0. | 0. | 1849. | 0. | 0. | 1849. | 3000. | 0. | 0. | 0. | .62 | 65. | 14.2 | B | 20.0 | 13.7 |
| * 11 | 2 | 1020. | 0. | 0. | 1849. | 0. | 0. | 1849. | 3000. | 0. | 0. | 0. | .62 | 65. | 14.2 | B | 20.0 | 13.7 |
| * 12 | 2 | 980. | 0. | 0. | 1849. | 0. | 0. | 1849. | 3000. | 0. | 0. | 0. | .62 | 65. | 14.2 | B | 20.0 | 13.7 |
| * 13 | 2 | 1800. | 0. | 0. | 1849. | 0. | 0. | 1849. | 3000. | 0. | 0. | 0. | .62 | 65. | 14.2 | B | 20.0 | 13.7 |
| * 14 | 2 | 1500. | 0. | 188. | 1849. | 0. | 188. | 1849. | 3000. | 0. | 0. | 0. | .62 | 65. | 14.2 | B | 20.0 | 13.7 |
| * 15 | 2 | 1300. | 0. | 0. | 1661. | 0. | 0. | 1661. | 3000. | 0. | 0. | 0. | .55 | 65. | 12.8 | B | 20.0 | 13.7 |
| * 16 | 2 | 1000. | 126. | 0. | 1787. | 126. | 0. | 1787. | 3000. | 0. | 0. | 0. | .60 | 65. | 13.7 | B | 20.0 | 13.7 |
| * 17 | 2 | 1100. | 0. | 0. | 1787. | 0. | 0. | 1787. | 3000. | 0. | 0. | 0. | .60 | 65. | 13.7 | B | 20.0 | 13.7 |
| * 18 | 2 | 1000. | 0. | 232. | 1787. | 0. | 232. | 1787. | 3000. | 0. | 0. | 0. | .60 | 65. | 13.7 | B | 20.0 | 13.7 |
| * 19 | 2 | 900. | 0. | 0. | 1555. | 0. | 0. | 1555. | 3000. | 0. | 0. | 0. | .52 | 65. | 12.0 | B | 20.0 | 13.7 |
| * 20 | 2 | 100. | 44. | 0. | 1599. | 44. | 0. | 1599. | 3000. | 0. | 0. | 0. | .53 | 65. | 12.3 | B | 20.0 | 13.7 |
| * 21 | 2 | 100. | 0. | 0. | 1599. | 0. | 0. | 1599. | 3000. | 0. | 0. | 0. | .53 | 65. | 12.3 | B | 20.0 | 13.7 |
| * 22 | 2 | 100. | 0. | 0. | 1599. | 0. | 0. | 1599. | 3000. | 0. | 0. | 0. | .53 | 65. | 12.3 | B | 20.0 | 13.7 |
| * 23 | 2 | 700. | 0. | 0. | 1599. | 0. | 0. | 1599. | 3000. | 0. | 0. | 0. | .53 | 65. | 12.3 | B | 20.0 | 13.7 |
| * 24 | 2 | 1500. | 0. | 215. | 1599. | 0. | 215. | 1599. | 3000. | 0. | 0. | 0. | .53 | 65. | 12.3 | B | 20.0 | 13.7 |
| * 25 | 2 | 800. | 0. | 0. | 1384. | 0. | 0. | 1384. | 3000. | 0. | 0. | 0. | .46 | 65. | 10.6 | A | 20.0 | 13.7 |
| * 26 | 2 | 1000. | 249. | 0. | 1632. | 249. | 0. | 1632. | 3000. | 0. | 0. | 0. | .54 | 65. | 12.6 | B | 20.0 | 13.7 |
| * 27 | 2 | 800. | 0. | 0. | 1632. | 0. | 0. | 1632. | 3000. | 0. | 0. | 0. | .54 | 65. | 12.6 | B | 20.0 | 13.7 |
| * 28 | 2 | 1000. | 0. | 103. | 1632. | 0. | 103. | 1632. | 3000. | 0. | 0. | 0. | .54 | 65. | 12.6 | B | 20.0 | 13.7 |
| * 29 | 2 | 8000. | 0. | 1529. | 1529. | 0. | 1529. | 1529. | 3000. | 0. | 0. | 0. | .51 | 65. | 11.8 | B | 20.0 | 13.7 |
| * 30 | | | | | | | | | | | | | | | | | | |
| * 31 | | | | | | | | | | | | | | | | | | |
| * 32 | | | | | | | | | | | | | | | | | | |
| * TOTAL | 140349. | = | 26.6 | MI L E S | | | | | | MAX(V/C) = 0.62 | | LOWEST LOS = B | | AVG = 65. | 14.0 | | 20.0 | 13.7 |

| | | | | | | | | |
|-----------------------------|--------|------------|--------|-------------------|--------|------------|--------|----------|
| CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | | |
| FREEWAY TRAVEL TIME = | 742. | VEH-HRS | 1484. | PASS-HRS | 742. | VEH-HRS | 1484. | PASS-HRS |
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 742. | VEH-HRS | 1484. | PASS-HRS | 742. | VEH-HRS | 1484. | PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 48220. | VEH-MI. | 96441. | PASS-MI. | 48220. | VEH-MI. | 96441. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 65. | MPH. | | | 65. | MPH. | | |
| AVERAGE DENSITY = | 14. | VPMP | | | 14. | VPMP | | |
| TOTAL FUEL = | 2411. | GALLONS | | | 2411. | GALLONS | | |
| TOTAL EMISSIONS = | 663. | KI LOGRAMS | | | 663. | KI LOGRAMS | | |

| | | | | | | | | | |
|--|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| ***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 ***** | | | | | | | | | |
| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | 30 | 0.00 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |
| ***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH ***** | | | | | | | | | |

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| ***** | | ***** | |
| ** | | ** | |
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| ***** | | ***** | |
| * ORIGINS | | * DESTINATIONS ACROSS | |
| * DOWN | | * DOWN | |
| * 1 | | * 2 | |
| * 2 | | * 3 | |
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| * 4 | | * 5 | |
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| * 99 | | * 100 | |


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FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQQ QQQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 PPP PPP EEE
FFFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP EEE
FFF RRR RRR EEE Q*UC* QQQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP EEEEEEEEE
    
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FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 35
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREWAY AND ARTERIAL DESIGN FEATURES

| ** SUB NO. | ** SSEC | ** SSEC | ** DESIG N | ** ORG | ** TRK | ** SSEC | ** PCT | ** PCT | ** DES | ** SPECIAL | ** FF. SPD. | ** CAP. | ** ART | ** GRADE | ** SUBSECTI ON | ** LOCATI ON |
|------------|---------|---------|------------|----------|--------|---------|--------|-----------|---------|-------------|-------------|---------|-------------|-------------|--------------------------|--------------|
| ** SEC | ** LNS | ** CAP | ** LENGTH | ** SPEED | ** DES | ** GRAD | ** TRK | ** TRUCKS | ** RAMP | ** ALT. RTE | ** ALT. RTE | ** TYPE | ** ALT. RTE | ** ALT. RTE | ** | ** |
| ** 1 | 5 | 12500. | 500. | 65 | OD | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Seeding | ** |
| ** 2 | 3 | 8660. | 99999. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | ** |
| ** 3 | 3 | 7000. | 2830. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-87 to DLC loop-on | ** |
| ** 4 | 3 | 7000. | 930. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | DLC loop on to dia-on | ** |
| ** 5 | 3 | 7000. | 1490. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | DLC dia-on to Tomas off | ** |
| ** 6 | 3 | 7000. | 3020. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas off to on | ** |
| ** 7 | 3 | 7000. | 1030. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas on to bowers off | ** |
| ** 8 | 3 | 7000. | 1440. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers off to loop-on | ** |
| ** 9 | 3 | 7000. | 1430. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers loop-on to dia | ** |
| ** 10 | 3 | 7000. | 3480. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers dia-on to law-off | ** |
| ** 11 | 3 | 7000. | 1020. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Law off to loop-on | ** |
| ** 12 | 3 | 7000. | 980. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawr Loop to diag | ** |
| ** 13 | 3 | 7000. | 1800. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Lawrence On-ramp | ** |
| ** 14 | 3 | 7000. | 1500. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks Off-Ramp | ** |
| ** 15 | 3 | 6000. | 1300. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Fair Oaks | ** |
| ** 16 | 3 | 6000. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Fair Oaks On-Ramp | ** |
| ** 17 | 3 | 6000. | 1100. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Mathilda | ** |
| ** 18 | 4 | 7860. | 1000. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda NB Off-Ramp | ** |
| ** 19 | 3 | 6000. | 900. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | ** |
| ** 20 | 3 | 6000. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda NB On-Ramp | ** |

FREeway AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT TRUCKS | DES RAMP | SPECIAL | FF.SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION | LOCATION |
|---------|----------|----------|-------------|--------------|---------|---------|-----------|---------|------------|----------|---------|------------------|---------------|----------|----------------|----------------------|----------|
| ** 21 | 3 | 6000. | 100. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | ** |
| ** 22 | 3 | 6000. | 100. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | | 0.0 | 0. | GOOD | 0.0 | Mathilda SB Off-ramp | ** |
| ** 23 | 3 | 6000. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | | 0.0 | 0. | GOOD | 0.0 | Mathilda / SR-237 | ** |
| ** 24 | 3 | 6000. | 1500. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | | 0.0 | 0. | GOOD | 0.0 | SR-237 WB Off-Ramp | ** |
| ** 25 | 3 | 6000. | 800. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | | 0.0 | 0. | GOOD | 0.0 | SR-237 / SR-237 | ** |
| ** 26 | 3 | 6000. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | | 0.0 | 0. | GOOD | 0.0 | SR-237 WB On-Ramp | ** |
| ** 27 | 3 | 6000. | 800. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | | 0.0 | 0. | GOOD | 0.0 | SR-237 / Ellis | ** |
| ** 28 | 3 | 6000. | 1000. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | | 0.0 | 0. | GOOD | 0.0 | Ellis Off-ramp | ** |
| ** 29 | 3 | 6000. | 8000. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | ** |
| ** 30 | 5 | 10000. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | NO | | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | ** |
| ** 31 | 5 | 6000. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | | 0.0 | 0. | GOOD | 0.0 | Dummy Bottleneck | ** |
| ** 32 | 5 | 6000. | 2640. | 65 | D | 1.00 | 0.0 | 0 | 0 | NO | | 0.0 | 0. | GOOD | 0.0 | End of Network | ** |

***** INPUT HAS BEEN COMPLETED *****

QUEUE COLLISION IN SECTION 16 T2 =0.661
 QUEUE COLLISION IN SECTION 15 T2 =0.449
 QUEUE COLLISION IN SECTION 14 T2 =0.461
 QUEUE COLLISION IN SECTION 3 T2 =0.862

FREeway TRAVEL TIME (MINUTES)

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | |
|--------------|---------------------|-------|-------|-------|-------|-------|
| | 1 | 2 | 3 | 4 | 5 | 6 |
| * 1 * | 0.09 | 31.51 | 33.83 | 35.89 | 38.38 | 47.43 |
| * 2 * | 0.00 | 0.00 | 1.44 | 3.49 | 5.98 | 15.04 |
| * 3 * | 0.00 | 0.00 | 0.00 | 1.50 | 4.00 | 13.05 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 1.73 | 10.78 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.80 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.64 |

 *
 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *
 *
 * SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMI SS *
 * SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP EFF LENGTH RATE RATIO MPH VPMP L LEVEL MPG GS/VM *
 *
 * 1 5 500. 9731. 1849. 9731. 9731. 1849. 9731. 12500. 0. 0. 0. .78 64. 30.6 D 19.8 13.5 *
 * 2 3 99999. 0. 0. 7882. 0. 0. 4253. 8660. 0. * 12689. 3629. .49 53. 26.5 F 21.7 12.2 *
 * 3 3 2830. 0. 0. 7882. 0. 0. 4253. 7000. 0. ** 2830. 2747. .61 35. 40.9 F 21.5 12.5 *
 * 4 3 930. 0. 0. 7882. 0. 0. 4253. 7000. 0. ** 930. 2747. .61 32. 44.6 F 21.0 12.9 *
 * 5 3 1490. 0. 0. 7882. 0. 0. 4253. 7000. 0. ** 1490. 2747. .61 30. 47.1 F 20.7 13.1 *
 * 6 3 3020. 0. 0. 7882. 0. 0. 4253. 7000. 0. ** 3020. 2747. .61 27. 51.8 F 20.0 13.6 *
 * 7 3 1030. 0. 0. 7882. 0. 0. 4253. 7000. 0. ** 1030. 2747. .61 25. 56.2 F 19.5 14.0 *
 * 8 3 1440. 0. 0. 7882. 0. 0. 4253. 7000. 0. ** 1440. 2747. .61 24. 59.0 F 19.2 14.3 *
 * 9 3 1430. 0. 0. 7882. 0. 0. 4253. 7000. 0. ** 1430. 2747. .61 23. 62.4 F 18.8 14.6 *
 * 10 3 3480. 0. 0. 7882. 0. 0. 4253. 7000. 0. ** 3480. 2747. .61 21. 68.3 F 18.1 15.2 *
 * 11 3 1020. 0. 0. 7882. 0. 0. 4253. 7000. 0. ** 1020. 2747. .61 19. 74.0 F 17.6 15.8 *
 * 12 3 980. 0. 0. 7882. 0. 0. 4253. 7000. 0. ** 980. 2747. .61 18. 76.7 F 17.3 16.1 *
 * 13 3 1800. 0. 0. 7882. 0. 0. 4253. 7000. 0. ** 1800. 2747. .61 18. 80.4 F 16.9 16.5 *
 * 14 3 1500. 0. 802. 7882. 0. 693. 4253. 6812. 0. ** 1500. 2559. .62 18. 78.6 F 17.3 16.3 *
 * 15 3 1300. 0. 0. 7080. 0. 0. 3560. 6000. 0. ** 1300. 2440. .59 17. 70.8 F 16.4 16.8 *
 * 16 3 1000. 864. 0. 7944. 764. 0. 4324. 5874. 0. ** 1000. 1550. .74 29. 49.4 F 20.6 13.6 *
 * 17 3 1100. 0. 0. 7944. 0. 0. 4324. 5874. 0. ** 1100. 1550. .72 28. 52.3 F 19.9 14.1 *
 * 18 4 1000. 0. 1128. 7944. 0. 837. 4324. 7628. 0. ** 1000. 1550. .57 19. 56.7 F 15.4 17.5 *
 * 19 3 900. 0. 0. 6816. 0. 0. 3487. 6000. 0. ** 900. 1550. .58 19. 62.4 F 15.8 17.3 *
 * 20 3 100. 230. 0. 7046. 230. 0. 3717. 5960. 0. ** 100. 1550. .62 20. 62.8 F 17.0 16.6 *
 * 21 3 100. 0. 0. 7046. 0. 0. 3717. 6000. 0. ** 100. 1550. .62 19. 63.7 F 16.8 16.7 *
 * 22 3 100. 0. 0. 7046. 0. 0. 3717. 6000. 0. ** 100. 1550. .62 19. 64.1 F 16.8 16.8 *
 * 23 3 700. 0. 0. 7046. 0. 0. 3717. 6000. 0. ** 700. 1550. .62 19. 65.6 F 16.6 16.9 *
 * 24 3 1500. 0. 1077. 7046. 0. 809. 3717. 5787. 0. ** 1500. 1550. .64 19. 66.0 F 17.0 16.8 *
 * 25 3 800. 0. 0. 5969. 0. 0. 2908. 6000. 0. ** 800. 1550. .48 12. 81.5 F 12.8 20.2 *
 * 26 3 1000. 1181. 0. 7150. 1181. 0. 4089. 5751. 0. ** 1000. 1550. .71 20. 69.2 F 17.8 16.3 *
 * 27 3 800. 0. 0. 7150. 0. 0. 4089. 6000. 0. ** 800. 1550. .68 18. 76.5 F 16.8 17.2 *
 * 28 3 1000. 0. 645. 7150. 0. 515. 4089. 5896. 0. ** 1000. 1550. .69 18. 76.9 F 16.9 17.2 *
 * 29 3 8000. 0. 0. 6505. 0. 0. 3574. 6000. 0. ** 8000. 1550. .60 11. 108.2 F 13.0 21.6 *
 * 30 5 100. 1526. 0. 8031. 1526. 0. 5100. 10000. 0. ** 100. 1550. .51 7. 148.0 F 9.8 26.4 *
 * 31 5 1000. 1000. 0. 9031. 900. 0. 6000. 6000. 0. 0. 0. 1.00 65. 18.5 E 19.2 14.0 *
 * 32 5 2640. 0. 9031. 9031. 0. 6000. 6000. 6000. 0. 0. 0. 1.00 65. 18.5 E 20.0 13.7 *
 *
 *
 * TOTAL 144589. = 27.4 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 39. 38.9 20.6 13.1 *
 *

CURRENT TIME SLICE CUMULATIVE VALUES
 FREEWAY TRAVEL TIME = 4907. VEH-HRS 4928. PASS-HRS 4907. VEH-HRS 4928. PASS-HRS
 FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
 ON-RAMP MRG/CAP DELAY = 100. VEH-HRS 110. PASS-HRS 100. VEH-HRS 110. PASS-HRS
 OFF-RAMP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
 TOTAL SYSTEM TRAVEL TIME = 5007. VEH-HRS 5038. PASS-HRS 5007. VEH-HRS 5038. PASS-HRS
 TOTAL TRAVEL DISTANCE = 192530. VEH-MI. 193591. PASS-MI. 192530. VEH-MI. 193591. PASS-MI.
 AVERAGE SYSTEM SPEED = 38. MPH 39. MPH
 AVERAGE DENSITY = 39. VPMP 39. VPMP
 TOTAL FUEL = 9400. GALLONS 9400. GALLONS
 TOTAL EMISSIONS = 2528. KILOGRAMS 2528. KILOGRAMS

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|--------|------------|-------|------------|--------|------------|--------|
| 1 | 0.30 | 2 | 491.99 | 3 | 47.20 | 4 | 18.20 | 5 | 31.92 |
| 6 | 75.16 | 7 | 28.84 | 8 | 43.05 | 9 | 45.90 | 10 | 124.82 |
| 11 | 40.11 | 12 | 40.04 | 13 | 77.39 | 14 | 61.33 | 15 | 50.40 |
| 16 | 19.08 | 17 | 22.99 | 18 | 36.72 | 19 | 28.22 | 20 | 3.02 |
| 21 | 3.08 | 22 | 3.10 | 23 | 22.34 | 24 | 47.60 | 25 | 36.94 |
| 26 | 31.35 | 27 | 28.67 | 28 | 35.73 | 29 | 436.89 | 30 | 12.54 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 1944.9 VEH-HRS ***** AVERAGE DELAY = 29.24 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-----------|-----------------------|---------------|--------------------------------|----------|---------|---------|----------|----------------------|
| ON-RAMP 2 | RAMP 100.00 | 50.00 | 3.47 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | FREEWAY 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 100.00 | 50.00 | 3.47 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| ON-RAMP 6 | RAMP 100.00 | 50.00 | 3.70 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | FREEWAY 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 100.00 | 50.00 | 3.70 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |

 ** FREeway TRAVEL TIME (MI NUTES) **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | |
|-----------|-------|-----------------------|-------|-------|-------|-------|-------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 |
| + | * 1 * | 0.09 | 44.55 | 46.76 | 49.09 | 51.82 | 60.01 |
| + | * 2 * | 0.00 | 0.00 | 1.45 | 3.78 | 6.51 | 14.70 |
| + | * 3 * | 0.00 | 0.00 | 0.00 | 1.63 | 4.36 | 12.54 |
| + | * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 1.83 | 10.02 |
| + | * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.79 |
| + | * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.64 |

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | |
|-----------|---------|------------|----------------|--------------------|-------------|-------------|-------------|-----------|-----------------|----------------|-----------|---------|--------|-------------|------|------|------|
| * SEC | * LNS | * LENGTH | * ORG DES SSEC | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP/L | * LEVEL | * MPG | * GS/VM | | | |
| * 1 | 5 | 500. | 8241. 1566. | 8241. 1566. | 8241. 1566. | 8241. 1566. | 8241. 1566. | 12500. | 0. | 0. | 0. | .66 | 65. | 25.4 | C | 19.2 | 14.0 |
| * 2 | 3 | 99999. | 0. 0. | 0. 6675. | 0. 0. | 0. 5774. | 8660. | 0. | * 24232. | 901. | .67 | 36. | 53.4 | F | 18.4 | 15.0 | |
| * 3 | 3 | 2830. | 0. 0. | 0. 6675. | 0. 0. | 0. 5774. | 7000. | 0. | ** 2830. | 901. | .82 | 18. | 104.8 | F | 17.7 | 17.0 | |
| * 4 | 3 | 930. | 0. 0. | 0. 6675. | 0. 0. | 0. 5774. | 7000. | 0. | ** 930. | 901. | .82 | 18. | 104.8 | F | 17.7 | 17.0 | |
| * 5 | 3 | 1490. | 0. 0. | 0. 6675. | 0. 0. | 0. 5774. | 7000. | 0. | ** 1490. | 901. | .82 | 18. | 104.8 | F | 17.7 | 17.0 | |
| * 6 | 3 | 3020. | 0. 0. | 0. 6675. | 0. 0. | 0. 5774. | 7000. | 0. | ** 3020. | 901. | .82 | 18. | 104.8 | F | 17.7 | 17.0 | |
| * 7 | 3 | 1030. | 0. 0. | 0. 6675. | 0. 0. | 0. 5774. | 7000. | 0. | ** 1030. | 901. | .82 | 18. | 104.8 | F | 17.7 | 17.0 | |
| * 8 | 3 | 1440. | 0. 0. | 0. 6675. | 0. 0. | 0. 5774. | 7000. | 0. | ** 1440. | 901. | .82 | 18. | 104.8 | F | 17.7 | 17.0 | |
| * 9 | 3 | 1430. | 0. 0. | 0. 6675. | 0. 0. | 0. 5774. | 7000. | 0. | ** 1430. | 901. | .82 | 18. | 104.8 | F | 17.7 | 17.0 | |
| * 10 | 3 | 3480. | 0. 0. | 0. 6675. | 0. 0. | 0. 5774. | 7000. | 0. | ** 3480. | 901. | .82 | 18. | 104.8 | F | 17.7 | 17.0 | |
| * 11 | 3 | 1020. | 0. 0. | 0. 6675. | 0. 0. | 0. 5774. | 7000. | 0. | ** 1020. | 901. | .82 | 18. | 104.8 | F | 17.7 | 17.0 | |
| * 12 | 3 | 980. | 0. 0. | 0. 6675. | 0. 0. | 0. 5774. | 7000. | 0. | ** 980. | 901. | .82 | 18. | 104.8 | F | 17.7 | 17.0 | |
| * 13 | 3 | 1800. | 0. 0. | 0. 6675. | 0. 0. | 0. 5774. | 7000. | 0. | ** 1800. | 901. | .82 | 18. | 104.8 | F | 17.7 | 17.0 | |
| * 14 | 3 | 1500. | 0. 729. | 6675. 0. | 729. 6675. | 0. 5774. | 6829. | 0. | ** 1500. | 901. | .85 | 20. | 97.9 | F | 18.3 | 16.3 | |
| * 15 | 3 | 1300. | 0. 0. | 0. 5946. | 0. 0. | 0. 5045. | 6000. | 0. | ** 1300. | 901. | .84 | 19. | 86.9 | F | 18.2 | 16.4 | |
| * 16 | 3 | 1000. | 814. 0. | 0. 6760. | 814. 0. | 0. 5859. | 5904. | 0. | ** 1000. | 45. | .99 | 34. | 57.6 | F | 22.4 | 12.0 | |
| * 17 | 3 | 1100. | 0. 0. | 0. 6760. | 0. 0. | 0. 5859. | 7546. | 0. | ** 1100. | 45. | .98 | 32. | 61.5 | F | 21.9 | 12.4 | |
| * 18 | 4 | 1000. | 0. 1546. | 6760. 0. | 1345. 5859. | 0. 4514. | 6000. | 0. | ** 1000. | 45. | .78 | 16. | 93.3 | F | 16.6 | 18.4 | |
| * 19 | 3 | 900. | 0. 0. | 0. 5214. | 0. 0. | 0. 4514. | 6000. | 0. | ** 900. | 45. | .75 | 15. | 103.4 | F | 15.9 | 19.2 | |
| * 20 | 3 | 100. | 314. 0. | 0. 5528. | 240. 0. | 0. 4754. | 5950. | 0. | ** 100. | 45. | .80 | 17. | 93.9 | F | 17.1 | 17.8 | |
| * 21 | 3 | 100. | 0. 0. | 0. 5528. | 0. 0. | 0. 4754. | 6000. | 0. | ** 100. | 45. | .79 | 17. | 95.9 | F | 16.9 | 18.0 | |
| * 22 | 3 | 100. | 0. 0. | 0. 5528. | 0. 0. | 0. 4754. | 6000. | 0. | ** 100. | 45. | .79 | 17. | 95.9 | F | 16.9 | 18.0 | |
| * 23 | 3 | 700. | 0. 0. | 0. 5528. | 0. 0. | 0. 4754. | 6000. | 0. | ** 700. | 45. | .79 | 17. | 95.9 | F | 16.9 | 18.0 | |
| * 24 | 3 | 1500. | 0. 1095. | 5528. 0. | 949. 4754. | 0. 5791. | 5791. | 0. | ** 1500. | 45. | .82 | 18. | 87.4 | F | 17.6 | 17.1 | |
| * 25 | 3 | 800. | 0. 0. | 0. 4433. | 0. 0. | 0. 3805. | 6000. | 0. | ** 800. | 45. | .63 | 10. | 125.5 | F | 13.2 | 22.7 | |
| * 26 | 3 | 1000. | 960. 0. | 0. 5393. | 960. 0. | 0. 4765. | 5805. | 0. | ** 1000. | 45. | .82 | 18. | 87.6 | F | 17.6 | 17.1 | |
| * 27 | 3 | 800. | 0. 0. | 0. 5393. | 0. 0. | 0. 4765. | 6000. | 0. | ** 800. | 45. | .79 | 17. | 95.6 | F | 16.9 | 17.9 | |
| * 28 | 3 | 1000. | 0. 647. | 5393. 0. | 578. 4765. | 0. 5902. | 5902. | 0. | ** 1000. | 45. | .81 | 17. | 91.6 | F | 17.3 | 17.5 | |
| * 29 | 3 | 8000. | 0. 0. | 0. 4746. | 0. 0. | 0. 4187. | 6000. | 0. | ** 8000. | 45. | .70 | 12. | 113.6 | F | 14.4 | 21.0 | |
| * 30 | 5 | 100. | 1113. 0. | 0. 5859. | 1113. 0. | 0. 5300. | 10000. | 0. | ** 100. | 45. | .53 | 7. | 144.9 | F | 10.1 | 26.0 | |
| * 31 | 5 | 1000. | 700. 0. | 0. 6559. | 700. 0. | 0. 6000. | 6000. | 0. | 0. | 0. | 1.00 | 65. | 18.5 | E | 19.2 | 14.0 | |
| * 32 | 5 | 2640. | 0. 6559. | 6559. 0. | 6000. 6000. | 0. 6000. | 6000. | 0. | 0. | 0. | 1.00 | 65. | 18.5 | E | 20.0 | 13.7 | |
| * TOTAL | 144589. | = | 27.4 | MI LES | | | | | MAX(V/C) = 1.00 | LOWEST LOS = F | AVG = 29. | 66.0 | 18.1 | 15.5 | | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 5861. VEH-HRS | 5882. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 237. VEH-HRS | 256. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 6098. VEH-HRS | 6138. PASS-HRS |
| TOTAL TRAV DISTANCE = | 168343. VEH-MI. | 169384. PASS-MI. |
| | | 10767. VEH-HRS |
| | | 10811. PASS-HRS |
| | | 0. VEH-HRS |
| | | 0. PASS-HRS |
| | | 337. VEH-HRS |
| | | 366. PASS-HRS |
| | | 0. VEH-HRS |
| | | 0. PASS-HRS |
| | | 11104. VEH-HRS |
| | | 11176. PASS-HRS |
| | | 360873. VEH-MI. |
| | | 362976. PASS-MI. |

AVERAGE SYSTEM SPEED = 28. MPH.
 AVERAGE DENSITY = 66. VPMP/L
 TOTAL FUEL = 9379. GALLONS
 TOTAL EMISSIONS = 2650. KI LOGRAMS

US-101_NB_AM_P2_2040_PE
 34. MPH.
 52. VPMP/L
 18779. GALLONS
 5177. KI LOGRAMS

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|--------|------------|-------|------------|--------|------------|--------|------------|--------|
| 1 | 0.01 | 2 | ***** | 3 | 120.96 | 4 | 39.75 | 5 | 63.69 |
| 6 | 129.08 | 7 | 44.03 | 8 | 61.55 | 9 | 61.12 | 10 | 148.75 |
| 11 | 43.60 | 12 | 41.89 | 13 | 76.94 | 14 | 58.19 | 15 | 45.06 |
| 16 | 15.68 | 17 | 19.69 | 18 | 53.60 | 19 | 41.04 | 20 | 3.95 |
| 21 | 4.07 | 22 | 4.07 | 23 | 28.46 | 24 | 53.74 | 25 | 48.15 |
| 26 | 35.92 | 27 | 32.34 | 28 | 38.16 | 29 | 418.63 | 30 | 12.18 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 3270.7 VEH-HRS ***** AVERAGE DELAY = 36.53 MIN/VEH *****

***** RAMP DELAYS *****

| | | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-----------|---------|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|
| ON-RAMP 2 | RAMP | 100. | 100.00 | 6.56 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 100.00 | 6.56 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP 3 | RAMP | 74. | 37.00 | 7.07 | 13.21 | 0.82 | 4.29 | 0.23 | 5.33 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 74. | 37.00 | 7.07 | 13.21 | 0.82 | 4.29 | 0.23 | 5.33 |
| ON-RAMP 6 | RAMP | 100. | 100.00 | 9.00 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 100.00 | 9.00 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |


```

**
** 19 2 3000. 900. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Mathilda / Mathilda **
** 20 2 3000. 100. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Mathilda NB On-Ramp **
**
*****

```

FREEWAY AND ARTERIAL DESIGN FEATURES

```

**
** SUB NO. SSEC SSEC DESIG N ORG TRK SSEC PCT PCT DES SPECIAL FF. SPD. CAP. ART GRADE SUBSECTI ON LOCATI ON **
** SEC LNS CAP LENGTH SPEED DES FAC GRAD TRK TRUCKS RAMP ALT. RTE ALT. RTE TYPE ALT. RTE **
**
** 21 2 3000. 100. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Mathilda / Mathilda **
** 22 2 3000. 100. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Mathilda SB Off-ramp **
** 23 2 3000. 700. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Mathilda / SR-237 **
** 24 2 3000. 1500. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 SR-237 WB Off-Ramp **
** 25 2 3000. 800. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 SR-237 / SR-237 **
** 26 2 3000. 1000. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 SR-237 WB On-Ramp **
** 27 2 3000. 800. 65 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 SR-237 / Ellis **
** 28 2 3000. 1000. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Ellis Off-ramp **
** 29 2 3000. 8000. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 HOV Dummy **
** 30 **
** 31 **
** 32 **
**
*****

```

FREEWAY TRAVEL TIME (MINUTES)

```

* O R I G I N S D E S T I N A T I O N S A C R O S S *
* D O W N 1 2 3 4 5 6 7 *
+
* * * * *
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 2 * 0.00 21.14 21.91 22.51 23.14 24.54 0.00 *
+
* 3 * 0.00 0.00 0.00 0.00 0.00 3.16 0.00 *
+
* 4 * 0.00 0.00 0.00 0.00 0.00 2.47 0.00 *
+
* 5 * 0.00 0.00 0.00 0.00 0.00 1.89 0.00 *
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
* * * * *

```

US-101_NB_AM_P2_2040_PL

| * SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMI SS | * SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP EFF LENGTH RATE RATIO MPH VPMPL LEVEL MPG GS/VM |
|---|--|
| * 1 | |
| * 2 2 99999. 1849. 0. 1849. 1849. 0. 1849. 3000. 0. 0. 0. .62 65. 14.2 B 20.0 13.7 | |
| * 3 2 2830. 0. 0. 1849. 0. 0. 1849. 3000. 0. 0. 0. .62 65. 14.2 B 20.0 13.7 | |
| * 4 2 930. 0. 0. 1849. 0. 0. 1849. 3000. 0. 0. 0. .62 65. 14.2 B 20.0 13.7 | |
| * 5 2 1490. 0. 0. 1849. 0. 0. 1849. 3000. 0. 0. 0. .62 65. 14.2 B 20.0 13.7 | |
| * 6 2 3020. 0. 0. 1849. 0. 0. 1849. 3000. 0. 0. 0. .62 65. 14.2 B 20.0 13.7 | |
| * 7 2 1030. 0. 0. 1849. 0. 0. 1849. 3000. 0. 0. 0. .62 65. 14.2 B 20.0 13.7 | |
| * 8 2 1440. 0. 0. 1849. 0. 0. 1849. 3000. 0. 0. 0. .62 65. 14.2 B 20.0 13.7 | |
| * 9 2 1430. 0. 0. 1849. 0. 0. 1849. 3000. 0. 0. 0. .62 65. 14.2 B 20.0 13.7 | |
| * 10 2 3480. 0. 0. 1849. 0. 0. 1849. 3000. 0. 0. 0. .62 65. 14.2 B 20.0 13.7 | |
| * 11 2 1020. 0. 0. 1849. 0. 0. 1849. 3000. 0. 0. 0. .62 65. 14.2 B 20.0 13.7 | |
| * 12 2 980. 0. 0. 1849. 0. 0. 1849. 3000. 0. 0. 0. .62 65. 14.2 B 20.0 13.7 | |
| * 13 2 1800. 0. 0. 1849. 0. 0. 1849. 3000. 0. 0. 0. .62 65. 14.2 B 20.0 13.7 | |
| * 14 2 1500. 0. 188. 1849. 0. 188. 1849. 3000. 0. 0. 0. .62 65. 14.2 B 20.0 13.7 | |
| * 15 2 1300. 0. 0. 1661. 0. 0. 1661. 3000. 0. 0. 0. .55 65. 12.8 B 20.0 13.7 | |
| * 16 2 1000. 126. 0. 1787. 126. 0. 1787. 3000. 0. 0. 0. .60 65. 13.7 B 20.0 13.7 | |
| * 17 2 1100. 0. 0. 1787. 0. 0. 1787. 3000. 0. 0. 0. .60 65. 13.7 B 20.0 13.7 | |
| * 18 2 1000. 0. 232. 1787. 0. 232. 1787. 3000. 0. 0. 0. .60 65. 13.7 B 20.0 13.7 | |
| * 19 2 900. 0. 0. 1555. 0. 0. 1555. 3000. 0. 0. 0. .52 65. 12.0 B 20.0 13.7 | |
| * 20 2 100. 40. 0. 1594. 40. 0. 1594. 3000. 0. 0. 0. .53 65. 12.3 B 20.0 13.7 | |
| * 21 2 100. 0. 0. 1594. 0. 0. 1594. 3000. 0. 0. 0. .53 65. 12.3 B 20.0 13.7 | |
| * 22 2 100. 0. 0. 1594. 0. 0. 1594. 3000. 0. 0. 0. .53 65. 12.3 B 20.0 13.7 | |
| * 23 2 700. 0. 0. 1594. 0. 0. 1594. 3000. 0. 0. 0. .53 65. 12.3 B 20.0 13.7 | |
| * 24 2 1500. 0. 213. 1594. 0. 213. 1594. 3000. 0. 0. 0. .53 65. 12.3 B 20.0 13.7 | |
| * 25 2 800. 0. 0. 1381. 0. 0. 1381. 3000. 0. 0. 0. .46 65. 10.6 A 20.0 13.7 | |
| * 26 2 1000. 249. 0. 1630. 249. 0. 1630. 3000. 0. 0. 0. .54 65. 12.5 B 20.0 13.7 | |
| * 27 2 800. 0. 0. 1630. 0. 0. 1630. 3000. 0. 0. 0. .54 65. 12.5 B 20.0 13.7 | |
| * 28 2 1000. 0. 104. 1630. 0. 104. 1630. 3000. 0. 0. 0. .54 65. 12.5 B 20.0 13.7 | |
| * 29 2 8000. 0. 1526. 1526. 0. 1526. 1526. 3000. 0. 0. 0. .51 65. 11.7 B 20.0 13.7 | |
| * 30 | |
| * 31 | |
| * 32 | |
| * TOTAL 140349. = 26.6 MILES MAX(V/C) = 0.62 LOWEST LOS = B AVG = 65. 14.0 20.0 13.7 | |

| CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|-----------------------------|--------------------------------|--------------------------------|--|
| FREWAY TRAVEL TIME = | 742. VEH-HRS 1484. PASS-HRS | 742. VEH-HRS 1484. PASS-HRS | |
| FREWAY MERGE DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS | |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS | |
| OFF-RAMP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS | |
| TOTAL SYSTEM TRAVEL TIME = | 742. VEH-HRS 1484. PASS-HRS | 742. VEH-HRS 1484. PASS-HRS | |
| TOTAL FRWAY TRAV DISTANCE = | 48216. VEH-MI. 96432. PASS-MI. | 48216. VEH-MI. 96432. PASS-MI. | |
| AVERAGE SYSTEM SPEED = | 65. MPH. | 65. MPH. | |
| AVERAGE DENSITY = | 14. VPMP. | 14. VPMP. | |
| TOTAL FUEL = | 2411. GALLONS | 2411. GALLONS | |
| TOTAL EMISSIONS = | 662. KILOGRAMS | 662. KILOGRAMS | |

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | 30 | 0.00 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** MAINTENANCE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****
 ***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

 ** FREWAY TRAVEL TIME (MINUTES) **

| ORIGINS | DESTINATIONS ACROSS | | | | | | |
|---------|---------------------|-------|-------|-------|-------|-------|------|
| DOWN | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 21.14 | 21.91 | 22.51 | 23.14 | 24.54 | 0.00 |

```

+
+
+
+
+
+
+
* 3 * 0.00 0.00 0.00 0.00 0.00 3.16 0.00
* 4 * 0.00 0.00 0.00 0.00 0.00 2.47 0.00
* 5 * 0.00 0.00 0.00 0.00 0.00 1.89 0.00
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
*
*
*****
    
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TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB SEC | NO. LNS | SSEC LENGTH | O-D DATA ORG | DEMANDS DES | SSEC | ADJUSTED VOLUMES ORG | DES | SSEC | SSEC CAP. | WEAVE EFF | CONGEST LENGTH | STORAGE RATE | V/C RATIO | SPEED MPH | DENSITY VPMP | LOS LEVEL | FUEL MPG | EMI SS GS/VM |
|---------|---------|-------------|--------------|-------------|------|----------------------|------|------|-----------|-----------|----------------|--------------|-----------------|----------------|--------------|-----------|----------|--------------|
| * 1 | | | | | | | | | | | | | | | | | | |
| * 2 | 2 | 99999 | 1566 | 0 | 1566 | 1566 | 0 | 1566 | 3000 | 0 | 0 | 0 | .52 | 65 | 12.0 | B | 20.0 | 13.7 |
| * 3 | 2 | 2830 | 0 | 0 | 1566 | 0 | 0 | 1566 | 3000 | 0 | 0 | 0 | .52 | 65 | 12.0 | B | 20.0 | 13.7 |
| * 4 | 2 | 930 | 0 | 0 | 1566 | 0 | 0 | 1566 | 3000 | 0 | 0 | 0 | .52 | 65 | 12.0 | B | 20.0 | 13.7 |
| * 5 | 2 | 1490 | 0 | 0 | 1566 | 0 | 0 | 1566 | 3000 | 0 | 0 | 0 | .52 | 65 | 12.0 | B | 20.0 | 13.7 |
| * 6 | 2 | 3020 | 0 | 0 | 1566 | 0 | 0 | 1566 | 3000 | 0 | 0 | 0 | .52 | 65 | 12.0 | B | 20.0 | 13.7 |
| * 7 | 2 | 1030 | 0 | 0 | 1566 | 0 | 0 | 1566 | 3000 | 0 | 0 | 0 | .52 | 65 | 12.0 | B | 20.0 | 13.7 |
| * 8 | 2 | 1440 | 0 | 0 | 1566 | 0 | 0 | 1566 | 3000 | 0 | 0 | 0 | .52 | 65 | 12.0 | B | 20.0 | 13.7 |
| * 9 | 2 | 1430 | 0 | 0 | 1566 | 0 | 0 | 1566 | 3000 | 0 | 0 | 0 | .52 | 65 | 12.0 | B | 20.0 | 13.7 |
| * 10 | 2 | 3480 | 0 | 0 | 1566 | 0 | 0 | 1566 | 3000 | 0 | 0 | 0 | .52 | 65 | 12.0 | B | 20.0 | 13.7 |
| * 11 | 2 | 1020 | 0 | 0 | 1566 | 0 | 0 | 1566 | 3000 | 0 | 0 | 0 | .52 | 65 | 12.0 | B | 20.0 | 13.7 |
| * 12 | 2 | 980 | 0 | 0 | 1566 | 0 | 0 | 1566 | 3000 | 0 | 0 | 0 | .52 | 65 | 12.0 | B | 20.0 | 13.7 |
| * 13 | 2 | 1800 | 0 | 0 | 1566 | 0 | 0 | 1566 | 3000 | 0 | 0 | 0 | .52 | 65 | 12.0 | B | 20.0 | 13.7 |
| * 14 | 2 | 1500 | 0 | 171 | 1566 | 0 | 171 | 1566 | 3000 | 0 | 0 | 0 | .52 | 65 | 12.0 | B | 20.0 | 13.7 |
| * 15 | 2 | 1300 | 0 | 0 | 1395 | 0 | 0 | 1395 | 3000 | 0 | 0 | 0 | .46 | 65 | 10.7 | A | 20.0 | 13.7 |
| * 16 | 2 | 1000 | 96 | 0 | 1491 | 96 | 0 | 1491 | 3000 | 0 | 0 | 0 | .50 | 65 | 11.5 | B | 20.0 | 13.7 |
| * 17 | 2 | 1100 | 0 | 0 | 1491 | 0 | 0 | 1491 | 3000 | 0 | 0 | 0 | .50 | 65 | 11.5 | B | 20.0 | 13.7 |
| * 18 | 2 | 1000 | 0 | 314 | 1491 | 0 | 314 | 1491 | 3000 | 0 | 0 | 0 | .50 | 65 | 11.5 | B | 20.0 | 13.7 |
| * 19 | 2 | 900 | 0 | 0 | 1176 | 0 | 0 | 1176 | 3000 | 0 | 0 | 0 | .39 | 65 | 9.0 | A | 20.0 | 13.7 |
| * 20 | 2 | 100 | 50 | 0 | 1226 | 50 | 0 | 1226 | 3000 | 0 | 0 | 0 | .41 | 65 | 9.4 | A | 20.0 | 13.7 |
| * 21 | 2 | 100 | 0 | 0 | 1226 | 0 | 0 | 1226 | 3000 | 0 | 0 | 0 | .41 | 65 | 9.4 | A | 20.0 | 13.7 |
| * 22 | 2 | 100 | 0 | 0 | 1226 | 0 | 0 | 1226 | 3000 | 0 | 0 | 0 | .41 | 65 | 9.4 | A | 20.0 | 13.7 |
| * 23 | 2 | 700 | 0 | 0 | 1226 | 0 | 0 | 1226 | 3000 | 0 | 0 | 0 | .41 | 65 | 9.4 | A | 20.0 | 13.7 |
| * 24 | 2 | 1500 | 0 | 209 | 1226 | 0 | 209 | 1226 | 3000 | 0 | 0 | 0 | .41 | 65 | 9.4 | A | 20.0 | 13.7 |
| * 25 | 2 | 800 | 0 | 0 | 1017 | 0 | 0 | 1017 | 3000 | 0 | 0 | 0 | .34 | 65 | 7.8 | A | 20.0 | 13.7 |
| * 26 | 2 | 1000 | 195 | 0 | 1212 | 195 | 0 | 1212 | 3000 | 0 | 0 | 0 | .40 | 65 | 9.3 | A | 20.0 | 13.7 |
| * 27 | 2 | 800 | 0 | 0 | 1212 | 0 | 0 | 1212 | 3000 | 0 | 0 | 0 | .40 | 65 | 9.3 | A | 20.0 | 13.7 |
| * 28 | 2 | 1000 | 0 | 98 | 1212 | 0 | 98 | 1212 | 3000 | 0 | 0 | 0 | .40 | 65 | 9.3 | A | 20.0 | 13.7 |
| * 29 | 2 | 8000 | 0 | 1113 | 1113 | 0 | 1113 | 1113 | 3000 | 0 | 0 | 0 | .37 | 65 | 8.6 | A | 20.0 | 13.7 |
| * 30 | | | | | | | | | | | | | | | | | | |
| * 31 | | | | | | | | | | | | | | | | | | |
| * 32 | | | | | | | | | | | | | | | | | | |
| * TOTAL | 140349 | = | 26.6 | MILES | | | | | | | | | MAX(V/C) = 0.52 | LOWEST LOS = B | AVG = 65 | 11.7 | 20.0 | 13.7 |

| | | |
|-----------------------------|---------------------------------|----------------------------------|
| | CURRENT TIME SLICE | CUMULATIVE VALUES |
| FREEWAY TRAVEL TIME = | 621. VEH-HRS 1241. PASS-HRS | 1362. VEH-HRS 2725. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 621. VEH-HRS 1241. PASS-HRS | 1362. VEH-HRS 2725. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 40346. VEH-MI 80692. PASS-MI | 88562. VEH-MI 177125. PASS-MI |
| AVERAGE SYSTEM SPEED = | 65. MPH | 65. MPH |
| AVERAGE DENSITY = | 12. VPMP | 13. VPMP |
| TOTAL FUEL = | 2017. GALLONS | 4428. GALLONS |
| TOTAL EMISSIONS = | 554. KILOGRAMS | 1217. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | 30 | 0.00 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****


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FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQQ QQQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP EEEEEEEEE
    
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FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREWAY AND ARTERIAL DESIGN FEATURES

| ** SUB NO. | ** SSEC | ** SSEC | ** DESIG N | ** ORG | ** TRK | ** SSEC | ** PCT | ** PCT | ** DES | ** SPECIAL | ** FF. SPD. | ** CAP. | ** ART | ** GRADE | ** SUBSECTI ON | ** LOCATI ON |
|------------|---------|---------|------------|----------|--------|---------|--------|-----------|---------|-------------|-------------|---------|-------------|-------------|--------------------------|--------------|
| ** SEC | ** LNS | ** CAP | ** LENGTH | ** SPEED | ** DES | ** GRAD | ** TRK | ** TRUCKS | ** RAMP | ** ALT. RTE | ** ALT. RTE | ** TYPE | ** ALT. RTE | ** ALT. RTE | ** LOCATION | ** LOCATION |
| ** 1 | 4 | 10000. | 500. | 65 | OD | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Seeding | ** |
| ** 2 | 3 | 7000. | 99999. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | ** |
| ** 3 | 3 | 7000. | 2830. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-87 to DLC loop-on | ** |
| ** 4 | 3 | 7000. | 930. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | DLC loop-on to dia-on | ** |
| ** 5 | 3 | 7000. | 1490. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | DLC dia-on to Tomas off | ** |
| ** 6 | 3 | 7000. | 3020. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas off to on | ** |
| ** 7 | 3 | 7000. | 1030. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas on to bowers off | ** |
| ** 8 | 3 | 7000. | 1440. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers off to loop-on | ** |
| ** 9 | 3 | 7000. | 1430. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers loop-on to dia | ** |
| ** 10 | 3 | 7000. | 3480. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers dia-on to law-off | ** |
| ** 11 | 3 | 7000. | 1020. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Law off to loop-on | ** |
| ** 12 | 3 | 7000. | 980. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawr Loop to diag | ** |
| ** 13 | 3 | 7000. | 1800. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Lawrence On-ramp | ** |
| ** 14 | 3 | 7000. | 1500. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks Off-Ramp | ** |
| ** 15 | 3 | 6000. | 1300. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Fair Oaks | ** |
| ** 16 | 3 | 6000. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Fair Oaks On-Ramp | ** |
| ** 17 | 3 | 6000. | 1100. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Mathilda | ** |
| ** 18 | 3 | 6000. | 1000. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda NB Off-Ramp | ** |
| ** 19 | 3 | 6000. | 900. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | ** |
| ** 20 | 3 | 6000. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda NB On-Ramp | ** |

FREEWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT TRUCKS | DES SPECIAL RAMP | FF SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION LOCATION |
|---------|----------|----------|-------------|--------------|---------|---------|-----------|---------|------------|------------------|------------------|---------------|----------|----------------|----------------------|
| ** 21 | 3 | 6000. | 100. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda |
| ** 22 | 3 | 6000. | 100. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda SB Off-ramp |
| ** 23 | 3 | 6000. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / SR-237 |
| ** 24 | 3 | 6000. | 1500. | 65 | D | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 WB Off-Ramp |
| ** 25 | 3 | 6000. | 800. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 / SR-237 |
| ** 26 | 3 | 6000. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 WB On-Ramp |
| ** 27 | 3 | 6000. | 800. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 / Ellis |
| ** 28 | 3 | 6000. | 1000. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Ellis Off-ramp |
| ** 29 | 3 | 6000. | 8000. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** 30 | 4 | 8000. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** 31 | 4 | 5500. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Dummy Bottleneck |
| ** 32 | 4 | 8000. | 2640. | 65 | D | 1.00 | 0.0 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End of Network |

***** INPUT HAS BEEN COMPLETED *****

- MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 4 IN TIME SLICE 1
--- THE MAXIMUM METERING RATE WILL PREVAIL.
- MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 4 IN TIME SLICE 2
--- THE MAXIMUM METERING RATE WILL PREVAIL.
- MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 6 IN TIME SLICE 2
--- THE MAXIMUM METERING RATE WILL PREVAIL.
- MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 4 IN TIME SLICE 3
--- THE MAXIMUM METERING RATE WILL PREVAIL.
- MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 6 IN TIME SLICE 3
--- THE MAXIMUM METERING RATE WILL PREVAIL.

FREEWAY TRAVEL TIME (MINUTES)

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | |
|--------------|---------------------|-------|-------|-------|-------|-------|-------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 0.09 | 22.00 | 22.85 | 23.07 | 23.47 | 24.34 | 32.05 |
| * 2 * | 0.00 | 0.00 | 0.61 | 0.84 | 1.23 | 2.10 | 9.81 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.06 | 0.45 | 1.33 | 9.03 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.74 | 8.44 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.81 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.64 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB SEC | NO. LNS | SSEC LENGTH | O-D ORG | DATA DES | DEMANDS SSEC | ADJUSTED ORG | VOLUMES DES | SSEC SSEC | SSEC CAP. | WEAVE EFF | CONGEST LENGTH | STORAGE RATE | V/C RATIO | SPEED MPH | DENSITY VPMP/L | LOS LEVEL | FUEL MPG | EMI SS GS/VM |
|---------|---------|-------------|---------|----------|--------------|--------------|-------------|-----------|-----------|-----------|----------------|--------------|-----------|-----------|----------------|-----------|----------|--------------|
| 1 | 4 | 500. | 6550. | 852. | 6550. | 6550. | 852. | 6550. | 10000. | 0. | 0. | 0. | .65 | 65. | 25.2 | C | 19.2 | 14.0 |
| 2 | 3 | 99999. | 0. | 0. | 5698. | 0. | 0. | 5698. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 3 | 3 | 2830. | 0. | 0. | 5698. | 0. | 0. | 5698. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 4 | 3 | 930. | 0. | 0. | 5698. | 0. | 0. | 5698. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 5 | 3 | 1490. | 0. | 0. | 5698. | 0. | 0. | 5698. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 6 | 3 | 3020. | 0. | 0. | 5698. | 0. | 0. | 5698. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 7 | 3 | 1030. | 0. | 0. | 5698. | 0. | 0. | 5698. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 8 | 3 | 1440. | 0. | 0. | 5698. | 0. | 0. | 5698. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 9 | 3 | 1430. | 0. | 0. | 5698. | 0. | 0. | 5698. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 10 | 3 | 3480. | 0. | 0. | 5698. | 0. | 0. | 5698. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 11 | 3 | 1020. | 0. | 0. | 5698. | 0. | 0. | 5698. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 12 | 3 | 980. | 0. | 0. | 5698. | 0. | 0. | 5698. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 13 | 3 | 1800. | 0. | 0. | 5698. | 0. | 0. | 5698. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 14 | 3 | 1500. | 0. | 557. | 5698. | 0. | 557. | 5698. | 6917. | 0. | 0. | 0. | .82 | 62. | 30.4 | D | 20.4 | 13.1 |
| 15 | 3 | 1300. | 0. | 0. | 5141. | 0. | 0. | 5141. | 6000. | 0. | 0. | 0. | .86 | 61. | 28.0 | D | 21.0 | 12.7 |
| 16 | 3 | 1000. | 467. | 0. | 5608. | 367. | 0. | 5508. | 5957. | 0. | 0. | 0. | .92 | 58. | 31.8 | D | 22.3 | 11.9 |
| 17 | 3 | 1100. | 0. | 0. | 5608. | 0. | 0. | 5508. | 6000. | 0. | 0. | 0. | .92 | 58. | 31.6 | D | 22.2 | 12.0 |
| 18 | 3 | 1000. | 0. | 273. | 5608. | 0. | 268. | 5508. | 5963. | 0. | 0. | 0. | .92 | 58. | 31.7 | D | 22.3 | 11.9 |
| 19 | 3 | 900. | 0. | 0. | 5335. | 0. | 0. | 5240. | 6000. | 0. | 0. | 0. | .87 | 60. | 28.9 | D | 21.4 | 12.5 |
| 20 | 3 | 100. | 173. | 0. | 5508. | 173. | 0. | 5413. | 5983. | 0. | 0. | 0. | .90 | 59. | 30.6 | D | 21.9 | 12.1 |
| 21 | 3 | 100. | 0. | 0. | 5508. | 0. | 0. | 5413. | 6000. | 0. | 0. | 0. | .90 | 59. | 30.6 | D | 21.9 | 12.1 |
| 22 | 3 | 100. | 0. | 837. | 5508. | 0. | 821. | 5413. | 5890. | 0. | 0. | 0. | .92 | 58. | 31.1 | D | 22.2 | 12.0 |
| 23 | 3 | 700. | 0. | 0. | 4671. | 0. | 0. | 4592. | 6000. | 0. | 0. | 0. | .77 | 64. | 23.9 | C | 19.7 | 13.6 |
| 24 | 3 | 1500. | 0. | 784. | 4671. | 0. | 769. | 4592. | 5897. | 0. | 0. | 0. | .78 | 64. | 24.1 | C | 19.8 | 13.5 |
| 25 | 3 | 800. | 0. | 0. | 3887. | 0. | 0. | 3823. | 6000. | 0. | 0. | 0. | .64 | 65. | 19.6 | C | 19.2 | 14.0 |
| 26 | 3 | 1000. | 1731. | 0. | 5618. | 1255. | 0. | 4254. | 5755. | 0. | 578. | 824. | .74 | 57. | 24.9 | F | 21.4 | 12.5 |
| 27 | 3 | 800. | 0. | 0. | 5618. | 0. | 0. | 4254. | 6000. | 0. | 800. | 824. | .71 | 44. | 32.1 | F | 19.8 | 13.6 |
| 28 | 3 | 1000. | 0. | 281. | 5618. | 0. | 252. | 4254. | 5975. | 0. | 1000. | 824. | .71 | 34. | 41.2 | F | 18.9 | 14.3 |
| 29 | 3 | 8000. | 0. | 0. | 5337. | 0. | 0. | 4002. | 6000. | 0. | 8000. | 824. | .67 | 13. | 101.2 | F | 13.6 | 19.8 |
| 30 | 4 | 100. | 798. | 0. | 6135. | 798. | 0. | 4800. | 8000. | 0. | 100. | 824. | .60 | 7. | 183.1 | F | 9.5 | 26.8 |
| 31 | 4 | 1000. | 800. | 0. | 6935. | 700. | 0. | 5500. | 5500. | 0. | 0. | 0. | 1.00 | 65. | 21.2 | E | 19.2 | 14.0 |
| 32 | 4 | 2640. | 0. | 6935. | 6935. | 0. | 5500. | 5500. | 8000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 20.0 | 13.7 |

TOTAL 144589. = 27.4 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 53. 34.0 19.8 13.5

| | | |
|----------------------------|--------------------|-------------------|
| | CURRENT TIME SLICE | CUMULATIVE VALUES |
| FREEWAY TRAVEL TIME = | 2858. VEH-HRS | 2858. VEH-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| ON-RAMP MRG/CAP DELAY = | 338. VEH-HRS | 338. VEH-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. VEH-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 3196. VEH-HRS | 3196. VEH-HRS |
| TOTAL TRAVEL DISTANCE = | 152445. VEH-MI. | 152445. VEH-MI. |
| AVERAGE SYSTEM SPEED = | 48. MPH. | 53. MPH. |
| AVERAGE DENSITY = | 34. VPMP/L | 34. VPMP/L |
| TOTAL FUEL = | 7817. GALLONS | 7817. GALLONS |
| TOTAL EMISSIONS = | 2109. KI LOGRAMS | 2109. KI LOGRAMS |

***** MAINTENANCE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|--------|------------|-------|
| 1 | 0.00 | 2 | 60.03 | 3 | 1.70 | 4 | 0.56 | 5 | 0.89 |
| 6 | 1.81 | 7 | 0.62 | 8 | 0.86 | 9 | 0.86 | 10 | 2.09 |
| 11 | 0.61 | 12 | 0.59 | 13 | 1.08 | 14 | 1.03 | 15 | 1.20 |
| 16 | 2.01 | 17 | 2.07 | 18 | 1.99 | 19 | 1.02 | 20 | 0.16 |
| 21 | 0.16 | 22 | 0.19 | 23 | 0.16 | 24 | 0.43 | 25 | 0.00 |
| 26 | 2.09 | 27 | 5.53 | 28 | 12.81 | 29 | 397.47 | 30 | 12.49 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 512.5 VEH-HRS ***** AVERAGE DELAY = 7.27 MIN/VEH *****

***** RAMP DELAYS *****

| ON-RAMP | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|---------|-----------------------|---------------|--------------------------------|----------|---------|---------|----------|----------------------|
| 2 | RAMP | 100. | 50.00 | 6.42 | 17.85 | 1.11 | 5.79 | 7.21 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 50.00 | 6.42 | 17.85 | 1.11 | 5.79 | 7.21 |

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | | | |
|----------------------------|--------------------|------------------|-------------------|------------------|--|--|
| FREEWAY TRAVEL TIME = | 3817. VEH-HRS | 3831. PASS-HRS | 6675. VEH-HRS | 6700. PASS-HRS | | |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | | |
| ON-RAMP MRG/CAP DELAY = | 1144. VEH-HRS | 1189. PASS-HRS | 1482. VEH-HRS | 1533. PASS-HRS | | |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | | |
| TOTAL SYSTEM TRAVEL TIME = | 4961. VEH-HRS | 5020. PASS-HRS | 8157. VEH-HRS | 8233. PASS-HRS | | |
| TOTAL TRAV DISTANCE = | 152603. VEH-MI. | 153221. PASS-MI. | 305048. VEH-MI. | 306288. PASS-MI. | | |
| AVERAGE SYSTEM SPEED = | 31. MPH. | | 46. MPH. | | | |
| AVERAGE DENSITY = | 46. VPMP | | 40. VPMP | | | |
| TOTAL FUEL = | 8407. GALLONS | | 16224. GALLONS | | | |
| TOTAL EMISSIONS = | 2301. KI LOGRAMS | | 4410. KI LOGRAMS | | | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|--------|------------|-------|
| 1 | 0.01 | 2 | 75.76 | 3 | 2.14 | 4 | 0.70 | 5 | 1.13 |
| 6 | 2.29 | 7 | 0.78 | 8 | 1.09 | 9 | 1.08 | 10 | 2.64 |
| 11 | 0.77 | 12 | 0.74 | 13 | 1.47 | 14 | 12.63 | 15 | 23.76 |
| 16 | 21.59 | 17 | 29.40 | 18 | 30.96 | 19 | 36.18 | 20 | 4.00 |
| 21 | 4.08 | 22 | 3.92 | 23 | 41.71 | 24 | 100.48 | 25 | 86.65 |
| 26 | 76.67 | 27 | 68.02 | 28 | 84.22 | 29 | 741.12 | 30 | 13.71 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 1469.7 VEH-HRS ***** AVERAGE DELAY = 23.19 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-----------|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|
| ON-RAMP 2 | RAMP 100. | 100.00 | 9.55 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 100. | 100.00 | 9.55 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP 4 | RAMP 920. | 698.00 | 17.31 | 249.24 | 15.46 | 80.86 | 4.29 | 100.61 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 920. | 698.00 | 17.31 | 249.24 | 15.46 | 80.86 | 4.29 | 100.61 |
| ON-RAMP 6 | RAMP 592. | 346.00 | 13.91 | 123.55 | 7.66 | 40.08 | 2.13 | 49.87 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 592. | 346.00 | 13.91 | 123.55 | 7.66 | 40.08 | 2.13 | 49.87 |

**
** FREEWAY TRAVEL TIME (MINUTES)
**

| * ORIGINS * DOWN | * DESTINATIONS ACROSS | | | | | | |
|---------------------|-----------------------|-------|-------|-------|-------|-------|-------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 0.09 | 25.88 | 31.29 | 32.81 | 36.51 | 42.46 | 55.56 |
| * 2 * | 0.00 | 0.00 | 3.53 | 5.05 | 8.75 | 14.70 | 27.80 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.35 | 4.05 | 10.00 | 23.11 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.76 | 16.87 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.83 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.64 |

*
* TIME SLICE FREEWAY PERFORMANCE TABLE
*

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|-----------|----------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|--------|---------|-----------|--------|---------|-------------|
| * SEC LNS | * LENGTH | * ORG | * DES | * ORG | * DES | * SSEC | * CAP | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * GS/VM |

US-101_NB_PM_NP_2040_PE

| | | | | | | | | | | | | | | | | | | | | | |
|-------|----|---|---------|-------|-------|---------|-------|-------|-------|--------|------------|------|--------------|------|-------|------|-------|------|------|------|---|
| * | 1 | 4 | 500. | 5769. | 750. | 5769. | 5769. | 750. | 5769. | 10000. | 0. | 0. | 0. | .58 | 65. | 22.2 | C | 19.2 | 14.0 | * | |
| * | 2 | 3 | 99999. | 0. | 0. | 5019. | 0. | 0. | 5019. | 7000. | 0. | 0. | 0. | .72 | 65. | 25.9 | C | 19.3 | 13.9 | * | |
| * | 3 | 3 | 2830. | 0. | 0. | 5019. | 0. | 0. | 5019. | 7000. | 0. | 0. | 0. | .72 | 65. | 25.9 | C | 19.3 | 13.9 | * | |
| * | 4 | 3 | 930. | 0. | 0. | 5019. | 0. | 0. | 5019. | 7000. | 0. | 0. | 0. | .72 | 65. | 25.9 | C | 19.3 | 13.9 | * | |
| * | 5 | 3 | 1490. | 0. | 0. | 5019. | 0. | 0. | 5019. | 7000. | 0. | 0. | 0. | .72 | 65. | 25.9 | C | 19.3 | 13.9 | * | |
| * | 6 | 3 | 3020. | 0. | 0. | 5019. | 0. | 0. | 5019. | 7000. | 0. | 0. | 0. | .72 | 65. | 25.9 | C | 19.3 | 13.9 | * | |
| * | 7 | 3 | 1030. | 0. | 0. | 5019. | 0. | 0. | 5019. | 7000. | 0. | 0. | 0. | .72 | 65. | 25.9 | C | 19.3 | 13.9 | * | |
| * | 8 | 3 | 1440. | 0. | 0. | 5019. | 0. | 0. | 5019. | 7000. | 0. | 0. | 0. | .72 | 65. | 25.9 | C | 19.3 | 13.9 | * | |
| * | 9 | 3 | 1430. | 0. | 0. | 5019. | 0. | 0. | 5019. | 7000. | 0. | 0. | 0. | .72 | 65. | 25.9 | C | 19.3 | 13.9 | * | |
| * | 10 | 3 | 3480. | 0. | 0. | 5019. | 0. | 0. | 4630. | 7000. | 0. | * | 366. | 389. | .66 | 63. | 24.6 | F | 19.3 | 13.9 | * |
| * | 11 | 3 | 1020. | 0. | 0. | 5019. | 0. | 0. | 4630. | 7000. | 0. | ** | 1020. | 389. | .66 | 26. | 59.3 | F | 16.5 | 16.2 | * |
| * | 12 | 3 | 980. | 0. | 0. | 5019. | 0. | 0. | 4630. | 7000. | 0. | ** | 980. | 389. | .66 | 15. | 101.1 | F | 14.1 | 19.0 | * |
| * | 13 | 3 | 1800. | 0. | 0. | 5019. | 0. | 0. | 4630. | 7000. | 0. | ** | 1800. | 389. | .66 | 10. | 161.9 | F | 11.7 | 23.0 | * |
| * | 14 | 3 | 1500. | 0. | 661. | 5019. | 0. | 661. | 4630. | 6901. | 0. | ** | 1500. | 389. | .67 | 8. | 191.0 | F | 10.8 | 25.1 | * |
| * | 15 | 3 | 1300. | 0. | 0. | 4358. | 0. | 0. | 3969. | 6000. | 0. | ** | 1300. | 389. | .66 | 8. | 168.5 | F | 10.6 | 25.3 | * |
| * | 16 | 3 | 1000. | 450. | 0. | 4808. | 450. | 0. | 4419. | 5961. | 0. | ** | 1000. | 389. | .74 | 10. | 146.7 | F | 13.2 | 22.8 | * |
| * | 17 | 3 | 1100. | 0. | 0. | 4808. | 0. | 0. | 4419. | 6000. | 0. | ** | 1100. | 389. | .74 | 10. | 148.9 | F | 13.0 | 22.9 | * |
| * | 18 | 3 | 1000. | 0. | 229. | 4808. | 0. | 229. | 4419. | 5969. | 0. | ** | 1000. | 389. | .74 | 10. | 147.1 | F | 13.2 | 22.8 | * |
| * | 19 | 3 | 900. | 0. | 0. | 4579. | 0. | 0. | 4189. | 6000. | 0. | ** | 900. | 389. | .70 | 9. | 158.9 | F | 11.6 | 24.2 | * |
| * | 20 | 3 | 100. | 148. | 0. | 4727. | 148. | 0. | 4337. | 5987. | 0. | ** | 100. | 389. | .72 | 10. | 151.7 | F | 12.5 | 23.4 | * |
| * | 21 | 3 | 100. | 0. | 0. | 4727. | 0. | 0. | 4337. | 6000. | 0. | ** | 100. | 389. | .72 | 9. | 152.5 | F | 12.4 | 23.4 | * |
| * | 22 | 3 | 100. | 0. | 706. | 4727. | 0. | 707. | 4337. | 5908. | 0. | ** | 100. | 389. | .73 | 10. | 147.2 | F | 12.9 | 23.0 | * |
| * | 23 | 3 | 700. | 0. | 0. | 4021. | 0. | 0. | 3630. | 6000. | 0. | ** | 700. | 389. | .61 | 7. | 183.3 | F | 9.5 | 26.8 | * |
| * | 24 | 3 | 1500. | 0. | 872. | 4021. | 0. | 872. | 3630. | 5887. | 0. | ** | 1500. | 389. | .62 | 7. | 176.8 | F | 9.7 | 26.5 | * |
| * | 25 | 3 | 800. | 0. | 0. | 3149. | 0. | 0. | 2758. | 6000. | 0. | ** | 800. | 389. | .46 | 4. | 221.2 | F | 8.4 | 28.7 | * |
| * | 26 | 3 | 1000. | 1390. | 0. | 4539. | 1303. | 0. | 4061. | 5803. | 0. | ** | 1000. | 389. | .70 | 9. | 153.3 | F | 11.6 | 24.2 | * |
| * | 27 | 3 | 800. | 0. | 0. | 4539. | 0. | 0. | 4061. | 6000. | 0. | ** | 800. | 389. | .68 | 8. | 164.5 | F | 11.0 | 24.9 | * |
| * | 28 | 3 | 1000. | 0. | 204. | 4539. | 0. | 207. | 4061. | 5982. | 0. | ** | 1000. | 389. | .68 | 8. | 163.4 | F | 11.0 | 24.8 | * |
| * | 29 | 3 | 8000. | 0. | 0. | 4335. | 0. | 0. | 3855. | 6000. | 0. | ** | 8000. | 389. | .64 | 7. | 173.5 | F | 10.2 | 25.8 | * |
| * | 30 | 4 | 100. | 648. | 0. | 4983. | 648. | 0. | 4503. | 8000. | 0. | ** | 100. | 389. | .56 | 6. | 194.3 | F | 8.9 | 27.7 | * |
| * | 31 | 4 | 1000. | 750. | 0. | 5733. | 998. | 0. | 5500. | 5500. | 0. | 0. | 0. | 1.00 | 65. | 21.2 | E | 19.2 | 14.0 | * | |
| * | 32 | 4 | 2640. | 0. | 5733. | 5733. | 0. | 5500. | 5500. | 8000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 20.0 | 13.7 | * | |
| ***** | | | | | | | | | | | | | | | | | | | | | |
| TOTAL | | | 144589. | = | 27.4 | MI L ES | | | | | | | | | | | | | | | |
| | | | | | | | | | | | MAX(V/C) = | 1.00 | LOWEST LOS = | F | AVG = | 33. | 49.2 | 17.5 | 15.4 | * | |
| ***** | | | | | | | | | | | | | | | | | | | | | |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 3 OF 3

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 4070. VEH-HRS | 4084. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 1532. VEH-HRS | 1593. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 5602. VEH-HRS | 5676. PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 133580. VEH-MI. | 134184. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 24. MPH | 41. MPH |
| AVERAGE DENSITY = | 49. VPMP | 43. VPMP |
| TOTAL FUEL = | 8184. GALLONS | 24407. GALLONS |
| TOTAL EMISSIONS = | 2273. KI LOGRAMS | 6683. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|--------|------------|--------|------------|--------|
| 1 | 0.00 | 2 | 8.80 | 3 | 0.25 | 4 | 0.08 | 5 | 0.13 |
| 6 | 0.27 | 7 | 0.09 | 8 | 0.13 | 9 | 0.13 | 10 | 1.95 |
| 11 | 21.94 | 12 | 45.03 | 13 | 143.59 | 14 | 142.54 | 15 | 109.44 |
| 16 | 70.47 | 17 | 78.91 | 18 | 70.73 | 19 | 70.27 | 20 | 7.36 |
| 21 | 7.40 | 22 | 7.10 | 23 | 65.48 | 24 | 134.84 | 25 | 94.14 |
| 26 | 75.25 | 27 | 65.29 | 28 | 81.03 | 29 | 698.72 | 30 | 13.41 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 2014.8 VEH-HRS ***** AVERAGE DELAY = 30.36 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH | DELAY | AVERAGE | GAS | HC | CO | NOX | TOTAL |
|-----------|--------------|---------|----------|-------|--------|-------|--------|-----------|
| | VEHICLES | VEH-HRS | METERING | GALS | KGMS | KGMS | KGMS | EMISSIONS |
| | | | DELAY | | | | | KGMS |
| | | | MI NUTES | | | | | |
| ON-RAMP 2 | RAMP | 100. | 100.00 | 10.91 | 35.71 | 2.22 | 11.58 | 0.61 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 100.00 | 10.91 | 35.71 | 2.22 | 11.58 | 0.61 |
| ON-RAMP 4 | RAMP | 1007. | 963.50 | 23.06 | 344.05 | 21.34 | 111.62 | 5.92 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 1007. | 963.50 | 23.06 | 344.05 | 21.34 | 111.62 | 5.92 |
| ON-RAMP 6 | RAMP | 345. | 468.25 | 22.58 | 167.20 | 10.37 | 54.25 | 2.88 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 345. | 468.25 | 22.58 | 167.20 | 10.37 | 54.25 | 2.88 |

US-101_NB_PM_NP_2040_PL

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**
** 19 2 3000. 900. 65 0.96 0.0 0 100 NO 0.0 0.0 GOOD 0.0 Mathilda / Mathilda
**
** 20 2 3000. 100. 65 0 0.96 0.0 0 100 YES 0.0 0.0 GOOD 0.0 Mathilda NB On-Ramp
**
*****

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FREEWAY AND ARTERIAL DESIGN FEATURES

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*****
**
**
**
**
**
** SUB NO. SSEC SSEC DESIG N ORG TRK SSEC PCT PCT DES SPECIAL FF.SPD. CAP. ART GRADE SUBSECTI ON LOCATI ON
** SEC LNS CAP LENGTH SPEED DES FAC GRAD TRK TRUCKS RAMP ALT. RTE ALT. RTE TYPE ALT. RTE
**
**
** 21 2 3000. 100. 65 0.96 0.0 0 100 NO 0.0 0.0 GOOD 0.0 Mathilda / Mathilda
**
** 22 2 3000. 100. 65 D 0.96 0.0 0 100 NO 0.0 0.0 GOOD 0.0 Mathilda SB Off-ramp
**
** 23 2 3000. 700. 65 0.96 0.0 0 100 NO 0.0 0.0 GOOD 0.0 Mathilda / SR-237
**
** 24 2 3000. 1500. 65 D 0.96 0.0 0 100 YES 0.0 0.0 GOOD 0.0 SR-237 WB Off-Ramp
**
** 25 2 3000. 800. 65 0.96 0.0 0 100 NO 0.0 0.0 GOOD 0.0 SR-237 / SR-237
**
** 26 2 3000. 1000. 65 0 0.96 0.0 0 100 YES 0.0 0.0 GOOD 0.0 SR-237 WB On-Ramp
**
** 27 2 3000. 800. 65 0.96 0.0 0 100 YES 0.0 0.0 GOOD 0.0 SR-237 / Ellis
**
** 28 2 3000. 1000. 65 D 0.96 0.0 0 100 NO 0.0 0.0 GOOD 0.0 Ellis Off-ramp
**
** 29 2 3000. 8000. 65 D 0.96 0.0 0 100 NO 0.0 0.0 GOOD 0.0 HOV Dummy
**
** 30
**
** 31
**
** 32
**
*****

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FREEWAY TRAVEL TIME (MINUTES)

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*****
* OR I G I N S D E S T I N A T I O N S A C R O S S
* D O W N
* 1 2 3 4 5 6 7 8
+
*
*
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 2 * 0.00 21.14 21.91 22.12 22.51 23.14 24.54 0.00
+
* 3 * 0.00 0.00 0.00 0.00 0.00 0.00 3.16 0.00
+
* 4 * 0.00 0.00 0.00 0.00 0.00 0.00 2.47 0.00
+
* 5 * 0.00 0.00 0.00 0.00 0.00 0.00 1.89 0.00
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
*
*****

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US-101_NB_PM_NP_2040_PL

| | | | | |
|-----------------------------|-----------------|------------------|-----------------|-------------------|
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 301. VEH-HRS | 601. PASS-HRS | 992. VEH-HRS | 1984. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 19546. VEH-MI . | 39092. PASS-MI . | 64472. VEH-MI . | 128943. PASS-MI . |
| AVERAGE SYSTEM SPEED = | 65. MPH. | | 65. MPH. | |
| AVERAGE DENSITY = | 6. VPMPPL | | 6. VPMPPL | |
| TOTAL FUEL = | 977. GALLONS | | 3224. GALLONS | |
| TOTAL EMISSIONS = | 269. KILOGRAMS | | 886. KILOGRAMS | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | 30 | 0.00 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

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FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQQ QQQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP EEEEEEEEE
    
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FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREWAY AND ARTERIAL DESIGN FEATURES

| ** SUB NO. | ** SSEC | ** SSEC | ** DESIG N | ** ORG | ** TRK | ** SSEC | ** PCT | ** PCT | ** DES | ** SPECIAL | ** FF. SPD. | ** CAP. | ** ART | ** GRADE | ** SUBSECTI ON | ** LOCATI ON |
|------------|---------|---------|------------|----------|--------|---------|--------|-----------|---------|-------------|-------------|---------|-------------|-------------|--------------------------|--------------|
| ** SEC | ** LNS | ** CAP | ** LENGTH | ** SPEED | ** DES | ** GRAD | ** TRK | ** TRUCKS | ** RAMP | ** ALT. RTE | ** ALT. RTE | ** TYPE | ** ALT. RTE | ** ALT. RTE | ** LOCATION | ** LOCATION |
| ** 1 | 4 | 10000. | 500. | 65 | OD | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Seeding | ** |
| ** 2 | 3 | 7000. | 99999. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | ** |
| ** 3 | 3 | 7000. | 2830. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-87 to DLC loop-on | ** |
| ** 4 | 3 | 7000. | 930. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | DLC loop on to dia-on | ** |
| ** 5 | 3 | 7000. | 1490. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | DLC dia-on to Tomas off | ** |
| ** 6 | 3 | 7000. | 3020. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas off to on | ** |
| ** 7 | 3 | 7000. | 1030. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Tomas on to bowers off | ** |
| ** 8 | 3 | 7000. | 1440. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers off to loop-on | ** |
| ** 9 | 3 | 7000. | 1430. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers loop-on to dia | ** |
| ** 10 | 3 | 7000. | 3480. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Bowers dia-on to law-off | ** |
| ** 11 | 3 | 7000. | 1020. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Law off to loop-on | ** |
| ** 12 | 3 | 7000. | 980. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Lawr Loop to diag | ** |
| ** 13 | 3 | 7000. | 1800. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Lawrence On-ramp | ** |
| ** 14 | 3 | 7000. | 1500. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks Off-Ramp | ** |
| ** 15 | 3 | 6000. | 1300. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Fair Oaks | ** |
| ** 16 | 3 | 6000. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Fair Oaks On-Ramp | ** |
| ** 17 | 3 | 6000. | 1100. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks / Mathilda | ** |
| ** 18 | 4 | 7350. | 1000. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda NB Off-Ramp | ** |
| ** 19 | 3 | 6000. | 900. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | ** |
| ** 20 | 3 | 6000. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda NB On-Ramp | ** |

FREEWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT TRUCKS | DES SPECIAL RAMP | FF.SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION LOCATION |
|---------|----------|----------|-------------|--------------|---------|---------|-----------|---------|------------|------------------|------------------|---------------|----------|----------------|----------------------|
| ** 21 | 3 | 6000. | 100. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda |
| ** 22 | 3 | 6000. | 100. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda SB Off-ramp |
| ** 23 | 3 | 6000. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / SR-237 |
| ** 24 | 3 | 6000. | 1500. | 65 | D | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 WB Off-Ramp |
| ** 25 | 3 | 6000. | 800. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 / SR-237 |
| ** 26 | 3 | 6000. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 WB On-Ramp |
| ** 27 | 3 | 6000. | 800. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 / Ellis |
| ** 28 | 3 | 6000. | 1000. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Ellis Off-ramp |
| ** 29 | 3 | 6000. | 8000. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** 30 | 4 | 8000. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** 31 | 4 | 5500. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Dummy Bottleneck |
| ** 32 | 4 | 8000. | 2640. | 65 | D | 1.00 | 0.0 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End of Network |

***** INPUT HAS BEEN COMPLETED *****

- MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 4 IN TIME SLICE 1
--- THE MAXIMUM METERING RATE WILL PREVAIL.
- MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 4 IN TIME SLICE 2
--- THE MAXIMUM METERING RATE WILL PREVAIL.
- MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 6 IN TIME SLICE 2
--- THE MAXIMUM METERING RATE WILL PREVAIL.
- MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 4 IN TIME SLICE 3
--- THE MAXIMUM METERING RATE WILL PREVAIL.
- MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 6 IN TIME SLICE 3
--- THE MAXIMUM METERING RATE WILL PREVAIL.

FREEWAY TRAVEL TIME (MINUTES)

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | |
|--------------|---------------------|-------|-------|-------|-------|-------|
| | 1 | 2 | 3 | 4 | 5 | 6 |
| * 1 * | 0.09 | 22.00 | 22.83 | 23.43 | 24.49 | 32.51 |
| * 2 * | 0.00 | 0.00 | 0.59 | 1.19 | 2.25 | 10.27 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.45 | 1.51 | 9.52 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.90 | 8.92 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.81 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.64 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB SEC | NO. LNS | SSEC LENGTH | O-D ORG | DATA DES | DEMANDS SSEC | ADJUSTED ORG | VOLUMES DES | SSEC SSEC | SSEC CAP | WEAVE EFF | CONGEST LENGTH | STORAGE RATE | V/C RATIO | SPEED MPH | DENSITY VPMP | LOS LEVEL | FUEL MPG | EMI SS GS/VM |
|---------|---------|-------------|---------|----------|--------------|--------------|-------------|-----------|----------|-----------|----------------|--------------|-----------|-----------|--------------|-----------|----------|--------------|
| 1 | 4 | 500. | 6550. | 852. | 6550. | 6550. | 852. | 6550. | 10000. | 0. | 0. | 0. | .65 | 65. | 25.2 | C | 19.2 | 14.0 |
| 2 | 3 | 99999. | 0. | 0. | 5698. | 0. | 0. | 5698. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 3 | 3 | 2830. | 0. | 0. | 5698. | 0. | 0. | 5698. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 4 | 3 | 930. | 0. | 0. | 5698. | 0. | 0. | 5698. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 5 | 3 | 1490. | 0. | 0. | 5698. | 0. | 0. | 5698. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 6 | 3 | 3020. | 0. | 0. | 5698. | 0. | 0. | 5698. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 7 | 3 | 1030. | 0. | 0. | 5698. | 0. | 0. | 5698. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 8 | 3 | 1440. | 0. | 0. | 5698. | 0. | 0. | 5698. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 9 | 3 | 1430. | 0. | 0. | 5698. | 0. | 0. | 5698. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 10 | 3 | 3480. | 0. | 0. | 5698. | 0. | 0. | 5698. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 11 | 3 | 1020. | 0. | 0. | 5698. | 0. | 0. | 5698. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 12 | 3 | 980. | 0. | 0. | 5698. | 0. | 0. | 5698. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 13 | 3 | 1800. | 0. | 0. | 5698. | 0. | 0. | 5698. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 14 | 3 | 1500. | 0. | 557. | 5698. | 0. | 557. | 5698. | 6917. | 0. | 0. | 0. | .82 | 62. | 30.4 | D | 20.4 | 13.1 |
| 15 | 3 | 1300. | 0. | 0. | 5141. | 0. | 0. | 5141. | 6000. | 0. | 0. | 0. | .86 | 61. | 28.0 | D | 21.0 | 12.7 |
| 16 | 3 | 1000. | 468. | 0. | 5609. | 368. | 0. | 5509. | 5958. | 0. | 0. | 0. | .92 | 58. | 31.8 | D | 22.3 | 11.9 |
| 17 | 3 | 1100. | 0. | 0. | 5609. | 0. | 0. | 5509. | 6000. | 0. | 0. | 0. | .92 | 58. | 31.6 | D | 22.2 | 12.0 |
| 18 | 4 | 1000. | 0. | 1118. | 5609. | 0. | 1096. | 5509. | 7198. | 0. | 0. | 0. | .77 | 65. | 21.2 | C | 19.2 | 14.0 |
| 19 | 3 | 900. | 0. | 0. | 4491. | 0. | 0. | 4413. | 6000. | 0. | 0. | 0. | .74 | 64. | 22.8 | C | 19.4 | 13.8 |
| 20 | 3 | 100. | 278. | 0. | 4769. | 240. | 0. | 4653. | 5968. | 0. | 0. | 0. | .78 | 64. | 24.4 | C | 19.8 | 13.5 |
| 21 | 3 | 100. | 0. | 0. | 4769. | 0. | 0. | 4653. | 6000. | 0. | 0. | 0. | .78 | 64. | 24.3 | C | 19.7 | 13.6 |
| 22 | 3 | 100. | 0. | 0. | 4769. | 0. | 0. | 4653. | 6000. | 0. | 0. | 0. | .78 | 64. | 24.3 | C | 19.7 | 13.6 |
| 23 | 3 | 700. | 0. | 0. | 4769. | 0. | 0. | 4653. | 6000. | 0. | 0. | 0. | .78 | 64. | 24.3 | C | 19.7 | 13.6 |
| 24 | 3 | 1500. | 0. | 793. | 4769. | 0. | 772. | 4653. | 5899. | 0. | 0. | 0. | .79 | 63. | 24.5 | C | 19.9 | 13.5 |
| 25 | 3 | 800. | 0. | 0. | 3976. | 0. | 0. | 2990. | 6000. | 0. | 374. | 891. | .50 | 59. | 16.9 | F | 19.0 | 14.1 |
| 26 | 3 | 1000. | 1698. | 0. | 5674. | 1260. | 0. | 4250. | 5760. | 0. | ** 1000. | 891. | .74 | 44. | 31.9 | F | 20.8 | 13.0 |
| 27 | 3 | 800. | 0. | 0. | 5674. | 0. | 0. | 4250. | 6000. | 0. | ** 800. | 891. | .71 | 35. | 40.2 | F | 19.1 | 14.2 |
| 28 | 3 | 1000. | 0. | 284. | 5674. | 0. | 255. | 4250. | 5975. | 0. | ** 1000. | 891. | .71 | 29. | 48.6 | F | 18.4 | 14.8 |
| 29 | 3 | 8000. | 0. | 0. | 5390. | 0. | 0. | 3995. | 6000. | 0. | ** 8000. | 891. | .67 | 13. | 105.6 | F | 13.4 | 20.1 |
| 30 | 4 | 100. | 805. | 0. | 6195. | 805. | 0. | 4800. | 8000. | 0. | ** 100. | 891. | .60 | 7. | 183.2 | F | 9.5 | 26.8 |
| 31 | 4 | 1000. | 800. | 0. | 6995. | 700. | 0. | 5500. | 5500. | 0. | 0. | 0. | 1.00 | 65. | 21.2 | E | 19.2 | 14.0 |
| 32 | 4 | 2640. | 0. | 6995. | 6995. | 0. | 5500. | 5500. | 8000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 20.0 | 13.7 |

TOTAL 144589. = 27.4 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 53. 34.2 19.7 13.6

| | | | |
|----------------------------|--------------------|------------------|----------------------------------|
| | CURRENT TIME SLICE | | CUMULATIVE VALUES |
| FREWAY TRAVEL TIME = | 2889. VEH-HRS | 2900. PASS-HRS | 2889. VEH-HRS 2900. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 338. VEH-HRS | 345. PASS-HRS | 338. VEH-HRS 345. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 3227. VEH-HRS | 3244. PASS-HRS | 3227. VEH-HRS 3244. PASS-HRS |
| TOTAL TRAV DISTANCE = | 152282. VEH-MI. | 152905. PASS-MI. | 152282. VEH-MI. 152905. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 47. MPH | | 53. MPH |
| AVERAGE DENSITY = | 34. VPMP | | 34. VPMP |
| TOTAL FUEL = | 7833. GALLONS | | 7833. GALLONS |
| TOTAL EMISSIONS = | 2114. KI LOGRAMS | | 2114. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|--------|------------|-------|
| 1 | 0.00 | 2 | 60.03 | 3 | 1.70 | 4 | 0.56 | 5 | 0.89 |
| 6 | 1.81 | 7 | 0.62 | 8 | 0.86 | 9 | 0.86 | 10 | 2.09 |
| 11 | 0.61 | 12 | 0.59 | 13 | 1.08 | 14 | 1.03 | 15 | 1.20 |
| 16 | 2.01 | 17 | 2.08 | 18 | 0.00 | 19 | 0.11 | 20 | 0.03 |
| 21 | 0.03 | 22 | 0.03 | 23 | 0.19 | 24 | 0.51 | 25 | 0.95 |
| 26 | 6.87 | 27 | 9.85 | 28 | 17.69 | 29 | 419.04 | 30 | 12.50 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 545.8 VEH-HRS ***** AVERAGE DELAY = 7.79 MIN/VEH *****

***** RAMP DELAYS *****

AVERAGE

TOTAL

| | | QUEUE LENGTH | DELAY | US-101_NB_PM_P1_2040_PE | | HC | CO | NOX | EMISSIONS | |
|---------|---|--------------|---------|-------------------------|------|-------|------|-------|-----------|-------|
| | | VEHICLES | VEH-HRS | METERING DELAY | GAS | KGMS | KGMS | KGMS | KGMS | |
| | | | | MI MINUTES | GALS | | | | | |
| ON-RAMP | 2 | RAMP | 100. | 50.00 | 6.41 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 50.00 | 6.41 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| ON-RAMP | 3 | RAMP | 38. | 19.00 | 4.10 | 6.78 | 0.42 | 2.20 | 0.12 | 2.74 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 38. | 19.00 | 4.10 | 6.78 | 0.42 | 2.20 | 0.12 | 2.74 |
| ON-RAMP | 4 | RAMP | 438. | 219.00 | 6.78 | 78.20 | 4.85 | 25.37 | 1.35 | 31.57 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 438. | 219.00 | 6.78 | 78.20 | 4.85 | 25.37 | 1.35 | 31.57 |
| ON-RAMP | 6 | RAMP | 100. | 50.00 | 4.31 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 50.00 | 4.31 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |

```
*****
**                                     **
**      FREEWAY TRAVEL TIME (MI MINUTES)      **
**                                     **
*****
```

```
*****
* ORIGINS DESTINATIONS ACROSS *
* DOWN   1   2   3   4   5   6   *
+-----+-----+-----+-----+-----+-----+
+
+ * 1 * 0.09 22.39 24.85 29.20 35.46 49.90 *
+
+ * 2 * 0.00 0.00 1.87 6.22 12.48 26.91 *
+
+ * 3 * 0.00 0.00 0.00 3.29 9.55 23.98 *
+
+ * 4 * 0.00 0.00 0.00 0.00 4.00 18.44 *
+
+ * 5 * 0.00 0.00 0.00 0.00 0.00 0.84 *
+
+ * 6 * 0.00 0.00 0.00 0.00 0.00 0.64 *
+
+ * * *
*****
```

```
*****
*                                     *
*      TIME SLICE FREEWAY PERFORMANCE TABLE      *
*                                     *
*****
```

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | | |
|-----------|----------|------------|-----------|------------|-----------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|-------|------|------|------|
| * SEC LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | | | |
| * 1 | 4 | 500. | 6681. | 869. | 6681. | 6681. | 869. | 6681. | 10000. | 0. | 0. | 0. | .67 | 65. | 25.7 | C | 19.2 | 14.0 | |
| * 2 | 3 | 99999. | 0. | 0. | 5812. | 0. | 0. | 5812. | 7000. | 0. | ** | 1500. | 865. | .72 | 37. | 45.0 | F | 19.1 | 14.2 |
| * 3 | 3 | 2830. | 0. | 0. | 5812. | 0. | 0. | 5812. | 7000. | 0. | ** | 1300. | 865. | .69 | 25. | 54.8 | F | 17.1 | 15.8 |
| * 4 | 3 | 930. | 0. | 0. | 5812. | 0. | 0. | 5812. | 7000. | 0. | ** | 1000. | 865. | .78 | 25. | 62.4 | F | 18.6 | 15.1 |
| * 5 | 3 | 1490. | 0. | 0. | 5812. | 0. | 0. | 5812. | 7000. | 0. | ** | 1100. | 865. | .77 | 22. | 71.0 | F | 17.8 | 15.9 |
| * 6 | 3 | 3020. | 0. | 0. | 5812. | 0. | 0. | 5812. | 7000. | 0. | ** | 1000. | 865. | .65 | 14. | 85.3 | F | 13.4 | 19.8 |
| * 7 | 3 | 1030. | 0. | 0. | 5812. | 0. | 0. | 5812. | 7000. | 0. | ** | 900. | 865. | .58 | 10. | 119.8 | F | 11.6 | 21.9 |
| * 8 | 3 | 1440. | 0. | 0. | 5812. | 0. | 0. | 5812. | 7000. | 0. | ** | 100. | 865. | .62 | 10. | 123.1 | F | 11.8 | 22.0 |
| * 9 | 3 | 1430. | 0. | 0. | 5812. | 0. | 0. | 5812. | 7000. | 0. | ** | 100. | 865. | .62 | 10. | 126.0 | F | 11.7 | 22.2 |
| * 10 | 3 | 3480. | 0. | 0. | 5812. | 0. | 0. | 5812. | 7000. | 0. | ** | 100. | 865. | .62 | 10. | 127.8 | F | 11.6 | 22.3 |
| * 11 | 3 | 1020. | 0. | 0. | 5812. | 0. | 0. | 5812. | 7000. | 0. | ** | 700. | 865. | .62 | 9. | 135.1 | F | 11.3 | 22.9 |
| * 12 | 3 | 980. | 0. | 0. | 5812. | 0. | 0. | 5812. | 7000. | 0. | ** | 1500. | 865. | .63 | 8. | 149.0 | F | 10.8 | 24.2 |
| * 13 | 3 | 1800. | 0. | 0. | 5812. | 0. | 0. | 4947. | 7000. | 0. | ** | 800. | 865. | .44 | 4. | 220.9 | F | 8.5 | 28.4 |
| * 14 | 3 | 1500. | 0. | 835. | 5812. | 0. | 835. | 4947. | 6875. | 0. | ** | 1000. | 865. | .68 | 8. | 156.8 | F | 11.1 | 24.7 |
| * 15 | 3 | 1300. | 0. | 0. | 4977. | 0. | 0. | 4112. | 6000. | 0. | ** | 800. | 865. | .66 | 8. | 170.1 | F | 10.5 | 25.5 |
| * 16 | 3 | 1000. | 527. | 0. | 5504. | 527. | 0. | 4639. | 5957. | 0. | ** | 1000. | 865. | .66 | 8. | 168.7 | F | 10.5 | 25.4 |
| * 17 | 3 | 1100. | 0. | 0. | 5504. | 0. | 0. | 4639. | 6000. | 0. | ** | 8000. | 865. | .61 | 7. | 182.2 | F | 9.6 | 26.7 |
| * 18 | 4 | 1000. | 0. | 1190. | 5504. | 0. | 1189. | 4639. | 7190. | 0. | ** | 100. | 865. | .55 | 6. | 197.9 | F | 8.8 | 28.0 |
| * 19 | 3 | 900. | 0. | 0. | 4314. | 0. | 0. | 3450. | 6000. | 0. | ** | 100. | 865. | .62 | 10. | 127.8 | F | 11.6 | 22.3 |
| * 20 | 3 | 100. | 300. | 0. | 4614. | 240. | 0. | 3690. | 5968. | 0. | ** | 100. | 865. | .62 | 10. | 126.0 | F | 11.7 | 22.2 |
| * 21 | 3 | 100. | 0. | 0. | 4614. | 0. | 0. | 3690. | 6000. | 0. | ** | 100. | 865. | .62 | 10. | 127.8 | F | 11.6 | 22.3 |
| * 22 | 3 | 100. | 0. | 0. | 4614. | 0. | 0. | 3690. | 6000. | 0. | ** | 100. | 865. | .62 | 10. | 127.8 | F | 11.6 | 22.3 |
| * 23 | 3 | 700. | 0. | 0. | 4614. | 0. | 0. | 3690. | 6000. | 0. | ** | 700. | 865. | .62 | 9. | 135.1 | F | 11.3 | 22.9 |
| * 24 | 3 | 1500. | 0. | 1044. | 4614. | 0. | 1024. | 3690. | 5870. | 0. | ** | 1500. | 865. | .63 | 8. | 149.0 | F | 10.8 | 24.2 |
| * 25 | 3 | 800. | 0. | 0. | 3570. | 0. | 0. | 2667. | 6000. | 0. | ** | 800. | 865. | .44 | 4. | 220.9 | F | 8.5 | 28.4 |
| * 26 | 3 | 1000. | 1673. | 0. | 5243. | 1266. | 0. | 3933. | 5766. | 0. | ** | 1000. | 865. | .68 | 8. | 156.8 | F | 11.1 | 24.7 |
| * 27 | 3 | 800. | 0. | 0. | 5243. | 0. | 0. | 3933. | 6000. | 0. | ** | 800. | 865. | .66 | 8. | 170.1 | F | 10.5 | 25.5 |
| * 28 | 3 | 1000. | 0. | 309. | 5243. | 0. | 278. | 3933. | 5975. | 0. | ** | 1000. | 865. | .66 | 8. | 168.7 | F | 10.5 | 25.4 |
| * 29 | 3 | 8000. | 0. | 0. | 4934. | 0. | 0. | 3655. | 6000. | 0. | ** | 8000. | 865. | .61 | 7. | 182.2 | F | 9.6 | 26.7 |
| * 30 | 4 | 100. | 737. | 0. | 5671. | 737. | 0. | 4392. | 8000. | 0. | ** | 100. | 865. | .55 | 6. | 197.9 | F | 8.8 | 28.0 |
| * 31 | 4 | 1000. | 1600. | 0. | 7271. | 1108. | 0. | 5500. | 5500. | 0. | ** | 1000. | 865. | .62 | 10. | 126.0 | F | 11.7 | 22.2 |
| | | | | | | | | | | 0. | ** | 1000. | 865. | .62 | 10. | 126.0 | F | 11.7 | 22.2 |

```

* 32 4 2640. 0. 7271. 7271. 0. 5500. 5500. US-101_NB_PM_P1_2040_PE 0. 0. .69 65. 21.2 C 20.0 13.7 *
*
*****
* TOTAL 144589. = 27.4 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 39. 46.7 18.9 14.1 *
*
*****

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UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
TIME SLICE 2 OF 3

| CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | |
|----------------------------|-----------------|------------------|-----------------|-------------------|--|--|--|
| FREWAY TRAVEL TIME = | 3917. VEH-HRS | 3931. PASS-HRS | 6806. VEH-HRS | 6831. PASS-HRS | | | |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | | | |
| ON-RAMP MRG/CAP DELAY = | 1156. VEH-HRS | 1200. PASS-HRS | 1494. VEH-HRS | 1545. PASS-HRS | | | |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | | | |
| TOTAL SYSTEM TRAVEL TIME = | 5072. VEH-HRS | 5131. PASS-HRS | 8299. VEH-HRS | 8376. PASS-HRS | | | |
| TOTAL TRAVEL DISTANCE = | 152271. VEH-MI. | 152890. PASS-MI. | 304553. VEH-MI. | 305795. PASS-MI. | | | |
| AVERAGE SYSTEM SPEED = | 30. MPH. | | 45. MPH. | | | | |
| AVERAGE DENSITY = | 47. VPMP | | 40. VPMP | | | | |
| TOTAL FUEL = | 8448. GALLONS | | 16281. GALLONS | | | | |
| TOTAL EMISSIONS = | 2309. KILOGRAMS | | 4423. KILOGRAMS | | | | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|--------|------------|-------|
| 1 | 0.01 | 2 | 75.91 | 3 | 2.15 | 4 | 0.71 | 5 | 1.13 |
| 6 | 2.29 | 7 | 0.78 | 8 | 1.09 | 9 | 1.09 | 10 | 2.64 |
| 11 | 0.77 | 12 | 0.74 | 13 | 3.53 | 14 | 19.20 | 15 | 28.73 |
| 16 | 24.53 | 17 | 32.61 | 18 | 55.51 | 19 | 56.92 | 20 | 6.34 |
| 21 | 6.50 | 22 | 6.60 | 23 | 48.83 | 24 | 114.27 | 25 | 94.68 |
| 26 | 77.61 | 27 | 68.14 | 28 | 84.37 | 29 | 742.89 | 30 | 13.71 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 1574.3 VEH-HRS ***** AVERAGE DELAY = 25.06 MIN/VEH *****

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UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
TIME SLICE 2 OF 3

***** RAMP DELAYS *****

| | | QUEUE LENGTH | DELAY | AVERAGE | GAS | HC | CO | NOX | TOTAL | |
|---------|---|--------------|---------|----------------|-------|--------|-------|-------|-----------|-------|
| | | VEHICLES | VEH-HRS | METERING DELAY | GALS | KGMS | KGMS | KGMS | EMISSIONS | |
| | | | | MINUTES | | | | | KGMS | |
| ON-RAMP | 2 | RAMP | 100. | 100.00 | 9.57 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 100.00 | 9.57 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP | 3 | RAMP | 98. | 68.00 | 12.07 | 24.28 | 1.51 | 7.88 | 0.42 | 9.80 |
| | | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 98. | 68.00 | 12.07 | 24.28 | 1.51 | 7.88 | 0.42 | 9.80 |
| ON-RAMP | 4 | RAMP | 845. | 641.50 | 16.41 | 229.07 | 14.21 | 74.32 | 3.94 | 92.47 |
| | | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 845. | 641.50 | 16.41 | 229.07 | 14.21 | 74.32 | 3.94 | 92.47 |
| ON-RAMP | 6 | RAMP | 592. | 346.00 | 13.91 | 123.55 | 7.66 | 40.08 | 2.13 | 49.87 |
| | | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 592. | 346.00 | 13.91 | 123.55 | 7.66 | 40.08 | 2.13 | 49.87 |

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UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
TIME SLICE 3 OF 3

**
** FREeway TRAVEL TIME (MINUTES) **
**

* ORIGINS DESTINATIONS ACROSS *
* DOWN 1 2 3 4 5 6 *

* * * * *
* 1 * 0.09 27.12 33.27 39.21 45.16 58.29 *
* 2 * 0.00 0.00 4.21 10.14 16.10 29.23 *
* 3 * 0.00 0.00 0.00 4.19 10.14 23.28 *
* 4 * 0.00 0.00 0.00 0.00 3.76 16.90 *
* 5 * 0.00 0.00 0.00 0.00 0.00 0.83 *

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB | * NO. | * SSEC | * O-D | * DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | |
|---------|---------|----------|-------|--------|-----------|------------|-----------|--------|---------|-----------------|----------------|-----------|---------|-----------|---------|--------|-------------|------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * SSEC | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP/L | * LEVEL | * MPG | * GS/VM | |
| * 1 | 4 | 500. | 5769. | 750. | 5769. | 5769. | 750. | 5769. | 10000. | 0. | 0. | 0. | .58 | 65. | 22.2 | C | 19.2 | 14.0 |
| * 2 | 3 | 99999. | 0. | 0. | 5019. | 0. | 0. | 5019. | 7000. | 0. | 0. | 0. | .72 | 65. | 25.9 | C | 19.3 | 13.9 |
| * 3 | 3 | 2830. | 0. | 0. | 5019. | 0. | 0. | 5019. | 7000. | 0. | 0. | 0. | .72 | 65. | 25.9 | C | 19.3 | 13.9 |
| * 4 | 3 | 930. | 0. | 0. | 5019. | 0. | 0. | 5019. | 7000. | 0. | 0. | 0. | .72 | 65. | 25.9 | C | 19.3 | 13.9 |
| * 5 | 3 | 1490. | 0. | 0. | 5019. | 0. | 0. | 5019. | 7000. | 0. | 0. | 0. | .72 | 65. | 25.9 | C | 19.3 | 13.9 |
| * 6 | 3 | 3020. | 0. | 0. | 5019. | 0. | 0. | 5019. | 7000. | 0. | 0. | 0. | .72 | 65. | 25.9 | C | 19.3 | 13.9 |
| * 7 | 3 | 1030. | 0. | 0. | 5019. | 0. | 0. | 5019. | 7000. | 0. | 0. | 0. | .72 | 65. | 25.9 | C | 19.3 | 13.9 |
| * 8 | 3 | 1440. | 0. | 0. | 5019. | 0. | 0. | 5019. | 7000. | 0. | 0. | 0. | .72 | 65. | 25.9 | C | 19.3 | 13.9 |
| * 9 | 3 | 1430. | 0. | 0. | 5019. | 0. | 0. | 5019. | 7000. | 0. | 0. | 0. | .72 | 65. | 25.9 | C | 19.3 | 13.9 |
| * 10 | 3 | 3480. | 0. | 0. | 5019. | 0. | 0. | 4564. | 7000. | 0. | * 1515. | .455. | .65 | 43. | 35.1 | F | 18.3 | 14.6 |
| * 11 | 3 | 1020. | 0. | 0. | 5019. | 0. | 0. | 4564. | 7000. | 0. | ** 1020. | .455. | .65 | 16. | 96.6 | F | 14.2 | 18.7 |
| * 12 | 3 | 980. | 0. | 0. | 5019. | 0. | 0. | 4564. | 7000. | 0. | ** 980. | .455. | .65 | 11. | 135.0 | F | 12.5 | 21.3 |
| * 13 | 3 | 1800. | 0. | 0. | 5019. | 0. | 0. | 4564. | 7000. | 0. | ** 1800. | .455. | .65 | 8. | 185.5 | F | 10.8 | 24.7 |
| * 14 | 3 | 1500. | 0. | 661. | 5019. | 0. | 661. | 4564. | 6901. | 0. | ** 1500. | .455. | .66 | 8. | 193.9 | F | 10.6 | 25.3 |
| * 15 | 3 | 1300. | 0. | 0. | 4358. | 0. | 0. | 3903. | 6000. | 0. | ** 1300. | .455. | .65 | 8. | 171.4 | F | 10.4 | 25.6 |
| * 16 | 3 | 1000. | 451. | 0. | 4809. | 451. | 0. | 4354. | 5961. | 0. | ** 1000. | .455. | .73 | 10. | 149.5 | F | 12.7 | 23.1 |
| * 17 | 3 | 1100. | 0. | 0. | 4809. | 0. | 0. | 4354. | 6000. | 0. | ** 1100. | .455. | .73 | 10. | 151.7 | F | 12.5 | 23.3 |
| * 18 | 4 | 1000. | 0. | 952. | 4809. | 0. | 953. | 4354. | 7222. | 0. | ** 1000. | .455. | .60 | 7. | 166.0 | F | 9.5 | 26.8 |
| * 19 | 3 | 900. | 0. | 0. | 3857. | 0. | 0. | 3400. | 6000. | 0. | ** 900. | .455. | .57 | 6. | 193.3 | F | 9.0 | 27.7 |
| * 20 | 3 | 100. | 235. | 0. | 4092. | 240. | 0. | 3640. | 5975. | 0. | ** 100. | .455. | .61 | 7. | 181.4 | F | 9.6 | 26.7 |
| * 21 | 3 | 100. | 0. | 0. | 4092. | 0. | 0. | 3640. | 6000. | 0. | ** 100. | .455. | .61 | 7. | 182.8 | F | 9.5 | 26.8 |
| * 22 | 3 | 100. | 0. | 0. | 4092. | 0. | 0. | 3640. | 6000. | 0. | ** 100. | .455. | .61 | 7. | 182.8 | F | 9.5 | 26.8 |
| * 23 | 3 | 700. | 0. | 0. | 4092. | 0. | 0. | 3640. | 6000. | 0. | ** 700. | .455. | .61 | 7. | 182.8 | F | 9.5 | 26.8 |
| * 24 | 3 | 1500. | 0. | 883. | 4092. | 0. | 884. | 3640. | 5889. | 0. | ** 1500. | .455. | .62 | 7. | 176.5 | F | 9.7 | 26.5 |
| * 25 | 3 | 800. | 0. | 0. | 3209. | 0. | 0. | 2756. | 6000. | 0. | ** 800. | .455. | .46 | 4. | 221.3 | F | 8.4 | 28.7 |
| * 26 | 3 | 1000. | 1364. | 0. | 4573. | 1306. | 0. | 4062. | 5806. | 0. | ** 1000. | .455. | .70 | 9. | 153.4 | F | 11.6 | 24.2 |
| * 27 | 3 | 800. | 0. | 0. | 4573. | 0. | 0. | 4062. | 6000. | 0. | ** 800. | .455. | .68 | 8. | 164.4 | F | 11.0 | 24.9 |
| * 28 | 3 | 1000. | 0. | 207. | 4573. | 0. | 212. | 4062. | 5982. | 0. | ** 1000. | .455. | .68 | 8. | 163.4 | F | 11.0 | 24.8 |
| * 29 | 3 | 8000. | 0. | 0. | 4366. | 0. | 0. | 3851. | 6000. | 0. | ** 8000. | .455. | .64 | 7. | 173.7 | F | 10.2 | 25.9 |
| * 30 | 4 | 100. | 652. | 0. | 5018. | 652. | 0. | 4503. | 8000. | 0. | ** 100. | .455. | .56 | 6. | 194.3 | F | 8.9 | 27.7 |
| * 31 | 4 | 1000. | 750. | 0. | 5768. | 998. | 0. | 5500. | 5500. | 0. | 0. | 0. | 1.00 | 65. | 21.2 | E | 19.2 | 14.0 |
| * 32 | 4 | 2640. | 0. | 5768. | 5768. | 0. | 5500. | 5500. | 8000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 20.0 | 13.7 |
| * TOTAL | 144589. | = | 27.4 | MILES | | | | | | MAX(V/C) = 1.00 | LOWEST LOS = F | AVG = 31. | 50.7 | | 17.3 | 15.5 | | |

| CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | | |
|----------------------------|---------|------------|---------|-------------------|---------|------------|---------|----------|
| FREEWAY TRAVEL TIME = | 4231. | VEH-HRS | 4245. | PASS-HRS | 11036. | VEH-HRS | 11076. | PASS-HRS |
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 1538. | VEH-HRS | 1599. | PASS-HRS | 3031. | VEH-HRS | 3144. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 5768. | VEH-HRS | 5844. | PASS-HRS | 14067. | VEH-HRS | 14219. | PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 133231. | VEH-MI. | 133836. | PASS-MI. | 437784. | VEH-MI. | 439631. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 23. | MPH | | | 40. | MPH | | |
| AVERAGE DENSITY = | 51. | VPMP/L | | | 44. | VPMP/L | | |
| TOTAL FUEL = | 8248. | GALLONS | | | 24530. | GALLONS | | |
| TOTAL EMISSIONS = | 2283. | KI LOGRAMS | | | 6706. | KI LOGRAMS | | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|--------|------------|--------|------------|--------|
| 1 | 0.00 | 2 | 8.80 | 3 | 0.25 | 4 | 0.08 | 5 | 0.13 |
| 6 | 0.27 | 7 | 0.09 | 8 | 0.13 | 9 | 0.13 | 10 | 25.17 |
| 11 | 44.82 | 12 | 64.29 | 13 | 166.97 | 14 | 145.27 | 15 | 111.81 |
| 16 | 72.27 | 17 | 80.88 | 18 | 113.04 | 19 | 89.92 | 20 | 9.25 |
| 21 | 9.33 | 22 | 9.33 | 23 | 65.29 | 24 | 134.51 | 25 | 94.19 |
| 26 | 75.32 | 27 | 65.28 | 28 | 81.01 | 29 | 699.61 | 30 | 13.41 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 2180.8 VEH-HRS ***** AVERAGE DELAY = 33.12 MIN/VEH *****

***** RAMP DELAYS *****

US-101_NB_PM_P1_2040_PE

| | | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-----------|---------|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|
| ON-RAMP 2 | RAMP | 100. | 100.00 | 10.89 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 100.00 | 10.89 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP 3 | RAMP | 93. | 95.50 | 17.21 | 34.10 | 2.12 | 11.06 | 0.59 | 13.77 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 93. | 95.50 | 17.21 | 34.10 | 2.12 | 11.06 | 0.59 | 13.77 |
| ON-RAMP 4 | RAMP | 903. | 874.00 | 21.82 | 312.09 | 19.36 | 101.25 | 5.37 | 125.98 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 903. | 874.00 | 21.82 | 312.09 | 19.36 | 101.25 | 5.37 | 125.98 |
| ON-RAMP 6 | RAMP | 345. | 468.25 | 22.58 | 167.20 | 10.37 | 54.25 | 2.88 | 67.50 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 345. | 468.25 | 22.58 | 167.20 | 10.37 | 54.25 | 2.88 | 67.50 |

| | | | | | | | | | | | | | | | | | | | |
|----|----|----|-------|------|----|----|------|-----|----|-----|-----|-----|----|------|-----|---------------------|----|----|----|
| ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** | ** |
| ** | 19 | 2 | 3000. | 900. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | ** | ** | ** |
| ** | 20 | 2 | 3000. | 100. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda NB On-Ramp | ** | ** | ** |

FREEWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SEC | LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT DES TRUCKS | SPECIAL RAMP | FF. SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION LOCATION |
|---------|-----|-----|----------|-------------|--------------|---------|---------|-----------|---------|----------------|--------------|-------------------|---------------|----------|----------------|----------------------|
| ** | 21 | 2 | 3000. | 100. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda |
| ** | 22 | 2 | 3000. | 100. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda SB Off-ramp |
| ** | 23 | 2 | 3000. | 700. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / SR-237 |
| ** | 24 | 2 | 3000. | 1500. | 65 | D | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 WB Off-Ramp |
| ** | 25 | 2 | 3000. | 800. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 / SR-237 |
| ** | 26 | 2 | 3000. | 1000. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 WB On-Ramp |
| ** | 27 | 2 | 3000. | 800. | 65 | | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 / Ellis |
| ** | 28 | 2 | 3000. | 1000. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Ellis Off-ramp |
| ** | 29 | 2 | 3000. | 8000. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** | 30 | | | | | | | | | | | | | | | |
| ** | 31 | | | | | | | | | | | | | | | |
| ** | 32 | | | | | | | | | | | | | | | |

FREEWAY TRAVEL TIME (MINUTES)

| ORIGINS DOWN | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
|--------------|------|-------|-------|-------|-------|-------|------|
| 1 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | 0.00 | 21.14 | 21.91 | 22.51 | 23.14 | 24.54 | 0.00 |
| 3 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.16 | 0.00 |
| 4 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.47 | 0.00 |
| 5 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.89 | 0.00 |
| 6 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 7 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

US-101_NB_PM_P1_2040_PL

Table with columns: SUB NO., SSEC, O-D DATA, DEMANDS, ADJUSTED VOLUMES, SSEC, WEAVE, CONGEST, STORAGE, V/C, SPEED, DENSITY, LOS, FUEL, EMISSIONS. Includes summary row: TOTAL 140349. = 26.6 MILES MAX(V/C) = 0.28 LOWEST LOS = A AVG = 65. 6.5 20.0 13.7

Table with columns: CURRENT TIME SLICE, CUMULATIVE VALUES. Rows include: FREeway TRAVEL TIME, FREeway MERGE DELAY, ON-RAMP MRG/CAP DELAY, OFF-RAMP DELAY, TOTAL SYSTEM TRAVEL TIME, TOTAL FRWAY TRAV DISTANCE, AVERAGE SYSTEM SPEED, AVERAGE DENSITY, TOTAL FUEL, TOTAL EMISSIONS.

***** MAINTENANCE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

Table with columns: SUBSECTION, DELAY. Rows 1-32 showing delay values for each subsection.

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

**
** FREEWAY TRAVEL TIME (MINUTES)
**

Table with columns: ORIGINS, DESTINATIONS ACROSS. Rows 1 and 2 showing origin and destination data.

 ** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | |
|-----------|--|-----------------------|-------|-------|-------|-------|-------|------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| + * 1 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + * 2 * | | 0.00 | 21.14 | 21.91 | 22.51 | 23.14 | 24.54 | 0.00 |
| + * 3 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.16 | 0.00 |
| + * 4 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.47 | 0.00 |
| + * 5 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.89 | 0.00 |
| + * 6 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + * 7 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB | * NO. | * SSEC | * O-D | * DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISS | | |
|---------|---------|----------|-------|--------|-----------|------------|-----------|--------|---------|-----------|-----------|--------|---------|-----------|----------------|-----------|---------|---------|------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | |
| * 1 | | | | | | | | | | | | | | | | | | | |
| * 2 | 2 | 99999. | 750. | 0. | 750. | 750. | 0. | 750. | 3000. | 0. | 0. | 0. | .25 | 65. | 5.8 | A | 20.0 | 13.7 | |
| * 3 | 2 | 2830. | 0. | 0. | 750. | 0. | 0. | 750. | 3000. | 0. | 0. | 0. | .25 | 65. | 5.8 | A | 20.0 | 13.7 | |
| * 4 | 2 | 930. | 0. | 0. | 750. | 0. | 0. | 750. | 3000. | 0. | 0. | 0. | .25 | 65. | 5.8 | A | 20.0 | 13.7 | |
| * 5 | 2 | 1490. | 0. | 0. | 750. | 0. | 0. | 750. | 3000. | 0. | 0. | 0. | .25 | 65. | 5.8 | A | 20.0 | 13.7 | |
| * 6 | 2 | 3020. | 0. | 0. | 750. | 0. | 0. | 750. | 3000. | 0. | 0. | 0. | .25 | 65. | 5.8 | A | 20.0 | 13.7 | |
| * 7 | 2 | 1030. | 0. | 0. | 750. | 0. | 0. | 750. | 3000. | 0. | 0. | 0. | .25 | 65. | 5.8 | A | 20.0 | 13.7 | |
| * 8 | 2 | 1440. | 0. | 0. | 750. | 0. | 0. | 750. | 3000. | 0. | 0. | 0. | .25 | 65. | 5.8 | A | 20.0 | 13.7 | |
| * 9 | 2 | 1430. | 0. | 0. | 750. | 0. | 0. | 750. | 3000. | 0. | 0. | 0. | .25 | 65. | 5.8 | A | 20.0 | 13.7 | |
| * 10 | 2 | 3480. | 0. | 0. | 750. | 0. | 0. | 750. | 3000. | 0. | 0. | 0. | .25 | 65. | 5.8 | A | 20.0 | 13.7 | |
| * 11 | 2 | 1020. | 0. | 0. | 750. | 0. | 0. | 750. | 3000. | 0. | 0. | 0. | .25 | 65. | 5.8 | A | 20.0 | 13.7 | |
| * 12 | 2 | 980. | 0. | 0. | 750. | 0. | 0. | 750. | 3000. | 0. | 0. | 0. | .25 | 65. | 5.8 | A | 20.0 | 13.7 | |
| * 13 | 2 | 1800. | 0. | 0. | 750. | 0. | 0. | 750. | 3000. | 0. | 0. | 0. | .25 | 65. | 5.8 | A | 20.0 | 13.7 | |
| * 14 | 2 | 1500. | 0. | 99. | 750. | 0. | 99. | 750. | 3000. | 0. | 0. | 0. | .25 | 65. | 5.8 | A | 20.0 | 13.7 | |
| * 15 | 2 | 1300. | 0. | 0. | 651. | 0. | 0. | 651. | 3000. | 0. | 0. | 0. | .22 | 65. | 5.0 | A | 20.0 | 13.7 | |
| * 16 | 2 | 1000. | 39. | 0. | 690. | 39. | 0. | 690. | 3000. | 0. | 0. | 0. | .23 | 65. | 5.3 | A | 20.0 | 13.7 | |
| * 17 | 2 | 1100. | 0. | 0. | 690. | 0. | 0. | 690. | 3000. | 0. | 0. | 0. | .23 | 65. | 5.3 | A | 20.0 | 13.7 | |
| * 18 | 2 | 1000. | 0. | 128. | 690. | 0. | 128. | 690. | 3000. | 0. | 0. | 0. | .23 | 65. | 5.3 | A | 20.0 | 13.7 | |
| * 19 | 2 | 900. | 0. | 0. | 562. | 0. | 0. | 562. | 3000. | 0. | 0. | 0. | .19 | 65. | 4.3 | A | 20.0 | 13.7 | |
| * 20 | 2 | 100. | 25. | 0. | 587. | 25. | 0. | 587. | 3000. | 0. | 0. | 0. | .20 | 65. | 4.5 | A | 20.0 | 13.7 | |
| * 21 | 2 | 100. | 0. | 0. | 587. | 0. | 0. | 587. | 3000. | 0. | 0. | 0. | .20 | 65. | 4.5 | A | 20.0 | 13.7 | |
| * 22 | 2 | 100. | 0. | 0. | 587. | 0. | 0. | 587. | 3000. | 0. | 0. | 0. | .20 | 65. | 4.5 | A | 20.0 | 13.7 | |
| * 23 | 2 | 700. | 0. | 0. | 587. | 0. | 0. | 587. | 3000. | 0. | 0. | 0. | .20 | 65. | 4.5 | A | 20.0 | 13.7 | |
| * 24 | 2 | 1500. | 0. | 111. | 587. | 0. | 111. | 587. | 3000. | 0. | 0. | 0. | .20 | 65. | 4.5 | A | 20.0 | 13.7 | |
| * 25 | 2 | 800. | 0. | 0. | 476. | 0. | 0. | 476. | 3000. | 0. | 0. | 0. | .16 | 65. | 3.7 | A | 20.0 | 13.7 | |
| * 26 | 2 | 1000. | 194. | 0. | 670. | 194. | 0. | 670. | 3000. | 0. | 0. | 0. | .22 | 65. | 5.2 | A | 20.0 | 13.7 | |
| * 27 | 2 | 800. | 0. | 0. | 670. | 0. | 0. | 670. | 3000. | 0. | 0. | 0. | .22 | 65. | 5.2 | A | 20.0 | 13.7 | |
| * 28 | 2 | 1000. | 0. | 18. | 670. | 0. | 18. | 670. | 3000. | 0. | 0. | 0. | .22 | 65. | 5.2 | A | 20.0 | 13.7 | |
| * 29 | 2 | 8000. | 0. | 652. | 652. | 0. | 652. | 652. | 3000. | 0. | 0. | 0. | .22 | 65. | 5.0 | A | 20.0 | 13.7 | |
| * 30 | | | | | | | | | | | | | | | | | | | |
| * 31 | | | | | | | | | | | | | | | | | | | |
| * 32 | | | | | | | | | | | | | | | | | | | |
| * TOTAL | 140349. | = | 26.6 | MILES | | | | | | | | | | 0.25 | LOWEST LOS = A | AVG = 65. | 5.7 | 20.0 | 13.7 |

FREWAY TRAVEL TIME = CURRENT TIME SLICE CUMULATIVE VALUES
 301. VEH-HRS 601. PASS-HRS 992. VEH-HRS 1983. PASS-HRS

US-101_NB_PM_P1_2040_PL

| | | | | |
|-----------------------------|----------------|-----------------|----------------|------------------|
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 301. VEH-HRS | 601. PASS-HRS | 992. VEH-HRS | 1983. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 19538. VEH-MI. | 39076. PASS-MI. | 64458. VEH-MI. | 128917. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 65. MPH. | | 65. MPH. | |
| AVERAGE DENSITY = | 6. VPMP | | 6. VPMP | |
| TOTAL FUEL = | 977. GALLONS | | 3223. GALLONS | |
| TOTAL EMISSIONS = | 268. KILOGRAMS | | 886. KILOGRAMS | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | 30 | 0.00 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

```

FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ      1111      222222 PPPPPPPP EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF      RRR      RRR EEE      QQQQQ QQQQQ 1111 222 222 PPP      PPP EEE
FFF      RRR      RRR EEE      QQQQ      QQQQ 1111      222 PPP      PPP EEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ      QQQQ 1111      222 PPPPPPPP EEEEEEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ      QQQQ 1111      222 PPPPPPPP EEEEEEE
FFF      RRR RRR EEE      QQQQ      QQQ QQQ 1111      2222 PPP      EEE
FFF      RRR RRR EEE      Q*UC*      QQQQ 1111      222 PPP      EEE
FFF      RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP      EEEEEEEEE
FFF      RRR      RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP      EEEEEEEEE
    
```

FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREWAY AND ARTERIAL DESIGN FEATURES

| ** SUB NO. | ** SSEC | ** SSEC | ** DESIG N | ** ORG | ** TRK | ** SSEC | ** PCT | ** PCT | ** DES | ** SPECIAL | ** FF. SPD. | ** CAP. | ** ART | ** GRADE | ** SUBSECTI ON | ** LOCATI ON |
|------------|---------|-----------|------------|----------|--------|---------|--------|-----------|---------|-------------|-------------|---------|-------------|-------------|------------------------------|--------------|
| ** SEC | ** LNS | ** CAP | ** LENGTH | ** SPEED | ** DES | ** GRAD | ** TRK | ** TRUCKS | ** RAMP | ** ALT. RTE | ** ALT. RTE | ** TYPE | ** ALT. RTE | ** ALT. RTE | ** LOCATION | ** LOCATION |
| ** 1 | ** 4 | ** 10000. | ** 500. | ** 65 | ** OD | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Seeding | ** |
| ** 2 | ** 3 | ** 7000. | ** 99999. | ** 65 | ** | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Queue Capture | ** |
| ** 3 | ** 3 | ** 7000. | ** 2830. | ** 65 | ** | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** SR-87 to DLC loop-on | ** |
| ** 4 | ** 3 | ** 7000. | ** 930. | ** 65 | ** | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** DLC loop on to di a-on | ** |
| ** 5 | ** 3 | ** 7000. | ** 1490. | ** 65 | ** | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** DLC di a-on to Tomas off | ** |
| ** 6 | ** 3 | ** 7000. | ** 3020. | ** 65 | ** | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Tomas off to on | ** |
| ** 7 | ** 3 | ** 7000. | ** 1030. | ** 65 | ** | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Tomas on to bowers off | ** |
| ** 8 | ** 3 | ** 7000. | ** 1440. | ** 65 | ** | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Bowers off to loop-on | ** |
| ** 9 | ** 3 | ** 7000. | ** 1430. | ** 65 | ** | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Bowers loop-on to dia | ** |
| ** 10 | ** 3 | ** 7000. | ** 3480. | ** 65 | ** | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Bowers di a-on to law-off | ** |
| ** 11 | ** 3 | ** 7000. | ** 1020. | ** 65 | ** | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Law off to loop-on | ** |
| ** 12 | ** 3 | ** 7000. | ** 980. | ** 65 | ** | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Lawr Loop to diag | ** |
| ** 13 | ** 3 | ** 7000. | ** 1800. | ** 65 | ** | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Lawrence On-ramp | ** |
| ** 14 | ** 3 | ** 7000. | ** 1500. | ** 65 | ** D | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Fair Oaks Off-Ramp | ** |
| ** 15 | ** 3 | ** 6000. | ** 1300. | ** 65 | ** | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Fair Oaks / Fair Oaks | ** |
| ** 16 | ** 3 | ** 6000. | ** 1000. | ** 65 | ** 0 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Fair Oaks On-Ramp | ** |
| ** 17 | ** 3 | ** 6000. | ** 1100. | ** 65 | ** | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Fair Oaks / Mathilda | ** |
| ** 18 | ** 4 | ** 7350. | ** 1000. | ** 65 | ** D | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Mathilda NB Off-Ramp | ** |
| ** 19 | ** 3 | ** 6000. | ** 900. | ** 65 | ** | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** NO | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Mathilda / Mathilda | ** |
| ** 20 | ** 3 | ** 6000. | ** 100. | ** 65 | ** 0 | ** 0.96 | ** 0.0 | ** 4 | ** 0 | ** YES | ** 0.0 | ** 0. | ** GOOD | ** 0.0 | ** Mathilda NB On-Ramp | ** |

FREeway AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT TRUCKS | DES SPECIAL RAMP | FF. SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION LOCATION |
|---------|----------|----------|-------------|--------------|---------|---------|-----------|---------|------------|------------------|-------------------|---------------|----------|----------------|----------------------|
| ** 21 | 3 | 6000. | 100. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda |
| ** 22 | 3 | 6000. | 100. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda SB Off-ramp |
| ** 23 | 3 | 6000. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / SR-237 |
| ** 24 | 3 | 6000. | 1500. | 65 | D | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 WB Off-Ramp |
| ** 25 | 3 | 6000. | 800. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 / SR-237 |
| ** 26 | 3 | 6000. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 WB On-Ramp |
| ** 27 | 3 | 6000. | 800. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 / Ellis |
| ** 28 | 3 | 6000. | 1000. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Ellis Off-ramp |
| ** 29 | 3 | 6000. | 8000. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** 30 | 4 | 8000. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy |
| ** 31 | 4 | 5500. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Dummy Bottleneck |
| ** 32 | 4 | 8000. | 2640. | 65 | D | 1.00 | 0.0 | 0 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | End of Network |

***** INPUT HAS BEEN COMPLETED *****

- MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 4 IN TIME SLICE 1
--- THE MAXIMUM METERING RATE WILL PREVAIL.
- MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 4 IN TIME SLICE 2
--- THE MAXIMUM METERING RATE WILL PREVAIL.
- MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 6 IN TIME SLICE 2
--- THE MAXIMUM METERING RATE WILL PREVAIL.
- MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 4 IN TIME SLICE 3
--- THE MAXIMUM METERING RATE WILL PREVAIL.
- MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 6 IN TIME SLICE 3
--- THE MAXIMUM METERING RATE WILL PREVAIL.

FREeway TRAVEL TIME (MINUTES)

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | |
|--------------|---------------------|-------|-------|-------|-------|-------|
| | 1 | 2 | 3 | 4 | 5 | 6 |
| * 1 * | 0.09 | 22.00 | 22.83 | 23.43 | 24.43 | 32.35 |
| * 2 * | 0.00 | 0.00 | 0.59 | 1.19 | 2.19 | 10.11 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.45 | 1.45 | 9.37 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.86 | 8.77 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.81 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.64 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB SEC | NO. LNS | SSEC LENGTH | O-D ORG | DATA DES | DEMANDS SSEC | ADJUSTED ORG | VOLUMES DES | SSEC SSEC | SSEC CAP. | WEAVE EFF | CONGEST LENGTH | STORAGE RATE | V/C RATIO | SPEED MPH | DENSITY VPMP | LOS LEVEL | FUEL MPG | EMI SS GS/VM |
|---------|---------|-------------|---------|----------|--------------|--------------|-------------|-----------|-----------|-----------|----------------|--------------|-----------|-----------|--------------|-----------|----------|--------------|
| 1 | 4 | 500. | 6552. | 852. | 6552. | 6552. | 852. | 6552. | 10000. | 0. | 0. | 0. | .66 | 65. | 25.2 | C | 19.2 | 14.0 |
| 2 | 3 | 99999. | 0. | 0. | 5700. | 0. | 0. | 5700. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 3 | 3 | 2830. | 0. | 0. | 5700. | 0. | 0. | 5700. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 4 | 3 | 930. | 0. | 0. | 5700. | 0. | 0. | 5700. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 5 | 3 | 1490. | 0. | 0. | 5700. | 0. | 0. | 5700. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 6 | 3 | 3020. | 0. | 0. | 5700. | 0. | 0. | 5700. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 7 | 3 | 1030. | 0. | 0. | 5700. | 0. | 0. | 5700. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 8 | 3 | 1440. | 0. | 0. | 5700. | 0. | 0. | 5700. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 9 | 3 | 1430. | 0. | 0. | 5700. | 0. | 0. | 5700. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 10 | 3 | 3480. | 0. | 0. | 5700. | 0. | 0. | 5700. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 11 | 3 | 1020. | 0. | 0. | 5700. | 0. | 0. | 5700. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 12 | 3 | 980. | 0. | 0. | 5700. | 0. | 0. | 5700. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 13 | 3 | 1800. | 0. | 0. | 5700. | 0. | 0. | 5700. | 7000. | 0. | 0. | 0. | .81 | 63. | 30.3 | D | 20.2 | 13.2 |
| 14 | 3 | 1500. | 0. | 557. | 5700. | 0. | 557. | 5700. | 6917. | 0. | 0. | 0. | .82 | 62. | 30.4 | D | 20.4 | 13.1 |
| 15 | 3 | 1300. | 0. | 0. | 5143. | 0. | 0. | 5143. | 6000. | 0. | 0. | 0. | .86 | 61. | 28.0 | D | 21.0 | 12.7 |
| 16 | 3 | 1000. | 468. | 0. | 5611. | 368. | 0. | 5611. | 5958. | 0. | 0. | 0. | .92 | 58. | 31.8 | D | 22.3 | 11.9 |
| 17 | 3 | 1100. | 0. | 0. | 5611. | 0. | 0. | 5611. | 6000. | 0. | 0. | 0. | .92 | 58. | 31.6 | D | 22.2 | 12.0 |
| 18 | 4 | 1000. | 0. | 1118. | 5611. | 0. | 1096. | 5611. | 7198. | 0. | 0. | 0. | .77 | 65. | 21.2 | C | 19.2 | 14.0 |
| 19 | 3 | 900. | 0. | 0. | 4493. | 0. | 0. | 4415. | 6000. | 0. | 0. | 0. | .74 | 64. | 22.9 | C | 19.4 | 13.8 |
| 20 | 3 | 100. | 224. | 0. | 4717. | 224. | 0. | 4639. | 5974. | 0. | 0. | 0. | .78 | 64. | 24.3 | C | 19.8 | 13.6 |
| 21 | 3 | 100. | 0. | 0. | 4717. | 0. | 0. | 4639. | 6000. | 0. | 0. | 0. | .77 | 64. | 24.2 | C | 19.7 | 13.6 |
| 22 | 3 | 100. | 0. | 0. | 4717. | 0. | 0. | 4639. | 6000. | 0. | 0. | 0. | .77 | 64. | 24.2 | C | 19.7 | 13.6 |
| 23 | 3 | 700. | 0. | 0. | 4717. | 0. | 0. | 4639. | 6000. | 0. | 0. | 0. | .77 | 64. | 24.2 | C | 19.7 | 13.6 |
| 24 | 3 | 1500. | 0. | 787. | 4717. | 0. | 773. | 4639. | 5899. | 0. | 0. | 0. | .79 | 63. | 24.4 | C | 19.9 | 13.5 |
| 25 | 3 | 800. | 0. | 0. | 3930. | 0. | 0. | 2996. | 6000. | 0. | 192. | 870. | .50 | 63. | 15.8 | F | 19.1 | 14.0 |
| 26 | 3 | 1000. | 1698. | 0. | 5628. | 1260. | 0. | 4256. | 5760. | 0. | ** 1000. | 870. | .74 | 48. | 29.8 | F | 21.0 | 12.8 |
| 27 | 3 | 800. | 0. | 0. | 5628. | 0. | 0. | 4256. | 6000. | 0. | ** 800. | 870. | .71 | 37. | 38.0 | F | 19.3 | 14.0 |
| 28 | 3 | 1000. | 0. | 282. | 5628. | 0. | 255. | 4256. | 5975. | 0. | ** 1000. | 870. | .71 | 30. | 46.5 | F | 18.5 | 14.7 |
| 29 | 3 | 8000. | 0. | 0. | 5346. | 0. | 0. | 4001. | 6000. | 0. | ** 8000. | 870. | .67 | 13. | 104.3 | F | 13.4 | 20.0 |
| 30 | 4 | 100. | 799. | 0. | 6145. | 799. | 0. | 4800. | 8000. | 0. | ** 100. | 870. | .60 | 7. | 183.2 | F | 9.5 | 26.8 |
| 31 | 4 | 1000. | 800. | 0. | 6945. | 700. | 0. | 5500. | 5500. | 0. | 0. | 0. | 1.00 | 65. | 21.2 | E | 19.2 | 14.0 |
| 32 | 4 | 2640. | 0. | 6945. | 6945. | 0. | 5500. | 5500. | 8000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 20.0 | 13.7 |

TOTAL 144589. = 27.4 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 53. 34.1 19.8 13.6

| | | | |
|----------------------------|--------------------|------------------|----------------------------------|
| | CURRENT TIME SLICE | | CUMULATIVE VALUES |
| FREWAY TRAVEL TIME = | 2879. VEH-HRS | 2890. PASS-HRS | 2879. VEH-HRS 2890. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 319. VEH-HRS | 326. PASS-HRS | 319. VEH-HRS 326. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 3198. VEH-HRS | 3215. PASS-HRS | 3198. VEH-HRS 3215. PASS-HRS |
| TOTAL TRAV DISTANCE = | 152333. VEH-MI. | 152954. PASS-MI. | 152333. VEH-MI. 152954. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 48. MPH | | 53. MPH |
| AVERAGE DENSITY = | 34. VPMP | | 34. VPMP |
| TOTAL FUEL = | 7824. GALLONS | | 7824. GALLONS |
| TOTAL EMISSIONS = | 2111. KI LOGRAMS | | 2111. KI LOGRAMS |

***** MAINTENANCE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|--------|------------|-------|
| 1 | 0.00 | 2 | 60.29 | 3 | 1.71 | 4 | 0.56 | 5 | 0.90 |
| 6 | 1.82 | 7 | 0.62 | 8 | 0.87 | 9 | 0.86 | 10 | 2.10 |
| 11 | 0.61 | 12 | 0.59 | 13 | 1.09 | 14 | 1.03 | 15 | 1.21 |
| 16 | 2.02 | 17 | 2.08 | 18 | 0.00 | 19 | 0.11 | 20 | 0.03 |
| 21 | 0.03 | 22 | 0.03 | 23 | 0.18 | 24 | 0.49 | 25 | 0.26 |
| 26 | 5.43 | 27 | 8.66 | 28 | 16.32 | 29 | 412.54 | 30 | 12.50 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 534.9 VEH-HRS ***** AVERAGE DELAY = 7.62 MIN/VEH *****

***** RAMP DELAYS *****

| ON-RAMP | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|---------|-----------------------|---------------|--------------------------------|----------|---------|---------|----------|----------------------|
| 2 | RAMP | 100. | 50.00 | 6.41 | 17.85 | 1.11 | 5.79 | 0.31 |
| | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 50.00 | 6.41 | 17.85 | 1.11 | 5.79 | 0.31 |

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
|----------------------------|--------------------|------------------|-------------------|------------------|
| FREEWAY TRAVEL TIME = | 3888. VEH-HRS | 3902. PASS-HRS | 6767. VEH-HRS | 6791. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 1088. VEH-HRS | 1133. PASS-HRS | 1407. VEH-HRS | 1458. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 4976. VEH-HRS | 5034. PASS-HRS | 8174. VEH-HRS | 8250. PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 152371. VEH-MI. | 152988. PASS-MI. | 304705. VEH-MI. | 305942. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 31. MPH. | | 45. MPH. | |
| AVERAGE DENSITY = | 46. VPMP | | 40. VPMP | |
| TOTAL FUEL = | 8417. GALLONS | | 16240. GALLONS | |
| TOTAL EMISSIONS = | 2297. KILOGRAMS | | 4408. KILOGRAMS | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|--------|------------|-------|
| 1 | 0.01 | 2 | 76.06 | 3 | 2.15 | 4 | 0.71 | 5 | 1.13 |
| 6 | 2.30 | 7 | 0.78 | 8 | 1.10 | 9 | 1.09 | 10 | 2.65 |
| 11 | 0.78 | 12 | 0.75 | 13 | 1.90 | 14 | 14.84 | 15 | 25.24 |
| 16 | 22.44 | 17 | 30.27 | 18 | 52.21 | 19 | 54.17 | 20 | 6.07 |
| 21 | 6.22 | 22 | 6.32 | 23 | 46.89 | 24 | 110.37 | 25 | 92.94 |
| 26 | 77.39 | 27 | 67.97 | 28 | 84.15 | 29 | 741.34 | 30 | 13.71 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 1543.9 VEH-HRS ***** AVERAGE DELAY = 24.55 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH | VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MI MINUTES | GAS GAL | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-----------|--------------|----------|---------------|-----------------------------------|---------|---------|---------|----------|----------------------|
| ON-RAMP 2 | RAMP | 100. | 100.00 | 9.58 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 100.00 | 9.58 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP 3 | RAMP | 1. | 0.50 | 0.12 | 0.18 | 0.01 | 0.06 | 0.00 | 0.07 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 1. | 0.50 | 0.12 | 0.18 | 0.01 | 0.06 | 0.00 | 0.07 |
| ON-RAMP 4 | RAMP | 845. | 641.50 | 16.41 | 229.07 | 14.21 | 74.32 | 3.94 | 92.47 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 845. | 641.50 | 16.41 | 229.07 | 14.21 | 74.32 | 3.94 | 92.47 |
| ON-RAMP 6 | RAMP | 592. | 346.00 | 13.91 | 123.55 | 7.66 | 40.08 | 2.13 | 49.87 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 592. | 346.00 | 13.91 | 123.55 | 7.66 | 40.08 | 2.13 | 49.87 |

**
** FREEWAY TRAVEL TIME (MINUTES)
**

```

*****
* ORIGINS DESTINATIONS ACROSS
* DOWN
* 1 2 3 4 5 6
+
*
+
* 1 * 0.09 26.32 32.34 38.25 44.20 57.30
+
* 2 * 0.00 0.00 4.12 10.03 15.98 29.08
+
* 3 * 0.00 0.00 0.00 4.21 10.15 23.25
+
* 4 * 0.00 0.00 0.00 0.00 3.76 16.86
+
* 5 * 0.00 0.00 0.00 0.00 0.00 0.83
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.64
*
*****

```

 *
 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *
 *
 * SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMI SS *
 * SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP EFF LENGTH RATE RATIO MPH VPMP L LEVEL MPG GS/VM *
 *
 * 1 4 500. 5770. 750. 5770. 5770. 750. 5770. 10000. 0. 0. 0. .58 65. 22.2 C 19.2 14.0 *
 * 2 3 99999. 0. 0. 5020. 0. 0. 5020. 7000. 0. 0. 0. .72 65. 25.9 C 19.3 13.9 *
 * 3 3 2830. 0. 0. 5020. 0. 0. 5020. 7000. 0. 0. 0. .72 65. 25.9 C 19.3 13.9 *
 * 4 3 930. 0. 0. 5020. 0. 0. 5020. 7000. 0. 0. 0. .72 65. 25.9 C 19.3 13.9 *
 * 5 3 1490. 0. 0. 5020. 0. 0. 5020. 7000. 0. 0. 0. .72 65. 25.9 C 19.3 13.9 *
 * 6 3 3020. 0. 0. 5020. 0. 0. 5020. 7000. 0. 0. 0. .72 65. 25.9 C 19.3 13.9 *
 * 7 3 1030. 0. 0. 5020. 0. 0. 5020. 7000. 0. 0. 0. .72 65. 25.9 C 19.3 13.9 *
 * 8 3 1440. 0. 0. 5020. 0. 0. 5020. 7000. 0. 0. 0. .72 65. 25.9 C 19.3 13.9 *
 * 9 3 1430. 0. 0. 5020. 0. 0. 5020. 7000. 0. 0. 0. .72 65. 25.9 C 19.3 13.9 *
 * 10 3 3480. 0. 0. 5020. 0. 0. 4607. 7000. 0. * 783. 413. .66 57. 27.1 F 19.0 14.1 *
 * 11 3 1020. 0. 0. 5020. 0. 0. 4607. 7000. 0. ** 1020. 413. .66 21. 73.7 F 15.6 17.2 *
 * 12 3 980. 0. 0. 5020. 0. 0. 4607. 7000. 0. ** 980. 413. .66 13. 114.2 F 13.5 19.9 *
 * 13 3 1800. 0. 0. 5020. 0. 0. 4607. 7000. 0. ** 1800. 413. .66 9. 171.7 F 11.3 23.7 *
 * 14 3 1500. 0. 661. 5020. 0. 661. 4607. 6901. 0. ** 1500. 413. .67 8. 192.0 F 10.7 25.2 *
 * 15 3 1300. 0. 0. 4359. 0. 0. 3946. 6000. 0. ** 1300. 413. .66 8. 169.5 F 10.5 25.4 *
 * 16 3 1000. 451. 0. 4810. 451. 0. 4397. 5961. 0. ** 1000. 413. .74 10. 147.6 F 13.1 22.9 *
 * 17 3 1100. 0. 0. 4810. 0. 0. 4397. 6000. 0. ** 1100. 413. .73 10. 149.9 F 12.8 23.1 *
 * 18 4 1000. 0. 952. 4810. 0. 953. 4397. 7222. 0. ** 1000. 413. .61 7. 164.5 F 9.6 26.7 *
 * 19 3 900. 0. 0. 3858. 0. 0. 3443. 6000. 0. ** 900. 413. .57 6. 191.4 F 9.1 27.5 *
 * 20 3 100. 189. 0. 4047. 190. 0. 3633. 5979. 0. ** 100. 413. .61 7. 181.9 F 9.6 26.7 *
 * 21 3 100. 0. 0. 4047. 0. 0. 3633. 6000. 0. ** 100. 413. .61 7. 183.1 F 9.5 26.8 *
 * 22 3 100. 0. 0. 4047. 0. 0. 3633. 6000. 0. ** 100. 413. .61 7. 183.1 F 9.5 26.8 *
 * 23 3 700. 0. 0. 4047. 0. 0. 3633. 6000. 0. ** 700. 413. .61 7. 183.1 F 9.5 26.8 *
 * 24 3 1500. 0. 875. 4047. 0. 875. 3633. 5889. 0. ** 1500. 413. .62 7. 176.8 F 9.7 26.5 *
 * 25 3 800. 0. 0. 3172. 0. 0. 2758. 6000. 0. ** 800. 413. .46 4. 221.2 F 8.4 28.7 *
 * 26 3 1000. 1364. 0. 4536. 1306. 0. 4064. 5806. 0. ** 1000. 413. .70 9. 153.3 F 11.6 24.2 *
 * 27 3 800. 0. 0. 4536. 0. 0. 4064. 6000. 0. ** 800. 413. .68 8. 164.3 F 11.0 24.9 *
 * 28 3 1000. 0. 205. 4536. 0. 209. 4064. 5982. 0. ** 1000. 413. .68 8. 163.3 F 11.0 24.8 *
 * 29 3 8000. 0. 0. 4331. 0. 0. 3856. 6000. 0. ** 8000. 413. .64 7. 173.4 F 10.2 25.8 *
 * 30 4 100. 647. 0. 4978. 647. 0. 4503. 8000. 0. ** 100. 413. .56 6. 194.3 F 8.9 27.7 *
 * 31 4 1000. 750. 0. 5728. 998. 0. 5500. 5500. 0. 0. 0. 1.00 65. 21.2 E 19.2 14.0 *
 * 32 4 2640. 0. 5728. 5728. 0. 5500. 5500. 8000. 0. 0. 0. .69 65. 21.2 C 20.0 13.7 *
 *
 *
 * TOTAL 144589. = 27.4 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 32. 49.9 17.4 15.4 *
 *

CURRENT TIME SLICE CUMULATIVE VALUES

| | | | | |
|----------------------------|------------------|------------------|------------------|------------------|
| FREWAY TRAVEL TIME = | 4167. VEH-HRS | 4181. PASS-HRS | 10933. VEH-HRS | 10972. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 1443. VEH-HRS | 1504. PASS-HRS | 2850. VEH-HRS | 2962. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 5610. VEH-HRS | 5685. PASS-HRS | 13783. VEH-HRS | 13934. PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 133381. VEH-MI. | 133984. PASS-MI. | 438086. VEH-MI. | 439926. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 24. MPH | | 40. MPH | |
| AVERAGE DENSITY = | 50. VPMP L | | 43. VPMP L | |
| TOTAL FUEL = | 8193. GALLONS | | 24434. GALLONS | |
| TOTAL EMISSIONS = | 2265. KI LOGRAMS | | 6673. KI LOGRAMS | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| | | | | | | | | | |
|------------|-------|------------|-------|------------|--------|------------|--------|------------|--------|
| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
| 1 | 0.00 | 2 | 8.84 | 3 | 0.25 | 4 | 0.08 | 5 | 0.13 |
| 6 | 0.27 | 7 | 0.09 | 8 | 0.13 | 9 | 0.13 | 10 | 7.45 |
| 11 | 30.84 | 12 | 52.48 | 13 | 153.33 | 14 | 143.49 | 15 | 110.26 |
| 16 | 71.08 | 17 | 79.57 | 18 | 111.85 | 19 | 88.84 | 20 | 9.28 |
| 21 | 9.35 | 22 | 9.35 | 23 | 65.42 | 24 | 134.81 | 25 | 94.14 |
| 26 | 75.26 | 27 | 65.23 | 28 | 80.95 | 29 | 698.50 | 30 | 13.41 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 2114.8 VEH-HRS ***** AVERAGE DELAY = 32.11 MIN/VEH *****

***** RAMP DELAYS *****

| | | | | | | | | | |
|---------|---|--------------|---------|----------|-------|------|-------|------|-----------|
| | | QUEUE LENGTH | DELAY | AVERAGE | GAS | HC | CO | NOX | TOTAL |
| | | VEHICLES | VEH-HRS | METERING | GALS | KGMS | KGMS | KGMS | EMISSIONS |
| | | | | DELAY | | | | | KGMS |
| | | | | MINUTES | | | | | |
| ON-RAMP | 2 | RAMP | 100. | 10.89 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 10.89 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP | 3 | RAMP | 0. | 0.01 | 0.18 | 0.01 | 0.06 | 0.00 | 0.07 |
| | | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

| | | | | US-101_NB_PM_P2_2040_PE | | | | | |
|-----------|---------|-------|--------|-------------------------|--------|--------|--------|--------|--------|
| | | TOTAL | | 0.01 | 0.18 | 0.01 | 0.06 | 0.00 | 0.07 |
| ON-RAMP 4 | TOTAL | 0. | 0.50 | | | | | | |
| | RAMP | 903. | 874.00 | 21.82 | 312.09 | 19.36 | 101.25 | 5.37 | 125.98 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 903. | 874.00 | 21.82 | 312.09 | 19.36 | 101.25 | 5.37 |
| ON-RAMP 6 | RAMP | 345. | 468.25 | 22.58 | 167.20 | 10.37 | 54.25 | 2.88 | 67.50 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 345. | 468.25 | 22.58 | 167.20 | 10.37 | 54.25 | 2.88 | 67.50 |


```

**
** 19 2 3000. 900. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Mathilda / Mathilda **
** 20 2 3000. 100. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Mathilda NB On-Ramp **
**
*****

```

FREEWAY AND ARTERIAL DESIGN FEATURES

```

**
** SUB NO. SSEC SSEC DESIG N ORG TRK SSEC PCT PCT DES SPECIAL FF. SPD. CAP. ART GRADE SUBSECTI ON LOCATI ON **
** SEC LNS CAP LENGTH SPEED DES FAC GRAD TRK TRUCKS RAMP ALT. RTE ALT. RTE TYPE ALT. RTE **
**
** 21 2 3000. 100. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Mathilda / Mathilda **
** 22 2 3000. 100. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Mathilda SB Off-ramp **
** 23 2 3000. 700. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Mathilda / SR-237 **
** 24 2 3000. 1500. 65 D 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 SR-237 WB Off-Ramp **
** 25 2 3000. 800. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 SR-237 / SR-237 **
** 26 2 3000. 1000. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 SR-237 WB On-Ramp **
** 27 2 3000. 800. 65 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 SR-237 / Ellis **
** 28 2 3000. 1000. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Ellis Off-ramp **
** 29 2 3000. 8000. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 HOV Dummy **
** 30 **
** 31 **
** 32 **
**
*****

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FREEWAY TRAVEL TIME (MINUTES)

```

* O R I G I N S D E S T I N A T I O N S A C R O S S *
* D O W N 1 2 3 4 5 6 7 *
+
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 2 * 0.00 21.14 21.91 22.51 23.14 24.54 0.00 *
+
* 3 * 0.00 0.00 0.00 0.00 0.00 3.16 0.00 *
+
* 4 * 0.00 0.00 0.00 0.00 0.00 2.47 0.00 *
+
* 5 * 0.00 0.00 0.00 0.00 0.00 1.89 0.00 *
+
* 6 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 7 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
* * *
*****

```

US-101_NB_PM_P2_2040_PL

| SUB SEC | NO. LNS | SSEC LENGTH | O-D ORG | DATA DES | DEMANDS SSEC | ADJUSTED ORG | VOLUMES DES | SSEC SSEC | WEAVE CAP. | CONGEST EFF | STORAGE LENGTH | V/C RATE | SPEED MPH | DENSITY VPMP | LOS LEVEL | FUEL MPG | EMI SS GS/VM | | |
|---------|---------|-------------|---------|----------|--------------|--------------|-------------|-----------|------------|-------------|----------------|----------|-----------|-----------------|----------------|-----------|--------------|------|------|
| * | 1 | | | | | | | | | | | | | | | | | | |
| * | 2 | 2 | 99999. | 852. | 0. | 852. | 852. | 0. | 852. | 3000. | 0. | 0. | 0. | .28 | 65. | 6.6 | A | 20.0 | 13.7 |
| * | 3 | 2 | 2830. | 0. | 0. | 852. | 0. | 0. | 852. | 3000. | 0. | 0. | 0. | .28 | 65. | 6.6 | A | 20.0 | 13.7 |
| * | 4 | 2 | 930. | 0. | 0. | 852. | 0. | 0. | 852. | 3000. | 0. | 0. | 0. | .28 | 65. | 6.6 | A | 20.0 | 13.7 |
| * | 5 | 2 | 1490. | 0. | 0. | 852. | 0. | 0. | 852. | 3000. | 0. | 0. | 0. | .28 | 65. | 6.6 | A | 20.0 | 13.7 |
| * | 6 | 2 | 3020. | 0. | 0. | 852. | 0. | 0. | 852. | 3000. | 0. | 0. | 0. | .28 | 65. | 6.6 | A | 20.0 | 13.7 |
| * | 7 | 2 | 1030. | 0. | 0. | 852. | 0. | 0. | 852. | 3000. | 0. | 0. | 0. | .28 | 65. | 6.6 | A | 20.0 | 13.7 |
| * | 8 | 2 | 1440. | 0. | 0. | 852. | 0. | 0. | 852. | 3000. | 0. | 0. | 0. | .28 | 65. | 6.6 | A | 20.0 | 13.7 |
| * | 9 | 2 | 1430. | 0. | 0. | 852. | 0. | 0. | 852. | 3000. | 0. | 0. | 0. | .28 | 65. | 6.6 | A | 20.0 | 13.7 |
| * | 10 | 2 | 3480. | 0. | 0. | 852. | 0. | 0. | 852. | 3000. | 0. | 0. | 0. | .28 | 65. | 6.6 | A | 20.0 | 13.7 |
| * | 11 | 2 | 1020. | 0. | 0. | 852. | 0. | 0. | 852. | 3000. | 0. | 0. | 0. | .28 | 65. | 6.6 | A | 20.0 | 13.7 |
| * | 12 | 2 | 980. | 0. | 0. | 852. | 0. | 0. | 852. | 3000. | 0. | 0. | 0. | .28 | 65. | 6.6 | A | 20.0 | 13.7 |
| * | 13 | 2 | 1800. | 0. | 0. | 852. | 0. | 0. | 852. | 3000. | 0. | 0. | 0. | .28 | 65. | 6.6 | A | 20.0 | 13.7 |
| * | 14 | 2 | 1500. | 0. | 83. | 852. | 0. | 83. | 852. | 3000. | 0. | 0. | 0. | .28 | 65. | 6.6 | A | 20.0 | 13.7 |
| * | 15 | 2 | 1300. | 0. | 0. | 768. | 0. | 0. | 768. | 3000. | 0. | 0. | 0. | .26 | 65. | 5.9 | A | 20.0 | 13.7 |
| * | 16 | 2 | 1000. | 42. | 0. | 811. | 42. | 0. | 811. | 3000. | 0. | 0. | 0. | .27 | 65. | 6.2 | A | 20.0 | 13.7 |
| * | 17 | 2 | 1100. | 0. | 0. | 811. | 0. | 0. | 811. | 3000. | 0. | 0. | 0. | .27 | 65. | 6.2 | A | 20.0 | 13.7 |
| * | 18 | 2 | 1000. | 0. | 152. | 811. | 0. | 152. | 811. | 3000. | 0. | 0. | 0. | .27 | 65. | 6.2 | A | 20.0 | 13.7 |
| * | 19 | 2 | 900. | 0. | 0. | 659. | 0. | 0. | 659. | 3000. | 0. | 0. | 0. | .22 | 65. | 5.1 | A | 20.0 | 13.7 |
| * | 20 | 2 | 100. | 26. | 0. | 685. | 26. | 0. | 685. | 3000. | 0. | 0. | 0. | .23 | 65. | 5.3 | A | 20.0 | 13.7 |
| * | 21 | 2 | 100. | 0. | 0. | 685. | 0. | 0. | 685. | 3000. | 0. | 0. | 0. | .23 | 65. | 5.3 | A | 20.0 | 13.7 |
| * | 22 | 2 | 100. | 0. | 0. | 685. | 0. | 0. | 685. | 3000. | 0. | 0. | 0. | .23 | 65. | 5.3 | A | 20.0 | 13.7 |
| * | 23 | 2 | 700. | 0. | 0. | 685. | 0. | 0. | 685. | 3000. | 0. | 0. | 0. | .23 | 65. | 5.3 | A | 20.0 | 13.7 |
| * | 24 | 2 | 1500. | 0. | 101. | 685. | 0. | 101. | 685. | 3000. | 0. | 0. | 0. | .23 | 65. | 5.3 | A | 20.0 | 13.7 |
| * | 25 | 2 | 800. | 0. | 0. | 583. | 0. | 0. | 583. | 3000. | 0. | 0. | 0. | .19 | 65. | 4.5 | A | 20.0 | 13.7 |
| * | 26 | 2 | 1000. | 240. | 0. | 823. | 240. | 0. | 823. | 3000. | 0. | 0. | 0. | .27 | 65. | 6.3 | A | 20.0 | 13.7 |
| * | 27 | 2 | 800. | 0. | 0. | 823. | 0. | 0. | 823. | 3000. | 0. | 0. | 0. | .27 | 65. | 6.3 | A | 20.0 | 13.7 |
| * | 28 | 2 | 1000. | 0. | 25. | 823. | 0. | 25. | 823. | 3000. | 0. | 0. | 0. | .27 | 65. | 6.3 | A | 20.0 | 13.7 |
| * | 29 | 2 | 8000. | 0. | 799. | 799. | 0. | 799. | 799. | 3000. | 0. | 0. | 0. | .27 | 65. | 6.1 | A | 20.0 | 13.7 |
| * | 30 | | | | | | | | | | | | | | | | | | |
| * | 31 | | | | | | | | | | | | | | | | | | |
| * | 32 | | | | | | | | | | | | | | | | | | |
| * | TOTAL | 140349. | = | 26.6 | MI L ES | | | | | | | | | MAX(V/C) = 0.28 | LOWEST LOS = A | AVG = 65. | 6.5 | 20.0 | 13.7 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/30/2016 16:24 PAGE 6
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE TIME SLICE 1 OF 3

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 344. VEH-HRS | 688. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 344. VEH-HRS | 688. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 22345. VEH-MI. | 44690. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 65. MPH. | 6. VPMP |
| AVERAGE DENSITY = | 6. VPMP | 1117. GALLONS |
| TOTAL FUEL = | 1117. GALLONS | 307. KILOGRAMS |
| TOTAL EMISSIONS = | 307. KILOGRAMS | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | 30 | 0.00 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PL REL 3.01 3/30/2016 16:24 PAGE 7
 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE TIME SLICE 2 OF 3

 ** FREEWAY TRAVEL TIME (MINUTES) **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN *
 * 1 2 3 4 5 6 7 *

 * * *
 * * *
 * 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
 * 2 * 0.00 21.14 21.91 22.51 23.14 24.54 0.00 *

 ** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGIN * DOWN | * DESTINATIONS ACROSS | | | | | | |
|--------------------|-----------------------|-------|-------|-------|-------|-------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 21.14 | 21.91 | 22.51 | 23.14 | 24.54 | 0.00 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.16 | 0.00 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.47 | 0.00 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.89 | 0.00 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB * SEC | * NO. * LNS | * SSEC * LENGTH | * O-D * ORG | * DATA * DES | * DEMANDS * SSEC | * ADJUSTED * ORG | * VOLUMES * DES | * SSEC * SSEC | * WEAVE * CAP | * CONGEST * EFF | * STORAGE * LENGTH | * V/C * RATE | * SPEED * RATIO | * DENSITY * MPH | * LOS * VPMP | * LEVEL | * FUEL * MPG | * EMISSIONS * GS/VM | |
|----------------|----------------|--------------------|----------------|-----------------|---------------------|---------------------|--------------------|------------------|------------------|--------------------|-----------------------|-----------------|--------------------|--------------------|-----------------|-----------|-----------------|------------------------|------|
| * 1 | | | | | | | | | | | | | | | | | | | |
| * 2 | 2 | 99999. | 750. | 0. | 750. | 750. | 0. | 750. | 3000. | 0. | 0. | 0. | .25 | 65. | 5.8 | A | 20.0 | 13.7 | |
| * 3 | 2 | 2830. | 0. | 0. | 750. | 0. | 0. | 750. | 3000. | 0. | 0. | 0. | .25 | 65. | 5.8 | A | 20.0 | 13.7 | |
| * 4 | 2 | 930. | 0. | 0. | 750. | 0. | 0. | 750. | 3000. | 0. | 0. | 0. | .25 | 65. | 5.8 | A | 20.0 | 13.7 | |
| * 5 | 2 | 1490. | 0. | 0. | 750. | 0. | 0. | 750. | 3000. | 0. | 0. | 0. | .25 | 65. | 5.8 | A | 20.0 | 13.7 | |
| * 6 | 2 | 3020. | 0. | 0. | 750. | 0. | 0. | 750. | 3000. | 0. | 0. | 0. | .25 | 65. | 5.8 | A | 20.0 | 13.7 | |
| * 7 | 2 | 1030. | 0. | 0. | 750. | 0. | 0. | 750. | 3000. | 0. | 0. | 0. | .25 | 65. | 5.8 | A | 20.0 | 13.7 | |
| * 8 | 2 | 1440. | 0. | 0. | 750. | 0. | 0. | 750. | 3000. | 0. | 0. | 0. | .25 | 65. | 5.8 | A | 20.0 | 13.7 | |
| * 9 | 2 | 1430. | 0. | 0. | 750. | 0. | 0. | 750. | 3000. | 0. | 0. | 0. | .25 | 65. | 5.8 | A | 20.0 | 13.7 | |
| * 10 | 2 | 3480. | 0. | 0. | 750. | 0. | 0. | 750. | 3000. | 0. | 0. | 0. | .25 | 65. | 5.8 | A | 20.0 | 13.7 | |
| * 11 | 2 | 1020. | 0. | 0. | 750. | 0. | 0. | 750. | 3000. | 0. | 0. | 0. | .25 | 65. | 5.8 | A | 20.0 | 13.7 | |
| * 12 | 2 | 980. | 0. | 0. | 750. | 0. | 0. | 750. | 3000. | 0. | 0. | 0. | .25 | 65. | 5.8 | A | 20.0 | 13.7 | |
| * 13 | 2 | 1800. | 0. | 0. | 750. | 0. | 0. | 750. | 3000. | 0. | 0. | 0. | .25 | 65. | 5.8 | A | 20.0 | 13.7 | |
| * 14 | 2 | 1500. | 0. | 99. | 750. | 0. | 99. | 750. | 3000. | 0. | 0. | 0. | .25 | 65. | 5.8 | A | 20.0 | 13.7 | |
| * 15 | 2 | 1300. | 0. | 0. | 651. | 0. | 0. | 651. | 3000. | 0. | 0. | 0. | .22 | 65. | 5.0 | A | 20.0 | 13.7 | |
| * 16 | 2 | 1000. | 39. | 0. | 690. | 39. | 0. | 690. | 3000. | 0. | 0. | 0. | .23 | 65. | 5.3 | A | 20.0 | 13.7 | |
| * 17 | 2 | 1100. | 0. | 0. | 690. | 0. | 0. | 690. | 3000. | 0. | 0. | 0. | .23 | 65. | 5.3 | A | 20.0 | 13.7 | |
| * 18 | 2 | 1000. | 0. | 128. | 690. | 0. | 128. | 690. | 3000. | 0. | 0. | 0. | .23 | 65. | 5.3 | A | 20.0 | 13.7 | |
| * 19 | 2 | 900. | 0. | 0. | 562. | 0. | 0. | 562. | 3000. | 0. | 0. | 0. | .19 | 65. | 4.3 | A | 20.0 | 13.7 | |
| * 20 | 2 | 100. | 21. | 0. | 583. | 21. | 0. | 583. | 3000. | 0. | 0. | 0. | .19 | 65. | 4.5 | A | 20.0 | 13.7 | |
| * 21 | 2 | 100. | 0. | 0. | 583. | 0. | 0. | 583. | 3000. | 0. | 0. | 0. | .19 | 65. | 4.5 | A | 20.0 | 13.7 | |
| * 22 | 2 | 100. | 0. | 0. | 583. | 0. | 0. | 583. | 3000. | 0. | 0. | 0. | .19 | 65. | 4.5 | A | 20.0 | 13.7 | |
| * 23 | 2 | 700. | 0. | 0. | 583. | 0. | 0. | 583. | 3000. | 0. | 0. | 0. | .19 | 65. | 4.5 | A | 20.0 | 13.7 | |
| * 24 | 2 | 1500. | 0. | 111. | 583. | 0. | 111. | 583. | 3000. | 0. | 0. | 0. | .19 | 65. | 4.5 | A | 20.0 | 13.7 | |
| * 25 | 2 | 800. | 0. | 0. | 471. | 0. | 0. | 471. | 3000. | 0. | 0. | 0. | .16 | 65. | 3.6 | A | 20.0 | 13.7 | |
| * 26 | 2 | 1000. | 194. | 0. | 665. | 194. | 0. | 665. | 3000. | 0. | 0. | 0. | .22 | 65. | 5.1 | A | 20.0 | 13.7 | |
| * 27 | 2 | 800. | 0. | 0. | 665. | 0. | 0. | 665. | 3000. | 0. | 0. | 0. | .22 | 65. | 5.1 | A | 20.0 | 13.7 | |
| * 28 | 2 | 1000. | 0. | 18. | 665. | 0. | 18. | 665. | 3000. | 0. | 0. | 0. | .22 | 65. | 5.1 | A | 20.0 | 13.7 | |
| * 29 | 2 | 8000. | 0. | 647. | 647. | 0. | 647. | 647. | 3000. | 0. | 0. | 0. | .22 | 65. | 5.0 | A | 20.0 | 13.7 | |
| * 30 | | | | | | | | | | | | | | | | | | | |
| * 31 | | | | | | | | | | | | | | | | | | | |
| * 32 | | | | | | | | | | | | | | | | | | | |
| * TOTAL | 140349. | = | 26.6 | MILES | | | | | | | | | | MAX(V/C) = 0.25 | LOWEST LOS = A | AVG = 65. | 5.7 | 20.0 | 13.7 |

FREEWAY TRAVEL TIME = CURRENT TIME SLICE 300. VEH-HRS 601. PASS-HRS CUMULATIVE VALUES 991. VEH-HRS 1982. PASS-HRS

US-101_NB_PM_P2_2040_PL

| | | | | |
|-----------------------------|-----------------|------------------|-----------------|-------------------|
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 300. VEH-HRS | 601. PASS-HRS | 991. VEH-HRS | 1982. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 19524. VEH-MI . | 39049. PASS-MI . | 64412. VEH-MI . | 128824. PASS-MI . |
| AVERAGE SYSTEM SPEED = | 65. MPH. | | 65. MPH. | |
| AVERAGE DENSITY = | 6. VPMPPL | | 6. VPMPPL | |
| TOTAL FUEL = | 976. GALLONS | | 3221. GALLONS | |
| TOTAL EMISSIONS = | 268. KILOGRAMS | | 885. KILOGRAMS | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | 30 | 0.00 |
| 31 | 0.00 | 32 | 0.00 | | | | | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

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FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQQ QQQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP EEEEEEEEE
    
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FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREEWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT TRUCKS | DES TRUCKS | SPECIAL RAMP | FF. SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION LOCATION |
|---------|----------|----------|-------------|--------------|---------|---------|-----------|---------|------------|------------|--------------|-------------------|---------------|----------|----------------|-------------------------|
| ** 1 | 5 | 10000. | 1370. | 65 | OD | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Seeding |
| ** 2 | 3 | 6226. | 99999. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Queue Capture |
| ** 3 | 3 | 6000. | 2740. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | SR-85 Off to Shore On |
| ** 4 | 3 | 6000. | 600. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Shore. On to Moffet Off |
| ** 5 | 3 | 6000. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Moffett Off to On |
| ** 6 | 3 | 6000. | 2630. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Moffett On to Ellis Off |
| ** 7 | 3 | 6000. | 2530. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Ellis Off to On-ramp |
| ** 8 | 4 | 6430. | 1500. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Ellis On-ramp |
| ** 9 | 4 | 6430. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Ellis / US 237 |
| ** 10 | 4 | 6430. | 1500. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | SR-237 EB Off-Ramp |
| ** 11 | 3 | 6000. | 750. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | SR-237 / SR-237 |
| ** 12 | 4 | 6610. | 350. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | SR-237 EB On-Ramp |
| ** 13 | 4 | 6610. | 350. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | US 237 / Mathilda |
| ** 14 | 4 | 6610. | 350. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Mathilda Off-Ramp |
| ** 15 | 3 | 6000. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Mathilda / Mathilda |
| ** 16 | 3 | 6000. | 900. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Mathilda SB On-Ramp |
| ** 17 | 3 | 6000. | 1400. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Mathilda NB On-Ramp |
| ** 18 | 3 | 6000. | 200. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Mathilda / Fair Oaks |
| ** 19 | 3 | 6000. | 1400. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Fair Oaks SB Off-Ramp |
| ** 20 | 3 | 6000. | 900. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Fair Oaks SB/ Fair Oaks |

FREeway AND ARTERIAL DESIGN FEATURES

| SUB NO. | SEC | LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC PCT GRAD | PCT TRK | DES TRUCKS | SPECIAL RAMP | FF.SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION | LOCATION |
|---------|-----|-----|----------|-------------|--------------|---------|---------|---------------|---------|------------|--------------|------------------|---------------|----------|----------------|------------------|-----------|
| ** 21 | 4 | | 6150. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Fair Oaks SB | On-Ramp |
| ** 22 | 4 | | 6150. | 100. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks NB | Off-Ramp |
| ** 23 | 3 | | 6000. | 600. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks NB/ | Fair Oaks |
| ** 24 | 3 | | 6000. | 1500. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Oaks On-Ramp | to Mid |
| ** 25 | 3 | | 6000. | 1500. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mid to Lawrence | Off-ramp |
| ** 26 | 3 | | 6000. | 8000. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | |
| ** 27 | 5 | | 10000. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | |
| ** 28 | 5 | | 7750. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Dummy Bottleneck | |
| ** 29 | 5 | | 9685. | 1000. | 65 | OD | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | End of Network | |

***** INPUT HAS BEEN COMPLETED *****

MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 3 IN TIME SLICE 1
--- THE MAXIMUM METERING RATE WILL PREVAIL.

MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 3 IN TIME SLICE 2
--- THE MAXIMUM METERING RATE WILL PREVAIL.

FREeway TRAVEL TIME (MINUTES)

| ORIGINS DOWN | DESTINATIONS ACROSS | 1 | 2 | 3 | 4 | 5 | 6 |
|--------------|---------------------|------|-------|-------|-------|-------|-------|
| * 1 * | | 0.24 | 20.98 | 21.29 | 22.10 | 22.29 | 24.75 |
| * 2 * | | 0.00 | 0.65 | 0.96 | 1.77 | 1.96 | 4.42 |
| * 3 * | | 0.00 | 0.00 | 0.18 | 0.99 | 1.19 | 3.64 |
| * 4 * | | 0.00 | 0.00 | 0.00 | 0.69 | 0.88 | 3.33 |
| * 5 * | | 0.00 | 0.00 | 0.00 | 0.53 | 0.72 | 3.18 |
| * 6 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.03 | 2.49 |
| * 7 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.35 |
| * 8 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.37 |
| * 9 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.35 |
| * 10 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 |

 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *

| * SUB SEC | * NO. LNS | * SSEC LENGTH | * O-D ORG | * DATA DES | * DEMANDS SSEC | * ADJUSTED ORG | * DES | * VOLUMES SSEC | * SSEC CAP. | * WEAVE EFF | * CONGEST LENGTH | * STORAGE RATE | * V/C RATIO | * SPEED MPH | * DENSITY VPMP | * LOS LEVEL | * FUEL MPG | * EMISSIONS GS/VM |
|-----------|-----------|---------------|-----------|------------|----------------|----------------|-------|----------------|-------------|-------------|------------------|----------------|-------------|-------------|----------------|-------------|------------|-------------------|
| * 1 | 5 | 1370. | 6299. | 1071. | 6299. | 6299. | 1071. | 6299. | 10000. | 0. | 0. | 0. | .63 | 65. | 19.4 | C | 19.2 | 14.0 |
| * 2 | 3 | 99999. | 0. | 0. | 5228. | 0. | 0. | 5228. | 6226. | 0. | 0. | 0. | .84 | 62. | 28.2 | D | 20.6 | 13.0 |
| * 3 | 3 | 2740. | 0. | 0. | 5228. | 0. | 0. | 5228. | 6000. | 0. | 0. | 0. | .87 | 61. | 28.8 | D | 21.3 | 12.5 |
| * 4 | 3 | 600. | 0. | 0. | 5228. | 0. | 0. | 5228. | 6000. | 0. | 0. | 0. | .87 | 61. | 28.8 | D | 21.3 | 12.5 |
| * 5 | 3 | 700. | 0. | 0. | 5228. | 0. | 0. | 5228. | 6000. | 0. | 0. | 0. | .87 | 61. | 28.8 | D | 21.3 | 12.5 |
| * 6 | 3 | 2630. | 0. | 0. | 5228. | 0. | 0. | 5228. | 6000. | 0. | 0. | 0. | .87 | 61. | 28.8 | D | 21.3 | 12.5 |
| * 7 | 3 | 2530. | 0. | 0. | 5228. | 0. | 0. | 5228. | 6000. | 0. | 0. | 0. | .87 | 61. | 28.8 | D | 21.3 | 12.5 |
| * 8 | 4 | 1500. | 298. | 0. | 5526. | 298. | 0. | 5526. | 6398. | 0. | 0. | 0. | .86 | 65. | 21.3 | C | 19.2 | 14.0 |
| * 9 | 4 | 700. | 0. | 0. | 5526. | 0. | 0. | 5526. | 6430. | 0. | 0. | 0. | .86 | 65. | 21.3 | C | 19.2 | 14.0 |
| * 10 | 4 | 1500. | 0. | 1903. | 5526. | 0. | 1903. | 5526. | 6063. | 0. | 0. | 0. | .91 | 65. | 21.3 | C | 19.2 | 14.0 |
| * 11 | 3 | 750. | 0. | 0. | 3623. | 0. | 0. | 3623. | 6000. | 0. | 0. | 0. | .60 | 65. | 18.6 | C | 19.2 | 14.0 |
| * 12 | 4 | 350. | 957. | 0. | 4580. | 900. | 0. | 4523. | 6448. | 0. | 0. | 0. | .70 | 65. | 17.4 | B | 19.2 | 14.0 |
| * 13 | 4 | 350. | 0. | 0. | 4580. | 0. | 0. | 4523. | 6610. | 0. | 0. | 0. | .68 | 65. | 17.4 | B | 19.2 | 14.0 |
| * 14 | 4 | 350. | 0. | 392. | 4580. | 0. | 387. | 4523. | 6552. | 0. | 0. | 0. | .69 | 65. | 17.4 | B | 19.2 | 14.0 |
| * 15 | 3 | 700. | 0. | 0. | 4188. | 0. | 0. | 4136. | 6000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 19.2 | 14.0 |
| * 16 | 3 | 900. | 93. | 0. | 4281. | 93. | 0. | 4229. | 5983. | 0. | 0. | 0. | .71 | 65. | 21.7 | C | 19.2 | 14.0 |
| * 17 | 3 | 1400. | 202. | 0. | 4483. | 202. | 0. | 4431. | 5962. | 0. | 0. | 0. | .74 | 64. | 23.0 | C | 19.5 | 13.8 |
| * 18 | 3 | 200. | 0. | 0. | 4483. | 0. | 0. | 4431. | 6000. | 0. | 0. | 0. | .74 | 64. | 23.0 | C | 19.5 | 13.8 |
| * 19 | 3 | 1400. | 0. | 268. | 4483. | 0. | 265. | 4431. | 5963. | 0. | 0. | 0. | .74 | 64. | 23.0 | C | 19.5 | 13.8 |
| * 20 | 3 | 900. | 0. | 0. | 4215. | 0. | 0. | 4167. | 6000. | 0. | 0. | 0. | .69 | 65. | 21.4 | C | 19.2 | 14.0 |
| * 21 | 4 | 100. | 208. | 0. | 4423. | 208. | 0. | 4375. | 6108. | 0. | 0. | 0. | .72 | 65. | 16.8 | B | 19.2 | 14.0 |
| * 22 | 4 | 100. | 0. | 82. | 4423. | 0. | 81. | 4375. | 6139. | 0. | 0. | 0. | .71 | 65. | 16.8 | B | 19.2 | 14.0 |
| * 23 | 3 | 600. | 0. | 0. | 4341. | 0. | 0. | 4294. | 6000. | 0. | 0. | 0. | .72 | 65. | 22.0 | C | 19.2 | 14.0 |
| * 24 | 3 | 1500. | 506. | 0. | 4847. | 506. | 0. | 4800. | 5896. | 0. | 0. | 0. | .81 | 63. | 25.5 | C | 20.2 | 13.2 |
| * 25 | 3 | 1500. | 0. | 0. | 4847. | 0. | 0. | 4800. | 6000. | 0. | 0. | 0. | .80 | 63. | 25.3 | C | 20.0 | 13.4 |
| * 26 | 3 | 8000. | 0. | 0. | 4847. | 0. | 0. | 4800. | 6000. | 0. | 0. | 0. | .80 | 63. | 25.3 | C | 20.0 | 13.4 |
| * 27 | 5 | 100. | 993. | 0. | 5840. | 993. | 0. | 5793. | 10000. | 0. | 0. | 0. | .58 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 28 | 5 | 1000. | 0. | 0. | 5840. | 0. | 0. | 5793. | 7750. | 0. | 0. | 0. | .75 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 29 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 30 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 31 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 32 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 33 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 34 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 35 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 36 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 37 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 38 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 39 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 40 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 41 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 42 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 43 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 44 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 45 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 46 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 47 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 48 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 49 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 50 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 51 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 52 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 53 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 54 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 55 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 56 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 57 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 58 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 59 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 60 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 61 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 62 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 63 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 64 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 65 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 66 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 67 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 68 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 69 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 70 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 71 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 72 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 73 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 74 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 75 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 76 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 77 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 78 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 79 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 80 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 81 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | 19.2 | 14.0 |
| * 82 | 5 | 1000. | 0. | 5840. | 5840. | 0. | 5793. | 5793. | 9685. | 0. | 0. | 0. | .60 | 65. | 17.8 | B | | |

US-101_SB_AM_NP_2040_PE

| ORIGINS | | DESTINATIONS ACROSS | | | | | |
|---------|---|---------------------|-------|-------|-------|-------|-------|
| DOWN | | 1 | 2 | 3 | 4 | 5 | 6 |
| 1 | * | 0.24 | 27.75 | 28.06 | 28.89 | 29.08 | 31.65 |
| 2 | * | 0.00 | 1.52 | 1.83 | 2.66 | 2.85 | 5.42 |
| 3 | * | 0.00 | 0.00 | 0.18 | 1.01 | 1.20 | 3.77 |
| 4 | * | 0.00 | 0.00 | 0.00 | 0.70 | 0.89 | 3.47 |
| 5 | * | 0.00 | 0.00 | 0.00 | 0.54 | 0.74 | 3.31 |
| 6 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.03 | 2.61 |
| 7 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.46 |
| 8 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.37 |
| 9 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.35 |
| 10 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB SEC | NO. LNS | SSEC LENGTH | O-D ORG | DATA DES | DEMANDS SSEC | ADJUSTED ORG | VOLUMES DES | SSEC SSEC | WEAVE CAP | CONGEST EFF | STORAGE LENGTH | V/C RATE | SPEED RATIO | DENSITY MPH | LOS VPMP | FUEL LEVEL | EMI SS MPG | |
|---------|---------|-------------|---------|-------------|--------------|-----------------|-------------|----------------|-----------|-------------|----------------|----------|-------------|-------------|----------|------------|------------|------|
| 1 | 5 | 1370. | 7501. | 1275. | 7501. | 7501. | 1275. | 7501. | 10000. | 0. | 0. | 0. | .75 | 64. | 23.4 | C | 19.5 | 13.7 |
| 2 | 3 | 99999. | 0. | 0. | 6226. | 0. | 0. | 6000. | 6226. | 0. | * 7488. | 226. | .96 | 50. | 40.3 | F | 23.6 | 11.3 |
| 3 | 3 | 2740. | 0. | 0. | 6226. | 0. | 0. | 5653. | 6000. | 0. | * 1833. | 347. | .94 | 48. | 39.3 | F | 23.4 | 11.4 |
| 4 | 3 | 600. | 0. | 0. | 6226. | 0. | 0. | 5653. | 6000. | 0. | ** 600. | 347. | .94 | 40. | 47.2 | F | 22.5 | 12.1 |
| 5 | 3 | 700. | 0. | 0. | 6226. | 0. | 0. | 5653. | 6000. | 0. | ** 700. | 347. | .94 | 37. | 50.7 | F | 22.2 | 12.4 |
| 6 | 3 | 2630. | 0. | 0. | 6226. | 0. | 0. | 5653. | 6000. | 0. | ** 2630. | 347. | .94 | 32. | 59.7 | F | 21.3 | 13.1 |
| 7 | 3 | 2530. | 0. | 0. | 6226. | 0. | 0. | 5653. | 6000. | 0. | ** 2530. | 347. | .94 | 26. | 73.9 | F | 20.0 | 14.4 |
| 8 | 4 | 1500. | 388. | 0. | 6614. | 338. | 0. | 5991. | 6388. | 0. | ** 1500. | 347. | .94 | 22. | 69.1 | F | 18.9 | 15.5 |
| 9 | 4 | 700. | 0. | 0. | 6614. | 0. | 0. | 5991. | 6430. | 0. | ** 700. | 347. | .93 | 20. | 76.6 | F | 18.2 | 16.4 |
| 10 | 4 | 1500. | 0. | 2291. | 6614. | 0. | 2074. | 5991. | 5991. | 0. | 0. | 0. | 1.00 | 52. | 28.7 | E | 23.8 | 11.1 |
| 11 | 3 | 750. | 0. | 0. | 4323. | 0. | 0. | 3917. | 6000. | 0. | 0. | 0. | .65 | 65. | 20.1 | C | 19.2 | 14.0 |
| 12 | 4 | 350. | 1340. | 0. | 5663. | 900. | 0. | 4817. | 6380. | 0. | 0. | 0. | .76 | 65. | 18.5 | C | 19.2 | 14.0 |
| 13 | 4 | 350. | 0. | 0. | 5663. | 0. | 0. | 4817. | 6610. | 0. | 0. | 0. | .73 | 65. | 18.5 | C | 19.2 | 14.0 |
| 14 | 4 | 350. | 0. | 534. | 5663. | 0. | 450. | 4817. | 6535. | 0. | 0. | 0. | .74 | 65. | 18.5 | C | 19.2 | 14.0 |
| 15 | 3 | 700. | 0. | 0. | 5129. | 0. | 0. | 4367. | 6000. | 0. | 0. | 0. | .73 | 64. | 22.6 | C | 19.4 | 13.8 |
| 16 | 3 | 900. | 130. | 0. | 5259. | 130. | 0. | 4497. | 5975. | 0. | 0. | 0. | .75 | 64. | 23.4 | C | 19.6 | 13.7 |
| 17 | 3 | 1400. | 275. | 0. | 5534. | 275. | 0. | 4772. | 5947. | 0. | 0. | 0. | .80 | 63. | 25.2 | C | 20.1 | 13.3 |
| 18 | 3 | 200. | 0. | 0. | 5534. | 0. | 0. | 4772. | 6000. | 0. | 0. | 0. | .80 | 63. | 25.1 | C | 20.0 | 13.4 |
| 19 | 3 | 1400. | 0. | 202. | 5534. | 0. | 174. | 4772. | 5974. | 0. | 0. | 0. | .80 | 63. | 25.2 | C | 20.0 | 13.4 |
| 20 | 3 | 900. | 0. | 0. | 5332. | 0. | 0. | 4598. | 6000. | 0. | 0. | 0. | .77 | 64. | 24.0 | C | 19.7 | 13.6 |
| 21 | 4 | 100. | 283. | 0. | 5615. | 283. | 0. | 4881. | 6093. | 0. | 0. | 0. | .80 | 65. | 18.8 | C | 19.2 | 14.0 |
| 22 | 4 | 100. | 0. | 126. | 5615. | 0. | 109. | 4881. | 6134. | 0. | 0. | 0. | .80 | 65. | 18.8 | C | 19.2 | 14.0 |
| 23 | 3 | 600. | 0. | 0. | 5489. | 0. | 0. | 4772. | 6000. | 0. | 0. | 0. | .80 | 63. | 25.2 | C | 20.0 | 13.4 |
| 24 | 3 | 1500. | 564. | 0. | 6053. | 564. | 0. | 5336. | 5884. | 0. | 0. | 0. | .91 | 59. | 30.2 | D | 22.0 | 12.1 |
| 25 | 3 | 1500. | 0. | 0. | 6053. | 0. | 0. | 5336. | 6000. | 0. | 0. | 0. | .89 | 60. | 29.8 | D | 21.7 | 12.3 |
| 26 | 3 | 8000. | 0. | 0. | 6053. | 0. | 0. | 5336. | 6000. | 0. | 0. | 0. | .89 | 60. | 29.8 | D | 21.7 | 12.3 |
| 27 | 5 | 100. | 1240. | 0. | 7293. | 1240. | 0. | 6576. | 10000. | 0. | 0. | 0. | .66 | 65. | 20.2 | C | 19.2 | 14.0 |
| 28 | 5 | 1000. | 0. | 0. | 7293. | 0. | 0. | 6576. | 7750. | 0. | 0. | 0. | .85 | 65. | 20.2 | C | 19.2 | 14.0 |
| 29 | 5 | 1000. | 0. | 7293. | 7293. | 0. | 6576. | 6576. | 9685. | 0. | 0. | 0. | .68 | 65. | 20.2 | C | 19.2 | 14.0 |
| TOTAL | | 135469. | = | 25.7 MI LES | | MAX(V/C) = 1.00 | | LOWEST LOS = F | | AVG = 49. | | 39.4 | | 22.9 | | 11.7 | | |

| | CURRENT TIME SLICE | | | CUMULATIVE VALUES | | | | |
|----------------------------|--------------------|------------|---------|-------------------|---------|------------|---------|----------|
| FREWAY TRAVEL TIME = | 3195. | VEH-HRS | 3208. | PASS-HRS | 5326. | VEH-HRS | 5350. | PASS-HRS |
| FREWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 302. | VEH-HRS | 302. | PASS-HRS | 331. | VEH-HRS | 331. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 3497. | VEH-HRS | 3510. | PASS-HRS | 5656. | VEH-HRS | 5680. | PASS-HRS |
| TOTAL TRAV DISTANCE = | 154975. | VEH-MI. | 155793. | PASS-MI. | 287475. | VEH-MI. | 289001. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 44. | MPH | | | 54. | MPH | | |
| AVERAGE DENSITY = | 39. | VPMP | | | 33. | VPMP | | |
| TOTAL FUEL = | 6890. | GALLONS | | | 13373. | GALLONS | | |
| TOTAL EMISSIONS = | 1859. | KI LOGRAMS | | | 3594. | KI LOGRAMS | | |

US-101_SB_AM_NP_2040_PE

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|--------|------------|-------|------------|-------|------------|-------|
| 1 | 0.38 | 2 | 559.34 | 3 | 16.92 | 4 | 6.53 | 5 | 9.03 |
| 6 | 47.49 | 7 | 65.90 | 8 | 52.84 | 9 | 28.49 | 10 | 6.41 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.07 |
| 16 | 0.16 | 17 | 0.60 | 18 | 0.08 | 19 | 0.57 | 20 | 0.21 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.23 | 24 | 2.46 | 25 | 2.06 |
| 26 | 10.96 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 810.7 VEH-HRS ***** AVERAGE DELAY = 8.22 MIN/VEH *****

***** RAMP DELAYS *****

| | | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|---------|---|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|
| ON-RAMP | 2 | RAMP | 50. | 25.00 | 3.87 | 8.93 | 0.55 | 2.90 | 3.60 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 50. | 25.00 | 3.87 | 8.93 | 0.55 | 2.90 | 3.60 |
| ON-RAMP | 3 | RAMP | 497. | 277.00 | 11.90 | 98.91 | 6.14 | 32.09 | 39.93 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 497. | 277.00 | 11.90 | 98.91 | 6.14 | 32.09 | 39.93 |

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FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQQ QQQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 PPP PPP LLL
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP LLL
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 2222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQ QQQQ 1111 2222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 1111111 222222222 PPP LLLLLLLLLL
    
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FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 2 AND 26 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 2.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

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*****
**
**
**          FREEWAY AND ARTERIAL DESIGN FEATURES          **
**
*****
**
** SUB NO.   SSEC   SSEC   DESIG N   ORG   TRK   SSEC PCT   PCT DES   SPECIAL   FF. SPD.   CAP.   ART   GRADE   SUBSECTI ON LOCATI ON
** SEC  LNS   CAP   LENGTH SPEED   DES   FAC   GRAD TRK   TRUCKS   RAMP     ALT. RTE   ALT. RTE   TYPE ALT. RTE
**
** 1
** 2  2  3000.  99999.  65    0  0.96  0.0 0   100   NO    0.0   0.   GOOD  0.0  Queue Capture
** 3  2  3000.   2740.  65    0  0.96  0.0 0   100   NO    0.0   0.   GOOD  0.0  SR-85 Off to Shore On
** 4  2  3000.   600.   65    0  0.96  0.0 0   100   NO    0.0   0.   GOOD  0.0  Shore. On to Moffet Off
** 5  2  3000.   700.   65    0  0.96  0.0 0   100   NO    0.0   0.   GOOD  0.0  Moffett Off to On
** 6  2  3000.  2630.  65    0  0.96  0.0 0   100   NO    0.0   0.   GOOD  0.0  Moffett On to Ellis Off
** 7  2  3000.  2530.  65    0  0.96  0.0 0   100   NO    0.0   0.   GOOD  0.0  Ellis Off to On-ramp
** 8  2  3000.  1500.  65    0  0.96  0.0 0   100   YES   0.0   0.   GOOD  0.0  Ellis On-ramp
** 9  2  3000.   700.   65    0  0.96  0.0 0   100   YES   0.0   0.   GOOD  0.0  Ellis / US 237
** 10 2  3000.  1500.  65    D  0.96  0.0 0   100   NO    0.0   0.   GOOD  0.0  SR-237 EB Off-Ramp
** 11 2  3000.   750.   65    0  0.96  0.0 0   100   NO    0.0   0.   GOOD  0.0  SR-237 / SR-237
** 12 2  3000.   350.   65    0  0.96  0.0 0   100   YES   0.0   0.   GOOD  0.0  SR-237 EB On-Ramp
** 13 2  3000.   350.   65    0  0.96  0.0 0   100   YES   0.0   0.   GOOD  0.0  US 237 / Mathilda
** 14 2  3000.   350.   65    D  0.96  0.0 0   100   NO    0.0   0.   GOOD  0.0  Mathilda Off-Ramp
** 15 2  3000.   700.   65    0  0.96  0.0 0   100   NO    0.0   0.   GOOD  0.0  Mathilda / Mathilda
** 16 2  3000.   900.   65    0  0.96  0.0 0   100   YES   0.0   0.   GOOD  0.0  Mathilda SB On-Ramp
** 17 2  3000.  1400.  65    0  0.96  0.0 0   100   YES   0.0   0.   GOOD  0.0  Mathilda NB On-Ramp
** 18 2  3000.   200.   65    0  0.96  0.0 0   100   NO    0.0   0.   GOOD  0.0  Mathilda / Fair Oaks
**
    
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US-101_SB_AM_NP_2040_PL

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**
** 19 2 3000. 1400. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks SB Off-Ramp **
**
** 20 2 3000. 900. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks SB/ Fair Oaks **
**
*****

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FREEWAY AND ARTERIAL DESIGN FEATURES

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*****
**
**
**
**
**
** SUB NO. SSEC SSEC DESIG N ORG TRK SSEC PCT PCT DES SPECIAL FF.SPD. CAP. ART GRADE SUBSECTI ON LOCATI ON **
** SEC LNS CAP LENGTH SPEED DES FAC GRAD TRK TRUCKS RAMP ALT. RTE ALT. RTE TYPE ALT. RTE **
**
** 21 2 3000. 100. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Fair Oaks SB On-Ramp **
**
** 22 2 3000. 100. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks NB Off-Ramp **
**
** 23 2 3000. 600. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks NB/ Fair Oaks **
**
** 24 2 3000. 1500. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Oaks On-Ramp to Mid **
**
** 25 2 3000. 1500. 65 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Mid to Lawrence Off-ramp **
**
** 26 2 3000. 8000. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 HOV Dummy **
**
** 27 **
** 28 **
** 29 **
**
*****

```

FREEWAY TRAVEL TIME (MINUTES)

```

*****
* O R I G I N S D E S T I N A T I O N S A C R O S S
* D O W N
* 1 2 3 4 5 6 7
+
*
*
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 2 * 0.00 19.74 20.05 20.86 21.05 23.08 0.00
+
* 3 * 0.00 0.00 0.00 0.00 1.96 3.99 0.00
+
* 4 * 0.00 0.00 0.00 0.00 0.00 3.21 0.00
+
* 5 * 0.00 0.00 0.00 0.00 0.00 2.90 0.00
+
* 6 * 0.00 0.00 0.00 0.00 0.00 2.74 0.00
+
* 7 * 0.00 0.00 0.00 0.00 0.00 2.06 0.00
+
* 8 * 0.00 0.00 0.00 0.00 0.00 1.92 0.00
+
* 9 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 10 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 11 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
*
*****

```

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB SEC | NO. LNS | SSEC LENGTH | O-D ORG | DATA DES | DEMANDS SSEC | ADJUSTED ORG | VOLUMES DES | SSEC SSEC | SSEC CAP. | WEAVE EFF | CONGEST LENGTH | STORAGE RATE | V/C RATIO | SPEED MPH | DENSITY VPMP | LOS LEVEL | FUEL MPG | EMI SS GS/VM |
|---------|---------|-------------|---------|----------|--------------|--------------|-------------|-----------|-----------|-----------------|----------------|--------------|-----------|-----------|--------------|-----------|----------|--------------|
| 1 | | | | | | | | | | | | | | | | | | |
| 2 | 2 | 99999 | 1071 | 0 | 1071 | 1071 | 0 | 1071 | 3000 | 0 | 0 | 0 | .36 | 65 | 8.2 | A | 20.0 | 13.7 |
| 3 | 2 | 2740 | 0 | 0 | 1071 | 0 | 0 | 1071 | 3000 | 0 | 0 | 0 | .36 | 65 | 8.2 | A | 20.0 | 13.7 |
| 4 | 2 | 600 | 0 | 0 | 1071 | 0 | 0 | 1071 | 3000 | 0 | 0 | 0 | .36 | 65 | 8.2 | A | 20.0 | 13.7 |
| 5 | 2 | 700 | 0 | 0 | 1071 | 0 | 0 | 1071 | 3000 | 0 | 0 | 0 | .36 | 65 | 8.2 | A | 20.0 | 13.7 |
| 6 | 2 | 2630 | 0 | 0 | 1071 | 0 | 0 | 1071 | 3000 | 0 | 0 | 0 | .36 | 65 | 8.2 | A | 20.0 | 13.7 |
| 7 | 2 | 2530 | 0 | 0 | 1071 | 0 | 0 | 1071 | 3000 | 0 | 0 | 0 | .36 | 65 | 8.2 | A | 20.0 | 13.7 |
| 8 | 2 | 1500 | 32 | 0 | 1103 | 32 | 0 | 1103 | 3000 | 0 | 0 | 0 | .37 | 65 | 8.5 | A | 20.0 | 13.7 |
| 9 | 2 | 700 | 0 | 0 | 1103 | 0 | 0 | 1103 | 3000 | 0 | 0 | 0 | .37 | 65 | 8.5 | A | 20.0 | 13.7 |
| 10 | 2 | 1500 | 0 | 367 | 1103 | 0 | 367 | 1103 | 3000 | 0 | 0 | 0 | .37 | 65 | 8.5 | A | 20.0 | 13.7 |
| 11 | 2 | 750 | 0 | 0 | 736 | 0 | 0 | 736 | 3000 | 0 | 0 | 0 | .25 | 65 | 5.7 | A | 20.0 | 13.7 |
| 12 | 2 | 350 | 162 | 0 | 898 | 162 | 0 | 898 | 3000 | 0 | 0 | 0 | .30 | 65 | 6.9 | A | 20.0 | 13.7 |
| 13 | 2 | 350 | 0 | 0 | 898 | 0 | 0 | 898 | 3000 | 0 | 0 | 0 | .30 | 65 | 6.9 | A | 20.0 | 13.7 |
| 14 | 2 | 350 | 0 | 58 | 898 | 0 | 58 | 898 | 3000 | 0 | 0 | 0 | .30 | 65 | 6.9 | A | 20.0 | 13.7 |
| 15 | 2 | 700 | 0 | 0 | 840 | 0 | 0 | 840 | 3000 | 0 | 0 | 0 | .28 | 65 | 6.5 | A | 20.0 | 13.7 |
| 16 | 2 | 900 | 17 | 0 | 858 | 17 | 0 | 858 | 3000 | 0 | 0 | 0 | .29 | 65 | 6.6 | A | 20.0 | 13.7 |
| 17 | 2 | 1400 | 38 | 0 | 895 | 38 | 0 | 895 | 3000 | 0 | 0 | 0 | .30 | 65 | 6.9 | A | 20.0 | 13.7 |
| 18 | 2 | 200 | 0 | 0 | 895 | 0 | 0 | 895 | 3000 | 0 | 0 | 0 | .30 | 65 | 6.9 | A | 20.0 | 13.7 |
| 19 | 2 | 1400 | 0 | 37 | 895 | 0 | 37 | 895 | 3000 | 0 | 0 | 0 | .30 | 65 | 6.9 | A | 20.0 | 13.7 |
| 20 | 2 | 900 | 0 | 0 | 859 | 0 | 0 | 859 | 3000 | 0 | 0 | 0 | .29 | 65 | 6.6 | A | 20.0 | 13.7 |
| 21 | 2 | 100 | 42 | 0 | 900 | 42 | 0 | 900 | 3000 | 0 | 0 | 0 | .30 | 65 | 6.9 | A | 20.0 | 13.7 |
| 22 | 2 | 100 | 0 | 11 | 900 | 0 | 11 | 900 | 3000 | 0 | 0 | 0 | .30 | 65 | 6.9 | A | 20.0 | 13.7 |
| 23 | 2 | 600 | 0 | 0 | 889 | 0 | 0 | 889 | 3000 | 0 | 0 | 0 | .30 | 65 | 6.8 | A | 20.0 | 13.7 |
| 24 | 2 | 1500 | 104 | 0 | 993 | 104 | 0 | 993 | 3000 | 0 | 0 | 0 | .33 | 65 | 7.6 | A | 20.0 | 13.7 |
| 25 | 2 | 1500 | 0 | 0 | 993 | 0 | 0 | 993 | 3000 | 0 | 0 | 0 | .33 | 65 | 7.6 | A | 20.0 | 13.7 |
| 26 | 2 | 8000 | 0 | 993 | 993 | 0 | 993 | 993 | 3000 | 0 | 0 | 0 | .33 | 65 | 7.6 | A | 20.0 | 13.7 |
| 27 | | | | | | | | | | | | | | | | | | |
| 28 | | | | | | | | | | | | | | | | | | |
| 29 | | | | | | | | | | | | | | | | | | |
| TOTAL | 131999 | = | 25.0 | MILES | | | | | | MAX(V/C) = 0.37 | LOWEST LOS = A | AVG = 65. | 8.1 | 20.0 | 13.7 | | | |

| | | | | | |
|-----------------------------|----------------|-----------------|-------------------|-----------------|---------------|
| FREEWAY TRAVEL TIME = | 405. VEH-HRS | 810. PASS-HRS | CUMULATIVE VALUES | 405. VEH-HRS | 810. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | |
| TOTAL SYSTEM TRAVEL TIME = | 405. VEH-HRS | 810. PASS-HRS | 405. VEH-HRS | 810. PASS-HRS | |
| TOTAL FRWAY TRAV DISTANCE = | 26322. VEH-MI. | 52645. PASS-MI. | 26322. VEH-MI. | 52645. PASS-MI. | |
| AVERAGE SYSTEM SPEED = | 65. MPH. | | 65. MPH. | | |
| AVERAGE DENSITY = | 8. VPMP | | 8. VPMP | | |
| TOTAL FUEL = | 1316. GALLONS | | 1316. GALLONS | | |
| TOTAL EMISSIONS = | 362. KILOGRAMS | | 362. KILOGRAMS | | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

** FREEWAY TRAVEL TIME (MINUTES) **

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | |
|--------------|---------------------|-------|-------|-------|-------|-------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 1 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | 0.00 | 19.74 | 20.05 | 20.86 | 21.05 | 23.08 | 0.00 |
| 3 | 0.00 | 0.00 | 0.00 | 0.00 | 1.96 | 3.99 | 0.00 |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****
US-101_SB_AM_NP_2040_PL

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FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQQ QQQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP EEEEEEEEE
    
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FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT DES TRUCKS | SPECIAL RAMP | FF. SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION LOCATION |
|---------|----------|----------|-------------|--------------|---------|---------|-----------|---------|----------------|--------------|-------------------|---------------|----------|----------------|-------------------------|
| ** 1 | 5 | 10000. | 1370. | 65 | OD | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Seeding |
| ** 2 | 3 | 6226. | 99999. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture |
| ** 3 | 3 | 6000. | 2740. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-85 Off to Shore On |
| ** 4 | 3 | 6000. | 600. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Shore. On to Moffet Off |
| ** 5 | 3 | 6000. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Moffett Off to On |
| ** 6 | 3 | 6000. | 2630. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Moffett On to Ellis Off |
| ** 7 | 3 | 6000. | 2530. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Ellis Off to On-ramp |
| ** 8 | 4 | 6430. | 1500. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Ellis On-ramp |
| ** 9 | 4 | 6430. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Ellis / US 237 |
| ** 10 | 4 | 6430. | 1500. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 EB Off-Ramp |
| ** 11 | 3 | 6000. | 750. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 / SR-237 |
| ** 12 | 4 | 7010. | 350. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 EB On-Ramp |
| ** 13 | 4 | 7010. | 350. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US 237 / Mathilda |
| ** 14 | 4 | 7010. | 350. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-Ramp |
| ** 15 | 3 | 6000. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda |
| ** 16 | 3 | 6000. | 900. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda SB On-Ramp |
| ** 17 | 3 | 6000. | 1400. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda NB On-Ramp |
| ** 18 | 3 | 6000. | 200. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Fair Oaks |
| ** 19 | 3 | 6000. | 1400. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks SB Off-Ramp |
| ** 20 | 3 | 6000. | 900. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks SB/ Fair Oaks |

 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *

| * SUB SEC | * NO. LNS | * SSEC LENGTH | * O-D ORG | * DATA DES | * DEMANDS SSEC | * ADJUSTED ORG | * DES | * VOLUMES SSEC | * SSEC CAP. | * WEAVE EFF | * CONGEST LENGTH | * STORAGE RATE | * V/C RATIO | * SPEED MPH | * DENSITY VPMP | * LOS LEVEL | * FUEL MPG | * EMISSIONS GS/VM | | |
|-----------|-----------|---------------|-----------|------------|----------------|----------------|-------|----------------|-------------|-------------|------------------|----------------|-----------------|-------------|----------------|-------------|------------|-------------------|------|------|
| * 1 | 5 | 1370. | 6300. | 1071. | 6300. | 6300. | 1071. | 6300. | 10000. | 0. | 0. | 0. | .63 | 65. | 19.4 | C | 19.2 | 14.0 | | |
| * 2 | 3 | 99999. | 0. | 0. | 5229. | 0. | 0. | 5229. | 6226. | 0. | 0. | 0. | .84 | 62. | 28.2 | D | 20.6 | 13.0 | | |
| * 3 | 3 | 2740. | 0. | 0. | 5229. | 0. | 0. | 5229. | 6000. | 0. | 0. | 0. | .87 | 61. | 28.8 | D | 21.3 | 12.5 | | |
| * 4 | 3 | 600. | 0. | 0. | 5229. | 0. | 0. | 5229. | 6000. | 0. | 0. | 0. | .87 | 61. | 28.8 | D | 21.3 | 12.5 | | |
| * 5 | 3 | 700. | 0. | 0. | 5229. | 0. | 0. | 5229. | 6000. | 0. | 0. | 0. | .87 | 61. | 28.8 | D | 21.3 | 12.5 | | |
| * 6 | 3 | 2630. | 0. | 0. | 5229. | 0. | 0. | 5229. | 6000. | 0. | 0. | 0. | .87 | 61. | 28.8 | D | 21.3 | 12.5 | | |
| * 7 | 3 | 2530. | 0. | 0. | 5229. | 0. | 0. | 5229. | 6000. | 0. | 0. | 0. | .87 | 61. | 28.8 | D | 21.3 | 12.5 | | |
| * 8 | 4 | 1500. | 297. | 0. | 5526. | 297. | 0. | 5526. | 6398. | 0. | 0. | 0. | .86 | 65. | 21.3 | C | 19.2 | 14.0 | | |
| * 9 | 4 | 700. | 0. | 0. | 5526. | 0. | 0. | 5526. | 6430. | 0. | 0. | 0. | .86 | 65. | 21.3 | C | 19.2 | 14.0 | | |
| * 10 | 4 | 1500. | 0. | 1660. | 5526. | 0. | 1660. | 5526. | 6110. | 0. | 0. | 0. | .90 | 65. | 21.3 | C | 19.2 | 14.0 | | |
| * 11 | 3 | 750. | 0. | 0. | 3866. | 0. | 0. | 3866. | 6000. | 0. | 0. | 0. | .64 | 65. | 19.8 | C | 19.2 | 14.0 | | |
| * 12 | 4 | 350. | 966. | 0. | 4832. | 900. | 0. | 4766. | 6856. | 0. | 0. | 0. | .70 | 65. | 18.3 | C | 19.2 | 14.0 | | |
| * 13 | 4 | 350. | 0. | 0. | 4832. | 0. | 0. | 4766. | 7010. | 0. | 0. | 0. | .68 | 65. | 18.3 | C | 19.2 | 14.0 | | |
| * 14 | 4 | 350. | 0. | 645. | 4832. | 0. | 635. | 4766. | 6914. | 0. | 0. | 0. | .69 | 65. | 18.3 | C | 19.2 | 14.0 | | |
| * 15 | 3 | 700. | 0. | 0. | 4187. | 0. | 0. | 4131. | 6000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 19.2 | 14.0 | | |
| * 16 | 3 | 900. | 101. | 0. | 4288. | 101. | 0. | 4232. | 5981. | 0. | 0. | 0. | .71 | 65. | 21.7 | C | 19.2 | 14.0 | | |
| * 17 | 3 | 1400. | 295. | 0. | 4583. | 295. | 0. | 4527. | 5945. | 0. | 0. | 0. | .76 | 64. | 23.6 | C | 19.6 | 13.7 | | |
| * 18 | 3 | 200. | 0. | 0. | 4583. | 0. | 0. | 4527. | 6000. | 0. | 0. | 0. | .75 | 64. | 23.5 | C | 19.6 | 13.7 | | |
| * 19 | 3 | 1400. | 0. | 274. | 4583. | 0. | 270. | 4527. | 5963. | 0. | 0. | 0. | .76 | 64. | 23.6 | C | 19.6 | 13.7 | | |
| * 20 | 3 | 900. | 0. | 0. | 4309. | 0. | 0. | 4257. | 6000. | 0. | 0. | 0. | .71 | 65. | 21.8 | C | 19.2 | 14.0 | | |
| * 21 | 4 | 100. | 208. | 0. | 4517. | 208. | 0. | 4465. | 6108. | 0. | 0. | 0. | .73 | 65. | 17.2 | B | 19.2 | 14.0 | | |
| * 22 | 4 | 100. | 0. | 84. | 4517. | 0. | 83. | 4465. | 6138. | 0. | 0. | 0. | .73 | 65. | 17.2 | B | 19.2 | 14.0 | | |
| * 23 | 3 | 600. | 0. | 0. | 4433. | 0. | 0. | 4382. | 6000. | 0. | 0. | 0. | .73 | 64. | 22.7 | C | 19.4 | 13.8 | | |
| * 24 | 3 | 1500. | 506. | 0. | 4939. | 506. | 0. | 4888. | 5896. | 0. | 0. | 0. | .83 | 62. | 26.2 | D | 20.4 | 13.1 | | |
| * 25 | 3 | 1500. | 0. | 0. | 4939. | 0. | 0. | 4888. | 6000. | 0. | 0. | 0. | .81 | 63. | 26.0 | C | 20.2 | 13.2 | | |
| * 26 | 3 | 8000. | 0. | 0. | 4939. | 0. | 0. | 4888. | 6000. | 0. | 0. | 0. | .81 | 63. | 26.0 | C | 20.2 | 13.2 | | |
| * 27 | 5 | 100. | 1012. | 0. | 5951. | 1012. | 0. | 5900. | 10000. | 0. | 0. | 0. | .59 | 65. | 18.2 | C | 19.2 | 14.0 | | |
| * 28 | 5 | 1000. | 0. | 0. | 5951. | 0. | 0. | 5900. | 7750. | 0. | 0. | 0. | .76 | 65. | 18.2 | C | 19.2 | 14.0 | | |
| * 29 | 5 | 1000. | 0. | 5951. | 5951. | 0. | 5900. | 5900. | 9685. | 0. | 0. | 0. | .61 | 65. | 18.2 | C | 19.2 | 14.0 | | |
| * TOTAL | 135469. | = | 25.7 | MI LNS | | | | | | | | | MAX(V/C) = 0.90 | | LOWEST LOS = D | | AVG = 62. | 27.2 | 20.5 | 13.0 |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 1 OF 2

| | | | |
|----------------------------|--------------------|------------------|-------------------------------------|
| | CURRENT TIME SLICE | | CUMULATIVE VALUES |
| FREWAY TRAVEL TIME = | 2139. VEH-HRS | 2150. PASS-HRS | 2139. VEH-HRS 2150. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 33. VEH-HRS | 33. PASS-HRS | 33. VEH-HRS 33. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 2172. VEH-HRS | 2183. PASS-HRS | 2172. VEH-HRS 2183. PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 132911. VEH-MI. | 133633. PASS-MI. | 132911. VEH-MI. 133633. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 61. MPH | | 62. MPH |
| AVERAGE DENSITY = | 27. VPMP | | 27. VPMP |
| TOTAL FUEL = | 6499. GALLONS | | 6499. GALLONS |
| TOTAL EMISSIONS = | 1739. KI LOGRAMS | | 1739. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 76.98 | 3 | 3.04 | 4 | 0.67 | 5 | 0.78 |
| 6 | 2.92 | 7 | 2.81 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.29 | 18 | 0.04 | 19 | 0.28 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.06 | 24 | 0.94 | 25 | 0.78 |
| 26 | 4.15 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 93.7 VEH-HRS ***** AVERAGE DELAY = 1.08 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MI NUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-----------|-----------------------|---------------|---------------------------------|----------|---------|---------|----------|----------------------|
| ON-RAMP 3 | RAMP | 66. | 33.00 | 2.05 | 11.78 | 0.73 | 3.82 | 0.20 |
| | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 66. | 33.00 | 2.05 | 11.78 | 0.73 | 3.82 | 0.20 |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 2

 **
 ** FREEWAY TRAVEL TIME (MI NUTES)
 **

US-101_SB_AM_P1_2040_PE

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | |
|-----------|--|-----------------------|-------|-------|-------|-------|-------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 |
| * 1 * | | 0.24 | 27.37 | 27.69 | 28.52 | 28.72 | 31.35 |
| * 2 * | | 0.00 | 1.46 | 1.78 | 2.61 | 2.81 | 5.44 |
| * 3 * | | 0.00 | 0.00 | 0.18 | 1.02 | 1.21 | 3.85 |
| * 4 * | | 0.00 | 0.00 | 0.00 | 0.71 | 0.91 | 3.54 |
| * 5 * | | 0.00 | 0.00 | 0.00 | 0.55 | 0.75 | 3.38 |
| * 6 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.03 | 2.67 |
| * 7 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.53 |
| * 8 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.37 |
| * 9 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.35 |
| * 10 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 2

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB | * NO. | * SSEC | * O-D | * DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | |
|---------|-------|-----------|-----------------|---------|-----------|-------------------|-----------|------------------|----------|-------------|-----------|---------|---------|-----------|---------|--------|-------------|--------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * SSEC | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | |
| * 1 | * 5 | * 1370. | * 7500. | * 1275. | * 7500. | * 7500. | * 1275. | * 7500. | * 10000. | * 0. | * 0. | * 0. | * .75 | * 64. | * 23.4 | * C | * 19.5 | * 13.7 |
| * 2 | * 3 | * 99999. | * 0. | * 0. | * 6225. | * 0. | * 0. | * 6000. | * 6226. | * 0. | * 7452. | * .225 | * .96 | * 50. | * 40.3 | * F | * 23.6 | * 11.3 |
| * 3 | * 3 | * 2740. | * 0. | * 0. | * 6225. | * 0. | * 0. | * 5718. | * 6000. | * 0. | * 264. | * 282. | * .95 | * 52. | * 36.6 | * F | * 23.8 | * 11.1 |
| * 4 | * 3 | * 600. | * 0. | * 0. | * 6225. | * 0. | * 0. | * 5718. | * 6000. | * 0. | * 600. | * 282. | * .95 | * 48. | * 39.8 | * F | * 23.4 | * 11.4 |
| * 5 | * 3 | * 700. | * 0. | * 0. | * 6225. | * 0. | * 0. | * 5718. | * 6000. | * 0. | * 700. | * 282. | * .95 | * 44. | * 43.6 | * F | * 23.0 | * 11.7 |
| * 6 | * 3 | * 2630. | * 0. | * 0. | * 6225. | * 0. | * 0. | * 5718. | * 6000. | * 0. | * 2630. | * 282. | * .95 | * 36. | * 53.4 | * F | * 22.0 | * 12.6 |
| * 7 | * 3 | * 2530. | * 0. | * 0. | * 6225. | * 0. | * 0. | * 5718. | * 6000. | * 0. | * 2530. | * 282. | * .95 | * 28. | * 69.0 | * F | * 20.5 | * 13.9 |
| * 8 | * 4 | * 1500. | * 387. | * 0. | * 6612. | * 337. | * 0. | * 6055. | * 6387. | * 0. | * 1500. | * 282. | * .95 | * 23. | * 66.2 | * F | * 19.4 | * 15.1 |
| * 9 | * 4 | * 700. | * 0. | * 0. | * 6612. | * 0. | * 0. | * 6055. | * 6430. | * 0. | * 700. | * 282. | * .94 | * 20. | * 74.3 | * F | * 18.6 | * 16.0 |
| * 10 | * 4 | * 1500. | * 0. | * 1955. | * 6612. | * 0. | * 1789. | * 6055. | * 6055. | * 0. | * 0. | * 0. | * 1.00 | * 52. | * 29.0 | * E | * 23.8 | * 11.1 |
| * 11 | * 3 | * 750. | * 0. | * 0. | * 4657. | * 0. | * 0. | * 4266. | * 6000. | * 0. | * 0. | * 0. | * .71 | * 65. | * 21.9 | * C | * 19.2 | * 14.0 |
| * 12 | * 4 | * 350. | * 1352. | * 0. | * 6009. | * 900. | * 0. | * 5166. | * 6793. | * 0. | * 0. | * 0. | * .76 | * 65. | * 19.9 | * C | * 19.2 | * 14.0 |
| * 13 | * 4 | * 350. | * 0. | * 0. | * 6009. | * 0. | * 0. | * 5166. | * 7010. | * 0. | * 0. | * 0. | * .74 | * 65. | * 19.9 | * C | * 19.2 | * 14.0 |
| * 14 | * 4 | * 350. | * 0. | * 883. | * 6009. | * 0. | * 752. | * 5166. | * 6883. | * 0. | * 0. | * 0. | * .75 | * 65. | * 19.9 | * C | * 19.2 | * 14.0 |
| * 15 | * 3 | * 700. | * 0. | * 0. | * 5126. | * 0. | * 0. | * 4413. | * 6000. | * 0. | * 0. | * 0. | * .74 | * 64. | * 22.8 | * C | * 19.4 | * 13.8 |
| * 16 | * 3 | * 900. | * 142. | * 0. | * 5268. | * 142. | * 0. | * 4555. | * 5973. | * 0. | * 0. | * 0. | * .76 | * 64. | * 23.7 | * C | * 19.6 | * 13.7 |
| * 17 | * 3 | * 1400. | * 408. | * 0. | * 5676. | * 408. | * 0. | * 4963. | * 5922. | * 0. | * 0. | * 0. | * .84 | * 62. | * 26.7 | * D | * 20.6 | * 13.0 |
| * 18 | * 3 | * 200. | * 0. | * 0. | * 5676. | * 0. | * 0. | * 4963. | * 6000. | * 0. | * 0. | * 0. | * .83 | * 62. | * 26.5 | * D | * 20.4 | * 13.1 |
| * 19 | * 3 | * 1400. | * 0. | * 207. | * 5676. | * 0. | * 181. | * 4963. | * 5973. | * 0. | * 0. | * 0. | * .83 | * 62. | * 26.6 | * D | * 20.5 | * 13.1 |
| * 20 | * 3 | * 900. | * 0. | * 0. | * 5469. | * 0. | * 0. | * 4782. | * 6000. | * 0. | * 0. | * 0. | * .80 | * 63. | * 25.2 | * C | * 20.0 | * 13.4 |
| * 21 | * 4 | * 100. | * 283. | * 0. | * 5752. | * 283. | * 0. | * 5065. | * 6093. | * 0. | * 0. | * 0. | * .83 | * 65. | * 19.5 | * C | * 19.2 | * 14.0 |
| * 22 | * 4 | * 100. | * 0. | * 128. | * 5752. | * 0. | * 112. | * 5065. | * 6133. | * 0. | * 0. | * 0. | * .83 | * 65. | * 19.5 | * C | * 19.2 | * 14.0 |
| * 23 | * 3 | * 600. | * 0. | * 0. | * 5624. | * 0. | * 0. | * 4953. | * 6000. | * 0. | * 0. | * 0. | * .83 | * 62. | * 26.5 | * D | * 20.4 | * 13.1 |
| * 24 | * 3 | * 1500. | * 564. | * 0. | * 6188. | * 564. | * 0. | * 5517. | * 5884. | * 0. | * 0. | * 0. | * .94 | * 57. | * 32.3 | * D | * 22.5 | * 11.7 |
| * 25 | * 3 | * 1500. | * 0. | * 0. | * 6188. | * 0. | * 0. | * 5517. | * 6000. | * 0. | * 0. | * 0. | * .92 | * 58. | * 31.7 | * D | * 22.2 | * 12.0 |
| * 26 | * 3 | * 8000. | * 0. | * 0. | * 6188. | * 0. | * 0. | * 5517. | * 6000. | * 0. | * 0. | * 0. | * .92 | * 58. | * 31.7 | * D | * 22.2 | * 12.0 |
| * 27 | * 5 | * 100. | * 1268. | * 0. | * 7456. | * 1268. | * 0. | * 6785. | * 10000. | * 0. | * 0. | * 0. | * .68 | * 65. | * 20.9 | * C | * 19.2 | * 14.0 |
| * 28 | * 5 | * 1000. | * 0. | * 0. | * 7456. | * 0. | * 0. | * 6785. | * 7750. | * 0. | * 0. | * 0. | * .88 | * 65. | * 20.9 | * C | * 19.2 | * 14.0 |
| * 29 | * 5 | * 1000. | * 0. | * 7456. | * 7456. | * 0. | * 6785. | * 6785. | * 9685. | * 0. | * 0. | * 0. | * .70 | * 65. | * 20.9 | * C | * 19.2 | * 14.0 |
| * TOTAL | | * 135469. | * = 25.7 MI LES | | | * MAX(V/C) = 1.00 | | * LOWEST LOS = F | | * AVG = 49. | | * 39.2 | | * 22.9 | | * 11.7 | | |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 2

| CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | | |
|----------------------------|---------|------------|---------|-------------------|---------|------------|---------|----------|
| FREWAY TRAVEL TIME = | 3180. | VEH-HRS | 3194. | PASS-HRS | 5319. | VEH-HRS | 5343. | PASS-HRS |
| FREWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 317. | VEH-HRS | 317. | PASS-HRS | 350. | VEH-HRS | 350. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 3497. | VEH-HRS | 3511. | PASS-HRS | 5669. | VEH-HRS | 5693. | PASS-HRS |
| TOTAL TRAV DISTANCE = | 155844. | VEH-MI. | 156683. | PASS-MI. | 288755. | VEH-MI. | 290316. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 45. | MPH | | | 54. | MPH | | |
| AVERAGE DENSITY = | 39. | VPMP | | | 33. | VPMP | | |
| TOTAL FUEL = | 6907. | GALLONS | | | 13405. | GALLONS | | |
| TOTAL EMISSIONS = | 1862. | KI LOGRAMS | | | 3601. | KI LOGRAMS | | |

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***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|--------|------------|-------|------------|-------|------------|-------|
| 1 | 0.38 | 2 | 558.14 | 3 | 11.84 | 4 | 3.73 | 5 | 5.91 |
| 6 | 37.19 | 7 | 58.14 | 8 | 49.15 | 9 | 27.12 | 10 | 6.48 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.08 |
| 16 | 0.19 | 17 | 1.00 | 18 | 0.12 | 19 | 0.92 | 20 | 0.36 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.37 | 24 | 3.41 | 25 | 2.87 |
| 26 | 15.33 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 782.7 VEH-HRS ***** AVERAGE DELAY = 7.90 MIN/VEH *****

***** RAMP DELAYS *****

| | | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|---------|---|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|
| ON-RAMP | 2 | RAMP | 50. | 25.00 | 3.88 | 8.93 | 0.55 | 2.90 | 3.60 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 50. | 25.00 | 3.88 | 8.93 | 0.55 | 2.90 | 3.60 |
| ON-RAMP | 3 | RAMP | 518. | 292.00 | 12.36 | 104.27 | 6.47 | 33.83 | 42.09 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 518. | 292.00 | 12.36 | 104.27 | 6.47 | 33.83 | 42.09 |

US-101_SB_AM_P1_2040_PL

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**
** 19 2 3000. 1400. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks SB Off-Ramp **
**
** 20 2 3000. 900. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks SB/ Fair Oaks **
**
*****

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FREEWAY AND ARTERIAL DESIGN FEATURES

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*****
**
**
**
**
**
** SUB NO. SSEC SSEC DESIG N ORG TRK SSEC PCT PCT DES SPECIAL FF.SPD. CAP. ART GRADE SUBSECTI ON LOCATI ON **
** SEC LNS CAP LENGTH SPEED DES FAC GRAD TRK TRUCKS RAMP ALT. RTE ALT. RTE TYPE ALT. RTE **
**
** 21 2 3000. 100. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Fair Oaks SB On-Ramp **
**
** 22 2 3000. 100. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks NB Off-Ramp **
**
** 23 2 3000. 600. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks NB/ Fair Oaks **
**
** 24 2 3000. 1500. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Oaks On-Ramp to Mid **
**
** 25 2 3000. 1500. 65 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Mid to Lawrence Off-ramp **
**
** 26 2 3000. 8000. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 HOV Dummy **
**
** 27 **
** 28 **
** 29 **
**
*****

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FREEWAY TRAVEL TIME (MINUTES)

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*****
* O R I G I N S D E S T I N A T I O N S A C R O S S
* D O W N
* 1 2 3 4 5 6 7
+
*
*
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 2 * 0.00 19.74 20.05 20.86 21.05 23.08 0.00
+
* 3 * 0.00 0.00 0.00 0.00 1.96 3.99 0.00
+
* 4 * 0.00 0.00 0.00 0.00 0.00 3.21 0.00
+
* 5 * 0.00 0.00 0.00 0.00 0.00 2.90 0.00
+
* 6 * 0.00 0.00 0.00 0.00 0.00 2.74 0.00
+
* 7 * 0.00 0.00 0.00 0.00 0.00 2.06 0.00
+
* 8 * 0.00 0.00 0.00 0.00 0.00 1.92 0.00
+
* 9 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 10 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 11 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
*
*****

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TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB SEC | NO. LNS | SSEC LENGTH | O-D ORG | DATA DES | DEMANDS SSEC | ADJUSTED ORG | VOLUMES DES | SSEC SSEC | WEAVE CAP. | CONGEST EFF | STORAGE LENGTH | V/C RATE | SPEED RATIO | DENSITY MPH | LOS VPMP | FUEL LEVEL | EMI SS MPG |
|---------|---------|-------------|---------|----------|--------------|--------------|-------------|-----------|------------|-----------------|----------------|-----------|-------------|-------------|----------|------------|------------|
| 1 | | | | | | | | | | | | | | | | | |
| 2 | 2 | 99999 | 1071 | 0 | 1071 | 1071 | 0 | 1071 | 3000 | 0 | 0 | 0 | .36 | 65 | 8.2 | A | 20.0 |
| 3 | 2 | 2740 | 0 | 0 | 1071 | 0 | 0 | 1071 | 3000 | 0 | 0 | 0 | .36 | 65 | 8.2 | A | 20.0 |
| 4 | 2 | 600 | 0 | 0 | 1071 | 0 | 0 | 1071 | 3000 | 0 | 0 | 0 | .36 | 65 | 8.2 | A | 20.0 |
| 5 | 2 | 700 | 0 | 0 | 1071 | 0 | 0 | 1071 | 3000 | 0 | 0 | 0 | .36 | 65 | 8.2 | A | 20.0 |
| 6 | 2 | 2630 | 0 | 0 | 1071 | 0 | 0 | 1071 | 3000 | 0 | 0 | 0 | .36 | 65 | 8.2 | A | 20.0 |
| 7 | 2 | 2530 | 0 | 0 | 1071 | 0 | 0 | 1071 | 3000 | 0 | 0 | 0 | .36 | 65 | 8.2 | A | 20.0 |
| 8 | 2 | 1500 | 32 | 0 | 1103 | 32 | 0 | 1103 | 3000 | 0 | 0 | 0 | .37 | 65 | 8.5 | A | 20.0 |
| 9 | 2 | 700 | 0 | 0 | 1103 | 0 | 0 | 1103 | 3000 | 0 | 0 | 0 | .37 | 65 | 8.5 | A | 20.0 |
| 10 | 2 | 1500 | 0 | 320 | 1103 | 0 | 320 | 1103 | 3000 | 0 | 0 | 0 | .37 | 65 | 8.5 | A | 20.0 |
| 11 | 2 | 750 | 0 | 0 | 784 | 0 | 0 | 784 | 3000 | 0 | 0 | 0 | .26 | 65 | 6.0 | A | 20.0 |
| 12 | 2 | 350 | 154 | 0 | 937 | 154 | 0 | 937 | 3000 | 0 | 0 | 0 | .31 | 65 | 7.2 | A | 20.0 |
| 13 | 2 | 350 | 0 | 0 | 937 | 0 | 0 | 937 | 3000 | 0 | 0 | 0 | .31 | 65 | 7.2 | A | 20.0 |
| 14 | 2 | 350 | 0 | 96 | 937 | 0 | 96 | 937 | 3000 | 0 | 0 | 0 | .31 | 65 | 7.2 | A | 20.0 |
| 15 | 2 | 700 | 0 | 0 | 841 | 0 | 0 | 841 | 3000 | 0 | 0 | 0 | .28 | 65 | 6.5 | A | 20.0 |
| 16 | 2 | 900 | 19 | 0 | 860 | 19 | 0 | 860 | 3000 | 0 | 0 | 0 | .29 | 65 | 6.6 | A | 20.0 |
| 17 | 2 | 1400 | 55 | 0 | 915 | 55 | 0 | 915 | 3000 | 0 | 0 | 0 | .30 | 65 | 7.0 | A | 20.0 |
| 18 | 2 | 200 | 0 | 0 | 915 | 0 | 0 | 915 | 3000 | 0 | 0 | 0 | .30 | 65 | 7.0 | A | 20.0 |
| 19 | 2 | 1400 | 0 | 37 | 915 | 0 | 37 | 915 | 3000 | 0 | 0 | 0 | .30 | 65 | 7.0 | A | 20.0 |
| 20 | 2 | 900 | 0 | 0 | 878 | 0 | 0 | 878 | 3000 | 0 | 0 | 0 | .29 | 65 | 6.8 | A | 20.0 |
| 21 | 2 | 100 | 42 | 0 | 920 | 42 | 0 | 920 | 3000 | 0 | 0 | 0 | .31 | 65 | 7.1 | A | 20.0 |
| 22 | 2 | 100 | 0 | 12 | 920 | 0 | 12 | 920 | 3000 | 0 | 0 | 0 | .31 | 65 | 7.1 | A | 20.0 |
| 23 | 2 | 600 | 0 | 0 | 908 | 0 | 0 | 908 | 3000 | 0 | 0 | 0 | .30 | 65 | 7.0 | A | 20.0 |
| 24 | 2 | 1500 | 104 | 0 | 1012 | 104 | 0 | 1012 | 3000 | 0 | 0 | 0 | .34 | 65 | 7.8 | A | 20.0 |
| 25 | 2 | 1500 | 0 | 0 | 1012 | 0 | 0 | 1012 | 3000 | 0 | 0 | 0 | .34 | 65 | 7.8 | A | 20.0 |
| 26 | 2 | 8000 | 0 | 1012 | 1012 | 0 | 1012 | 1012 | 3000 | 0 | 0 | 0 | .34 | 65 | 7.8 | A | 20.0 |
| 27 | | | | | | | | | | | | | | | | | |
| 28 | | | | | | | | | | | | | | | | | |
| 29 | | | | | | | | | | | | | | | | | |
| TOTAL | 131999 | = | 25.0 | MI | LES | | | | | MAX(V/C) = 0.37 | LOWEST LOS = A | AVG = 65. | 8.1 | | | 20.0 | 13.7 |

| | | | | | |
|-----------------------------|----------------|-----------------|-------------------|-----------------|---------------|
| FREEWAY TRAVEL TIME = | 406. VEH-HRS | 812. PASS-HRS | CUMULATIVE VALUES | 406. VEH-HRS | 812. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | |
| TOTAL SYSTEM TRAVEL TIME = | 406. VEH-HRS | 812. PASS-HRS | 406. VEH-HRS | 812. PASS-HRS | |
| TOTAL FRWAY TRAV DISTANCE = | 26394. VEH-MI. | 52789. PASS-MI. | 26394. VEH-MI. | 52789. PASS-MI. | |
| AVERAGE SYSTEM SPEED = | 65. MPH. | | 65. MPH. | | |
| AVERAGE DENSITY = | 8. VPMP | | 8. VPMP | | |
| TOTAL FUEL = | 1320. GALLONS | | 1320. GALLONS | | |
| TOTAL EMISSIONS = | 363. KILOGRAMS | | 363. KILOGRAMS | | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

 ** FREEWAY TRAVEL TIME (MINUTES) **

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | |
|--------------|---------------------|-------|-------|-------|-------|-------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 1 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | 0.00 | 19.74 | 20.05 | 20.86 | 21.05 | 23.08 | 0.00 |
| 3 | 0.00 | 0.00 | 0.00 | 0.00 | 1.96 | 3.99 | 0.00 |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****
US-101_SB_AM_P1_2040_PL

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FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQQ QQQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP EEE
FFF RRR RRR EEE Q*UC* QQQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*QQ 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP EEEEEEEEE
    
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FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT DES TRUCKS | SPECIAL RAMP | FF. SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION LOCATION |
|---------|----------|----------|-------------|--------------|---------|---------|-----------|---------|----------------|--------------|-------------------|---------------|----------|----------------|-------------------------|
| ** 1 | 5 | 10000. | 1370. | 65 | OD | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Seeding |
| ** 2 | 3 | 6226. | 99999. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture |
| ** 3 | 3 | 6000. | 2740. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-85 Off to Shore On |
| ** 4 | 3 | 6000. | 600. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Shore. On to Moffet Off |
| ** 5 | 3 | 6000. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Moffett Off to On |
| ** 6 | 3 | 6000. | 2630. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Moffett On to Ellis Off |
| ** 7 | 3 | 6000. | 2530. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Ellis Off to On-ramp |
| ** 8 | 4 | 6430. | 1500. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Ellis On-ramp |
| ** 9 | 4 | 6430. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Ellis / US 237 |
| ** 10 | 4 | 6430. | 1500. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 EB Off-Ramp |
| ** 11 | 3 | 6000. | 750. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 / SR-237 |
| ** 12 | 4 | 7010. | 350. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 EB On-Ramp |
| ** 13 | 4 | 7010. | 350. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US 237 / Mathilda |
| ** 14 | 4 | 7010. | 350. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-Ramp |
| ** 15 | 3 | 6000. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda |
| ** 16 | 3 | 6000. | 900. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda SB On-Ramp |
| ** 17 | 3 | 6000. | 1400. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda NB On-Ramp |
| ** 18 | 3 | 6000. | 200. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Fair Oaks |
| ** 19 | 3 | 6000. | 1400. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks SB Off-Ramp |
| ** 20 | 3 | 6000. | 900. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks SB/ Fair Oaks |

FREeway AND ARTERIAL DESIGN FEATURES

| SUB NO. SEC | LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC PCT GRAD | PCT TRK | DES TRUCKS | SPECIAL RAMP | FF SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION | LOCATION |
|----------------|-----|-------------|----------------|-----------------|------------|------------|------------------|------------|---------------|-----------------|---------------------|------------------|-------------|-------------------|--------------------------|----------|
| ** 21 | 4 | 6150. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Fair Oaks SB On-Ramp | ** |
| ** 22 | 4 | 6150. | 100. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks NB Off-Ramp | ** |
| ** 23 | 3 | 6000. | 600. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks NB/ Fair Oaks | ** |
| ** 24 | 3 | 6000. | 1500. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Oaks On-Ramp to Mid | ** |
| ** 25 | 3 | 6000. | 1500. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mid to Lawrence Off-ramp | ** |
| ** 26 | 3 | 6000. | 8000. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | ** |
| ** 27 | 5 | 10000. | 100. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | HOV Dummy | ** |
| ** 28 | 5 | 7750. | 1000. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Dummy Bottleneck | ** |
| ** 29 | 5 | 9685. | 1000. | 65 | OD | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | End of Network | ** |

***** INPUT HAS BEEN COMPLETED *****

MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 3 IN TIME SLICE 1
--- THE MAXIMUM METERING RATE WILL PREVAIL.

MAXIMUM METERING RATE AND MAXIMUM QUEUE LENGTH CONFLICT AT ON-RAMP 3 IN TIME SLICE 2
--- THE MAXIMUM METERING RATE WILL PREVAIL.

FREeway TRAVEL TIME (MINUTES)

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | |
|-----------------|---------------------|-------|-------|-------|-------|-------|
| | 1 | 2 | 3 | 4 | 5 | 6 |
| * 1 * | 0.24 | 20.98 | 21.29 | 22.10 | 22.30 | 24.76 |
| * 2 * | 0.00 | 0.65 | 0.96 | 1.77 | 1.97 | 4.43 |
| * 3 * | 0.00 | 0.00 | 0.18 | 0.99 | 1.19 | 3.65 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.69 | 0.88 | 3.34 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.53 | 0.72 | 3.19 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.03 | 2.50 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.36 |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.37 |
| * 9 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.35 |
| * 10 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 |

 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *

| * SUB SEC | * NO. LNS | * SSEC LENGTH | * O-D ORG | * DATA DES | * DEMANDS SSEC | * ADJUSTED ORG | * DES | * VOLUMES SSEC | * SSEC CAP. | * WEAVE EFF | * CONGEST LENGTH | * STORAGE RATE | * V/C RATIO | * SPEED MPH | * DENSITY VPMP/L | * LOS LEVEL | * FUEL MPG | * EMISSIONS GS/VM | | |
|-----------|-----------|---------------|-----------|------------|----------------|----------------|-------|----------------|-------------|-------------|------------------|----------------|-----------------|-------------|------------------|-------------|------------|-------------------|------|------|
| * 1 | 5 | 1370. | 6300. | 1071. | 6300. | 6300. | 1071. | 6300. | 10000. | 0. | 0. | 0. | .63 | 65. | 19.4 | C | 19.2 | 14.0 | | |
| * 2 | 3 | 99999. | 0. | 0. | 5229. | 0. | 0. | 5229. | 6226. | 0. | 0. | 0. | .84 | 62. | 28.2 | D | 20.6 | 13.0 | | |
| * 3 | 3 | 2740. | 0. | 0. | 5229. | 0. | 0. | 5229. | 6000. | 0. | 0. | 0. | .87 | 61. | 28.8 | D | 21.3 | 12.5 | | |
| * 4 | 3 | 600. | 0. | 0. | 5229. | 0. | 0. | 5229. | 6000. | 0. | 0. | 0. | .87 | 61. | 28.8 | D | 21.3 | 12.5 | | |
| * 5 | 3 | 700. | 0. | 0. | 5229. | 0. | 0. | 5229. | 6000. | 0. | 0. | 0. | .87 | 61. | 28.8 | D | 21.3 | 12.5 | | |
| * 6 | 3 | 2630. | 0. | 0. | 5229. | 0. | 0. | 5229. | 6000. | 0. | 0. | 0. | .87 | 61. | 28.8 | D | 21.3 | 12.5 | | |
| * 7 | 3 | 2530. | 0. | 0. | 5229. | 0. | 0. | 5229. | 6000. | 0. | 0. | 0. | .87 | 61. | 28.8 | D | 21.3 | 12.5 | | |
| * 8 | 4 | 1500. | 297. | 0. | 5526. | 297. | 0. | 5526. | 6398. | 0. | 0. | 0. | .86 | 65. | 21.3 | C | 19.2 | 14.0 | | |
| * 9 | 4 | 700. | 0. | 0. | 5526. | 0. | 0. | 5526. | 6430. | 0. | 0. | 0. | .86 | 65. | 21.3 | C | 19.2 | 14.0 | | |
| * 10 | 4 | 1500. | 0. | 1660. | 5526. | 0. | 1660. | 5526. | 6110. | 0. | 0. | 0. | .90 | 65. | 21.3 | C | 19.2 | 14.0 | | |
| * 11 | 3 | 750. | 0. | 0. | 3866. | 0. | 0. | 3866. | 6000. | 0. | 0. | 0. | .64 | 65. | 19.8 | C | 19.2 | 14.0 | | |
| * 12 | 4 | 350. | 966. | 0. | 4832. | 900. | 0. | 4766. | 6856. | 0. | 0. | 0. | .70 | 65. | 18.3 | C | 19.2 | 14.0 | | |
| * 13 | 4 | 350. | 0. | 0. | 4832. | 0. | 0. | 4766. | 7010. | 0. | 0. | 0. | .68 | 65. | 18.3 | C | 19.2 | 14.0 | | |
| * 14 | 4 | 350. | 0. | 645. | 4832. | 0. | 635. | 4766. | 6914. | 0. | 0. | 0. | .69 | 65. | 18.3 | C | 19.2 | 14.0 | | |
| * 15 | 3 | 700. | 0. | 0. | 4187. | 0. | 0. | 4131. | 6000. | 0. | 0. | 0. | .69 | 65. | 21.2 | C | 19.2 | 14.0 | | |
| * 16 | 3 | 900. | 93. | 0. | 4280. | 93. | 0. | 4224. | 5983. | 0. | 0. | 0. | .71 | 65. | 21.7 | C | 19.2 | 14.0 | | |
| * 17 | 3 | 1400. | 261. | 0. | 4541. | 261. | 0. | 4485. | 5951. | 0. | 0. | 0. | .75 | 64. | 23.3 | C | 19.6 | 13.7 | | |
| * 18 | 3 | 200. | 0. | 0. | 4541. | 0. | 0. | 4485. | 6000. | 0. | 0. | 0. | .75 | 64. | 23.3 | C | 19.5 | 13.7 | | |
| * 19 | 3 | 1400. | 0. | 271. | 4541. | 0. | 267. | 4485. | 5963. | 0. | 0. | 0. | .75 | 64. | 23.3 | C | 19.5 | 13.7 | | |
| * 20 | 3 | 900. | 0. | 0. | 4270. | 0. | 0. | 4218. | 6000. | 0. | 0. | 0. | .70 | 65. | 21.6 | C | 19.2 | 14.0 | | |
| * 21 | 4 | 100. | 208. | 0. | 4478. | 208. | 0. | 4426. | 6108. | 0. | 0. | 0. | .72 | 65. | 17.0 | B | 19.2 | 14.0 | | |
| * 22 | 4 | 100. | 0. | 83. | 4478. | 0. | 82. | 4426. | 6138. | 0. | 0. | 0. | .72 | 65. | 17.0 | B | 19.2 | 14.0 | | |
| * 23 | 3 | 600. | 0. | 0. | 4395. | 0. | 0. | 4344. | 6000. | 0. | 0. | 0. | .72 | 65. | 22.3 | C | 19.2 | 14.0 | | |
| * 24 | 3 | 1500. | 506. | 0. | 4901. | 506. | 0. | 4850. | 5896. | 0. | 0. | 0. | .82 | 62. | 25.9 | C | 20.3 | 13.1 | | |
| * 25 | 3 | 1500. | 0. | 0. | 4901. | 0. | 0. | 4850. | 6000. | 0. | 0. | 0. | .81 | 63. | 25.7 | C | 20.1 | 13.3 | | |
| * 26 | 3 | 8000. | 0. | 0. | 4901. | 0. | 0. | 4850. | 6000. | 0. | 0. | 0. | .81 | 63. | 25.7 | C | 20.1 | 13.3 | | |
| * 27 | 5 | 100. | 1004. | 0. | 5905. | 1004. | 0. | 5854. | 10000. | 0. | 0. | 0. | .59 | 65. | 18.0 | C | 19.2 | 14.0 | | |
| * 28 | 5 | 1000. | 0. | 0. | 5905. | 0. | 0. | 5854. | 7750. | 0. | 0. | 0. | .76 | 65. | 18.0 | C | 19.2 | 14.0 | | |
| * 29 | 5 | 1000. | 0. | 5905. | 5905. | 0. | 5854. | 5854. | 9685. | 0. | 0. | 0. | .60 | 65. | 18.0 | C | 19.2 | 14.0 | | |
| * TOTAL | 135469. | = | 25.7 | MI LNS | | | | | | | | | MAX(V/C) = 0.90 | | LOWEST LOS = D | | AVG = 62. | 27.2 | 20.5 | 13.1 |

1 INSTITUTE OF TRANSPORTATION STUDIES FREQ12PE REL 3.01 3/30/2016 16:26 PAGE 6
 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 1 OF 2

| | | | |
|----------------------------|------------------|-------------------|-------------------------------------|
| CURRENT TIME SLICE | | CUMULATIVE VALUES | |
| FREWAY TRAVEL TIME = | 2136. VEH-HRS | 2147. PASS-HRS | 2136. VEH-HRS 2147. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 33. VEH-HRS | 33. PASS-HRS | 33. VEH-HRS 33. PASS-HRS |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 2169. VEH-HRS | 2180. PASS-HRS | 2169. VEH-HRS 2180. PASS-HRS |
| TOTAL TRAV DISTANCE = | 132776. VEH-MI. | 133492. PASS-MI. | 132776. VEH-MI. 133492. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 61. MPH | | 62. MPH |
| AVERAGE DENSITY = | 27. VPMP/L | | 27. VPMP/L |
| TOTAL FUEL = | 6495. GALLONS | | 6495. GALLONS |
| TOTAL EMISSIONS = | 1738. KI LOGRAMS | | 1738. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| | | | | | | | | | |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
| 1 | 0.00 | 2 | 76.98 | 3 | 3.04 | 4 | 0.67 | 5 | 0.78 |
| 6 | 2.92 | 7 | 2.81 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.25 | 18 | 0.03 | 19 | 0.24 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.86 | 25 | 0.71 |
| 26 | 3.78 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 93.1 VEH-HRS ***** AVERAGE DELAY = 1.07 MIN/VEH *****

***** RAMP DELAYS *****

| | | | | | | | | |
|-----------|--------------|---------|----------|-------|------|------|------|-----------|
| | QUEUE LENGTH | DELAY | AVERAGE | GAS | HC | CO | NOX | TOTAL |
| | VEHICLES | VEH-HRS | METERING | GALS | KGMS | KGMS | KGMS | EMISSIONS |
| | | | MI NUTES | | | | | KGMS |
| ON-RAMP 3 | RAMP | 66. | 2.05 | 11.78 | 0.73 | 3.82 | 0.20 | 4.76 |
| | FREWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 66. | 2.05 | 11.78 | 0.73 | 3.82 | 0.20 | 4.76 |

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 TIME SLICE 2 OF 2

 **
 ** FREEWAY TRAVEL TIME (MI NUTES) **
 **

US-101_SB_AM_P2_2040_PE

| ORIGINS | | DESTINATIONS ACROSS | | | | | |
|---------|--|---------------------|-------|-------|-------|-------|-------|
| DOWN | | 1 | 2 | 3 | 4 | 5 | 6 |
| * 1 * | | 0.24 | 27.37 | 27.69 | 28.52 | 28.71 | 31.32 |
| * 2 * | | 0.00 | 1.46 | 1.78 | 2.61 | 2.80 | 5.41 |
| * 3 * | | 0.00 | 0.00 | 0.18 | 1.01 | 1.21 | 3.82 |
| * 4 * | | 0.00 | 0.00 | 0.00 | 0.70 | 0.90 | 3.51 |
| * 5 * | | 0.00 | 0.00 | 0.00 | 0.55 | 0.74 | 3.35 |
| * 6 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.03 | 2.64 |
| * 7 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.50 |
| * 8 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.37 |
| * 9 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.35 |
| * 10 * | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.17 |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 2

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | | |
|-----------|----------|------------|-----------|--------------------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|------|---|------|------|
| * SEC LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES SSEC | * CAP | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | | | |
| * 1 | 5 | 1370. | 7500. | 1275. | 7500. | 7500. | 1275. | 7500. | 10000. | 0. | 0. | 0. | .75 | 64. | 23.4 | C | 19.5 | 13.7 |
| * 2 | 3 | 99999. | 0. | 0. | 6225. | 0. | 0. | 6000. | 6226. | 0. | * 7452. | 225. | .96 | 50. | 40.3 | F | 23.6 | 11.3 |
| * 3 | 3 | 2740. | 0. | 0. | 6225. | 0. | 0. | 5718. | 6000. | 0. | * 264. | 282. | .95 | 52. | 36.6 | F | 23.8 | 11.1 |
| * 4 | 3 | 600. | 0. | 0. | 6225. | 0. | 0. | 5718. | 6000. | 0. | ** 600. | 282. | .95 | 48. | 39.8 | F | 23.4 | 11.4 |
| * 5 | 3 | 700. | 0. | 0. | 6225. | 0. | 0. | 5718. | 6000. | 0. | ** 700. | 282. | .95 | 44. | 43.6 | F | 23.0 | 11.7 |
| * 6 | 3 | 2630. | 0. | 0. | 6225. | 0. | 0. | 5718. | 6000. | 0. | ** 2630. | 282. | .95 | 36. | 53.4 | F | 22.0 | 12.6 |
| * 7 | 3 | 2530. | 0. | 0. | 6225. | 0. | 0. | 5718. | 6000. | 0. | ** 2530. | 282. | .95 | 28. | 69.0 | F | 20.5 | 13.9 |
| * 8 | 4 | 1500. | 387. | 0. | 6612. | 337. | 0. | 6055. | 6387. | 0. | ** 1500. | 282. | .95 | 23. | 66.2 | F | 19.4 | 15.1 |
| * 9 | 4 | 700. | 0. | 0. | 6612. | 0. | 0. | 6055. | 6430. | 0. | ** 700. | 282. | .94 | 20. | 74.3 | F | 18.6 | 16.0 |
| * 10 | 4 | 1500. | 0. | 1955. | 6612. | 0. | 1789. | 6055. | 6055. | 0. | 0. | 0. | 1.00 | 52. | 29.0 | E | 23.8 | 11.1 |
| * 11 | 3 | 750. | 0. | 0. | 4657. | 0. | 0. | 4266. | 6000. | 0. | 0. | 0. | .71 | 65. | 21.9 | C | 19.2 | 14.0 |
| * 12 | 4 | 350. | 1352. | 0. | 6009. | 900. | 0. | 5166. | 6793. | 0. | 0. | 0. | .76 | 65. | 19.9 | C | 19.2 | 14.0 |
| * 13 | 4 | 350. | 0. | 0. | 6009. | 0. | 0. | 5166. | 7010. | 0. | 0. | 0. | .74 | 65. | 19.9 | C | 19.2 | 14.0 |
| * 14 | 4 | 350. | 0. | 883. | 6009. | 0. | 752. | 5166. | 6883. | 0. | 0. | 0. | .75 | 65. | 19.9 | C | 19.2 | 14.0 |
| * 15 | 3 | 700. | 0. | 0. | 5126. | 0. | 0. | 4413. | 6000. | 0. | 0. | 0. | .74 | 64. | 22.8 | C | 19.4 | 13.8 |
| * 16 | 3 | 900. | 122. | 0. | 5248. | 122. | 0. | 4535. | 5977. | 0. | 0. | 0. | .76 | 64. | 23.6 | C | 19.6 | 13.7 |
| * 17 | 3 | 1400. | 353. | 0. | 5601. | 353. | 0. | 4888. | 5932. | 0. | 0. | 0. | .82 | 62. | 26.1 | D | 20.4 | 13.1 |
| * 18 | 3 | 200. | 0. | 0. | 5601. | 0. | 0. | 4888. | 6000. | 0. | 0. | 0. | .81 | 63. | 26.0 | C | 20.2 | 13.2 |
| * 19 | 3 | 1400. | 0. | 203. | 5601. | 0. | 177. | 4888. | 5973. | 0. | 0. | 0. | .82 | 63. | 26.0 | D | 20.3 | 13.2 |
| * 20 | 3 | 900. | 0. | 0. | 5398. | 0. | 0. | 4711. | 6000. | 0. | 0. | 0. | .79 | 63. | 24.7 | C | 19.8 | 13.5 |
| * 21 | 4 | 100. | 283. | 0. | 5681. | 283. | 0. | 4994. | 6093. | 0. | 0. | 0. | .82 | 65. | 19.2 | C | 19.2 | 14.0 |
| * 22 | 4 | 100. | 0. | 127. | 5681. | 0. | 111. | 4994. | 6133. | 0. | 0. | 0. | .81 | 65. | 19.2 | C | 19.2 | 14.0 |
| * 23 | 3 | 600. | 0. | 0. | 5554. | 0. | 0. | 4883. | 6000. | 0. | 0. | 0. | .81 | 63. | 25.9 | C | 20.2 | 13.2 |
| * 24 | 3 | 1500. | 564. | 0. | 6118. | 564. | 0. | 5447. | 5884. | 0. | 0. | 0. | .93 | 58. | 31.5 | D | 22.3 | 11.9 |
| * 25 | 3 | 1500. | 0. | 0. | 6118. | 0. | 0. | 5447. | 6000. | 0. | 0. | 0. | .91 | 59. | 30.9 | D | 22.0 | 12.1 |
| * 26 | 3 | 8000. | 0. | 0. | 6118. | 0. | 0. | 5447. | 6000. | 0. | 0. | 0. | .91 | 59. | 30.9 | D | 22.0 | 12.1 |
| * 27 | 5 | 100. | 1253. | 0. | 7371. | 1253. | 0. | 6700. | 10000. | 0. | 0. | 0. | .67 | 65. | 20.6 | C | 19.2 | 14.0 |
| * 28 | 5 | 1000. | 0. | 0. | 7371. | 0. | 0. | 6700. | 7750. | 0. | 0. | 0. | .86 | 65. | 20.6 | C | 19.2 | 14.0 |
| * 29 | 5 | 1000. | 0. | 7371. | 7371. | 0. | 6700. | 6700. | 9685. | 0. | 0. | 0. | .69 | 65. | 20.6 | C | 19.2 | 14.0 |

* TOTAL 135469. = 25.7 MI LES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 49. 39.1 22.9 11.7

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 UNIVERSITY OF CALIFORNIA, BERKELEY SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 2

| | CURRENT TIME SLICE | | CUMULATIVE VALUES | | | | | |
|----------------------------|--------------------|------------|-------------------|----------|---------|------------|---------|----------|
| FREEWAY TRAVEL TIME = | 3173. | VEH-HRS | 3187. | PASS-HRS | 5309. | VEH-HRS | 5333. | PASS-HRS |
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 317. | VEH-HRS | 317. | PASS-HRS | 350. | VEH-HRS | 350. | PASS-HRS |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 3490. | VEH-HRS | 3504. | PASS-HRS | 5659. | VEH-HRS | 5683. | PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 155596. | VEH-MI. | 156426. | PASS-MI. | 288372. | VEH-MI. | 289918. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 45. | MPH | | | 54. | MPH | | |
| AVERAGE DENSITY = | 39. | VPMP | | | 33. | VPMP | | |
| TOTAL FUEL = | 6902. | GALLONS | | | 13396. | GALLONS | | |
| TOTAL EMISSIONS = | 1861. | KI LOGRAMS | | | 3599. | KI LOGRAMS | | |

US-101_SB_AM_P2_2040_PE

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|--------|------------|-------|------------|-------|------------|-------|
| 1 | 0.38 | 2 | 558.14 | 3 | 11.84 | 4 | 3.73 | 5 | 5.91 |
| 6 | 37.19 | 7 | 58.14 | 8 | 49.15 | 9 | 27.12 | 10 | 6.48 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.08 |
| 16 | 0.18 | 17 | 0.82 | 18 | 0.10 | 19 | 0.77 | 20 | 0.29 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.31 | 24 | 3.01 | 25 | 2.53 |
| 26 | 13.51 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 779.7 VEH-HRS ***** AVERAGE DELAY = 7.87 MIN/VEH *****

***** RAMP DELAYS *****

| | | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|---------|---|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|
| ON-RAMP | 2 | RAMP | 50. | 25.00 | 3.88 | 8.93 | 0.55 | 2.90 | 3.60 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 50. | 25.00 | 3.88 | 8.93 | 0.55 | 2.90 | 3.60 |
| ON-RAMP | 3 | RAMP | 518. | 292.00 | 12.36 | 104.27 | 6.47 | 33.83 | 42.09 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 518. | 292.00 | 12.36 | 104.27 | 6.47 | 33.83 | 42.09 |


```

**
** 19 2 3000. 1400. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks SB Off-Ramp **
**
** 20 2 3000. 900. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks SB/ Fair Oaks **
**
*****

```

FREEWAY AND ARTERIAL DESIGN FEATURES

```

*****
**
** SUB NO. SSEC SSEC DESIG N ORG TRK SSEC PCT PCT DES SPECIAL FF.SPD. CAP. ART GRADE SUBSECTI ON LOCATI ON **
** SEC LNS CAP LENGTH SPEED DES FAC GRAD TRK TRUCKS RAMP ALT. RTE ALT. RTE TYPE ALT. RTE **
**
** 21 2 3000. 100. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Fair Oaks SB On-Ramp **
**
** 22 2 3000. 100. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks NB Off-Ramp **
**
** 23 2 3000. 600. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks NB/ Fair Oaks **
**
** 24 2 3000. 1500. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Oaks On-Ramp to Mid **
**
** 25 2 3000. 1500. 65 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Mid to Lawrence Off-ramp **
**
** 26 2 3000. 8000. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 HOV Dummy **
**
** 27 **
** 28 **
** 29 **
*****

```

FREEWAY TRAVEL TIME (MINUTES)

```

*****
* O R I G I N S D E S T I N A T I O N S A C R O S S
* D O W N
* 1 2 3 4 5 6 7
+
*
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 2 * 0.00 19.74 20.05 20.86 21.05 23.08 0.00
+
* 3 * 0.00 0.00 0.00 0.00 1.96 3.99 0.00
+
* 4 * 0.00 0.00 0.00 0.00 0.00 3.21 0.00
+
* 5 * 0.00 0.00 0.00 0.00 0.00 2.90 0.00
+
* 6 * 0.00 0.00 0.00 0.00 0.00 2.74 0.00
+
* 7 * 0.00 0.00 0.00 0.00 0.00 2.06 0.00
+
* 8 * 0.00 0.00 0.00 0.00 0.00 1.92 0.00
+
* 9 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 10 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
+
* 11 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00
*
*****

```

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB SEC | NO. LNS | SSEC LENGTH | O-D ORG | DATA DES | DEMANDS SSEC | ADJUSTED ORG | VOLUMES DES | SSEC SSEC | WEAVE CAP | CONGEST EFF | STORAGE LENGTH | V/C RATE | SPEED RATIO | DENSITY MPH | LOS VPMP | FUEL LEVEL | EMI SS MPG |
|---------|---------|-------------|---------|----------|--------------|--------------|-------------|-----------|-----------------|----------------|----------------|----------|-------------|-------------|----------|------------|------------|
| 1 | | | | | | | | | | | | | | | | | |
| 2 | 2 | 99999 | 1071 | 0 | 1071 | 1071 | 0 | 1071 | 3000 | 0 | 0 | 0 | .36 | 65 | 8.2 | A | 20.0 |
| 3 | 2 | 2740 | 0 | 0 | 1071 | 0 | 0 | 1071 | 3000 | 0 | 0 | 0 | .36 | 65 | 8.2 | A | 20.0 |
| 4 | 2 | 600 | 0 | 0 | 1071 | 0 | 0 | 1071 | 3000 | 0 | 0 | 0 | .36 | 65 | 8.2 | A | 20.0 |
| 5 | 2 | 700 | 0 | 0 | 1071 | 0 | 0 | 1071 | 3000 | 0 | 0 | 0 | .36 | 65 | 8.2 | A | 20.0 |
| 6 | 2 | 2630 | 0 | 0 | 1071 | 0 | 0 | 1071 | 3000 | 0 | 0 | 0 | .36 | 65 | 8.2 | A | 20.0 |
| 7 | 2 | 2530 | 0 | 0 | 1071 | 0 | 0 | 1071 | 3000 | 0 | 0 | 0 | .36 | 65 | 8.2 | A | 20.0 |
| 8 | 2 | 1500 | 32 | 0 | 1103 | 32 | 0 | 1103 | 3000 | 0 | 0 | 0 | .37 | 65 | 8.5 | A | 20.0 |
| 9 | 2 | 700 | 0 | 0 | 1103 | 0 | 0 | 1103 | 3000 | 0 | 0 | 0 | .37 | 65 | 8.5 | A | 20.0 |
| 10 | 2 | 1500 | 0 | 320 | 1103 | 0 | 320 | 1103 | 3000 | 0 | 0 | 0 | .37 | 65 | 8.5 | A | 20.0 |
| 11 | 2 | 750 | 0 | 0 | 784 | 0 | 0 | 784 | 3000 | 0 | 0 | 0 | .26 | 65 | 6.0 | A | 20.0 |
| 12 | 2 | 350 | 154 | 0 | 937 | 154 | 0 | 937 | 3000 | 0 | 0 | 0 | .31 | 65 | 7.2 | A | 20.0 |
| 13 | 2 | 350 | 0 | 0 | 937 | 0 | 0 | 937 | 3000 | 0 | 0 | 0 | .31 | 65 | 7.2 | A | 20.0 |
| 14 | 2 | 350 | 0 | 96 | 937 | 0 | 96 | 937 | 3000 | 0 | 0 | 0 | .31 | 65 | 7.2 | A | 20.0 |
| 15 | 2 | 700 | 0 | 0 | 841 | 0 | 0 | 841 | 3000 | 0 | 0 | 0 | .28 | 65 | 6.5 | A | 20.0 |
| 16 | 2 | 900 | 17 | 0 | 858 | 17 | 0 | 858 | 3000 | 0 | 0 | 0 | .29 | 65 | 6.6 | A | 20.0 |
| 17 | 2 | 1400 | 49 | 0 | 907 | 49 | 0 | 907 | 3000 | 0 | 0 | 0 | .30 | 65 | 7.0 | A | 20.0 |
| 18 | 2 | 200 | 0 | 0 | 907 | 0 | 0 | 907 | 3000 | 0 | 0 | 0 | .30 | 65 | 7.0 | A | 20.0 |
| 19 | 2 | 1400 | 0 | 37 | 907 | 0 | 37 | 907 | 3000 | 0 | 0 | 0 | .30 | 65 | 7.0 | A | 20.0 |
| 20 | 2 | 900 | 0 | 0 | 870 | 0 | 0 | 870 | 3000 | 0 | 0 | 0 | .29 | 65 | 6.7 | A | 20.0 |
| 21 | 2 | 100 | 42 | 0 | 912 | 42 | 0 | 912 | 3000 | 0 | 0 | 0 | .30 | 65 | 7.0 | A | 20.0 |
| 22 | 2 | 100 | 0 | 12 | 912 | 0 | 12 | 912 | 3000 | 0 | 0 | 0 | .30 | 65 | 7.0 | A | 20.0 |
| 23 | 2 | 600 | 0 | 0 | 900 | 0 | 0 | 900 | 3000 | 0 | 0 | 0 | .30 | 65 | 6.9 | A | 20.0 |
| 24 | 2 | 1500 | 104 | 0 | 1004 | 104 | 0 | 1004 | 3000 | 0 | 0 | 0 | .33 | 65 | 7.7 | A | 20.0 |
| 25 | 2 | 1500 | 0 | 0 | 1004 | 0 | 0 | 1004 | 3000 | 0 | 0 | 0 | .33 | 65 | 7.7 | A | 20.0 |
| 26 | 2 | 8000 | 0 | 1004 | 1004 | 0 | 1004 | 1004 | 3000 | 0 | 0 | 0 | .33 | 65 | 7.7 | A | 20.0 |
| 27 | | | | | | | | | | | | | | | | | |
| 28 | | | | | | | | | | | | | | | | | |
| 29 | | | | | | | | | | | | | | | | | |
| TOTAL | 131999 | = | 25.0 | MI | LES | | | | MAX(V/C) = 0.37 | LOWEST LOS = A | | | AVG = 65 | 8.1 | | 20.0 | 13.7 |

| | | | | | |
|-----------------------------|----------------|----------------|-------------------|----------------|---------------|
| FREEWAY TRAVEL TIME = | 406. VEH-HRS | 811. PASS-HRS | CUMULATIVE VALUES | 406. VEH-HRS | 811. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | |
| OFF-RAMP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS | 0. PASS-HRS | |
| TOTAL SYSTEM TRAVEL TIME = | 406. VEH-HRS | 811. PASS-HRS | 406. VEH-HRS | 811. PASS-HRS | |
| TOTAL FRWAY TRAV DISTANCE = | 26371. VEH-MI | 52742. PASS-MI | 26371. VEH-MI | 52742. PASS-MI | |
| AVERAGE SYSTEM SPEED = | 65. MPH | | 65. MPH | | |
| AVERAGE DENSITY = | 8. VPMP | | 8. VPMP | | |
| TOTAL FUEL = | 1319. GALLONS | | 1319. GALLONS | | |
| TOTAL EMISSIONS = | 362. KILOGRAMS | | 362. KILOGRAMS | | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

** FREEWAY TRAVEL TIME (MINUTES) **

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | |
|--------------|---------------------|-------|-------|-------|-------|-------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 1 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2 | 0.00 | 19.74 | 20.05 | 20.86 | 21.05 | 23.08 | 0.00 |
| 3 | 0.00 | 0.00 | 0.00 | 0.00 | 1.96 | 3.99 | 0.00 |

| | * | 4 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.21 | 0.00 | | | | | | |
|---|---|----|---|------|------|------|------|------|------|------|------|------|--|--|--|--|--|--|
| + | | | | | | | | | | | | | | | | | | |
| | * | 5 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.90 | 0.00 | | | | | | | |
| + | | | | | | | | | | | | | | | | | | |
| | * | 6 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.74 | 0.00 | | | | | | | |
| + | | | | | | | | | | | | | | | | | | |
| | * | 7 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.06 | 0.00 | | | | | | | |
| + | | | | | | | | | | | | | | | | | | |
| | * | 8 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.92 | 0.00 | | | | | | | |
| + | | | | | | | | | | | | | | | | | | |
| | * | 9 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | | | | | | |
| + | | | | | | | | | | | | | | | | | | |
| | * | 10 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | | | | | | |
| + | | | | | | | | | | | | | | | | | | |
| | * | 11 | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | | | | | | | |
| + | | | | | | | | | | | | | | | | | | |
| | * | * | * | | | | | | | | | | | | | | | |
| | * | * | * | | | | | | | | | | | | | | | |

 *
 * TIME SLICE FREEWAY PERFORMANCE TABLE *
 *
 *
 * SUB NO. SSEC O-D DATA DEMANDS ADJUSTED VOLUMES SSEC WEAVE CONGEST STORAGE V/C SPEED DENSITY LOS FUEL EMI SS *
 * SEC LNS LENGTH ORG DES SSEC ORG DES SSEC CAP. EFF LENGTH RATE RATIO MPH VPMPL LEVEL MPG GS/VM *
 *
 * 1 *
 * 2 2 99999. 1275. 0. 1275. 1275. 0. 1275. 3000. 0. 0. 0. .43 65. 9.8 A 20.0 13.7 *
 * 3 2 2740. 0. 0. 1275. 0. 0. 1275. 3000. 0. 0. 0. .43 65. 9.8 A 20.0 13.7 *
 * 4 2 600. 0. 0. 1275. 0. 0. 1275. 3000. 0. 0. 0. .43 65. 9.8 A 20.0 13.7 *
 * 5 2 700. 0. 0. 1275. 0. 0. 1275. 3000. 0. 0. 0. .43 65. 9.8 A 20.0 13.7 *
 * 6 2 2630. 0. 0. 1275. 0. 0. 1275. 3000. 0. 0. 0. .43 65. 9.8 A 20.0 13.7 *
 * 7 2 2530. 0. 0. 1275. 0. 0. 1275. 3000. 0. 0. 0. .43 65. 9.8 A 20.0 13.7 *
 * 8 2 1500. 43. 0. 1318. 43. 0. 1318. 3000. 0. 0. 0. .44 65. 10.1 A 20.0 13.7 *
 * 9 2 700. 0. 0. 1318. 0. 0. 1318. 3000. 0. 0. 0. .44 65. 10.1 A 20.0 13.7 *
 * 10 2 1500. 0. 375. 1318. 0. 375. 1318. 3000. 0. 0. 0. .44 65. 10.1 A 20.0 13.7 *
 * 11 2 750. 0. 0. 943. 0. 0. 943. 3000. 0. 0. 0. .31 65. 7.3 A 20.0 13.7 *
 * 12 2 350. 217. 0. 1160. 217. 0. 1160. 3000. 0. 0. 0. .39 65. 8.9 A 20.0 13.7 *
 * 13 2 350. 0. 0. 1160. 0. 0. 1160. 3000. 0. 0. 0. .39 65. 8.9 A 20.0 13.7 *
 * 14 2 350. 0. 127. 1160. 0. 127. 1160. 3000. 0. 0. 0. .39 65. 8.9 A 20.0 13.7 *
 * 15 2 700. 0. 0. 1033. 0. 0. 1033. 3000. 0. 0. 0. .34 65. 7.9 A 20.0 13.7 *
 * 16 2 900. 23. 0. 1057. 23. 0. 1057. 3000. 0. 0. 0. .35 65. 8.1 A 20.0 13.7 *
 * 17 2 1400. 68. 0. 1124. 68. 0. 1124. 3000. 0. 0. 0. .37 65. 8.6 A 20.0 13.7 *
 * 18 2 200. 0. 0. 1124. 0. 0. 1124. 3000. 0. 0. 0. .37 65. 8.6 A 20.0 13.7 *
 * 19 2 1400. 0. 27. 1124. 0. 27. 1124. 3000. 0. 0. 0. .37 65. 8.6 A 20.0 13.7 *
 * 20 2 900. 0. 0. 1098. 0. 0. 1098. 3000. 0. 0. 0. .37 65. 8.4 A 20.0 13.7 *
 * 21 2 100. 57. 0. 1154. 57. 0. 1154. 3000. 0. 0. 0. .38 65. 8.9 A 20.0 13.7 *
 * 22 2 100. 0. 17. 1154. 0. 17. 1154. 3000. 0. 0. 0. .38 65. 8.9 A 20.0 13.7 *
 * 23 2 600. 0. 0. 1138. 0. 0. 1138. 3000. 0. 0. 0. .38 65. 8.8 A 20.0 13.7 *
 * 24 2 1500. 116. 0. 1253. 116. 0. 1253. 3000. 0. 0. 0. .42 65. 9.6 A 20.0 13.7 *
 * 25 2 1500. 0. 0. 1253. 0. 0. 1253. 3000. 0. 0. 0. .42 65. 9.6 A 20.0 13.7 *
 * 26 2 8000. 0. 1253. 1253. 0. 1253. 1253. 3000. 0. 0. 0. .42 65. 9.6 A 20.0 13.7 *
 * 27 *
 * 28 *
 * 29 *
 *
 *
 *
 * TOTAL 131999. = 25.0 MILES MAX(V/C) = 0.44 LOWEST LOS = A AVG = 65. 9.7 20.0 13.7 *
 *
 *

| | | | | | |
|-----------------------------|--------|--------------------|--------|-------------------|--------|
| | | CURRENT TIME SLICE | | CUMULATIVE VALUES | |
| FREWAY TRAVEL TIME = | 486. | VEH-HRS | 972. | PASS-HRS | 892. |
| FREWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. |
| OFF-RAMP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. |
| TOTAL SYSTEM TRAVEL TIME = | 486. | VEH-HRS | 972. | PASS-HRS | 892. |
| TOTAL FRWAY TRAV DISTANCE = | 31588. | VEH-MI. | 63175. | PASS-MI. | 57959. |
| AVERAGE SYSTEM SPEED = | 65. | MPH. | | | 65. |
| AVERAGE DENSITY = | 10. | VPMPPL | | | 9. |
| TOTAL FUEL = | 1579. | GALLONS | | | 2898. |
| TOTAL EMISSIONS = | 434. | KILOGRAMS | | | 796. |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****
US-101_SB_AM_P2_2040_PL

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FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQQ QQQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP EEE
FFF RRR RRR EEE Q*UC* QQQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*QQ 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP EEEEEEEEE
    
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FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREWAY AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT TRUCKS | DES TRUCKS | SPECIAL RAMP | FF. SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION LOCATION |
|---------|----------|----------|-------------|--------------|---------|---------|-----------|---------|------------|------------|--------------|-------------------|---------------|----------|----------------|-------------------------|
| ** 1 | 5 | 10000. | 1370. | 65 | OD | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Seeding |
| ** 2 | 3 | 7360. | 99999. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Queue Capture |
| ** 3 | 3 | 6000. | 2740. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | SR-85 Off to Shore On |
| ** 4 | 3 | 6000. | 600. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Shore. On to Moffet Off |
| ** 5 | 3 | 6000. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Moffett Off to On |
| ** 6 | 3 | 6000. | 2630. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Moffett On to Ellis Off |
| ** 7 | 3 | 6000. | 2530. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Ellis Off to On-ramp |
| ** 8 | 4 | 6770. | 1500. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Ellis On-ramp |
| ** 9 | 4 | 6770. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Ellis / US 237 |
| ** 10 | 4 | 6770. | 1500. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | SR-237 EB Off-Ramp |
| ** 11 | 3 | 6000. | 750. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | SR-237 / SR-237 |
| ** 12 | 4 | 6880. | 350. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | SR-237 EB On-Ramp |
| ** 13 | 4 | 6880. | 350. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | US 237 / Mathilda |
| ** 14 | 4 | 6880. | 350. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Mathilda Off-Ramp |
| ** 15 | 3 | 6000. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Mathilda / Mathilda |
| ** 16 | 3 | 6000. | 900. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Mathilda SB On-Ramp |
| ** 17 | 3 | 6000. | 1400. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Mathilda NB On-Ramp |
| ** 18 | 3 | 6000. | 200. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Mathilda / Fair Oaks |
| ** 19 | 3 | 6000. | 1400. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Fair Oaks SB Off-Ramp |
| ** 20 | 3 | 6000. | 900. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0.0 | 0.0 | GOOD | 0.0 | Fair Oaks SB/ Fair Oaks |

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB SEC | NO. LNS | SSEC LENGTH | O-D ORG | DATA DES | DEMANDS SSEC | ADJUSTED ORG | VOLUMES DES | SSEC SSEC | WEAVE CAP. | CONGEST EFF | STORAGE LENGTH | V/C RATE | SPEED MPH | DENSITY VPMP | LOS LEVEL | FUEL MPG | EMI SS GS/VM | | |
|---------|---------|-------------|---------|----------|--------------|--------------|-------------|-----------|------------|-------------|-----------------|----------------|-----------|--------------|-----------|----------|--------------|------|------|
| * | 1 | 5 | 1370. | 9199. | 1840. | 9199. | 9199. | 1840. | 9199. | 10000. | 0. | 0. | 0. | .92 | 58. | 31.7 | D | 22.2 | 12.0 |
| * | 2 | 3 | 99999. | 0. | 0. | 7359. | 0. | 0. | 6000. | 7360. | 0. | * 21659. | 1359. | .82 | 41. | 49.0 | F | 22.5 | 12.0 |
| * | 3 | 3 | 2740. | 0. | 0. | 7359. | 0. | 0. | 6000. | 6000. | 0. | 0. | 0. | 1.00 | 52. | 38.3 | E | 23.8 | 11.1 |
| * | 4 | 3 | 600. | 0. | 0. | 7359. | 0. | 0. | 3055. | 6000. | 0. | * 413. | 2945. | .51 | 51. | 19.9 | F | 23.7 | 11.2 |
| * | 5 | 3 | 700. | 0. | 0. | 7359. | 0. | 0. | 3055. | 6000. | 0. | ** 700. | 2945. | .51 | 46. | 21.9 | F | 23.2 | 11.4 |
| * | 6 | 3 | 2630. | 0. | 0. | 7359. | 0. | 0. | 3055. | 6000. | 0. | ** 2630. | 2945. | .51 | 37. | 27.5 | F | 22.1 | 11.9 |
| * | 7 | 3 | 2530. | 0. | 0. | 7359. | 0. | 0. | 3055. | 6000. | 0. | ** 2530. | 2945. | .51 | 28. | 36.7 | F | 20.4 | 12.7 |
| * | 8 | 4 | 1500. | 643. | 0. | 8002. | 593. | 0. | 3648. | 6673. | 0. | ** 1500. | 2945. | .55 | 24. | 38.4 | F | 19.0 | 13.6 |
| * | 9 | 4 | 700. | 0. | 0. | 8002. | 0. | 0. | 3648. | 6770. | 0. | ** 700. | 2945. | .54 | 21. | 42.8 | F | 18.1 | 14.2 |
| * | 10 | 4 | 1500. | 0. | 1825. | 8002. | 0. | 1085. | 3648. | 6355. | 0. | ** 1500. | 2707. | .57 | 24. | 38.6 | F | 19.0 | 13.7 |
| * | 11 | 3 | 750. | 0. | 0. | 6177. | 0. | 0. | 2196. | 6000. | 0. | ** 750. | 2707. | .37 | 15. | 47.6 | F | 16.7 | 15.6 |
| * | 12 | 4 | 350. | 700. | 0. | 6877. | 650. | 0. | 2846. | 6740. | 0. | ** 350. | 2707. | .42 | 16. | 45.8 | F | 15.4 | 16.8 |
| * | 13 | 4 | 350. | 0. | 0. | 6877. | 0. | 0. | 2846. | 6880. | 0. | ** 350. | 2707. | .41 | 14. | 49.3 | F | 15.2 | 17.0 |
| * | 14 | 4 | 350. | 0. | 690. | 6877. | 0. | 560. | 2846. | 6742. | 0. | ** 350. | 2707. | .42 | 14. | 50.5 | F | 15.0 | 17.2 |
| * | 15 | 3 | 700. | 0. | 0. | 6187. | 0. | 0. | 2287. | 6000. | 0. | ** 700. | 2707. | .38 | 12. | 61.4 | F | 15.7 | 16.4 |
| * | 16 | 3 | 900. | 808. | 0. | 6995. | 708. | 0. | 2995. | 5818. | 0. | ** 900. | 2707. | .51 | 15. | 66.3 | F | 16.0 | 15.8 |
| * | 17 | 3 | 1400. | 302. | 0. | 7297. | 240. | 0. | 3235. | 5932. | 0. | ** 1400. | 2697. | .55 | 15. | 73.6 | F | 15.7 | 16.2 |
| * | 18 | 3 | 200. | 0. | 0. | 7297. | 0. | 0. | 3235. | 6000. | 0. | ** 200. | 2697. | .54 | 14. | 78.7 | F | 15.1 | 16.7 |
| * | 19 | 3 | 1400. | 0. | 488. | 7297. | 0. | 398. | 3235. | 5919. | 0. | ** 1400. | 2684. | .55 | 13. | 81.3 | F | 14.9 | 17.0 |
| * | 20 | 3 | 900. | 0. | 0. | 6809. | 0. | 0. | 2837. | 6000. | 0. | ** 900. | 2684. | .47 | 10. | 90.9 | F | 13.8 | 18.1 |
| * | 21 | 4 | 100. | 257. | 0. | 7066. | 240. | 0. | 3077. | 6187. | 0. | ** 100. | 2684. | .50 | 11. | 72.2 | F | 12.7 | 19.8 |
| * | 22 | 4 | 100. | 0. | 136. | 7066. | 0. | 112. | 3077. | 6226. | 0. | ** 100. | 2684. | .49 | 10. | 73.4 | F | 12.7 | 19.9 |
| * | 23 | 3 | 600. | 0. | 0. | 6930. | 0. | 0. | 2965. | 6000. | 0. | ** 600. | 2684. | .49 | 10. | 97.4 | F | 13.4 | 18.7 |
| * | 24 | 3 | 1500. | 224. | 0. | 7154. | 224. | 0. | 3189. | 5944. | 0. | ** 1500. | 2684. | .54 | 10. | 101.9 | F | 13.2 | 19.0 |
| * | 25 | 3 | 1500. | 0. | 0. | 7154. | 0. | 0. | 3189. | 6000. | 0. | ** 1500. | 2684. | .53 | 9. | 113.4 | F | 12.4 | 20.1 |
| * | 26 | 3 | 8000. | 0. | 0. | 7154. | 0. | 0. | 3189. | 6000. | 0. | ** 8000. | 2684. | .53 | 7. | 151.6 | F | 10.4 | 23.6 |
| * | 27 | 5 | 100. | 1789. | 0. | 8943. | 1789. | 0. | 4978. | 10000. | 0. | ** 100. | 2684. | .50 | 5. | 202.7 | F | 8.6 | 28.0 |
| * | 28 | 5 | 1000. | 1560. | 0. | 10503. | 1212. | 0. | 6190. | 7750. | 0. | ** 1000. | 1560. | .80 | 12. | 100.6 | F | 14.4 | 20.9 |
| * | 29 | 5 | 1000. | 1560. | 12063. | 12063. | 1560. | 7750. | 7750. | 7750. | 0. | 0. | 0. | 1.00 | 52. | 29.7 | E | 23.8 | 11.1 |
| * | TOTAL | 135469. | = | 25.7 | MI LES | | | | | | MAX(V/C) = 1.00 | LOWEST LOS = F | AVG = 31. | 56.5 | | 20.9 | 12.8 | | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREWAY TRAVEL TIME = | 5515. VEH-HRS | 5555. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 314. VEH-HRS | 348. PASS-HRS |
| OFF-RAMP DELAY = | 183. VEH-HRS | 184. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 6011. VEH-HRS | 6088. PASS-HRS |
| TOTAL TRAV DISTANCE = | 170587. VEH-MI. | 171677. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 28. MPH | 31. MPH |
| AVERAGE DENSITY = | 56. VPMP | 56. VPMP |
| TOTAL FUEL = | 8341. GALLONS | 8341. GALLONS |
| TOTAL EMISSIONS = | 2249. KI LOGRAMS | 2249. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|--------|------------|-------|------------|-------|------------|-------|------------|--------|
| 1 | 4.39 | 2 | ***** | 3 | 11.72 | 4 | 2.86 | 5 | 4.84 |
| 6 | 33.28 | 7 | 54.54 | 8 | 44.81 | 9 | 24.23 | 10 | 43.59 |
| 11 | 29.08 | 12 | 15.29 | 13 | 16.65 | 14 | 16.98 | 15 | 34.40 |
| 16 | 40.12 | 17 | 66.47 | 18 | 10.19 | 19 | 73.20 | 20 | 56.25 |
| 21 | 6.36 | 22 | 6.47 | 23 | 38.94 | 24 | 96.97 | 25 | 106.45 |
| 26 | 704.43 | 27 | 18.02 | 28 | 77.66 | 29 | 5.53 | | |

***** TOTAL DELAY = 2890.1 VEH-HRS ***** AVERAGE DELAY = 42.97 MIN/VEH *****

***** RAMP DELAYS *****

| QUEUE LENGTH VEHCLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|----------------------|---------------|--------------------------------|----------|---------|---------|----------|----------------------|
|----------------------|---------------|--------------------------------|----------|---------|---------|----------|----------------------|

| US-101_SB_PM_NP_2040_PE | | | | | | | | | | | | | | | | | | | | | |
|-------------------------|----|---|-------|-------|-------|-------|-------|-------|-------|--------|----|----|-------|-------|------|-----|-------|---|------|------|---|
| * | 9 | 4 | 700. | 0. | 0. | 7512. | 0. | 0. | 5393. | 6770. | 0. | ** | 700. | 1279. | .80 | 12. | 112.7 | F | 14.2 | 21.2 | * |
| * | 10 | 4 | 1500. | 0. | 1788. | 7512. | 0. | 1098. | 5393. | 6368. | 0. | ** | 1500. | 975. | .85 | 14. | 95.6 | F | 15.6 | 19.5 | * |
| * | 11 | 3 | 750. | 0. | 0. | 5724. | 0. | 0. | 3875. | 6000. | 0. | ** | 750. | 975. | .65 | 7. | 172.6 | F | 10.3 | 25.8 | * |
| * | 12 | 4 | 350. | 681. | 0. | 6405. | 681. | 0. | 4556. | 6751. | 0. | ** | 350. | 975. | .67 | 8. | 139.3 | F | 10.9 | 24.9 | * |
| * | 13 | 4 | 350. | 0. | 0. | 6405. | 0. | 0. | 4556. | 6880. | 0. | ** | 350. | 975. | .66 | 8. | 144.8 | F | 10.6 | 25.3 | * |
| * | 14 | 4 | 350. | 0. | 722. | 6405. | 0. | 625. | 4556. | 6738. | 0. | ** | 350. | 975. | .68 | 8. | 138.7 | F | 11.0 | 24.9 | * |
| * | 15 | 3 | 700. | 0. | 0. | 5683. | 0. | 0. | 3930. | 6000. | 0. | ** | 700. | 975. | .66 | 8. | 170.2 | F | 10.5 | 25.5 | * |
| * | 16 | 3 | 900. | 859. | 0. | 6542. | 859. | 0. | 4789. | 5814. | 0. | ** | 900. | 975. | .82 | 13. | 122.2 | F | 14.9 | 20.4 | * |
| * | 17 | 3 | 1400. | 321. | 0. | 6863. | 283. | 0. | 5072. | 5930. | 0. | ** | 1400. | 858. | .86 | 15. | 116.4 | F | 15.9 | 19.2 | * |
| * | 18 | 3 | 200. | 0. | 0. | 6863. | 0. | 0. | 5072. | 6000. | 0. | ** | 200. | 858. | .85 | 14. | 120.4 | F | 15.6 | 19.6 | * |
| * | 19 | 3 | 1400. | 0. | 606. | 6863. | 0. | 520. | 5072. | 5904. | 0. | ** | 1400. | 832. | .86 | 15. | 115.0 | F | 16.1 | 19.1 | * |
| * | 20 | 3 | 900. | 0. | 0. | 6257. | 0. | 0. | 4552. | 6000. | 0. | ** | 900. | 832. | .76 | 11. | 143.1 | F | 13.5 | 22.3 | * |
| * | 21 | 4 | 100. | 274. | 0. | 6531. | 240. | 0. | 4792. | 6184. | 0. | ** | 100. | 832. | .77 | 11. | 107.3 | F | 13.8 | 21.9 | * |
| * | 22 | 4 | 100. | 0. | 193. | 6531. | 0. | 165. | 4792. | 6218. | 0. | ** | 100. | 832. | .77 | 11. | 108.8 | F | 13.7 | 22.0 | * |
| * | 23 | 3 | 600. | 0. | 0. | 6338. | 0. | 0. | 4627. | 6000. | 0. | ** | 600. | 832. | .77 | 11. | 139.8 | F | 13.7 | 22.0 | * |
| * | 24 | 3 | 1500. | 200. | 0. | 6538. | 200. | 0. | 4827. | 5950. | 0. | ** | 1500. | 832. | .81 | 13. | 128.3 | F | 14.6 | 20.8 | * |
| * | 25 | 3 | 1500. | 0. | 0. | 6538. | 0. | 0. | 4827. | 6000. | 0. | ** | 1500. | 832. | .80 | 12. | 131.1 | F | 14.4 | 21.0 | * |
| * | 26 | 3 | 8000. | 0. | 0. | 6538. | 0. | 0. | 4827. | 6000. | 0. | ** | 8000. | 832. | .80 | 12. | 131.1 | F | 14.4 | 21.0 | * |
| * | 27 | 5 | 100. | 1635. | 0. | 8173. | 1635. | 0. | 6462. | 10000. | 0. | ** | 100. | 832. | .65 | 7. | 172.5 | F | 10.3 | 25.7 | * |
| * | 28 | 5 | 1000. | 520. | 0. | 8693. | 768. | 0. | 7230. | 7750. | 0. | ** | 1000. | 520. | .93 | 19. | 75.6 | F | 18.1 | 16.6 | * |
| * | 29 | 5 | 1000. | 520. | 9213. | 9213. | 520. | 7750. | 7750. | 7750. | 0. | ** | 0. | 0. | 1.00 | 52. | 29.7 | E | 23.8 | 11.1 | * |

 * TOTAL 135469. = 25.7 MI L E S MAX(V/C) = 1.00 LOWEST LOS = F AVG = 20. 82.3 16.9 16.1 *

| CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | | |
|----------------------------|---------|------------|---------|-------------------|---------|------------|---------|----------|
| FREEWAY TRAVEL TIME = | 7740. | VEH-HRS | 7776. | PASS-HRS | 13255. | VEH-HRS | 13332. | PASS-HRS |
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 539. | VEH-HRS | 584. | PASS-HRS | 853. | VEH-HRS | 932. | PASS-HRS |
| OFF-RAMP DELAY = | 577. | VEH-HRS | 579. | PASS-HRS | 760. | VEH-HRS | 763. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 8856. | VEH-HRS | 8939. | PASS-HRS | 14867. | VEH-HRS | 15027. | PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 152275. | VEH-MI. | 153374. | PASS-MI. | 322861. | VEH-MI. | 325051. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 17. | MPH | | | 24. | MPH | | |
| AVERAGE DENSITY = | 82. | VPMP/L | | | 69. | VPMP/L | | |
| TOTAL FUEL = | 9387. | GALLONS | | | 17728. | GALLONS | | |
| TOTAL EMISSIONS = | 2612. | KI LOGRAMS | | | 4860. | KI LOGRAMS | | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|--------|------------|--------|------------|--------|------------|-------|------------|-------|
| 1 | 2.07 | 2 | ***** | 3 | 162.74 | 4 | 37.98 | 5 | 44.38 |
| 6 | 166.75 | 7 | 160.41 | 8 | 99.86 | 9 | 48.77 | 10 | 85.02 |
| 11 | 65.09 | 12 | 32.28 | 13 | 33.74 | 14 | 32.13 | 15 | 59.67 |
| 16 | 49.91 | 17 | 71.93 | 18 | 10.73 | 19 | 70.75 | 20 | 61.24 |
| 21 | 6.73 | 22 | 6.84 | 23 | 39.58 | 24 | 88.22 | 25 | 90.65 |
| 26 | 483.44 | 27 | 14.45 | 28 | 50.52 | 29 | 5.53 | | |

***** TOTAL DELAY = 5397.8 VEH-HRS ***** AVERAGE DELAY = 68.01 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH | DELAY | AVERAGE | GAS | HC | CO | NOX | TOTAL |
|------------|--------------|---------|----------------|-------|--------|-------|-------|-----------|
| | VEHICLES | VEH-HRS | METERING DELAY | GALS | KGMS | KGMS | KGMS | EMISSIONS |
| | | | MINUTES | | | | | KGMS |
| ON-RAMP 2 | RAMP | 50. | 50.00 | 4.16 | 17.85 | 1.11 | 5.79 | 7.21 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 50. | 50.00 | 4.16 | 17.85 | 1.11 | 5.79 | 7.21 |
| ON-RAMP 3 | RAMP | 50. | 50.00 | 4.10 | 17.85 | 1.11 | 5.79 | 7.21 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 50. | 50.00 | 4.10 | 17.85 | 1.11 | 5.79 | 7.21 |
| ON-RAMP 4 | RAMP | 100. | 100.00 | 6.26 | 35.71 | 2.22 | 11.58 | 14.41 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 100.00 | 6.26 | 35.71 | 2.22 | 11.58 | 14.41 |
| ON-RAMP 5 | RAMP | 100. | 81.00 | 12.69 | 28.92 | 1.79 | 9.38 | 11.68 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 81.00 | 12.69 | 28.92 | 1.79 | 9.38 | 11.68 |
| ON-RAMP 6 | RAMP | 51. | 34.00 | 7.01 | 12.14 | 0.75 | 3.94 | 4.90 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 51. | 34.00 | 7.01 | 12.14 | 0.75 | 3.94 | 4.90 |
| ON-RAMP 9 | RAMP | 100. | 224.00 | 17.59 | 79.99 | 4.96 | 25.95 | 32.29 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 224.00 | 17.59 | 79.99 | 4.96 | 25.95 | 32.29 |
| OFF-RAMP 2 | OUTPUT POINT | 786. | 576.53 | | 205.87 | 12.77 | 66.79 | 83.10 |

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FREEWAY TRAVEL TIME = 9435. VEH-HRS 9471. PASS-HRS 22690. VEH-HRS 22803. PASS-HRS
 FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
 ON-RAMP MRG/CAP DELAY = 440. VEH-HRS 460. PASS-HRS 1293. VEH-HRS 1392. PASS-HRS
 OFF-RAMP DELAY = 968. VEH-HRS 972. PASS-HRS 1728. VEH-HRS 1735. PASS-HRS
 TOTAL SYSTEM TRAVEL TIME = 10843. VEH-HRS 10903. PASS-HRS 25711. VEH-HRS 25930. PASS-HRS
 TOTAL TRAV DISTANCE = 138567. VEH-MI. 139616. PASS-MI. 461428. VEH-MI. 464667. PASS-MI.
 AVERAGE SYSTEM SPEED = 13. MPH. 20. MPH.
 AVERAGE DENSITY = 109. VPML 83. VPML
 TOTAL FUEL = 10008. GALLONS 27736. GALLONS
 TOTAL EMISSIONS = 2806. KI LOGRAMS 7666. KI LOGRAMS

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|--------|------------|--------|------------|--------|------------|-------|------------|-------|
| 1 | 0.64 | 2 | ***** | 3 | 168.04 | 4 | 36.81 | 5 | 42.95 |
| 6 | 161.37 | 7 | 155.23 | 8 | 103.89 | 9 | 50.23 | 10 | 90.17 |
| 11 | 66.35 | 12 | 31.96 | 13 | 33.61 | 14 | 32.31 | 15 | 58.28 |
| 16 | 53.63 | 17 | 77.80 | 18 | 11.47 | 19 | 76.44 | 20 | 64.12 |
| 21 | 7.10 | 22 | 7.17 | 23 | 41.57 | 24 | 91.06 | 25 | 93.97 |
| 26 | 501.15 | 27 | 15.04 | 28 | 56.88 | 29 | 5.53 | | |

***** TOTAL DELAY = 7303.4 VEH-HRS ***** AVERAGE DELAY = 91.36 MIN/VEH *****

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***** RAMP DELAYS *****

| | | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|------------|--------------|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|
| ON-RAMP 2 | RAMP | 50. | 50.00 | 5.24 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 50. | 50.00 | 5.24 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| ON-RAMP 3 | RAMP | 50. | 50.00 | 3.73 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 50. | 50.00 | 3.73 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| ON-RAMP 4 | RAMP | 100. | 100.00 | 7.68 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 100.00 | 7.68 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP 5 | RAMP | 100. | 100.00 | 16.90 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 100.00 | 16.90 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP 6 | RAMP | 29. | 40.00 | 8.92 | 14.28 | 0.89 | 4.63 | 0.25 | 5.77 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 29. | 40.00 | 8.92 | 14.28 | 0.89 | 4.63 | 0.25 | 5.77 |
| ON-RAMP 9 | RAMP | 100. | 100.00 | 8.57 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 100.00 | 8.57 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| OFF-RAMP 2 | OUTPUT POINT | 1150. | 968.24 | | 345.74 | 21.45 | 112.17 | 5.95 | 139.57 |

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**
** 19 2 3000. 1400. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks SB Off-Ramp **
**
** 20 2 3000. 900. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks SB/ Fair Oaks **
**
*****

```

FREEWAY AND ARTERIAL DESIGN FEATURES

```

**
** SUB NO. SSEC SSEC DESIG N ORG TRK SSEC PCT PCT DES SPECIAL FF.SPD. CAP. ART GRADE SUBSECTI ON LOCATI ON **
** SEC LNS CAP LENGTH SPEED DES FAC GRAD TRK TRUCKS RAMP ALT. RTE ALT. RTE TYPE ALT. RTE **
**
** 21 2 3000. 100. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Fair Oaks SB On-Ramp **
**
** 22 2 3000. 100. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks NB Off-Ramp **
**
** 23 2 3000. 600. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks NB/ Fair Oaks **
**
** 24 2 3000. 1500. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Oaks On-Ramp to Mid **
**
** 25 2 3000. 1500. 65 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Mid to Lawrence Off-ramp **
**
** 26 2 3000. 8000. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 HOV Dummy **
**
** 27 **
** 28 **
** 29 **
**
*****

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FREEWAY TRAVEL TIME (MINUTES)

```

*****
* OR I G I N S D E S T I N A T I O N S A C R O S S *
* D O W N 1 2 3 4 5 6 7 *
+
* * * * *
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 2 * 0.00 19.74 20.05 20.86 21.05 23.08 0.00 *
+
* 3 * 0.00 0.00 0.00 0.00 1.96 3.99 0.00 *
+
* 4 * 0.00 0.00 0.00 0.00 0.00 3.21 0.00 *
+
* 5 * 0.00 0.00 0.00 0.00 0.00 2.90 0.00 *
+
* 6 * 0.00 0.00 0.00 0.00 0.00 2.74 0.00 *
+
* 7 * 0.00 0.00 0.00 0.00 0.00 2.06 0.00 *
+
* 8 * 0.00 0.00 0.00 0.00 0.00 1.92 0.00 *
+
* 9 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 10 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 11 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
* * * * *
*****

```

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TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB SEC | NO. LNS | SSEC LENGTH | O-D ORG | DATA DES | DEMANDS SSEC | ADJUSTED ORG | VOLUMES DES | SSEC SSEC | WEAVE CAP. | CONGEST EFF | STORAGE LENGTH | V/C RATE | SPEED MPH | DENSITY VPMP | LOS LEVEL | FUEL MPG | EMI SS GS/VM |
|---------|---------|-------------|---------|----------|--------------|--------------|-------------|-----------|------------|-----------------|----------------|----------|-----------|--------------|-----------|----------|--------------|
| 1 | | | | | | | | | | | | | | | | | |
| 2 | 2 | 99999 | 1840 | 0 | 1840 | 1840 | 0 | 1840 | 3000 | 0 | 0 | .61 | 65 | 14.2 | B | 20.0 | 13.7 |
| 3 | 2 | 2740 | 0 | 0 | 1840 | 0 | 0 | 1840 | 3000 | 0 | 0 | .61 | 65 | 14.2 | B | 20.0 | 13.7 |
| 4 | 2 | 600 | 0 | 0 | 1840 | 0 | 0 | 1840 | 3000 | 0 | 0 | .61 | 65 | 14.2 | B | 20.0 | 13.7 |
| 5 | 2 | 700 | 0 | 0 | 1840 | 0 | 0 | 1840 | 3000 | 0 | 0 | .61 | 65 | 14.2 | B | 20.0 | 13.7 |
| 6 | 2 | 2630 | 0 | 0 | 1840 | 0 | 0 | 1840 | 3000 | 0 | 0 | .61 | 65 | 14.2 | B | 20.0 | 13.7 |
| 7 | 2 | 2530 | 0 | 0 | 1840 | 0 | 0 | 1840 | 3000 | 0 | 0 | .61 | 65 | 14.2 | B | 20.0 | 13.7 |
| 8 | 2 | 1500 | 97 | 0 | 1937 | 97 | 0 | 1937 | 3000 | 0 | 0 | .65 | 65 | 14.9 | B | 20.0 | 13.7 |
| 9 | 2 | 700 | 0 | 0 | 1937 | 0 | 0 | 1937 | 3000 | 0 | 0 | .65 | 65 | 14.9 | B | 20.0 | 13.7 |
| 10 | 2 | 1500 | 0 | 415 | 1937 | 0 | 278 | 1937 | 3000 | 0 | 0 | .65 | 65 | 14.9 | B | 20.0 | 13.7 |
| 11 | 2 | 750 | 0 | 0 | 1522 | 0 | 0 | 1522 | 3000 | 0 | 0 | .51 | 65 | 11.7 | B | 20.0 | 13.7 |
| 12 | 2 | 350 | 140 | 0 | 1662 | 140 | 0 | 1662 | 3000 | 0 | 0 | .55 | 65 | 12.8 | B | 20.0 | 13.7 |
| 13 | 2 | 350 | 0 | 0 | 1662 | 0 | 0 | 1662 | 3000 | 0 | 0 | .55 | 65 | 12.8 | B | 20.0 | 13.7 |
| 14 | 2 | 350 | 0 | 138 | 1662 | 0 | 138 | 1662 | 3000 | 0 | 0 | .55 | 65 | 12.8 | B | 20.0 | 13.7 |
| 15 | 2 | 700 | 0 | 0 | 1524 | 0 | 0 | 1524 | 3000 | 0 | 0 | .51 | 65 | 11.7 | B | 20.0 | 13.7 |
| 16 | 2 | 900 | 182 | 0 | 1706 | 182 | 0 | 1706 | 3000 | 0 | 0 | .57 | 65 | 13.1 | B | 20.0 | 13.7 |
| 17 | 2 | 1400 | 68 | 0 | 1774 | 68 | 0 | 1774 | 3000 | 0 | 0 | .59 | 65 | 13.6 | B | 20.0 | 13.7 |
| 18 | 2 | 200 | 0 | 0 | 1774 | 0 | 0 | 1774 | 3000 | 0 | 0 | .59 | 65 | 13.6 | B | 20.0 | 13.7 |
| 19 | 2 | 1400 | 0 | 81 | 1774 | 0 | 81 | 1774 | 3000 | 0 | 0 | .59 | 65 | 13.6 | B | 20.0 | 13.7 |
| 20 | 2 | 900 | 0 | 0 | 1693 | 0 | 0 | 1693 | 3000 | 0 | 0 | .56 | 65 | 13.0 | B | 20.0 | 13.7 |
| 21 | 2 | 100 | 63 | 0 | 1756 | 63 | 0 | 1756 | 3000 | 0 | 0 | .59 | 65 | 13.5 | B | 20.0 | 13.7 |
| 22 | 2 | 100 | 0 | 24 | 1756 | 0 | 24 | 1756 | 3000 | 0 | 0 | .59 | 65 | 13.5 | B | 20.0 | 13.7 |
| 23 | 2 | 600 | 0 | 0 | 1733 | 0 | 0 | 1733 | 3000 | 0 | 0 | .58 | 65 | 13.3 | B | 20.0 | 13.7 |
| 24 | 2 | 1500 | 56 | 0 | 1789 | 56 | 0 | 1789 | 3000 | 0 | 0 | .60 | 65 | 13.8 | B | 20.0 | 13.7 |
| 25 | 2 | 1500 | 0 | 0 | 1789 | 0 | 0 | 1789 | 3000 | 0 | 0 | .60 | 65 | 13.8 | B | 20.0 | 13.7 |
| 26 | 2 | 8000 | 0 | 1789 | 1789 | 0 | 1789 | 1789 | 3000 | 0 | 0 | .60 | 65 | 13.8 | B | 20.0 | 13.7 |
| 27 | | | | | | | | | | | | | | | | | |
| 28 | | | | | | | | | | | | | | | | | |
| 29 | | | | | | | | | | | | | | | | | |
| TOTAL | 131999 | = | 25.0 | MILES | | | | | | MAX(V/C) = 0.65 | LOWEST LOS = B | AVG = 65 | 14.1 | | | 20.0 | 13.7 |

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 TIME SLICE 1 OF 3

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 704. VEH-HRS | 1407. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| OFF-RAMP DELAY = | 68. VEH-HRS | 137. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 772. VEH-HRS | 1544. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 45738. VEH-MI. | 91475. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 59. MPH. | 65. MPH. |
| AVERAGE DENSITY = | 14. VPMP | 14. VPMP |
| TOTAL FUEL = | 2310. GALLONS | 2310. GALLONS |
| TOTAL EMISSIONS = | 638. KILOGRAMS | 638. KILOGRAMS |

***** MAINTENANCE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

***** RAMP DELAYS *****

| OFF-RAMP | NO. LNS | OUTPUT POINT | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|----------|---------|--------------|-----------------------|---------------|----------|---------|---------|----------|----------------------|
| 2 | 2 | OUTPUT POINT | 137. | 68.48 | 23.49 | 1.48 | 7.72 | 0.41 | 9.62 |

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 UNIVERSITY OF CALIFORNIA, BERKELEY SHORT TERM SIMULATION OF PRIORITY LANE
 TIME SLICE 2 OF 3

 **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 **

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | |
|--------------|---------------------|---|---|---|---|---|---|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| | | | | | | | |

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| | | | | | | | | | |
|----|------|----|------|----|------|----|------|----|------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

***** RAMP DELAYS *****

| OFF-RAMP | 2 | OUTPUT POINT | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|----------|---|--------------|--------------------------|------------------|-------------|------------|------------|-------------|----------------------------|
| | | | 264. | 200.26 | 68.69 | 4.33 | 22.59 | 1.20 | 28.12 |

 **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | |
|-----------|------|-----------------------|-------|-------|-------|-------|-------|------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| + * | 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + * | 2 * | 0.00 | 19.74 | 20.05 | 20.86 | 21.05 | 23.08 | 0.00 |
| + * | 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 1.96 | 3.99 | 0.00 |
| + * | 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.21 | 0.00 |
| + * | 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.90 | 0.00 |
| + * | 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.74 | 0.00 |
| + * | 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.06 | 0.00 |
| + * | 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.92 | 0.00 |
| + * | 9 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + * | 10 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| + * | 11 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB | * NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | |
|-------|-------|----------|------------|-----------|--------------------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|------|------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * ORG | * DES | * CAP | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | |
| * 1 | | | | | | | | | | | | | | | | | |
| * 2 | 2 | 99999. | 1554. | 0. | 1554. | 1554. | 0. | 1554. | 3000. | 0. | 0. | .52 | 65. | 12.0 | B | 20.0 | 13.7 |
| * 3 | 2 | 2740. | 0. | 0. | 1554. | 0. | 0. | 1554. | 3000. | 0. | 0. | .52 | 65. | 12.0 | B | 20.0 | 13.7 |
| * 4 | 2 | 600. | 0. | 0. | 1554. | 0. | 0. | 1554. | 3000. | 0. | 0. | .52 | 65. | 12.0 | B | 20.0 | 13.7 |
| * 5 | 2 | 700. | 0. | 0. | 1554. | 0. | 0. | 1554. | 3000. | 0. | 0. | .52 | 65. | 12.0 | B | 20.0 | 13.7 |
| * 6 | 2 | 2630. | 0. | 0. | 1554. | 0. | 0. | 1554. | 3000. | 0. | 0. | .52 | 65. | 12.0 | B | 20.0 | 13.7 |
| * 7 | 2 | 2530. | 0. | 0. | 1554. | 0. | 0. | 1554. | 3000. | 0. | 0. | .52 | 65. | 12.0 | B | 20.0 | 13.7 |
| * 8 | 2 | 1500. | 77. | 0. | 1631. | 77. | 0. | 1631. | 3000. | 0. | 0. | .54 | 65. | 12.5 | B | 20.0 | 13.7 |
| * 9 | 2 | 700. | 0. | 0. | 1631. | 0. | 0. | 1631. | 3000. | 0. | 0. | .54 | 65. | 12.5 | B | 20.0 | 13.7 |
| * 10 | 2 | 1500. | 0. | 360. | 1631. | 0. | 279. | 1631. | 3000. | 0. | 0. | .54 | 65. | 12.5 | B | 20.0 | 13.7 |
| * 11 | 2 | 750. | 0. | 0. | 1271. | 0. | 0. | 1271. | 3000. | 0. | 0. | .42 | 65. | 9.8 | A | 20.0 | 13.7 |
| * 12 | 2 | 350. | 146. | 0. | 1416. | 146. | 0. | 1416. | 3000. | 0. | 0. | .47 | 65. | 10.9 | A | 20.0 | 13.7 |
| * 13 | 2 | 350. | 0. | 0. | 1416. | 0. | 0. | 1416. | 3000. | 0. | 0. | .47 | 65. | 10.9 | A | 20.0 | 13.7 |
| * 14 | 2 | 350. | 0. | 115. | 1416. | 0. | 115. | 1416. | 3000. | 0. | 0. | .47 | 65. | 10.9 | A | 20.0 | 13.7 |
| * 15 | 2 | 700. | 0. | 0. | 1302. | 0. | 0. | 1302. | 3000. | 0. | 0. | .43 | 65. | 10.0 | A | 20.0 | 13.7 |
| * 16 | 2 | 900. | 149. | 0. | 1450. | 149. | 0. | 1450. | 3000. | 0. | 0. | .48 | 65. | 11.2 | B | 20.0 | 13.7 |
| * 17 | 2 | 1400. | 55. | 0. | 1506. | 55. | 0. | 1506. | 3000. | 0. | 0. | .50 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 18 | 2 | 200. | 0. | 0. | 1506. | 0. | 0. | 1506. | 3000. | 0. | 0. | .50 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 19 | 2 | 1400. | 0. | 85. | 1506. | 0. | 85. | 1506. | 3000. | 0. | 0. | .50 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 20 | 2 | 900. | 0. | 0. | 1420. | 0. | 0. | 1420. | 3000. | 0. | 0. | .47 | 65. | 10.9 | A | 20.0 | 13.7 |
| * 21 | 2 | 100. | 52. | 0. | 1473. | 52. | 0. | 1473. | 3000. | 0. | 0. | .49 | 65. | 11.3 | B | 20.0 | 13.7 |
| * 22 | 2 | 100. | 0. | 30. | 1473. | 0. | 30. | 1473. | 3000. | 0. | 0. | .49 | 65. | 11.3 | B | 20.0 | 13.7 |
| * 23 | 2 | 600. | 0. | 0. | 1443. | 0. | 0. | 1443. | 3000. | 0. | 0. | .48 | 65. | 11.1 | B | 20.0 | 13.7 |
| * 24 | 2 | 1500. | 60. | 0. | 1503. | 60. | 0. | 1503. | 3000. | 0. | 0. | .50 | 65. | 11.6 | B | 20.0 | 13.7 |

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US-101_SB_PM_NP_2040_PL
* 25 2 1500. 0. 0. 1503. 0. 0. 1503. 3000. 0. 0. .50 65. 11.6 B 20.0 13.7 *
* 26 2 8000. 0. 1503. 1503. 0. 1503. 1503. 3000. 0. 0. .50 65. 11.6 B 20.0 13.7 *
* 27 *
* 28 *
* 29 *
*****
*
* TOTAL 131999. = 25.0 MILES MAX(V/C) = 0.54 LOWEST LOS = B AVG = 65. 11.9 20.0 13.7 *
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CURRENT TIME SLICE CUMULATIVE VALUES
FREEWAY TRAVEL TIME = 594. VEH-HRS 1188. PASS-HRS 1951. VEH-HRS 3901. PASS-HRS
FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 304. VEH-HRS 609. PASS-HRS 573. VEH-HRS 1146. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 898. VEH-HRS 1797. PASS-HRS 2524. VEH-HRS 5047. PASS-HRS
TOTAL FRWAY TRAV DISTANCE = 38612. VEH-MI. 77223. PASS-MI. 126785. VEH-MI. 253570. PASS-MI.
AVERAGE SYSTEM SPEED = 43. MPH. 65. MPH.
AVERAGE DENSITY = 12. VPMP 13. VPMP
TOTAL FUEL = 2035. GALLONS 6536. GALLONS
TOTAL EMISSIONS = 573. KILOGRAMS 1822. KILOGRAMS

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***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

***** RAMP DELAYS *****

| OFF-RAMP | 2 | OUTPUT POINT | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|----------|---|--------------|--------------------------|------------------|-------------|------------|------------|-------------|----------------------------|
| OFF-RAMP | 2 | OUTPUT POINT | 345. | 304.41 | 104.41 | 6.58 | 34.34 | 1.83 | 42.74 |

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FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQQ QQQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP EEEEEEEEE
    
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FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREWAY AND ARTERIAL DESIGN FEATURES

| ** SUB NO. | ** SSEC | ** SSEC | ** DESIG N | ** ORG | ** TRK | ** SSEC | ** PCT | ** PCT | ** DES | ** SPECIAL | ** FF. SPD. | ** CAP. | ** ART | ** GRADE | ** SUBSECTI ON | ** LOCATI ON |
|------------|---------|---------|------------|----------|--------|---------|--------|-----------|---------|-------------|-------------|---------|-------------|-------------|-------------------------|--------------|
| ** SEC | ** LNS | ** CAP | ** LENGTH | ** SPEED | ** DES | ** GRAD | ** TRK | ** TRUCKS | ** RAMP | ** ALT. RTE | ** ALT. RTE | ** TYPE | ** ALT. RTE | ** ALT. RTE | ** LOCATION | ** LOCATION |
| ** 1 | 5 | 10000. | 1370. | 65 | OD | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Seeding | ** |
| ** 2 | 3 | 7360. | 99999. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | ** |
| ** 3 | 3 | 6000. | 2740. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-85 Off to Shore On | ** |
| ** 4 | 3 | 6000. | 600. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Shore. On to Moffet Off | ** |
| ** 5 | 3 | 6000. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Moffett Off to On | ** |
| ** 6 | 3 | 6000. | 2630. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Moffett On to Ellis Off | ** |
| ** 7 | 3 | 6000. | 2530. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Ellis Off to On-ramp | ** |
| ** 8 | 4 | 6770. | 1500. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Ellis On-ramp | ** |
| ** 9 | 4 | 6770. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Ellis / US 237 | ** |
| ** 10 | 4 | 6770. | 1500. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 EB Off-Ramp | ** |
| ** 11 | 3 | 6000. | 750. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 / SR-237 | ** |
| ** 12 | 4 | 7010. | 350. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 EB On-Ramp | ** |
| ** 13 | 4 | 7010. | 350. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US 237 / Mathilda | ** |
| ** 14 | 4 | 7010. | 350. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-Ramp | ** |
| ** 15 | 3 | 6000. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | ** |
| ** 16 | 3 | 6000. | 900. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda SB On-Ramp | ** |
| ** 17 | 3 | 6000. | 1400. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda NB On-Ramp | ** |
| ** 18 | 3 | 6000. | 200. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Fair Oaks | ** |
| ** 19 | 3 | 6000. | 1400. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks SB Off-Ramp | ** |
| ** 20 | 3 | 6000. | 900. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks SB/ Fair Oaks | ** |

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB NO. | SSEC | O-D DATA | DEMANDS | ADJUSTED | VOLUMES | SSEC | WEAVE | CONGEST | STORAGE | V/C | SPEED | DENSITY | LOS | FUEL | EMI SS | |
|---------|------|----------|--------------|--------------|--------------|--------|--------|---------|----------|-------|-------|---------|-------|------|--------|------|
| SEC | LNS | LENGTH | ORG DES SSEC | ORG DES SSEC | ORG DES SSEC | CAP | EFF | LENGTH | RATE | RATIO | MPH | VPMPPL | LEVEL | MPG | GS/VM | |
| 1 | 5 | 1370. | 9198. 1840. | 9198. | 9198. 1840. | 10000. | 0. | 0. | 0. | .92 | 58. | 31.7 | D | 22.2 | 12.0 | |
| 2 | 3 | 99999. | 0. 0. | 7358. | 0. 0. | 6000. | 7360. | 0. | * 21640. | 1358. | .82 | 41. | 49.0 | F | 22.5 | 12.0 |
| 3 | 3 | 2740. | 0. 0. | 7358. | 0. 0. | 2989. | 6000. | 0. | * 121. | 3011. | .50 | 52. | 19.1 | F | 23.8 | 11.1 |
| 4 | 3 | 600. | 0. 0. | 7358. | 0. 0. | 2989. | 6000. | 0. | ** 600. | 3011. | .50 | 49. | 20.4 | F | 23.5 | 11.3 |
| 5 | 3 | 700. | 0. 0. | 7358. | 0. 0. | 2989. | 6000. | 0. | ** 700. | 3011. | .50 | 44. | 22.5 | F | 23.0 | 11.4 |
| 6 | 3 | 2630. | 0. 0. | 7358. | 0. 0. | 2989. | 6000. | 0. | ** 2630. | 3011. | .50 | 36. | 28.0 | F | 21.9 | 12.0 |
| 7 | 3 | 2530. | 0. 0. | 7358. | 0. 0. | 2989. | 6000. | 0. | ** 2530. | 3011. | .50 | 27. | 37.3 | F | 20.3 | 12.8 |
| 8 | 4 | 1500. | 643. 0. | 8001. | 593. 0. | 3582. | 6673. | 0. | ** 1500. | 3011. | .54 | 23. | 39.0 | F | 18.8 | 13.7 |
| 9 | 4 | 700. | 0. 0. | 8001. | 0. 0. | 3582. | 6770. | 0. | ** 700. | 3011. | .53 | 21. | 43.4 | F | 17.9 | 14.3 |
| 10 | 4 | 1500. | 0. 1711. | 8001. | 0. 1111. | 3582. | 6381. | 0. | ** 1500. | 2799. | .56 | 22. | 40.2 | F | 18.6 | 13.9 |
| 11 | 3 | 750. | 0. 0. | 6290. | 0. 0. | 2215. | 6000. | 0. | ** 750. | 2799. | .37 | 15. | 49.7 | F | 16.7 | 15.5 |
| 12 | 4 | 350. | 702. 0. | 6992. | 652. 0. | 2867. | 6873. | 0. | ** 350. | 2799. | .42 | 15. | 48.6 | F | 15.3 | 16.9 |
| 13 | 4 | 350. | 0. 0. | 6992. | 0. 0. | 2867. | 7010. | 0. | ** 350. | 2799. | .41 | 14. | 52.2 | F | 15.1 | 17.1 |
| 14 | 4 | 350. | 0. 804. | 6992. | 0. 654. | 2867. | 6848. | 0. | ** 350. | 2799. | .42 | 13. | 53.1 | F | 14.9 | 17.3 |
| 15 | 3 | 700. | 0. 0. | 6188. | 0. 0. | 2213. | 6000. | 0. | ** 700. | 2799. | .37 | 12. | 62.9 | F | 15.6 | 16.4 |
| 16 | 3 | 900. | 711. 0. | 6899. | 611. 0. | 2824. | 5840. | 0. | ** 900. | 2799. | .48 | 14. | 68.2 | F | 15.8 | 16.0 |
| 17 | 3 | 1400. | 490. 0. | 7389. | 390. 0. | 3214. | 5890. | 0. | ** 1400. | 2676. | .55 | 15. | 71.9 | F | 15.8 | 16.1 |
| 18 | 3 | 200. | 0. 0. | 7389. | 0. 0. | 3214. | 6000. | 0. | ** 200. | 2676. | .54 | 14. | 77.5 | F | 15.2 | 16.7 |
| 19 | 3 | 1400. | 0. 496. | 7389. | 0. 397. | 3214. | 5919. | 0. | ** 1400. | 2676. | .54 | 13. | 80.6 | F | 14.9 | 17.0 |
| 20 | 3 | 900. | 0. 0. | 6893. | 0. 0. | 2816. | 6000. | 0. | ** 900. | 2676. | .47 | 10. | 90.1 | F | 13.9 | 18.1 |
| 21 | 4 | 100. | 257. 0. | 7150. | 240. 0. | 3056. | 6187. | 0. | ** 100. | 2676. | .49 | 11. | 71.7 | F | 12.8 | 19.8 |
| 22 | 4 | 100. | 0. 138. | 7150. | 0. 111. | 3056. | 6226. | 0. | ** 100. | 2676. | .49 | 10. | 72.9 | F | 12.7 | 19.8 |
| 23 | 3 | 600. | 0. 0. | 7012. | 0. 0. | 2945. | 6000. | 0. | ** 600. | 2676. | .49 | 10. | 96.7 | F | 13.4 | 18.6 |
| 24 | 3 | 1500. | 224. 0. | 7236. | 224. 0. | 3169. | 5944. | 0. | ** 1500. | 2676. | .53 | 10. | 101.3 | F | 13.2 | 19.0 |
| 25 | 3 | 1500. | 0. 0. | 7236. | 0. 0. | 3169. | 6000. | 0. | ** 1500. | 2676. | .53 | 9. | 113.0 | F | 12.4 | 20.0 |
| 26 | 3 | 8000. | 0. 0. | 7236. | 0. 0. | 3169. | 6000. | 0. | ** 8000. | 2676. | .53 | 7. | 151.7 | F | 10.4 | 23.6 |
| 27 | 5 | 100. | 1809. 0. | 9045. | 1809. 0. | 4978. | 10000. | 0. | ** 100. | 2676. | .50 | 5. | 202.6 | F | 8.6 | 28.0 |
| 28 | 5 | 1000. | 1560. 0. | 10605. | 1212. 0. | 6190. | 7750. | 0. | ** 1000. | 1560. | .80 | 12. | 100.6 | F | 14.4 | 20.9 |
| 29 | 5 | 1000. | 1560. 12165. | 12165. | 1560. 7750. | 7750. | 7750. | 0. | 0. | 0. | 1.00 | 52. | 29.7 | E | 23.8 | 11.1 |

TOTAL 135469. = 25.7 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 31. 56.1 20.9 12.8

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 5535. VEH-HRS | 5576. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 333. VEH-HRS | 367. PASS-HRS |
| OFF-RAMP DELAY = | 128. VEH-HRS | 128. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 5995. VEH-HRS | 6072. PASS-HRS |
| TOTAL TRAV DISTANCE = | 170433. VEH-MI. | 171523. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 28. MPH | 31. MPH |
| AVERAGE DENSITY = | 56. VPMPPL | 56. VPMPPL |
| TOTAL FUEL = | 8325. GALLONS | 8325. GALLONS |
| TOTAL EMISSIONS = | 2242. KI LOGRAMS | 2242. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|--------|------------|-------|------------|-------|------------|-------|------------|--------|
| 1 | 4.39 | 2 | ***** | 3 | 11.75 | 4 | 3.45 | 5 | 5.61 |
| 6 | 36.38 | 7 | 57.79 | 8 | 46.92 | 9 | 25.27 | 10 | 47.31 |
| 11 | 30.70 | 12 | 16.50 | 13 | 17.89 | 14 | 18.10 | 15 | 36.35 |
| 16 | 43.30 | 17 | 64.85 | 18 | 10.05 | 19 | 72.74 | 20 | 55.99 |
| 21 | 6.33 | 22 | 6.45 | 23 | 38.81 | 24 | 96.76 | 25 | 106.39 |
| 26 | 706.54 | 27 | 18.02 | 28 | 77.66 | 29 | 5.53 | | |

***** TOTAL DELAY = 2913.0 VEH-HRS ***** AVERAGE DELAY = 43.85 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH | DELAY | AVERAGE | GAS | HC | CO | NOX | TOTAL |
|---------|--------------|---------|----------------|------|------|------|------|-----------|
| ON-RAMP | VEHICLES | VEH-HRS | METERING DELAY | GALS | KGMS | KGMS | KGMS | EMISSIONS |
| | | | MINUTES | | | | | KGMS |
| RAMP 2 | 50. | 25.00 | 2.33 | 8.93 | 0.55 | 2.90 | 0.15 | 3.60 |

| | | US-101_SB_PM_P1_2040_PE | | | | | | | | |
|----------|---|-------------------------|------|--------|------|-------|------|-------|------|-------|
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| | | TOTAL | 50. | 25.00 | 2.33 | 8.93 | 0.55 | 2.90 | 0.15 | 3.60 |
| ON-RAMP | 3 | RAMP | 50. | 25.00 | 2.14 | 8.93 | 0.55 | 2.90 | 0.15 | 3.60 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 50. | 25.00 | 2.14 | 8.93 | 0.55 | 2.90 | 0.15 | 3.60 |
| ON-RAMP | 4 | RAMP | 100. | 50.00 | 4.22 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 50.00 | 4.22 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| ON-RAMP | 5 | RAMP | 100. | 50.00 | 6.12 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 50.00 | 6.12 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| ON-RAMP | 6 | RAMP | 17. | 8.50 | 1.98 | 3.04 | 0.19 | 0.98 | 0.05 | 1.23 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 17. | 8.50 | 1.98 | 3.04 | 0.19 | 0.98 | 0.05 | 1.23 |
| ON-RAMP | 9 | RAMP | 348. | 174.00 | 8.37 | 62.13 | 3.85 | 20.16 | 1.07 | 25.08 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 348. | 174.00 | 8.37 | 62.13 | 3.85 | 20.16 | 1.07 | 25.08 |
| OFF-RAMP | 2 | OUTPUT POINT | 256. | 127.79 | | 45.63 | 2.83 | 14.80 | 0.79 | 18.42 |

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 QUEUE COLLISION IN SECTION 3 T2 =0.108

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 TIME SLICE 2 OF 3
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 **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 **

| | | ORIGINS DESTINATIONS ACROSS | | | | | |
|---|---|-----------------------------|-------|-------|-------|-------|-------|
| | | DOWN | | | | | |
| | | 1 | 2 | 3 | 4 | 5 | 6 |
| + | * | ***** | | | | | |
| + | * | ***** | | | | | |
| + | * | 1 | 2 | 3 | 4 | 5 | 6 |
| + | * | ***** | | | | | |
| + | * | 1 | 2 | 3 | 4 | 5 | 6 |
| + | * | 0.25 | 64.84 | 67.58 | 71.96 | 73.14 | 85.00 |
| + | * | 2 | 3 | 4 | 5 | 6 | |
| + | * | 0.00 | 3.50 | 6.24 | 10.62 | 11.80 | 23.65 |
| + | * | 3 | 4 | 5 | 6 | | |
| + | * | 0.00 | 0.00 | 1.57 | 5.95 | 7.13 | 18.99 |
| + | * | 4 | 5 | 6 | | | |
| + | * | 0.00 | 0.00 | 0.00 | 3.26 | 4.44 | 16.30 |
| + | * | 5 | 6 | | | | |
| + | * | 0.00 | 0.00 | 0.00 | 2.34 | 3.53 | 15.38 |
| + | * | 6 | | | | | |
| + | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.21 | 12.06 |
| + | * | 7 | | | | | |
| + | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 11.23 |
| + | * | 8 | | | | | |
| + | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.96 |
| + | * | 9 | | | | | |
| + | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.81 |
| + | * | 10 | | | | | |
| + | * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.22 |
| + | * | ***** | | | | | |
| + | * | ***** | | | | | |

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TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB | * NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS |
|-------|-------|----------|------------|-----------|------------|-----------|---------|---------|-----------|-----------|----------|---------|-----------|---------|---------|-------------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * CAP. | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM |
| * 1 | * 5 | * 1370. | * 8549. | * 1710. | * 8549. | * 8549. | * 1710. | * 8549. | * 10000. | * 0. | * 0. | * 61. | * 27.9 | * D | * 20.9 | * 12.8 |
| * 2 | * 3 | * 99999. | * 0. | * 0. | * 6839. | * 0. | * 0. | * 4578. | * 7360. | * 0. | * 42274. | * 2261. | * .62 | * 22. | * 69.2 | * F |
| * 3 | * 3 | * 2740. | * 0. | * 0. | * 6839. | * 0. | * 0. | * 4578. | * 6000. | * 0. | * 2740. | * 1422. | * .76 | * 11. | * 134.4 | * F |
| * 4 | * 3 | * 600. | * 0. | * 0. | * 6839. | * 0. | * 0. | * 4577. | * 6000. | * 0. | * 600. | * 1422. | * .76 | * 11. | * 142.0 | * F |
| * 5 | * 3 | * 700. | * 0. | * 0. | * 6839. | * 0. | * 0. | * 4577. | * 6000. | * 0. | * 700. | * 1422. | * .76 | * 11. | * 142.0 | * F |
| * 6 | * 3 | * 2630. | * 0. | * 0. | * 6839. | * 0. | * 0. | * 4577. | * 6000. | * 0. | * 2630. | * 1422. | * .76 | * 11. | * 142.0 | * F |
| * 7 | * 3 | * 2530. | * 0. | * 0. | * 6839. | * 0. | * 0. | * 4577. | * 6000. | * 0. | * 2530. | * 1422. | * .76 | * 11. | * 142.0 | * F |
| * 8 | * 4 | * 1500. | * 672. | * 0. | * 7511. | * 672. | * 0. | * 5250. | * 6674. | * 0. | * 1500. | * 1422. | * .79 | * 12. | * 113.3 | * F |
| * 9 | * 4 | * 700. | * 0. | * 0. | * 7511. | * 0. | * 0. | * 5250. | * 6770. | * 0. | * 700. | * 1422. | * .78 | * 11. | * 117.4 | * F |

US-101_SB_PM_P1_2040_PE

| | | | | | | | | | | | | | | | | | | | | | |
|---|----|---|-------|-------|-------|-------|-------|-------|-------|--------|----|----|-------|-------|------|-----|-------|---|------|------|---|
| * | 10 | 4 | 1500. | 0. | 1666. | 7511. | 0. | 1126. | 5250. | 6396. | 0. | ** | 1500. | 1146. | .82 | 13. | 101.4 | F | 14.8 | 20.5 | * |
| * | 11 | 3 | 750. | 0. | 0. | 5845. | 0. | 0. | 3829. | 6000. | 0. | ** | 750. | 1146. | .64 | 7. | 174.6 | F | 10.1 | 26.0 | * |
| * | 12 | 4 | 350. | 670. | 0. | 6515. | 670. | 0. | 4499. | 6886. | 0. | ** | 350. | 1146. | .65 | 8. | 146.9 | F | 10.4 | 25.6 | * |
| * | 13 | 4 | 350. | 0. | 0. | 6515. | 0. | 0. | 4499. | 7010. | 0. | ** | 350. | 1146. | .64 | 7. | 152.2 | F | 10.2 | 25.9 | * |
| * | 14 | 4 | 350. | 0. | 842. | 6515. | 0. | 732. | 4499. | 6843. | 0. | ** | 350. | 1146. | .66 | 8. | 145.0 | F | 10.5 | 25.4 | * |
| * | 15 | 3 | 700. | 0. | 0. | 5673. | 0. | 0. | 3768. | 6000. | 0. | ** | 700. | 1146. | .63 | 7. | 177.3 | F | 9.9 | 26.2 | * |
| * | 16 | 3 | 900. | 757. | 0. | 6430. | 757. | 0. | 4525. | 5836. | 0. | ** | 900. | 1146. | .78 | 11. | 135.0 | F | 13.8 | 21.9 | * |
| * | 17 | 3 | 1400. | 526. | 0. | 6956. | 526. | 0. | 5051. | 5886. | 0. | ** | 1400. | 835. | .86 | 15. | 114.9 | F | 16.0 | 19.1 | * |
| * | 18 | 3 | 200. | 0. | 0. | 6956. | 0. | 0. | 5051. | 6000. | 0. | ** | 200. | 835. | .84 | 14. | 121.4 | F | 15.5 | 19.7 | * |
| * | 19 | 3 | 1400. | 0. | 614. | 6956. | 0. | 519. | 5051. | 5904. | 0. | ** | 1400. | 835. | .86 | 15. | 115.9 | F | 15.9 | 19.2 | * |
| * | 20 | 3 | 900. | 0. | 0. | 6342. | 0. | 0. | 4532. | 6000. | 0. | ** | 900. | 835. | .76 | 10. | 144.0 | F | 13.4 | 22.4 | * |
| * | 21 | 4 | 100. | 274. | 0. | 6616. | 240. | 0. | 4772. | 6184. | 0. | ** | 100. | 835. | .77 | 11. | 108.0 | F | 13.7 | 22.0 | * |
| * | 22 | 4 | 100. | 0. | 196. | 6616. | 0. | 165. | 4772. | 6218. | 0. | ** | 100. | 835. | .77 | 11. | 109.4 | F | 13.6 | 22.1 | * |
| * | 23 | 3 | 600. | 0. | 0. | 6420. | 0. | 0. | 4607. | 6000. | 0. | ** | 600. | 835. | .77 | 11. | 140.7 | F | 13.6 | 22.1 | * |
| * | 24 | 3 | 1500. | 200. | 0. | 6620. | 200. | 0. | 4807. | 5950. | 0. | ** | 1500. | 835. | .81 | 12. | 129.1 | F | 14.5 | 20.9 | * |
| * | 25 | 3 | 1500. | 0. | 0. | 6620. | 0. | 0. | 4807. | 6000. | 0. | ** | 1500. | 835. | .80 | 12. | 132.0 | F | 14.3 | 21.1 | * |
| * | 26 | 3 | 8000. | 0. | 0. | 6620. | 0. | 0. | 4807. | 6000. | 0. | ** | 8000. | 835. | .80 | 12. | 132.0 | F | 14.3 | 21.1 | * |
| * | 27 | 5 | 100. | 1655. | 0. | 8275. | 1655. | 0. | 6462. | 10000. | 0. | ** | 100. | 835. | .65 | 7. | 172.5 | F | 10.3 | 25.7 | * |
| * | 28 | 5 | 1000. | 520. | 0. | 8795. | 768. | 0. | 7230. | 7750. | 0. | ** | 1000. | 520. | .93 | 19. | 75.6 | F | 18.1 | 16.6 | * |
| * | 29 | 5 | 1000. | 520. | 9315. | 9315. | 520. | 7750. | 7750. | 7750. | 0. | ** | 0. | 0. | 1.00 | 52. | 29.7 | E | 23.8 | 11.1 | * |

 * TOTAL 135469. = 25.7 MI LBS MAX(V/C) = 1.00 LOWEST LOS = F AVG = 19. 83.6 16.7 16.2 *

| CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | | |
|----------------------------|---------|------------|---------|-------------------|---------|------------|---------|----------|
| FREEWAY TRAVEL TIME = | 7975. | VEH-HRS | 8011. | PASS-HRS | 13510. | VEH-HRS | 13587. | PASS-HRS |
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 558. | VEH-HRS | 603. | PASS-HRS | 891. | VEH-HRS | 970. | PASS-HRS |
| OFF-RAMP DELAY = | 403. | VEH-HRS | 405. | PASS-HRS | 531. | VEH-HRS | 533. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 8936. | VEH-HRS | 9019. | PASS-HRS | 14932. | VEH-HRS | 15090. | PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 150714. | VEH-MI. | 151813. | PASS-MI. | 321148. | VEH-MI. | 323336. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 17. | MPH | | | 24. | MPH | | |
| AVERAGE DENSITY = | 84. | VPMP | | | 70. | VPMP | | |
| TOTAL FUEL = | 9376. | GALLONS | | | 17701. | GALLONS | | |
| TOTAL EMISSIONS = | 2587. | KI LOGRAMS | | | 4829. | KI LOGRAMS | | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|--------|------------|--------|------------|--------|------------|-------|------------|-------|
| 1 | 2.06 | 2 | ***** | 3 | 175.51 | 4 | 40.41 | 5 | 47.15 |
| 6 | 177.13 | 7 | 170.40 | 8 | 105.78 | 9 | 51.54 | 10 | 92.30 |
| 11 | 66.03 | 12 | 34.35 | 13 | 35.76 | 14 | 33.87 | 15 | 62.82 |
| 16 | 57.15 | 17 | 70.78 | 18 | 10.85 | 19 | 71.60 | 20 | 61.74 |
| 21 | 6.79 | 22 | 6.90 | 23 | 39.91 | 24 | 89.05 | 25 | 91.48 |
| 26 | 487.87 | 27 | 14.45 | 28 | 50.52 | 29 | 5.53 | | |

***** TOTAL DELAY = 5656.6 VEH-HRS ***** AVERAGE DELAY = 73.15 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|------------|-----------------------|---------------|--------------------------------|----------|---------|---------|----------|----------------------|
| ON-RAMP 2 | RAMP 50. | 50.00 | 4.16 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 50. | 50.00 | 4.16 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| ON-RAMP 3 | RAMP 50. | 50.00 | 4.17 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 50. | 50.00 | 4.17 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| ON-RAMP 4 | RAMP 100. | 100.00 | 7.00 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 100. | 100.00 | 7.00 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP 5 | RAMP 100. | 100.00 | 9.58 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 100. | 100.00 | 9.58 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP 6 | RAMP 51. | 34.00 | 7.01 | 12.14 | 0.75 | 3.94 | 0.21 | 4.90 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 51. | 34.00 | 7.01 | 12.14 | 0.75 | 3.94 | 0.21 | 4.90 |
| ON-RAMP 9 | RAMP 100. | 224.00 | 17.59 | 79.99 | 4.96 | 25.95 | 1.38 | 32.29 |
| | FREEWAY 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL 100. | 224.00 | 17.59 | 79.99 | 4.96 | 25.95 | 1.38 | 32.29 |
| OFF-RAMP 2 | OUTPUT POINT 550. | 402.95 | | 143.88 | 8.93 | 46.68 | 2.48 | 58.08 |

FREEWAY TRAVEL TIME (MINUTES)

Table with columns: ORIGINS, DESTINATIONS ACROSS (1-6), and various travel time values for 10 different origin-destination pairs.

TIME SLICE FREEWAY PERFORMANCE TABLE

Table with columns: SUB SEC, NO. LNS, SSEC LENGTH, O-D DATA, DEMANDS, ADJUSTED VOLUMES, SSEC CAP, WEAVE EFF, CONGEST LENGTH, STORAGE RATE, V/C RATIO, SPEED MPH, DENSITY VPMP, LOS LEVEL, FUEL MPG, EMISSIONS GS/VM. Contains 29 rows of performance data.

TOTAL 135469. = 25.7 MILES MAX(V/C) = 1.00 LOWEST LOS = F AVG = 14. 111.0 14.3 19.0

FREEWAY TRAVEL TIME = CURRENT TIME SLICE 9682. VEH-HRS 9719. PASS-HRS CUMULATIVE VALUES 23193. VEH-HRS 23306. PASS-HRS

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FREEMERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
 ON-RAMP MRG/CAP DELAY = 440. VEH-HRS 460. PASS-HRS 1331. VEH-HRS 1430. PASS-HRS
 OFF-RAMP DELAY = 677. VEH-HRS 680. PASS-HRS 1208. VEH-HRS 1212. PASS-HRS
 TOTAL SYSTEM TRAVEL TIME = 10799. VEH-HRS 10858. PASS-HRS 25731. VEH-HRS 25948. PASS-HRS
 TOTAL TRAVEL DISTANCE = 137215. VEH-MI. 138264. PASS-MI. 458363. VEH-MI. 461600. PASS-MI.
 AVERAGE SYSTEM SPEED = 13. MPH. 20. MPH.
 AVERAGE DENSITY = 111. VPMP 84. VPMP
 TOTAL FUEL = 9966. GALLONS 27667. GALLONS
 TOTAL EMISSIONS = 2766. KI LOGRAMS 7595. KI LOGRAMS

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|--------|------------|--------|------------|--------|------------|-------|------------|-------|
| 1 | 0.64 | 2 | ***** | 3 | 174.34 | 4 | 38.19 | 5 | 44.56 |
| 6 | 167.41 | 7 | 161.05 | 8 | 107.34 | 9 | 51.84 | 10 | 94.69 |
| 11 | 66.24 | 12 | 33.50 | 13 | 35.10 | 14 | 33.58 | 15 | 60.22 |
| 16 | 58.67 | 17 | 76.85 | 18 | 11.57 | 19 | 77.12 | 20 | 64.52 |
| 21 | 7.15 | 22 | 7.22 | 23 | 41.84 | 24 | 91.72 | 25 | 94.63 |
| 26 | 504.69 | 27 | 15.04 | 28 | 56.88 | 29 | 5.53 | | |

***** TOTAL DELAY = 7571.3 VEH-HRS ***** AVERAGE DELAY = 96.17 MIN/VEH *****

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***** RAMP DELAYS *****

| | | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|----------|---|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|
| ON-RAMP | 2 | RAMP | 50. | 50.00 | 5.24 | 17.85 | 1.11 | 5.79 | 7.21 |
| | | FREEMERGE | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 50. | 50.00 | 5.24 | 17.85 | 1.11 | 5.79 | 7.21 |
| ON-RAMP | 3 | RAMP | 50. | 50.00 | 3.76 | 17.85 | 1.11 | 5.79 | 7.21 |
| | | FREEMERGE | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 50. | 50.00 | 3.76 | 17.85 | 1.11 | 5.79 | 7.21 |
| ON-RAMP | 4 | RAMP | 100. | 100.00 | 8.57 | 35.71 | 2.22 | 11.58 | 14.41 |
| | | FREEMERGE | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 100.00 | 8.57 | 35.71 | 2.22 | 11.58 | 14.41 |
| ON-RAMP | 5 | RAMP | 100. | 100.00 | 11.56 | 35.71 | 2.22 | 11.58 | 14.41 |
| | | FREEMERGE | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 100.00 | 11.56 | 35.71 | 2.22 | 11.58 | 14.41 |
| ON-RAMP | 6 | RAMP | 29. | 40.00 | 8.92 | 14.28 | 0.89 | 4.63 | 5.77 |
| | | FREEMERGE | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 29. | 40.00 | 8.92 | 14.28 | 0.89 | 4.63 | 5.77 |
| ON-RAMP | 9 | RAMP | 100. | 100.00 | 8.57 | 35.71 | 2.22 | 11.58 | 14.41 |
| | | FREEMERGE | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 100.00 | 8.57 | 35.71 | 2.22 | 11.58 | 14.41 |
| OFF-RAMP | 2 | OUTPUT POINT | 803. | 676.87 | | 241.70 | 14.99 | 78.41 | 4.16 |
| | | | | | | | | | 97.57 |

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FFFFFFFFR RRRRRRRR EEEEEEEEEE QQQQQQ 1111 222222 P P P P P P L L L
FFFFFFFFR RRRRRRRR EEEEEEEEEE Q*A. D. MAY*Q 111111 222 222 P P P P P P P P L L L
FFF RRR RRR EEE QQQQQ QQQQQ 1111 222 222 PPP PPP L L L
FFF RRR RRR EEE QQQQ QQQQ 1111 222 PPP PPP L L L
FFFFFFFFR RRRRRRRR EEEEEEEEEE QQQQ QQQQ 1111 222 P P P P P P P P L L L
FFFFFFFFR RRRRRRRR EEEEEEEEEE QQQQ QQQQ 1111 2222 P P P P P P P P L L L
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP L L L
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP L L L
FFF RRR RRR EEEEEEEEEE Q*REGENTS*Q 1111 222 PPP L L L L L L L L L L L L L
FFF RRR RRR EEEEEEEEEE Q*1988*Q QQQ 11111111 2222222222 PPP L L L L L L L L L L L
    
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FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 2 AND 26 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 2.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

| ***** FREeway AND ARTERIAL DESIGN FEATURES ***** | | | | | | | | | | | | | | | | |
|--|------|-------|--------|-----|-----|------|-----|--------|------|----------|----------|------|----------|-------|-------------------------|----------|
| SUB NO. | SSEC | SSEC | DESIGN | ORG | TRK | SSEC | PCT | PCT | DES | SPECIAL | FF. SPD. | CAP. | ART | GRADE | SUBSECTION | LOCATION |
| SEC | LNS | CAP | LENGTH | DES | FAC | GRAD | TRK | TRUCKS | RAMP | ALT. RTE | ALT. RTE | TYPE | ALT. RTE | | | |
| 1 | | | | | | | | | | | | | | | | |
| 2 | 2 | 3000. | 99999. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | |
| 3 | 2 | 3000. | 2740. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-85 Off to Shore On | |
| 4 | 2 | 3000. | 600. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Shore. On to Moffet Off | |
| 5 | 2 | 3000. | 700. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Moffett Off to On | |
| 6 | 2 | 3000. | 2630. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Moffett On to Ellis Off | |
| 7 | 2 | 3000. | 2530. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Ellis Off to On-ramp | |
| 8 | 2 | 3000. | 1500. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Ellis On-ramp | |
| 9 | 2 | 3000. | 700. | 65 | | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Ellis / US 237 | |
| 10 | 2 | 3000. | 1500. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 EB Off-Ramp | |
| 11 | 2 | 3000. | 750. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 / SR-237 | |
| 12 | 2 | 3000. | 350. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 EB On-Ramp | |
| 13 | 2 | 3000. | 350. | 65 | | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | US 237 / Mathilda | |
| 14 | 2 | 3000. | 350. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-Ramp | |
| 15 | 2 | 3000. | 700. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | |
| 16 | 2 | 3000. | 900. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda SB On-Ramp | |
| 17 | 2 | 3000. | 1400. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda NB On-Ramp | |
| 18 | 2 | 3000. | 200. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Fair Oaks | |

```

**
** 19 2 3000. 1400. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks SB Off-Ramp **
**
** 20 2 3000. 900. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks SB/ Fair Oaks **
**
*****

```

FREEWAY AND ARTERIAL DESIGN FEATURES

```

*****
**
**
**
**
**
** SUB NO. SSEC SSEC DESIG N ORG TRK SSEC PCT PCT DES SPECIAL FF.SPD. CAP. ART GRADE SUBSECTI ON LOCATI ON **
** SEC LNS CAP LENGTH SPEED DES FAC GRAD TRK TRUCKS RAMP ALT. RTE ALT. RTE TYPE ALT. RTE **
**
** 21 2 3000. 100. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Fair Oaks SB On-Ramp **
**
** 22 2 3000. 100. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks NB Off-Ramp **
**
** 23 2 3000. 600. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks NB/ Fair Oaks **
**
** 24 2 3000. 1500. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Oaks On-Ramp to Mid **
**
** 25 2 3000. 1500. 65 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Mid to Lawrence Off-ramp **
**
** 26 2 3000. 8000. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 HOV Dummy **
**
** 27 **
** 28 **
** 29 **
**
*****

```

FREEWAY TRAVEL TIME (MINUTES)

```

*****
* OR I G I N S D E S T I N A T I O N S A C R O S S *
* D O W N 1 2 3 4 5 6 7 *
+
* * * * *
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 2 * 0.00 19.74 20.05 20.86 21.05 23.08 0.00 *
+
* 3 * 0.00 0.00 0.00 0.00 1.96 3.99 0.00 *
+
* 4 * 0.00 0.00 0.00 0.00 0.00 3.21 0.00 *
+
* 5 * 0.00 0.00 0.00 0.00 0.00 2.90 0.00 *
+
* 6 * 0.00 0.00 0.00 0.00 0.00 2.74 0.00 *
+
* 7 * 0.00 0.00 0.00 0.00 0.00 2.06 0.00 *
+
* 8 * 0.00 0.00 0.00 0.00 0.00 1.92 0.00 *
+
* 9 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 10 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 11 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
* * * * *
*****

```

US-101_SB_PM_P1_2040_PL

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB SEC | NO. LNS | SSEC LENGTH | O-D ORG | DATA DES | DEMANDS SSEC | ADJUSTED ORG | VOLUMES DES | SSEC SSEC | WEAVE CAP. | CONGEST EFF | STORAGE LENGTH | V/C RATIO | SPEED MPH | DENSITY VPMP | LOS LEVEL | FUEL MPG | EMI SS GS/VM | |
|---------|---------|-------------|---------|----------|--------------|--------------|-------------|-----------|------------|-----------------|----------------|-----------|-----------|--------------|-----------|----------|--------------|------|
| 1 | | | | | | | | | | | | | | | | | | |
| 2 | 2 | 99999 | 1840. | 0. | 1840. | 1840. | 0. | 1840. | 3000. | 0. | 0. | 0. | .61 | 65. | 14.2 | B | 20.0 | 13.7 |
| 3 | 2 | 2740. | 0. | 0. | 1840. | 0. | 0. | 1840. | 3000. | 0. | 0. | 0. | .61 | 65. | 14.2 | B | 20.0 | 13.7 |
| 4 | 2 | 600. | 0. | 0. | 1840. | 0. | 0. | 1840. | 3000. | 0. | 0. | 0. | .61 | 65. | 14.2 | B | 20.0 | 13.7 |
| 5 | 2 | 700. | 0. | 0. | 1840. | 0. | 0. | 1840. | 3000. | 0. | 0. | 0. | .61 | 65. | 14.2 | B | 20.0 | 13.7 |
| 6 | 2 | 2630. | 0. | 0. | 1840. | 0. | 0. | 1840. | 3000. | 0. | 0. | 0. | .61 | 65. | 14.2 | B | 20.0 | 13.7 |
| 7 | 2 | 2530. | 0. | 0. | 1840. | 0. | 0. | 1840. | 3000. | 0. | 0. | 0. | .61 | 65. | 14.2 | B | 20.0 | 13.7 |
| 8 | 2 | 1500. | 97. | 0. | 1937. | 97. | 0. | 1937. | 3000. | 0. | 0. | 0. | .65 | 65. | 14.9 | B | 20.0 | 13.7 |
| 9 | 2 | 700. | 0. | 0. | 1937. | 0. | 0. | 1937. | 3000. | 0. | 0. | 0. | .65 | 65. | 14.9 | B | 20.0 | 13.7 |
| 10 | 2 | 1500. | 0. | 389. | 1937. | 0. | 278. | 1937. | 3000. | 0. | 0. | 0. | .65 | 65. | 14.9 | B | 20.0 | 13.7 |
| 11 | 2 | 750. | 0. | 0. | 1548. | 0. | 0. | 1548. | 3000. | 0. | 0. | 0. | .52 | 65. | 11.9 | B | 20.0 | 13.7 |
| 12 | 2 | 350. | 137. | 0. | 1685. | 137. | 0. | 1685. | 3000. | 0. | 0. | 0. | .56 | 65. | 13.0 | B | 20.0 | 13.7 |
| 13 | 2 | 350. | 0. | 0. | 1685. | 0. | 0. | 1685. | 3000. | 0. | 0. | 0. | .56 | 65. | 13.0 | B | 20.0 | 13.7 |
| 14 | 2 | 350. | 0. | 162. | 1685. | 0. | 162. | 1685. | 3000. | 0. | 0. | 0. | .56 | 65. | 13.0 | B | 20.0 | 13.7 |
| 15 | 2 | 700. | 0. | 0. | 1524. | 0. | 0. | 1524. | 3000. | 0. | 0. | 0. | .51 | 65. | 11.7 | B | 20.0 | 13.7 |
| 16 | 2 | 900. | 160. | 0. | 1684. | 160. | 0. | 1684. | 3000. | 0. | 0. | 0. | .56 | 65. | 13.0 | B | 20.0 | 13.7 |
| 17 | 2 | 1400. | 110. | 0. | 1794. | 110. | 0. | 1794. | 3000. | 0. | 0. | 0. | .60 | 65. | 13.8 | B | 20.0 | 13.7 |
| 18 | 2 | 200. | 0. | 0. | 1794. | 0. | 0. | 1794. | 3000. | 0. | 0. | 0. | .60 | 65. | 13.8 | B | 20.0 | 13.7 |
| 19 | 2 | 1400. | 0. | 81. | 1794. | 0. | 81. | 1794. | 3000. | 0. | 0. | 0. | .60 | 65. | 13.8 | B | 20.0 | 13.7 |
| 20 | 2 | 900. | 0. | 0. | 1714. | 0. | 0. | 1714. | 3000. | 0. | 0. | 0. | .57 | 65. | 13.2 | B | 20.0 | 13.7 |
| 21 | 2 | 100. | 63. | 0. | 1776. | 63. | 0. | 1776. | 3000. | 0. | 0. | 0. | .59 | 65. | 13.7 | B | 20.0 | 13.7 |
| 22 | 2 | 100. | 0. | 24. | 1776. | 0. | 24. | 1776. | 3000. | 0. | 0. | 0. | .59 | 65. | 13.7 | B | 20.0 | 13.7 |
| 23 | 2 | 600. | 0. | 0. | 1753. | 0. | 0. | 1753. | 3000. | 0. | 0. | 0. | .58 | 65. | 13.5 | B | 20.0 | 13.7 |
| 24 | 2 | 1500. | 56. | 0. | 1809. | 56. | 0. | 1809. | 3000. | 0. | 0. | 0. | .60 | 65. | 13.9 | B | 20.0 | 13.7 |
| 25 | 2 | 1500. | 0. | 0. | 1809. | 0. | 0. | 1809. | 3000. | 0. | 0. | 0. | .60 | 65. | 13.9 | B | 20.0 | 13.7 |
| 26 | 2 | 8000. | 0. | 1809. | 1809. | 0. | 1809. | 1809. | 3000. | 0. | 0. | 0. | .60 | 65. | 13.9 | B | 20.0 | 13.7 |
| 27 | | | | | | | | | | | | | | | | | | |
| 28 | | | | | | | | | | | | | | | | | | |
| 29 | | | | | | | | | | | | | | | | | | |
| TOTAL | 131999 | = | 25.0 | MILES | | | | | | MAX(V/C) = 0.65 | LOWEST LOS = B | | AVG = 65. | 14.1 | | 20.0 | 13.7 | |

| CURRENT TIME SLICE | | | | CUMULATIVE VALUES | | | | |
|-----------------------------|--------|-----------|--------|-------------------|--------|-----------|--------|----------|
| FREEWAY TRAVEL TIME = | 705. | VEH-HRS | 1409. | PASS-HRS | 705. | VEH-HRS | 1409. | PASS-HRS |
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| OFF-RAMP DELAY = | 56. | VEH-HRS | 111. | PASS-HRS | 56. | VEH-HRS | 111. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 760. | VEH-HRS | 1520. | PASS-HRS | 760. | VEH-HRS | 1520. | PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 45798. | VEH-MI. | 91596. | PASS-MI. | 45798. | VEH-MI. | 91596. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 60. | MPH. | | | 65. | MPH. | | |
| AVERAGE DENSITY = | 14. | VPMP | | | 14. | VPMP | | |
| TOTAL FUEL = | 2309. | GALLONS | | | 2309. | GALLONS | | |
| TOTAL EMISSIONS = | 637. | KILOGRAMS | | | 637. | KILOGRAMS | | |

***** MAINTENANCE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

***** RAMP DELAYS *****

| OFF-RAMP | NO. | OUTPUT POINT | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|----------|-----|--------------|-----------------------|---------------|----------|---------|---------|----------|----------------------|
| OFF-RAMP | 2 | OUTPUT POINT | 111. | 55.54 | 19.05 | 1.20 | 6.27 | 0.33 | 7.80 |

 **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 **

 * ORIGINS DESTINATIONS ACROSS *
 * DOWN *
 * 1 2 3 4 5 6 7 *
 * *****

| ID | ORIGIN | DESTINATION | VOLUME | AVG SPEED | AVG DENSITY | LOS | FUEL | EMISSIONS |
|--------|--------|-------------|--------|-----------|-------------|-------|------|-----------|
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 19.74 | 20.05 | 20.86 | 21.05 | 23.08 | 0.00 | |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 1.96 | 3.99 | 0.00 | |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.21 | 0.00 | |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.90 | 0.00 | |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.74 | 0.00 | |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.06 | 0.00 | |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.92 | 0.00 | |
| * 9 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| * 10 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| * 11 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB SEC | NO. LNS | SSEC LENGTH | O-D ORG | DATA DES | DEMANDS SSEC | ADJUSTED ORG | DES | VOLUMES SSEC | SSEC CAP. | WEAVE EFF | CONGEST LENGTH | STORAGE RATE | V/C RATIO | SPEED MPH | DENSITY VPMP | LOS LEVEL | FUEL MPG | EMISSIONS GS/VM |
|---------|---------|-------------|---------|----------|--------------|--------------|-------|--------------|-----------|-----------|----------------|--------------|-----------|-----------|--------------|-----------|----------|-----------------|
| * 1 | | | | | | | | | | | | | | | | | | |
| * 2 | 2 | 99999. | 1710. | 0. | 1710. | 1710. | 0. | 1710. | 3000. | 0. | 0. | 0. | .57 | 65. | 13.2 | B | 20.0 | 13.7 |
| * 3 | 2 | 2740. | 0. | 0. | 1710. | 0. | 0. | 1710. | 3000. | 0. | 0. | 0. | .57 | 65. | 13.2 | B | 20.0 | 13.7 |
| * 4 | 2 | 600. | 0. | 0. | 1710. | 0. | 0. | 1710. | 3000. | 0. | 0. | 0. | .57 | 65. | 13.2 | B | 20.0 | 13.7 |
| * 5 | 2 | 700. | 0. | 0. | 1710. | 0. | 0. | 1710. | 3000. | 0. | 0. | 0. | .57 | 65. | 13.2 | B | 20.0 | 13.7 |
| * 6 | 2 | 2630. | 0. | 0. | 1710. | 0. | 0. | 1710. | 3000. | 0. | 0. | 0. | .57 | 65. | 13.2 | B | 20.0 | 13.7 |
| * 7 | 2 | 2530. | 0. | 0. | 1710. | 0. | 0. | 1710. | 3000. | 0. | 0. | 0. | .57 | 65. | 13.2 | B | 20.0 | 13.7 |
| * 8 | 2 | 1500. | 96. | 0. | 1806. | 96. | 0. | 1806. | 3000. | 0. | 0. | 0. | .60 | 65. | 13.9 | B | 20.0 | 13.7 |
| * 9 | 2 | 700. | 0. | 0. | 1806. | 0. | 0. | 1806. | 3000. | 0. | 0. | 0. | .60 | 65. | 13.9 | B | 20.0 | 13.7 |
| * 10 | 2 | 1500. | 0. | 374. | 1806. | 0. | 275. | 1806. | 3000. | 0. | 0. | 0. | .60 | 65. | 13.9 | B | 20.0 | 13.7 |
| * 11 | 2 | 750. | 0. | 0. | 1432. | 0. | 0. | 1432. | 3000. | 0. | 0. | 0. | .48 | 65. | 11.0 | B | 20.0 | 13.7 |
| * 12 | 2 | 350. | 124. | 0. | 1556. | 124. | 0. | 1556. | 3000. | 0. | 0. | 0. | .52 | 65. | 12.0 | B | 20.0 | 13.7 |
| * 13 | 2 | 350. | 0. | 0. | 1556. | 0. | 0. | 1556. | 3000. | 0. | 0. | 0. | .52 | 65. | 12.0 | B | 20.0 | 13.7 |
| * 14 | 2 | 350. | 0. | 167. | 1556. | 0. | 167. | 1556. | 3000. | 0. | 0. | 0. | .52 | 65. | 12.0 | B | 20.0 | 13.7 |
| * 15 | 2 | 700. | 0. | 0. | 1389. | 0. | 0. | 1389. | 3000. | 0. | 0. | 0. | .46 | 65. | 10.7 | A | 20.0 | 13.7 |
| * 16 | 2 | 900. | 164. | 0. | 1553. | 164. | 0. | 1553. | 3000. | 0. | 0. | 0. | .52 | 65. | 11.9 | B | 20.0 | 13.7 |
| * 17 | 2 | 1400. | 114. | 0. | 1667. | 114. | 0. | 1667. | 3000. | 0. | 0. | 0. | .56 | 65. | 12.8 | B | 20.0 | 13.7 |
| * 18 | 2 | 200. | 0. | 0. | 1667. | 0. | 0. | 1667. | 3000. | 0. | 0. | 0. | .56 | 65. | 12.8 | B | 20.0 | 13.7 |
| * 19 | 2 | 1400. | 0. | 96. | 1667. | 0. | 96. | 1667. | 3000. | 0. | 0. | 0. | .56 | 65. | 12.8 | B | 20.0 | 13.7 |
| * 20 | 2 | 900. | 0. | 0. | 1571. | 0. | 0. | 1571. | 3000. | 0. | 0. | 0. | .52 | 65. | 12.1 | B | 20.0 | 13.7 |
| * 21 | 2 | 100. | 66. | 0. | 1637. | 66. | 0. | 1637. | 3000. | 0. | 0. | 0. | .55 | 65. | 12.6 | B | 20.0 | 13.7 |
| * 22 | 2 | 100. | 0. | 32. | 1637. | 0. | 32. | 1637. | 3000. | 0. | 0. | 0. | .55 | 65. | 12.6 | B | 20.0 | 13.7 |
| * 23 | 2 | 600. | 0. | 0. | 1605. | 0. | 0. | 1605. | 3000. | 0. | 0. | 0. | .54 | 65. | 12.3 | B | 20.0 | 13.7 |
| * 24 | 2 | 1500. | 50. | 0. | 1655. | 50. | 0. | 1655. | 3000. | 0. | 0. | 0. | .55 | 65. | 12.7 | B | 20.0 | 13.7 |
| * 25 | 2 | 1500. | 0. | 0. | 1655. | 0. | 0. | 1655. | 3000. | 0. | 0. | 0. | .55 | 65. | 12.7 | B | 20.0 | 13.7 |
| * 26 | 2 | 8000. | 0. | 1655. | 1655. | 0. | 1655. | 1655. | 3000. | 0. | 0. | 0. | .55 | 65. | 12.7 | B | 20.0 | 13.7 |
| * 27 | | | | | | | | | | | | | | | | | | |
| * 28 | | | | | | | | | | | | | | | | | | |
| * 29 | | | | | | | | | | | | | | | | | | |

TOTAL 131999. = 25.0 MILES MAX(V/C) = 0.60 LOWEST LOS = B AVG = 65. 13.1 20.0 13.7

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|-----------------------------|-----------------------------------|------------------------------------|
| FREWAY TRAVEL TIME = | 654. VEH-HRS 1308. PASS-HRS | 1358. VEH-HRS 2717. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 161. VEH-HRS 321. PASS-HRS | 216. VEH-HRS 432. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 814. VEH-HRS 1629. PASS-HRS | 1575. VEH-HRS 3149. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 42496. VEH-MI. 84993. PASS-MI. | 88294. VEH-MI. 176589. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 52. MPH. | 65. MPH. |
| AVERAGE DENSITY = | 13. VPMP | 14. VPMP |
| TOTAL FUEL = | 2180. GALLONS | 4489. GALLONS |
| TOTAL EMISSIONS = | 606. KILOGRAMS | 1244. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| | | | | | | | | | |

US-101_SB_PM_P1_2040_PL

| | | | | | | | | | |
|----|------|----|------|----|------|----|------|----|------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

***** RAMP DELAYS *****

| OFF-RAMP | 2 | OUTPUT POINT | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|----------|---|--------------|--------------------------|------------------|-------------|------------|------------|-------------|----------------------------|
| | | | 210. | 160.61 | 55.09 | 3.47 | 18.12 | 0.96 | 22.55 |

 ** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS | | * DESTINATIONS ACROSS | | | | | | |
|-----------|------|-----------------------|-------|-------|-------|-------|------|------|
| * DOWN | | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 19.74 | 20.05 | 20.86 | 21.05 | 23.08 | 0.00 | |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 1.96 | 3.99 | 0.00 | |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.21 | 0.00 | |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.90 | 0.00 | |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.74 | 0.00 | |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.06 | 0.00 | |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.92 | 0.00 | |
| * 9 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| * 10 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| * 11 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |

 * TIME SLICE FREEWAY PERFORMANCE TABLE *

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | | |
|-----------|----------|------------|-----------|--------------------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|------|---|------|------|
| * SEC LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES SSEC | * CAP | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | | | |
| * 1 | | | | | | | | | | | | | | | | | | |
| * 2 | 2 | 99999. | 1554. | 0. | 1554. | 1554. | 0. | 1554. | 3000. | 0. | 0. | 0. | .52 | 65. | 12.0 | B | 20.0 | 13.7 |
| * 3 | 2 | 2740. | 0. | 0. | 1554. | 0. | 0. | 1554. | 3000. | 0. | 0. | 0. | .52 | 65. | 12.0 | B | 20.0 | 13.7 |
| * 4 | 2 | 600. | 0. | 0. | 1554. | 0. | 0. | 1554. | 3000. | 0. | 0. | 0. | .52 | 65. | 12.0 | B | 20.0 | 13.7 |
| * 5 | 2 | 700. | 0. | 0. | 1554. | 0. | 0. | 1554. | 3000. | 0. | 0. | 0. | .52 | 65. | 12.0 | B | 20.0 | 13.7 |
| * 6 | 2 | 2630. | 0. | 0. | 1554. | 0. | 0. | 1554. | 3000. | 0. | 0. | 0. | .52 | 65. | 12.0 | B | 20.0 | 13.7 |
| * 7 | 2 | 2530. | 0. | 0. | 1554. | 0. | 0. | 1554. | 3000. | 0. | 0. | 0. | .52 | 65. | 12.0 | B | 20.0 | 13.7 |
| * 8 | 2 | 1500. | 77. | 0. | 1631. | 77. | 0. | 1631. | 3000. | 0. | 0. | 0. | .54 | 65. | 12.5 | B | 20.0 | 13.7 |
| * 9 | 2 | 700. | 0. | 0. | 1631. | 0. | 0. | 1631. | 3000. | 0. | 0. | 0. | .54 | 65. | 12.5 | B | 20.0 | 13.7 |
| * 10 | 2 | 1500. | 0. | 338. | 1631. | 0. | 279. | 1631. | 3000. | 0. | 0. | 0. | .54 | 65. | 12.5 | B | 20.0 | 13.7 |
| * 11 | 2 | 750. | 0. | 0. | 1293. | 0. | 0. | 1293. | 3000. | 0. | 0. | 0. | .43 | 65. | 9.9 | A | 20.0 | 13.7 |
| * 12 | 2 | 350. | 142. | 0. | 1435. | 142. | 0. | 1435. | 3000. | 0. | 0. | 0. | .48 | 65. | 11.0 | B | 20.0 | 13.7 |
| * 13 | 2 | 350. | 0. | 0. | 1435. | 0. | 0. | 1435. | 3000. | 0. | 0. | 0. | .48 | 65. | 11.0 | B | 20.0 | 13.7 |
| * 14 | 2 | 350. | 0. | 135. | 1435. | 0. | 135. | 1435. | 3000. | 0. | 0. | 0. | .48 | 65. | 11.0 | B | 20.0 | 13.7 |
| * 15 | 2 | 700. | 0. | 0. | 1300. | 0. | 0. | 1300. | 3000. | 0. | 0. | 0. | .43 | 65. | 10.0 | A | 20.0 | 13.7 |
| * 16 | 2 | 900. | 131. | 0. | 1431. | 131. | 0. | 1431. | 3000. | 0. | 0. | 0. | .48 | 65. | 11.0 | B | 20.0 | 13.7 |
| * 17 | 2 | 1400. | 91. | 0. | 1522. | 91. | 0. | 1522. | 3000. | 0. | 0. | 0. | .51 | 65. | 11.7 | B | 20.0 | 13.7 |
| * 18 | 2 | 200. | 0. | 0. | 1522. | 0. | 0. | 1522. | 3000. | 0. | 0. | 0. | .51 | 65. | 11.7 | B | 20.0 | 13.7 |
| * 19 | 2 | 1400. | 0. | 85. | 1522. | 0. | 85. | 1522. | 3000. | 0. | 0. | 0. | .51 | 65. | 11.7 | B | 20.0 | 13.7 |
| * 20 | 2 | 900. | 0. | 0. | 1437. | 0. | 0. | 1437. | 3000. | 0. | 0. | 0. | .48 | 65. | 11.1 | B | 20.0 | 13.7 |
| * 21 | 2 | 100. | 52. | 0. | 1489. | 52. | 0. | 1489. | 3000. | 0. | 0. | 0. | .50 | 65. | 11.5 | B | 20.0 | 13.7 |
| * 22 | 2 | 100. | 0. | 30. | 1489. | 0. | 30. | 1489. | 3000. | 0. | 0. | 0. | .50 | 65. | 11.5 | B | 20.0 | 13.7 |
| * 23 | 2 | 600. | 0. | 0. | 1459. | 0. | 0. | 1459. | 3000. | 0. | 0. | 0. | .49 | 65. | 11.2 | B | 20.0 | 13.7 |
| * 24 | 2 | 1500. | 60. | 0. | 1519. | 60. | 0. | 1519. | 3000. | 0. | 0. | 0. | .51 | 65. | 11.7 | B | 20.0 | 13.7 |

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US-101_SB_PM_P1_2040_PL
* 25 2 1500. 0. 0. 1519. 0. 0. 1519. 3000. 0. 0. .51 65. 11.7 B 20.0 13.7 *
* 26 2 8000. 0. 1519. 1519. 0. 1519. 1519. 3000. 0. 0. .51 65. 11.7 B 20.0 13.7 *
* 27 *
* 28 *
* 29 *
*****
*
* TOTAL 131999. = 25.0 MILES MAX(V/C) = 0.54 LOWEST LOS = B AVG = 65. 11.9 20.0 13.7 *
*****

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CURRENT TIME SLICE CUMULATIVE VALUES
FREEWAY TRAVEL TIME = 595. VEH-HRS 1190. PASS-HRS 1953. VEH-HRS 3906. PASS-HRS
FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 240. VEH-HRS 480. PASS-HRS 456. VEH-HRS 912. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 835. VEH-HRS 1669. PASS-HRS 2409. VEH-HRS 4818. PASS-HRS
TOTAL FRWAY TRAV DISTANCE = 38664. VEH-MI. 77327. PASS-MI. 126958. VEH-MI. 253916. PASS-MI.
AVERAGE SYSTEM SPEED = 46. MPH. 65. MPH.
AVERAGE DENSITY = 12. VPMP 13. VPMP
TOTAL FUEL = 2015. GALLONS 6504. GALLONS
TOTAL EMISSIONS = 565. KILOGRAMS 1808. KILOGRAMS

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***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

***** RAMP DELAYS *****

| OFF-RAMP | OUTPUT POINT | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|----------|--------------|--------------------------|------------------|-------------|------------|------------|-------------|----------------------------|
| 2 | OUTPUT POINT | 270. | 239.85 | 82.27 | 5.18 | 27.06 | 1.44 | 33.68 |

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FFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQ 1111 222222 PPPPPPPP EEEEEEEEE
FFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP EEEEEEEEE
FFF RRR RRR EEE QQQQQ QQQQQ 1111 222 222 PPP PPP EEE
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP EEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP EEEEEEE
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP EEE
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP EEE
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP EEEEEEEEE
FFF RRR RRR EEEEEEEEE Q*1999*Q QQQ 1111111 222222222 PPP EEEEEEEEE
    
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FREQ12PEB

1. THE OBJECTIVE FUNCTION WILL MAXIMIZE PASSENGER INPUT RATE.
2. THERE ARE 1.0 TIME SLICES PER HOUR.
3. WEAVING ANALYSIS IS NOT ENGAGED.
4. NO ALTERNATE ROUTE IS PROVIDED.
5. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
6. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
7. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
8. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
9. REDUCED CAPACITIES ARE SUPPLIED BY THE USER.
10. THE CAPACITY BUFFER IS 0.00 (V/C).

FREWAY AND ARTERIAL DESIGN FEATURES

| ** SUB NO. | ** SSEC | ** SSEC | ** DESIG N | ** ORG | ** TRK | ** SSEC | ** PCT | ** PCT | ** DES | ** SPECIAL | ** FF. SPD. | ** CAP. | ** ART | ** GRADE | ** SUBSECTI ON | ** LOCATI ON |
|------------|---------|---------|------------|----------|--------|---------|--------|-----------|---------|-------------|-------------|---------|-------------|-------------|-------------------------|--------------|
| ** SEC | ** LNS | ** CAP | ** LENGTH | ** SPEED | ** DES | ** GRAD | ** TRK | ** TRUCKS | ** RAMP | ** ALT. RTE | ** ALT. RTE | ** TYPE | ** ALT. RTE | ** ALT. RTE | ** LOCATION | ** LOCATION |
| ** 1 | 5 | 10000. | 1370. | 65 | OD | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Seeding | ** |
| ** 2 | 3 | 7360. | 99999. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture | ** |
| ** 3 | 3 | 6000. | 2740. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-85 Off to Shore On | ** |
| ** 4 | 3 | 6000. | 600. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Shore. On to Moffet Off | ** |
| ** 5 | 3 | 6000. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Moffett Off to On | ** |
| ** 6 | 3 | 6000. | 2630. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Moffett On to Ellis Off | ** |
| ** 7 | 3 | 6000. | 2530. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Ellis Off to On-ramp | ** |
| ** 8 | 4 | 6770. | 1500. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Ellis On-ramp | ** |
| ** 9 | 4 | 6770. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Ellis / US 237 | ** |
| ** 10 | 4 | 6770. | 1500. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 EB Off-Ramp | ** |
| ** 11 | 3 | 6000. | 750. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 / SR-237 | ** |
| ** 12 | 4 | 7010. | 350. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 EB On-Ramp | ** |
| ** 13 | 4 | 7010. | 350. | 65 | | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | US 237 / Mathilda | ** |
| ** 14 | 4 | 7010. | 350. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-Ramp | ** |
| ** 15 | 3 | 6000. | 700. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda | ** |
| ** 16 | 3 | 6000. | 900. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda SB On-Ramp | ** |
| ** 17 | 3 | 6000. | 1400. | 65 | 0 | 0.96 | 0.0 | 4 | 0 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda NB On-Ramp | ** |
| ** 18 | 3 | 6000. | 200. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Fair Oaks | ** |
| ** 19 | 3 | 6000. | 1400. | 65 | D | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks SB Off-Ramp | ** |
| ** 20 | 3 | 6000. | 900. | 65 | | 0.96 | 0.0 | 4 | 0 | NO | 0.0 | 0. | GOOD | 0.0 | Fair Oaks SB/ Fair Oaks | ** |

TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB SEC | NO. LNS | SSEC LENGTH | O-D ORG | DATA DES | DEMANDS SSEC | ADJUSTED ORG | VOLUMES DES | SSEC SSEC | SSEC CAP | WEAVE EFF | CONGEST LENGTH | STORAGE RATE | V/C RATIO | SPEED MPH | DENSITY VPMP | LOS LEVEL | FUEL MPG | EMI SS GS/VM | |
|---------|---------|-------------|---------|----------|--------------|--------------|-------------|-----------|----------|-----------|-----------------|----------------|-----------|-----------|--------------|-----------|----------|--------------|------|
| * | 1 | 5 | 1370. | 9199. | 1840. | 9199. | 9199. | 1840. | 9199. | 10000. | 0. | 0. | 0. | .92 | 58. | 31.7 | D | 22.2 | 12.0 |
| * | 2 | 3 | 99999. | 0. | 0. | 7359. | 0. | 0. | 6000. | 7360. | 0. | * 21659. | 1359. | .82 | 41. | 49.0 | F | 22.5 | 12.0 |
| * | 3 | 3 | 2740. | 0. | 0. | 7359. | 0. | 0. | 6000. | 6000. | 0. | 0. | 0. | 1.00 | 52. | 38.3 | E | 23.8 | 11.1 |
| * | 4 | 3 | 600. | 0. | 0. | 7359. | 0. | 0. | 3062. | 6000. | 0. | * 294. | 2938. | .51 | 52. | 19.8 | F | 23.7 | 11.2 |
| * | 5 | 3 | 700. | 0. | 0. | 7359. | 0. | 0. | 3062. | 6000. | 0. | ** 700. | 2938. | .51 | 47. | 21.6 | F | 23.3 | 11.3 |
| * | 6 | 3 | 2630. | 0. | 0. | 7359. | 0. | 0. | 3062. | 6000. | 0. | ** 2630. | 2938. | .51 | 38. | 27.1 | F | 22.2 | 11.8 |
| * | 7 | 3 | 2530. | 0. | 0. | 7359. | 0. | 0. | 3062. | 6000. | 0. | ** 2530. | 2938. | .51 | 28. | 36.3 | F | 20.5 | 12.7 |
| * | 8 | 4 | 1500. | 642. | 0. | 8001. | 592. | 0. | 3654. | 6673. | 0. | ** 1500. | 2938. | .55 | 24. | 38.0 | F | 19.0 | 13.6 |
| * | 9 | 4 | 700. | 0. | 0. | 8001. | 0. | 0. | 3654. | 6770. | 0. | ** 700. | 2938. | .54 | 22. | 42.4 | F | 18.2 | 14.2 |
| * | 10 | 4 | 1500. | 0. | 1711. | 8001. | 0. | 1111. | 3654. | 6381. | 0. | ** 1500. | 2727. | .57 | 23. | 39.1 | F | 18.9 | 13.7 |
| * | 11 | 3 | 750. | 0. | 0. | 6290. | 0. | 0. | 2287. | 6000. | 0. | ** 750. | 2727. | .38 | 16. | 48.5 | F | 16.8 | 15.5 |
| * | 12 | 4 | 350. | 702. | 0. | 6992. | 652. | 0. | 2939. | 6873. | 0. | ** 350. | 2727. | .43 | 16. | 47.3 | F | 15.4 | 16.8 |
| * | 13 | 4 | 350. | 0. | 0. | 6992. | 0. | 0. | 2939. | 7010. | 0. | ** 350. | 2727. | .42 | 14. | 50.9 | F | 15.2 | 17.0 |
| * | 14 | 4 | 350. | 0. | 804. | 6992. | 0. | 654. | 2939. | 6848. | 0. | ** 350. | 2727. | .43 | 14. | 51.8 | F | 15.0 | 17.2 |
| * | 15 | 3 | 700. | 0. | 0. | 6188. | 0. | 0. | 2285. | 6000. | 0. | ** 700. | 2727. | .38 | 12. | 61.6 | F | 15.7 | 16.4 |
| * | 16 | 3 | 900. | 733. | 0. | 6921. | 633. | 0. | 2918. | 5834. | 0. | ** 900. | 2727. | .50 | 15. | 66.7 | F | 15.9 | 15.9 |
| * | 17 | 3 | 1400. | 407. | 0. | 7328. | 307. | 0. | 3225. | 5908. | 0. | ** 1400. | 2683. | .55 | 15. | 72.7 | F | 15.7 | 16.2 |
| * | 18 | 3 | 200. | 0. | 0. | 7328. | 0. | 0. | 3225. | 6000. | 0. | ** 200. | 2683. | .54 | 14. | 78.1 | F | 15.1 | 16.7 |
| * | 19 | 3 | 1400. | 0. | 489. | 7328. | 0. | 396. | 3225. | 5919. | 0. | ** 1400. | 2683. | .54 | 13. | 81.1 | F | 14.9 | 17.0 |
| * | 20 | 3 | 900. | 0. | 0. | 6839. | 0. | 0. | 2829. | 6000. | 0. | ** 900. | 2683. | .47 | 10. | 90.6 | F | 13.8 | 18.1 |
| * | 21 | 4 | 100. | 257. | 0. | 7096. | 240. | 0. | 3069. | 6187. | 0. | ** 100. | 2683. | .50 | 11. | 72.0 | F | 12.7 | 19.8 |
| * | 22 | 4 | 100. | 0. | 136. | 7096. | 0. | 111. | 3069. | 6226. | 0. | ** 100. | 2683. | .49 | 10. | 73.3 | F | 12.7 | 19.9 |
| * | 23 | 3 | 600. | 0. | 0. | 6960. | 0. | 0. | 2958. | 6000. | 0. | ** 600. | 2683. | .49 | 10. | 97.2 | F | 13.4 | 18.7 |
| * | 24 | 3 | 1500. | 224. | 0. | 7184. | 224. | 0. | 3182. | 5944. | 0. | ** 1500. | 2683. | .54 | 10. | 101.7 | F | 13.2 | 19.0 |
| * | 25 | 3 | 1500. | 0. | 0. | 7184. | 0. | 0. | 3182. | 6000. | 0. | ** 1500. | 2683. | .53 | 9. | 113.3 | F | 12.4 | 20.0 |
| * | 26 | 3 | 8000. | 0. | 0. | 7184. | 0. | 0. | 3182. | 6000. | 0. | ** 8000. | 2683. | .53 | 7. | 151.7 | F | 10.4 | 23.6 |
| * | 27 | 5 | 100. | 1796. | 0. | 8980. | 1796. | 0. | 4978. | 10000. | 0. | ** 100. | 2683. | .50 | 5. | 202.7 | F | 8.6 | 28.0 |
| * | 28 | 5 | 1000. | 1560. | 0. | 10540. | 1212. | 0. | 6190. | 7750. | 0. | ** 1000. | 1560. | .80 | 12. | 100.6 | F | 14.4 | 20.9 |
| * | 29 | 5 | 1000. | 1560. | 12100. | 12100. | 1560. | 7750. | 7750. | 7750. | 0. | 0. | 0. | 1.00 | 52. | 29.7 | E | 23.8 | 11.1 |
| * | TOTAL | 135469. | = | 25.7 | MILES | | | | | | MAX(V/C) = 1.00 | LOWEST LOS = F | AVG = 31. | 56.5 | | | 20.9 | 12.8 | |

| | CURRENT TIME SLICE | CUMULATIVE VALUES |
|----------------------------|--------------------|-------------------|
| FREEWAY TRAVEL TIME = | 5514. VEH-HRS | 5555. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 333. VEH-HRS | 367. PASS-HRS |
| OFF-RAMP DELAY = | 128. VEH-HRS | 128. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 5974. VEH-HRS | 6050. PASS-HRS |
| TOTAL TRAV DISTANCE = | 170614. VEH-MI. | 171705. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 29. MPH | 31. MPH |
| AVERAGE DENSITY = | 56. VPMP | 56. VPMP |
| TOTAL FUEL = | 8328. GALLONS | 8328. GALLONS |
| TOTAL EMISSIONS = | 2243. KI LOGRAMS | 2243. KI LOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|--------|------------|-------|------------|-------|------------|-------|------------|--------|
| 1 | 4.39 | 2 | ***** | 3 | 11.72 | 4 | 2.72 | 5 | 4.55 |
| 6 | 32.18 | 7 | 53.45 | 8 | 44.12 | 9 | 23.90 | 10 | 44.40 |
| 11 | 28.91 | 12 | 15.60 | 13 | 16.98 | 14 | 17.21 | 15 | 34.65 |
| 16 | 41.13 | 17 | 65.57 | 18 | 10.11 | 19 | 73.13 | 20 | 56.21 |
| 21 | 6.35 | 22 | 6.47 | 23 | 38.92 | 24 | 96.94 | 25 | 106.47 |
| 26 | 705.28 | 27 | 18.02 | 28 | 77.66 | 29 | 5.53 | | |

***** TOTAL DELAY = 2889.0 VEH-HRS ***** AVERAGE DELAY = 42.96 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GAL | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-----------|-----------------------|---------------|--------------------------------|---------|---------|---------|----------|----------------------|
| ON-RAMP 2 | RAMP 50. | 25.00 | 2.34 | 8.93 | 0.55 | 2.90 | 0.15 | 3.60 |

| | | US-101_SB_PM_P2_2040_PE | | | | | | | |
|----------|---|-------------------------|------|--------|------|-------|------|-------|------|
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 50. | 25.00 | 2.34 | 8.93 | 0.55 | 2.90 | 0.15 |
| ON-RAMP | 3 | RAMP | 50. | 25.00 | 2.14 | 8.93 | 0.55 | 2.90 | 0.15 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 50. | 25.00 | 2.14 | 8.93 | 0.55 | 2.90 | 0.15 |
| ON-RAMP | 4 | RAMP | 100. | 50.00 | 4.09 | 17.85 | 1.11 | 5.79 | 0.31 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 50.00 | 4.09 | 17.85 | 1.11 | 5.79 | 0.31 |
| ON-RAMP | 5 | RAMP | 100. | 50.00 | 7.37 | 17.85 | 1.11 | 5.79 | 0.31 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 50.00 | 7.37 | 17.85 | 1.11 | 5.79 | 0.31 |
| ON-RAMP | 6 | RAMP | 17. | 8.50 | 1.98 | 3.04 | 0.19 | 0.98 | 0.05 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 17. | 8.50 | 1.98 | 3.04 | 0.19 | 0.98 | 0.05 |
| ON-RAMP | 9 | RAMP | 348. | 174.00 | 8.37 | 62.13 | 3.85 | 20.16 | 1.07 |
| | | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 348. | 174.00 | 8.37 | 62.13 | 3.85 | 20.16 | 1.07 |
| OFF-RAMP | 2 | OUTPUT POINT | 256. | 127.80 | | 45.64 | 2.83 | 14.81 | 0.79 |

1 INSTITUTE OF TRANSPORTATION STUDIES
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 SIMULATION AFTER CONTROL, NO DIVERSION
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 QUEUE COLLISION IN SECTION 3 T2 =0.129

1 INSTITUTE OF TRANSPORTATION STUDIES
 UNIVERSITY OF CALIFORNIA, BERKELEY
 FREQ12PE REL 3.01
 SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 3
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 **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 **

| | | ORIGINS DESTINATIONS ACROSS | | | | | | |
|---|---|-----------------------------|------|-------|-------|-------|-------|-------|
| | | DOWN | | | | | | |
| | | 1 | 2 | 3 | 4 | 5 | 6 | |
| + | * | 1 | 0.25 | 62.73 | 65.36 | 69.63 | 70.80 | 82.57 |
| + | * | 2 | 0.00 | 3.36 | 5.99 | 10.26 | 11.43 | 23.20 |
| + | * | 3 | 0.00 | 0.00 | 1.51 | 5.78 | 6.96 | 18.72 |
| + | * | 4 | 0.00 | 0.00 | 0.00 | 3.20 | 4.37 | 16.13 |
| + | * | 5 | 0.00 | 0.00 | 0.00 | 2.33 | 3.51 | 15.27 |
| + | * | 6 | 0.00 | 0.00 | 0.00 | 0.00 | 0.21 | 11.97 |
| + | * | 7 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 11.15 |
| + | * | 8 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.96 |
| + | * | 9 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.81 |
| + | * | 10 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.22 |
| + | * | * | * | * | * | * | * | * |

1 INSTITUTE OF TRANSPORTATION STUDIES
 UNIVERSITY OF CALIFORNIA, BERKELEY
 FREQ12PE REL 3.01
 SIMULATION AFTER CONTROL, NO DIVERSION
 TIME SLICE 2 OF 3
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TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB | * NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED | * VOLUMES | * SSEC | * WEAVE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | |
|-------|-------|----------|------------|-----------|------------|-----------|---------|---------|-----------|-----------|----------|---------|-----------|--------|---------|-------------|--------|--------|
| * SEC | * LNS | * LENGTH | * ORG | * DES | * SSEC | * ORG | * DES | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * GS/VM | | |
| * 1 | * 5 | * 1370. | * 8550. | * 1710. | * 8550. | * 8550. | * 1710. | * 8550. | * 10000. | * 0. | * 0. | * .86 | * 61. | * 27.9 | * D | * 20.9 | * 12.8 | |
| * 2 | * 3 | * 99999. | * 0. | * 0. | * 6840. | * 0. | * 0. | * 4662. | * 7360. | * 0. | * 41706. | * 2178. | * .63 | * 23. | * 68.4 | * F | * 17.6 | * 15.0 |
| * 3 | * 3 | * 2740. | * 0. | * 0. | * 6840. | * 0. | * 0. | * 4662. | * 6000. | * 0. | * 2740. | * 1338. | * .78 | * 12. | * 128.6 | * F | * 14.4 | * 20.9 |
| * 4 | * 3 | * 600. | * 0. | * 0. | * 6840. | * 0. | * 0. | * 4662. | * 6000. | * 0. | * 600. | * 1338. | * .78 | * 11. | * 137.8 | * F | * 13.8 | * 21.8 |
| * 5 | * 3 | * 700. | * 0. | * 0. | * 6840. | * 0. | * 0. | * 4661. | * 6000. | * 0. | * 700. | * 1338. | * .78 | * 11. | * 138.4 | * F | * 13.8 | * 21.8 |
| * 6 | * 3 | * 2630. | * 0. | * 0. | * 6840. | * 0. | * 0. | * 4661. | * 6000. | * 0. | * 2630. | * 1338. | * .78 | * 11. | * 138.4 | * F | * 13.8 | * 21.8 |
| * 7 | * 3 | * 2530. | * 0. | * 0. | * 6840. | * 0. | * 0. | * 4661. | * 6000. | * 0. | * 2530. | * 1338. | * .78 | * 11. | * 138.4 | * F | * 13.8 | * 21.8 |
| * 8 | * 4 | * 1500. | * 672. | * 0. | * 7512. | * 672. | * 0. | * 5334. | * 6674. | * 0. | * 1500. | * 1338. | * .80 | * 12. | * 110.5 | * F | * 14.3 | * 21.2 |
| * 9 | * 4 | * 700. | * 0. | * 0. | * 7512. | * 0. | * 0. | * 5334. | * 6770. | * 0. | * 700. | * 1338. | * .79 | * 12. | * 114.6 | * F | * 14.0 | * 21.5 |

US-101_SB_PM_P2_2040_PE

| | | | | | | | | | | | | | | | | | | | | | |
|-------|-------|---------|-------|-------|-------|-------|-------|-------|-------|--------|----|----|-----------------|----------------|-----------|------|-------|---|------|------|---|
| * | 10 | 4 | 1500. | 0. | 1666. | 7512. | 0. | 1126. | 5334. | 6396. | 0. | ** | 1500. | 1062. | .83 | 14. | 98.7 | F | 15.2 | 20.0 | * |
| * | 11 | 3 | 750. | 0. | 0. | 5846. | 0. | 0. | 3913. | 6000. | 0. | ** | 750. | 1062. | .65 | 8. | 170.9 | F | 10.4 | 25.6 | * |
| * | 12 | 4 | 350. | 670. | 0. | 6516. | 670. | 0. | 4583. | 6886. | 0. | ** | 350. | 1062. | .67 | 8. | 144.1 | F | 10.7 | 25.2 | * |
| * | 13 | 4 | 350. | 0. | 0. | 6516. | 0. | 0. | 4583. | 7010. | 0. | ** | 350. | 1062. | .65 | 8. | 149.4 | F | 10.4 | 25.5 | * |
| * | 14 | 4 | 350. | 0. | 842. | 6516. | 0. | 731. | 4583. | 6843. | 0. | ** | 350. | 1062. | .67 | 8. | 142.3 | F | 10.8 | 25.1 | * |
| * | 15 | 3 | 700. | 0. | 0. | 5674. | 0. | 0. | 3852. | 6000. | 0. | ** | 700. | 1062. | .64 | 7. | 173.6 | F | 10.2 | 25.9 | * |
| * | 16 | 3 | 900. | 779. | 0. | 6453. | 779. | 0. | 4631. | 5831. | 0. | ** | 900. | 1062. | .79 | 12. | 130.0 | F | 14.2 | 21.3 | * |
| * | 17 | 3 | 1400. | 436. | 0. | 6889. | 436. | 0. | 5067. | 5906. | 0. | ** | 1400. | 837. | .86 | 15. | 115.3 | F | 16.0 | 19.1 | * |
| * | 18 | 3 | 200. | 0. | 0. | 6889. | 0. | 0. | 5067. | 6000. | 0. | ** | 200. | 837. | .84 | 14. | 120.7 | F | 15.5 | 19.6 | * |
| * | 19 | 3 | 1400. | 0. | 608. | 6889. | 0. | 520. | 5067. | 5904. | 0. | ** | 1400. | 837. | .86 | 15. | 115.2 | F | 16.0 | 19.1 | * |
| * | 20 | 3 | 900. | 0. | 0. | 6281. | 0. | 0. | 4547. | 6000. | 0. | ** | 900. | 837. | .76 | 11. | 143.3 | F | 13.5 | 22.3 | * |
| * | 21 | 4 | 100. | 274. | 0. | 6555. | 240. | 0. | 4787. | 6184. | 0. | ** | 100. | 837. | .77 | 11. | 107.5 | F | 13.8 | 21.9 | * |
| * | 22 | 4 | 100. | 0. | 194. | 6555. | 0. | 165. | 4787. | 6218. | 0. | ** | 100. | 837. | .77 | 11. | 108.9 | F | 13.7 | 22.0 | * |
| * | 23 | 3 | 600. | 0. | 0. | 6361. | 0. | 0. | 4622. | 6000. | 0. | ** | 600. | 837. | .77 | 11. | 140.0 | F | 13.7 | 22.0 | * |
| * | 24 | 3 | 1500. | 200. | 0. | 6561. | 200. | 0. | 4822. | 5950. | 0. | ** | 1500. | 837. | .81 | 13. | 128.5 | F | 14.6 | 20.8 | * |
| * | 25 | 3 | 1500. | 0. | 0. | 6561. | 0. | 0. | 4822. | 6000. | 0. | ** | 1500. | 837. | .80 | 12. | 131.3 | F | 14.4 | 21.0 | * |
| * | 26 | 3 | 8000. | 0. | 0. | 6561. | 0. | 0. | 4822. | 6000. | 0. | ** | 8000. | 837. | .80 | 12. | 131.3 | F | 14.4 | 21.0 | * |
| * | 27 | 5 | 100. | 1640. | 0. | 8201. | 1640. | 0. | 6462. | 10000. | 0. | ** | 100. | 837. | .65 | 7. | 172.5 | F | 10.3 | 25.7 | * |
| * | 28 | 5 | 1000. | 520. | 0. | 8721. | 768. | 0. | 7230. | 7750. | 0. | ** | 1000. | 520. | .93 | 19. | 75.6 | F | 18.1 | 16.6 | * |
| * | 29 | 5 | 1000. | 520. | 9241. | 9241. | 520. | 7750. | 7750. | 7750. | 0. | ** | 0. | 0. | 1.00 | 52. | 29.7 | E | 23.8 | 11.1 | * |
| ***** | | | | | | | | | | | | | | | | | | | | | |
| * | TOTAL | 135469. | = | 25.7 | MI | LES | | | | | | | MAX(V/C) = 1.00 | LOWEST LOS = F | AVG = 19. | 82.5 | | | 16.9 | 16.1 | * |
| ***** | | | | | | | | | | | | | | | | | | | | | |

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 TIME SLICE 2 OF 3

| | CURRENT TIME SLICE | | | CUMULATIVE VALUES | | | | |
|----------------------------|--------------------|------------|---------|-------------------|---------|------------|---------|----------|
| FREEWAY TRAVEL TIME = | 7810. | VEH-HRS | 7846. | PASS-HRS | 13324. | VEH-HRS | 13401. | PASS-HRS |
| FREEWAY MERGE DELAY = | 0. | VEH-HRS | 0. | PASS-HRS | 0. | VEH-HRS | 0. | PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 558. | VEH-HRS | 603. | PASS-HRS | 891. | VEH-HRS | 970. | PASS-HRS |
| OFF-RAMP DELAY = | 403. | VEH-HRS | 404. | PASS-HRS | 531. | VEH-HRS | 533. | PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 8771. | VEH-HRS | 8854. | PASS-HRS | 14745. | VEH-HRS | 14904. | PASS-HRS |
| TOTAL TRAVEL DISTANCE = | 151773. | VEH-MI. | 152873. | PASS-MI. | 322387. | VEH-MI. | 324578. | PASS-MI. |
| AVERAGE SYSTEM SPEED = | 17. | MPH | | | 24. | MPH | | |
| AVERAGE DENSITY = | 83. | VPMP | | | 69. | VPMP | | |
| TOTAL FUEL = | 9345. | GALLONS | | | 17673. | GALLONS | | |
| TOTAL EMISSIONS = | 2587. | KI LOGRAMS | | | 4830. | KI LOGRAMS | | |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|--------|------------|--------|------------|--------|------------|-------|------------|-------|
| 1 | 2.07 | 2 | ***** | 3 | 166.26 | 4 | 38.88 | 5 | 45.52 |
| 6 | 171.03 | 7 | 164.53 | 8 | 102.30 | 9 | 49.91 | 10 | 88.82 |
| 11 | 64.29 | 12 | 33.54 | 13 | 34.94 | 14 | 33.05 | 15 | 61.19 |
| 16 | 54.36 | 17 | 71.06 | 18 | 10.76 | 19 | 70.97 | 20 | 61.36 |
| 21 | 6.75 | 22 | 6.86 | 23 | 39.66 | 24 | 88.43 | 25 | 90.85 |
| 26 | 484.55 | 27 | 14.45 | 28 | 50.52 | 29 | 5.53 | | |

***** TOTAL DELAY = 5475.4 VEH-HRS ***** AVERAGE DELAY = 69.69 MIN/VEH *****

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 TIME SLICE 2 OF 3

***** RAMP DELAYS *****

| | QUEUE LENGTH | DELAY | AVERAGE | GAS | HC | CO | NOX | TOTAL | |
|------------|--------------|---------|----------------|-------|--------|------|-------|-----------|-------|
| | VEHICLES | VEH-HRS | METERING DELAY | GALS | KGMS | KGMS | KGMS | EMISSIONS | |
| | | | MINUTES | | | | | KGMS | |
| ON-RAMP 2 | RAMP | 50. | 50.00 | 4.16 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 50. | 50.00 | 4.16 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| ON-RAMP 3 | RAMP | 50. | 50.00 | 4.17 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 50. | 50.00 | 4.17 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| ON-RAMP 4 | RAMP | 100. | 100.00 | 6.83 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 100.00 | 6.83 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP 5 | RAMP | 100. | 100.00 | 11.19 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 100.00 | 11.19 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP 6 | RAMP | 51. | 34.00 | 7.01 | 12.14 | 0.75 | 3.94 | 0.21 | 4.90 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 51. | 34.00 | 7.01 | 12.14 | 0.75 | 3.94 | 0.21 | 4.90 |
| ON-RAMP 9 | RAMP | 100. | 224.00 | 17.59 | 79.99 | 4.96 | 25.95 | 1.38 | 32.29 |
| | FREEWAY | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | TOTAL | 100. | 224.00 | 17.59 | 79.99 | 4.96 | 25.95 | 1.38 | 32.29 |
| OFF-RAMP 2 | OUTPUT POINT | 550. | 402.89 | | 143.86 | 8.92 | 46.67 | 2.48 | 58.07 |

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FREEMERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
 ON-RAMP MRG/CAP DELAY = 440. VEH-HRS 460. PASS-HRS 1331. VEH-HRS 1430. PASS-HRS
 OFF-RAMP DELAY = 677. VEH-HRS 679. PASS-HRS 1207. VEH-HRS 1212. PASS-HRS
 TOTAL SYSTEM TRAVEL TIME = 10599. VEH-HRS 10658. PASS-HRS 25344. VEH-HRS 25562. PASS-HRS
 TOTAL TRAVEL DISTANCE = 138358. VEH-MI. 139408. PASS-MI. 460745. VEH-MI. 463987. PASS-MI.
 AVERAGE SYSTEM SPEED = 13. MPH. 20. MPH.
 AVERAGE DENSITY = 109. VPMP 83. VPMP
 TOTAL FUEL = 9918. GALLONS 27591. GALLONS
 TOTAL EMISSIONS = 2765. KI LOGRAMS 7596. KI LOGRAMS

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|--------|------------|--------|------------|--------|------------|-------|------------|-------|
| 1 | 0.64 | 2 | ***** | 3 | 168.96 | 4 | 37.01 | 5 | 43.18 |
| 6 | 162.25 | 7 | 156.08 | 8 | 104.40 | 9 | 50.46 | 10 | 91.74 |
| 11 | 64.76 | 12 | 32.80 | 13 | 34.41 | 14 | 32.88 | 15 | 58.83 |
| 16 | 56.42 | 17 | 77.07 | 18 | 11.49 | 19 | 76.62 | 20 | 64.20 |
| 21 | 7.11 | 22 | 7.18 | 23 | 41.62 | 24 | 91.18 | 25 | 94.09 |
| 26 | 501.82 | 27 | 15.04 | 28 | 56.88 | 29 | 5.53 | | |

***** TOTAL DELAY = 7353.4 VEH-HRS ***** AVERAGE DELAY = 92.16 MIN/VEH *****

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***** RAMP DELAYS *****

| | | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | AVERAGE METERING DELAY MINUTES | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS | |
|----------|---|--------------------------|------------------|--------------------------------------|-------------|------------|------------|-------------|----------------------------|-------|
| ON-RAMP | 2 | RAMP | 50. | 50.00 | 5.24 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | | FREEMERGE | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 50. | 50.00 | 5.24 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| ON-RAMP | 3 | RAMP | 50. | 50.00 | 3.76 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| | | FREEMERGE | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 50. | 50.00 | 3.76 | 17.85 | 1.11 | 5.79 | 0.31 | 7.21 |
| ON-RAMP | 4 | RAMP | 100. | 100.00 | 8.39 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | | FREEMERGE | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 100.00 | 8.39 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP | 5 | RAMP | 100. | 100.00 | 13.48 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | | FREEMERGE | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 100.00 | 13.48 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| ON-RAMP | 6 | RAMP | 29. | 40.00 | 8.92 | 14.28 | 0.89 | 4.63 | 0.25 | 5.77 |
| | | FREEMERGE | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 29. | 40.00 | 8.92 | 14.28 | 0.89 | 4.63 | 0.25 | 5.77 |
| ON-RAMP | 9 | RAMP | 100. | 100.00 | 8.57 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| | | FREEMERGE | 0. | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| | | TOTAL | 100. | 100.00 | 8.57 | 35.71 | 2.22 | 11.58 | 0.61 | 14.41 |
| OFF-RAMP | 2 | OUTPUT POINT | 803. | 676.72 | | 241.64 | 14.99 | 78.40 | 4.16 | 97.55 |

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FFFFFFFFF RRRRRRRR EEEEEEEEE QQQQQQQ 1111 222222 PPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEEEE Q*A. D. MAY*Q 111111 222 222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQQ QQQQ 1111 222 222 PPP PPP LLL
FFF RRR RRR EEE QQQQ QQQQ 1111 222 222 PPP PPP LLL
FFFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 222 PPPPPPPP LLL
FFFFFFFFF RRRRRRRR EEEEEEE QQQQ QQQQ 1111 2222 PPPPPPPP LLL
FFF RRR RRR EEE QQQQ QQQ QQQ 1111 2222 PPP LLL
FFF RRR RRR EEE Q*UC* QQQQ 1111 222 PPP LLL
FFF RRR RRR EEEEEEEEE Q*REGENTS*Q 1111 222 PPP LLLLLLLLLL
FFF RRR RRR EEEEEEEEE Q*1988*Q QQQ 11111111 2222222222 PPP LLLLLLLLLL
    
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FREQ12PLB

1. A TYPE 1 PRIORITY LANE BETWEEN SUBSECTIONS 2 AND 26 WILL BE SIMULATED.
2. SHORT TERM CONSEQUENCES ARE REQUESTED.
3. THERE ARE 1.0 TIME SLICES PER HOUR.
4. WEAVING ANALYSIS IS NOT ENGAGED.
5. NO ALTERNATE ROUTE IS PROVIDED.
6. SPEED FLOW DATA IS SUPPLIED BY THE PROGRAM. DEFAULT FREE-FLOW SPEED = 65
LOWER LIMB (AT V/C=1) = 25
7. THE MAINLINE DELAY CALCULATION IS ENGAGED AT 65. MPH.
8. FUEL DATA ARE SUPPLIED BY THE PROGRAM.
9. EMISSION RATES SELECTED FROM PROGRAM TABLES: EMFAC2002 2005 - 75 DEGREES F.
10. NUMBER OF PRIORITY LANES = 2.
11. PRIORITY CUTOFF LIMIT = 2.

INPUT HAS BEEN COMPLETED

FREeway AND ARTERIAL DESIGN FEATURES

| SUB NO. | SSEC LNS | SSEC CAP | SSEC LENGTH | DESIGN SPEED | ORG DES | TRK FAC | SSEC GRAD | PCT TRK | PCT DES TRUCKS | SPECIAL RAMP | FF SPD. ALT. RTE | CAP. ALT. RTE | ART TYPE | GRADE ALT. RTE | SUBSECTION LOCATION |
|---------|----------|----------|-------------|--------------|---------|---------|-----------|---------|----------------|--------------|------------------|---------------|----------|----------------|-------------------------|
| ** 1 | | | | | | | | | | | | | | | |
| ** 2 | 2 | 3000. | 99999. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Queue Capture |
| ** 3 | 2 | 3000. | 2740. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-85 Off to Shore On |
| ** 4 | 2 | 3000. | 600. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Shore. On to Moffet Off |
| ** 5 | 2 | 3000. | 700. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Moffett Off to On |
| ** 6 | 2 | 3000. | 2630. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Moffett On to Ellis Off |
| ** 7 | 2 | 3000. | 2530. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Ellis Off to On-ramp |
| ** 8 | 2 | 3000. | 1500. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Ellis On-ramp |
| ** 9 | 2 | 3000. | 700. | 65 | | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Ellis / US 237 |
| ** 10 | 2 | 3000. | 1500. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 EB Off-Ramp |
| ** 11 | 2 | 3000. | 750. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | SR-237 / SR-237 |
| ** 12 | 2 | 3000. | 350. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | SR-237 EB On-Ramp |
| ** 13 | 2 | 3000. | 350. | 65 | | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | US 237 / Mathilda |
| ** 14 | 2 | 3000. | 350. | 65 | D | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda Off-Ramp |
| ** 15 | 2 | 3000. | 700. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Mathilda |
| ** 16 | 2 | 3000. | 900. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda SB On-Ramp |
| ** 17 | 2 | 3000. | 1400. | 65 | 0 | 0.96 | 0.0 | 0 | 100 | YES | 0.0 | 0. | GOOD | 0.0 | Mathilda NB On-Ramp |
| ** 18 | 2 | 3000. | 200. | 65 | | 0.96 | 0.0 | 0 | 100 | NO | 0.0 | 0. | GOOD | 0.0 | Mathilda / Fair Oaks |

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**
** 19 2 3000. 1400. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks SB Off-Ramp **
**
** 20 2 3000. 900. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks SB/ Fair Oaks **
**
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FREEWAY AND ARTERIAL DESIGN FEATURES

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**
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**
**
**
** SUB NO. SSEC SSEC DESIG N ORG TRK SSEC PCT PCT DES SPECIAL FF.SPD. CAP. ART GRADE SUBSECTI ON LOCATI ON **
** SEC LNS CAP LENGTH SPEED DES FAC GRAD TRK TRUCKS RAMP ALT. RTE ALT. RTE TYPE ALT. RTE **
**
** 21 2 3000. 100. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Fair Oaks SB On-Ramp **
**
** 22 2 3000. 100. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks NB Off-Ramp **
**
** 23 2 3000. 600. 65 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 Fair Oaks NB/ Fair Oaks **
**
** 24 2 3000. 1500. 65 0 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Oaks On-Ramp to Mid **
**
** 25 2 3000. 1500. 65 0.96 0.0 0 100 YES 0.0 0. GOOD 0.0 Mid to Lawrence Off-ramp **
**
** 26 2 3000. 8000. 65 D 0.96 0.0 0 100 NO 0.0 0. GOOD 0.0 HOV Dummy **
**
** 27 **
** 28 **
** 29 **
**
*****

```

FREEWAY TRAVEL TIME (MINUTES)

```

*****
* OR I G I N S D E S T I N A T I O N S A C R O S S *
* D O W N 1 2 3 4 5 6 7 *
+
* * * * *
+
* 1 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 2 * 0.00 19.74 20.05 20.86 21.05 23.08 0.00 *
+
* 3 * 0.00 0.00 0.00 0.00 1.96 3.99 0.00 *
+
* 4 * 0.00 0.00 0.00 0.00 0.00 3.21 0.00 *
+
* 5 * 0.00 0.00 0.00 0.00 0.00 2.90 0.00 *
+
* 6 * 0.00 0.00 0.00 0.00 0.00 2.74 0.00 *
+
* 7 * 0.00 0.00 0.00 0.00 0.00 2.06 0.00 *
+
* 8 * 0.00 0.00 0.00 0.00 0.00 1.92 0.00 *
+
* 9 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 10 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
+
* 11 * 0.00 0.00 0.00 0.00 0.00 0.00 0.00 *
* * * * *
*****

```


TIME SLICE FREEWAY PERFORMANCE TABLE

| SUB SEC | NO. LNS | SSEC LENGTH | O-D ORG | DATA DES | DEMANDS SSEC | ADJUSTED ORG | VOLUMES DES | SSEC SSEC | WEAVE CAP. | CONGEST EFF | STORAGE LENGTH | V/C RATIO | SPEED MPH | DENSITY VPMP | LOS LEVEL | FUEL MPG | EMI SS GS/VM | |
|---------|---------|-------------|---------|----------|--------------|--------------|-------------|-----------|------------|-----------------|----------------|-----------|-----------|--------------|-----------|----------|--------------|------|
| 1 | | | | | | | | | | | | | | | | | | |
| 2 | 2 | 99999 | 1840. | 0. | 1840. | 1840. | 0. | 1840. | 3000. | 0. | 0. | 0. | .61 | 65. | 14.2 | B | 20.0 | 13.7 |
| 3 | 2 | 2740. | 0. | 0. | 1840. | 0. | 0. | 1840. | 3000. | 0. | 0. | 0. | .61 | 65. | 14.2 | B | 20.0 | 13.7 |
| 4 | 2 | 600. | 0. | 0. | 1840. | 0. | 0. | 1840. | 3000. | 0. | 0. | 0. | .61 | 65. | 14.2 | B | 20.0 | 13.7 |
| 5 | 2 | 700. | 0. | 0. | 1840. | 0. | 0. | 1840. | 3000. | 0. | 0. | 0. | .61 | 65. | 14.2 | B | 20.0 | 13.7 |
| 6 | 2 | 2630. | 0. | 0. | 1840. | 0. | 0. | 1840. | 3000. | 0. | 0. | 0. | .61 | 65. | 14.2 | B | 20.0 | 13.7 |
| 7 | 2 | 2530. | 0. | 0. | 1840. | 0. | 0. | 1840. | 3000. | 0. | 0. | 0. | .61 | 65. | 14.2 | B | 20.0 | 13.7 |
| 8 | 2 | 1500. | 97. | 0. | 1937. | 97. | 0. | 1937. | 3000. | 0. | 0. | 0. | .65 | 65. | 14.9 | B | 20.0 | 13.7 |
| 9 | 2 | 700. | 0. | 0. | 1937. | 0. | 0. | 1937. | 3000. | 0. | 0. | 0. | .65 | 65. | 14.9 | B | 20.0 | 13.7 |
| 10 | 2 | 1500. | 0. | 389. | 1937. | 0. | 278. | 1937. | 3000. | 0. | 0. | 0. | .65 | 65. | 14.9 | B | 20.0 | 13.7 |
| 11 | 2 | 750. | 0. | 0. | 1548. | 0. | 0. | 1548. | 3000. | 0. | 0. | 0. | .52 | 65. | 11.9 | B | 20.0 | 13.7 |
| 12 | 2 | 350. | 137. | 0. | 1686. | 137. | 0. | 1686. | 3000. | 0. | 0. | 0. | .56 | 65. | 13.0 | B | 20.0 | 13.7 |
| 13 | 2 | 350. | 0. | 0. | 1686. | 0. | 0. | 1686. | 3000. | 0. | 0. | 0. | .56 | 65. | 13.0 | B | 20.0 | 13.7 |
| 14 | 2 | 350. | 0. | 162. | 1686. | 0. | 162. | 1686. | 3000. | 0. | 0. | 0. | .56 | 65. | 13.0 | B | 20.0 | 13.7 |
| 15 | 2 | 700. | 0. | 0. | 1524. | 0. | 0. | 1524. | 3000. | 0. | 0. | 0. | .51 | 65. | 11.7 | B | 20.0 | 13.7 |
| 16 | 2 | 900. | 166. | 0. | 1690. | 166. | 0. | 1690. | 3000. | 0. | 0. | 0. | .56 | 65. | 13.0 | B | 20.0 | 13.7 |
| 17 | 2 | 1400. | 92. | 0. | 1782. | 92. | 0. | 1782. | 3000. | 0. | 0. | 0. | .59 | 65. | 13.7 | B | 20.0 | 13.7 |
| 18 | 2 | 200. | 0. | 0. | 1782. | 0. | 0. | 1782. | 3000. | 0. | 0. | 0. | .59 | 65. | 13.7 | B | 20.0 | 13.7 |
| 19 | 2 | 1400. | 0. | 81. | 1782. | 0. | 81. | 1782. | 3000. | 0. | 0. | 0. | .59 | 65. | 13.7 | B | 20.0 | 13.7 |
| 20 | 2 | 900. | 0. | 0. | 1701. | 0. | 0. | 1701. | 3000. | 0. | 0. | 0. | .57 | 65. | 13.1 | B | 20.0 | 13.7 |
| 21 | 2 | 100. | 63. | 0. | 1764. | 63. | 0. | 1764. | 3000. | 0. | 0. | 0. | .59 | 65. | 13.6 | B | 20.0 | 13.7 |
| 22 | 2 | 100. | 0. | 24. | 1764. | 0. | 24. | 1764. | 3000. | 0. | 0. | 0. | .59 | 65. | 13.6 | B | 20.0 | 13.7 |
| 23 | 2 | 600. | 0. | 0. | 1740. | 0. | 0. | 1740. | 3000. | 0. | 0. | 0. | .58 | 65. | 13.4 | B | 20.0 | 13.7 |
| 24 | 2 | 1500. | 56. | 0. | 1796. | 56. | 0. | 1796. | 3000. | 0. | 0. | 0. | .60 | 65. | 13.8 | B | 20.0 | 13.7 |
| 25 | 2 | 1500. | 0. | 0. | 1796. | 0. | 0. | 1796. | 3000. | 0. | 0. | 0. | .60 | 65. | 13.8 | B | 20.0 | 13.7 |
| 26 | 2 | 8000. | 0. | 1796. | 1796. | 0. | 1796. | 1796. | 3000. | 0. | 0. | 0. | .60 | 65. | 13.8 | B | 20.0 | 13.7 |
| 27 | | | | | | | | | | | | | | | | | | |
| 28 | | | | | | | | | | | | | | | | | | |
| 29 | | | | | | | | | | | | | | | | | | |
| TOTAL | 131999 | = | 25.0 | MILES | | | | | | MAX(V/C) = 0.65 | LOWEST LOS = B | AVG = 65. | 14.1 | | | 20.0 | 13.7 | |

| | | |
|-----------------------------|--------------------------------|--------------------------------|
| | CURRENT TIME SLICE | CUMULATIVE VALUES |
| FREEWAY TRAVEL TIME = | 704. VEH-HRS 1408. PASS-HRS | 704. VEH-HRS 1408. PASS-HRS |
| FREEWAY MERGE DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 56. VEH-HRS 111. PASS-HRS | 56. VEH-HRS 111. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 760. VEH-HRS 1519. PASS-HRS | 760. VEH-HRS 1519. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 45765. VEH-MI. 91531. PASS-MI. | 45765. VEH-MI. 91531. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 60. MPH. | 65. MPH. |
| AVERAGE DENSITY = | 14. VPMP | 14. VPMP |
| TOTAL FUEL = | 2307. GALLONS | 2307. GALLONS |
| TOTAL EMISSIONS = | 637. KILOGRAMS | 637. KILOGRAMS |

***** MAINTENANCE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

***** RAMP DELAYS *****

| OFF-RAMP | NO. | OUTPUT POINT | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|----------|-----|--------------|-----------------------|---------------|----------|---------|---------|----------|----------------------|
| OFF-RAMP | 2 | OUTPUT POINT | 111. | 55.54 | 19.05 | 1.20 | 6.27 | 0.33 | 7.80 |

 **
 ** FREEWAY TRAVEL TIME (MINUTES) **
 **

| ORIGINS DOWN | DESTINATIONS ACROSS | | | | | | |
|--------------|---------------------|---|---|---|---|---|---|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| | | | | | | | |

| | * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
|--|--------|------|-------|-------|-------|-------|-------|------|------|
| | * 2 * | 0.00 | 19.74 | 20.05 | 20.86 | 21.05 | 23.08 | 0.00 | |
| | * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 1.96 | 3.99 | 0.00 | |
| | * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.21 | 0.00 | |
| | * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.90 | 0.00 | |
| | * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.74 | 0.00 | |
| | * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.06 | 0.00 | |
| | * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.92 | 0.00 | |
| | * 9 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| | * 10 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |
| | * 11 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB SEC | * NO. LNS | * SSEC LENGTH | * O-D ORG | * DATA DES | * DEMANDS SSEC | * ADJUSTED ORG | * DES | * VOLUMES SSEC | * SSEC CAP. | * WEAVE EFF | * CONGEST LENGTH | * STORAGE RATE | * V/C RATIO | * SPEED MPH | * DENSITY VPMP | * LOS LEVEL | * FUEL MPG | * EMISSIONS GS/VM |
|-----------|-----------|---------------|-----------|------------|----------------|----------------|-------|----------------|-------------|-------------|------------------|----------------|-------------|-------------|----------------|-------------|------------|-------------------|
| * 1 | | | | | | | | | | | | | | | | | | |
| * 2 | 2 | 99999 | 1710 | 0 | 1710 | 1710 | 0 | 1710 | 3000 | 0 | 0 | 0 | .57 | 65 | 13.2 | B | 20.0 | 13.7 |
| * 3 | 2 | 2740 | 0 | 0 | 1710 | 0 | 0 | 1710 | 3000 | 0 | 0 | 0 | .57 | 65 | 13.2 | B | 20.0 | 13.7 |
| * 4 | 2 | 600 | 0 | 0 | 1710 | 0 | 0 | 1710 | 3000 | 0 | 0 | 0 | .57 | 65 | 13.2 | B | 20.0 | 13.7 |
| * 5 | 2 | 700 | 0 | 0 | 1710 | 0 | 0 | 1710 | 3000 | 0 | 0 | 0 | .57 | 65 | 13.2 | B | 20.0 | 13.7 |
| * 6 | 2 | 2630 | 0 | 0 | 1710 | 0 | 0 | 1710 | 3000 | 0 | 0 | 0 | .57 | 65 | 13.2 | B | 20.0 | 13.7 |
| * 7 | 2 | 2530 | 0 | 0 | 1710 | 0 | 0 | 1710 | 3000 | 0 | 0 | 0 | .57 | 65 | 13.2 | B | 20.0 | 13.7 |
| * 8 | 2 | 1500 | 96 | 0 | 1806 | 96 | 0 | 1806 | 3000 | 0 | 0 | 0 | .60 | 65 | 13.9 | B | 20.0 | 13.7 |
| * 9 | 2 | 700 | 0 | 0 | 1806 | 0 | 0 | 1806 | 3000 | 0 | 0 | 0 | .60 | 65 | 13.9 | B | 20.0 | 13.7 |
| * 10 | 2 | 1500 | 0 | 374 | 1806 | 0 | 275 | 1806 | 3000 | 0 | 0 | 0 | .60 | 65 | 13.9 | B | 20.0 | 13.7 |
| * 11 | 2 | 750 | 0 | 0 | 1432 | 0 | 0 | 1432 | 3000 | 0 | 0 | 0 | .48 | 65 | 11.0 | B | 20.0 | 13.7 |
| * 12 | 2 | 350 | 124 | 0 | 1556 | 124 | 0 | 1556 | 3000 | 0 | 0 | 0 | .52 | 65 | 12.0 | B | 20.0 | 13.7 |
| * 13 | 2 | 350 | 0 | 0 | 1556 | 0 | 0 | 1556 | 3000 | 0 | 0 | 0 | .52 | 65 | 12.0 | B | 20.0 | 13.7 |
| * 14 | 2 | 350 | 0 | 167 | 1556 | 0 | 167 | 1556 | 3000 | 0 | 0 | 0 | .52 | 65 | 12.0 | B | 20.0 | 13.7 |
| * 15 | 2 | 700 | 0 | 0 | 1389 | 0 | 0 | 1389 | 3000 | 0 | 0 | 0 | .46 | 65 | 10.7 | A | 20.0 | 13.7 |
| * 16 | 2 | 900 | 169 | 0 | 1558 | 169 | 0 | 1558 | 3000 | 0 | 0 | 0 | .52 | 65 | 12.0 | B | 20.0 | 13.7 |
| * 17 | 2 | 1400 | 94 | 0 | 1653 | 94 | 0 | 1653 | 3000 | 0 | 0 | 0 | .55 | 65 | 12.7 | B | 20.0 | 13.7 |
| * 18 | 2 | 200 | 0 | 0 | 1653 | 0 | 0 | 1653 | 3000 | 0 | 0 | 0 | .55 | 65 | 12.7 | B | 20.0 | 13.7 |
| * 19 | 2 | 1400 | 0 | 96 | 1653 | 0 | 96 | 1653 | 3000 | 0 | 0 | 0 | .55 | 65 | 12.7 | B | 20.0 | 13.7 |
| * 20 | 2 | 900 | 0 | 0 | 1556 | 0 | 0 | 1556 | 3000 | 0 | 0 | 0 | .52 | 65 | 12.0 | B | 20.0 | 13.7 |
| * 21 | 2 | 100 | 66 | 0 | 1622 | 66 | 0 | 1622 | 3000 | 0 | 0 | 0 | .54 | 65 | 12.5 | B | 20.0 | 13.7 |
| * 22 | 2 | 100 | 0 | 32 | 1622 | 0 | 32 | 1622 | 3000 | 0 | 0 | 0 | .54 | 65 | 12.5 | B | 20.0 | 13.7 |
| * 23 | 2 | 600 | 0 | 0 | 1590 | 0 | 0 | 1590 | 3000 | 0 | 0 | 0 | .53 | 65 | 12.2 | B | 20.0 | 13.7 |
| * 24 | 2 | 1500 | 50 | 0 | 1640 | 50 | 0 | 1640 | 3000 | 0 | 0 | 0 | .55 | 65 | 12.6 | B | 20.0 | 13.7 |
| * 25 | 2 | 1500 | 0 | 0 | 1640 | 0 | 0 | 1640 | 3000 | 0 | 0 | 0 | .55 | 65 | 12.6 | B | 20.0 | 13.7 |
| * 26 | 2 | 8000 | 0 | 1640 | 1640 | 0 | 1640 | 1640 | 3000 | 0 | 0 | 0 | .55 | 65 | 12.6 | B | 20.0 | 13.7 |
| * 27 | | | | | | | | | | | | | | | | | | |
| * 28 | | | | | | | | | | | | | | | | | | |
| * 29 | | | | | | | | | | | | | | | | | | |

TOTAL 131999 = 25.0 MILES MAX(V/C) = 0.60 LOWEST LOS = B AVG = 65. 13.1 20.0 13.7

| | CURRENT TIME SLICE | | CUMULATIVE VALUES |
|-----------------------------|--------------------|-----------------|------------------------------------|
| FREWAY TRAVEL TIME = | 653. VEH-HRS | 1306. PASS-HRS | 1357. VEH-HRS 2714. PASS-HRS |
| FREWAY MERGE DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| ON-RAMP MRG/CAP DELAY = | 0. VEH-HRS | 0. PASS-HRS | 0. VEH-HRS 0. PASS-HRS |
| OFF-RAMP DELAY = | 161. VEH-HRS | 321. PASS-HRS | 216. VEH-HRS 432. PASS-HRS |
| TOTAL SYSTEM TRAVEL TIME = | 814. VEH-HRS | 1627. PASS-HRS | 1573. VEH-HRS 3147. PASS-HRS |
| TOTAL FRWAY TRAV DISTANCE = | 42453. VEH-MI. | 84906. PASS-MI. | 88218. VEH-MI. 176436. PASS-MI. |
| AVERAGE SYSTEM SPEED = | 52. MPH. | | 65. MPH. |
| AVERAGE DENSITY = | 13. VPMP | | 14. VPMP |
| TOTAL FUEL = | 2178. GALLONS | | 4485. GALLONS |
| TOTAL EMISSIONS = | 606. KILOGRAMS | | 1242. KILOGRAMS |

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|

US-101_SB_PM_P2_2040_PL

| | | | | | | | | | |
|----|------|----|------|----|------|----|------|----|------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

***** RAMP DELAYS *****

| | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|-------------------------|--------------------------|------------------|-------------|------------|------------|-------------|----------------------------|
| OFF-RAMP 2 OUTPUT POINT | 210. | 160.61 | 55.09 | 3.47 | 18.12 | 0.96 | 22.55 |

 ** FREEWAY TRAVEL TIME (MINUTES) **

| * ORIGINS DOWN | * DESTINATIONS ACROSS | | | | | | |
|-------------------|-----------------------|-------|-------|-------|-------|-------|------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| * 1 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 2 * | 0.00 | 19.74 | 20.05 | 20.86 | 21.05 | 23.08 | 0.00 |
| * 3 * | 0.00 | 0.00 | 0.00 | 0.00 | 1.96 | 3.99 | 0.00 |
| * 4 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 3.21 | 0.00 |
| * 5 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.90 | 0.00 |
| * 6 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.74 | 0.00 |
| * 7 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.06 | 0.00 |
| * 8 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 1.92 | 0.00 |
| * 9 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 10 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| * 11 * | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

TIME SLICE FREEWAY PERFORMANCE TABLE

| * SUB NO. | * SSEC | * O-D DATA | * DEMANDS | * ADJUSTED VOLUMES | * SSEC | * WEAWE | * CONGEST | * STORAGE | * V/C | * SPEED | * DENSITY | * LOS | * FUEL | * EMISSIONS | | | | |
|-----------|----------|------------|-----------|--------------------|--------|---------|-----------|-----------|---------|---------|-----------|---------|--------|-------------|------|---|------|------|
| * SEC LNS | * LENGTH | * ORG DES | * SSEC | * ORG DES SSEC | * CAP. | * EFF | * LENGTH | * RATE | * RATIO | * MPH | * VPMP | * LEVEL | * MPG | * GS/VM | | | | |
| * 1 | | | | | | | | | | | | | | | | | | |
| * 2 | 2 | 99999. | 1554. | 0. | 1554. | 1554. | 0. | 1554. | 3000. | 0. | 0. | 0. | .52 | 65. | 12.0 | B | 20.0 | 13.7 |
| * 3 | 2 | 2740. | 0. | 0. | 1554. | 0. | 0. | 1554. | 3000. | 0. | 0. | 0. | .52 | 65. | 12.0 | B | 20.0 | 13.7 |
| * 4 | 2 | 600. | 0. | 0. | 1554. | 0. | 0. | 1554. | 3000. | 0. | 0. | 0. | .52 | 65. | 12.0 | B | 20.0 | 13.7 |
| * 5 | 2 | 700. | 0. | 0. | 1554. | 0. | 0. | 1554. | 3000. | 0. | 0. | 0. | .52 | 65. | 12.0 | B | 20.0 | 13.7 |
| * 6 | 2 | 2630. | 0. | 0. | 1554. | 0. | 0. | 1554. | 3000. | 0. | 0. | 0. | .52 | 65. | 12.0 | B | 20.0 | 13.7 |
| * 7 | 2 | 2530. | 0. | 0. | 1554. | 0. | 0. | 1554. | 3000. | 0. | 0. | 0. | .52 | 65. | 12.0 | B | 20.0 | 13.7 |
| * 8 | 2 | 1500. | 77. | 0. | 1631. | 77. | 0. | 1631. | 3000. | 0. | 0. | 0. | .54 | 65. | 12.5 | B | 20.0 | 13.7 |
| * 9 | 2 | 700. | 0. | 0. | 1631. | 0. | 0. | 1631. | 3000. | 0. | 0. | 0. | .54 | 65. | 12.5 | B | 20.0 | 13.7 |
| * 10 | 2 | 1500. | 0. | 338. | 1631. | 0. | 279. | 1631. | 3000. | 0. | 0. | 0. | .54 | 65. | 12.5 | B | 20.0 | 13.7 |
| * 11 | 2 | 750. | 0. | 0. | 1293. | 0. | 0. | 1293. | 3000. | 0. | 0. | 0. | .43 | 65. | 9.9 | A | 20.0 | 13.7 |
| * 12 | 2 | 350. | 142. | 0. | 1435. | 142. | 0. | 1435. | 3000. | 0. | 0. | 0. | .48 | 65. | 11.0 | B | 20.0 | 13.7 |
| * 13 | 2 | 350. | 0. | 0. | 1435. | 0. | 0. | 1435. | 3000. | 0. | 0. | 0. | .48 | 65. | 11.0 | B | 20.0 | 13.7 |
| * 14 | 2 | 350. | 0. | 135. | 1435. | 0. | 135. | 1435. | 3000. | 0. | 0. | 0. | .48 | 65. | 11.0 | B | 20.0 | 13.7 |
| * 15 | 2 | 700. | 0. | 0. | 1300. | 0. | 0. | 1300. | 3000. | 0. | 0. | 0. | .43 | 65. | 10.0 | A | 20.0 | 13.7 |
| * 16 | 2 | 900. | 134. | 0. | 1434. | 134. | 0. | 1434. | 3000. | 0. | 0. | 0. | .48 | 65. | 11.0 | B | 20.0 | 13.7 |
| * 17 | 2 | 1400. | 75. | 0. | 1509. | 75. | 0. | 1509. | 3000. | 0. | 0. | 0. | .50 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 18 | 2 | 200. | 0. | 0. | 1509. | 0. | 0. | 1509. | 3000. | 0. | 0. | 0. | .50 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 19 | 2 | 1400. | 0. | 85. | 1509. | 0. | 85. | 1509. | 3000. | 0. | 0. | 0. | .50 | 65. | 11.6 | B | 20.0 | 13.7 |
| * 20 | 2 | 900. | 0. | 0. | 1424. | 0. | 0. | 1424. | 3000. | 0. | 0. | 0. | .47 | 65. | 11.0 | A | 20.0 | 13.7 |
| * 21 | 2 | 100. | 52. | 0. | 1476. | 52. | 0. | 1476. | 3000. | 0. | 0. | 0. | .49 | 65. | 11.4 | B | 20.0 | 13.7 |
| * 22 | 2 | 100. | 0. | 30. | 1476. | 0. | 30. | 1476. | 3000. | 0. | 0. | 0. | .49 | 65. | 11.4 | B | 20.0 | 13.7 |
| * 23 | 2 | 600. | 0. | 0. | 1446. | 0. | 0. | 1446. | 3000. | 0. | 0. | 0. | .48 | 65. | 11.1 | B | 20.0 | 13.7 |
| * 24 | 2 | 1500. | 60. | 0. | 1506. | 60. | 0. | 1506. | 3000. | 0. | 0. | 0. | .50 | 65. | 11.6 | B | 20.0 | 13.7 |

```

US-101_SB_PM_P2_2040_PL
* 25 2 1500. 0. 0. 1506. 0. 0. 1506. 3000. 0. 0. .50 65. 11.6 B 20.0 13.7 *
* 26 2 8000. 0. 1506. 1506. 0. 1506. 1506. 3000. 0. 0. .50 65. 11.6 B 20.0 13.7 *
* 27 *
* 28 *
* 29 *
*****
*
* TOTAL 131999. = 25.0 MILES MAX(V/C) = 0.54 LOWEST LOS = B AVG = 65. 11.9 20.0 13.7 *
*****

```

```

CURRENT TIME SLICE CUMULATIVE VALUES
FREEWAY TRAVEL TIME = 594. VEH-HRS 1189. PASS-HRS 1951. VEH-HRS 3903. PASS-HRS
FREEWAY MERGE DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
ON-RAMP MRG/CAP DELAY = 0. VEH-HRS 0. PASS-HRS 0. VEH-HRS 0. PASS-HRS
OFF-RAMP DELAY = 240. VEH-HRS 480. PASS-HRS 456. VEH-HRS 912. PASS-HRS
TOTAL SYSTEM TRAVEL TIME = 834. VEH-HRS 1668. PASS-HRS 2407. VEH-HRS 4815. PASS-HRS
TOTAL FRWAY TRAV DISTANCE = 38626. VEH-MI. 77253. PASS-MI. 126844. VEH-MI. 253689. PASS-MI.
AVERAGE SYSTEM SPEED = 46. MPH. 65. MPH.
AVERAGE DENSITY = 12. VPML 13. VPML
TOTAL FUEL = 2014. GALLONS 6499. GALLONS
TOTAL EMISSIONS = 564. KILOGRAMS 1807. KILOGRAMS

```

***** MAINLINE DELAY (VEH-HRS) ***** DESIRED SPEED = 65.0 *****

| SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY | SUBSECTION | DELAY |
|------------|-------|------------|-------|------------|-------|------------|-------|------------|-------|
| 1 | 0.00 | 2 | 0.00 | 3 | 0.00 | 4 | 0.00 | 5 | 0.00 |
| 6 | 0.00 | 7 | 0.00 | 8 | 0.00 | 9 | 0.00 | 10 | 0.00 |
| 11 | 0.00 | 12 | 0.00 | 13 | 0.00 | 14 | 0.00 | 15 | 0.00 |
| 16 | 0.00 | 17 | 0.00 | 18 | 0.00 | 19 | 0.00 | 20 | 0.00 |
| 21 | 0.00 | 22 | 0.00 | 23 | 0.00 | 24 | 0.00 | 25 | 0.00 |
| 26 | 0.00 | 27 | 0.00 | 28 | 0.00 | 29 | 0.00 | | |

***** TOTAL DELAY = 0.0 VEH-HRS ***** AVERAGE DELAY = 0.00 MIN/VEH *****

***** RAMP DELAYS *****

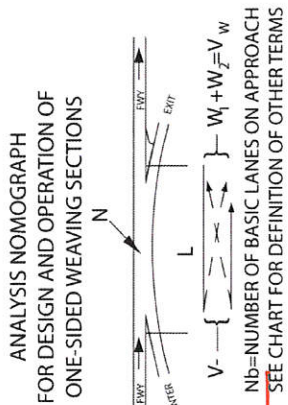
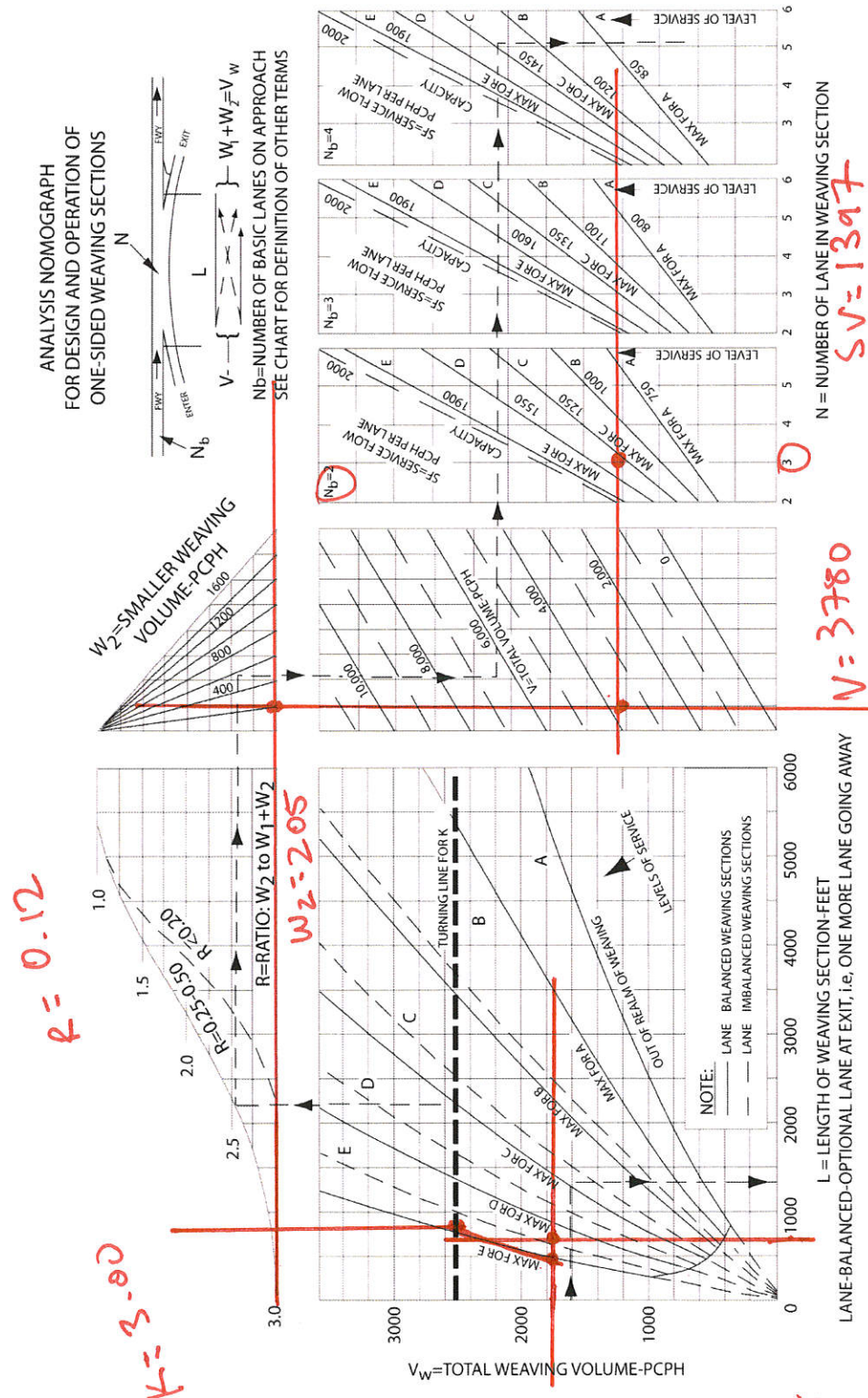
| OFF-RAMP | 2 | OUTPUT POINT | QUEUE LENGTH VEHICLES | DELAY VEH-HRS | GAS GALS | HC KGMS | CO KGMS | NOX KGMS | TOTAL EMISSIONS KGMS |
|----------|---|--------------|--------------------------|------------------|-------------|------------|------------|-------------|----------------------------|
| OFF-RAMP | 2 | OUTPUT POINT | 270. | 239.85 | 82.27 | 5.18 | 27.06 | 1.44 | 33.68 |

APPENDIX Q – YEAR 2040 LEISCH WEAVING ANALYSIS SHEETS



LOS D

Figure 504.7A Design Curve for Freeway and Collector Weaving



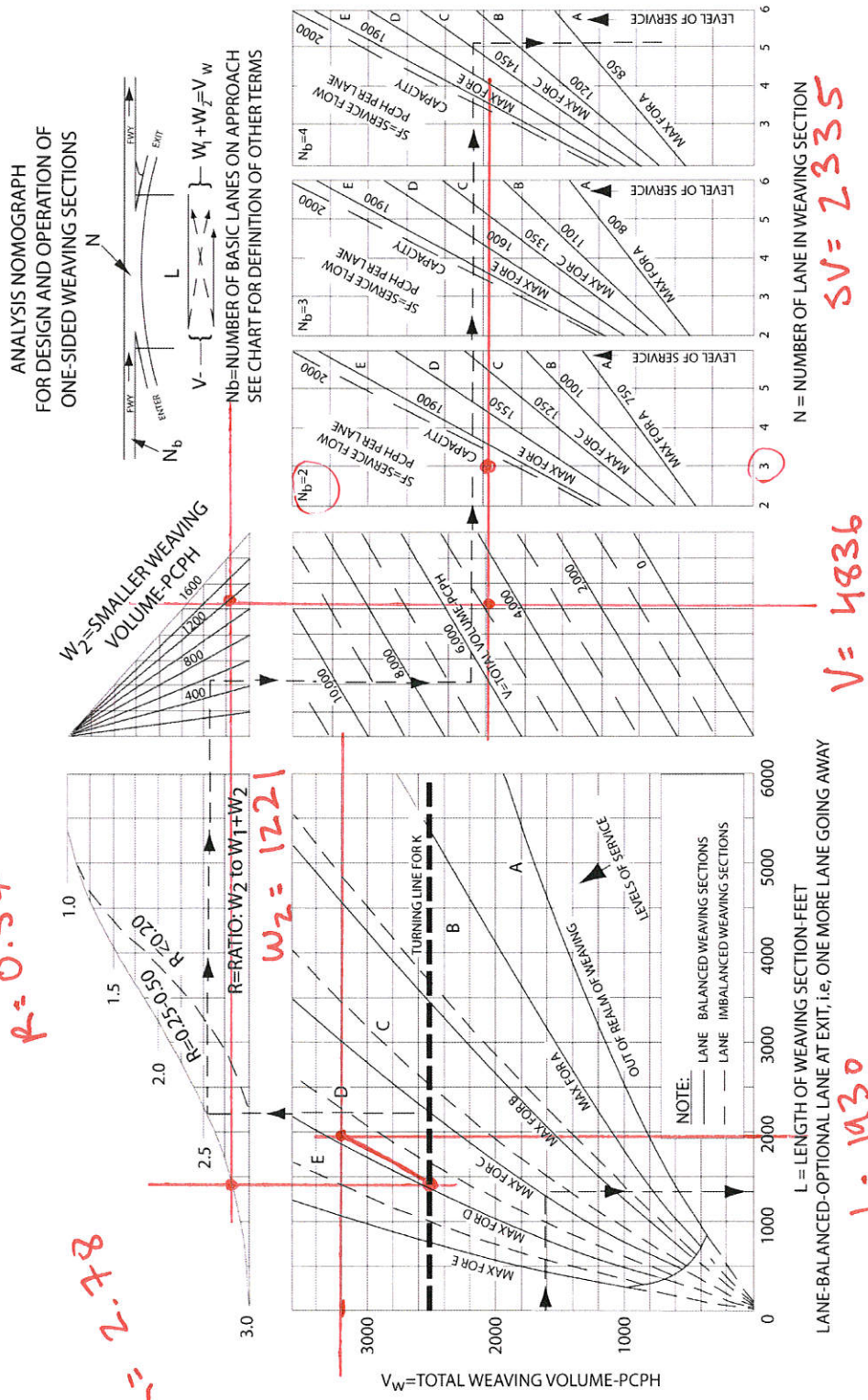
NOTE: EXTRAPOLATION OF CHART BEYOND THE BOUNDARIES GIVEN IS NOT ADVISED.

Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, $W_1 + W_2$ (or $V \cdot W$) followed by projection to the right, intersecting the desired weaving LOS; a vertical drop from this point provides weaving distance $L = 1300$ ft. Returning to first intersection point of $V \cdot W$ with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K ". From here the solution line is extended vertically to intersect the K values curve, from which a horizontal extension meets the desired W_2 volume. Then a downward turn to total volume, V , from which the line is horizontally projected to the right, intersection (in this case) the desired LOS = C curve having an SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields a N of 5.2; this would be rounded to $N = 5$ lanes.

$W_1 + W_2 = 1717$

LOS F

Figure 504.7A
Design Curve for Freeway and Collector Weaving



NOTE: EXTRAPOLATION OF CHART BEYOND THE BOUNDARIES GIVEN IS NOT ADVISED.

Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, $W_1 + W_2$ (or $V \cdot W$) followed by projection to the right, intersecting the desired weaving LOS; a vertical drop from this point provides weaving distance $L = 1300$ ft. Returning to first intersection point of $V \cdot W$ with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K ;" from here the solution line is extended vertically to intersect the K values curve, from which a horizontal extension meets the desired W_2 volume. Then a downward turn to total volume, V , from which the line is horizontally projected to the right, intersection (in this case) the desired LOS = C curve having an SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields a N of 5.2; this would be rounded to $N = 5$ lanes.

$W_1 + W_2 = 2761$

$SV = 2335$

Figure 504.7A
Design Curve for Freeway and Collector Weaving

LOS D

2040 No Build AM - US-101 SB: SR-237 to Mathilda

R = 0.30

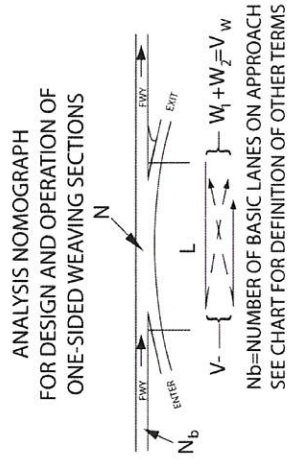
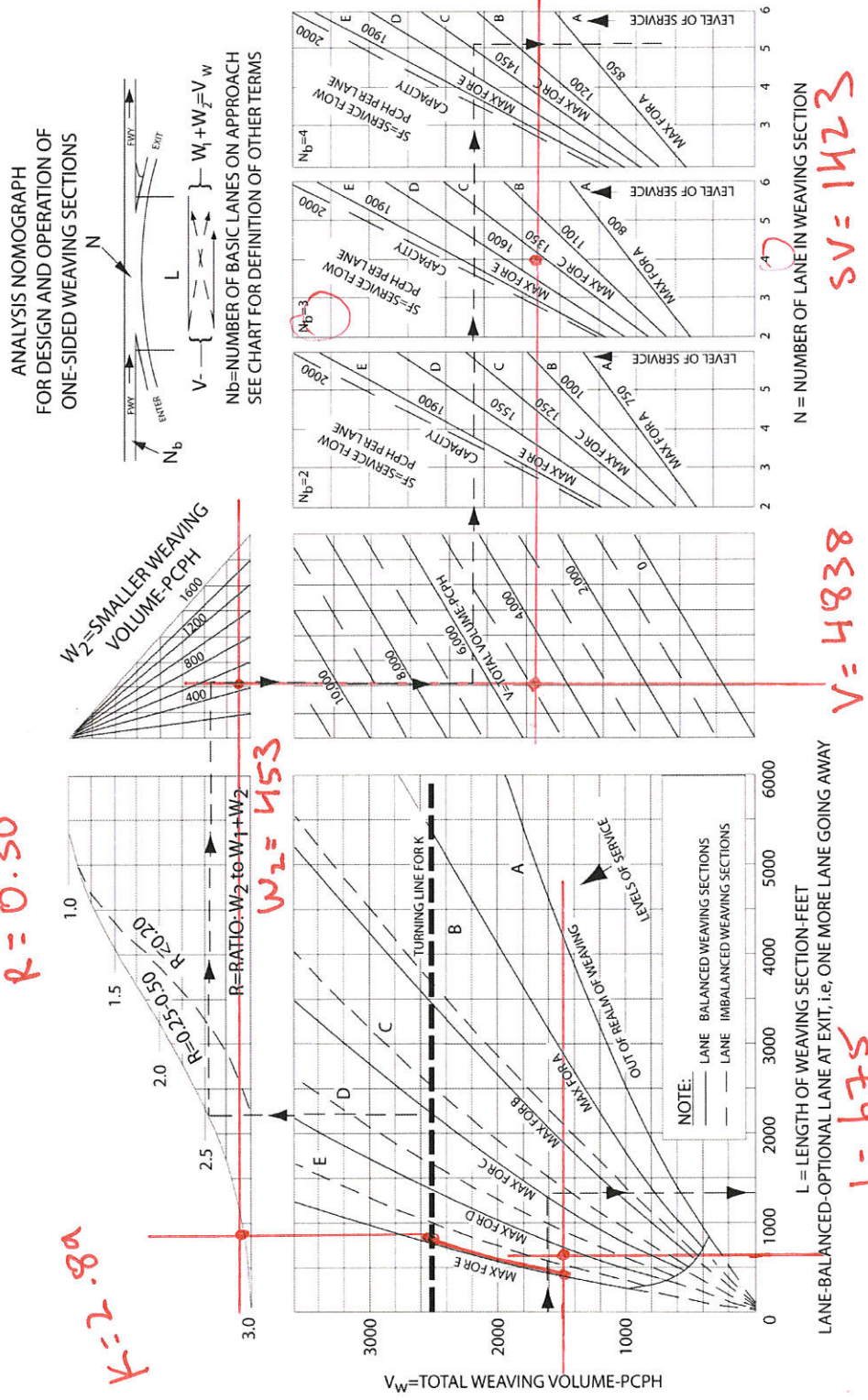
K = 2.80

W1 = 453

L = 675

V = 4838

SV = 1423



Nb = NUMBER OF BASIC LANES ON APPROACH
SEE CHART FOR DEFINITION OF OTHER TERMS

NOTE: EXTRAPOLATION OF CHART BEYOND THE BOUNDARIES GIVEN IS NOT ADVISED.

Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, W_1+W_2 (or V_w) followed by projection to the right, intersecting the desired weaving LOS; a vertical drop from this point provides weaving distance, $L = 1300$ ft. Returning to first intersection point of V_w with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K ": from here the solution line is extended vertically to intersect the K values curve, from which a horizontal extension meets the desired W_2 volume. Then a downward turn to total volume, V , from which the line is horizontally projected to the right, intersection (in this case) the desired LOS = C curve having an SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields: a N of 5.2; this would be rounded to $N = 5$ lanes.

22

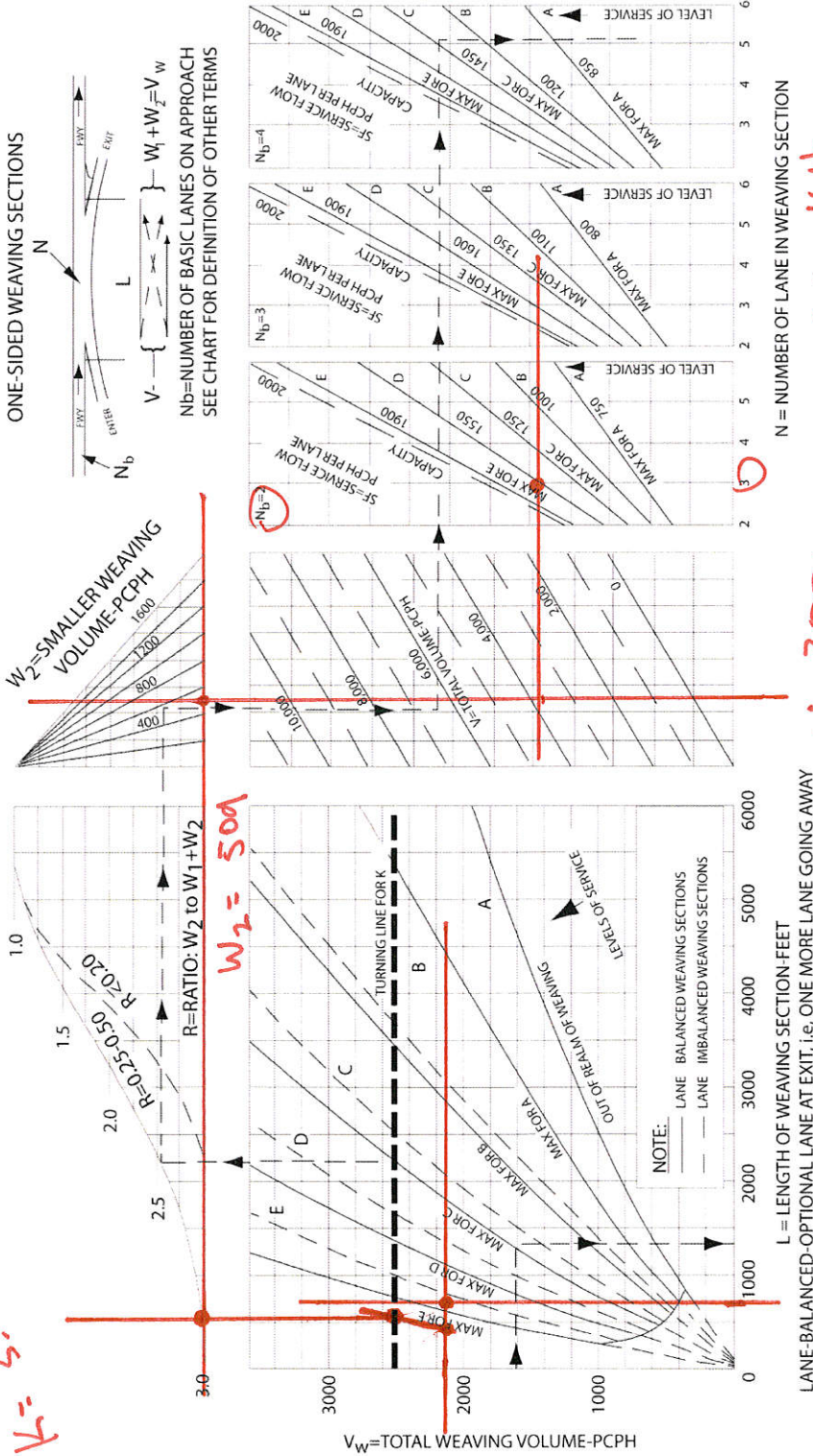
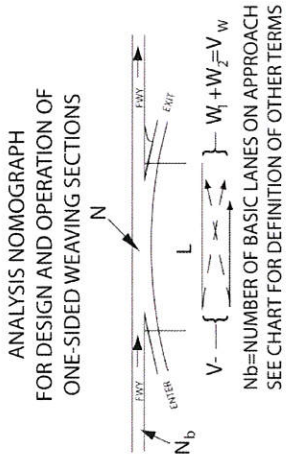
Figure 504.7A
Design Curve for Freeway and Collector Weaving

LOSE

2040 No Build PM - SR-237 WB: Mathilda to US-101

$R = 0.25$

$K = 3.00$



$SV = 1616$

$V = 3831$

$L = 680$

$2171 + 22 = 2193$

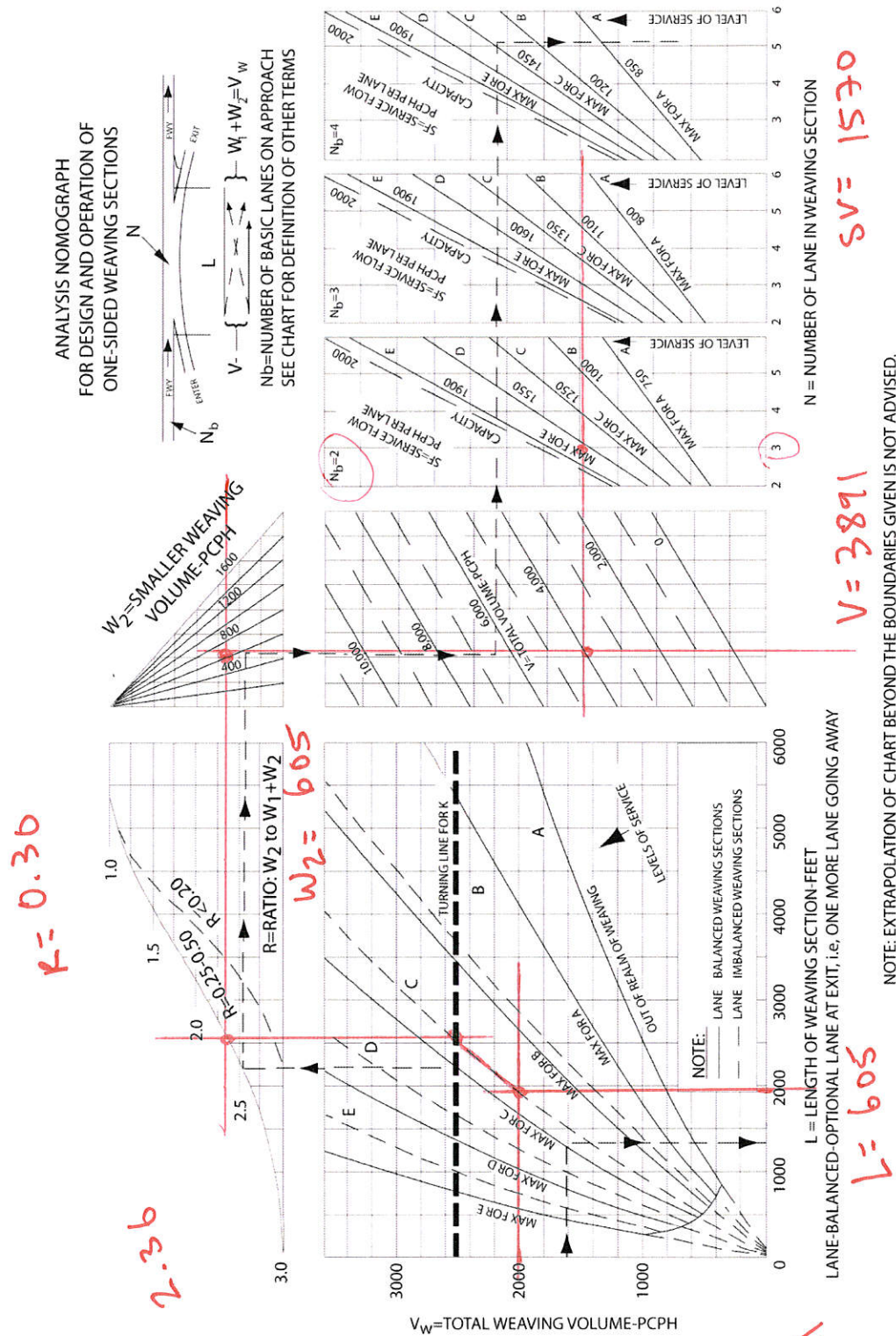
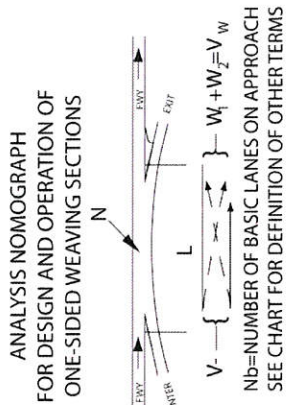
NOTE: EXTRAPOLATION OF CHART BEYOND THE BOUNDARIES GIVEN IS NOT ADVISED.

Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, $W_1 + W_2$ (or VW) followed by projection to the right, intersecting the desired weaving LOS; a vertical drop from this point provides weaving distance $L = 1300$ ft. Returning to first intersection point of VW with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K ". From here the solution line is extended vertically to intersect the K values curve, from which a horizontal extension meets the desired W_2 volume. Then a downward turn to total volume, V , from which the line is horizontally projected to the right, intersection in this case) the desired LOS = C curve having an SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields a N of 5.2; this would be rounded to $N = 5$ lanes.

Figure 504.7A
Design Curve for Freeway and Collector Weaving

LOS E

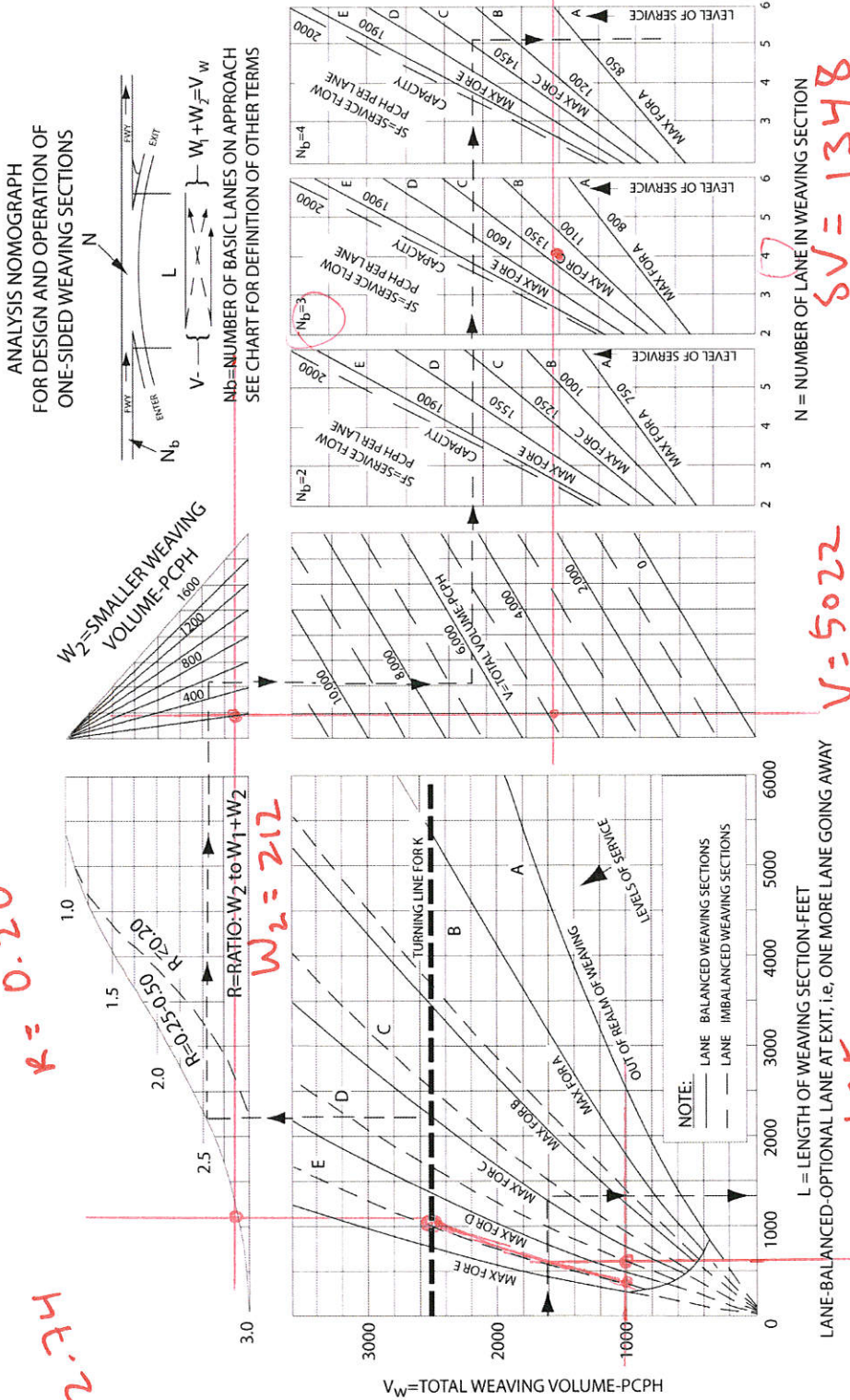
2040 No Build PM - SR-237 EB: US-101 to Mathilda



NOTE: EXTRAPOLATION OF CHART BEYOND THE BOUNDARIES GIVEN IS NOT ADVISED.

Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, W₁ + W₂ (or V_w) followed by projection to the right, intersecting the desired weaving LOS; a vertical drop from this point provides weaving distance L = 1300 ft. Returning to first intersection point of V_w with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K"; from here the solution line is extended vertically to intersect the K values curve; from which a horizontal extension meets the desired W₂ volume. Then a downward turn to total volume, V, from which the line is horizontally projected to the right, intersection (in this case) the desired LOS = C curve having an SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields a N of 5.2; this would be rounded to N = 5 lanes.

Figure 504.7A
Design Curve for Freeway and Collector Weaving



NOTE: EXTRAPOLATION OF CHART BEYOND THE BOUNDARIES GIVEN IS NOT ADVISED.

Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, $W_1 + W_2$, (or V_w) followed by projection to the right, intersecting the desired weaving LOS; a vertical drop from this point provides weaving distance $L = 1300$ ft. Returning to first intersection point of V_w with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K"; from here the solution line is extended vertically to intersect the K values curve, from which a horizontal extension meets the desired W_2 volume. Then a downward turn to total volume, V , from which the line is horizontally projected to the right, intersection (in this case) the desired LOS = C curve having an SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields a N of 5.2; this would be rounded to $N = 5$ lanes.

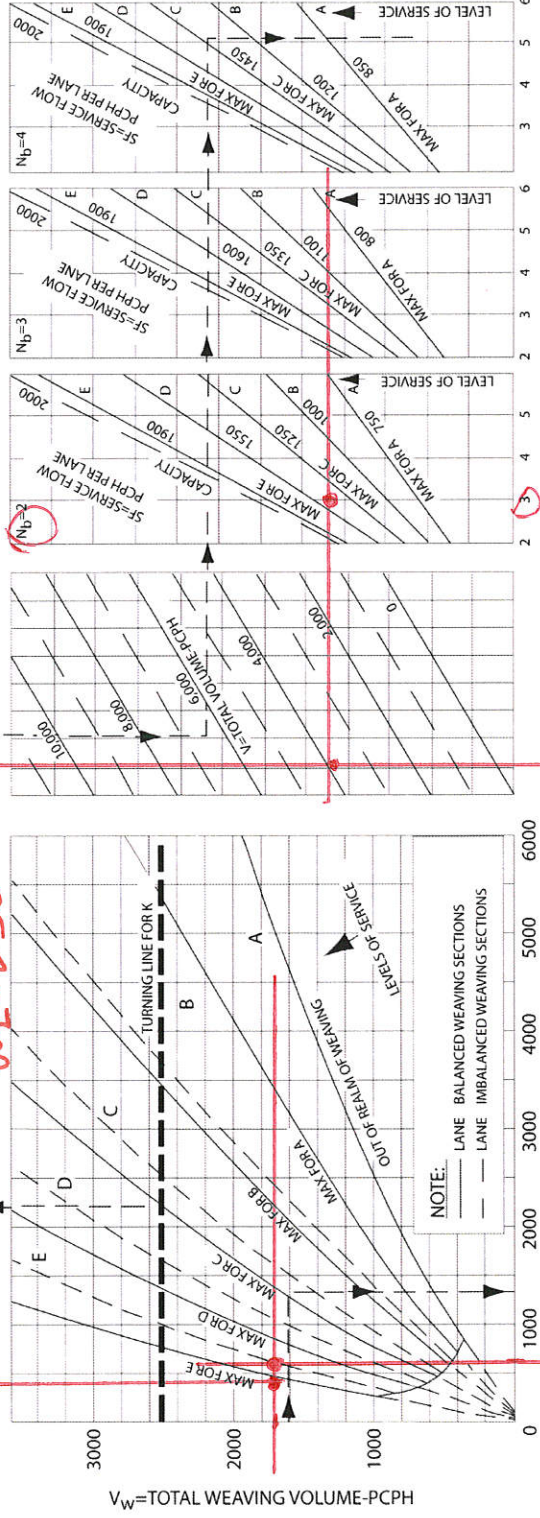
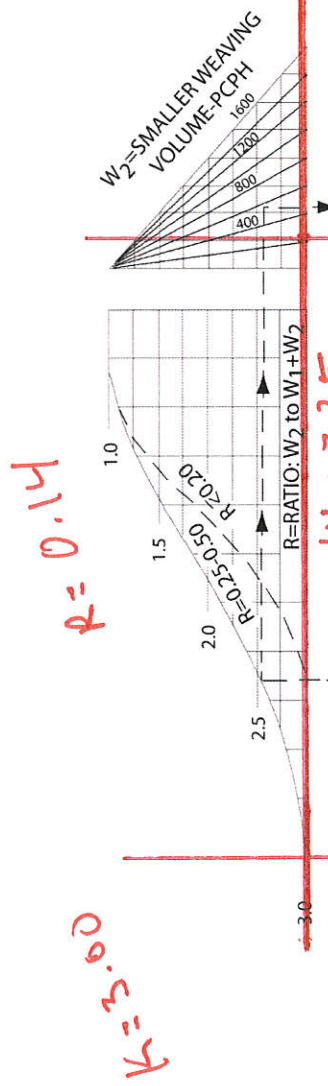
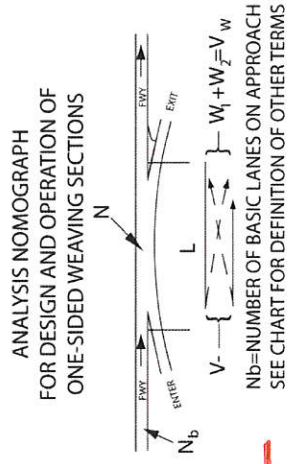
LOS C

2040 No Build PM - US-101 SB: SR-237 to Mathilda

$W_1 + W_2 = 1058$

Figure 504.7A
Design Curve for Freeway and Collector Weaving

LOS D



$N = \text{NUMBER OF LANE IN WEAVING SECTION}$

$V = 3804$

$SV = 1424$

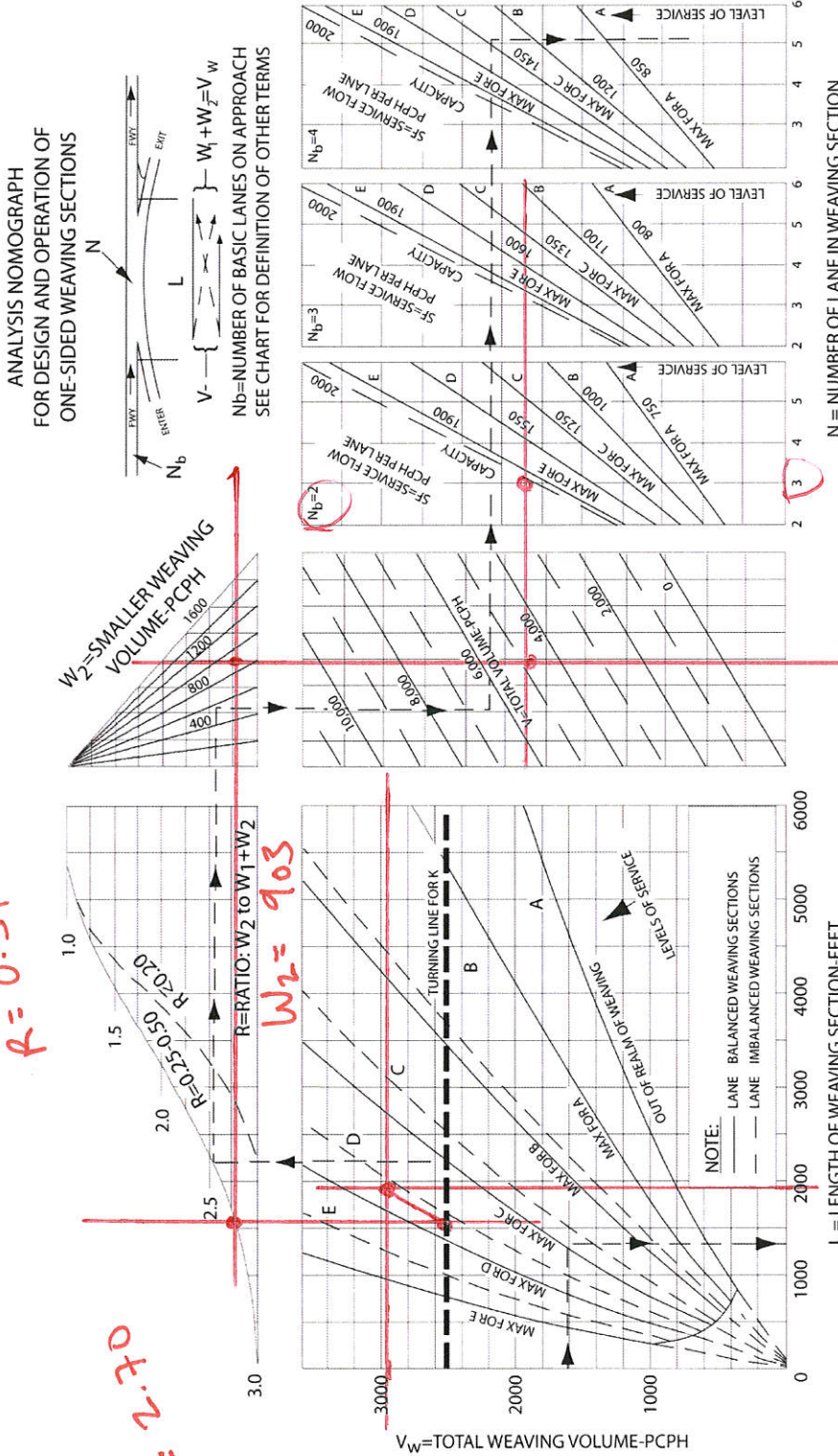
$L = 680$

NOTE: EXTRAPOLATION OF CHART BEYOND THE BOUNDARIES GIVEN IS NOT ADVISED.

Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, $W_1 + W_2$, (or V_w) followed by projection to the right, intersecting the desired weaving LOS; a vertical drop from this point provides weaving distance, $L = 1300$ ft. Returning to first intersection point of V_w with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K ." From here the solution line is extended vertically to intersect the K values curve, from which a horizontal extension meets the desired W_2 volume. Then a downward turn to total volume, V , from which the line is horizontally projected to the right, intersection (in this case) the desired LOS = C curve having an SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields a N of 5.2; this would be rounded to $N = 5$ lanes.

$N_1 + 2N_2 = 1729$

Figure 504.7A
Design Curve for Freeway and Collector Weaving



LOS F

R = 0.31

K = 2.70

R = RATIO: W_2 TO $W_1 + W_2$
 $W_2 = 903$

L = 1930

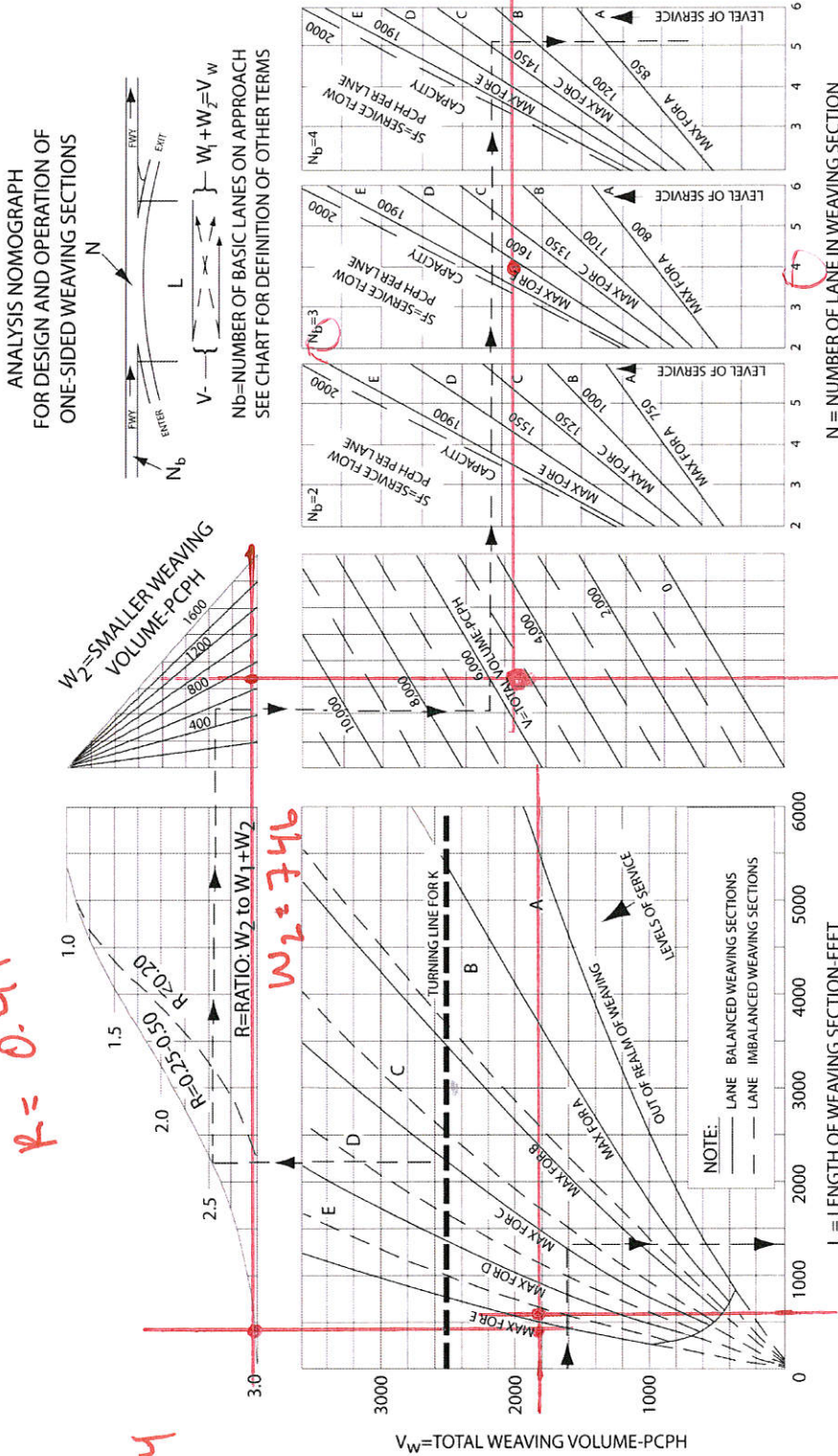
V = 4745

SV = 2094

$W_1 + W_2 = 2443$

Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, $W_1 + W_2$, (or V_w) followed by projection to the right, intersecting the desired weaving LOS; a vertical drop from this point provides weaving distance $L = 1300$ ft. Returning to first intersection point of V_w with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K". From here the solution line is extended vertically to intersect the K values curve, from which a horizontal extension meets the desired W_2 volume. Then a downward turn to total volume, V , from which the line is horizontally projected to the right, intersection (in this case) the desired LOS = C curve having an SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields a N of 5.2; this would be rounded to $N = 5$ lanes.

Figure 504.7A
Design Curve for Freeway and Collector Weaving



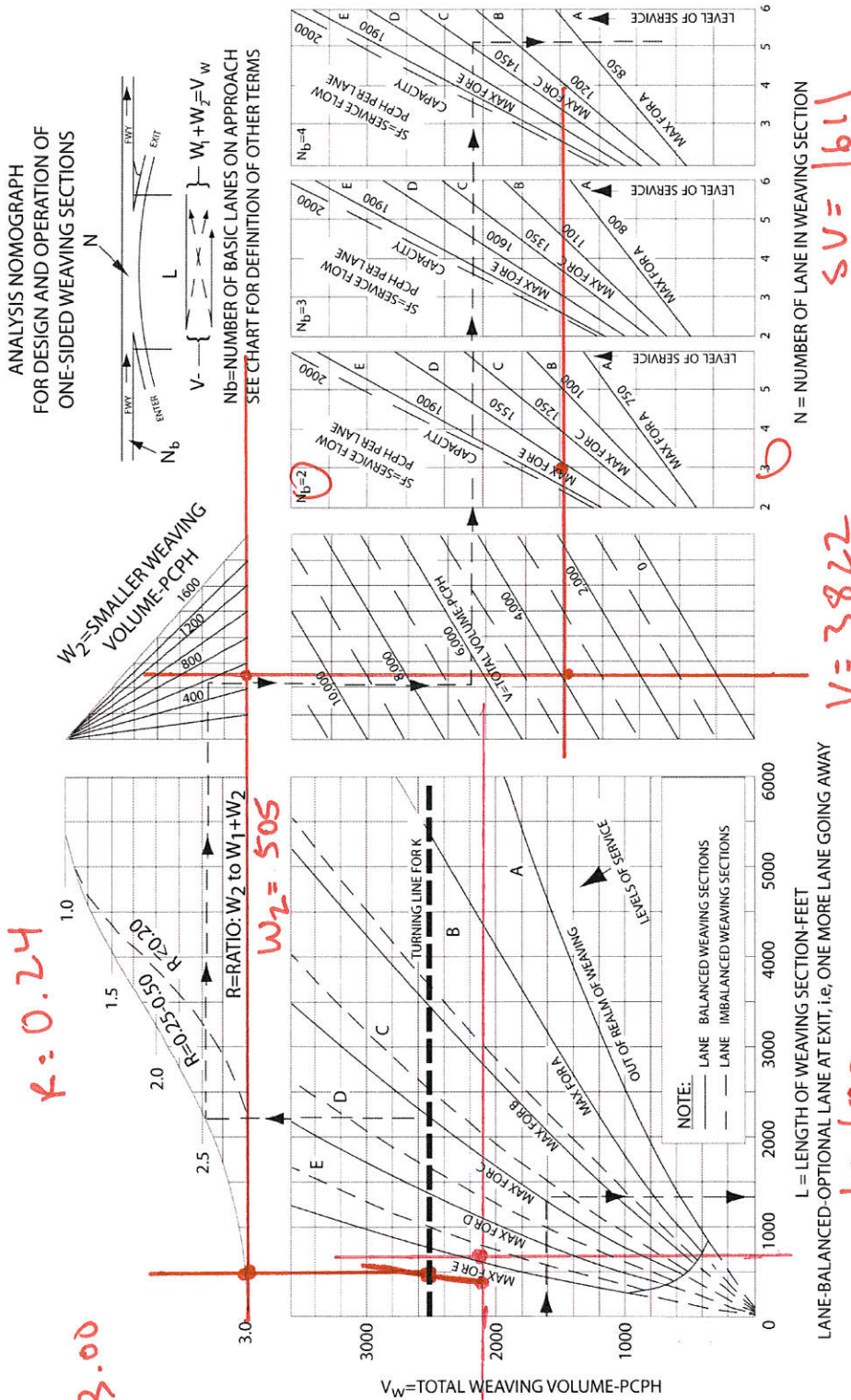
NOTE: EXTRAPOLATION OF CHART BEYOND THE BOUNDARIES GIVEN IS NOT ADVISED.

Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, $W_1 + W_2$, (or V) followed by projection to the right, intersecting the desired weaving LOS; a vertical drop from this point provides weaving distance $L = 1300$ ft. Returning to first intersection point of V with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K": from here the solution line is extended vertically to intersect the K values curve, from which a horizontal extension meets the desired W_2 volume. Then a downward turn to total volume, V , from which the line is horizontally projected to the right, intersection (in this case) the desired LOS = C curve having an SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields a N of 5.2; this would be rounded to N = 5 lanes.

2040 Build 1 AM -US-101 SB: SR-237 to Mathilda

LOS

Figure 504.7A
Design Curve for Freeway and Collector Weaving



NOTE: EXTRAPOLATION OF CHART BEYOND THE BOUNDARIES GIVEN IS NOT ADVISED.

Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, $W_1 + W_2$, (or V_w) followed by projection to the right, intersecting the desired weaving LOS; a vertical drop from this point provides weaving distance $L = 1300$ ft. Returning to first intersection point of V_w with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K"; from here the solution line is extended vertically to intersect the K values curve, from which a horizontal extension meets the desired W_2 volume. Then a downward turn to total volume, V , from which the line is horizontally projected to the right, intersection (in this case) the desired LOS = C curve having an SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields a N of 5.2; this would be rounded to N = 5 lanes.

LOS E

2040 Build 1 PM - SR-237 WB: Mathilda to US-101

k = 0.24

k = 3.00

W2 = 505

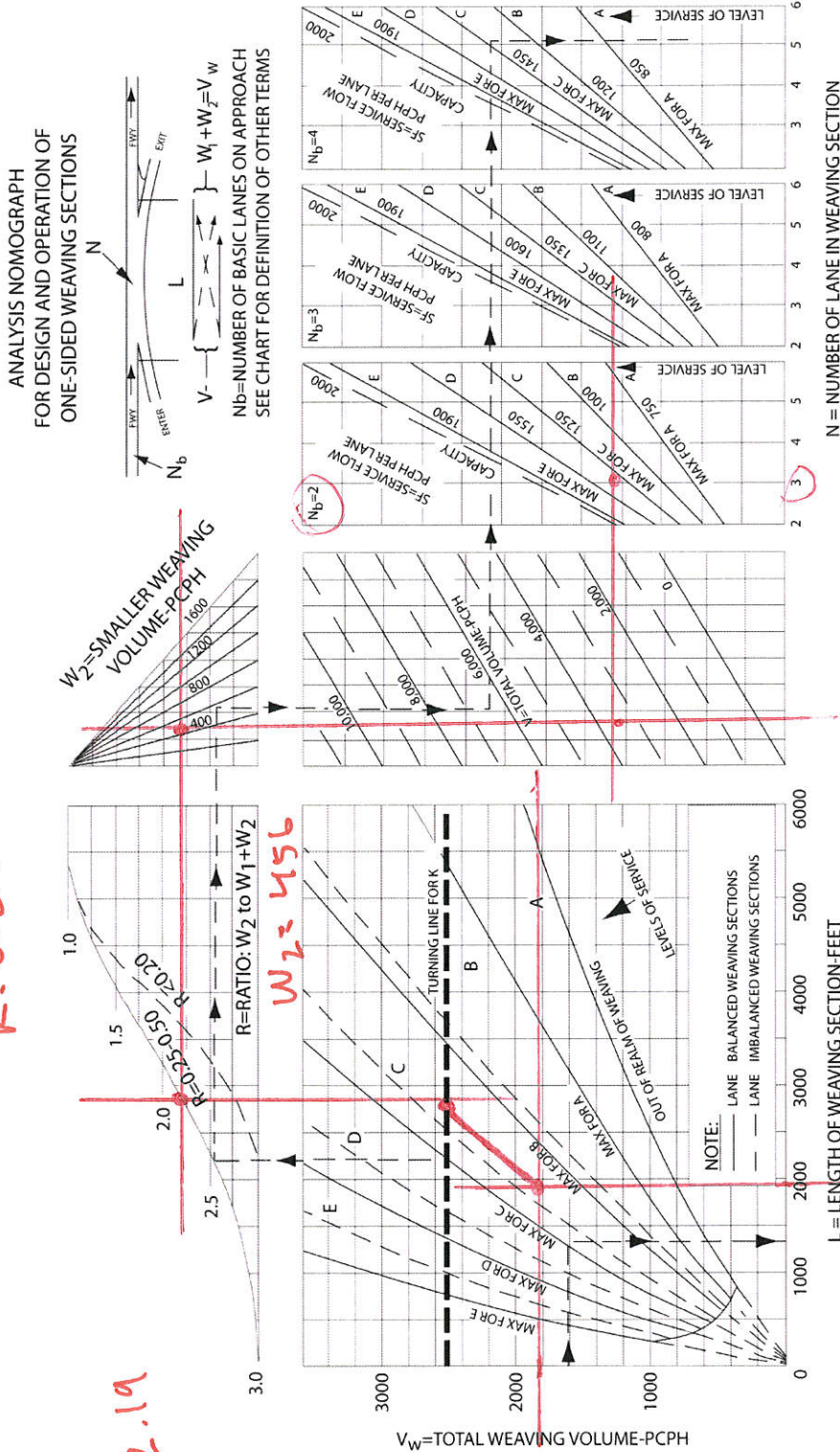
L = 680

V = 3822

SV = 1611

W1 + W2 = 2131

Figure 504.7A
Design Curve for Freeway and Collector Weaving



2040 Build 1 PM - SR-237 EB: US-101 to Mathilda

$K = 0.26$

$K = 2.19$

$W_2 = 456$

$V = 3441$

$SV = 1328$

$L = 1930$

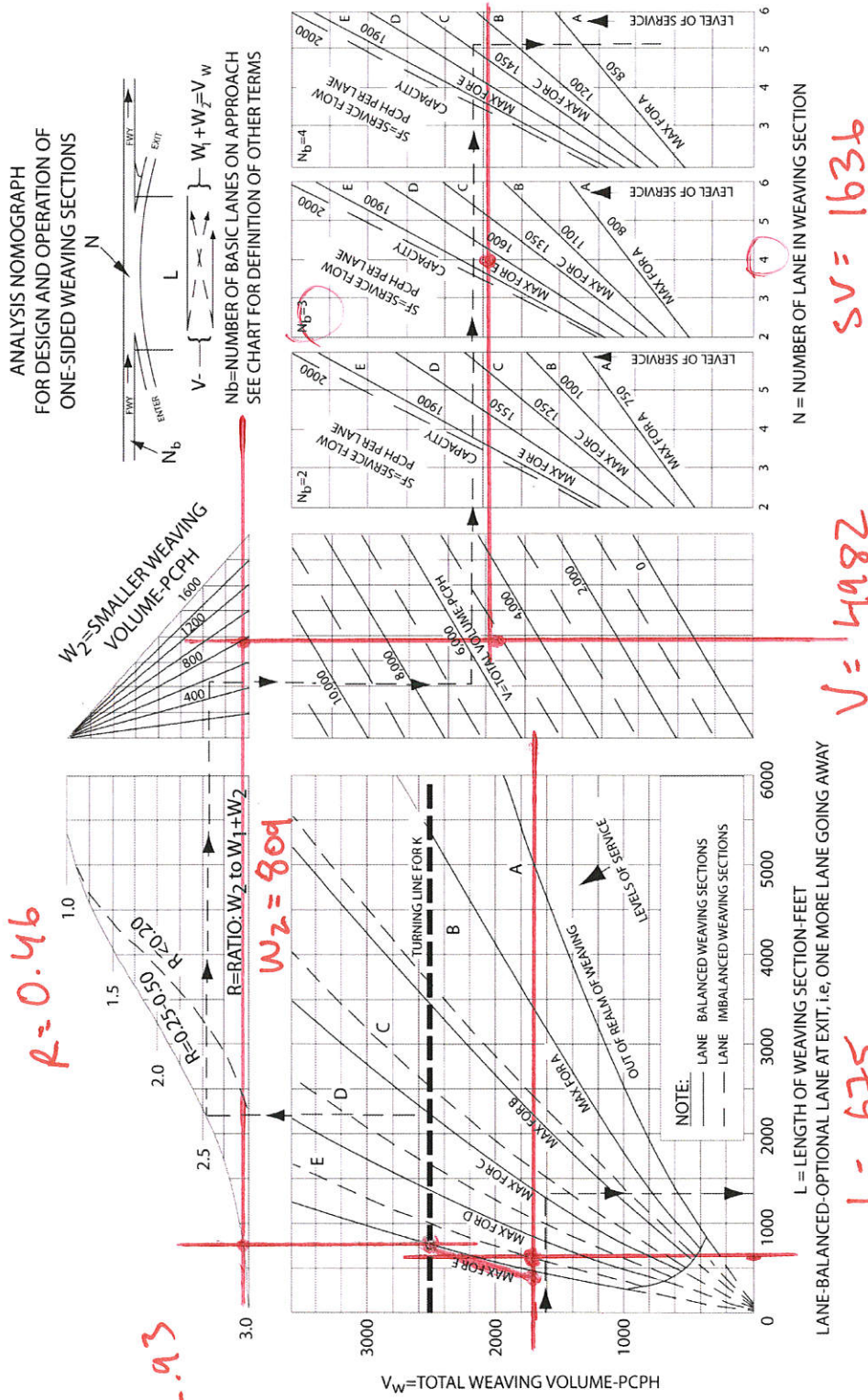
$W_1 + W_2 = 1780$

LOS D

Figure 504.7A
Design Curve for Freeway and Collector Weaving

LOS E

2040 Build 1 PM - US-101 SB: SR-237 to Mathilda



SV = 1636

V = 4982

L = 675

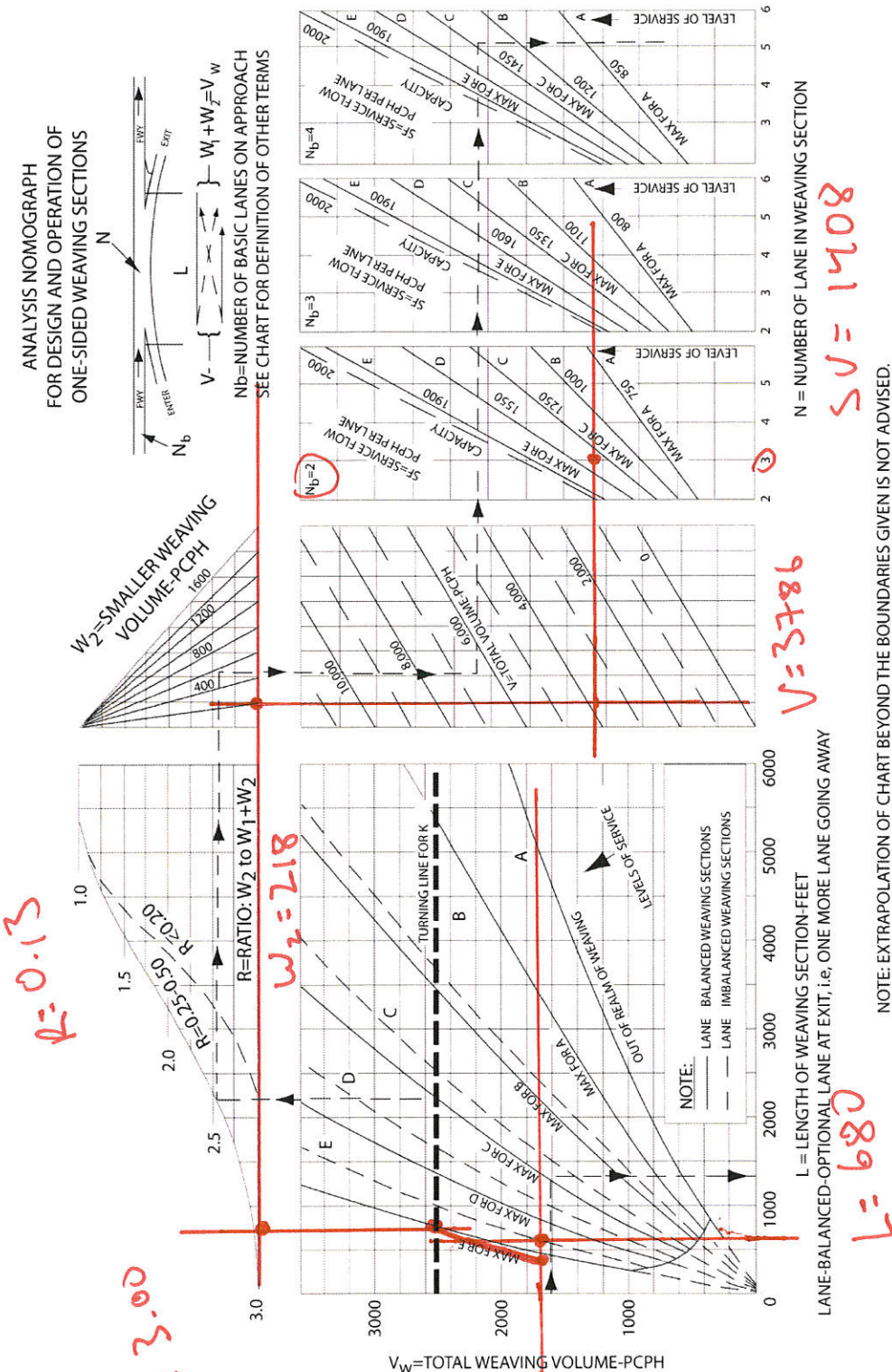
$W_1 + W_2 = 1744$

R = 0.46

k = 2.93

W2 = 800

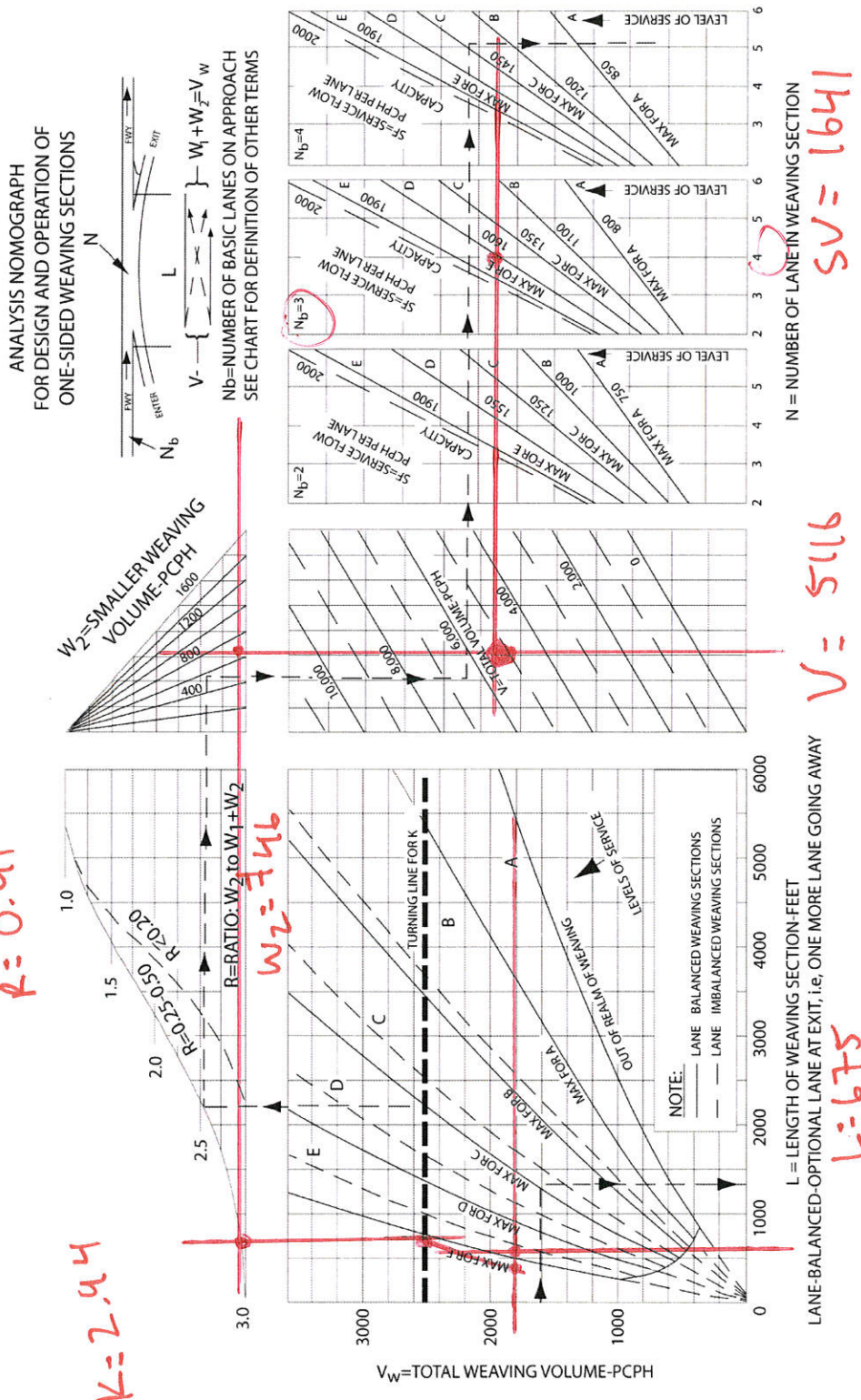
Figure 504.7A
Design Curve for Freeway and Collector Weaving



NOTE: EXTRAPOLATION OF CHART BEYOND THE BOUNDARIES GIVEN IS NOT ADVISED.

Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, $W_1 + W_2$, (or V_w) followed by projection to the right, intersecting the desired weaving LOS; a vertical drop from this point provides weaving distance $L = 1300$ ft. Returning to first intersection point of V_w with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K"; from here the solution line is extended vertically to intersect the K values curve, from which a horizontal extension meets the desired W_2 volume. Then a downward turn to total volume, V , from which the line is horizontally projected to the right, intersection (in this case) the desired LOS = C curve having an SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields a N of 5.2; this would be rounded to $N = 5$ lanes.

Figure 504.7A
Design Curve for Freeway and Collector Weaving



$W_1 + W_2 = 1820$

2040 Build 2 PM - SR-237 EB: US-101 to Mathilda

LOS D

R = 0.26

K = 2.18

W2 = 456

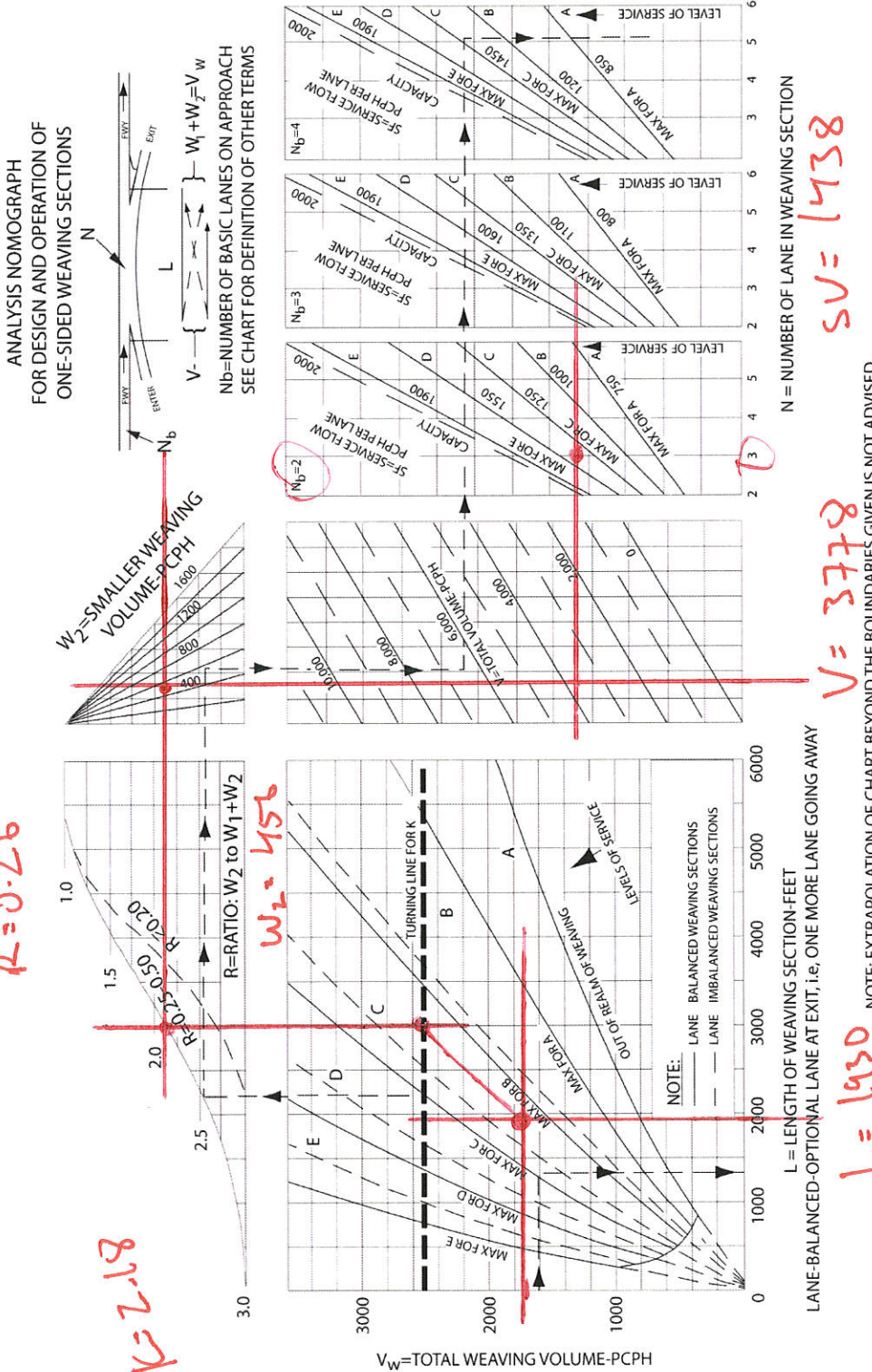
L = 1930

V = 3778

SU = 1738

W1 + W2 = 1779

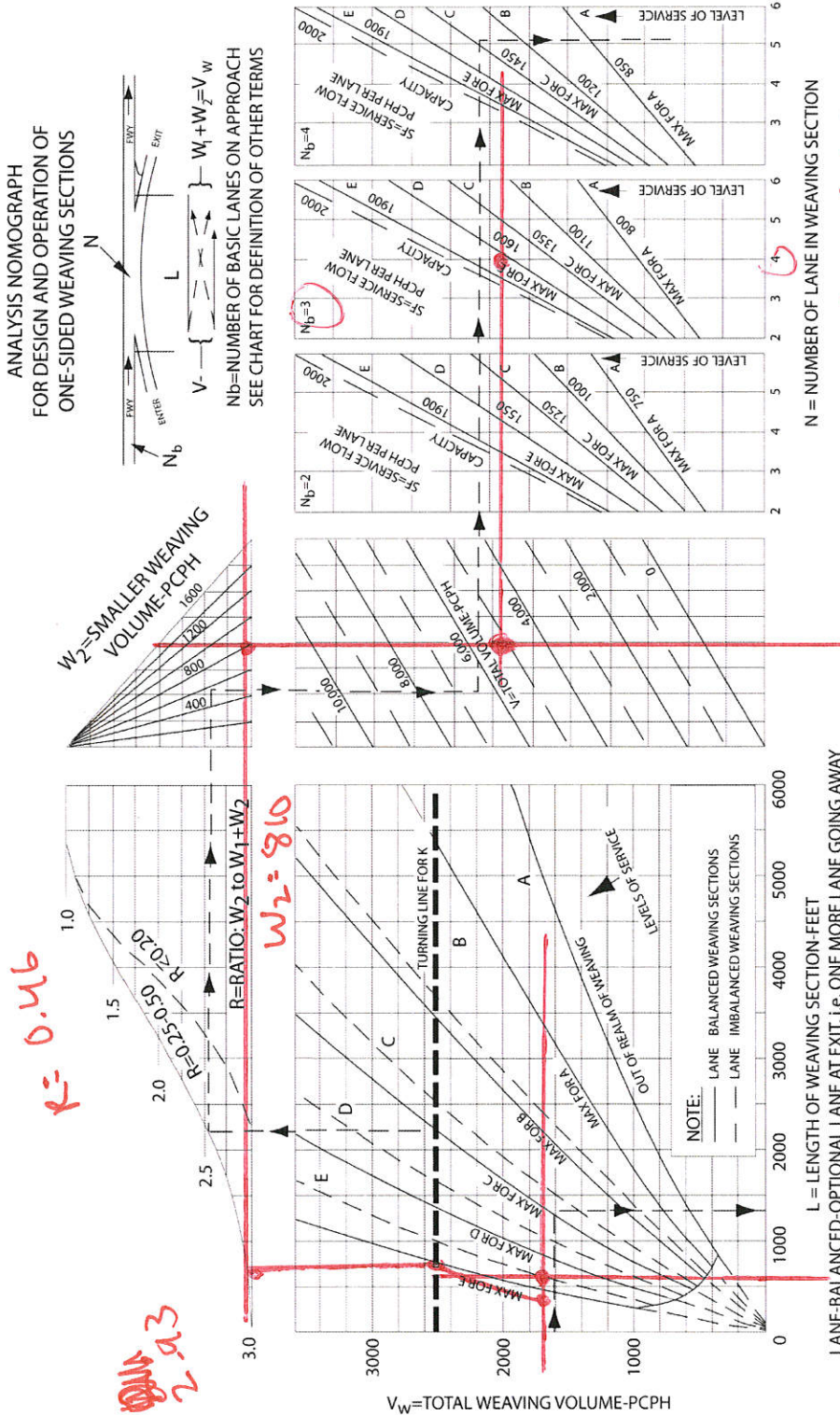
Figure 504.7A Design Curve for Freeway and Collector Weaving



NOTE: EXTRAPOLATION OF CHART BEYOND THE BOUNDARIES GIVEN IS NOT ADVISED.

Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, $W_1 + W_2$ (or V) followed by projection to the right, intersecting the desired weaving LOS: a vertical drop from this point provides weaving distance $L = 1300$ ft. Returning to first intersection point of V with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K ": from here the solution line is extended vertically to intersect the K values curve, from which a horizontal extension meets the desired W_2 volume. Then a downward turn to total volume, V , from which the line is horizontally projected to the right, intersection (in this case) the desired LOS = C curve having an SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields a N of 5.2; this would be rounded to $N = 5$ lanes.

Figure 504.7A
Design Curve for Freeway and Collector Weaving



$N = 5$

$V = 5076$

$L = 675$

$W_1 + W_2 = 1745$

$SV = 1660$

NOTE: EXTRAPOLATION OF CHART BEYOND THE BOUNDARIES GIVEN IS NOT ADVISED.

Example: The nomograph is entered on the left (see dashed line and arrows) with weaving volume, $W_1 + W_2$, (or V_w) followed by projection to the right, intersecting the desired weaving LOS; a vertical drop from this point provides weaving distance $L = 1300$ ft. Returning to first intersection point of V_w with LOS line, an upward projection along the LOS line is intersected with the horizontal, heavy dashed, "turning line for K"; from here the solution line is extended vertically to intersect the K values curve; from which a horizontal extension meets the desired W_2 volume. Then a downward turn to total volume, V , from which the line is horizontally projected to the right, intersection (in this case) the desired LOS = C curve having an SF of 1450 (representing the overall or composite operation of the weaving section), from which a downward extension yields a N of 5.2; this would be rounded to $N = 5$ lanes.

LOS E

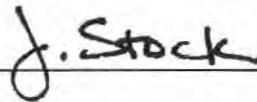
VISUAL IMPACT ASSESSMENT

Mathilda Avenue Improvements at SR 237 and US 101 Project

May 2016

California Department of Transportation
District 4, Santa Clara County, SR 237 and US 101
SR 237 PM 2.7/3.3
US 101 PM 45.2/45.8
EA 04-4H2900

Prepared by: _____



Date: May 13, 2016

Jennifer Stock

Project Landscape Architect

ICF International

CA License # 5155

Approved by: _____



Date: 5/17/16

Kimberly White

Branch Chief, Design A

CA License # 4683

(510) 286-6370

Caltrans, District 4

Statement of Compliance: Produced in compliance with California Environmental Quality Act (CEQA) requirements, as appropriate, to meet the level of analysis and documentation that has been determined necessary for this project.

VISUAL IMPACT ASSESSMENT

Mathilda Avenue Improvements at SR 237 and US 101 Project

PURPOSE OF STUDY AND ASSESSMENT METHOD

The purpose of this visual impact assessment (VIA) is to document potential visual impacts caused by the Mathilda Avenue Improvements at State Route 237 (SR 237) and United States Highway (US 101) project (project) and propose measures to lessen any detrimental impacts that are identified. Visual impacts are demonstrated by identifying visual resources in the project area, measuring the amount of change that would occur as a result of the project, and predicting how the affected public would respond to or perceive those changes. This VIA follows the guidance outlined in *Visual Impact Assessment for Highway Projects*, published by the Federal Highway Administration (FHWA) in March 1988.

PROJECT DESCRIPTION

The project is proposing to improve Mathilda Avenue in the City of Sunnyvale from Almanor Avenue/Ahwanee Avenue to Innovation Way, including on- and off-ramp improvements at SR 237/Mathilda Avenue and US 101/Mathilda Avenue interchanges. On SR 237, the project limits are from 0.3 miles east of the US 101/SR 237 interchange (post mile [PM] 2.7) to 0.3 miles east of the Mathilda Avenue undercrossing (PM 3.3). On US 101, the project limits are from 0.5 miles south of Mathilda Avenue overcrossing (PM 45.2) to 0.3 miles south of SR 237/US 101 interchange (PM 45.8). The total length of the project on Mathilda Avenue is approximately one (1) mile. **Figure 1** shows the location of the project.

The project alternatives include Build Alternative 1, Build Alternative 2, and the No-Build Alternative. The design features of the two Build Alternatives (**Figures 2a and 2b**) include reconfiguration of the US 101/Mathilda Avenue and SR 237/Mathilda Avenue interchanges. The Build Alternatives include design variations for reconfigured roadways and intersections, and construction of new signalized intersections. Proposed improvements included in the Build Alternatives south of Ross Drive on Mathilda Avenue and at the US 101 interchange are identical. This includes new bicycle and pedestrian facilities, utility relocations, new storm water treatment facilities, enhanced lighting, ramp metering modifications, modification of overhead signage, and a new retaining wall. In addition to the improvements listed above, Build Alternative 2 includes construction of a diverging diamond interchange (DDI)¹ north of Ross Drive on Mathilda Avenue (**Figure 3**).

The Build Alternatives would consist of the following roadway improvements:

- Provide three continuous through lanes in each direction of Mathilda Avenue.
- Remove northbound US 101 loop off-ramp and shift traffic to northbound US 101 diagonal off-ramp.

¹ A diverging diamond interchange (DDI), also called a double crossover diamond interchange (DCD) is a type of diamond interchange where traffic briefly crosses over to the left (opposite) side of the roadway, guided by traffic signals at each crossover. This allows vehicles to turn left onto freeway on-ramps without stopping and without conflicting with through traffic. The signals at ramp terminal intersections can be operated with two signal phases (phases when a traffic signal allows for traffic at an intersection to cycle through specific movements for each direction) instead of three.

- Realign and widen northbound US 101 ramps and signalize ramp intersection with Mathilda Avenue, and construct left-turn lane on southbound Mathilda Avenue to access northbound US Highway 101 loop on-ramp.
- Realign southbound US 101 off-ramp and loop on-ramp, and signalize ramp intersection with Mathilda Avenue.
- Modify Mathilda Avenue / Ross Drive signal intersection.
- Close Moffett Park Drive between Bordeaux Drive and Mathilda Avenue, replace with a Class I bikeway (as described below), and shift traffic to Bordeaux Drive and Innovation Way.
- Remove westbound SR 237 ramp signal intersection. Realign westbound SR 237 off-ramp opposite Moffett Park Drive and modify signal intersection.
- Build Alternative 1 would modify westbound SR 237 ramps to provide a diamond configuration.
- Build Alternative 2 would modify Mathilda Avenue and SR 237 ramps to provide a DDI configuration. Eastbound Moffett Park Drive between Innovation Way and Mathilda Avenue would be diverted to Innovation Way to access Mathilda Avenue.

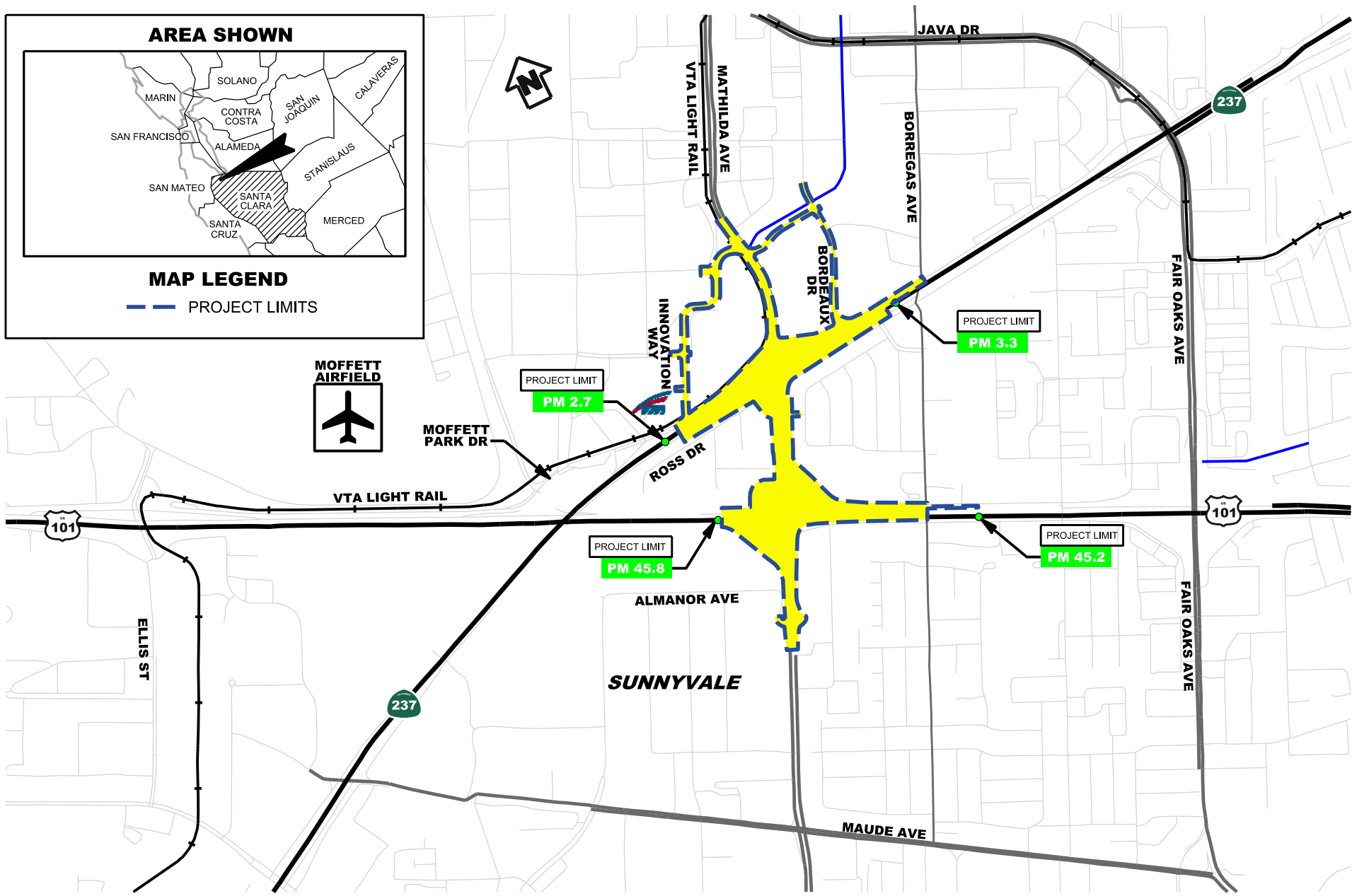
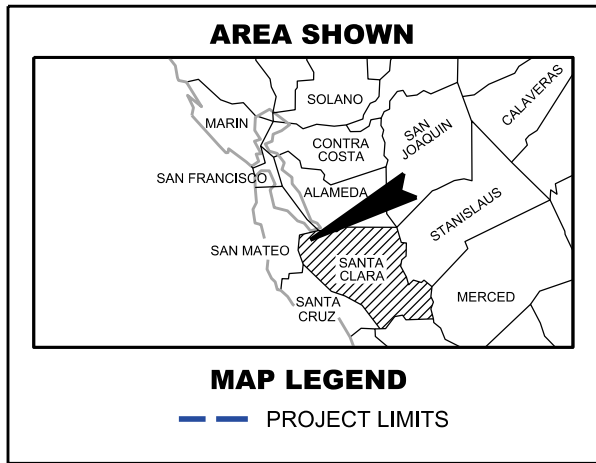
Enhanced bicycle and pedestrian facilities would be provided. Bicycle improvements on Mathilda Avenue would consist of both Class II and Class III bikeways, based on available pavement widths within the project limits, and would connect to the existing Class III bikeway north of Innovation Way and Class I bikeway on the Sunnyvale West Channel. Bicycle improvements on Moffett Park Drive would consist of a Class I bikeway between Bordeaux Drive and Mathilda Avenue. Between Mathilda Avenue and Innovation Way, Class II and Class III bikeways would be considered based on available pavement widths within the project limits. A continuous sidewalk would be provided on the east side of Mathilda Avenue within the project limits with crosswalks, curb ramps, and pedestrian countdown signals at each intersection. The new crosswalks at the reconfigured ramp intersections would be signalized. In addition, both Build Alternatives would provide replacement planting within the US 101 and SR 237 interchanges with Mathilda Avenue and along Mathilda Avenue within the project limits.

Under the No-Build Alternative, no changes would be made to the existing local roadways or freeway system within the project limits.

PROJECT LOCATION AND SETTING

The project location and setting provides the context for determining the type and severity of changes to the existing visual environment. The project is located on Mathilda Avenue, generally between Innovation Way and Almanor Avenue, in the City of Sunnyvale, California. The project is located in the Central Coast biogeographic province, just south of the southern portion of San Francisco Bay (Bay) and the associated Baylands. The project vicinity consists of South Bay urban development, Bay waters, and the Baylands' salt evaporation ponds, salt marshes, and wetlands. The Baylands provide relatively flat open expanses of natural wetland features that have both sinuous and geometric shapes and earth-toned colors that provide an undeveloped, more natural visual contrast to the nearby, densely populated urban area that is characteristic of the project corridor.

The project corridor is defined as the area of land that is visible from, adjacent to, and outside the highway Right of Way (ROW), and is determined by topography, vegetation, and viewing distance. The project corridor is generally flat, except at the highway interchanges that are built up to accommodate the grade-separated crossing of SR 237 over Mathilda Avenue and the crossing of Mathilda Avenue over US 101. Land uses primarily include hotels and office complexes located on either side of Mathilda Avenue; single-



NO SCALE November 2015

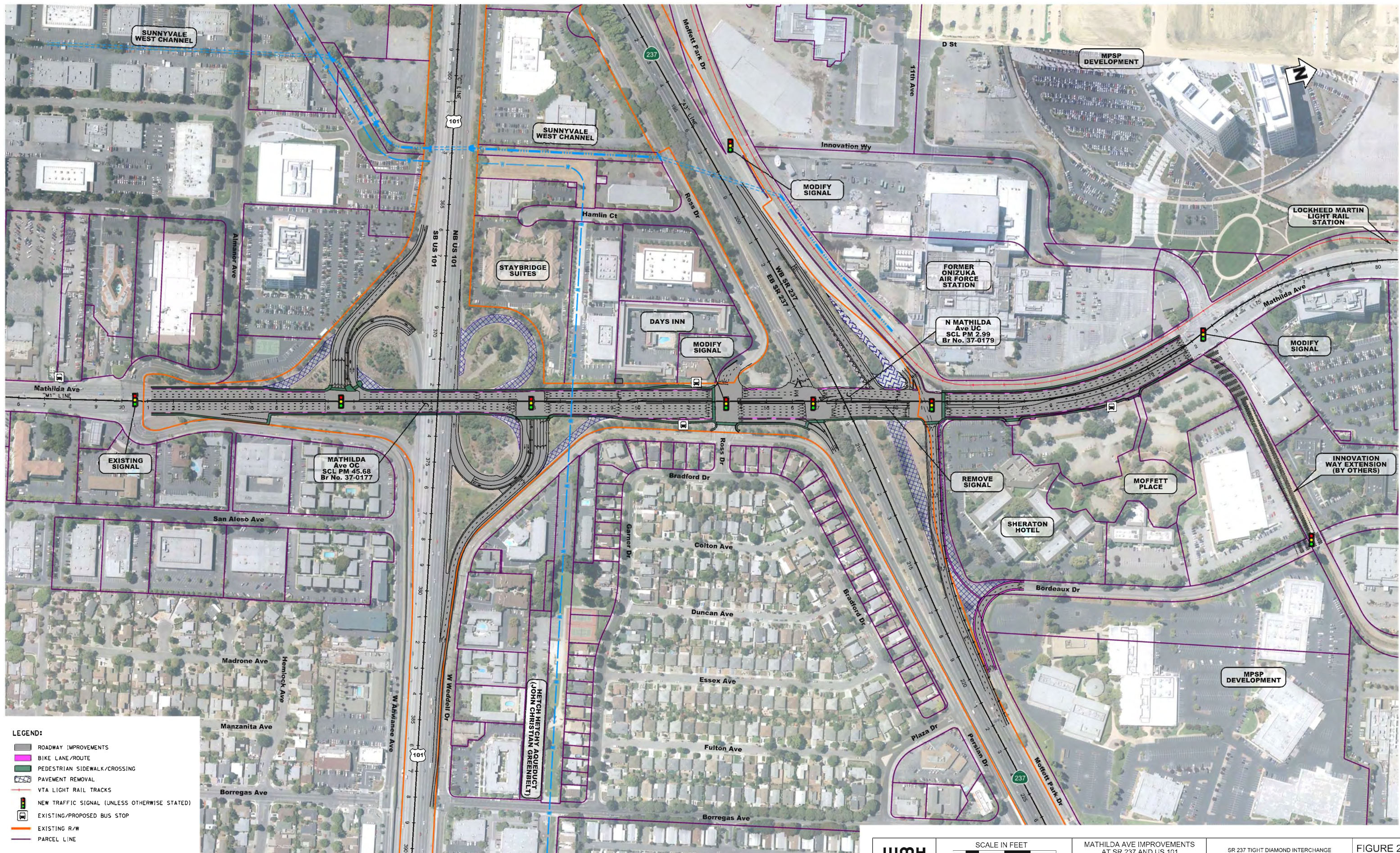


Prepared By: **WMH**

Mathilda Avenue Improvement at SR 237 and US 101

PROJECT LOCATION MAP

Figure
1



- LEGEND:**
- ROADWAY IMPROVEMENTS
 - BIKE LANE/ROUTE
 - PEDESTRIAN SIDEWALK/CROSSING
 - PAVEMENT REMOVAL
 - VTA LIGHT RAIL TRACKS
 - NEW TRAFFIC SIGNAL (UNLESS OTHERWISE STATED)
 - EXISTING/PROPOSED BUS STOP
 - EXISTING R/W
 - PARCEL LINE

wmh

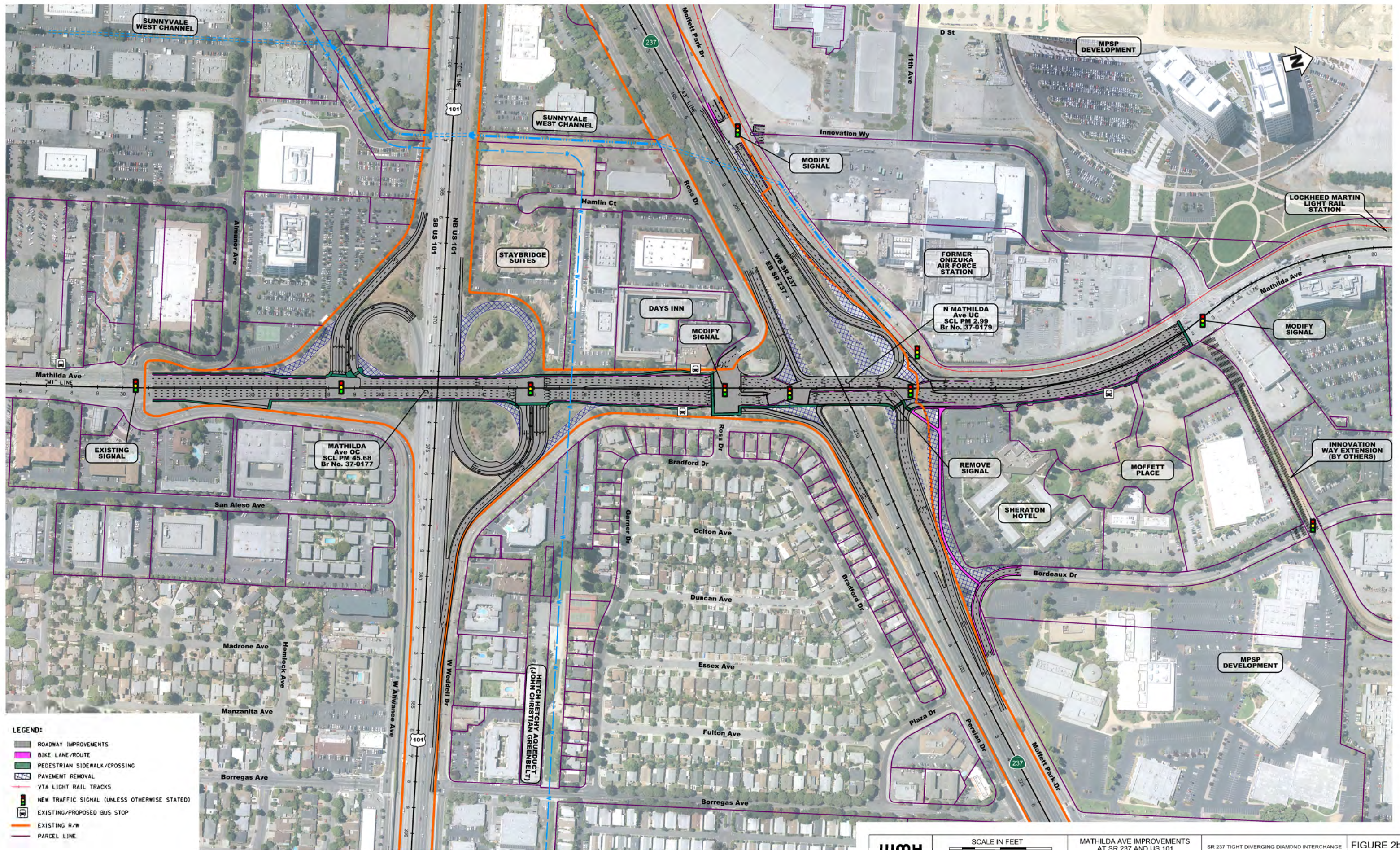


MATHILDA AVE IMPROVEMENTS
AT SR 237 AND US 101
SCL 237 - PM 2.7/3.3
SCL 101 - PM 45.4/45.8

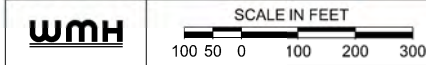
SR 237 TIGHT DIAMOND INTERCHANGE
AND US 101 FULL PAR-CLO INTERCHANGE

FIGURE 2a
JULY 2015

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- LEGEND:**
- ROADWAY IMPROVEMENTS
 - BIKE LANE /ROUTE
 - PEDESTRIAN SIDEWALK/CROSSING
 - PAVEMENT REMOVAL
 - VTA LIGHT RAIL TRACKS
 - NEW TRAFFIC SIGNAL (UNLESS OTHERWISE STATED)
 - EXISTING/PROPOSED BUS STOP
 - EXISTING R/W
 - PARCEL LINE



**MATHILDA AVE IMPROVEMENTS
AT SR 237 AND US 101**
 SCL 237 - PM 2.7/3.3
 SCL 101 - PM 4.4/5.8

SR 237 TIGHT DIVERGING DIAMOND INTERCHANGE
 AND US 101 FULL PAR-CLO INTERCHANGE

FIGURE 2b
 JULY 2015

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family and multi-family residences located east of Mathilda Avenue; and major and minor transportation facilities associated with SR 237, US 101, Mathilda Avenue, and adjoining local roadways and associated signage. The Sunnyvale General Plan Community Character – Design Element identifies that SR 237, US 101, and Mathilda Avenue at US 101 are City gateways that could be improved through the use of special landscaping, signage, patterned pavement, and monuments or artwork (City of Sunnyvale 2011: 4-4). Mature trees and shrubs are present within two median plantings, plantings within interchange loops, and roadside landscaping associated with businesses and residential areas to provide visual buffering from Mathilda Avenue, SR 237, and US 101.

While not scenic vistas, the wide corridors of Mathilda Avenue, SR 237, US 101 and the elevated SR 237/Mathilda Avenue and Mathilda Avenue/US 101 overcrossings allow for scenic background views of the Diablo Range to the northeast and the Santa Cruz Mountains to the southwest. Vista views are not available due to buildings, infrastructure, and mature trees that intervene within potential vista views. There is no roadway within or near the project area that is designated in federal, State, or local plans as a scenic highway or route worthy of protection for maintaining and enhancing scenic viewsheds (Caltrans 2016, City of Sunnyvale 2011).

US 101 is classified by Caltrans as a Landscaped Freeway between PM 45.57 and 47.14 (Caltrans 2014a). Along US 101, this designation begins approximately at the gore of northbound Mathilda Avenue exit ramp and continues north past the project limits on US 101. As defined by the Outdoor Advertising Act, a landscaped freeway “means a section or sections of a freeway that is now, or hereafter may be, improved by the planting at least on one side or on the median of the freeway ROW of lawns, trees, shrubs, flowers, or other ornamental vegetation requiring reasonable maintenance.” Landscaped freeways must have planting areas that are at least 1,000 feet in length that are in healthy condition and improve the aesthetic appearance of the highway. Functional plantings (i.e., plantings for erosion control, traffic safety, reduction of fire hazards, and traffic noise abatement, or other non-ornamental purposes) do not qualify. The placement of advertising is prohibited within 660 feet of the edge of the ROW of a landscaped freeway. (Caltrans 2014b.)

The project corridor is well-lit from street lighting along Mathilda Avenue and at the SR 237 and US 101 interchanges, safety lighting in parking lots, and interior and exterior building lighting associated with residences and businesses.

VISUAL RESOURCES AND RESOURCE CHANGE

Visual resources of the project setting are defined and identified below by assessing *visual character* and *visual quality* in the project corridor. *Resource change* is assessed by evaluating the visual character and the visual quality of the visual resources that comprise the project corridor before and after the construction of the project.

The visual character of the project would be compatible with the existing visual character of the corridor. The project and its Build Alternatives would reconfigure the SR 237 and US 101 interchange ramps and reconfigure Mathilda Avenue to accommodate new signalized intersections and left-turn lanes. To accommodate this, mature trees and shrubs would be removed at the median planting between Stations² 47+00 to 51+00 and 64+00 to 68+00 on Mathilda Avenue, within the SR 237 and US 101 interchange loops to accommodate the shifted ramps, west of Mathilda Avenue to accommodate a new retaining wall between

² Refer to Figures 2 and 3a for stationing.

Stations 46+00 and 49+50, and east of Mathilda Avenue between Stations 49+00 and 56+00 to accommodate new lanes for the SR 237 onramp and right hand turns onto Ross Drive. These changes would impact the views from nearby property owners and views from the roadway corridor. However, most of the areas with existing landscaping that would be disturbed during construction would receive replacement plantings to restore the aesthetic qualities that such landscaping provides. In addition, new landscape plantings would occur where paved portions of ramps are removed to accommodate the reconfigurations, improving aesthetics; the reconfigured ramps would not greatly alter the appearance of the SR 237 and US 101 interchanges with Mathilda Avenue. Therefore, the visual character of the corridor and land adjacent to the ROW would not be greatly altered. Signalized intersections, bicycle and pedestrian facilities, street lighting, ramp metering, signage, and light rail crossing facilities are all existing elements associated with the project corridor and changes associated with these features would be implemented in a manner that maintains the existing visual character. Similarly, modifications to existing retaining walls and sound walls would be consistent with existing conditions and would not greatly alter views associated with the corridor.

The visual quality of the existing corridor would be slightly altered by the project. Generally, the corridor would be slightly wider, but would retain its form, line, color, and texture in a manner that is consistent with existing conditions. Views from the project corridor to the surrounding landscape would be much the same because the Build Alternatives would only result in minor changes along the existing corridor to accommodate the project and landscaping would be replaced, retaining the existing vividness, intactness, and unity. Views of the Diablo Range and Santa Cruz Mountains would not be altered. Views of the project corridor from neighbors and from the roadway corridor would be slightly altered in a manner that would result in a slight reduction in the overall visual quality, largely due to vegetation removal. While these areas would be landscaped as part of the project, it would take several years for the vegetation to mature.

As a result, Resource Change (changes to visual resources as measured by changes in visual character and visual quality) would be moderate-low.

VIEWERS AND VIEWER RESPONSE

Neighbors (people with views *to* the road) and *roadway users* (people with views *from* the road) will be affected by the project. Neighbors consist of employees and patrons at nearby businesses and residents that immediately border the project corridor. Neighbors also include roadway users connecting to the project corridor from local roadways. Business occupants and residents are considered to have high visual sensitivity because while they are accustomed to views of the existing roadways and passing traffic, they generally view the project site for an extended period. Therefore, business occupants and residents are likely to have a high sense of ownership over local views, and are more likely to be affected by changes in the views from their businesses or homes than the visiting, business patrons or those passing by the site on local roadways. Business patrons are more focused on visiting businesses than on the project corridor and they have intermittent and limited views of the project corridor. Therefore, business patrons are likely to have moderate-low visual sensitivity.

Roadway users include local commuters traveling to and from work, shoppers, recreational travelers, and commercial vehicles on Mathilda Avenue, SR 237, US 101, Moffett Park Drive, Bordeaux Drive, and Innovation Way. Roadway users travel at speeds ranging from a stop to approaching 75 miles per hour (the posted speed limit is 65 miles per hour) on SR 237 and US 101, 55 miles per hour (the posted speed limit is 45 miles per hour) on Mathilda Avenue, 55 miles per hour (the posted speed limit is 45 miles per hour) on Bordeaux Drive, and 35 miles per hour (the posted speed limit is 25 miles per hour) on Innovation Way.

Depending on speed, drivers and passengers are able to take in brief to longer views of the scenery around them. Most views from the project corridor are of surrounding development; however, sections of the roadway provide for more scenic views of a vegetated roadway corridor with views to the hillsides and mountains in the background. Therefore, roadway users are considered to have moderate visual sensitivity.

Public scoping comments generally focus on providing feedback and questions on specific elements of the project, such as bicycle and pedestrian safety considerations. The public comments did not express opposition to the project. Therefore, while not specifically stated, the responses tend to indicate general public support of improving the project corridor. Therefore, it is anticipated that the average response of all viewer groups will be moderate due to viewer group sensitivities and public interest surrounding the project.

VISUAL IMPACT

Visual impacts are determined by assessing changes to the visual resources and predicting viewer response to those changes. As discussed above in *Project Location and Setting*, there are no officially designated scenic roadways within or near the project corridor. In addition, scenic vista views are not available from the corridors of Mathilda Avenue, SR 237, and US 101 at the project site due to buildings, infrastructure, and mature trees that intervene within these potential vista views. Therefore, implementation of the project would not damage scenic resources, such as trees, rock outcroppings, and historic buildings along a scenic highway or scenic vistas. Impacts to visual resources resulting from changes to the existing visual character and quality of the site and changes in light and glare are discussed below.

Build Alternatives

As described in the *Project Description*, Build Alternatives 1 and 2 have the same footprint for the US 101 interchange with Mathilda Avenue, and the same roadway cross section between the US 101/Mathilda Avenue interchange and Ross Drive, the Moffett Park Drive connection to Bordeaux Drive, and between the Sheraton Sunnyvale parking lot entrance on Mathilda Avenue and the Innovation Way extension to Mathilda Avenue. These changes would look the same under both Build Alternatives. The primary difference is that Build Alternative 1 would have a diamond configuration while Build Alternative 2 would have a DDI configuration. Both of these configurations would have a similar visual character and would result in similar impacts to existing features within the project corridor. Because the Build Alternatives would be visually similar, temporary and permanent impacts are discussed together below. Simulations for key observation points (KOPs) were used to evaluate project impacts. The KOPs are mapped on **Figure 4** and the simulations are provided in **Figure 5 to Figure 7**.

Temporary Impacts – Build Alternatives 1 and 2

General construction activities, construction staging/stockpiling, the storage of road-widening/building materials, the presence of construction equipment, and temporary traffic barricades would result in temporary construction impacts by altering the composition of the view available from and to the project corridor. Under both Build Alternatives, the greatest focus of visible activities associated with construction would be on roadway and ramp modifications. Other visible activities occurring during construction under both Build Alternatives, which have the potential to result in visual impacts are described in more detail under *Permanent Impacts – Build Alternatives 1 and 2*, and include the removal of mature landscaping including trees, shrubs, and/ or vines; replacement of the sound wall between Weddell Drive and the northbound US 101 off-ramp; the installation of the new retaining wall that would be located within existing state ROW on the west side of Mathilda Avenue north of the existing northbound US 101 loop off-

ramp; the modification of the local roadway intersection connections and driveway entrances to Mathilda Avenues; the relocation of utilities; the modification and installation of lighting, ramp metering, and overhead signage; and the enhancement of bicycle and pedestrian facilities. During construction, these activities would be seen as a continuation of construction activities associated with roadway and ramp improvements and would only result in minor visual changes as the modifications are occurring. In addition, construction staging areas would be temporarily visible within the US 101 interchange with Mathilda Avenue and between the westbound SR 237 ramps and Moffett Park Drive, where some trees and shrubs would be affected to accommodate staging.

Individuals most affected by construction would be single-family residences along Weddell Drive and Persian Drive and multi-family residences along Weddell Drive. Single-family residences along Weddell Drive and Persian Drive face Bradford Drive. Privacy fences and Weddell Drive and Bradford Drive separate their back yards from Mathilda Avenue. These residents would experience visually disruptive construction activities within close proximity to their homes. Construction occurring north of SR 237 would not greatly affect businesses in this area because there has been and continues to be a great deal of construction occurring within this area due to its redevelopment, and existing businesses would be accustomed to seeing construction activities. Construction activities would be visible from SR 237 and US 101, but roadway users would pass by the Mathilda Avenue interchanges very quickly and would have only brief, passing views lasting a few seconds at normal highway speeds. Businesses located west of Mathilda Avenue, off of Hamlin Court, would have extremely limited views of construction associated with vegetation removal to install a new retaining wall. The majority of construction activities would be visible to roadway users on Mathilda Avenue, where the bulk of construction would take place. Specific equipment that would be used for construction includes graders, excavators, pavers, compactors, and various types of construction vehicles. In general, the visual presence of construction activities is considered temporary because the project would take 12 months to construct. Temporary visual changes from construction signaling, signage, and lighting would occur, though they are not considered to be adverse. Nighttime construction would likely occur and some nighttime lighting at the construction site would be required and could result in nuisance light if not properly designed. Avoidance, Minimization, and/or Mitigation Measure, *Minimize Fugitive Light from Portable Sources Used for Construction*, would ensure that lighting used for construction would be directed downward and that spill light would be minimized to the greatest extent possible.

Permanent Impacts – Build Alternatives 1 and 2

There are no scenic roadways or scenic vista views in or near the project area, so there would be no affect to such resources. Minor visual changes would result from the project and its Build Alternatives. The presence of relocated utilities would be consistent with existing conditions, because they are already an existing visual element within the project corridor. Therefore, their relocation would not alter the visual character of views of and from the project corridor. Underground utilities would be relocated and would not be seen because they would again be placed underground, consistent with existing conditions. Slightly modified business entrances would not be very noticeable under both Build Alternatives, would be visually consistent with existing conditions, and would not alter the appearance of these driveways. Similarly, ramp metering facilities and overhead signage already exists within the project corridor and relocating and modifying ramp meters and overhead signs would be visually consistent with existing conditions and would not result in notable changes to the visual appearance of the project corridor. Therefore, the most notable visual changes resulting from both Build Alternatives would be modifications to Mathilda Avenue, modifications to the SR 237 and US 101 on- and off-ramps, and associated vegetation removal. Both Build Alternatives would require removal of mature landscaping including trees, shrubs, and/ or vines at the following locations:

- At the US 101 interchange with Mathilda Avenue and between the westbound SR 237 ramps and Moffett Park Drive to accommodate construction staging areas;
- Within the Mathilda Avenue medians between Stations 47+00 to 51+00 and Stations 64+00 to 68+00 to accommodate lane modifications;
- Within the SR 237 and US 101 interchange loops to accommodate staging, ramp modifications, and the clear recovery zone;
- Between Weddell Drive and the northbound US 101 off-ramp to slightly shift and relocate the sound wall;
- West of Mathilda Avenue between Stations 46+00 to 49+50 to accommodate a new retaining wall; and
- East of Mathilda Avenue between Stations 49+00 to 56+00 to accommodate new lanes for the SR 237 onramp and right hand turns onto Ross Drive.

Mature landscaping is considered to be an attractive visual resource. Most of these areas would be replanted as a part of the project. This includes portions of areas disturbed for construction staging that would be converted to vegetated, grassy bioretention basins while other portions would be re-landscaped. Implementation of Avoidance, Minimization, and/or Mitigation Measures, *Restore Highway Planting* and *Incorporate Bioretention Basins in Planting Design*, would ensure that replacement planting and bioretention basins will be designed to blend with highway planting and create a cohesive landscape.

As shown in the *Simulated Views* for KOP 1 (**Figure 5**) and KOP 2 (**Figure 6**), changes to the Mathilda Avenue corridor to accommodate turn lanes, bicycle facilities, and intersection improvements would result in slight alterations to views associated with the project corridor, but the changes would be largely consistent with the existing visual character of the multi-lane corridor. As shown in the simulations, changes to landscaping on both sides of the northbound US 101 on- and off-ramp to accommodate the reconfigured ramp, west of Mathilda Avenue to accommodate the new retaining wall; and east of Mathilda Avenue to accommodate new lanes for the SR 237 onramp and right hand turns onto Ross Drive would result in slight visual changes but views would still be largely vegetated with replacement plantings.

As seen in the *Simulated View* for KOP 1, some vegetation removal would be needed to shift the ramps over to create a perpendicular connection for the proposed northbound US 101 on- and off-ramps to Mathilda Avenue. The relocated sidewalk and crosswalk would be slightly more visible from this vantage. New elements within this view would be the new traffic signal and a short, concrete barrier that would be seen on the ramp to separate traffic that is entering and exiting the ramp. Groundcovers and accent shrubs would be planted where the old ramp alignment is removed. These changes would create a slightly wider ramp but would allow for the existing northbound US 101 off-ramp to be removed and revegetated. The proposed southbound on- and off-ramps would also result in similar visual changes associated with creating a perpendicular intersection with Mathilda Avenue. These changes would be visible to roadway users on Mathilda Avenue and using the ramps and to pedestrians using sidewalks.

Both Build Alternatives would involve the installation of one new retaining wall that would be located within the existing state ROW on the west side of Mathilda Avenue, north of the existing northbound US 101 loop off-ramp. The wall would be approximately 400 feet long and vary in height from 2 to 4 feet. The face of the wall would be adjacent to the existing ROW line and require vegetation removal to construct the wall. Removal of mature trees and shrubs west of Mathilda Avenue would slightly detract from views, but this area would be replanted with screening shrubs and the new retaining wall would not be visible from Mathilda Avenue because it would be even with or at a slightly lower elevation than the roadway,



Figure 4
KOP Simulation Location Map
 Mathilda Avenue Improvements at SR 237 and US 101 Project



Existing



Simulation

Graphics ... 00522.13 (5-2-2016) tm



Figure 5
KOP 1 – Existing and Simulated Views for Build Alternatives 1 and 2
Mathilda Avenue Improvements at SR 237 and US 101 Project



Existing



Simulation

Graphics ... 00522.13 (5-2-2016).tm



Figure 6
KOP 2 – Existing and Simulated Views for Build Alternatives 1 and 2
Mathilda Avenue Improvements at SR 237 and US 101 Project



Graphics ... 00522.13 (5-12-2016) tm



Figure 7
KOP 3 – Existing and Simulated Views for Build Alternatives 1 and 2
Mathilda Avenue Improvements at SR 237 and US 101 Project

as shown in the *Simulated View* for KOP 1. Views from the parking lot of businesses to the west of this new retaining wall would be slightly affected by tree removal. However, views of the wall would be screened by the existing privacy fencing along the parking lot that buffers views of the roadway and replanting with screening shrubs would help to replace some of the screening that existing trees and shrubs provide. As shown in the *Simulated View* for KOP 2, the landscaping changes west of Mathilda Avenue are not very noticeable because they would blend in with the existing roadside vegetation. Avoidance, Minimization, and/or Mitigation Measure, *Implement Aesthetic Treatments on Bridge Barriers, Sound Walls, and Retaining Walls*, would ensure that the aesthetic treatment of any visible wall surface will be included.

Both Build Alternatives would also require that the vegetation between Mathilda Avenue and Persian and Weddell Drives, between Stations 49+00 and 56+00, be removed to accommodate new lanes for the SR 237 onramp and right hand turns onto Ross Drive, which can be seen in the *Simulated Views* for KOP 1 and KOP 2. Removing this vegetation would slightly detract from views associated with the project under both Build Alternatives. As shown in the simulations, this area would be replanted with trees, shrubs, and groundcovers but it would take several years for this landscaping to mature and provide the same level of vegetative cover and shade. However, the landscaping would still be attractive and aid in maintaining a vegetated roadway corridor. These changes would be most visible to roadway users and pedestrians. It would not be readily visible to adjacent residences because the existing noise barrier along Mathilda Avenue would remain and residential privacy fencing and residential landscaping helps to limit views. However, at some locations, the tall evergreen trees growing in this landscaped area (refer to *Existing View* for KOP 2) would no longer be visible rising above the fence lines because they would be removed.

The roadway widening would slightly increase the roadway surface area and roadway striping would be altered but would not substantially change the character of the roadway under both Build Alternatives. As shown in the *Existing View* for KOPs 1 and 2, cobbles pave the thinner portions of the median that is located between Stations 47+00 and 51+00 and mature trees are growing where the median is slightly wider. Under both Build Alternatives, as shown in the simulations, the median footprint would be slightly modified and cobbles would still be used to pave thinner portions of the median. As shown in KOP 1, the thinner median sections would not be wide enough to accommodate replacement plantings, which would result in views of a slightly wider roadway corridor. As shown in the simulation for KOP2, instead of trees, low-growing groundcover and accent shrubs would be planted in the median near the Mathilda Avenue intersection with Ross Drive, which would slightly alter views but would not substantially alter the visual character of the project corridor. The medians from the US 101 ramps and south to Almanor Avenue and north of Ross Drive would be slightly reconfigured, but would remain paved with cobbles and concrete, consistent with existing views. However, wider portions of these reconfigured medians would also be planted with low-growing groundcover and accent shrubs. This would increase the amount of plantings within medians under both Build Alternatives. In addition, while trees would also be removed from the median located between Stations 64+00 and 68+00, both Build Alternatives would include replacement tree plantings within this median. The primary difference between Build Alternatives 1 and 2 is that the DDI configuration associated with Build Alternative 2 creates slightly more areas within which low-growing groundcover and accent shrubs would be planted north of Ross Drive for a slightly greener view within this portion of the project corridor.

Pedestrian facilities along Mathilda Avenue would be very similar to existing conditions, under both Build Alternatives, and sidewalks would only be slightly shifted to accommodate turn lanes as shown in the *Simulated Views* for KOP 1 and KOP 2. Similarly, under both Build Alternatives, striping would be added to delineate bicycle facilities as shown in the simulations. Both Build Alternatives would have the same layout for bicycle facilities south of Ross Drive and the layouts to the north of Ross Drive would differ slightly due

to the diamond versus DDI configurations. South of Ross Drive, striping would be used to delineate the bike lanes. The existing concrete barrier on the Mathilda Avenue Bridge over US 101 that separates vehicular from pedestrian traffic would be removed. A bike lane would be on both sides of the bridge, separated from traffic only by striping. In addition, the sidewalk along the southbound lanes of the bridge would be removed and only the sidewalk along northbound lanes of the bridge would remain, separated from traffic by the new bike lane. The outermost bridge barrier would be replaced with a new barrier. This would slightly alter views on the bridge by removing the intermediate barrier between roadway travel lanes and sidewalks and using roadway striping in place of the barrier. Avoidance, Minimization, and/or Mitigation Measure, *Implement Aesthetic Treatments on Bridge Barriers, Sound Walls, and Retaining Walls*, would ensure that the aesthetic treatment of any visible barrier surface will be included. Regardless of Build Alternative, bicycle facilities to the north of Ross Drive would have the same visual character that is associated with striping to delineate the bike lanes. Bicycle facilities associated with the project would increase recreational viewer access because bicycle facilities within the existing project corridor are limited.

The SR 237 ramp connections to Mathilda Avenue would also result in small areas of vegetation removal that would be needed for the ramp reconfigurations and these changes are primarily associated with the westbound SR 237 ramps. However, shifting the westbound off-ramp under Build Alternative 1 to follow the current alignment of Moffett Park Drive creates a newly available space for planting in the area where the old ramp segment would be removed. Build Alternative 2, in a similar fashion, would remove the connection of Moffett Park Drive to Mathilda Avenue between Mathilda Avenue and Bordeaux Drive and this area would be planted. Both Build Alternatives would provide bicycle facilities between Mathilda Avenue and Bordeaux Drive, in a very similar connection design. Both Build Alternatives would also connect Moffett Park Drive to Bordeaux Drive, in the same manner, to maintain vehicular access to Mathilda Avenue via Innovation Way. The westbound SR 237 on-ramp would be slightly reconfigured under both Build Alternatives. Build Alternative 1 would have a grassy bioretention area while Build Alternative 2 would provide more room for landscaping, in addition to a smaller, grassy bioretention area.

The diamond versus DDI configurations associated with Build Alternatives 1 and 2, respectively, would result in a similar visual character along Mathilda Avenue. While there would be a visible difference in traffic patterns, both Build Alternatives would have signalized intersections, a similar width, a similar number of lanes, lane striping and directional arrows, bicycle and pedestrian facilities, medians, and roadway signage. This would result in a very similar visual character for both Build Alternatives even though, as described above, Build Alternative 2 would have slightly more planted areas.

Views from SR 237 and US 101 would not be greatly altered by either Build Alternative. Under both Build Alternatives, roadway users on the freeways would quickly pass by the interchanges. At highway speeds, viewers would notice changes resulting from the vegetation removal. Implementation of Avoidance, Minimization, and/or Mitigation Measure, *Restore Highway Planting*, would ensure that infill plantings will be provided to further supplement replacement plantings proposed under the Build Alternatives and create a visually cohesive highway landscape. The eastbound SR 237 on- and off-ramps would not result in visually apparent changes when seen in passing on the freeway because changes would primarily be lane striping occurring further up the ramps, closer to the intersection with Mathilda Avenue. Views from westbound SR 237 would be slightly visible in passing but would be of slightly wider ramp exits and altered lane striping to accommodate an addition off-ramp lane.

From US 101, there would be noticeable visual changes due to hardscape changes associated with ramp reconfiguration, landscape changes associated with vegetation removal, the installation of replacement plantings under both Build Alternatives, and changes resulting from the modification and installation of

safety barriers. As shown in the *Simulated View* for KOP 3 (**Figure 7**), the southbound US 101 off-ramp would be slightly wider and the off-ramp intersection with Mathilda Avenue would be a little more exposed. The wider ramp would slightly increase the amount of visible pavement and make it so that passing traffic on Mathilda Avenue would be a little more visible from this vantage. As shown in the foreground of the simulation, the most notable changes from this vantage would be associated with vegetation removal along the right side of the ramp. Removing the existing mature trees and shrubs and replanting this area with shorter shrubbery would expose and create more direct views of the office building, parking lot, parked cars, and fencing located at 525 Almanor Avenue which, as shown in the simulation, would be visible above the shorter replacement plantings. A limited amount of vegetation would also be removed to the left of the ramp to accommodate the ramp realignment that would be replanted with low-growing groundcovers. In addition, portions of existing vegetation within the ramp loop, not visible within the simulation behind existing vegetation to remain, would be affected by the project. However, most of these areas would be replanted with low-growing groundcovers and shrubs, as part of the project, except for within the clear recovery zone and in the areas that would be converted to bioretention basins. While replacement plantings proposed under the Build Alternatives would aid in improving project aesthetics, implementation of Avoidance, Minimization, and/or Mitigation Measure, *Restore Highway Planting*, would ensure that infill plantings will be provided to further supplement proposed replacement plantings and further improve project aesthetics.

The bioretention basins would not be visible to viewers from the vantage of KOP 3 due to screening from existing and newly planted trees and shrubs, as illustrated by the simulation. The bioretention basins would mostly be seen by roadway users traveling on the US 101 ramps who would see sunken, grassy depressions that would hold water for short periods of time until the water infiltrates or enters the drainage system. Implementation of Avoidance and Minimization Measure *Incorporate Bioretention Basins in Planting Design*, would use design means to blend the bioretention basins with the overall highway planting, thus improving project aesthetics.

Similar visual changes associated with vegetation removal, replacement plantings, and bioretention basins would be seen when traveling on northbound US 101. Reconfiguration of the existing northbound US 101 off-ramp to northbound Mathilda Avenue would occur in the project area that corresponds to the Classified Landscaped Freeway portion of US 101. Replacement plantings would occur in this area. Consequently, views of this section of US 101 would not be greatly affected and the replacement planting would serve to retain Classified Landscaped Freeway designation. In addition, landscaping would be planted where the northbound loop off-ramp is removed, increasing the overall amount of landscaping associated with the interchange. Implementation of Avoidance, Minimization, and/or Mitigation Measure, *Restore Highway Planting*, would ensure that additional plantings will be provided to supplement replacement plantings proposed under the Build Alternatives and create a visually cohesive highway landscape.

The modified outer barrier along the Mathilda Avenue Bridge over US 101 and barriers along the ramps, placed to separate traffic traveling in opposite direction, would be visible from the vantage of KOP 3, as shown in the *Simulated View*. Avoidance, Minimization, and/or Mitigation Measure, *Implement Aesthetic Treatments on Bridge Barriers, Sound Walls, and Retaining Walls*, would ensure that the aesthetic treatment of any visible barrier surface will be included. This would ensure that changes resulting from the outer bridge barrier would not be visually apparent when seen in passing on the freeway because the changes would be consistent with transportation corridor aesthetics. The barrier along the ramp would be hard to seek out and focus upon in passing at fast freeway speeds but would be visible to roadway

users on the ramps as they drive past the barrier. As shown in the simulation, new lane striping on the ramps would be consistent with existing visual conditions and would not stand out.

The sound wall between Weddell Drive and the northbound US 101 off-ramp would be replaced. The new wall would be the same height and would be shifted three feet towards Weddell Drive to accommodate the slightly wider ramp at this location. This would not allow enough space on the Weddell Drive side of the wall to replant the creeping vines that would be removed during construction. Therefore, the bare wall surface would remain visible along this affected segment. While this is a relatively short segment of sound wall, this would negatively affect views seen from multi-family residences located along this portion of Weddell Drive and as seen by pedestrians, recreationists, and roadway users using Weddell Drive and its associated sidewalks. These viewers would now see a stark wall surface, instead of a more pleasing, vegetated wall surface. It would also detract from views seen by roadway users along us 101 and the northbound US 101 off-ramp, although briefly since viewers tend to pass this location quickly. The replaced sound wall would use materials, colors, and texture that improve its aesthetic quality and complement the existing surroundings. Avoidance, Minimization, and/or Mitigation Measure, *Implement Aesthetic Treatments on Bridge Barriers, Sound Walls, and Retaining Walls*, would ensure that aesthetic treatment of the visible sound wall surfaces will be included.

The project would result in a nominal increase in daytime glare by increasing the paved area and by removing some of the mature roadside vegetation that provides shade. However, the pavement would be grey, similar to existing conditions, which would reduce glare, and mature roadside vegetation would remain along the ROW to provide some shade. In addition, while it would take a few years to mature and provide the same level of shading, new highway and street planting would be provided within the project corridor. Therefore, the project would not create a new source of substantial glare that would adversely affect daytime or nighttime views in the area.

Both Build Alternatives propose very similar changes to signalized intersections and street lighting. The Mathilda Avenue intersections with Innovation Way, Moffett Park Drive, SR 237 West, SR 237 East, Ross Drive, and Almanor Avenue; and the Innovation Way intersection with Moffett Park Drive are signalized. Under both Build Alternatives, the signal at Mathilda Avenue and Almanor Avenue would not be affected; the signal at Mathilda Avenue and Moffett Park Drive would be removed; the Mathilda Avenue signals at Innovation Way and Ross Drive and at Innovation Way's intersection with Moffett Park Drive would be modified, including the associated light rail crossing signals and facilities; the Mathilda Avenue signals for westbound and eastbound SR 237 would be removed and new signals would be installed for the relocated ramp entrances; and new traffic signals would be installed at the Mathilda Avenue intersection with northbound and southbound US 101. Signal modification and the overall contribution of one additional signalized intersection compared to existing conditions would result in an inconsequential increase in lighting from signals in an area that is already well-lit. Under both Build Alternatives, the existing overhead cobra street lighting would also need to be modified to accommodate the new, slightly expanded roadway corridor and reconfigured ramps. Lighting would be relocated where the widened corridor would affect existing light posts along the edge of the roadway and ramps and within the median near Moffett Place. In addition, lighting would be enhanced for security and safety purpose increasing the amount of lighting within the corridor. While improving safety, the increased lighting level could negatively affect nearby roadway neighbors if not properly designed. Lights can negatively affect humans by increasing nuisance light and glare, in addition to increasing ambient light glow, if shielding is not provided and blue-rich white light lamps (BRWL) are used (International Dark-Sky Association 2010a, 2010b, 2015). This would result in a substantial source of nighttime light and glare that could adversely affect nighttime views in the area.

Avoidance, Minimization, and/or Mitigation Measure, *Apply Minimum Lighting Standards*, would ensure that adverse effects associate with lighting are reduced.

No-Build Alternative

Under the No-Build Alternative, the project would not be constructed and there would be no visual impacts on the existing visual character, visual quality, or affected viewer groups.

AVOIDANCE, MINIMIZATION, and/or MITIGATION MEASURES

Avoidance, minimization, and/or mitigation measures have been identified and can lessen visual impacts caused by the project. Also, the inclusion of aesthetic features in the project design previously discussed can help generate public acceptance of a project. This section describes additional avoidance, minimization, and/or mitigation measures to address specific visual impacts. These will be designed and implemented with concurrence of the District Landscape Architect.

The following measures to avoid or minimize visual impacts will be incorporated into the project:

- **Implement Aesthetic Treatments on Bridge Barriers, Sound Walls, and Retaining Wall.** The project will incorporate architectural treatment on new bridge barriers, sound walls and the visible side of the retaining wall.
- **Restore Highway Planting.** A restored highway landscape will be provided within the interchanges of S.R 237 and U.S. 101 with Mathilda Avenue. A cohesive highway planting design, including additional plantings in areas not directly impacted by project construction, will ensure that replacement plantings are integrated with the existing landscape to meet community expectations. A plant establishment period of three (3) years will be provided to ensure that new planting matures.
- **Incorporate Bioretention Basins in Planting Design.** The design of bioretention basins will be integrated with the overall highway planting design, using techniques such as landform grading and/ or the incorporation of varied plant materials.
- **Apply Minimum Lighting Standards.** All artificial outdoor lighting and overhead street lighting will be designed to have minimum impact on the surrounding environment. Design measures used to reduce light pollution will use the technologies available at the time of project design to allow for the highest potential reduction in light pollution. Such measures will include the use of down-cast, cut-off type fixtures that are shielded and that direct the minimum necessary light only toward objects requiring illumination.
- **Minimize Fugitive Light from Portable Sources Used for Construction.** At a minimum, the construction contractor shall minimize project-related light and glare to the maximum extent feasible, given safety considerations. Color-corrected halide lights will be used. Portable lights will be operated at the lowest allowable wattage and height and will be raised to a height no greater than 20 feet. All lights will be screened and directed downward toward work activities and away from the night sky and highway users and highway neighbors, particularly residential areas, to the maximum extent possible. The number of nighttime lights used will be minimized to the greatest extent possible.

CONCLUSIONS

Build Alternatives 1 and 2 would result in similar visual impacts. Both Build Alternatives would slightly widen Mathilda Avenue and modify the SR 237 and US 101 interchanges with Mathilda Avenue. Changes and modifications associated with sound walls, barriers, signage, ramp metering, lane striping, utility relocations, lighting, signalization, and bicycle and pedestrian facilities would be very similar under both Build Alternatives. All of these project features are existing corridors elements. Consequently, changes to these elements associated with roadway reconfiguration would not greatly alter the visual character of the project area. Additionally, light and glare affects would likely be minimal. Although mature trees and shrubs would be removed under Build Alternatives 1 and 2, both Build Alternatives would replant medians, roadside locations east and west of Mathilda Avenue, and the areas within the interchanges. Restoring the highway landscape will enhance the proposed replacement planting and minimize visual impacts from the loss of mature vegetation, especially trees and vines that cannot be replaced in their original locations. The restored highway planting can be expected to compensate for vegetation loss within 5 years of installation.

While there would be a visible difference in traffic patterns, the diamond versus DDI configurations associated with Build Alternatives 1 and 2, respectively, would result in a similar visual character along Mathilda Avenue. The primary difference between Build Alternatives 1 and 2 is that the DDI configuration associated with Build Alternative 2 creates slightly more areas within which low-growing groundcover and accent shrubs would be planted north of Ross Drive for a slightly greener view within this portion of the project corridor, compared to Build Alternative 1.

The Avoidance, Minimization, and/or Mitigation Measures would improve the aesthetics of built project features, provide attractive landscaping, reduce the effects of nighttime construction, and reduce light and glare impacts from lighting enhancements. With the incorporation of the specified minimization measures, the proposed Build Alternatives will not have an adverse significant impact.

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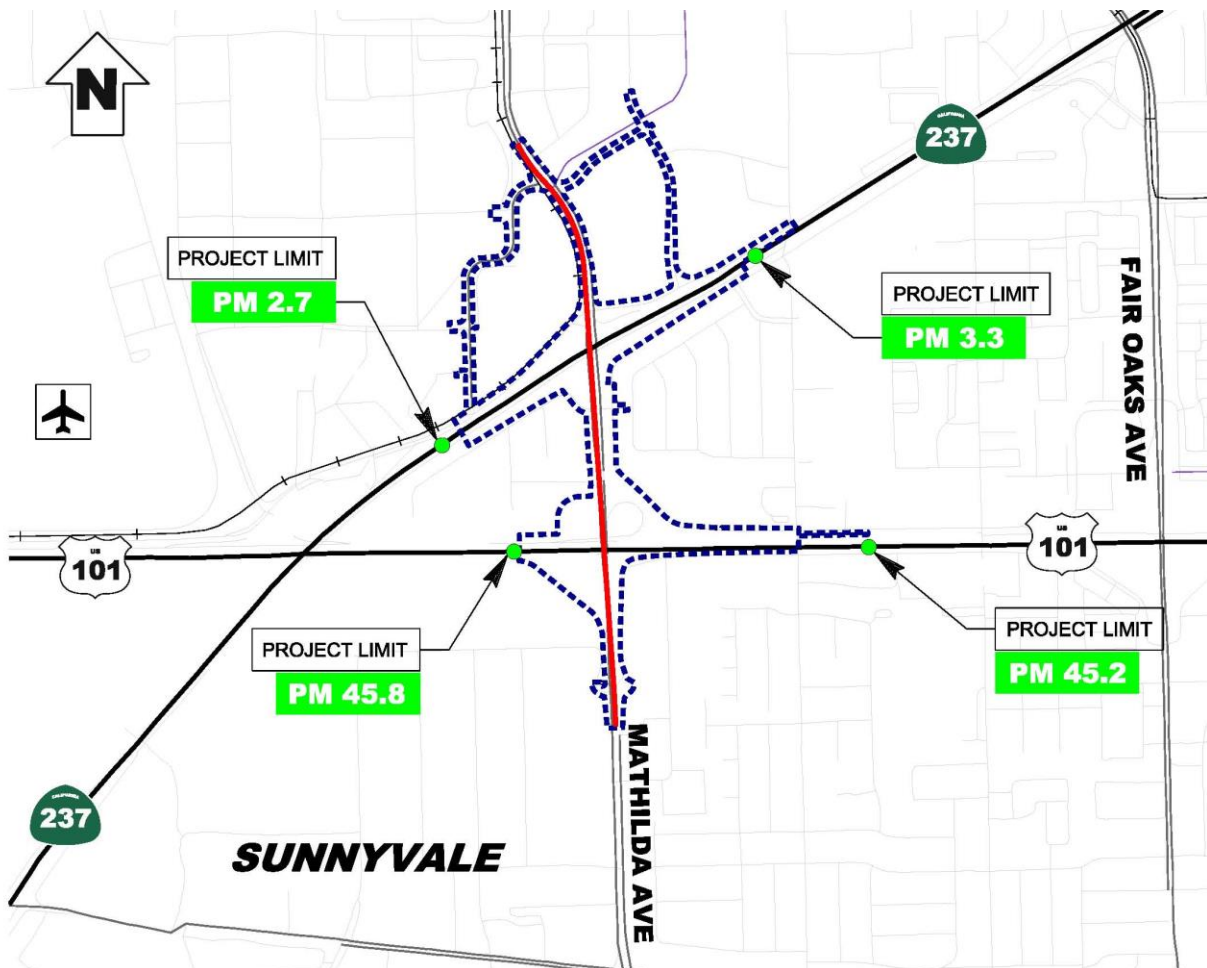
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Water Quality Assessment Report

for the

MATHILDA AVENUE IMPROVEMENTS AT SR 237 AND US 101 PROJECT



Prepared for:

Santa Clara Valley Transportation Authority

California Department of Transportation
District 4

Prepared by:

WRECO

Dated: January 2016

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Executive Summary

The California Department of Transportation (Caltrans), in cooperation with the Santa Clara Valley Transportation Authority (VTA) and the City of Sunnyvale, is proposing the “Mathilda Avenue Improvements at SR 237 and US 101 Project” (Project) to improve Mathilda Avenue in the City of Sunnyvale from Almanor Avenue to Innovation Way, including on- and off-ramp improvements at the State Route (SR) 237/Mathilda Avenue and U.S. Highway 101 (US 101)/Mathilda Avenue interchanges. On SR 237, the Project limits are from 0.3 mile east of the US 101/SR 237 interchange (post mile [PM] 2.7) to 0.3 mile east of the Mathilda Avenue undercrossing (PM 3.3). On US 101, the Project limits are from 0.3 mile south of the Mathilda Avenue overcrossing (PM 45.2) to 0.3 mile south of the SR 237/US 101 interchange (PM 45.8). The total length of the Project on Mathilda Avenue is approximately one mile.

A No-Build Alternative and two Build Alternatives are being considered for the Project. The primary differences between the alternatives relate to construction of a diverging diamond interchange for Build Alternative 2.

The purpose of the Water Quality Assessment Report (Report) is to fulfill the requirements of the California Environmental Quality Act (CEQA), and to provide information, to the extent possible, for National Pollutant Discharge Elimination System (NPDES) permitting. The report examines the potential for any proposed Project activity to result in impacts to water resources or potential increases in sediment load and other pollutants to surface and groundwater.

The Project is within the jurisdiction of the San Francisco Bay Regional Water Quality Control Board. The approximately 3-mile-long Sunnyvale West Channel is the receiving water body. The channel originates at Maude Avenue as a concrete pipe culvert until it reaches Almanor Avenue in the northeastern direction. The channel becomes an earth-excavated channel from Almanor Avenue to Mathilda Avenue. The channel flows northeast to Guadalupe Slough via Moffett Channel, and then ultimately drains to San Francisco Bay. Within the Project limits, the channel crosses SR 237 through a culvert at approximately PM 2.80 near Innovation Way and again at Mathilda Avenue about 100 feet south of Innovation Way.

Sunnyvale West Channel was identified as a non-wetland water of the United States. However, no Project activities will take place within the channel, therefore no federal permits (Section 401 or 404) will be required. No wetlands or other jurisdictional areas were found within the study area.

In compliance with National Pollutant Discharge Elimination System Program (NPDES) Permits for Caltrans (Order No. 2014-0077-DWQ) and the San Francisco Bay Region (Municipal Regional Permit R2-2015-0049), the Project must comply with Clean Water Act Section 402. The Project would be also required to comply with the State Water Resources Control Board Construction General Permit (CGP) (Order No. 2012-0006-DWQ).

Project activities within the City of Sunnyvale right-of-way would result in insignificant amounts of disturbed soil or impervious area (see tables ES-1 and ES-2). Nearly all of the disturbed soil area (DSA) would be within Caltrans right-of-way. Both Build Alternatives would have a DSA of more than one acre and would add and reworked impervious surface areas. Therefore, the Project would have the potential to cause water quality impacts to Sunnyvale West Channel. To address short-term and long-term water

quality impacts, the Project would implement Caltrans-approved best management practices (BMPs) to avoid and minimize temporary construction impacts and permanent operational impacts.

Table ES-1. Disturbed Soil, Existing and Added Impervious and Reworked Areas for Build Alternative 1

| Right-of-Way | Disturbed Soil Area (acre) | Existing Impervious Area (acre) | Added Impervious Area (acre) | Reworked Impervious Area (acre) | Added and Reworked Impervious Area (acre) |
|-------------------|----------------------------|---------------------------------|------------------------------|---------------------------------|---|
| Caltrans | 20 | 45.5 | 2 | 4 | 6 |
| City of Sunnyvale | 0.011 | 4.5 | 0.01 | 0.001 | 0.011 |
| | | | | | |
| Total | 20.011 | 50 | 2.01 | 4.001 | 6.011 |

Source: WMH

Table ES-2. Disturbed Soil, Existing and Added Impervious and Reworked Areas for Build Alternative 2

| Right-of-Way | Disturbed Soil Area (acre) | Existing Impervious Area (acre) | Added Impervious Area (acre) | Reworked Impervious Area (acre) | Added and Reworked Impervious Area (acre) |
|-------------------|----------------------------|---------------------------------|------------------------------|---------------------------------|---|
| Caltrans | 22 | 45.5 | 3 | 5 | 8 |
| City of Sunnyvale | 0.011 | 4.5 | 0.01 | 0.001 | 0.011 |
| | | | | | |
| Total | 22.011 | 50 | 3.01 | 5.001 | 8.011 |

The CGP requires determination of a project risk level to establish the applicable monitoring and sampling requirements during construction. A Storm Water Pollution Prevention Plan (SWPPP) is required for all risk levels. The calculated R factor for this Project is 35, the weighted average K factor within the Project area is 0.28, and the LS factor within the Project area is 0.36. The product of these values is 3.53; the Project would be classified as having a low sediment risk. The Project also has a low receiving water risk; therefore, the Project would be classified as Risk Level 1 under the CGP.

The Project would not include work in Sunnyvale West Channel. Nevertheless, the Project would add impervious area and, therefore, could potentially increase the volume and velocity of stormwater flow to the downstream receiving water body. The goal of the Project drainage design would be to maintain the existing drainage patterns; however, the amount of runoff from the added impervious area may result in minimal impacts to the existing hydrograph (including minimal increases in low and peak flow velocity and volume). However, the Project is located in an area where the catchment drains to a hardened channel and/or tidal areas, so hydromodification management (HM) is not required per the Santa Clara Valley Urban Runoff Pollution Prevention Program (SCVURPPP) *C.3 Stormwater Handbook* and *SCVURPPP Hydromodification Plan*.

Any stormwater impacts would be addressed through proper implementation of approved design, pollution prevention, and permanent treatment BMPs. High groundwater at the Project site may affect the choice of treatment BMPs and may require dewatering during construction. Due to potential shallow groundwater and soil type (hydrologic soil group C), biofiltration swales are anticipated to be

the preferred BMP and infiltration may not be practical. Treatment BMPs will be further evaluated in the PS&E phase when further hydrologic and geologic field work is conducted.

The general approach of the Project would be to avoid or minimize impacts and to implement measures for any unavoidable impacts. This Project would have minimal impacts to water quality if the avoidance and minimization measures in compliance with the applicable NPDES permits are incorporated. Because the Project would meet water quality goals, incorporate other applicable NPDES permit requirements, and comply with Project-specific permit or agreement requirements, the Project is expected to have a less-than-significant impact on water resources.

Acronyms

| | |
|----------|--|
| ADA | Americans with Disabilities Act |
| ASBS | Areas of Special Biological Significance |
| BFE | base flood elevation |
| bgs | below ground surface |
| BMP | best management practices |
| Caltrans | California Department of Transportation |
| CFR | Code of Federal Regulations |
| CGP | Construction General Permit |
| CEQA | California Environmental Quality Act |
| CPUC | California Public Utilities Commission |
| CWA | Clean Water Act |
| DCD | double crossover diamond interchange |
| DDI | diverging diamond interchange |
| DSA | disturbed soil area |
| DWQ | Division of Water Quality |
| EB | eastbound |
| EPA | U.S. Environmental Protection Agency |
| FEMA | Federal Emergency Management Agency |
| FHWA | Federal Highway Administration |
| FIRM | Flood Insurance Rate Map |
| FIS | Flood Insurance Study |
| GO | General Order |
| HMP | Hydromodification Management Plan |
| HSA | hydrologic sub-area |
| I- | Interstate |
| LID | low impact development |
| LRT | Light Rail Transit |
| LUST | Leaking Underground Storage Tank |
| MS4 | Municipal Separate Storm Sewer System |
| NB | northbound |
| NOAA | National Oceanic and Atmospheric Administration |
| NOP | Notice of Preparation |
| NPDES | National Pollutant Discharge Elimination System |
| NRCS | Natural Resources Conservation Service |
| PA/ED | Project Approval/Environmental Document |
| PG&E | Pacific Gas & Electric |
| PM | Post Mile |
| POTW | Publicly Owned Treatment Works |
| PPDG | <i>Project Planning and Design Guide</i> |
| PS&E | Plans, Specifications, and Estimates |
| RWQCB | Regional Water Quality Control Board |
| SB | southbound |
| SCVURPPP | Santa Clara Valley Urban Runoff Pollution Prevention Program |
| SFPUC | San Francisco Public Utilities Commission |
| SMARTS | Storm Water Multiple Application and Report Tracking System |

| | |
|-------|---------------------------------------|
| SR | State Route |
| SWMP | Storm Water Management Plan |
| SWPPP | Storm Water Pollution Prevention Plan |
| SWRCB | State Water Resources Control Board |
| TMDL | total maximum daily load |
| TDM | Transportation Demand Management |
| TSM | Transportation System Management |
| USACE | U.S. Army Corps of Engineers |
| VTA | Valley Transportation Authority |
| WDR | Waste Discharge Requirement |
| WB | westbound |
| WPCP | Water Pollution Control Program |

1 INTRODUCTION

The California Department of Transportation (Caltrans), in cooperation with the Santa Clara Valley Transportation Authority (VTA) and the City of Sunnyvale, is proposing the “Mathilda Avenue Improvements at SR 237 and US 101 Project” (Project) to improve Mathilda Avenue in the City of Sunnyvale from Almanor Avenue to Innovation Way, including on- and off-ramp improvements at the State Route (SR) 237/Mathilda Avenue and U.S. Highway 101 (US 101)/Mathilda Avenue interchanges. On SR 237, the Project limits are from 0.3 mile east of the US 101/SR 237 interchange (post mile [PM] 2.7) to 0.3 mile east of the Mathilda Avenue undercrossing (PM 3.3). On US 101, the Project limits are from 0.3 mile south of the Mathilda Avenue overcrossing (PM 45.2) to 0.3 mile south of the SR 237/US 101 interchange (PM 45.8). The total length of the Project on Mathilda Avenue is approximately one mile. Figure 1 shows the location of the Project, and Figure 2 shows the vicinity of the Project.

1.1 Purpose and Need

The primary purpose of the Project is to improve traffic operations on Mathilda Avenue through the US 101 and SR 237 interchanges. Specifically, the goals and objectives of the Project are to:

- Reduce congestion and improve traffic operations along Mathilda Avenue and at the SR 237/Mathilda Avenue and US 101/Mathilda Avenue interchanges.
- Improve mobility for all travel modes in the area including motor vehicles, transit, bicycles, and pedestrians.
- Provide standard crosswalks and sidewalks along Mathilda Avenue, improving access to local destinations such as Moffett Park, the VTA Light Rail Transit (LRT) stations, and downtown Sunnyvale.

The Project is needed for the following reasons:

- Regional growth and new local development combined with inefficient roadway operations has resulted in substantial traffic congestion on Mathilda Avenue.
- Efficient access for all travel modes into and out of downtown Sunnyvale and development to the north of SR 237 is critical to a healthy and sustainable economy. Congestion on Mathilda Avenue adversely affects the economic vitality of the City of Sunnyvale.

Overall, the Project is needed to address several issues in the Project area including roadway deficiencies, lack of or discontinuous bicycle and pedestrian access, improvement of local roadway and freeway ramp operations, and provision of access to current and future economic development.

1.2 Project Description and Alternatives

The Project alternatives that were developed to meet the purpose and need of the Project include Build Alternative 1, Build Alternative 2, and the No-Build Alternative (refer to Figure 3 and Figure 4). Under the No-Build Alternative, no changes would be made to the existing local roadways or freeway system within the Project limits. No construction activities would occur, and there would be no change in the operations of the existing facilities.

The design features of the two Build Alternatives include reconfiguration of the US 101 and SR 237 interchanges with Mathilda Avenue. The Build Alternatives include design variations for reconfigured roadways and intersections, and construction of new signalized intersections. Proposed improvements included in the Build Alternatives south of Ross Drive on Mathilda Avenue and at the US 101

interchange, are identical. This includes new bicycle and pedestrian facilities, utility relocations, new stormwater treatment facilities, new safety lighting, ramp metering modifications, modification of overhead signage, and a new retaining wall. Unique improvements, north of Ross Drive on Mathilda Avenue, primarily include improvements related to construction of a diverging diamond interchange (DDI)¹ under Build Alternative 2 (Figure 4).

Roadway Improvements

The Build Alternatives would consist of the following roadway improvements:

- Provide three continuous through lanes in each direction of Mathilda Avenue
- Remove northbound US 101 loop off-ramp and shift traffic to northbound US 101 diagonal off-ramp
- Realign and widen northbound ramps and signalize ramp intersection with Mathilda Avenue, and construct left-turn lane on southbound Mathilda Avenue to access northbound US 101 loop on-ramp
- Realign southbound US 101 off-ramp and loop on-ramp and signalize ramp intersection with Mathilda Avenue
- Modify Mathilda Avenue/Ross Drive signal intersection
- Close Moffett Park Drive between Bordeaux Drive and Mathilda Avenue, replace with a Class I bikeway (as described below), and shift traffic to Bordeaux Drive and Innovation Way.²
- Remove westbound SR 237 ramp signal intersection. Realign westbound SR 237 off-ramp opposite Moffett Park Drive and modify signal intersection
- Build Alternative 1 would modify westbound SR 237 ramps to provide a diamond configuration (see Figure 3)
- Build Alternative 2 would modify Mathilda Avenue and SR 237 ramps to provide a diverging diamond configuration (see Figure 4). Eastbound Moffett Park Drive between Innovation Way and Mathilda Way would be diverted to Innovation Way to access Mathilda Avenue

Bicycle and Pedestrian Facilities

Enhanced bicycle and pedestrian facilities would be provided. Bicycle improvements on Mathilda Avenue would consider both Class II and Class III bikeways³, based on available pavement widths within the project limits, and would connect to the existing Class III bikeway north of Innovation Way and Class I bikeway on the Sunnyvale West Channel. Bicycle improvements on Moffett Park Drive would consist of a Class I bikeway between Bordeaux Drive and Mathilda Avenue. Between Mathilda Avenue and Innovation Way, Class II and Class III bikeways would be considered based on available pavement widths within the project limits. A continuous sidewalk would be provided on the east side of Mathilda Avenue

¹ A diverging diamond interchange (DDI), also called a double crossover diamond interchange (DCD), is a type of diamond interchange where traffic briefly crosses over to the left (opposite) side of the roadway, guided by traffic signals at each crossover. This allows vehicles to turn left onto freeway on-ramps without stopping and without conflicting with through traffic. The signals at ramp terminal intersections can be operated with two signal phases (a signal phase allows for traffic at an intersection to cycle through specific movements for each direction) instead of three.

² Innovation Way would be extended from Mathilda Avenue to Bordeaux Drive by the Moffett Place development project.

³ Class I bikeway is a bicycle path. Class II bikeway is a bicycle lane. Class III bikeway is bicycle route [Source: Highway Design Manual Index 1002.1]

within the project limits with crosswalks, curb ramps, and pedestrian countdown signals at each intersection. The new crosswalks at the reconfigured ramp intersections would be signalized.

1.3 Approach to Water Quality Assessment

The purpose of the Water Quality Assessment Report (Report) is to fulfill the requirements of the California Environmental Quality Act (CEQA), and to provide information, to the extent possible, for National Pollutant Discharge Elimination System (NPDES) permitting. The document includes a discussion of the proposed Project, the regulatory framework, and physical setting of the Project area with respect to water quality. It also provides data on surface water and groundwater resources within the Project area and the quality of these waters, describes water quality impairments and beneficial uses, identifies potential water quality impacts/benefits associated with the Project, and recommends avoidance and/or minimization measures for potentially adverse impacts.

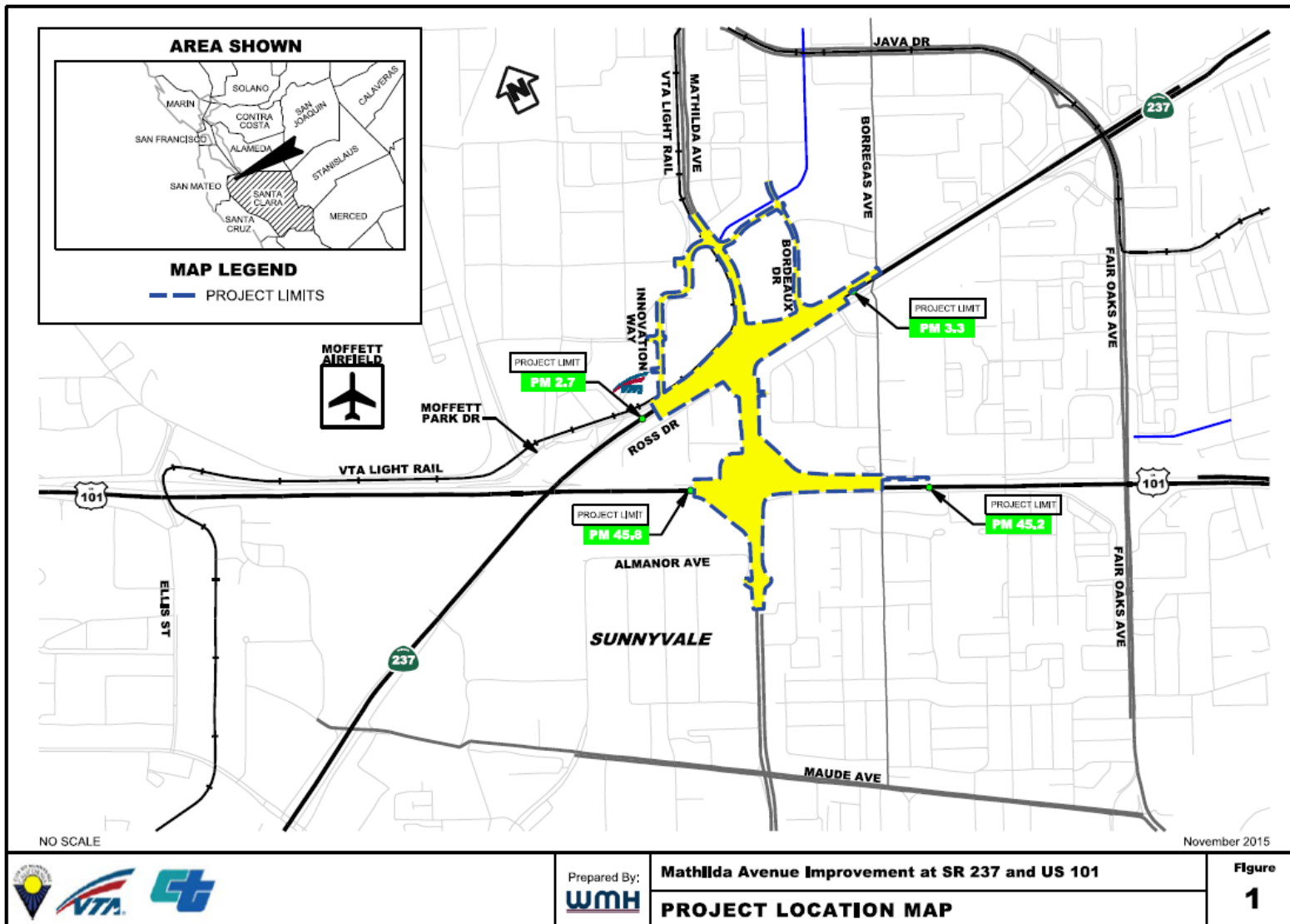


Figure 1. Project Location Map

Source: WMH Corporation

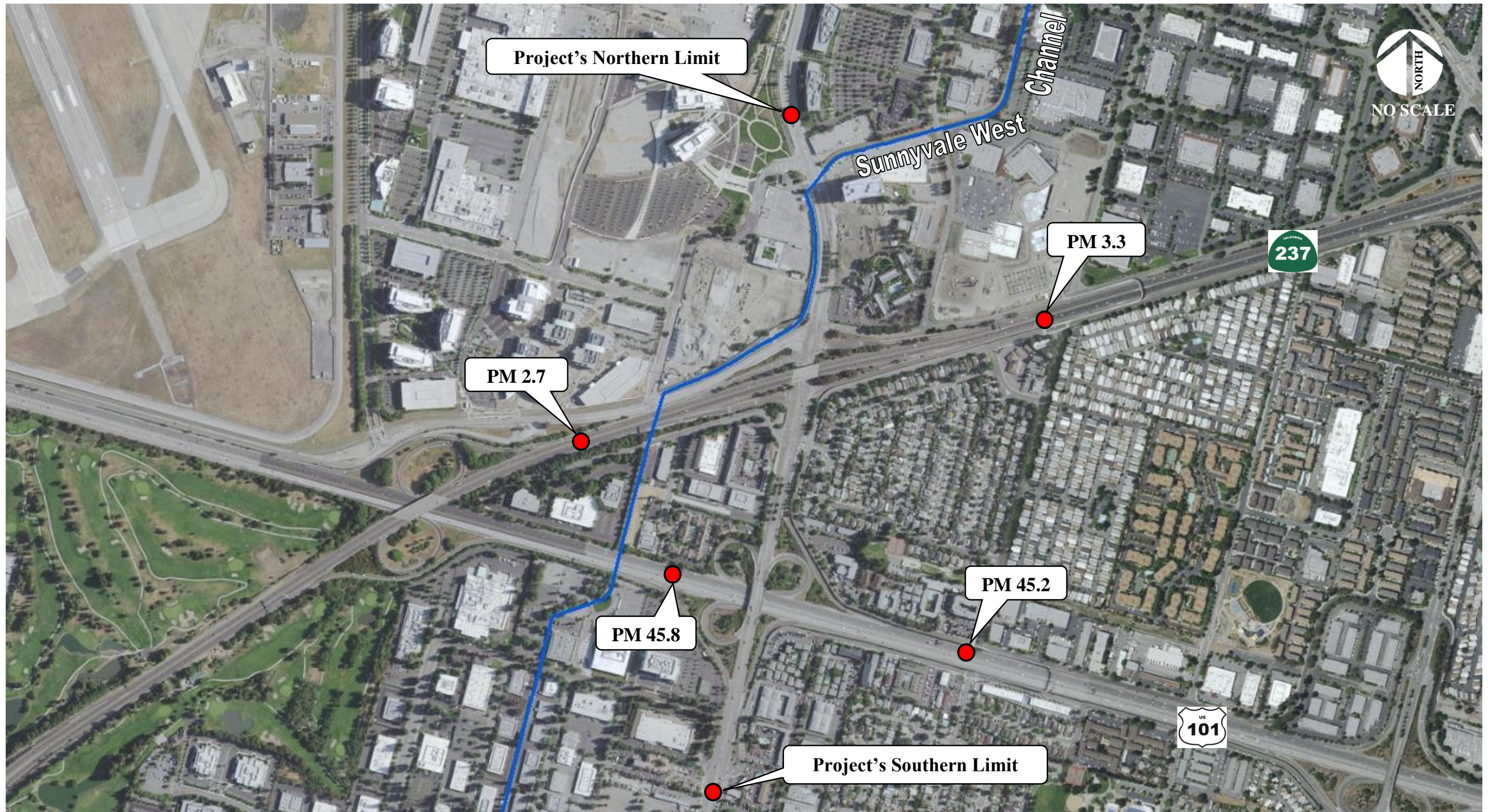


Figure 2. Project Vicinity Map

Source: Caltrans, Environmental System Research Institute (ESRI) and Santa Clara Valley Water District

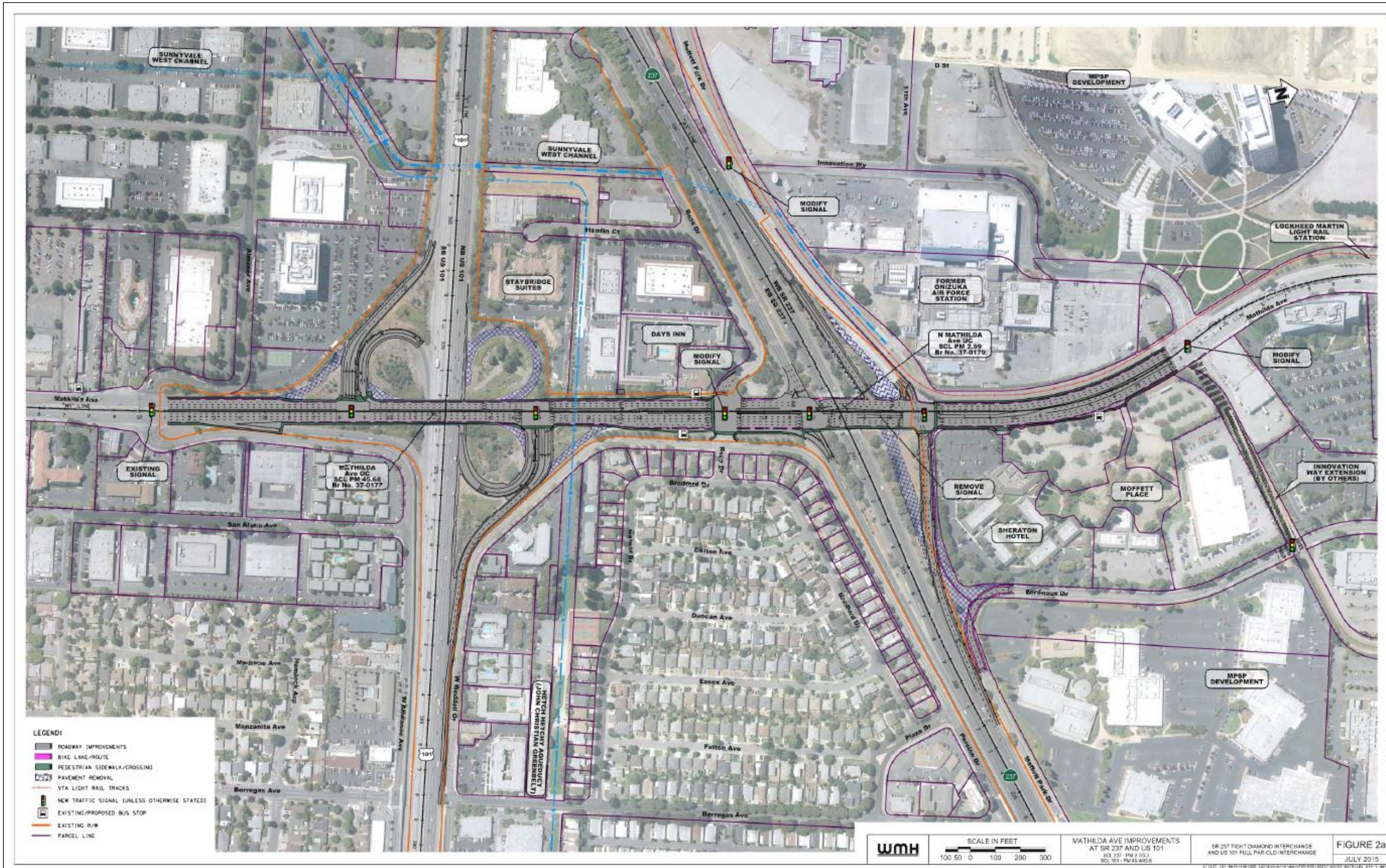


Figure 3. Build Alternative 1

Source: WMH Corporation

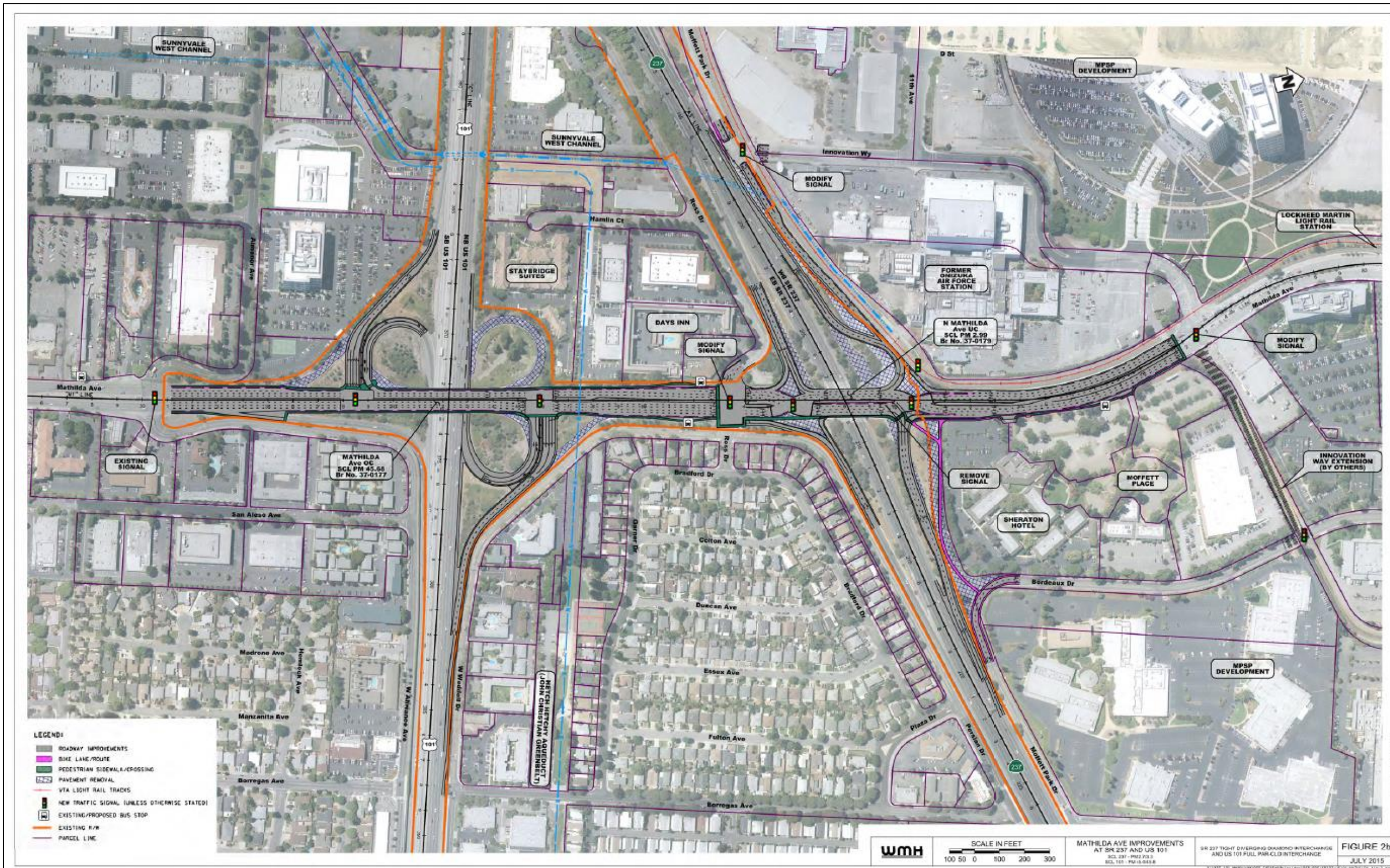


Figure 4. Build Alternative 2

Source: WMH Corporation

2 REGULATORY SECTION

This section summarizes the regulatory requirements associated with the issues of water quality that are mandated at federal, state, and local levels.

2.1 Federal Laws and Requirements

The Clean Water Act (CWA) regulates the quality of surface and groundwater at the federal level. The objective of the CWA is “to restore and maintain the chemical, physical, and biological integrity of the Nation’s waters.” Details of the CWA are discussed below.

2.1.1 Clean Water Act

In 1972 Congress amended the Federal Water Pollution Control Act, making the addition of pollutants to the waters of the U.S. from any point source unlawful unless the discharge is in compliance with an NPDES permit. Known today as the Clean Water Act (CWA), Congress has amended it several times. In the 1987 amendments, Congress directed dischargers of stormwater from municipal and industrial/construction point sources to comply with the NPDES permit scheme. Important CWA sections are:

- Sections 303 and 304 require states to promulgate water quality standards, criteria, and guidelines.
- Section 401 requires that an applicant for a federal license or permit for any activity potentially resulting in a discharge to waters of the U.S. must obtain certification from the State that the discharge will comply with other provisions of the act. It is most frequently required in tandem with a Section 404 permit request.
- Section 402 establishes the NPDES, a permitting system for the discharges (except for dredge or fill material) of any pollutant into waters of the U.S. Each Regional Water Quality Control Boards (RWQCB) administer this permitting program in California. Section 402(p) requires permits for discharges of stormwater from industrial/construction and Municipal Separate Storm Sewer Systems (MS4s).
- Section 404 establishes a permit program for the discharge of dredge or fill material into waters of the U.S. This permit program is administered by the U.S. Army Corps of Engineers (USACE).

Sunnyvale West Channel, the Project receiving water body, has been designated as a non-wetland water of the United States (Section 3.1.5). Because no Project activities will take place within the channel, no federal permits (Section 401 or 404) will be required. In compliance with the Caltrans and City NPDES Permits (Section 2.2.1), the Project must comply with Section 402.

2.1.2 National Pollutant Discharge Elimination System Program

2.1.2.1 Municipal Separate Storm Sewer Systems (MS4)

Section 402(p) of the CWA requires the issuance of NPDES permits for five categories of stormwater dischargers, including MS4s. The U.S. EPA defines an MS4 as “any conveyance or system of conveyances (roads with drainage systems, municipal streets, catch basins, curbs, gutters, ditches, human-made channels, and storm drains) owned or operated by a state, city, town, county, or other public body having jurisdiction over stormwater, that are designed or used for collecting or conveying stormwater.” The SWRCB has identified Caltrans as an owner/operator of an MS4 pursuant to federal regulations. Caltrans’ MS4 permit covers all Caltrans rights-of-way, properties, facilities, and activities in the State. The SWRCB or the RWQCB

issues NPDES permits for five years, and permit requirements remain active until a new permit has been adopted.

Caltrans' MS4 Permit (Order No. 2014-0077-DWQ), which became effective in July 2014, applies to projects that did not complete their Project Initiation Design (PID) phase before July 1, 2013. This permit applies to the Project because the Project did not complete the PID phase prior to this date. It contains three basic requirements:

- Compliance with the requirements of the Construction General Permit (CGP; see Section 2.1.2.2)
- Implementation of a year-round program in all parts of the State to effectively control stormwater and non-stormwater discharges; and
- Stormwater discharges must meet water quality standards through implementation of permanent and temporary (construction) best management practices (BMPs) to the maximum extent practicable, and other measures as the SWRCB determines to be necessary to meet water quality standards.

To comply with the permit, Caltrans developed the Statewide Stormwater Management Plan (SWMP) to address stormwater pollution controls related to highway planning, design, construction, and maintenance activities throughout California. The SWMP assigns responsibilities within Caltrans for implementing stormwater management procedures and practices as well as training, public education and participation, monitoring and research, program evaluation, and reporting activities. The SWMP describes the minimum procedures and practices that Caltrans uses to reduce pollutants in stormwater and non-stormwater discharges. It outlines procedures and responsibilities for protecting water quality, including the selection and implementation of BMPs. The Project would be required to follow the guidelines and procedures outlined in the SWMP (May 2003, revised July 2012) to address stormwater runoff.

The Project is in a high trash-generating area and will consider appropriate trash capture BMPs in the PS&E phase. The Permit requires timely implementation of controls in all high trash-generating areas for the prohibition of discharge of trash and include the following:

- Implementation of full capture systems, treatment controls, and/or enhanced maintenance controls for storm drains or catchment that service the significant trash generating areas.
- Coordinate with neighboring MS4 permittees to construct, operate and maintain those controls listed above.
- Assess for the effectiveness of enhanced maintenance controls implemented in high generating trash areas, as well as coordination with local municipalities.
- Abate trash from construction and reconstruction projects.
- Include trash capture devices on the outlets of treatment systems for new and redeveloped highway projects to achieve the full trash capture standard.

2.1.2.2 Construction General Permit

The Construction General Permit (CGP) (Order No. 2012-0006-DWQ) became effective on July 17, 2012. The CGP regulates stormwater discharges from construction sites that result in a disturbed soil area (DSA) of one acre or greater, and/or are smaller sites that are part of a larger common plan of development. For all

projects subject to the CGP, applicants are required to develop and implement an effective Stormwater Pollution Prevention Plan (SWPPP). This Project is subject to the CGP.

By law, all construction activity (e.g. clearing, grading, and excavation) that results in soil disturbance of at least one acre is subject to the provisions of the CGP. Operators of regulated construction sites are required to develop SWPPPs; implement sediment, erosion, and pollution prevention control measures; and obtain coverage under the CGP.

The CGP separates projects into risk levels 1, 2, or 3. Risk levels are determined during the planning and design phases and are based on potential erosion and transport to receiving waters. Requirements apply according to the risk level determined. For example, a Risk Level 3 (highest risk) project would require compulsory stormwater runoff pH and turbidity monitoring, and pre- and post-construction aquatic biological assessments during specified seasonal windows. The Project is risk level 1 (see Section 5.1.1)

2.2 Regional and Local Requirements

2.2.1 San Francisco Bay RWQCB Basin Plan

The Project is under the jurisdiction of the San Francisco Bay RWQCB. The RWQCB implements the San Francisco Bay Basin Water Quality Control Plan (Basin Plan; 2015) to regulate surface and groundwater quality in the region. The Basin Plan lists beneficial uses and water quality objectives to protect those uses.

2.2.2 Municipal Separate Storm Sewer Systems (MS4s)

Almost all of the DSA resulting from the Project would be within Caltrans right-of-way, but would include some restriping and signal work on City of Sunnyvale streets. Runoff from the Project would discharge to Caltrans' and the City of Sunnyvale's drainage systems.

The City of Sunnyvale is a member of the Santa Clara Valley Urban Runoff Pollution Prevention Program (SCVURPPP), an association of 15 agencies in Santa Clara Valley that are part of a region-wide permit to discharge stormwater to local waterways and the San Francisco Bay. The Municipal Regional Stormwater NPDES Permit (R2-2015-0049) was first issued in 1990 and has been reissued four times (1995, 2001, 2009 and 2015). According to the SCVURPPP C.3 Stormwater Handbook (April 2012), hydromodification management (HM) is not required (see Section 2.2.3 for details).

The City of Sunnyvale has prepared a *Long-Term Trash Load Reduction Plan and Assessment Strategy* (2014) in compliance with the NPDES permit. The Project will evaluate appropriate trash reduction and capture BMPs during the PS&E phase.

2.2.3 Hydromodification Management Requirements

According to the SCVURPPP C.3 *Stormwater Handbook* (April 2012) and SCVURPPP Hydromodification Plan (April 2005), the Project is in a catchment draining to hardened channel and/or tidal areas, so HM is not required (see Figure 5).

The project is subject to Caltrans' NPDES Permit (Order No 2014-0077-DWQ). Therefore, treatment and hydromodification controls would be required based on the amount of added and reworked impervious areas in Caltrans' right-of-way. Caltrans may propose, subject to Caltrans Headquarters' approval, that no

hydromodification controls would be necessary for this Project because none is required under local regulations.

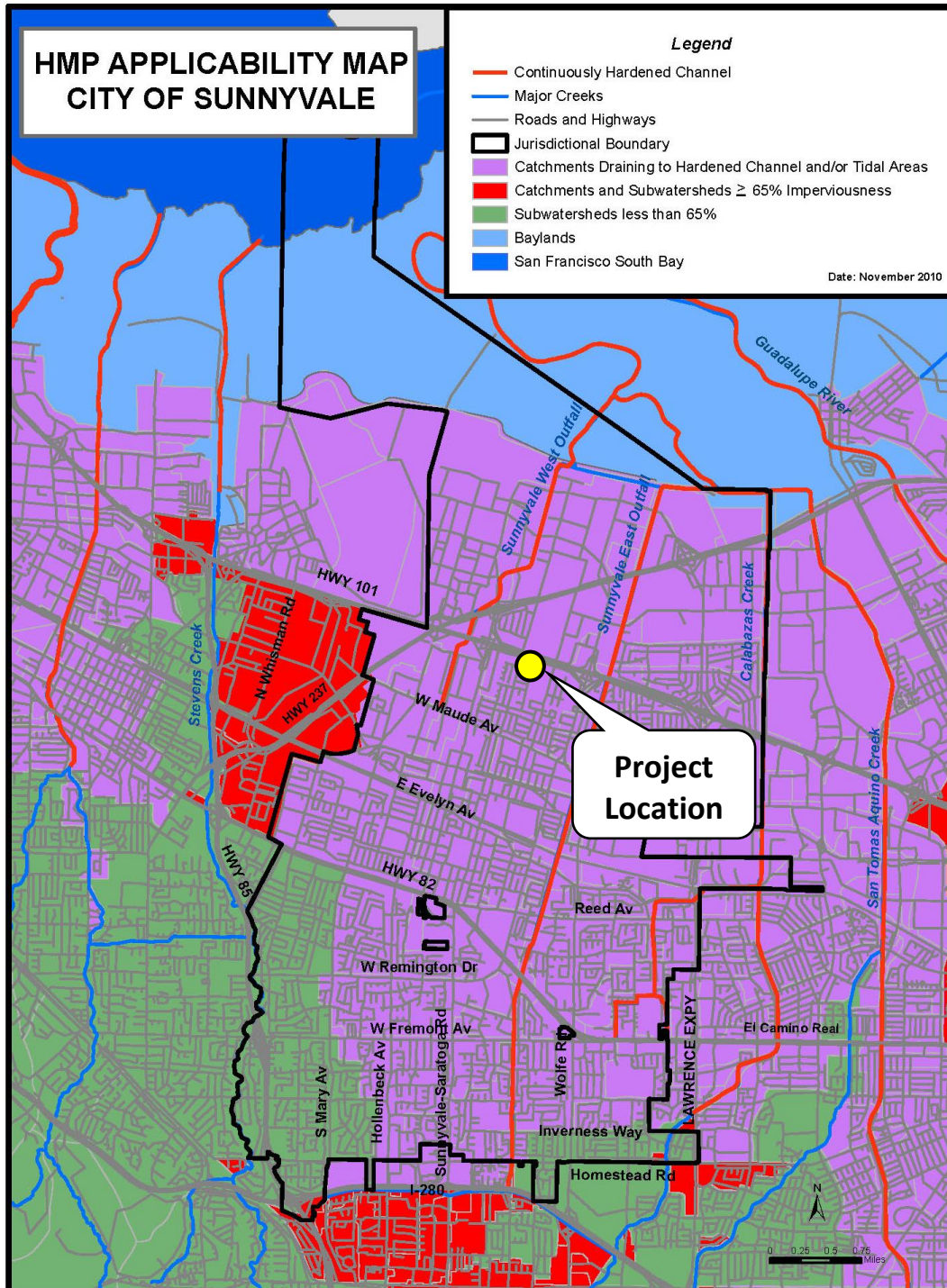


Figure 5. Hydromodification Applicability Map for the City of Sunnyvale

Source: SCVURPPP

3 AFFECTED ENVIRONMENT/EXISTING CONDITIONS

This section describes the physical setting of the Project area. The Project limits cover approximately one mile along Mathilda Avenue between US 101 and SR 237 in the City of Sunnyvale.

3.1 General Setting

3.1.1 Population and Land Use

The *2010 Census Data for the City of Sunnyvale* shows that the City of Sunnyvale had a population of 140,081. By 2025, Sunnyvale is expected to have a population of 150,600, according to the *General Plan (City of Sunnyvale 2011)*. The largest groups of employers include professional, scientific and management, and administrative and waste management services. Several technology companies including Yahoo! Inc., Network Appliance, Inc., and Juniper Networks have headquarters in Sunnyvale. Residential areas comprised about half (52%) of the City's land use in 2011, according to the Consolidated General Plan (City of Sunnyvale 2011), followed by Industrial/Office (26%). The City has about 8% open space, excluding the Baylands. The Baylands—consisting of landfill hills, treatment ponds, salt ponds, recreational trails, and parks—border Sunnyvale at the southwest corner of San Francisco Bay.

Mathilda Avenue is a main thoroughfare in the City. Industry and hotels surround the Project area except to the west and southwest, which are residential (see Figure 3 and Figure 4).

3.1.2 Topography

The Federal Emergency Agency (FEMA) Flood Insurance Study (FIS, No. 06085CV002B) for Santa Clara County (FEMA 2014) states that Santa Clara County is primarily in a flat alluvial plain that lies between the Santa Cruz Mountains and the Diablo Range. Most of the area consists of basically level terrain; toward the east and west, this gives way to rolling foothills. These foothill areas, in turn, become steeper and graduate into the mountain ranges that flank the City of Gilroy. The land slopes toward the south.

Based on the Project's topographic drawings, the elevation of SR 237 within the Project limits drops from approximately 35 feet in the northeast to 21 feet in the southwest. The elevation of US 101 in the Project area is flat with an elevation range of 32 to 34 feet.

3.1.3 Hydrology

3.1.3.1 Regional Hydrology

The Project area is located within the Sunnyvale West Watershed (Figure 6). The watershed sits on the alluvial plain of the Santa Clara Valley. It drains 7.6 square miles and is almost entirely urbanized.

Precipitation and Climate

The climate of the City of Sunnyvale is characterized by warm, dry summers and cool, moist winters. According to the *Community Fact Sheet for Sunnyvale* (City of Sunnyvale 2015), temperature averages range from 58°F in January to 78°F in July. Average annual rainfall is 11.85 inches. Violent thunderstorms, snowfall, and other extreme weather conditions are rare.

Surface Streams

The Project would drain to Sunnyvale West Channel. Within the Project limits, the channel crosses SR 237 through a culvert at approximately PM 2.80 near Innovation Way and again at Mathilda Avenue about 100 feet south of Innovation Way. The channel was built in 1964 to alleviate flooding in the watershed. Runoff from the Project is expected to be collected by Caltrans' and the City's drainage systems, which eventually drain to the channel.

The Sunnyvale West Channel is the receiving water body, and it is approximately 3 miles in length. The channel originates at Maude Avenue as a concrete pipe culvert until it reaches Almanor Avenue in the northeastern direction. The channel becomes an earth-excavated channel from Almanor Avenue to Mathilda Avenue. The channel flows northeast to Guadalupe Slough via the Moffett Channel, and then ultimately drains to San Francisco Bay. Figure 6 and Figure 7 show waterways near the Project.

Floodplains

FEMA issues the Flood Insurance Rate Maps (FIRMs) that delineate flood hazard zones. The 1% annual chance flood and floodplain have been adopted as a common design and regulatory standard in the United States.

The *Floodplain Encroachment Technical Memorandum* (WRECO 2015a) prepared for the Project describes the floodplain characteristics in detail and describes potential impacts and whether avoidance, minimization or mitigation measures would be needed. The FIRM for the Project is Map Number 06085C0045H, shown in Figure 8 (FEMA 2009).

A Zone AE floodplain area is associated with Sunnyvale West Channel. The description of Zone AE in the Project vicinity is "1% annual chance flood discharge contained in channel." The northern limit of the Project would extend into Zone AE; however, no major construction is anticipated to occur in that area. Signal modifications, restriping, and/or other minor improvements may be performed.

The FIRM identifies SR 237, US 101, and Mathilda Avenue in the Project limits as being within areas classified as shaded Zone X. The description of shaded Zone X in this FIRM is "areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood."

Municipal Supply

The water supply system in Santa Clara County includes surface sources (reservoirs, creeks and others) and groundwater found in aquifers. The City of Sunnyvale obtains its drinking water from eight local groundwater wells, as well as from imported water from the Santa Clara Valley Water District, Hetch Hetchy, and Sunol Valley water supply from the San Francisco Public Utilities Commission (SFPUC).

There are no drinking water reservoirs or recharge facilities within the Project limits. There are no reservoirs in the Sunnyvale West Channel watershed.

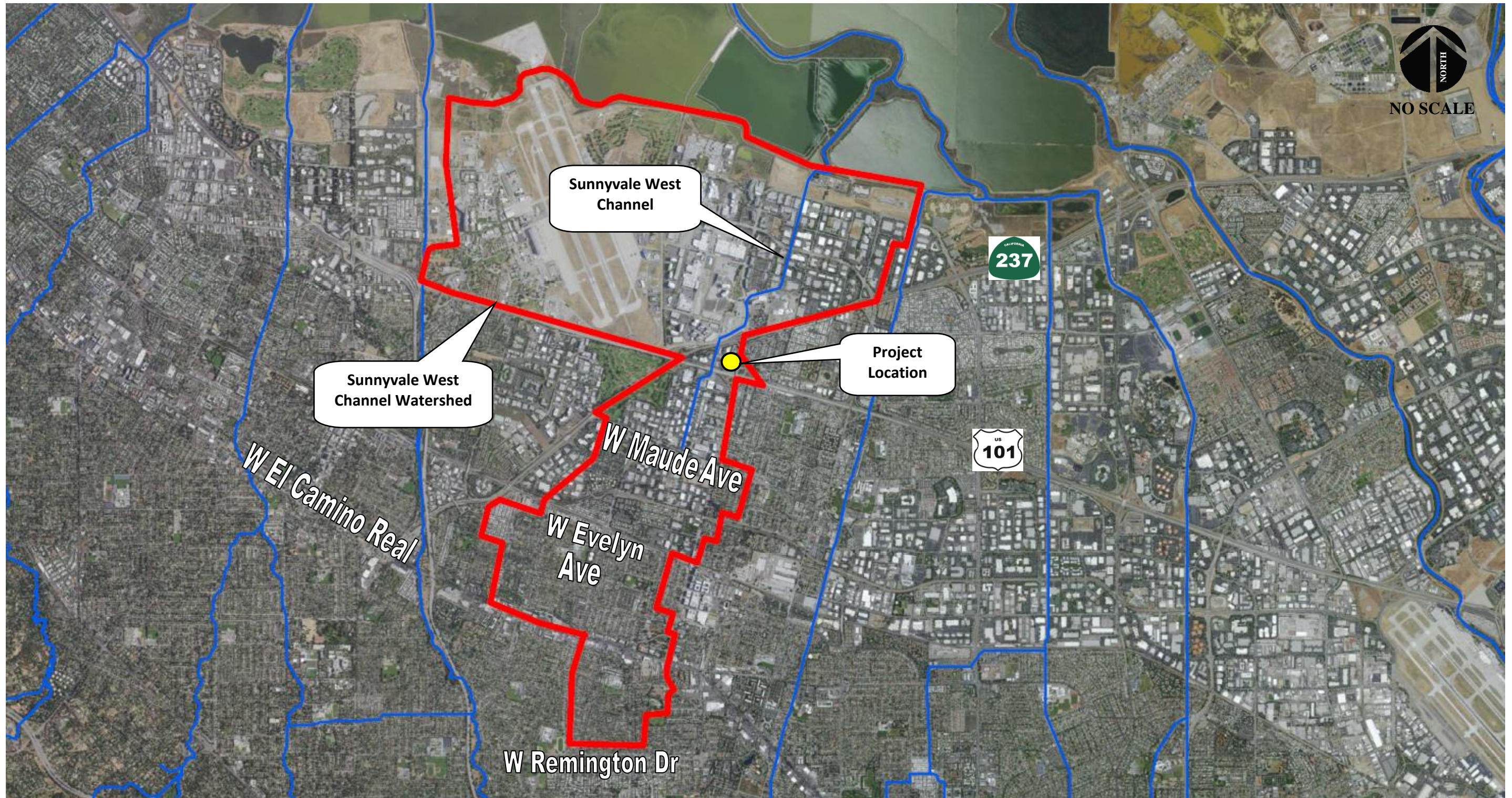


Figure 6. Sunnyvale West Watershed

Source: Santa Clara County

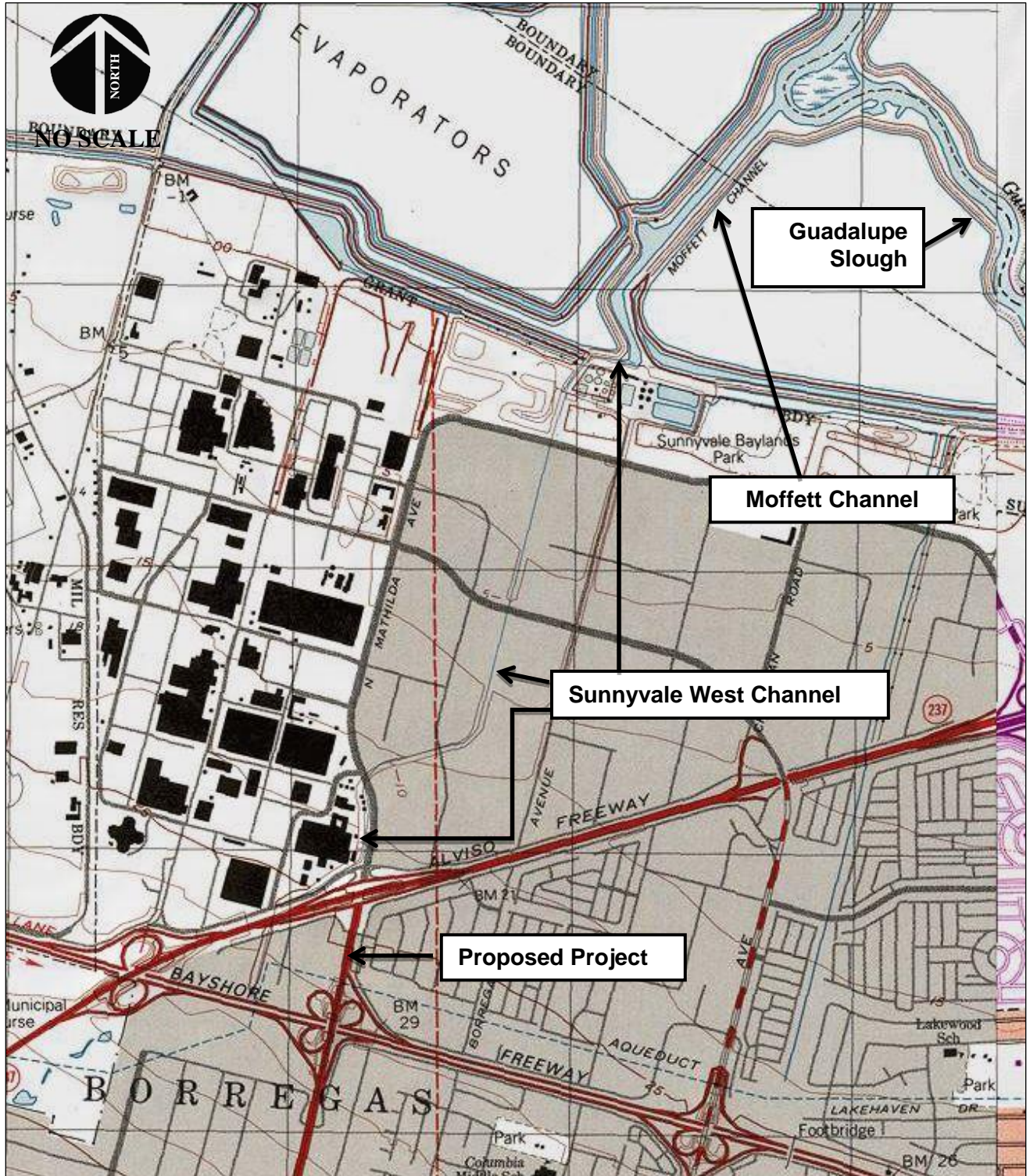


Figure 7. Topographic Map of Project Area

Source: USGS

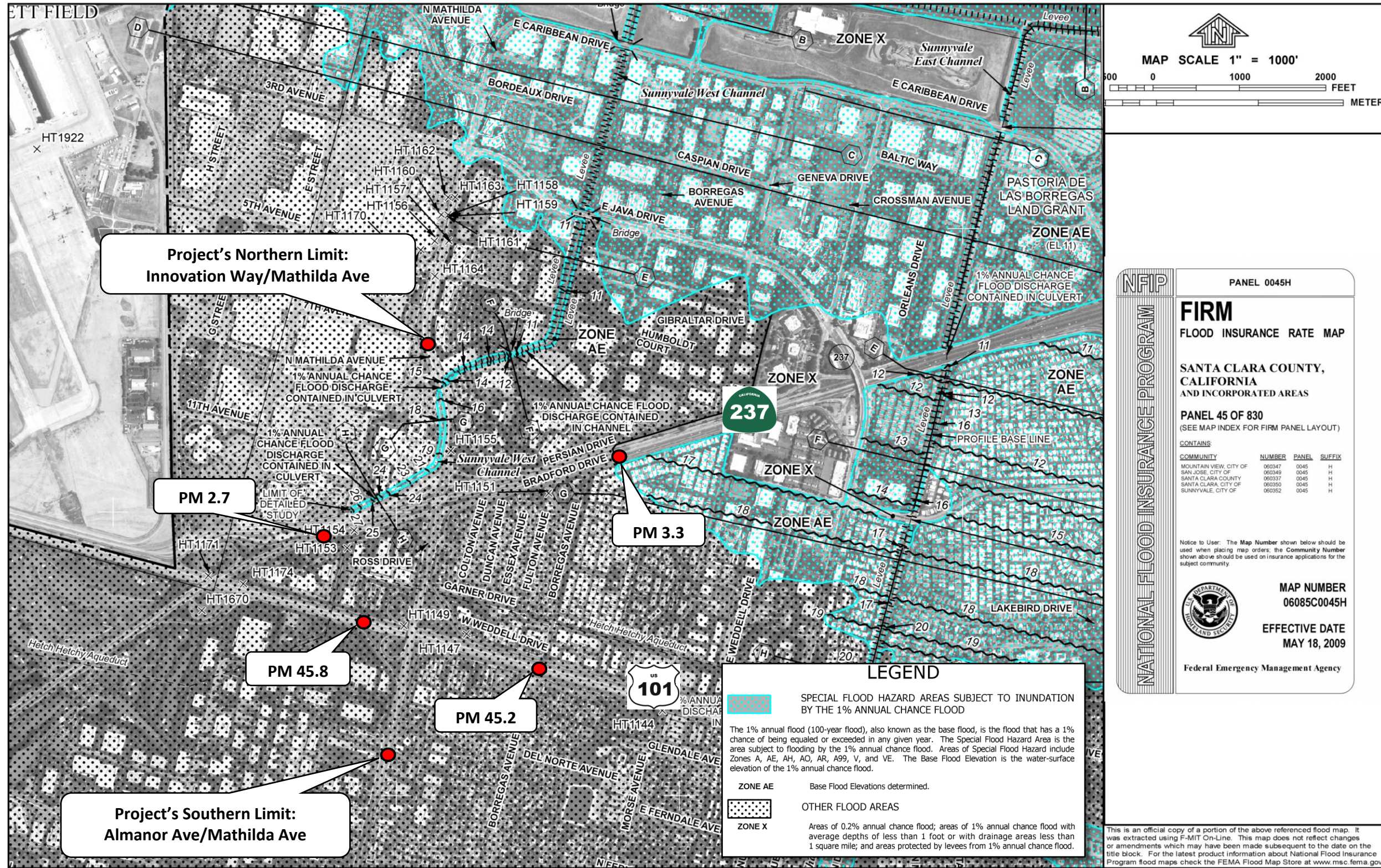


Figure 8. FIRM for Santa Clara County, California, and Incorporated Areas

Source: FEMA

3.1.3.2 Groundwater Hydrology

The Flood Insurance Study (FIS) for Santa Clara County (FEMA 2014) states that the rapid urbanization of the Santa Clara Valley has lowered the water table, with resulting subsidence of the lands adjacent to San Francisco Bay. Subsidence ceased after 1970 when water was brought into the area. The Santa Clara Valley Water District periodically releases water from reservoirs into stream channels and percolation basins, so it can percolate down to the water table.

Project-specific soil borings are not available at this phase. The *Preliminary Geological Assessment* (PGA) conducted by BASELINE Environmental Consulting (2015) used GeoTracker to review ambient groundwater-level data for sites at 724 Mathilda Avenue and 102 Persian Drive. Depth to groundwater ranged from 7 to 15 feet below ground surface (bgs). Based on the regional topography and previously measured groundwater levels, groundwater is expected to flow to the north-northeast across the Project site.

High groundwater may affect the choice of treatment BMPs and may require dewatering during construction. If there is high groundwater, infiltration devices may not be feasible for the Project. Hydrologic information will be updated when additional field work is performed during the PS&E phase.

3.1.4 Geology/Soils

The PGA indicates that the Project is generally underlain by Holocene alluvium with an average thickness of about 55 ft. As part of the PGA, the Web Soil Survey from the [Natural Resources Conservation Service](#) (NRCS) was reviewed for the Project. The Project area is entirely Urbanland-Hangerone complex, 0 to 2 percent slopes, drained. According to the Web Soil Survey, this soil is within hydrologic soil group (HSG) C. According to the NRCS (2007), HSG C soils have moderately high runoff potential and restricted water transmission.

The low permeability of this soil group suggests that infiltration devices may not be feasible for the Project. Amended or engineered soil media can be used to increase the infiltration potential of proposed treatment BMPs in these areas. The design feasibility of infiltration devices should be further evaluated during the PS&E phase once detailed infiltration studies have been conducted and appropriate soil amendments or engineered soil mixes have been developed. An underdrain will likely be necessary to convey water from the site.

Geologic information will be updated when additional field work is performed during the PS&E phase.

3.1.4.1 Soil Erosion Potential

According to the PGA, the Project is located in the Coast Ranges Geomorphic Province of northern California, consisting of northwest-trending folds and faults associated with the San Andreas Fault Zone. Due to the Project location, the site could impact or be impacted by soil erosion, expansive soils, corrosive soils, seismic ground shaking, and liquefaction. These hazards could affect the structural integrity of Project structures, including new pavement, new retaining walls, and traffic operations.

The Project would be designed in accordance with the Caltrans Seismic Design Criteria. During the PS&E phase, additional data would be collected to confirm site conditions and determine appropriate construction measures based on the geologic conditions.

3.1.5 Wetlands/Waters

ICF International conducted a delineation of waters of the U.S. for the Project (ICF 2015). Sunnyvale West Channel was identified as a non-wetland water of the United States. Because no Project activities will take place within the channel, no federal permits (Section 401 or 404) will be required. No wetlands or other jurisdictional areas were found within the study area.

3.2 Water Quality Objectives/Standards and Beneficial Uses

The beneficial uses of water are defined in the Basin Plan as those necessary for the survival or well-being of humans, plants, and wildlife. Examples of beneficial uses include drinking water supplies, swimming, industrial and agricultural water supply, and the support of freshwater and marine habitats and their organisms.

3.2.1 Surface Water Quality Objectives

The general water quality objectives established for surface waters within the San Francisco Bay region include bacteria, bioaccumulation biostimulatory substances, color, dissolved oxygen, floating material, oil and grease, population and community ecology, pH, radioactivity, salinity, sediment, settleable material, suspended material, sulfide, taste and odors, temperature, toxicity, turbidity, and un-ionized ammonia (Appendix A.1). All urban creeks in the region are subject to a water quality attainment strategy and TMDL for diazinon and pesticide-related toxicity (Appendix A).

The Basin Plan does not list any existing beneficial uses for Sunnyvale West Channel. The Project is located more than one mile from Moffett Channel and Guadalupe Slough, and no impacts to those water bodies are anticipated.

3.2.2 Groundwater Quality Objectives

The “maintenance of existing high quality of groundwater” is the primary groundwater objective. General water quality objectives established for groundwater within the San Francisco Bay region include bacteria, organic and inorganic chemical constituents, radioactivity, and taste and odors. Additional objectives are established for municipal and agricultural supply. The relevant water quality objectives from the Basin Plan are included in Appendix A.

The Santa Clara Groundwater Sub-basin has the following existing beneficial uses (San Francisco Bay RWQCB 2015):

- Existing municipal and domestic water supply (MUN)
- Potential industrial process water supply (PROC)
- Potential industrial service water supply (IND)
- Existing agricultural water supply (AGR)

3.3 Existing Water Quality

This section describes the water quality in the existing condition of the Project area.

3.3.1 List of Impaired Waters

There are no impaired waters listed on the CWA 303(d) list within the Project limits.

3.3.2 Trash Load Reduction

Sunnyvale is the second largest city in Santa Clara County and the fifth largest in the San Francisco Bay area. The Project is in a High to Very High trash generation area (City of Sunnyvale 2014; WRECO 2015b). Appropriate trash capture BMPs will be evaluated in the PS&E phase.

4 ENVIRONMENTAL CONSEQUENCES

The following sections present the potential temporary and permanent water quality impacts from the proposed Project activities.

Temporary water quality impacts can result from sediment discharge from DSAs and construction near water resources. Permanent impacts to water quality result from the addition of impervious area; this additional impervious area prevents runoff from naturally dispersing and infiltrating into the ground, resulting in increased concentrated flow.

Table 1 and Table 2 summarize the anticipated DSAs, reworked impervious areas, and added impervious areas for each Build Alternative. The No-Build Alternative would not result in any DSA or modification to impervious areas. Build Alternative 2 would have the greatest DSA (22 acres), added impervious area (3 acres), and reworked impervious area (5 acres). The DSA values and impervious areas would be further refined during the PS&E phase when the limits of grading and locations of construction staging and other areas of disturbance are further defined.

Table 1. Disturbed Soil, Existing and Added Impervious, and Reworked Areas for Build Alternative 1

| Right-of-Way | Disturbed Soil Area (acre) | Existing Impervious Area (acre) | Added Impervious Area (acre) | Reworked Impervious Area (acre) | Added and Reworked Impervious Area (acre) |
|-------------------|----------------------------|---------------------------------|------------------------------|---------------------------------|---|
| Caltrans | 20 | 45.5 | 2 | 4 | 6 |
| City of Sunnyvale | 0.011 | 4.5 | 0.01 | 0.001 | 0.011 |
| | | | | | |
| Total | 20.011 | 50 | 2.01 | 4.001 | 6.011 |

Source: WMH

Table 2. Disturbed Soil, Existing and Added Impervious, and Reworked Areas for Build Alternative 2

| Right-of-Way | Disturbed Soil Area (acre) | Existing Impervious Area (acre) | Added Impervious Area (acre) | Reworked Impervious Area (acre) | Added and Reworked Impervious Area (acre) |
|-------------------|----------------------------|---------------------------------|------------------------------|---------------------------------|---|
| Caltrans | 22 | 45.5 | 3 | 5 | 8 |
| City of Sunnyvale | 0.011 | 4.5 | 0.01 | 0.001 | 0.011 |
| | | | | | |
| Total | 22.011 | 50 | 3.01 | 5.001 | 8.011 |

4.1 Potential Impacts to Water Quality

The Project would add impervious area and therefore could potentially impact water quality. Stormwater runoff from the Project corridor would drain to Sunnyvale West Channel via storm drains. Of the two Build Alternatives, Alternative 2 has the potential for greater impact, with one additional acre compared to Alternative 1.

4.1.1 Anticipated Changes to the Physical/Chemical Characteristics of the Aquatic Environment

The Project would add impervious area and therefore could potentially increase the volume and velocity of the stormwater flow to receiving water bodies. In addition, the pollutant loading could increase. The added impervious area is directly related to the potential for permanent water quality impacts and changes to the hydrograph due to increased flow and velocity. Disturbed soil from construction activities could potentially result in soil particles entering receiving waters. Any stormwater impacts would be minimized through proper implementation of permanent design pollution prevention and treatment BMPs.

4.1.1.1 Currents, Circulation, or Drainage Patterns

The Project drainage design would strive to maintain the existing drainage patterns. The additional runoff from the added impervious area may result in minimal impacts to the existing hydrograph, including minimal increases in low and peak flow velocity and volume. The Project may require modifications to some existing drainages. Existing underground drainage systems and cross culverts may be upgraded as needed to accommodate the Project.

4.1.1.2 Suspended Particulates (Turbidity)

The Project would result in the creation of two to three acres of additional impervious area, which increases the amount of runoff that does not infiltrate or disperse over unpaved surfaces. This non-infiltrated and concentrated runoff could result in the direct discharge of sediment-laden flow from the roadway to receiving water bodies. Any stormwater impacts would be minimized through proper implementation of permanent design pollution prevention and treatment BMPs. Realignment, removal, and construction of traffic lanes, on- and off-ramps, and bicycle and pedestrian facilities will disturb at least 20 acres of soil, potentially increasing the particulates available for discharge into receiving waters. Temporary site management BMPs will be used to minimize potential construction-related impacts.

4.1.1.3 Oil, Grease, and Chemical Pollutants

Heavy metals associated with vehicle tire and brake wear, oil and grease, and exhaust emissions are the primary pollutants associated with transportation corridors. Generally, highway stormwater runoff has the following pollutants: total suspended solids, nitrate nitrogen, total kjeldahl nitrogen, phosphorus, ortho-phosphate, copper, lead, and zinc. The pollutants are dispersed from aerially deposited pollutants that accumulate on tree leaves, combustion products from fossil fuels, and the wearing of brake pads and tires. The No-build Alternative would have potential permanent water quality impacts due to increasing congestion, leading to a greater deposition of particulates from exhaust and heavy metals from braking. The two Build Alternatives would also potentially increase deposition of particulates from increased traffic loads due to the widening of the northbound ramps.

The removal and construction of concrete roadways, as well as the use of cleaning supplies, could potentially release phosphates, VOCs, and SVOCs into the environment. Temporary site management BMPs will be used to minimize potential construction-related impacts.

4.1.1.4 pH

Sand and curing compounds used in the production of concrete, and the resultant concrete washout wastewater can increase pH if released into receiving waters. Cement used in the repair and maintenance of culverts can also cause a pH increase as water contacts the newly applied material. Existing underground drainage systems and cross culverts may need to be upgraded to accommodate the Project, causing the potential for water flow to be exposed to cement. Temporary site management BMPs will be used to minimize potential construction-related impacts. Non-stormwater BMPs will be considered for the Project.

4.1.1.5 Aquifer Recharge/Groundwater

This Project would result in the addition of impervious area but would not substantially reduce the amount of unpaved area available to allow runoff to infiltrate into the soil. The reduction of runoff infiltrating through native soils has the potential to result in loss in volume or amount of water that previously recharged localized aquifers and to reduce regional groundwater volumes. While the increase in impervious area would reduce the available area for infiltration of stormwater, as shown in Table 3, the increase in impervious surface area compared to the total watershed area would be minimal for both alternatives. Therefore, the amount of surface runoff that infiltrates into the groundwater system would be minimally affected.

Table 3. Increase in Impervious Area Compared to Watershed

| Build Alternative | Added and Reworked Impervious Area (acre) | Watershed Area (acre) | % Increase of Impervious Area in Watershed |
|-------------------|---|-----------------------|--|
| 1 | 6.011 | 147,267 | 0.004 |
| 2 | 8.011 | | 0.005 |

4.1.2 Short-Term Impacts During Construction

During construction, runoff from DSAs could cause potentially sediment-laden flows to enter storm drainage facilities. Earth-moving and other construction activities could cause minor erosion and runoff of top soils into the drainage systems along the Project corridor, which could temporarily affect water quality in local waterways. Sources of sediment that could result in increases in turbidity include uncovered or improperly covered active and non-active stockpiles, unstabilized slopes, and construction staging areas. These impacts would be minimized through the use of construction site BMPs (Caltrans 2003).

Stormwater runoff from the Project site during construction may transport pollutants to the Sunnyvale West Channel and storm drains; therefore, both Build Alternatives for the Project would have potential short-term water quality impacts. Any stormwater impacts would be minimized through proper implementation of construction site pollution prevention BMPs.

If fueling or maintenance of construction vehicles occurs within the Project site during construction, there is a risk of accidental spills or releases of fuels, oils, or other potentially toxic materials. An accidental release of these materials may pose a threat to water quality if contaminants enter storm drains, open channels, or surface water receiving bodies. The magnitude of the impact from an accidental release depends on the amount and type of material spilled.

The Project would involve excavations that may affect groundwater resources, and construction may have localized impacts to the flow of groundwater. Dewatering would be needed at locations of excavation work with high groundwater.

Overall, the Project would have temporary impacts during construction. These impacts would be minimized through the use of BMPs as described in Section 5.1.

4.2 Cumulative Impacts

There may be a cumulative impact from the Project and other nearby projects. The approved Moffett Place complex, located between Borregas Drive and Mathilda Avenue, includes six eight-story buildings, two parking structures, an amenities building, and an extension of Innovation Way to Bordeaux Drive. However, because each project would be subject to NPDES requirements and implement BMPs, the cumulative impacts would be minimal.

5 AVOIDANCE AND MINIMIZATION MEASURES

This Project would have minimal impacts to water quality if the following avoidance and minimization measures are incorporated.

As mentioned in Section 2.3.3, the Project is in a catchment draining to hardened channel and is exempt from SCVURPPP hydromodification requirements. The Project will be subject to Caltrans treatment and hydromodification controls unless Caltrans proposes (and gets Headquarters' approval), that no hydromodification controls would be necessary for this Project because none is required under local regulations.

As mentioned in Section 3.1.5, no work will be done inside Sunnyvale West Channel, and neither a 401 nor a 404 permit is required.

5.1 Temporary Avoidance and Minimization Measures

5.1.1 Construction General Permit

The Project would involve more than one acre of DSA and therefore must comply with the Construction General Permit (CGP). Projects subject to the CGP must perform a risk level assessment to determine BMP implementation, sampling and analysis, and reporting requirements related to construction activities. A project's risk level is determined from the receiving water risk and sediment risk. The Project is classified as having a low receiving water risk because Project receiving waters (Sunnyvale West Channel, which drains to Moffett Channel and Guadalupe Slough) are not on the CWA 303(d) list as impaired for sedimentation or siltation, and do not have the combined existing beneficial uses of cold freshwater habitat (COLD), fish migration (MIGR), and fish spawning (SPWN).

The sediment risk factor is determined from the product of the rainfall erosivity factor (R), the soil erosion factor (K), and the length-slope factor (LS). Based on the planned construction duration from May 5, 2018, to May 3, 2019, the R factor was calculated for this period to be 35. Per the Natural Resources Conservation Service Web Soil Survey, the weighted average K factor within the Project area is 0.28. The Caltrans Water Quality Planning Tool identifies the LS factor within the Project area as 0.36. The product of these values is 3.53; because this value is less than 15, the Project would be classified as having a low sediment risk. The sediment risk would be updated during the PS&E phase as detailed Project information becomes available.

Table 4 summarizes the sediment and receiving water risk and presents the calculated risk level. The factors used to determine the planning watershed sediment risk are included in Appendix B.

The risk level is classified as Risk Level 1 if both the sediment and receiving water risk are low, is classified as Risk Level 3 if both the sediment and receiving water risk are high, and all other combinations are classified as Risk Level 2. Based on the low receiving water risk and the low sediment risk, the Project would be classified as Risk Level 1 under the CGP.

Table 4. Sediment Risk Factors

| R Factor | K Factor | LS Factor | Product (R*K*LS) | Sediment Risk | Receiving Water Risk | RISK LEVEL |
|----------|----------|-----------|------------------|---------------|----------------------|------------|
| 35 | 0.28 | 0.36 | 3.53 | Low | Low | 1 |

All risk levels are subject to temporary construction site BMP implementation and visual monitoring requirements. The BMP implementation and sampling required under each risk level are measures that will minimize impacts to receiving water bodies and water resources. The risk level presented in this section is based on planning-level information available at the time of preparation of this Water Quality Assessment Report. The actual Project risk level would be refined during the Project design phase.

5.1.2 Storm Water Pollution Prevention Plan

Risk Level 1 projects are subject to BMP and visual monitoring requirements. A Storm Water Pollution Prevention Plan (SWPPP) must be prepared by the contractor and approved by the Caltrans Resident Engineer prior to the start of construction. The SWPPP must comply with the conditions of Caltrans' MS4 permit and the CGP to address temporary water quality impacts resulting from construction activities associated with the Project. The SWPPP includes the development of a Construction Site Monitoring Program that presents procedures and methods related to the visual monitoring and sampling and analysis plans for non-visible pollutants, sediment and turbidity, and pH.

Because the Project must comply with the CGP, a Notice of Intent would be filed. To obtain permit coverage under the CGP, all dischargers must electronically file Permit Registration Documents through the SWRCB's Stormwater Multiple Application and Report Tracking System (SMARTS). Notice of Termination, changes of information, sampling and monitoring information, annual reporting, and other compliance documents are also filed via SMARTS.

The SWPPP is intended to address construction-phase impacts, and include, at a minimum, the following elements:

- Project Description – The project description includes maps and other information related to construction activities and potential sources of pollutants.
- Minimum Construction Control Measures – These measures may include limiting construction access routes, stabilization of areas denuded by construction, and using sediment controls and filtration.
- Erosion and Sediment Control – The SWPPP is required to contain a description of soil stabilization practices, control measures to prevent a net increase in sediment load in stormwater, controls to reduce tracking sediment onto roads, and controls to reduce wind erosion.
- Non-Storm Water Management – The SWPPP includes provisions to reduce and control discharges other than stormwater.
- Post-Construction Storm Water Management – The SWPPP includes a list of stormwater control measures that provide ongoing (permanent) protection for water resources.
- Waste Management and Disposal – The SWPPP includes a waste management section including equipment maintenance waste, used oil, batteries, etc. All waste must be disposed of as required by state and federal law.

- Maintenance, Inspection, and Repair – The SWPPP requires an ongoing program to ensure that all controls are in place and operating as designed.
- Monitoring – This provision requires documented inspections of the control measures.
- Reports – The contractor would prepare an annual report on the construction project and submit this report on September 1 each year. This report would be submitted on the SMARTS website to the SWRCB.
- Training – The SWPPP provides documentation on the training and qualifications of the designated Qualified SWPPP Developer and Qualified SWPPP Practitioner. Trained personnel must do inspections, maintenance, and repair of construction site BMPs.
- Construction Site Monitoring Program – The SWPPP includes a Construction Site Monitoring Program detailing the procedures and methods related to the visual monitoring and sampling and analysis plans for non-visible pollutants.

5.1.3 List of Proposed Temporary Construction Site Best Management Practices

Caltrans is required to reduce pollutants in stormwater discharges to the maximum extent practicable during construction. Pollutants must be reduced using the Best Available Technology Economically Achievable, and conventional pollutants (i.e. total suspended solids and pH) must be reduced using the Best Conventional Technology.

Construction work for this Project is expected to take 250 days. When possible, the scheduling of earth-disturbing construction activities should not be made during anticipated rain events. To avoid and minimize any potential sediment-laden or contaminated runoff or run-on within the Project area, construction site BMPs should be installed prior to the start of construction or as early as feasibly possible during construction.

High groundwater may affect the choice of treatment BMPs and may require dewatering during construction.

Temporary impacts to water quality can be avoided or minimized by implementing standard BMPs recommended for a particular construction activity. The selected temporary BMPs are consistent with the practices required under the CGP and the Caltrans MS4 permit and are intended to achieve compliance with the requirements of the permits. Compliance with the requirements of these permits, and adherence to the conditions, reduces or avoids potentially significant construction-related impacts.

Adverse impacts can occur during construction-related activities. Soil erosion, especially during heavy rainfall, can increase the suspended solids, dissolved solids, and organic pollutants in stormwater runoff generated within the project limits. These conditions would persist until completion of construction activities and implementation of long-term erosion control measures.

Utilities installations and cross culvert extensions or modifications may require dewatering. Contract documents would address any necessary permits for dewatering.

Non-stormwater waste management is also essential to minimize the potential for water quality impacts. Accidental spills of petroleum hydrocarbons (such as fuels and lubricating oils), concrete wastewater, and possibly sanitary wastes from construction work site wash facilities are also of concern during construction activities.

A spill on the roadway would trigger immediate response actions to report, contain, and mitigate the incident. The California Office of Emergency Services has developed a Hazardous Materials Incident Contingency Plan, which provides a program for response to spills involving hazardous materials. The plan designates a chain of command for notification, evacuation, response, and cleanup of spills. Caltrans also has spill contingency procedures and response crews.

Temporary erosion control measures can be applied to all exposed areas during construction, including the trapping of sediment within the construction area through the placing of barriers, such as silt fences, at the perimeter of downstream drainage points or through the construction of temporary detention basins. Other methods of minimizing erosion impacts include the implementation of hydromulching and/or limiting the amount and length of exposure of graded soil. In addition to these erosion control measures, the use of compost is strongly encouraged by Caltrans. Compost not only improves erosion resistance and vegetation establishment, but it also helps immobilize heavy metals that are common along highways. Compost can be considered or specified during the design phase of the Project.

The suggested minimum temporary control BMPs that would be necessary for the Project are included in Table 5. Further evaluation of the BMPs necessary for this Project to comply with the CGP and the Caltrans MS4 permit would be detailed during the PS&E phase. The proposed construction site BMPs would be reviewed and approved by the Caltrans District 4 Stormwater Coordinator during the PS&E phase.

Table 5. Temporary Best Management Practices

| Temporary BMP | Purpose |
|---|--|
| Soil Stabilization | |
| Move-In/Move-Out | To stabilize material storage areas. |
| Hydromulch | To stabilize idle disturbed areas during construction, especially slopes. |
| Temporary Cover | Plastic covers for stockpiles. |
| Sediment Control | |
| Temporary Silt Fence | Linear, permeable fabric barriers to intercept sediment-laden sheet flow. Placed downslope of exposed soil areas, along channels and project perimeter. |
| Temporary Gravel Bag Berm | Single row of gravel bags installed end-to-end to form a barrier across a slope to intercept runoff. Can be used to divert or detain moderately concentrated flows. |
| Temporary Check Dams | Small constructed device of rock or other product placed across a channel or ditch to reduce flow velocity. |
| Temporary Drainage Inlet Protection | Runoff detention devices used at storm drain inlets that are subject to runoff from construction activities. |
| Tracking Control | |
| Temporary Construction Entrances/Exits | Points of entrance/exit to a construction site that are stabilized to reduce the tracking of mud and dirt onto public roads. |
| Street Sweeping | Removal of tracked sediment to prevent it from entering a storm drain or watercourse. |
| Non-Stormwater Management | |
| Dewatering | For managing groundwater within excavations due to anticipated high groundwater. |
| All other anticipated non-stormwater management measures are covered under Job Site Management. | |
| Waste Management and Materials Pollution Control | |
| Temporary Concrete Washout Facilities | Specified vehicle washing areas to contain concrete waste materials. |
| All other anticipated waste management and materials pollution control measures are covered under Job Site Management. | |
| Job Site Management | |
| <p>General measures covered under job site management include:</p> <ul style="list-style-type: none"> • spill prevention and control • materials management • stockpile management • waste management • hazardous waste management • contaminated soil • concrete waste • sanitary and septic waste and liquid waste <p>Miscellaneous job site management includes:</p> <ul style="list-style-type: none"> • training of employees and subcontractors • proper selection, deployment and repair of construction site BMPs | <p>Non-stormwater management consists of:</p> <ul style="list-style-type: none"> • water control and conservation • illegal connection and discharge detection and reporting • vehicle and equipment cleaning • vehicle and equipment fueling and maintenance • paving, sealing, saw cutting and grinding operations • thermoplastic striping and pavement markers • concrete curing and concrete finishing |

Source: Caltrans

5.2 Permanent Avoidance and Minimization Measures

The section describes the permanent BMPs that would be considered for implementation.

5.2.1 Permanent Pollution Prevention Design Measures

The Caltrans MS4 permit contains provisions to reduce pollutant loadings from the facility once construction is complete. The permit stipulates that permanent measures that control pollutant discharges must be considered and implemented for all new or reconstructed facilities. Permanent control measures located within Caltrans right-of-way reduce pollutants in stormwater runoff from the roadway. These measures reduce the suspended particulate loads, and thus pollutants associated with the particles, from entering waterways. The measures would be incorporated into the final engineering design or landscape design of the Project and would take into account expected runoff from the roadway. In addition, the permit also stipulates that an operation and maintenance program be implemented for permanent control measures. This category of water quality control measures can be identified as including both design pollution prevention BMPs and treatment BMPs.

5.2.1.1 Proposed Design Pollution Prevention BMPs

The estimated added and reworked impervious areas for each alternative within the Project limits are shown in Table 1 and Table 2.

The following design pollution prevention BMPs would be incorporated into the project design:

- Conserve natural areas, to the extent feasible, including existing trees, stream buffer areas, vegetation and soils;
- Minimize the impervious footprint of the project;
- Minimize disturbances to natural drainages;
- Design and construct pervious areas to effectively receive runoff from impervious areas, taking into consideration the pervious areas' soil conditions, slope and other pertinent factors;
- Implement landscape and soil-based BMPs such as compost-amended soils and vegetated strips and swales;
- Use climate-appropriate landscaping that minimizes irrigation and runoff, promotes surface infiltration, and minimizes the use of pesticides and fertilizers; and
- Design all landscapes to comply with State, local, and Caltrans requirements.

5.2.1.2 Proposed Treatment BMPs

Under the Caltrans MS4 permit, Caltrans is required to implement post-construction treatment control BMPs for projects that create one acre or more of new impervious surface. The estimated added and reworked impervious areas within the Project limits are shown in Table 1 and Table 2.

High groundwater may affect the choice of treatment BMPs. Consistent with Caltrans' MS4 permit, treatment control BMPs constructed for Caltrans projects would be designed according to the following priorities (in order of preference):

- a) Infiltrate, harvest and re-use, and/or evapotranspire the stormwater runoff;
- b) Capture and treat the stormwater runoff.

Because the site soil is HSG C, infiltration devices would likely not be feasible, but this will be verified when more information becomes available during the PS&E phase.

Caltrans has an approved list of treatment BMPs that have been studied and verified to remove targeted design constituents and provide general pollutant removal. The stormwater treatment facilities for both build alternatives may include any of the following:

- Biofiltration swales/strips
- Dry weather flow diversion
- Infiltration devices
- Detention devices
- Gross solids removal devices
- Media filters
- Multi-chambered treatment train
- Wet basin

Due to potential shallow groundwater and soil type, biofiltration swales are anticipated to be the preferred BMP. Because the water will likely not infiltrate completely, an underdrain will likely be needed for conveyance. Any underdrains or infiltration trenches would need to be lined with an impermeable layer to prevent comingling of groundwater with runoff. The area is largely flat, and exposed soil would be hydroseeded. Treatment BMPs will be further evaluated in the PS&E phase when further hydrologic and geologic field work is conducted.

The Project is in a high trash-generating area, and additional trash production and release is a concern. Appropriate trash capture BMPs will be evaluated in the PS&E phase.

5.2.2 Project Operation and Maintenance

Maintenance of facilities would be provided by Caltrans, unless a maintenance agreement is established. Maintenance of facilities and agreements would be further investigated during the design phase of the Project. The Maintenance Unit field representatives have unique insight into local problems and maintenance and safety concerns. Maintenance coordination for Project-related issues includes:

- Drainage patterns (particularly known areas of flooding, debris, etc.)
- Possible material borrow or spoil sites
- Concerns of the local residents
- Existing and potential erosion problems
- Facilities within the right-of-way that would affect alternative designs
- Whether facilities are safe to maintain
- Known environmentally sensitive areas

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Appendix A **Excerpts from the *Water Quality Control Plan for the San Francisco Bay Region (Basin Plan)***

Appendix A.1 Water Quality Objectives for Surface Water and Groundwater

CHAPTER 3: WATER QUALITY OBJECTIVES

The overall goals of water quality regulation are to protect and maintain thriving aquatic ecosystems and the resources those systems provide to society and to accomplish these in an economically and socially sound manner. California's regulatory framework uses water quality objectives both to define appropriate levels of environmental quality and to control activities that can adversely affect aquatic systems.

3.1 WATER QUALITY OBJECTIVES

There are two types of objectives: narrative and numerical. Narrative objectives present general descriptions of water quality that must be attained through pollutant control measures and watershed management. They also serve as the basis for the development of detailed numerical objectives.

Historically, numerical objectives were developed primarily to limit the adverse effect of pollutants in the water column. Two decades of regulatory experience and extensive research in environmental science have demonstrated that beneficial uses are not fully protected unless pollutant levels in all parts of the aquatic system are also monitored and controlled. The Regional Board is actively working towards an integrated set of objectives, including numerical sediment objectives, that will ensure the protection of all current and potential beneficial uses.

Numerical objectives typically describe pollutant concentrations, physical/chemical conditions of the water itself, and the toxicity of the water to aquatic organisms. These objectives are designed to represent the maximum amount of pollutants that can remain in the water column without causing any adverse effect on organisms using the aquatic system as habitat, on people consuming those organisms or water, and on other current or potential beneficial uses (as described in [Chapter 2](#)).

The technical bases of the region's water quality objectives include extensive biological, chemical, and physical partitioning information reported in the scientific literature, national water quality criteria, studies conducted by other agencies, and information gained from local environmental and discharge monitoring (as described in [Chapter 6](#)). The Regional Board recognizes that limited information exists in some cases, making it difficult to establish definitive numerical objectives, but the Regional Board believes its conservative approach to setting objectives has been proper. In addition to the technical review, the overall feasibility of reaching objectives in terms of technological, institutional, economic, and administrative factors is considered at many different stages of objective derivation and implementation of the water quality control plan.

Together, the narrative and numerical objectives define the level of water quality that shall be maintained within the region. In instances where water quality is better than that prescribed by the objectives, the state Antidegradation Policy applies ([State Board Resolution 68-16: Statement of Policy With Respect to Maintaining High Quality of Waters in California](#)). This policy is aimed at protecting relatively uncontaminated aquatic systems where they exist and preventing further degradation. The state's Antidegradation Policy is consistent with the federal Antidegradation Policy, as interpreted by the State Water Resources Control Board in State Board Order No. 86-17.

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When uncontrollable water quality factors result in the degradation of water quality beyond the levels or limits established herein as water quality objectives, the Regional Board will conduct a case-by-case analysis of the benefits and costs of preventing further degradation. In cases where this analysis indicates that beneficial uses will be adversely impacted by allowing further degradation, then the Regional Board will not allow controllable water quality factors to cause any further degradation of water quality. Controllable water quality factors are those actions, conditions, or circumstances resulting from human activities that may influence the quality of the waters of the state and that may be reasonably controlled.

The Regional Board establishes and enforces waste discharge requirements for point and nonpoint source of pollutants at levels necessary to meet numerical and narrative water quality objectives. In setting waste discharge requirements, the Regional Board will consider, among other things, the potential impact on beneficial uses within the area of influence of the discharge, the existing quality of receiving waters, and the appropriate water quality objectives.

In general, the objectives are intended to govern the concentration of pollutant constituents in the main water mass. The same objectives cannot be applied at or immediately adjacent to submerged effluent discharge structures. Zones of initial dilution within which higher concentrations can be tolerated will be allowed for such discharges.

For a submerged buoyant discharge, characteristic of most municipal and industrial wastes that are released from submerged outfalls, the momentum of the discharge and its initial buoyancy act together to produce turbulent mixing. Initial dilution in this case is completed when the diluting wastewater ceases to rise in the water column and first begins to spread horizontally.

For shallow water submerged discharges, surface discharges, and nonbuoyant discharges, characteristic of cooling water wastes and some individual discharges, turbulent mixing results primarily from the momentum of discharge. Initial dilution, in these cases, is considered to be completed when the momentum-induced velocity of the discharge ceases to produce significant mixing of the waste, or the diluting plume reaches a fixed distance from the discharge to be specified by the Regional Board, whichever results in the lower estimate for initial dilution.

Compliance with water quality objectives may be prohibitively expensive or technically impossible in some cases. The Regional Board will consider modification of specific water quality objectives as long as the discharger can demonstrate that the alternate objective will protect existing beneficial uses, is scientifically defensible, and is consistent with the state [Antidegradation Policy](#). This exception clause properly indicates that the Regional Board will conservatively compare benefits and costs in these cases because of the difficulty in quantifying beneficial uses.

These water quality objectives are considered necessary to protect the present and potential beneficial uses described in [Chapter 2](#) of this Plan and to protect existing high quality waters of the state. These objectives will be achieved primarily through establishing and enforcing waste discharge requirements and by implementing this water quality control plan.

3.2 OBJECTIVES FOR OCEAN WATERS

The provisions of the State Board's "Water Quality Control Plan for Ocean Waters of California" ([Ocean Plan](#)) and "Water Quality Control Plan for Control of Temperature in the Coastal and Interstate Waters and Enclosed Bays and Estuaries of California" ([Thermal Plan](#)) and any revision to them will apply to ocean waters. These plans describe objectives and effluent limitations for ocean waters.

3.3 OBJECTIVES FOR SURFACE WATERS

The following objectives apply to all surface waters within the region, except the Pacific Ocean.

3.3.1 BACTERIA

[Table 3-1](#) provides a summary of the bacterial water quality objectives and identifies the sources of those objectives. [Table 3-2](#) summarizes U.S. EPA's water quality criteria for water contact recreation based on the frequency of use a particular area receives. These criteria will be used to differentiate between pollution sources or to supplement objectives for water contact recreation.

3.3.3.1 Implementation Provisions for Water Contact Recreation Bacteria Objectives

Water quality objectives for bacteria in [Table 3-1](#) shall be strictly applied except when otherwise provided for in a TMDL. In the context of a TMDL, the Water Board may implement the objectives in fresh and marine waters by using a "reference system and antidegradation approach" as discussed below. Implementation of water quality objectives for bacteria using a "reference system and antidegradation approach" requires control of bacteria from all anthropogenic sources so that bacteriological water quality is consistent with that of a reference system. A reference system is defined as an area (e.g., a subwatershed or catchment) and associated monitoring point(s) that is minimally impacted by human activities that potentially affect bacteria densities in the reference receiving water body.

This approach recognizes that there are natural sources of bacteria (defined as non-anthropogenic sources) that may cause or contribute to exceedances of the objectives for indicator bacteria. It also avoids requiring treatment or diversion of water bodies or treatment of natural sources of bacteria from undeveloped areas. Such requirements, if imposed by the Water Board, could have the potential to adversely affect valuable aquatic life and wildlife beneficial uses supported by water bodies in the region.

Under the reference system approach, a certain frequency of exceedance of the single-sample objectives shall be permitted. The permitted number of exceedances shall be based on the observed exceedance frequency in a selected reference system(s) or the targeted water body, whichever is less. The "reference system and antidegradation approach" ensures that bacteriological water quality is at least as good as that of a reference system and that no degradation of existing bacteriological water quality is permitted where existing bacteriological water quality is better than that of the selected reference system(s).

The appropriateness of this approach, the specific exceedance frequencies to be permitted under it, and the permittees to whom it would apply will be evaluated within the context of TMDL development for a specific water body, and decided by the Water Board when considering

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adoption of a TMDL. These implementation provisions may only be used within the context of a TMDL addressing municipal stormwater (including discharges regulated under statewide municipal NPDES waste discharge requirements), discharges from confined animal facilities, and discharges from nonpoint sources.

3.3.2 BIOACCUMULATION

Many pollutants can accumulate on particles, in sediment, or bioaccumulate in fish and other aquatic organisms. Controllable water quality factors shall not cause a detrimental increase in concentrations of toxic substances found in bottom sediments or aquatic life. Effects on aquatic organisms, wildlife, and human health will be considered.

3.3.3 BIOSTIMULATORY SUBSTANCES

Waters shall not contain biostimulatory substances in concentrations that promote aquatic growths to the extent that such growths cause nuisance or adversely affect beneficial uses. Changes in chlorophyll a and associated phytoplankton communities follow complex dynamics that are sometimes associated with a discharge of biostimulatory substances. Irregular and extreme levels of chlorophyll a or phytoplankton blooms may indicate exceedance of this objective and require investigation.

3.3.4 COLOR

Waters shall be free of coloration that causes nuisance or adversely affects beneficial uses.

3.3.5 DISSOLVED OXYGEN

For all tidal waters, the following objectives shall apply:

In the Bay:

| | |
|--------------------------------|------------------|
| Downstream of Carquinez Bridge | 5.0 mg/l minimum |
| Upstream of Carquinez Bridge | 7.0 mg/l minimum |

For nontidal waters, the following objectives shall apply:

Waters designated as:

| | |
|--------------------|------------------|
| Cold water habitat | 7.0 mg/l minimum |
| Warm water habitat | 5.0 mg/l minimum |

The median dissolved oxygen concentration for any three consecutive months shall not be less than 80 percent of the dissolved oxygen content at saturation.

Dissolved oxygen is a general index of the state of the health of receiving waters. Although minimum concentrations of 5 mg/l and 7 mg/l are frequently used as objectives to protect fish life,

higher concentrations are generally desirable to protect sensitive aquatic forms. In areas unaffected by waste discharges, a level of about 85 percent of oxygen saturation exists. A three-month median objective of 80 percent of oxygen saturation allows for some degradation from this level, but still requires a consistently high oxygen content in the receiving water.

3.3.6 FLOATING MATERIAL

Waters shall not contain floating material, including solids, liquids, foams, and scum, in concentrations that cause nuisance or adversely affect beneficial uses.

3.3.7 OIL AND GREASE

Waters shall not contain oils, greases, waxes, or other materials in concentrations that result in a visible film or coating on the surface of the water or on objects in the water, that cause nuisance, or that otherwise adversely affect beneficial uses.

3.3.8 POPULATION AND COMMUNITY ECOLOGY

All waters shall be maintained free of toxic substances in concentrations that are lethal to or that produce significant alterations in population or community ecology or receiving water biota. In addition, the health and life history characteristics of aquatic organisms in waters affected by controllable water quality factors shall not differ significantly from those for the same waters in areas unaffected by controllable water quality factors.

3.3.9 pH

The pH shall not be depressed below 6.5 nor raised above 8.5. This encompasses the pH range usually found in waters within the basin. Controllable water quality factors shall not cause changes greater than 0.5 units in normal ambient pH levels.

3.3.10 RADIOACTIVITY

Radionuclides shall not be present in concentrations that result in the accumulation of radionuclides in the food web to an extent that presents a hazard to human, plant, animal, or aquatic life. Waters designated for use as domestic or municipal supply shall not contain concentrations of radionuclides in excess of the limits specified in Table 4 of Section 64443 (Radioactivity) of Title 22 of the California Code of Regulations (CCR), which is incorporated by reference into this Plan. This incorporation is prospective, including future changes to the incorporated provisions as the changes take effect (see [Table 3-5](#)).

3.3.11 SALINITY

Controllable water quality factors shall not increase the total dissolved solids or salinity of waters of the state so as to adversely affect beneficial uses, particularly fish migration and estuarine habitat.

3.3.12 SEDIMENT

The suspended sediment load and suspended sediment discharge rate of surface waters shall not be altered in such a manner as to cause nuisance or adversely affect beneficial uses.

Controllable water quality factors shall not cause a detrimental increase in the concentrations of toxic pollutants in sediments or aquatic life.

3.3.13 SETTLEABLE MATERIAL

Waters shall not contain substances in concentrations that result in the deposition of material that cause nuisance or adversely affect beneficial uses.

3.3.14 SUSPENDED MATERIAL

Waters shall not contain suspended material in concentrations that cause nuisance or adversely affect beneficial uses.

3.3.15 SULFIDE

All water shall be free from dissolved sulfide concentrations above natural background levels. Sulfide occurs in Bay muds as a result of bacterial action on organic matter in an anaerobic environment.

Concentrations of only a few hundredths of a milligram per liter can cause a noticeable odor or be toxic to aquatic life. Violation of the sulfide objective will reflect violation of dissolved oxygen objectives as sulfides cannot exist to a significant degree in an oxygenated environment.

3.3.16 TASTES AND ODORS

Waters shall not contain taste- or odor-producing substances in concentrations that impart undesirable tastes or odors to fish flesh or other edible products of aquatic origin, that cause nuisance, or that adversely affect beneficial uses.

3.3.17 TEMPERATURE

Temperature objectives for enclosed bays and estuaries are as specified in the "[Water Quality Control Plan for Control of Temperature in the Coastal and Interstate Waters and Enclosed Bays of California](#)," including any revisions to the plan.

In addition, the following temperature objectives apply to surface waters:

- The natural receiving water temperature of inland surface waters shall not be altered unless it can be demonstrated to the satisfaction of the Regional Board that such alteration in temperature does not adversely affect beneficial uses.
- The temperature of any cold or warm freshwater habitat shall not be increased by more than 5°F (2.8°C) above natural receiving water temperature

3.3.18 TOXICITY

All waters shall be maintained free of toxic substances in concentrations that are lethal to or that produce other detrimental responses in aquatic organisms. Detrimental responses include, but are not limited to, decreased growth rate and decreased reproductive success of resident or indicator species. There shall be no acute toxicity in ambient waters. Acute toxicity is defined as a median of less than 90 percent survival, or less than 70 percent survival, 10 percent of the time, of test organisms in a 96-hour static or continuous flow test.

There shall be no chronic toxicity in ambient waters. Chronic toxicity is a detrimental biological effect on growth rate, reproduction, fertilization success, larval development, population abundance, community composition, or any other relevant measure of the health of an organism, population, or community.

Attainment of this objective will be determined by analyses of indicator organisms, species diversity, population density, growth anomalies, or toxicity tests (including those described in [Chapter 4](#)), or other methods selected by the Water Board. The Water Board will also consider other relevant information and numeric criteria and guidelines for toxic substances developed by other agencies as appropriate.

The health and life history characteristics of aquatic organisms in waters affected by controllable water quality factors shall not differ significantly from those for the same waters in areas unaffected by controllable water quality factors.

3.3.19 TURBIDITY

Waters shall be free of changes in turbidity that cause nuisance or adversely affect beneficial uses. Increases from normal background light penetration or turbidity relatable to waste discharge shall not be greater than 10 percent in areas where natural turbidity is greater than 50 NTU.

3.3.20 UN-IONIZED AMMONIA

The discharge of wastes shall not cause receiving waters to contain concentrations of un-ionized ammonia in excess of the following limits (in mg/l as N):

| | |
|---|-------|
| Annual Median | 0.025 |
| Maximum, Central Bay (as depicted in Figure 2-5) and upstream | 0.16 |
| Maximum, Lower Bay (as depicted in Figures 2-6 and 2-7): | 0.4 |

The intent of this objective is to protect against the chronic toxic effects of ammonia in the receiving waters. An ammonia objective is needed for the following reasons:

- Ammonia (specifically un-ionized ammonia) is a demonstrated toxicant. Ammonia is generally accepted as one of the principle toxicants in municipal waste discharges. Some industries also discharge significant quantities of ammonia.

Water Quality Control Plan for the San Francisco Bay Basin

- Exceptions to the effluent toxicity limitations in [Chapter 4](#) of the Plan allow for the discharge of ammonia in toxic amounts. In most instances, ammonia will be diluted or degraded to a nontoxic state fairly rapidly. However, this does not occur in all cases, the South Bay being a notable example. The ammonia limit is recommended in order to preclude any build up of ammonia in the receiving water.
- A more stringent maximum objective is desirable for the northern reach of the Bay for the protection of the migratory corridor running through Central Bay, San Pablo Bay, and upstream reaches.

3.3.21 OBJECTIVES FOR SPECIFIC CHEMICAL CONSTITUENTS

Surface waters shall not contain concentrations of chemical constituents in amounts that adversely affect any designated beneficial use. Water quality objectives for selected toxic pollutants for surface waters are given in Tables [3-3](#), [3-3A](#), [3-3B](#), [3-3C](#), [3-4](#) and [3-4A](#).

The Water Board intends to work towards the derivation of site-specific objectives for the Bay-Delta estuarine system. Site-specific objectives to be considered by the Water Board shall be developed in accordance with the provisions of the federal Clean Water Act, the State Water Code, State Board water quality control plans, and this Plan. These site-specific objectives will take into consideration factors such as all available scientific information and monitoring data and the latest U.S. EPA guidance, and local environmental conditions and impacts caused by bioaccumulation. The objectives in Tables [3-3](#) and [3-4](#) apply throughout the region except as otherwise indicated in the tables or when site-specific objectives for the pollutant parameter have been adopted. Site-specific objectives have been adopted for copper in segments of San Francisco Bay (see [Figure 7.2-1-01](#)), for nickel in South San Francisco Bay ([Table 3-3A](#)), and for cyanide in all San Francisco Bay segments ([Table 3-3C](#)). Objectives for mercury that apply to San Francisco Bay are listed in [Table 3-3B](#). Objectives for mercury that apply to Walker Creek, Soulajule Reservoir, and their tributaries, and to waters of the Guadalupe River watershed are listed in [Table 3-4A](#).

South San Francisco Bay south of the Dumbarton Bridge is a unique, water-quality-limited, hydrodynamic and biological environment that merits continued special attention by the Water Board. Controlling urban and upland runoff sources is critical to the success of maintaining water quality in this portion of the Bay. Site-specific water quality objectives have been adopted for dissolved copper and nickel in this Bay segment. Site-specific objectives may be appropriate for other pollutants of concern, but this determination will be made on a case-by-case basis, and after it has been demonstrated that all other reasonable treatment, source control and pollution prevention measures have been exhausted. The Water Board will determine whether revised water quality objectives and/or effluent limitations are appropriate based on sound technical information and scientific studies, stakeholder input, and the need for flexibility to address priority problems in the watershed.

3.3.22 CONSTITUENTS OF CONCERN FOR MUNICIPAL AND AGRICULTURAL WATER SUPPLIES

At a minimum, surface waters designated for use as domestic or municipal supply (MUN) shall not contain concentrations of constituents in excess of the maximum (MCLs) or secondary maximum contaminant levels (SMCLs) specified in the following provisions of Title 22, which are incorporated by reference into this plan: Table 64431-A (Inorganic Chemicals) of Section 64431,

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and Table 64433.2-A (Fluoride) of Section 64433.2, Table 64444-A (Organic Chemicals) of Section 64444, and Table 64449-A (SMCLs-Consumer Acceptance Limits) and 64449-B (SMCLs-Ranges) of Section 64449. This incorporation-by-reference is prospective, including future changes to the incorporated provisions as the changes take effect. [Table 3-5](#) contains water quality objectives for municipal supply, including the MCLs contained in various sections of Title 22 as of the adoption of this plan.

At a minimum, surface waters designated for use as agricultural supply ([AGR](#)) shall not contain concentrations of constituents in excess of the levels specified in [Table 3-6](#).

3.4 OBJECTIVES FOR GROUNDWATER

Groundwater objectives consist primarily of narrative objectives combined with a limited number of numerical objectives. Additionally, the Water Board will establish basin- and/or site-specific numerical groundwater objectives as necessary. For example, the Water Board has groundwater basin-specific objectives for the Alameda Creek watershed above Niles to include the Livermore-Amador Valley as shown in [Table 3-7](#).

The maintenance of existing high quality of groundwater (i.e., "background") is the primary groundwater objective.

In addition, at a minimum, groundwater shall not contain concentrations of bacteria, chemical constituents, radioactivity, or substances producing taste and odor in excess of the objectives described below unless naturally occurring background concentrations are greater. Under existing law, the Water Board regulates waste discharges to land that could affect water quality, including both groundwater and surface water quality. Waste discharges that reach groundwater are regulated to protect both groundwater and any surface water in continuity with groundwater. Waste discharges that affect groundwater that is in continuity with surface water cannot cause violations of any applicable surface water standards.

3.4.1 BACTERIA

In groundwater with a beneficial use of [municipal and domestic supply](#), the median of the most probable number of coliform organisms over any seven-day period shall be less than 1.1 most probable number per 100 milliliters (MPN/100 mL) (based on multiple tube fermentation technique; equivalent test results based on other analytical techniques as specified in the National Primary Drinking Water Regulation, 40 CFR, Part 141.21 (f), revised June 10, 1992, are acceptable).

3.4.2 ORGANIC AND INORGANIC CHEMICAL CONSTITUENTS

All groundwater shall be maintained free of organic and inorganic chemical constituents in concentrations that adversely affect beneficial uses. To evaluate compliance with water quality objectives, the Water Board will consider all relevant and scientifically valid evidence, including relevant and scientifically valid numerical criteria and guidelines developed and/or published by other agencies and organizations (e.g., U.S. Environmental Protection Agency (U.S. EPA), the State Water Board, California Department of Health Services (DHS), U.S. Food and Drug

Water Quality Control Plan for the San Francisco Bay Basin

Administration, National Academy of Sciences, California Environmental Protection Agency's (Cal/EPA) Office of Environmental Health Hazard Assessment (OEHHA), U.S. Agency for Toxic Substances and Disease Registry, Cal/EPA Department of Toxic Substances Control (DTSC), and other appropriate organizations.)

At a minimum, groundwater designated for use as [domestic or municipal supply](#) (MUN) shall not contain concentrations of constituents in excess of the maximum (MCLs) or secondary maximum contaminant levels (SMCLs) specified in the following provisions of Title 22, which are incorporated by reference into this plan: Tables 64431-A (Inorganic Chemicals) of Section 64431, Table 64433.2-A (Fluoride) of Section 64433.2, and Table 64444-A (Organic Chemicals) of Section 64444. This incorporation-by-reference is prospective, including future changes to the incorporated provisions as the changes take effect. (See [Table 3-5](#).)

Groundwater with a beneficial use of agricultural supply shall not contain concentrations of chemical constituents in amounts that adversely affect such beneficial use. In determining compliance with this objective, the Water Board will consider as evidence relevant and scientifically valid water quality goals from sources such as the Food and Agricultural Organizations of the United Nations; University of California Cooperative Extension, Committee of Experts; and McKee and Wolf's "Water Quality Criteria," as well as other relevant and scientifically valid evidence. At a minimum, groundwater designated for use as agricultural supply (AGR) shall not contain concentrations of constituents in excess of the levels specified in [Table 3-6](#).

Groundwater with a beneficial use of freshwater replenishment shall not contain concentrations of chemicals in amounts that will adversely affect the beneficial use of the receiving surface water.

Groundwater with a beneficial use of industrial service supply or industrial process supply shall not contain pollutant levels that impair current or potential industrial uses.

3.4.3 RADIOACTIVITY

At a minimum, groundwater designated for use as [domestic or municipal supply](#) (MUN) shall not contain concentrations of radionuclides in excess of the MCLs specified in Table 4 (Radioactivity) of Section 64443 of Title 22, which is incorporated by reference into this plan. This incorporation-by-reference is prospective, including future changes to the incorporated provisions as the changes take effect. (See [Table 3-5](#).)

3.4.4 TASTE AND ODOR

Groundwater designated for use as [domestic or municipal supply](#) (MUN) shall not contain taste- or odor-producing substances in concentrations that cause a nuisance or adversely affect beneficial uses. At a minimum, groundwater designated for use as domestic or municipal supply shall not contain concentrations in excess of the SMCLs specified in Tables 64449-A (Secondary MCLs-Consumer Acceptance Limits) and 64449-B (Secondary MCLs-Ranges) of Section 64449 of [Title 22](#), which is incorporated by reference into this plan. This incorporation-by-reference is

Water Quality Control Plan for the San Francisco Bay Basin

prospective, including future changes to the incorporated provisions as the changes take effect. (See [Table 3-5](#).)

3.5 OBJECTIVES FOR THE DELTA

The objectives contained in the State Water Board's 1995 "[Water Quality Control Plan for the San Francisco Bay/Sacramento-San Joaquin Delta Estuary](#)" and any revisions thereto shall apply to the waters of the Sacramento-San Joaquin Delta and adjacent waters as specified in that plan.

3.6 OBJECTIVES FOR ALAMEDA CREEK WATERSHED

The water quality objectives contained in [Table 3-7](#) apply to the surface and groundwaters of the Alameda Creek watershed above Niles.

Wastewater discharges that cause the surface water limits in [Table 3-7](#) to be exceeded may be allowed if they are part of an overall wastewater resource operational program developed by those agencies affected and approved by the Water Board.

TABLES

[Table 3-1: Water Quality Objectives for Bacteria](#)

[Table 3-2: U.S. EPA Bacteriological Criteria for Water Contact Recreation](#)

[Table 3-3: Marine Water Quality Objectives for Toxic Pollutants for Surface Waters](#)

[Table 3-3A: Water Quality Objectives for Copper and Nickel in San Francisco Bay Segments](#)

[Table 3-3B: Marine Water Quality Objectives for Mercury in San Francisco Bay](#)

[Table 3-3C: Marine Water Quality Objectives for Cyanide in San Francisco Bay](#)

[Table 3-4: Freshwater Water Quality Objectives for Toxic Pollutants for Surface Waters](#)

[Table 3-4A: Freshwater Water Quality Objectives for Mercury in Walker Creek, Soulajule Reservoir, and All Tributary Waters](#)

[Table 3-5: Water Quality Objectives for Municipal Supply](#)

[Table 3-6: Water Quality Objectives for Agricultural Supply](#)

[Table 3-7: Water Quality Objectives for the Alameda Creek Watershed above Niles](#)

Water Quality Assessment Report
Mathilda Avenue Improvements at SR 237 and US 101 Project
City of Sunnyvale, California

04-SCL-237 PM 2.7/3.3
04-SCL-101 PM 45.2/45.8
EA 04-4H2900
Project ID: 0413000204

Appendix A.2 Water Quality Objectives for Municipal Supply and Agricultural Uses

Table 3-5: Water Quality Objectives for Municipal Supply

| <u>Parameter</u> | <u>Objective (in MG/L)</u> | <u>Parameter</u> | <u>Objective (in MG/L)</u> | <u>Parameter</u> | <u>Objective (in MG/L)</u> | | |
|--|-------------------------------------|--|--------------------------------|---|--|--|--|
| Physical: | | | | | | | |
| Color (units) ^a | 15.0 | Synthetic Organic Chemicals: | | | | | |
| Odor (number) ^a | 3.0 | Alachor ^h | 0.002 | Volatile Organic Chemicals (cont'd): | | | |
| Turbidity (NTU) ^a | 5.0 | Atrazine ^h | 0.001 | 1,1,2-Trichloro-1,2,2 trifluoromethane ^h | 1.2 | | |
| pH ^b | 6.0 - 8.5 | Bentazon ^h | 0.018 | Toluene ^h | 0.15 | | |
| TDS ^c | 500.0 | Benzo(a)pyrene ^h | 0.0002 | Vinyl Chloride ^h | 0.0005 | | |
| EC (mmhos/cm) ^c | 900 | Dalapon ^h | 0.2 | Xylenes (single or sum of isomers) ^h | 1.750 | | |
| Corrosivity | non-corrosive | Dinoseb ^h | 0.007 | Radioactivity: | | | |
| Inorganic Parameters: | | | | | | | |
| Aluminum ^d | 1.0 ^d / 0.2 ^a | Diquat ^h | 0.02 | Combined Radium-226 and Radium-228 ⁱ | 5 | | |
| Antimony ^d | 0.006 | Endothall ^h | 0.1 | Gross Alpha Particle Activity ^j | 15 | | |
| Arsenic ^d | 0.05 | Ethylene dibromide ^h | 0.0005 | Tritium ⁱ | 20,000 | | |
| Asbestos ^d | 7 MFL ^e | Glyphosate ^h | 0.7 | Strontium-90 ⁱ | 8 | | |
| Barium ^d | 1.0 | Heptachlor ^h | 0.00001 | Gross Beta Particle Activity ^j | 50 | | |
| Beryllium ^d | 0.004 | Heptachlor epoxide ^h | 0.00001 | Uranium ⁱ | 20 | | |
| Chloride ^c | 250.0 | Hexachloreyclopentadiene ^h | 0.001 | NOTES: | | | |
| Cadmium ^d | 0.005 | Molinate ^h | 0.02 | a. | Secondary Maximum Contaminant Levels as specified in Table 64449- A of Section 64449, Title 22 of the California Code of Regulations, as June 3, 2005. | | |
| Chromium ^d | 0.05 | Oxaryl ^h | 0.05 | b. | Table III-2, 1986 Basin Plan | | |
| Copper ^a | 1.0 | Pentachlorophenol ^h | 0.001 | c. | Secondary Maximum Contaminant Levels as specified in Table 64449-B of Section 64449, Title 22 of the California Code of Regulations, as of June 3, 2005. (Levels indicated are "recommended" levels. Table 64449-B contains a complete list of upper and short-term ranges.) | | |
| Cyanide ^d | 0.15 | Picloram ^h | 0.5 | d. | Maximum Contaminant Levels as specified in Table 64431-A (Inorganic Chemicals) of Section 64431, Title 22 of the California Code of Regulations, as of June 3, 2005. | | |
| Fluoride ^f | 0.6 - 1.7 ^g | Polychlorinated Biphenyls ^h | 0.0005 | e. | MFL = million fibers per liter; MCL for fibers exceeding 10 um in length. | | |
| Iron ^a | 0.3 | Simazine ^h | 0.004 | f. | Flouride objectives depend on temperature. | | |
| Lead ^b | 0.05 | Thiobencarb ^h | 0.07 / 0.001 | g. | A complete list of optimum and limiting concentrations is specified in Table 64433.2-A of Section 64433.2, Title 22 of the California Code of Regulations, as of June 3, 2005. | | |
| Manganese ^a | 0.05 | Volatile Organic Chemicals: | | | | | |
| Mercury ^d | 0.002 | Benzene ^h | 0.001 | h. | Maximum Contaminant Levels as specified in Table 64444-A (Organic Chemicals) of Section 64444, Title 22 of the California Code of Regulations, as of June 3, 2005. | | |
| Nickel ^d | 0.1 | Carbon Tetrachloride ^h | 0.005 | i. | Maximum Contaminant Levels as specified in Table 4 (Radioactivity) of Section 64443, Title 22 of the California Code of Regulations, as of June 3, 2005. | | |
| Nitrate (as NO ₃) ^d | 45.0 | 1,2-Dibromo-3-chloropropane ^h | 0.0002 | j. | Included Radium-226 but excludes Radon and Uranium. | | |
| Nitrate + Nitrite (as N) ^d | 10.0 | 1,2-Dichlorobenzene ^h | 0.6 | | | | |
| Nitrite (as N) ^d | 1.0 | 1,4-Dichlorobenzene ^h | 0.005 | | | | |
| Selenium ^d | 0.05 | 1,1-Dichloroethane ^h | 0.005 | | | | |
| Silver ^b | 0.1 | 1,2-Dichloroethane ^h | 0.0005 | | | | |
| Sulfate ^c | 250.0 | cis-1,2-Dichloroethylene ^h | 0.006 | | | | |
| Thallium ^d | 0.002 | trans-1,2-Dichloroethylene ^h | 0.01 | | | | |
| Zinc ^a | 5.0 | 1,1-Dichloroethylene ^h | 0.006 | | | | |
| Organic Parameters: | | | | | | | |
| MBAS (Foaming agents) ^a | 0.5 | Dichloromethane ^h | 0.005 | | | | |
| Oil and grease ^b | none | 1,2-Dichloropropane ^h | 0.005 | | | | |
| Phenols ^b | 0.001 | 1,3-Dichloropropane ^h | 0.0005 | | | | |
| Trihalomethanes ^b | 0.1 | Ethylbenzene ^h | 0.7 | | | | |
| Chlorinated Hydrocarbons: | | | | | | | |
| Endrin ^h | 0.002 | Methyl-tert-butyl ether ^h | 0.013 / 0.005 | | | | |
| Lindane ^h | 0.0002 | Monochlorobenzene ^h | 0.07 | | | | |
| Methoxychlor ^h | 0.03 | Styrene ^h | 0.1 | | | | |
| Toxaphene ^h | 0.003 | 1,1,2,2-Tetrachloroethane ^h | 0.001 | | | | |
| 2,3,7,8-TCDD (Dioxin) ^h | 3 x 10 ⁻⁸ | Tetrachloroethylene ^h | 0.005 | | | | |
| 2,4-D ^h | 0.07 | 1,2,4-Trichlorobenzene ^h | 0.005 | | | | |
| 2,4,4-TP Silvex ^h | 0.05 | 1,1,1-Trichloroethane ^h | 0.200 | | | | |
| | | 1,1,2-Trichloroethane ^h | 0.005 | | | | |
| | | Trichloroethylene ^h | 0.005 | | | | |
| | | Trichlorofluoromethane | 0.15 | | | | |

MG/L Milligrams per liter
pCi/L pico Curries per liter

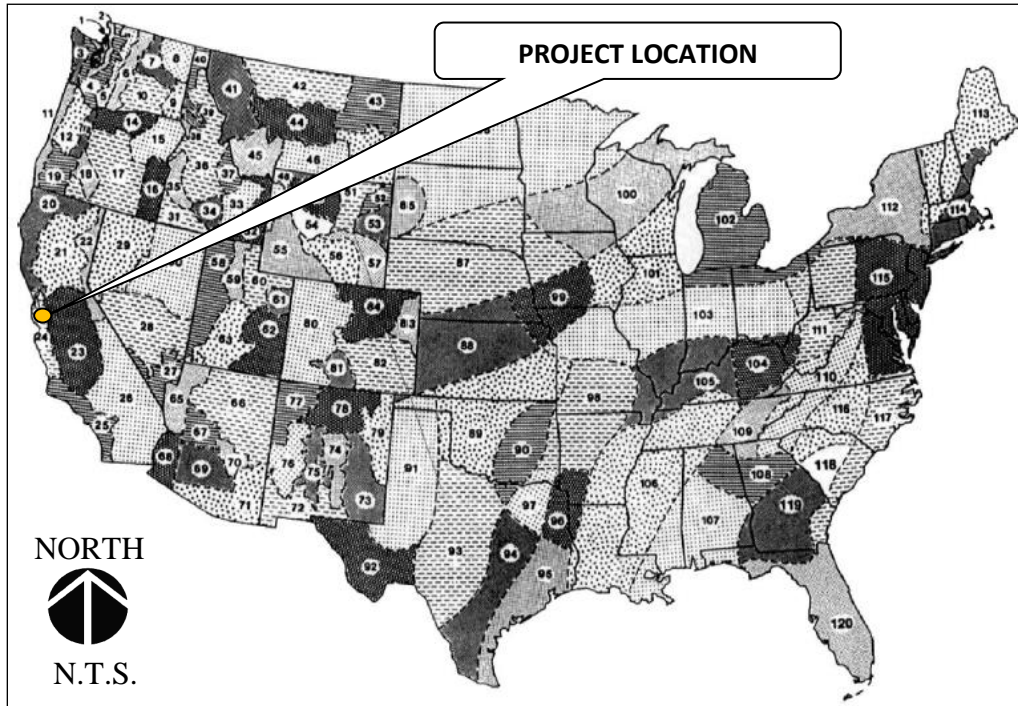
Table 3-6: Water Quality Objectives for Agricultural Supply^a (in mg/l)

| Parameter | Threshold | Limit | Limit for Livestock Watering |
|---|-----------|------------------|------------------------------|
| <i>Physical:</i> | | | |
| pH | 5.5-8.3 | 4.5-9.0 | |
| TDS | | | 10,000.0 |
| EC (mmhos / cm) | | 0.2-3.0 | |
| <i>Inorganic Parameters:</i> | | | |
| Aluminum | 5.0 | 20.0 | 5.0 |
| Arsenic | 0.1 | 2.0 | 0.2 |
| Beryllium | 0.1 | 0.5 | |
| Boron | 0.5 | 2.0 | 5.0 |
| Chloride | 142.0 | 355.0 | |
| Cadmium | 0.01 | 0.5 | 0.05 |
| Chromium | 0.1 | 1.0 | 1.0 |
| Cobalt | 0.05 | 5.0 | 1.0 |
| Copper | 0.2 | 5.0 | 0.5 |
| Flouride | 1.0 | 15.0 | 2.0 |
| Iron | 5.0 | 20.0 | |
| Lead | 5.0 | 10.0 | 0.1 |
| Lithium | | 2.5 ^b | |
| Manganese | 0.2 | 10.0 | |
| Molybdenum | 0.01 | 0.05 | 0.5 |
| Nickel | 0.2 | 2.0 | |
| NO ₃ + NO ₂ (as N) | 5.0 | 30 ^c | 100.0 |
| Selenium | | 0.02 | 0.05 |
| Sodium adsorption ratio (adjusted) ^d | 3.0 | 9.0 | |
| Vanadium | 0.1 | 1.0 | 0.1 |
| Zinc | 2.0 | 10.0 | 25 |

Appendix B Risk Level Determination Information

R Factor

Erosivity Index distribution zone = 24



Erosivity Index Zone Map

Source: EPA

N.T.

Table 1. Erosivity Index (%EI Values extracted from USDA Manual 703)

All values are at the end of the day listed below - Linear interpolation between dates is acceptable.
 EI as a percentage of Average Annual R Value Computed for Geographic Areas Shown in Figure 1

| Month | Jan 1 | Jan 16 | Jan 31 | Feb 15 | Mar 1 | Mar 16 | Mar 31 | Apr 15 | Apr 30 | May 15 | May 30 | Jun 14 | Jun 29 | Jul 14 | Jul 29 | Aug 13 | Aug 28 | Sept 12 | Sept 27 | Oct 12 | Oct 27 | Nov 11 | Nov 26 | Dec 11 | Dec 31 |
|-------|-------|--------|--------|--------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|---------|--------|--------|--------|--------|--------|--------|
| 1 | 0 | 4.3 | 8.3 | 12.8 | 17.3 | 21.6 | 25.1 | 28 | 30.9 | 34.9 | 39.1 | 42.6 | 45.4 | 48.2 | 50.8 | 53 | 56 | 60.8 | 66.8 | 71 | 75.7 | 82 | 89.1 | 95.2 | 100 |
| 2 | 0 | 4.3 | 8.3 | 12.8 | 17.3 | 21.6 | 25.1 | 28.0 | 30.9 | 34.9 | 39.1 | 42.6 | 45.4 | 48.2 | 50.8 | 53.0 | 56.0 | 60.8 | 66.8 | 71.0 | 75.7 | 82.0 | 89.1 | 95.2 | 100 |
| 3 | 0 | 7.4 | 13.8 | 20.9 | 26.5 | 31.8 | 35.3 | 38.5 | 40.2 | 41.6 | 42.5 | 43.6 | 44.5 | 45.1 | 45.7 | 46.4 | 47.7 | 49.4 | 52.8 | 57.0 | 64.5 | 73.1 | 83.3 | 92.3 | 100 |
| 4 | 0 | 3.9 | 7.9 | 12.6 | 17.4 | 21.6 | 25.2 | 28.7 | 31.9 | 35.1 | 38.2 | 42.0 | 44.9 | 46.7 | 48.2 | 50.1 | 53.1 | 56.6 | 62.2 | 67.9 | 75.2 | 83.5 | 90.5 | 96.0 | 100 |
| 5 | 0 | 2.3 | 3.6 | 4.7 | 6.0 | 7.7 | 10.7 | 13.9 | 17.8 | 21.2 | 24.5 | 28.1 | 31.1 | 33.1 | 35.3 | 38.2 | 43.2 | 48.7 | 57.3 | 67.8 | 77.9 | 86.0 | 91.3 | 96.9 | 100 |
| 6 | 0 | 0.0 | 0.0 | 0.5 | 2.0 | 4.1 | 8.1 | 12.6 | 17.6 | 21.6 | 25.5 | 29.6 | 34.5 | 40.0 | 45.7 | 50.7 | 55.6 | 60.2 | 66.5 | 75.5 | 85.6 | 95.9 | 99.5 | 99.9 | 100 |
| 7 | 0 | 0.0 | 0.0 | 0.0 | 0.0 | 1.2 | 4.9 | 8.5 | 13.9 | 19.0 | 26.0 | 35.4 | 43.9 | 48.8 | 53.9 | 64.5 | 73.4 | 77.5 | 80.4 | 84.8 | 89.9 | 96.6 | 99.2 | 99.7 | 100 |
| 8 | 0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.9 | 3.6 | 7.8 | 15.0 | 20.2 | 27.4 | 38.1 | 49.8 | 57.9 | 65.0 | 75.6 | 82.7 | 86.8 | 89.4 | 93.4 | 96.3 | 99.1 | 100.0 | 100.0 | 100 |
| 9 | 0 | 0.8 | 3.1 | 4.7 | 7.4 | 11.7 | 17.8 | 22.5 | 27.0 | 31.4 | 36.0 | 41.6 | 46.4 | 50.1 | 53.4 | 57.4 | 61.7 | 64.9 | 69.7 | 79.0 | 89.6 | 97.4 | 100.0 | 100.0 | 100 |
| 10 | 0 | 0.3 | 0.5 | 0.9 | 2.0 | 4.3 | 9.2 | 13.1 | 18.0 | 22.7 | 29.2 | 39.5 | 46.3 | 48.8 | 51.1 | 57.2 | 64.4 | 67.7 | 71.1 | 77.2 | 85.1 | 92.5 | 96.5 | 99.0 | 100 |
| 11 | 0 | 5.4 | 11.3 | 18.8 | 26.3 | 33.2 | 37.4 | 40.7 | 42.5 | 44.3 | 45.4 | 46.5 | 47.1 | 47.4 | 47.8 | 48.3 | 49.4 | 50.7 | 53.6 | 57.5 | 65.5 | 76.2 | 87.4 | 94.8 | 100 |
| 12 | 0 | 3.5 | 7.8 | 14.0 | 21.1 | 27.4 | 31.5 | 35.0 | 37.3 | 39.8 | 41.9 | 44.3 | 45.6 | 46.3 | 46.8 | 47.9 | 50.0 | 52.9 | 57.9 | 62.3 | 69.3 | 81.3 | 91.5 | 96.7 | 100 |
| 13 | 0 | 0.0 | 0.0 | 1.8 | 7.2 | 11.9 | 16.7 | 19.7 | 24.0 | 31.2 | 42.4 | 55.0 | 60.0 | 60.8 | 61.2 | 62.6 | 65.3 | 67.6 | 71.6 | 76.1 | 83.1 | 93.3 | 98.2 | 99.6 | 100 |
| 14 | 0 | 0.7 | 1.8 | 3.3 | 6.9 | 16.5 | 26.6 | 29.9 | 32.0 | 35.4 | 40.2 | 45.1 | 51.9 | 61.1 | 67.5 | 70.7 | 72.8 | 75.4 | 78.6 | 81.9 | 86.4 | 93.6 | 97.7 | 99.3 | 100 |
| 15 | 0 | 0.0 | 0.0 | 0.5 | 2.0 | 4.4 | 8.7 | 12.0 | 16.6 | 21.4 | 29.7 | 44.5 | 56.0 | 60.8 | 63.9 | 69.1 | 74.5 | 79.1 | 83.1 | 87.0 | 90.9 | 96.6 | 99.1 | 99.8 | 100 |
| 16 | 0 | 0.0 | 0.0 | 0.5 | 2.0 | 5.5 | 12.3 | 16.2 | 20.9 | 26.4 | 35.2 | 48.1 | 58.1 | 63.1 | 66.5 | 71.9 | 77.0 | 81.6 | 85.1 | 88.4 | 91.5 | 96.3 | 98.7 | 99.6 | 100 |
| 17 | 0 | 0.0 | 0.0 | 0.7 | 2.8 | 6.1 | 10.7 | 12.9 | 16.1 | 21.9 | 32.8 | 45.9 | 55.5 | 60.3 | 64.0 | 71.2 | 77.2 | 80.3 | 83.1 | 87.7 | 92.6 | 97.2 | 99.1 | 99.8 | 100 |
| 18 | 0 | 0.0 | 0.0 | 0.6 | 2.5 | 6.2 | 12.4 | 16.4 | 20.2 | 23.9 | 29.3 | 37.7 | 45.6 | 49.8 | 53.3 | 58.4 | 64.3 | 69.0 | 75.0 | 86.6 | 93.9 | 96.6 | 98.0 | 100.0 | 100 |
| 19 | 0 | 1.0 | 2.6 | 7.4 | 16.4 | 23.5 | 28.0 | 31.0 | 33.5 | 37.0 | 41.7 | 48.1 | 51.1 | 52.0 | 52.5 | 53.6 | 55.7 | 57.6 | 61.1 | 65.8 | 74.7 | 88.0 | 95.8 | 98.7 | 100 |
| 20 | 0 | 9.8 | 18.5 | 25.4 | 30.2 | 35.6 | 38.9 | 41.5 | 42.9 | 44.0 | 45.2 | 48.2 | 50.8 | 51.7 | 52.5 | 54.6 | 57.4 | 58.5 | 60.1 | 63.2 | 69.6 | 76.7 | 85.4 | 92.4 | 100 |
| 21 | 0 | 7.5 | 13.6 | 18.1 | 21.1 | 24.4 | 27.0 | 29.4 | 31.7 | 34.6 | 37.3 | 39.6 | 41.6 | 43.4 | 45.4 | 48.1 | 51.3 | 53.3 | 56.6 | 62.4 | 72.4 | 81.3 | 88.9 | 94.7 | 100 |
| 22 | 0 | 1.2 | 1.6 | 1.6 | 1.6 | 1.6 | 1.6 | 2.2 | 3.9 | 4.6 | 6.4 | 14.2 | 32.8 | 47.2 | 58.8 | 69.1 | 76.0 | 82.0 | 87.1 | 96.7 | 99.9 | 99.9 | 99.9 | 99.9 | 100 |
| 23 | 0 | 7.9 | 15.0 | 20.9 | 25.7 | 31.1 | 35.7 | 40.2 | 43.2 | 46.2 | 47.7 | 48.8 | 49.4 | 49.9 | 50.7 | 51.8 | 54.1 | 57.7 | 62.8 | 65.9 | 70.1 | 77.3 | 86.8 | 93.5 | 100 |
| 24 | 0 | 12.2 | 23.6 | 33.0 | 39.7 | 47.1 | 51.7 | 55.9 | 57.7 | 58.6 | 58.9 | 59.1 | 59.1 | 59.2 | 59.2 | 59.3 | 59.5 | 60.0 | 61.4 | 63.0 | 66.5 | 71.8 | 81.3 | 89.6 | 100 |
| 25 | 0 | 9.8 | 20.8 | 30.2 | 37.6 | 45.8 | 50.6 | 54.4 | 56.0 | 56.8 | 57.1 | 57.1 | 57.2 | 57.6 | 58.5 | 59.8 | 62.2 | 65.3 | 67.5 | 68.2 | 69.4 | 74.8 | 86.6 | 93.0 | 100 |

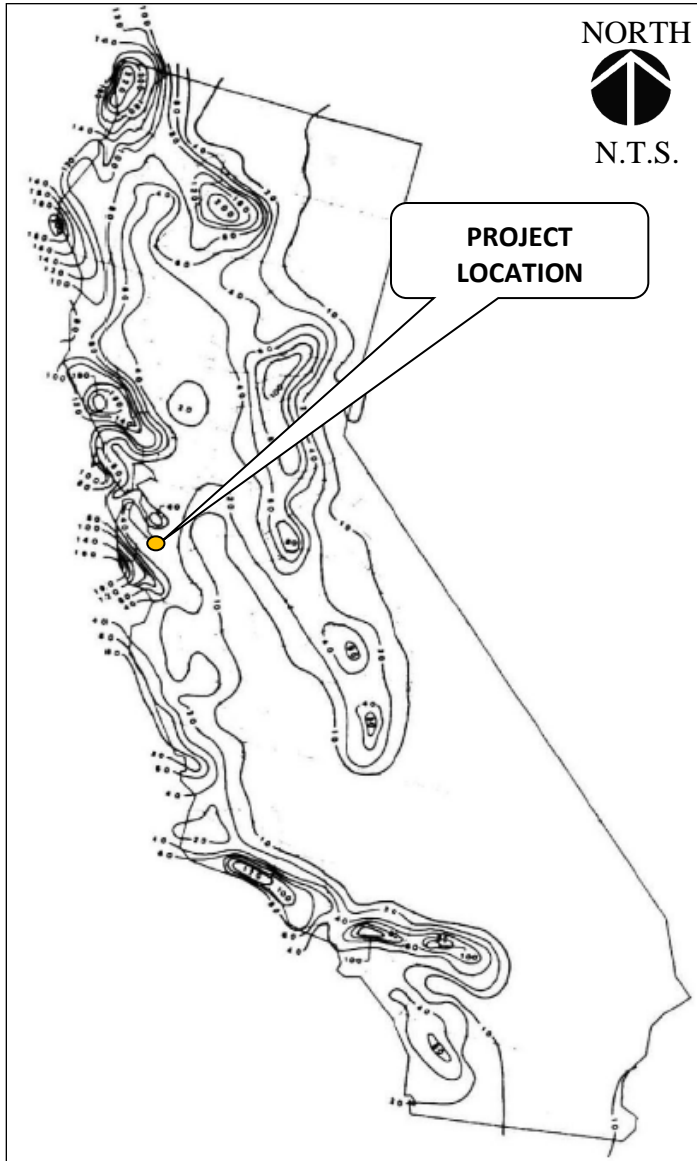
Source: EPA

Project duration: May 5, 2018 to May 3, 2019

EI percentage from May 1 to December 31: $100\% - 39.7\% = 60.3\%$

EI percentage from January 1 to May 1: $39.7\% - 0\% = 39.7\%$

Total EI percentage for 1 year duration: $60.3\% + 39.7\% = 100\%$



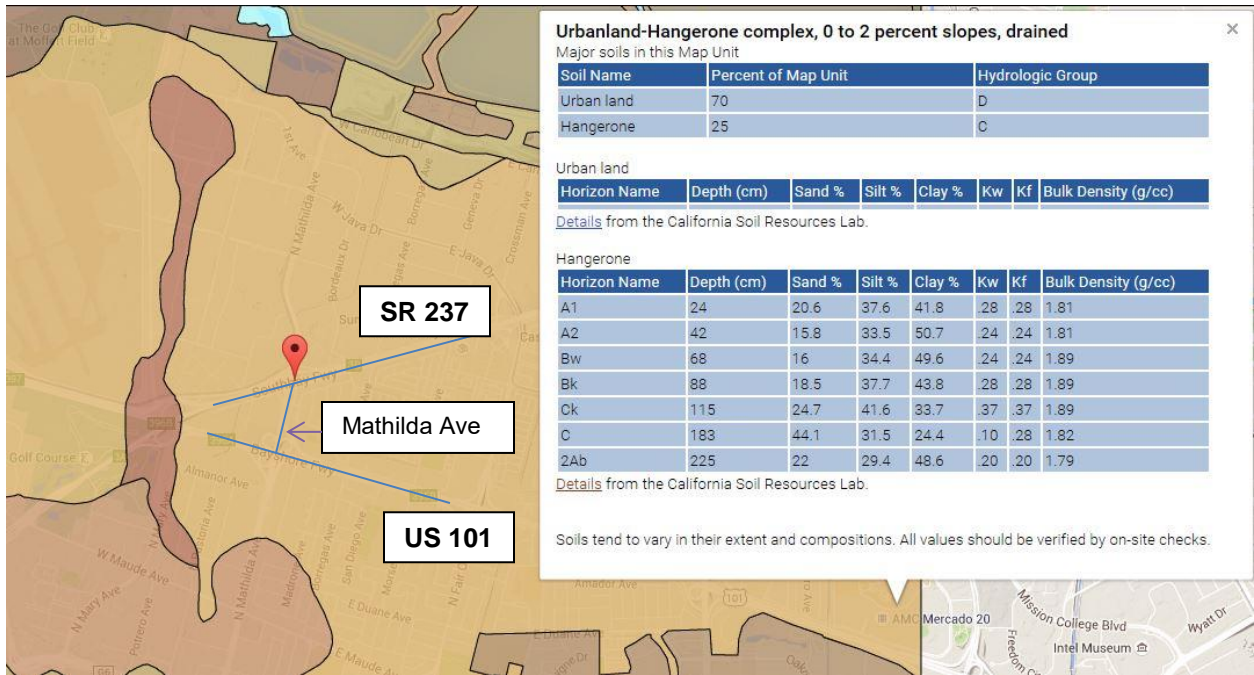
Isoerodent Map of California

Source: EPA

Annual Isoerodent = 35

R Factor for 1 year construction: $35 \times 100\% = 35$

R Factor = 35



K Factor

Source: Caltrans Water Quality Planning Tool



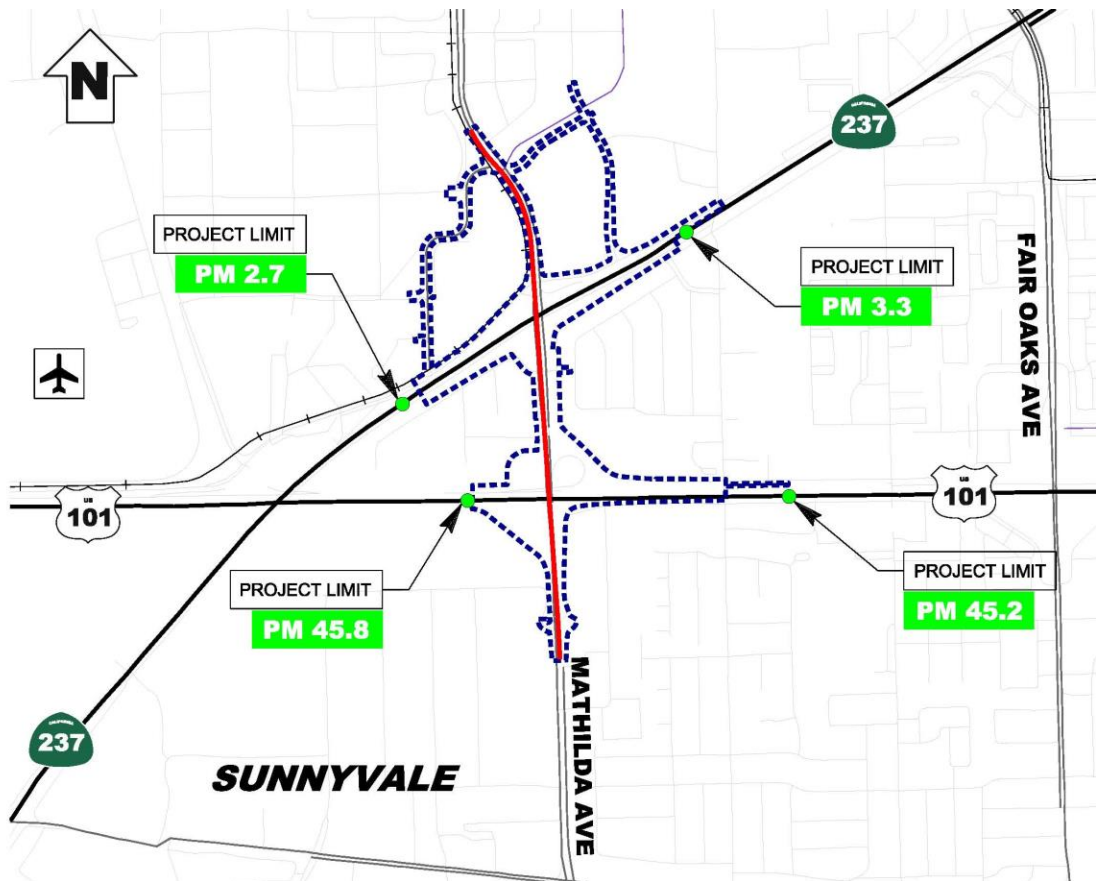
LS Factor

Source: Caltrans Water Quality Planning Tool

WETLANDS ASSESSMENT

for the

MATHILDA AVENUE IMPROVEMENTS AT SR 237 AND US 101 PROJECT



Prepared for:

Santa Clara Valley Transportation Authority
California Department of Transportation
District 4

Prepared by:

ICF, International

Dated: December 2015

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WETLANDS ASSESSMENT

for the

MATHILDA AVENUE IMPROVEMENTS AT SR 237 AND US 101 PROJECT

on Mathilda Avenue from Almanor Avenue to Innovation Way; on SR 237 from 0.3 mile south of US 101/SR 237 Junction to 0.3 mile east of Mathilda Avenue Undercrossing; and on US 101 from 0.5 mile south of Mathilda Avenue to SR 237/US 101/SR 237 Junction in City of Sunnyvale, in Santa Clara County

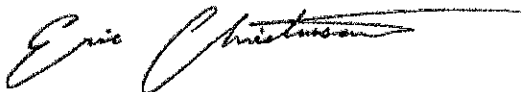
SCL-237-PM 2.7/3.3; SCL-101-PM 45.2/45.8
EA 04-4H2900/Project ID 0413000204

December 2015

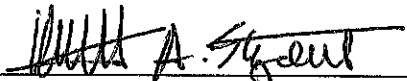
U.S. DEPARTMENT OF TRANSPORTATION
STATE OF CALIFORNIA

and

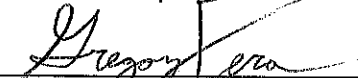
Cooperating Agency: Santa Clara Valley Transportation Authority

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Statement of Compliance: Produced in compliance with California Environmental Quality Act (CEQA) requirements, as appropriate, to meet the level of analysis and documentation that has been determined necessary for this project.

Mathilda Avenue Improvements at SR 237 and US 101

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Project Introduction and Purpose

The California Department of Transportation (Caltrans), in cooperation with the Santa Clara Valley Transportation Authority (VTA) and the City of Sunnyvale, is proposing the “Mathilda Avenue Improvements at SR 237 and US 101 Project” (Project) to improve Mathilda Avenue in the City of Sunnyvale from Almanor Avenue to Innovation Way, including on- and off-ramp improvements at SR 237/Mathilda Avenue and US 101/Mathilda Avenue interchanges. The primary purpose of the Project is to improve traffic operations on Mathilda Avenue through the US 101 and SR 237 interchanges. Figure 1 (Attachment A) shows the location of the Project. ICF International (ICF) conducted a delineation of waters of the United States within the Biological Study Area (BSA) of the Project in March and July 2015.

Site Description

The Project site is located within the City of Sunnyvale in Santa Clara County, California (Figure 1, Attachment A). It occurs in the Mountain View U.S. Geological Survey (USGS) 7.5-minute quadrangle. The BSA for the Project is based on the Project’s limits (Figure 2, Attachment A). On SR 237, the Project limits are from 0.3-mile east of the US 101/SR 237 interchange (post mile [PM] 2.7) to 0.3-mile east of the Mathilda Avenue undercrossing (PM 3.3). On US 101, the Project limits are from 0.3-mile south of Mathilda Avenue overcrossing (PM 45.4) to 0.3-mile south of SR 237/US 101 interchange (PM 45.8). The total length of the Project on Mathilda Avenue is approximately one mile. The BSA includes a proposed road that would connect Mathilda Avenue to Bordeaux Drive; however, this road would be completed by the Moffett Place Project separate from the Mathilda Avenue Improvements at SR 237 and US 101 Project. The Mathilda Avenue Improvements at SR 237 and US 101 Project proposes to construct traffic signals and paint bicycle lanes on the road after it is constructed by the Moffett Place Project.

Elevations in the BSA range from approximately 15 feet in low-lying areas to 40 feet on raised highway ramps (Google Earth Pro 2015). Topography within the BSA is relatively flat with a gentle slope downwards from US 101 to SR 237. The BSA has an estimated mean annual temperature of 59 degrees Fahrenheit and an estimated mean annual precipitation of 15.71 inches (U.S. Department of Agriculture, Natural Resources Conservation Service 2015).

Vegetation

Land cover types within the BSA include developed areas (existing roadways, parking lots, etc.), ornamental landscaping, and ruderal ground cover. Typical ornamental landscaping species include purple lantana (*Lantana montevidensis*), pepper tree (*Schinus molle*), flowering cherry (*Prunus serrulata*), deodar cedar (*Cedrus deodara*), silver-dollar gum (*Eucalyptus polyanthemus*), southern magnolia (*Magnolia grandiflora*), white Lady Banks rose (*Rosa banksiae*), and olive (*Olea europaea*), to name a few. The ruderal ground cover consists predominantly of wild oat (*Avena* sp.), ripgut grass (*Bromus diandrus*), summer mustard (*Hirschfeldia incana*), Italian thistle (*Carduus pycnocephalus* subsp. *pycnocephalus*), bristly ox-tongue (*Helminthotheca echioides*), smilo grass (*Stipa miliaceae* var. *miliaceae*), and prickly lettuce (*Lactuca serriola*).

Soil

Soil at the Project site is composed of Urbanland-Hangerone complex with 0 to 2 percent slopes, drained (Figure 3, Attachment A). The Urbanland-Hangerone complex is listed as hydric by the U.S.

Department of Agriculture, Natural Resources Conservation Service (USDA NRCS 2014). The major soil types in this map unit are urban land (70%) and Hangerone (25%) with inclusions of Bayshore (2%), Clear Lake (2%), and Embarcadero (1%). The map unit aggregated data indicate that the soils typically occur on basin floors and are poorly drained (Natural Resources Conservation Service 2013).

Hydrology

Stormwater drainage ditches and the Sunnyvale West Channel occur within the BSA (Figure 4, Attachment A). The ditches drain stormwater runoff during rain events but flow does not persist after rain events. The Sunnyvale West Channel provides flood control protection and water flows through the channel to the San Francisco Bay via Guadalupe Slough (Figure 5, Attachment A). The Sunnyvale West Channel was constructed in the 1960s in response to flooding caused by a combination of major storm events, land subsidence, and inadequate drainage to the San Francisco Bay (Santa Clara Valley Water District 2015).

Methods

Prior to conducting fieldwork, ICF reviewed U.S. Fish and Wildlife Service's Wetlands Mapper (USFWS) (U.S. Fish and Wildlife Service 2015) and Google Earth aerial imagery (Google Earth Pro 2015) to identify areas with the potential to support waters of the United States, based on apparent signatures of hydrology, topography, and/or vegetation composition.

ICF wetland specialists conducted the delineation fieldwork on March 6 and July 29, 2015 within the BSA. Both site visits occurred on days with no precipitation. The delineation was conducted using the routine onsite determination method described in the *1987 U.S. Army Corps of Engineers Wetlands Delineation Manual* (Environmental Laboratory 1987) and the supplemental procedures and wetland indicators provided in the *Regional Supplement to the Corps of Engineers Wetland Delineation Manual: Arid West Region* (U.S. Army Corps of Engineers 2008a). Delineation data were collected to support a preliminary jurisdictional determination from U.S. Army Corps of Engineers (USACE).

Wetland boundaries were determined by establishing representative sampling points to evaluate the presence of positive indicators of hydrophytic vegetation, hydric soil, and wetland hydrology. The boundaries of nonwetland waters (other waters) in the BSA were identified by locating the ordinary high water mark (OHWM), which represents the lateral limit of USACE jurisdiction over non-tidal, non-wetland waters in the absence of adjacent wetlands (33 Code of Federal Regulations [CFR] 328.4[c]). The OHWM of intermittent streams was identified using the field indicators provided in 33 CFR 328.3(e) and 329.11(a)(1) and *A Field Guide to the Identification of the Ordinary High Water Mark in the Arid West Region of the Western United States* (U.S. Army Corps of Engineers 2008b). Historic and current Section 10 waters do not occur within the BSA and, therefore, were not evaluated during the delineation.

The base map used during fieldwork consisted of the BSA overlaid on 2012 aerial imagery obtained from Microsoft Bing Maps at a scale of 1"= 50'. The delineators used a resource-grade GPS (global positioning system) unit with sub-meter accuracy, supplemented with aerial photograph interpretation, to map sampling points, the boundaries of wetlands and other waters, and the

locations of representative photos in the BSA. All GPS data collected in the field were downloaded and differentially corrected using the nearest available base-station data to produce the delineation maps.

Results

The Sunnyvale West Channel occurs within the northwestern area of the BSA (Figure 4, Attachment A). The Sunnyvale West Channel is assumed to be subject to USACE jurisdiction under Section 404 of the Clean Water Act (CWA) and thus was identified by ICF as a water of the United States.

No other potential waters of the United States, including Section 404 wetlands and nonwetland waters or Section 10 waters, were observed within the BSA. Nonjurisdictional stormwater drainage ditches were noted along the eastern boundary of Mathilda Avenue and within the traffic circles (Photos 1-3, Attachment B).

Vegetation

Hydrophytic vegetation indicators (1-Dominance Test, 2-Prevalence Test, or 3-Morphological Adaptations) described in *Regional Supplement to the Corps of Engineers Wetland Delineation Manual: Arid West Region* (U.S. Army Corps of Engineers 2008a) were not observed within the BSA.

Soil

Hydric soil indicators described in the *Regional Supplement* (U.S. Army Corps of Engineers 2008a) were not observed within the BSA.

Hydrology

Indicators of wetland hydrology described in the *Regional Supplement* (U.S. Army Corps of Engineers 2008a) were not observed within the BSA.

Discussion

The Sunnyvale West Channel is a concrete-lined, culverted channel that is assumed to be a jurisdictional feature due to its direct hydrologic connection to the San Francisco Bay (Figure 5, Attachment A).

The ditches observed within the BSA do not meet the technical criteria to qualify as waters of the United States based on the Clean Water Rule: Definition of "Waters of the United States"; Final Rule (USACE 2015, US EPA 2015). The ditches are excavated in dry land, and do not drain wetlands or relocate tributaries. The ditches drain stormwater runoff during rain events, but flow does not persist after rain events. Where there is vegetation associated with the ditches, instead of bare ground or gravel/cobble, the vegetation consists of ruderal or weedy species including wild oat, Italian thistle, and riggut grass (Photos 1-3, Attachment B).

Conclusions

The Sunnyvale West Channel is assumed to be subject to USACE jurisdiction under CWA Section 404. Other waters of the United States are not present in the BSA or Project site. A portion of the Sunnyvale West Channel occurs within the BSA (specifically at the proposed road connecting Mathilda Avenue and Bordeaux Drive); however, as mentioned above, this proposed connection would be constructed by the Moffett Place Project, not the Mathilda Avenue Improvements at SR 237 and US 101 Project. Because the Mathilda Avenue Improvements at SR 237 and US 101 Project will not affect the Sunnyvale West Channel, a Section 404 permit from the USACE should not be required to authorize Project construction.

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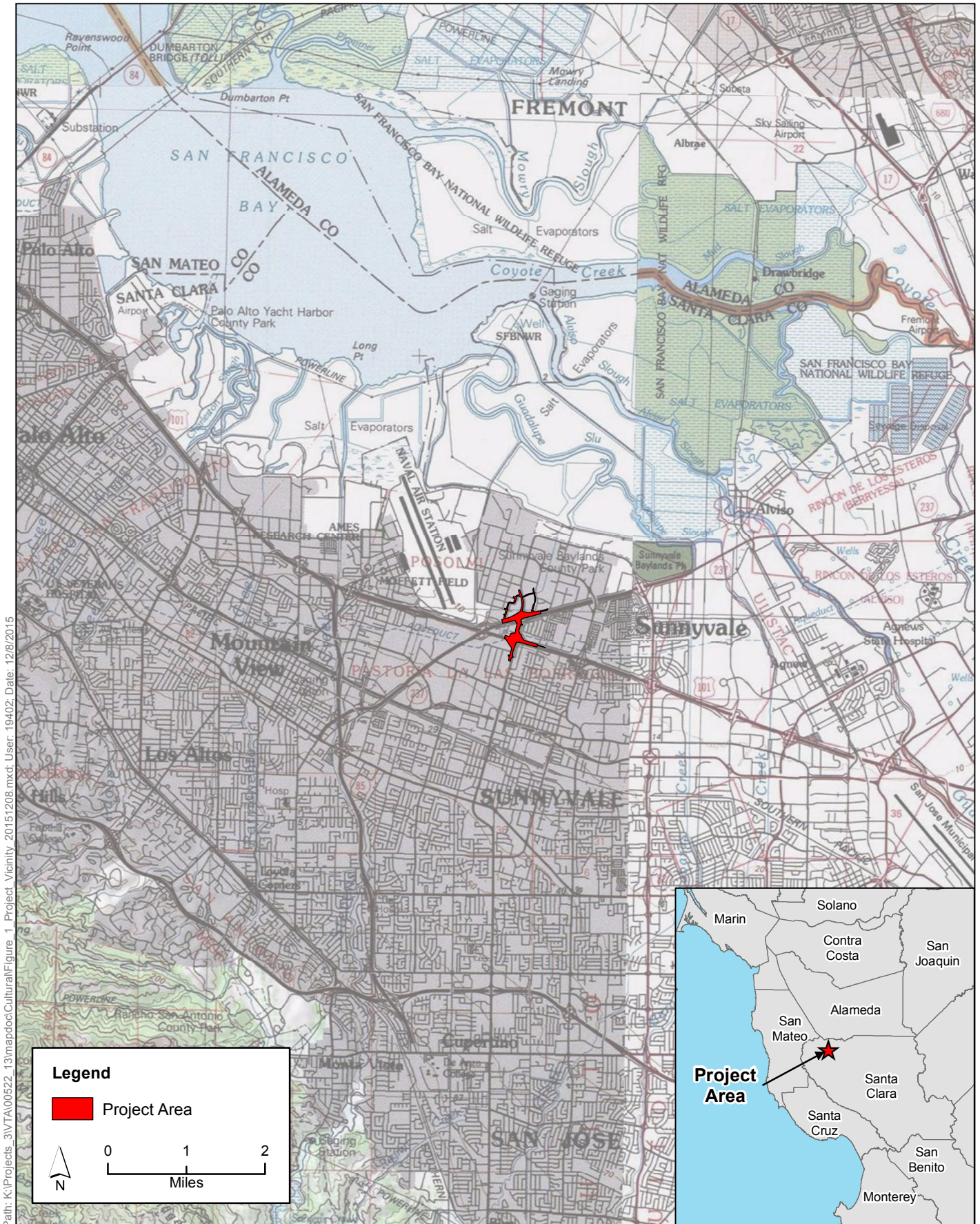
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Attachment A
Figures



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Figure 1
Project Vicinity
Mathilda Avenue Improvements at SR 237 and US 101



Figure 2
Biological Study Area
Mathilda Avenue Improvements at SR 237 and US 101 Project

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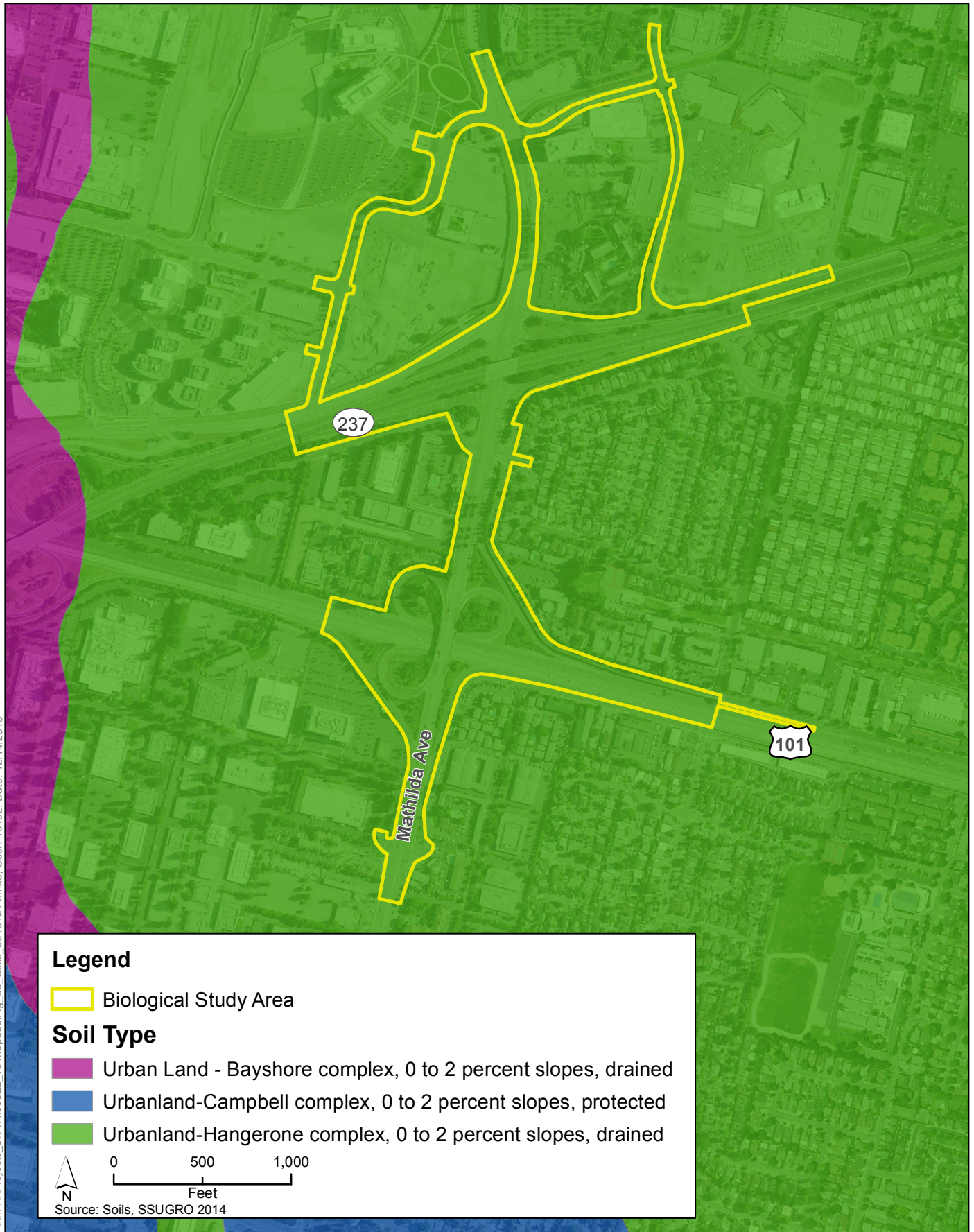
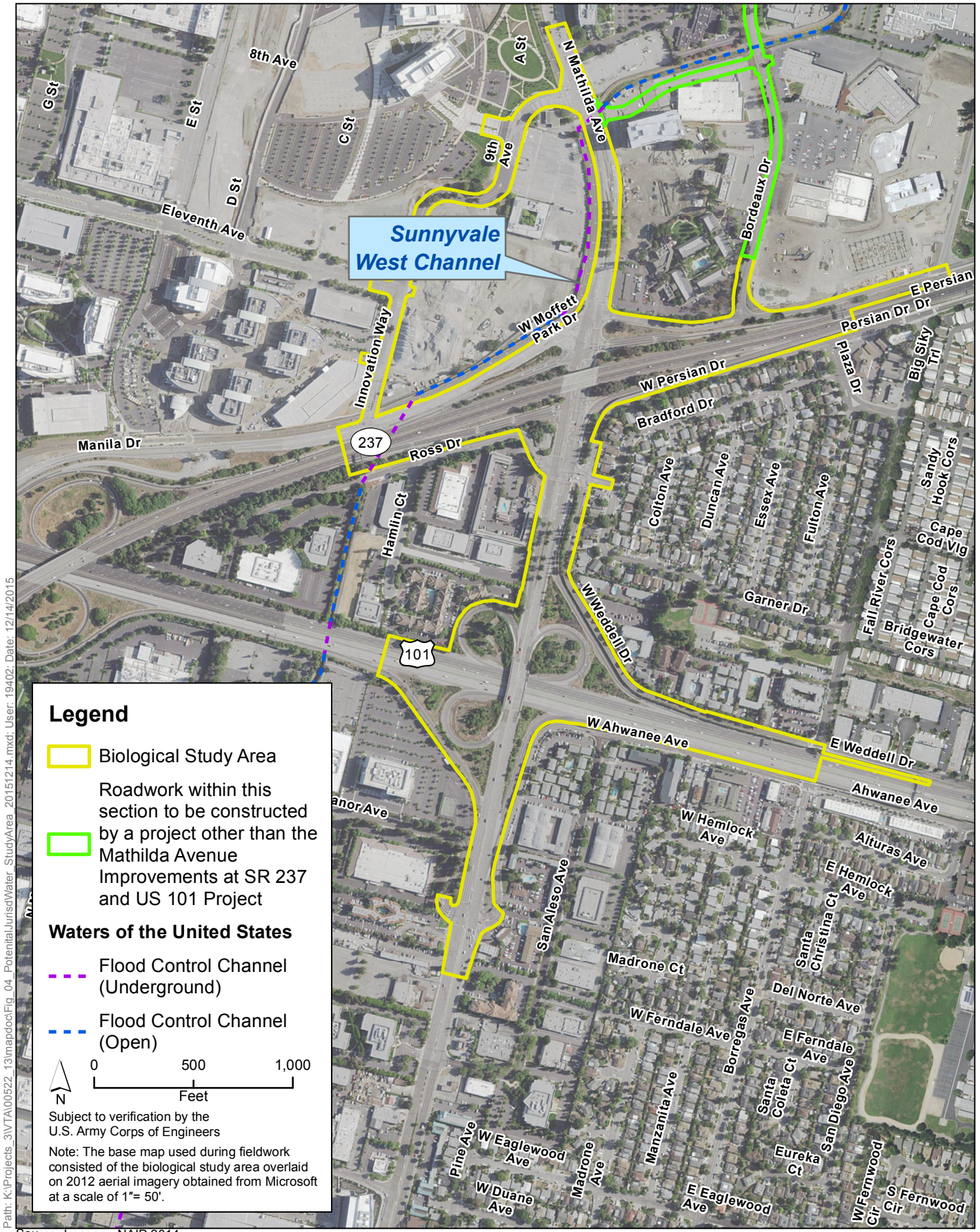


Figure 3
Soils
Mathilda Avenue Improvements at SR 237 and US 101 Project



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Source: Imagery; NAIP 2014

Figure 4
Waters of the United States within the Biological Study Area
 Mathilda Avenue Improvements at SR 237 and US 101 Project

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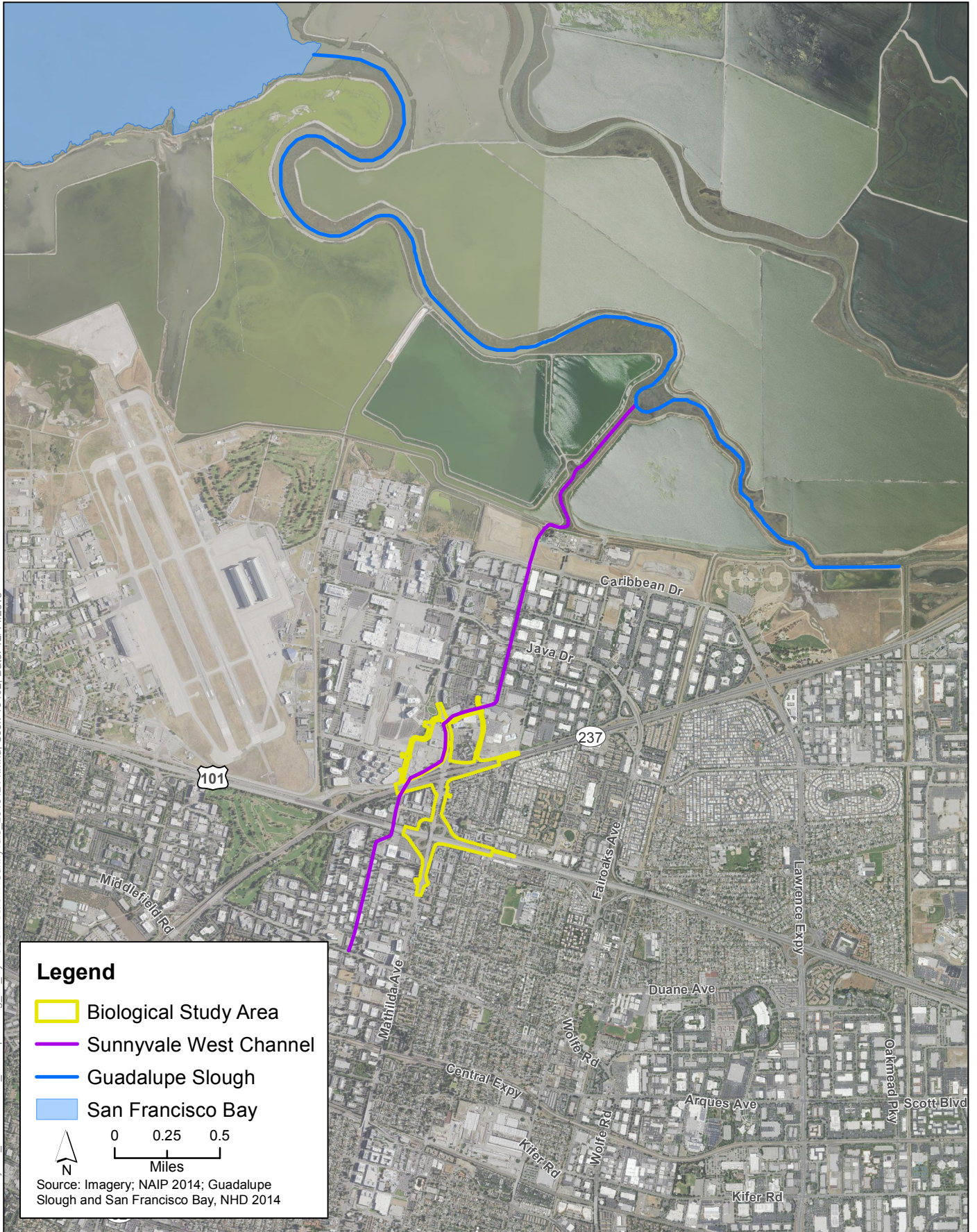


Figure 5
Hydrological Connection of Sunnyvale West Channel and the San Francisco Bay
Mathilda Avenue Improvements at SR 237 and US 101 Project

Attachment B
Photographs



Photo 1. Drainage parallel to Mathilda Avenue, facing south.



Photo 2. Drainage within the area immediately north of the Mathilda Avenue northbound to US 101 northbound interchange loop ramp, facing north.



Photo 3. Drainage within US 101 northbound to Mathilda Avenue southbound interchange loop ramp, facing southeast.